M.O. 279

Air Ministry

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METEOROLOGICAL OFFICE

OBSERVATORIES' YEAR BOOK 1923

Comprising the results obtained from autographic records and eye observations at the observatories at Lerwick, Aberdeen, Eskdalemuir, Cahirciveen (Valencia Observatory), Richmond (Kew Observatory), and Benson.

Published by the authority of the METEOROLOGICAL COMMITTEE



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PREFACE.

Up to the end of 1921, the serial statistical publications of the Meteorological Office were grouped together as though they were parts of one comprehensive book. This book, which was entitled "The British Meteorological and Magnetic Year Book," consisted of:—

Part I					The Weekly Weather Report.
Part II					The Monthly Weather Report.
Part III,	Section	ı I	• •	• •	Daily Readings at Meteorological stations of the First and Second Orders.
	Section	ı II	• •	• •	Geophysical Journal, Daily Values of Meteorological and Geophysical Ele- ments.
Part IV,	Section	n I	••		Hourly Values from Autographic Records. Meteorological Section.
	Section	n II	• •	• •	Hourly Values from Autographic Records. Geophysical Section.
Part V					Réseau Mondial.

The data for the year 1922 and subsequent years will be found in the following publications, each of which will be issued either as a complete and independent volume or in parts which may be bound into annual volumes:—

New Publication from 1922.	Corresponding parts of the British Meteor- ological and Magnetic Year Book until the end of 1921.
The Weekly Weather Report	Part I.
The Monthly Weather Report	Part II.
The Observatories' Year Book	{Part III, Section II. Part IV, Section I.* Part IV, Section II.
The Réseau Mondial	Part V.

It will be noticed that Part III, Section I, of the old publication is not included in the new issues. This part contained "Daily Readings at Meteorological Stations of the First and Second Orders," and it has been decided that as the new Observatories' Year Book will contain daily values of the meteorological elements for the principal first order stations and the Daily Weather Report contains daily values for 39 other stations, it is not necessary to revive the issue of this section which ceased with the data for 1921.

The present volume is the second of the Observatories' Year Book. It contains data from Lerwick, Aberdeen, Eskdalemuir, Valencia and Kew, and in addition a section dealing with upper air observations made from Benson with registering balloons. Data from the new geophysical observatory, which was established at Lerwick in the Shetland Islands during 1921, are included in this publication for the first time.

For assistance in the preparation of this volume, thanks are due to Dr. C. Chree, F.R.S., who, since his retirement from the Meteorological Office in April 1925, has contributed the discussion on the magnetic results obtained at Lerwick (p. 24), and has also compiled Tables 492 and 493, containing annual values of magnetic elements at various observatories.

^{*} Part IV, Section I—Hourly Values from Autographic Records, Meteorological Section, was discontinued after the data for 1913 had been published, and it is not proposed to continue it to the end of 1921 as is the case with the other sections.

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			ERR	ATA TO VOLUME FOR 1922.	
		e 15. Inte	ensity of Gra	vity. For grams per second per second read centimetres	s per second
p. 100	0. 7	Γable 103.		For 975·5 at 11h. read 075·5. For 975·4 at Noon read 075·4.	
p. 27 4			March 13th. April 24th.	For 027·3 at 13h. read 207·3. For i05·7 at 24h. read 005·7.	
p. 278	5. 7	Γable 372.	June 13th.	For 061.0 at 16h. read 016.0.	4.
p. 3 09	9. 7	Γable 441.	In date colu	nn. For 11 and 12 (where repeated) read 14 and 15.	³ G
(198	889)	LE	RWICK	DECLINATION	В

LIST OF OBSERVATORIES.

	Latitude.	Longitude.	G.M.T. of Local Mean Noon.	Height above M.S.L. in metres.
	0 /	0 /	h m	
Lerwick	60 8 N.	I II W.	12 5	81.7
Aberdeen	57 10 N.	2 6 W.	12 8	14.0
Eskdalemuir, Dumfries-shire	55 19 N.	3 12 W.	12 13	242.0
Valencia Observatory, Cahirciveen, Co. Kerry.	51 56 N.	10 15 W.	12 41	9·1
Kew Observatory, Richmond, Surrey	51 28 N.	o 19 W.	12 I	5.2
Benson, Oxfordshire	51 37 N.	1 7 W.	12 4	57

- Notes.—(1) The height given is that of the site of the rain-gauge. The heights of other meteorological instruments are shown under the appropriate Tables.
 - (2) Values printed within brackets, (), in the following tables are obtained by interpolation.
 - (3) Daily Mean Values are computed as 1/24 { $\frac{1}{2}$ (0 + 24) + 1 + 2 + + 23} where 0, 1, 2 24 denote the tabulated values of the element for each of the hours of the day, 0 being the initial, and 24 the final midnight.
 - (4) The standard of time used throughout is Greenwich Mean Civil Time, except in the case of the element sunshine, for which Local Apparent Time is used.
 - (5) Maximum and Minimum Values are printed in heavy type.
 - (6) Monthly and annual normals of pressure, dry bulb temperature, relative humidity, wind speed and rainfall for each hour of the day and for the period of 45 years 1871–1915 are published for the observatories Aberdeen, Cahirciveen, Richmond and Falmouth in Hourly Values from Autographic Records, 1917 (Part IV of the British Meteorological and Magnetic Year Book, 1917), and in previous volumes of that series. Corresponding normals of sunshine are also published there for the same observatories and for the period of 35 years 1881–1915.

For Eskdalemuir the same publications gives hourly averages for the months and for the year referred to the period 1911-1915.

GENERAL INTRODUCTION TO THE METEOROLOGICAL TABLES.

The elements dealt with in the following meteorological tables for the Observatories at Aberdeen, Eskdalemuir, Cahirciveen and Richmond are:—barometric pressure, air temperature, humidity, rainfall, sunshine, wind speed and direction, minimum night temperature on the grass, cloud and weather, and in some cases temperature in the ground, solar radiation and level of underground water.

The positions of the Observatories and the heights of the sites are given on p. 10.

Notes on the Instruments and Tabulation of the Records.

A detailed description of the barograph, thermograph, cup anemometer and Beckley raingauge used for obtaining the records of pressure, temperature, humidity, wind speed and direction,* and rainfall is given in the *Reports* of the Meteorological Office for the years 1867 and 1869; for a description of other instruments in use reference may be made to the *Observer's Handbook* and to the article on Meteorological Instruments in the *Dictionary of Applied Physics*, Vol. III. The following notes are supplementary and are given partly for reference and partly as containing information necessary for the interpretation of the tables.

Barometer.—The record of barometric pressure is obtained photographically from a mercurial barometer.

A beam of light is passed through the space between the surface of the column of mercury and the top of the tube, and, after passing through a diaphragm which reduces the width of the beam of light to a very narrow sharp line, is focussed upon a sheet of sensitised paper (ordinary "bromide" paper is employed) carried upon a cylinder which is rotated by clockwork and makes one revolution about its vertical axis in rather more than 48 hours.

The barogram is therefore a continuous photograph of this narrow vertical line, and appears as a horizontal ribbon, the depth of which is constantly varying with

the rise or fall of the mercury in the tube of the barometer.

The expansion of a zinc rod is utilised to compensate for the effect of temperature upon the height of the barometric column; the arrangement produces mechanically a lengthening of the beam of light at its upper end as it becomes shortened at its lower extremity by the expansion of the mercury in the tube. A time-scale is recorded upon the barogram by means of a shutter actuated by the clock. This shutter cuts off the light for the space of four minutes every two hours, thus producing interruptions which appear as narrow white spaces on the record corresponding with known points of time. Until 1918 these time-breaks occurred at the even hours, 2h, 4h, 6h, etc., but it was found that when the edge of the record was not critically sharp owing to various causes, a systematic error was introduced when measuring the records, whereby the values at the even hours were slightly in excess of those at the odd hours where no time-break existed. From 1918 onwards the clock was so arranged that the time-breaks should occur half an hour before the even hours; by this means both even and odd hour-values are measured at points on the trace which are unaffected by any systematic difference.

Control readings of a standard barometer are taken three times a day by different observers so that any personal equation is probably eliminated. The control readings are first corrected for index error, temperature and gravity, and then compared with the corresponding readings of the barogram. The differences between the control readings and the corresponding tabulated values are then found and the mean correction derived therefrom is applied to all the tabulated values. This correction, known as the "residual correction," is so applied as to run smoothly throughout the whole length of each record—a period of 48 hours—and alterations in the amount of the correction occur, where necessary, in steps not exceeding 0·1 millibar.

^{*} At Eskdalemuir wind speed and direction are recorded by a Dines tube anemograph (see p. 96).

The scale value of the barograms is found from a comparison of a series of such standard and curve readings. The indications of a curve are converted into numerical values by measuring the ordinates with a tabulating instrument, graduated according to the ascertained scale value.

Thermometers.—The air temperature data at each Observatory are derived from records obtained photographically from two mercurial thermometers. One thermometer is used as a dry-bulb and the other as a wet-bulb thermometer.

Each thermometer has a large cylindrical bulb four inches long and a very long stem. The latter is bent twice at right angles to enable the bulb to be exposed outside the building in a louvred screen attached to the north wall of the Observatory.* The column of mercury in the vertical portion of the stem inside the building is broken at a convenient point by a small air space which moves up or down the stem with rise or fall of temperature. The record is obtained by passing a reflected beam of light through the air space and photographing its image upon a moving sheet of "bromide" paper in the same manner as described in the case of the barometer. A base line is traced on the paper by a pencil of light passing through a small aperture in the brass frame carrying the recording thermometer. The time-scale is automatically recorded upon the curves, a time-break occurring half an hour before each even hour.

Two large standard thermometers with very open scales graduated in degrees absolute and having bulbs similar to those of the thermograph are mounted in the screen side by side and close to the thermograph bulbs. Control readings of these thermometers are made three times a day for comparison with the corresponding readings obtained from the thermograms.

The scale value of the curves is found by a comparison of the readings of the standard thermometers, corrected for any errors they may have, with the corresponding measurements of the curves. The curves are measured by means of a plate of glass ruled with lines corresponding with the ascertained scale-value of the record, both for degrees and for time. The scale is graduated so as to read degrees vertically and hours horizontally.

Two alternative methods of reading the curves have been adopted.

(a) At Kew and Valencia observatories the scale is set by the base-line and after hourly readings have been obtained for the whole record comparisons are made with the control readings. The residual correction so determined (normally the same for the whole record of 48 hours) is applied to the tabulations.

(b) At Aberdeen and Eskdalemuir observatories, the practice is to adjust the glass scale so that the readings at the control hours on the trace are made to show general agreement with the corresponding eye-readings of the standard thermometers. The temperature equivalent of any part of the curve can then be read off. The base line photographed on the record serves as a useful check.

Rainfall.—This element is recorded by a Beckley self-registering raingauge, in which the rain as it falls is collected in a receiver supported on a float in a vessel of mercury. As the rain passes into the receiver, the float gradually sinks, carrying with it a pen which records its position upon a paper stretched upon a clock-driven cylinder. The displacement of the mercury by the float is arranged so as to give an uniform scale throughout. When five millimetres (two-tenths of an inch) of rain have entered the receiver a siphon comes into action, and, by discharging its contents, causes the float to rise again till the pen is brought back to the zero line, from which the record begins again.

The collecting funnel of the Beckley raingauge has an area of approximately 100 square inches. Each gauge stands on level ground and its distance from every other object is greater than twice the height of the object. A check gauge with funnel 8 inches in diameter is installed near by.

The records obtained from the Beckley self-registering raingauge are subjected to a proportional correction whereby they are brought into agreement with the amount of rainfall as recorded by the check raingauge read twice daily.

Sunshine.—The record of sunshine is obtained from a Campbell-Stokes recorder, in which instrument the sun's rays are focussed through a 4-inch spherical lens of crown glass upon a strip of blue card, which is scorched, or burned right through, according to the intensity of the sun's rays. Three different patterns of card are used at different seasons of the year. The cards are exposed in a metal bowl, and the focussed image of the sun leaves its mark behind it as it travels along the surface of the card with the apparent motion of the sun through the heavens. The intensity of the burn is not measured, but the record is regarded as that of "bright" sunshine whenever the card has been distinctly scorched. In the case of intermittent burns, an allowance is made for the extension of the trace by the charring of the card.

Wind Speed and Direction.—Except at Eskdalemuir, the records of these elements are obtained by means of a Robinson cup-anemograph, with which a Beckley windmill-vane has been combined for giving the record of direction.

Speed.—The diameter of the cups for obtaining the speed of the wind is 9 inches (0.23 m.) and the length of the arms upon which they are carried is 2 feet (0.61 m.) so that the horizontal travel of a cup-centre when 7,000 revolutions of the cups have been made is, in round numbers, 88,000 feet (26,800 m.).

The revolutions of the cups are reduced by a suitable gearing of wheels so that this number of turns shall produce one complete turn of a spiral pencil, which makes a mark upon a sheet of metallic paper carried upon a clock-driven cylinder; the pencil is so arranged that when the trace passes one extreme of the scale it recommences at the other.

Dr. Robinson concluded, as the result of a series of experiments made by him, that the rate of movement of the cup-centres was one-third of the horizontal movement of the wind current by which the cups were turned; and as the instruments were constructed in accordance with this conclusion, the 7,000 turns of the cups mentioned above were regarded as indicating the passage of 50 miles (80·4 km.) of wind.

More recent investigations into the relation between the speed of the wind and the rate of movement of the cups have led to the conclusion that Dr. Robinson's factor, 3, is too large for anemometers of the dimensions indicated above, and that the correct mean value of the factor is $2 \cdot 2$. The larger factor 3, was employed in deducing the wind velocities published in the preceding volumes of this series up to that for 1904; the factor $2 \cdot 2$ was substituted for it from the beginning of the year 1905.

If it is desired to compare the wind speeds given in the volumes previous to 1905 with those of the present year it will be necessary to reduce the former by four-fifteenths, and convert into metres per second, which may readily be done by means of a suitable conversion table. (See Computer's Handbook. Introduction p. 54.) If the degree of accuracy required does not exceed 2 per cent., the tabulated values in miles per hour (factor 3) may be converted into metres per second (factor 2·2) simply by dividing by "3."

The values of the hourly wind speed are means for periods of 60 minutes centered at the hours named. They have been given as recorded, no correction having been made for the effect of friction, which is of no importance except in the case of light winds, when it is doubtless different in the case of each instrument.

(19889)

Direction.—The direction of the wind is recorded by a pencil similar to that which records the speed. Each printed value represents the general direction* for the 60 minutes centered at the hour named, as estimated from the anemogram.

Owing to the weight of some of its moving parts, the windmill-vane is undoubtedly sluggish in light airs, its records under these conditions being untrustworthy. All wind directions have, therefore, been omitted from the tables when the velocity was 1.5 metres per second or less.

Tube anemograph.—At Eskdalemuir the speed and direction of the wind are obtained from a Dines' Tube Anemograph, while at each of the observatories information regarding the highest instantaneous wind speed and the frequencies of winds of varying speeds is also obtained from instruments of this type.

The vane-head of the tube anemograph consists essentially of (a) a horizontal tube mounted in the vane and open at the end which faces the wind, and (b) a vertical annular tube, forming part of the vane support, connected to the outside air by means of small circular holes drilled symmetrically in rows around the outer wall of the tube. An increase of pressure is produced in the horizontal tube of the vane, while the wind blowing across the rows of circular holes in the annular tube gives rise therein to a diminution in pressure, the "suction" effect. In the recorder a float of sheet copper, placed in water contained in a cylindrical tank, is capable of upward and downward movement under the influence of the pressure and suction effects, which are communicated from the vane-head by suitable piping to the space inside and the space above the float respectively. The geometrical form of the internal surface of the float is such that displacement of the float from its zero position is proportional to the speed of the wind. To the float is attached a vertical spindle which projects upwards through the lid of the cylindrical tank and carries a suitable pen at its upper extremity. This pen records the movements of the float, and therefore the variations in wind speed, on a ruled chart carried by a drum which rotates once in 24 hours.

Minimum Night Temperature on the Grass.—For determining this temperature a minimum thermometer exposed freely over the surface of the grass is used. The thermometer is enclosed in an outer glass jacket which surrounds its stem, but leaves the spirit bulb freely exposed to the air. The thermometer is supported on two small Y-shaped pieces of wood so that it lies horizontally, with its bulb about one or two inches above the ground which is covered with short grass. When snow has fallen the thermometer is supported so as to lie just above the surface of the fallen snow, but not touching it.

The thermometer is laid out at 18h each day, having been kept in an upright position, bulb downwards, inside the Stevenson Screen during the daytime so that any spirit that may have condensed in the upper part of the stem may be able to run down and join the main spirit column.

Notes on the Tables.

Standard of Time.—The observations are referred to Greenwich Mean Time except as regards sunshine, for which element local apparent time is used.

Units.—In accordance with the practice introduced in 1911, as a consequence of certain resolutions of the Gassiot Committee of the Royal Society, the values in the tables are expressed throughout in units based upon the C.G.S. System: tables for conversion to other units are given in the *British Meteorological and Magnetic Year Book (Part IV)* for 1913 and are also to be found in the *Computer's Handbook*.

^{*} Formerly it was the practice to take the direction at the exact hour. The present rule was adopted as from 1st May, 1915 (see also Introduction to Hourly Values from Autographic Records, 1913, p. xv).

Daily Mean Values.—The daily means of pressure, temperature, relative humidity and wind speed are obtained by adding half the sum of the values for the initial and final midnights to the sum of the 23 intermediate hourly values and dividing by 24.

In the preparation of the tables of diurnal inequalities for individual months and for the year, it is assumed that the difference of value between the means for the initial and final midnights, which may be termed, so far as the hourly variations are concerned, the non-cyclic variation, is equally distributed over the whole 24-hour period. Thus, in a table of diurnal inequalities the entry d_n for the hour n is given by

$$d_n = x_n - \bar{x} - (n - 12) (x_{24} - x_0)/24.$$

 x_n being the value of the element at hour n and \bar{x} the mean for 24 hours.

Atmospheric Pressure.—All pressures recorded in this volume are expressed in *millibars*, one millibar being equal to 1000 dynes per square centimetre. The following are the values of physical constants used in evaluating the data:—

Density of Mercury = 13.5955 grams per cc. at o°C.

Intensity of Gravity at Sea Level (Lat. 45°) = 980.617 centimetres per second per second.

I inch = $25 \cdot 4000$ millimetres.

Hence 1000 millibars corresponds with a reading of 750·076 millimetres, on a mercury barometer at temperature o°C. in Lat. 45°, or 29·5306 inches under standard conditions of temperature (mercury at freezing point, scale at 62°F.) in Lat. 45°.

As a millibar is a pressure, it can only be obtained from the reading of a barometer

after the latter has been suitably corrected for

- (a) index error,
- (b) temperature,
- (c) gravity.

All these corrections have therefore been applied to the barometer readings in obtaining the pressure values published in this volume. The corrections for temperature and latitude have been obtained from the *International Meteorological Tables*. (Gauthier-Villars, Paris).

Unless otherwise stated all pressure values refer to the level of the observatory as given in the headings of the tables. The reduction to Mean Sea Level, if made, has been calculated from tables prepared for each observatory from those given in

the International Meteorological Tables.

The tables contain values of pressure at exact hours obtained from the photographic barograms in the manner described on p. II; also daily, monthly and annual means of hourly values, together with the monthly and annual means of diurnal inequalities. Monthly and annual means of the hourly values after reduction to mean sea level are also given.

There is also a table showing the daily extremes of pressure, i.e. the maximum

and minimum values recorded during each day.

Temperature.—The scale on which temperatures are recorded is such that the freezing point of water under atmospheric pressure is 273 a. precisely. Other temperatures differ by $273 \cdot 0$ from readings on the Centigrade scale.

The scale approximates to the absolute scale defined by Lord Kelvin, on which the temperature of the freezing point is $273 \cdot 1$ to the nearest tenth of a degree.* Accordingly, to convert temperatures published in this volume to the Kelvin scale, a correction $+0 \cdot 1$ is to be added to each reading.

As an alternative to the application of this correction, modified values may be used for the constants which enter certain formulæ. For example:—At temperature t on the scale adopted in the Year Book, the radiation according to Stefan's Law† is

 $5.709 \times 10^{-5} (t + 0.1)^4 \text{ erg./(cm.}^2 \text{ sec. deg.}^4)$; or $5.717 \times 10^{-5} t^4 \text{ erg./(cm.}^2 \text{ sec. deg.}^4)$

In using the modified formulæ we are virtually adopting a scale of temperature with the degrees greater than those of the Centigrade scale, in the ratio of 273·1 to 273. This is the practice of the Computer's Handbook of the Meteorological Office.

^{*} A. L. Day and R. B. Sosman, *Dict. of Applied Physics*. Macmillan, London, 1922. Vol. I, p. 840. † 5.709 is the value which has been adopted by the International Research Council for publication in the International Critical Tables.

The tables give the values of temperature at exact hours obtained from the photographic thermograms; also daily, monthly and annual means of hourly values, together with the monthly and annual means of diurnal inequalities. There is also a table showing the daily extremes of temperature.

Humidity.—When the temperature of the wet bulb is above 273a, values of relative humidity at exact hours are deduced from the corresponding values of dry and wet-bulb temperature obtained from the photographic thermograms, complete saturation being taken as 100. The tables employed in effecting the reductions appear in the *Computer's Handbook* (Section I). These tables are based on Glaisher's factors and make no allowance for the effect of the wind.

When the wet-bulb reading does not exceed 273a, the above method of reduction is not followed, but values of relative humidity are derived from the record of the hair hygrograph. To these values are applied appropriate corrections based on a comparison between the readings of the record of that instrument and the corresponding values of humidity computed from dry and wet-bulb readings during neighbouring periods when the wet-bulb readings exceed 273a.

Tables are printed giving the values of relative humidity at exact hours together with daily, monthly and annual means of hourly values. Means of vapour pressure computed from the corresponding mean values of temperature and relative humidity, together with monthly and annual means of diurnal inequalities of relative humidity, are also given.

Rainfall.—Tables are given showing for the 60 minute intervals between exact hours* the amount of precipitation, expressed in millimetres, derived from the record of the Beckley gauge (see p. 12). Totals of amount are given for each day, and for each month; the latter totals referring both to the complete days of the month, and to each of the hours of the day. When zero rainfall is assigned to a particular hour, the entry appears as "...". Corresponding totals of duration of rainfall are also given, the duration being regarded as the number of hours during which rain falls at a rate of not less than o.I millimetre per hour. If slight precipitation, due to rain, snow, fog or dew, extends over some hours, and if the amounts collected in some or all of the hours are less than ·1 mm., the fact is indicated by a succession of entries, each of which is enclosed within brackets, covering the period over which precipitation is known or believed to have occurred. In such cases entries of (·1) are allocated evenly among the hours concerned in such a way that their sum is equal to the aggregate fall during the period, and the remaining entries are (...), (*), (≡) or (□) according as the precipitation took the form of rain, snow, fog or dew. When it is impossible to determine the hourly amounts of precipitation, e.g. during snowfall or on occasions when the record has failed, the normal procedure is to consider each case on its merits, and to assign hourly values derived from estimates made by the observers as soon as possible after the event. Such values are also enclosed in brackets.

Annual totals of hourly amounts and duration and notes on special features of the rainfall of the year are also given.

Sunshine.—Tables are given showing for each of the 60-minute intervals between exact hours† according to *local apparent time*, from sunrise to sunset, the duration of bright sunshine recorded by the Campbell-Stokes instrument. The sums and means of hourly amounts are also given. For each day is shown the total duration of bright sunshine, and also the percentage this represents of the "possible" duration for the day. The "possible" for each day is computed as the period of time beginning and

^{*} For the years 1904 to 1920 it was the practice to tabulate rainfall for the period of 60 minutes centered at the exact hours; the reversion to the method in use for 1903 et ante occurred on 1st January, 1921.

[†] Previous to 1st January, 1921, sunshine was tabulated for the period of 60 minutes centered at exact hours.

ending at the instants when the centre of the sun is apparently on the horizon, due allowance being made for atmospheric refraction. Even on a clear day the sun, when at an altitude less than $2\frac{1}{2}$ ° to 3° above the horizon, fails to make a scorch on the card of the Campbell-Stokes recorder.

A distinction is made in the tables between (a) sunshine not possible, and (b) sunshine possible but none recorded. If, in any hour, sunshine is not possible, the symbol "—" is used; if more than 3 minutes of "possible" sunshine falls in the 60-minute interval between exact hours according to local apparent time, and if no sunshine was recorded the symbol ". . ." is printed.

Wind.—Tables are printed giving the hourly values of wind speed and direction, together with the mean speed for each day, each hour and for the month. Values of speed are expressed in metres per second (\mathbf{r} metre per second = $\mathbf{r} \cdot \mathbf{r}$) miles per hour): those of direction are given in degrees from true north. The values of direction and speed are averages for periods of sixty minutes, centered at the exact

hours of Greenwich Mean Time.

For speeds not exceeding 1.5 m/s the wind directions are regarded as indeterminate and are omitted.

The daily values of the speed and time of occurrence of the maximum gust and the monthly distribution of wind derived from records from Tube Anemographs are shown in other tables.

Minimum Night Temperature on the Grass.—Values are given for each day of the year together with monthly mean values. The interval to which the reading refers is given at the top of the table. The reading is entered to the day of observation.

Diary of Cloud and Weather.—Tables are printed giving particulars of amount of cloud and of the weather at 7h, 9h, 13h, 15h, 18h, 21h daily, while cloud forms are shown for the three hours 7h, 13h, and 18h. The cloud forms are in accordance with the International classification and are indicated by the following abbreviations:—

Cirrus					 Ci.
Cirro-Stratus					 Ci-St.
Cirro-Cumulus					 Ci-Cu.
Alto-Cumulus					 A-Cu.
Alto-Stratus			• •		 A-St.
Strato-Cumulus					 St-Cu.
Nimbus					 Nb.
Cumulus			• •		 Cu.
Cumulo-Nimbus			• •	• •	 Cu-Nb.
Stratus					 St.
Stratus-cumulifor			• •		 St-Cuf.
Fracto- (prefix, as					 Fr
-lenticularis (affix		ı stratu	s-lentic	cularis)	 -lent.
Mammato-cumulu	ıs				 MCu.

The figure given for the amount of cloud denotes the proportion of sky covered by cloud: the numerical scale running from o, cloudless, to 10, completely overcast. In the columns for form of cloud all the forms noted by the observer at the time of observation are printed where space permits. When the number of forms is too great to permit this, the predominating forms selected at the time of observation to give the best representation of the cloud canopy are printed. If high or medium cloud can be seen, one of the selected types is normally a high or medium cloud. The amounts of cloud given indicate, however, the total cloudiness irrespective of form. In the case of fog through which it is impossible to discern the sun or stars the cloud amount is entered as 10, but if cloud can be seen through the fog the form and amount are entered in the usual way. If the sun or stars are visible through fog and if there is no evidence of cloud above the fog the amount is entered as 0.

For the purposes of the summary of the weather for each day, contained in the "Remarks" column, it is usual to consider the day as divided into three portions,

viz., morning, afternoon and night, denoted by a, p, n, respectively, but it should be noted that no arrangements are made for regular eye observation of weather

changes in the period 21h 30m to 6h 30m.

In the "Remarks" and "Weather" columns the entries consist very largely of International weather symbols and the letters of the Beaufort scale. symbols and letters are as follows:-

```
Beaufort Notation and International Weather Symbols.
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```
blue sky. (Cloud amount 0, 1, 2, 3.) some cloud. (Cloud amount 4, 5, 6.)
b
bc
          cloudy. (Cloud amount 7, 8.)
С
0
          overcast.
                      (Cloud amount 9, 10.)
          gloomy, dull appearance.
g
          ugly, threatening appearance.
u
     0
          visibility, unusually clear atmosphere.
V
\mathbf{z}
     \infty
     ≡°
          mist, light fog.
m
f
          fog.
     =
          wet fog, i.e. fog which deposits water copiously on exposed surfaces.
fe
W
     Δ
          hoar frost.
\mathbf{x}
          ice crystals in the air.
     <del>---</del>
          rime.
          glazed frost.
          water deposited copiously on exposed surfaces, without rain falling.
e
          dry air. (Relative humidity less than 60 per cent.).
y
          passing showers.
p
d
          drizzling rain.
          rain.
r
S
    *
          snow.
          sleet.
rs
          drift snow.
          snowlying. (More than half the surrounding country covered with snow.)
h
          soft hail.
     Δ
t.
     Т
          thunder.
1
          lightning.
    く
tlr
          thunderstorm.
          gale.
          squalls.
q
          solar corona.
     Φ
         solar halo.
    \oplus
         lunar corona.
    (I)
    W
         lunar halo.
         rainbow.
         aurora.
    Ж
          zodiacal light.
     The
          mirage.
```

The letter j preceding a letter or symbol which denotes some form of precipitation, denotes that the precipitation is within sight, though not actually falling at the station. To indicate "intermittent" or "occasional" the prefix "i" is used.

The figure $\,^{0}$ attached to a symbol indicates slight, whilst the figure $\,^{2}$ indicates strong or heavy: thus •° slight rain, •2 heavy rain. The gale symbol — is normally used in this publication to indicate that the wind as recorded by the anemograph averaged at least 17·2 m/s for one or more "centred" hours. At Richmond (Kew Observatory) the symbol has been used with the word gust in brackets to indicate the occurrence of gusts reaching $17 \cdot 2 \, m/s$.

M.O. 279 (Lerwick)

Air Ministry

METEOROLOGICAL OFFICE

OBSERVATORIES' YEAR BOOK 1923

Comprising the results obtained from autographic records and eye observations at the observatories at Lerwick, Aberdeen, Eskdalemuir, Cahirciveen (Valencia Observatory), Richmond (Kew Observatory), and Benson.

LERWICK

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LERWICK OBSERVATORY.

INTRODUCTION.

GENERAL REMARKS.

In 1919 the establishment of an observatory in the Shetlands was included in the programme of the Meteorological Office. A wireless station built in 1913 by the Admiralty and transferred after the war to the Post Office, but used by that Department only in case of emergency, offered suitable accommodation in the way of offices and living quarters. It proved possible to make an arrangement under which the Air Ministry, on condition of maintenance of wireless plant, has the use of the station as an observatory and of the wireless plant for the transmission of meteorological

reports and time signals.

The Observatory was opened on the 7th June, 1921, when the first instalment of the instrumental equipment arrived. Later on in the same year the construction of a magnetograph house and of huts for absolute magnetic and auroral observations was commenced. The magnetograph house is a heavy concrete structure with walls 2 feet 6 inches (76 cm.) thick, of internal dimensions 16 feet by 10 feet (4.9 m. × 3 m.), and after construction several months had to elapse before the thick concrete walls and roof could be thoroughly dried and the recording instruments placed in position. These instruments, which are described below, consist of magnetographs recording magnetic declination and horizontal and vertical force. In addition, in order to obtain a record of the more minute changes in the vertical component of terrestrial magnetic force, a line of twin cable was laid in an approximately horizontal plane round Loch Trebister, the terminals of the cable being connected to a suitable galvanometer on which could be measured the current induced in the cable by changes in the vertical component of terrestrial magnetic force. The arrangement is similar to one in use at Eskdalemuir Observatory, but no records from either have yet been included in official publications.

Other instruments installed at the Observatory include barometers, barograph, hygrograph, psychrometers, nephoscope, raingauges (ordinary and self-recording), sunshine recorder and Dines tube anemograph. But meteorological observations have been restricted, and the time of the somewhat limited staff available has been devoted

chiefly to magnetic work.

The first complete year of magnetic observations is 1923. Many instrumental difficulties have, however, been experienced and it has been decided to restrict publication to the monthly means extracted from the records, a summary of the absolute observations, and diurnal inequalities in declination and horizontal force.

The site and the work in Terrestrial Magnetism will now be described.

SITE.

The Observatory is situated on a ridge of high ground about a mile and a half (2·4 km.) to the south-west of Lerwick and adjoins the main road between Lerwick and Scalloway. The site slopes upward from west-north-west to east-south-east, the average height above M.S.L. being about 280 feet (85 metres). The ground to the east and south-east rises slightly for about $\frac{1}{4}$ mile (·4 km.) then slopes sharply down to the sea. In other directions there is a downward slope for about $\frac{1}{4}$ mile extending to the Loch of Trebister on the south-west, Sandy Loch to north-west, and to the

Burn of Sound to north-north-west; beyond these and distant about $\frac{3}{4}$ mile (1·2 km.) from the Observatory are small hills—Munger Hill to the south is about 320 feet (97 metres) above M.S.L., Shurton Hill to west-north-west rising to 576 feet (176 metres), and Stony Hill to the north about 400 feet (122 metres). In clear weather it is possible to see the Outer Skerries, $25\frac{1}{2}$ miles (41 km.) north-east by north, and Sumburgh Head, 20 miles (32 km.) south by west; the horizon in other directions is limited to a few miles.

The average depth of soil in the vicinity is about a foot, and outcrops of sandstone occur in many places. The surrounding country is barren and desolate, the only vegetation being coarse grass, stunted heather, and moss, with occasional patches of bare black peat. The Observatory ground is of a very uneven nature, and, owing to lack of proper drainage, is frequently water-logged; in winter it may be almost submerged for considerable periods. Views of the station are shown in Figs. 3, 4 and 5, and the arrangement of buildings and situation of instruments are set out on the site plan in Fig. 1.

TERRESTRIAL MAGNETISM.

Notes on Instruments.—Declination and horizontal force are recorded by the Adie magnetographs which were in use at Falmouth until 1912; the vertical force is recorded by an instrument designed by the late Prof. W. Watson, F.R.S. The set had been stored for several years, but was reconditioned by the makers and tested at Kew before being installed at Lerwick in November, 1922.

The declination magnet has a unifilar suspension, and the torsion correction is negligible. The scale value is constant for all positions of the light dot on the sheet; throughout the year it was I mm. of ordinate to I 93 minutes of arc. In the horizontal force instrument the magnet is maintained in a position approximately perpendicular to the magnetic meridian by torsion of the bifilar suspension. The vertical force instrument is of similar construction to that in use at Eskdalemuir Observatory, but consists of only six magnets. Copper damping plates are fitted to each instrument and the recording mechanism is similar to that used at Eskdalemuir. The arrangement of the instruments in the magnetograph house is shown in Fig. 2.

The chief instrumental defects encountered during the year were:—

- (a) A persistent tendency of the trace, in the case of the H force instrument, to drift away from its base-line.
 - (b) Unsteadiness of the vertical force system.

These troubles may have been largely due to the dampness of the magnetograph house, but although different types of driers were used they were not overcome during 1923. A new suspension was fitted to the horizontal instrument in November,

but this also proved to be ineffectual in stopping the drift.

Adjustments to the horizontal and vertical force instruments were made on many occasions, and in consequence determinations of the scale values had to be taken frequently; the scale values have been assigned to periods between the discontinuities recorded, instead of for each month. The determinations are made by Broun's method, the deflecting magnet being placed in the "broadside on" position and at a distance of 55·9 cm. from the recording magnets. A larger deflection distance would render the error due to inequality of the distribution co-efficients for the H, D and V magnets less appreciable, but cannot be used owing to the restricted size of the magnetograph house. The double deflections produced are approximately 87 mm. for D, 98 mm. for H, and 59 mm. for V, giving scale values for the horizontal and vertical force instruments of about 7·2γ per mm. and 12γ per mm. respectively.

It is estimated that, in general, an accuracy to within I per cent. has been obtained in the scale values, but it has been impossible to assign scale values to a number of vertical force records owing to the erratic behaviour of the instrument.

The records of declination, horizontal force and vertical force have been tabulated hour by hour. The values are read off by means of graduated celluloid scales, a value being the mean reading for 60 minutes centering at the hour.

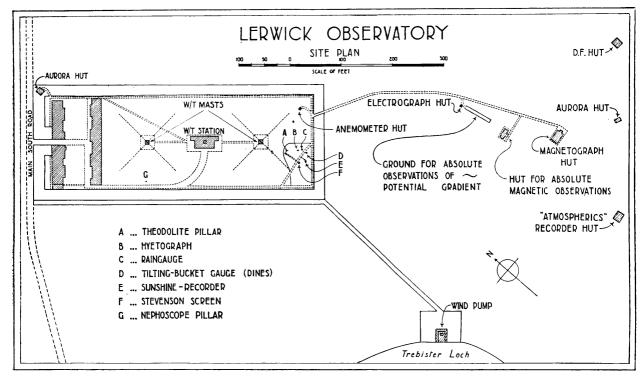


FIG. 1. SITE PLAN.

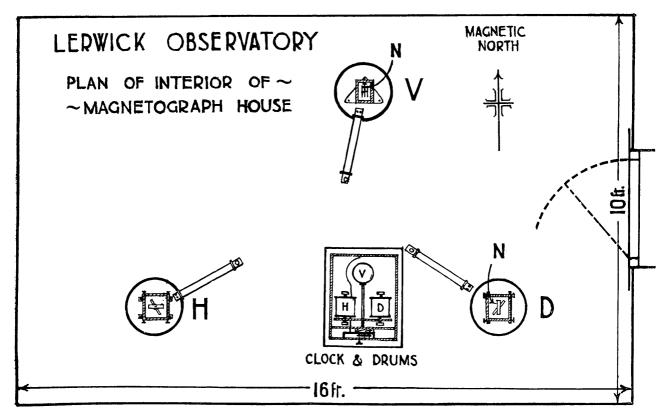


FIG. 2. ARRANGEMENT OF MAGNETOGRAPHS.

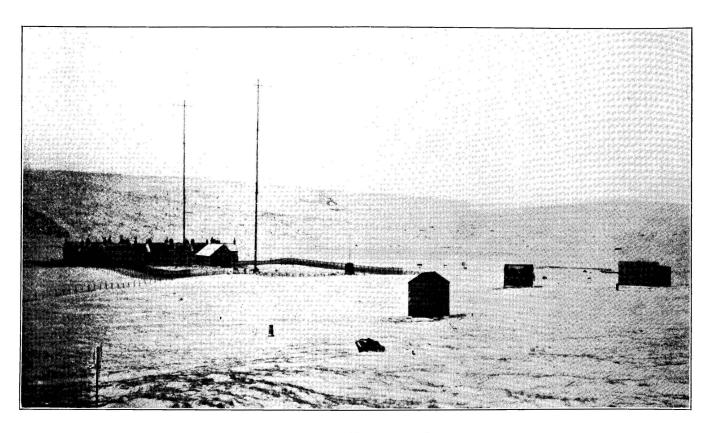


Fig. 3. General View from South.

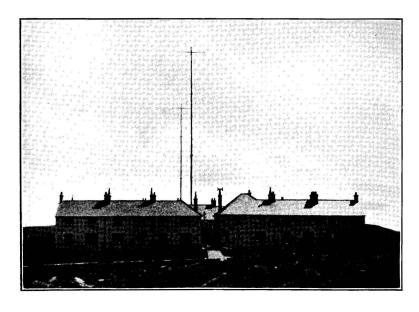


Fig. 4. Main Entrance and Front View (from N.W.)

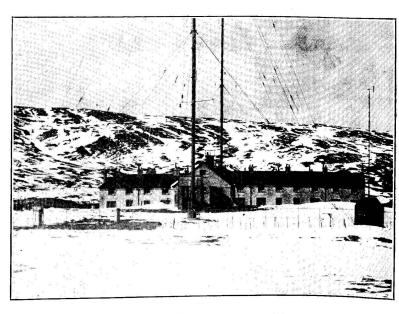


Fig. 5. Near View of Buildings and Meteorological Instruments (from S.E.)

To face p. 23.]

Base values for the records are obtained from the results of absolute observations taken twice weekly. Horizontal force and declination are determined with Unifilar No. L 3951 (Cambridge Instrument Co.) using magnets 3951A and 3951C. The magnetometer is used on the centre pillar (No. 2) of the absolute hut, the azimuth of the fixed mark being taken as 8° 43′ 2″ east of south. Inclination is measured with Dover Circle No. 238 placed on the East pillar (No. 3), using $3\frac{1}{2}$ inch needles. In the deflection experiment three distances 25, 30 and 35 cm. are used, the P and Q corrections adopted for the year being as follows:—

P and Q used for	: .	Derived from Months.	Mean Value at 25 cm. of $\log_{10} (1+Pr^{-2}+Qr^{-4})$.
January February March 1st-15th March 16th-31st April May June July August September October November	}	January and February April–July April–July April–August April–September April–October May–November June–December July–January August–February September–March	1.99782 1.99782 1.99782 1.99866 1.99866 1.99862 1.99841 1.99832 1.99821 1.99816 1.99810 1.99795 1.99788

The scheme approved was the calculation for each month of a P and Q from the observations of seven months centering in that month, and this scheme was applied from July onwards. An accident which befell the magnet in March required special measures to be adopted for the earlier months.

Aurora.—During the auroral season, i.e. from about September to April, a watch is maintained normally until about 23.00 G.M.T. each evening, and observations—as a rule at intervals of 15 to 20 minutes—are made of the northern horizon and of general meteorological conditions. The records form what is called the auroral log, a brief summary of which is given in Table 12. When any auroral display is observed, a second observer is called and detailed observations are maintained until the display subsides. So far these detailed observations have been mainly non-instrumental and have consisted in noting and making descriptions of the phenomena seen during the display. These notes are entered in a second log reserved for records of actual auroral displays. Extracts from this latter log may be obtained by anyone requiring the detailed information.

Notes on the Tables.—Tables 6, 7, 8 contain the mean diurnal inequalities of Magnetic Declination for the months, year, and seasons, for "all," quiet, and disturbed days respectively. Tables 9, 10, 11 deal similarly with Horizontal Force. Tables 1, 2 and 3 contain respectively, the Ranges of the Diurnal Inequalities, the Average Departure from the Mean of the Day and the Non-Cyclic Change.

Table 4 contains the Absolute Daily Ranges of the Declination. Table 5 contains the Mean Monthly and Annual Values of Declination, Inclination, and Horizontal Force, as deduced from the results of the absolute observations; the

dates on which these absolute observations were made are also given.

Review of Results.—Magnetic phenomena at Lerwick are so different from those hitherto encountered in this country, especially in the south of England, and the instrumental conditions there during 1923 were so exceptional, that the real significance of the results can be appreciated only when regard is had to a variety of considerations. In 1890, when a system of magnetic quiet days was first introduced in this country, the beliefs generally entertained were apparently those expressed by Rücker and

Thorpe in their great work* on the magnetic survey of the United Kingdom for the epoch 1891. The view was then taken that there were two quite distinct phenomena, viz., a regular diurnal variation and irregular movements. The former was uninfluenced by the latter, being the same on quiet and disturbed days, and when expressed in terms of local time was practically the same over very considerable areas, such as the British Isles. Disturbance was supposed to follow universal time, corresponding changes at different places being simultaneous, but it was also supposed to be practically invariable in amplitude within the British Isles. The hypothetical nature of these conclusions was clearly recognised by Rücker and Thorpe, but they believed them sufficiently good approximations to the truth to justify their referring all their field observations to a single base station, Kew Observatory, in the south of England.

If these conclusions were correct, it obviously mattered little whether a station acting as successor to Kew Observatory were situated in England or in Scotland, and Eskdalemuir was accordingly selected owing to its presumptive security from artificial disturbances. As soon, however, as records became available from Eskdalemuir, it was obvious that natural magnetic disturbance was considerably larger there than at Kew, and the desirability of records from a British station a good deal to the north of Eskdalemuir was gradually recognised. That disturbance would prove to be larger at Lerwick than at Eskdalemuir was confidently anticipated, but the increase has been so large that it emphasises certain difficulties much less acutely

felt in the average observatory.

If the regular diurnal variation, as Rücker and Thorpe supposed, were a phenomenon unaffected by disturbance, its character for a single month might obviously be obtained with greater accuracy from a single quiet day at the middle of that month than from all the days of the month quiet and disturbed combined. The occurrence, however, of a very quiet day at the middle of a month is exceptional. Also there are usually trifling irregularities in the traces from even the quietest of days. Thus practical considerations pointed to the employment of several quiet days a month, and five was selected as the best number, because even at highly disturbed times there are few months when an Observatory in the south of England does not have at least that number of days free from large disturbance. In the choice of days, whether as made originally at Greenwich, or now at De Bilt, attention has been paid to the desirability that the mean date from the selected days should fall near the middle of the month. This is a matter of very sensible importance, at least in those months in

which the type or amplitude of the diurnal variation is changing rapidly.

Rücker and Thorpe's conclusion as to the simultaneity of disturbance within the British Isles appears to be true in a limited sense. If such a thing as an absolute standard of disturbance existed, it would probably prove to be the case that when the days of a month were arranged in descending order of disturbance, the order would be nearly the same for the north of Scotland as for the south of England. But irregular movements are so much larger at Lerwick than at Kew, that their elimination from diurnal inequalities tends to be decidedly less complete at the more northern station than it used to be at Kew in days prior to the existence of electric traction. Minor irregularities may be seen in the sequence of hourly values at Lerwick in certain months even in the quiet day inequalities, and in the case of all days they are visible even in the seasonal diurnal inequalities and in that for the whole year. In the disturbed day inequalities such irregularities are to be expected, even at the quietest of stations. At any station, especially at one so disturbed as Lerwick, it has to be remembered that disturbed day inequalities for a single month of a single year are data having quite a different rôle from quiet day inequalities at the ordinary station. The quiet day data can claim to be representative of a particular month of the year in a measure to which the disturbed day data can make no claim. At the ordinary station there are few months in which the five quiet days do not make a fair approach to the ideal quiet day, especially in quiet years like 1923. On the present international scale the magnetic

^{*} Royal Soc. Phil. Trans. A. 188 (1896).

character of individual days varies from 0.0 to 2.0 (highly disturbed). In 1923 two of the December quiet days were of character 0.2. Each of the other 58 international quiet days was of character 0.0 or 0.1, and the mean character figure for the five quiet days of the month varied only between o or (October) and o og (December). Thus the quiet day inequality of a single month represents a standard of quietness which is not indeed absolutely invariable, but still varies only within comparatively narrow limits. Again the mean date of the five quiet days usually falls very near the middle of the month. In 1923 it fell on the 14th, 15th, or 16th in ten months out of the twelve, and in the other two months on the 12th and 19th. On the other hand, the international disturbed days necessarily vary enormously as regards disturbance. September 27th and October 16th had characters 2.0. The significance of international character figures fluctuates according as the year is quiet or otherwise, but even in a quiet year character 2.0 implies a really notable magnetic storm. The highest daily character figures allotted in August and April, 1923, were only 1 · 1 and 1 · 2 respectively. and the mean character figures for the five disturbed days of these two months were only 0.88 and 1.08, as against means of 1.58 in October and 1.44 in March. the more disturbed days of a month may fall predominantly in one half of the month. In December, 1923, for example, the five were consecutive days, their mean date being the 25th, while in August 1923,, their mean date was the 10th.

If it were not for the II-year period, the quiet day inequality of any single month, say March, 1923, would be fairly representative of the average March, but no such claim can be made for the disturbed day inequality. For example, as appears from Table I, the disturbed day inequality ranges for September and October, 1923, were much in excess of those for April, but no inference can be drawn as to the relative amplitudes of the diurnal variation on disturbed days in these three months in the average year. In short the disturbed day data—and to some extent even the all-day data—must be regarded as material which must accumulate for a number of years, before final conclusions can be drawn as to the differences between individual months of the year. This applies, though to a less extent, even to the diurnal inequalities for

the three seasons of the year.

One of the phenomena unexpectedly encountered in magnetic quiet days was the non-cyclic (n.c.) change. So far as declination (D) is concerned, in temperate latitudes, the quiet day does not differ much in that respect from the average day, but it is otherwise with horizontal force (H) and vertical force (V). As is now well known, the average international quiet day shows a decided increase in H in the 24 hours. The increase seems to be larger in lower than in middle latitudes, and to be larger near sunspot maximum, when disturbance is usually greater, than near sunspot minimum. At Kew in the average year it is of the order of 3γ. It is usually recognised that a diurnal inequality—a term naturally suggestive of a change periodic in the 24 hours ought not to contain a non-periodic element; and it is usual to apply a correction which assumes that the n.c. change has come in at a uniform rate throughout the This is probably, in general, only an approach to the truth, but no better assumption seems possible in our present state of knowledge. It has the great advantage of simplicity, and when the amplitude of the n.c. correction applied is given, anyone who desires to reproduce the original uncorrected variation can easily do so. In the present case we have to do with a n.c. change of instrumental origin in the H tabulations on all days, which in most months largely exceeded the natural n.c. change characteristic of quiet days. It has been allowed for in the usual way by a n.c. correction, which assumed the change to come in at a uniform rate. instrumental change which persists in one direction for many months, in an instrument situated in a chamber with a very small diurnal range of temperature, seems very unlikely à priori to be sensibly more rapid at one hour of the day than another. Thus there are strong reasons for hoping that the diurnal inequalities now published for H are substantially correct, especially in the earlier months of the year, when the instrumental change was comparatively slow.

The secular change in H at present is so small that its contribution to the daily n.c. change is practically negligible, and we shall not be far wrong if we regard the

n.c. change given in Table 3 for all days as representing the instrumental change. It would thus appear that during the first four months it was nearly invariable (about 6.5 per diem). A marked rise occurred during the next three months, followed by a decline during August to a fairly steady rate of about 18 y per diem in September and October. During the early days of November the drift was apparently much bigger, but after a few days it fell again to a value only a little over 20 y per diem, and remained at this until the 21st when the wire suspension broke. It was replaced the same day, but for some days the drift was enormous, and several days' traces were discarded, including those of the 22nd to the 25th, which were respectively, international disturbed and quiet days. The 27th and 29th were also international disturbed days; and as the creep though still very rapid had become approximately uniform, these two days were used and the 3rd was substituted as a disturbed day for the 22nd. The creep diminished a good deal during December, but in a gradual way, and the application of a n.c. correction, though less satisfactory than in the earlier months, seemed a preferable alternative to omitting December entirely. Still the n.c. correction was so large compared with the natural daily range that the results for that month are admittedly more open to doubt than the others. to publish H inequalities at all was only taken after some hesitation. It was not based altogether on à priori ideas as to the unlikelihood of the instrumental creep having any considerable diurnal variation. The results would not have been published unless they had shown a consistency and reasonableness which appeared adequate testimony to their generally satisfactory character. December, as we have seen, showed an enormous instrumental creep as compared with January and February, but there is much more similarity—as there ought to be—between the quiet day inequalities obtained for December and January than between those obtained for January and February. Other favourable evidence is derivable from a comparison of the n.c. results from the different classes of days. No conclusion can be drawn from the November and December data. Two of the November disturbed days—used also in the all-day inequalities—followed the breakage of the suspension, while the 4 quiet days used all preceded it. Again in December all the disturbed days came near the end of the month, when the creep was much reduced. If, however, we confine ourselves to the first ten months of the year, when the conditions of the days of different types were fairly similar, we find as mean values of the n.c. corrections in Table 3 + 15.8γ from "all" (a) days, + 18.7γ from quiet (q) days, and + 8.8γ from disturbed (d) days. As already explained, we may regard the n.c. change from a days as representing the instrumental creep. Subtracting it from the n.c. change for q days, we get $+2.9\gamma$ as the real n.c. change on the average quiet day due to natural causes. This compares well with the mean value from the 11 years, 1890 to 1900, at Kew, viz., $+3.3\gamma$. Again, subtracting the n.c. change on a days from that for d days, we get -7.0γ as the real natural n.c. change on the average disturbed day. This would seem to be of at least the right sign and order of magnitude, because the mean n.c. change derived at Kew from the 200 most disturbed days of the period 1890 to 1900—days with a much higher average of disturbance than the 60 selected disturbed days of 1923—was -13.2γ .

The December results may serve to illustrate a point in connection with H quiet day inequalities which is apt to be overlooked. It will presumably be admitted that the diurnal inequality ascribed to a month should be independent of the hour we may select for the commencement of the "day." For example, we might just as well have taken Greenwich noon as Greenwich midnight for the commencement of the international magnetic day. But if we had, as in December at Lerwick, a n.c. change of + 55 γ per diem, and a regular periodic change of only some 6γ , it is obvious that if no n.c. correction were applied we should find the minimum for the day within an hour or two of its commencement, and the maximum for the day within an hour or two of its termination, irrespective of the hour we chose for the day's

commencement.

The curves were measured in the same way as at Kew and Eskdalemuir, and as there the quiet and disturbed days were those selected at De Bilt, except for the slight departures in November already mentioned. The D inequalities obtained respectively from a, q and d days are given in Tables 6, 7 and 8. The corresponding H inequalities are given in Tables 9, 10 and 11. The algebraically greatest and least of the hourly values are in heavy type. The seasons include the same months as at Kew and Eskdalemuir. \ddagger

A double daily oscillation of D is easily recognisable on q days in some months, including January, October, November and December, and in the winter season. It is not very clearly indicated in a days in any single month owing to the greater irregularity of the figures, but it is recognisable in the diurnal inequalities for equinox and the whole year. There are no clear indications of it in any summer month, whether for q or a days, and the summer diurnal inequalities, whether for a, q or a days,

suggest only a single daily oscillation.

Whether a double oscillation is visible or not, the principal maximum—i.e. the westerly extreme—always appears, even in the d day inequalities, in the early afternoon. On q and a days it appears at 13h in every season and month except as follows:—June (14h both q and a), July (a 14h) and November (12h both q and a). On d days it is never earlier than 13h; but appears at 14h in July, November and summer, at 15h in January, May, October and December, and at 17h in June. There seems thus a decided tendency for disturbance to delay the hour of maximum.

The time of the minimum or principal minimum is much more variable. It has a decided seasonal variation, and is also influenced by disturbance. Throughout the greater part of the year a principal minimum at 7h or 8h seems normal on q days. But even on q days the principal minimum appears near midnight in December and January and in the winter season, and there is a prominent secondary minimum near midnight in November. In the a inequalities the principal minimum falls near midnight except in the five months April to August. It appears at 2h in the equinoctial as well as the winter season; but it still appears at 7h in the inequalities for the whole year and for summer.

In the d inequalities the relative prominence of the night minimum is further increased. The inequality for summer has its principal minimum at 6h, but in three of the constituent months the hour is pushed back nearer midnight. In the d inequality for the year there is not even a suggestion of a minimum at 7h or 8h, the normal time for quiet days. The tendency in the compass needle to an enhanced easterly position near midnight in winter days and on d days at all seasons—a phenomenon which prevails in the south of England—would appear to be very prominent in Lerwick.

The most constant feature in the D diurnal variation is the movement to the west from 8h or earlier until the maximum in the early afternoon, and the subsequent reverse movement proceeding until at least a late evening hour. The westerly day movement is largest relative to the afternoon easterly movement in summer. The easterly movement in the afternoon increases in relative importance as the day shortens,

and as more and more disturbance prevails.

In H, a and q diurnal inequalities alike suggest a double daily oscillation throughout the whole year. In some of the summer and equinoctial months the forenoon maximum is hardly recognisable, but there is always at least a hesitation preceding the plunge to the day minimum. This minimum is recognisable in every inequality, and is the principal minimum in a and q days in every season and in every month except December, when a slightly lower value appears at 24h on q days. The hour of occurrence of the day minimum is 10h in the July q inequality, and 12h in the q inequality for March and in the a inequalities for January and February. With these few exceptions it is found at 11h in every month and season, alike in a and q days. Even on d days the principal minimum occurs between 10h and 12h in six individual months and in the summer season. But in the other d inequalities it appears near midnight, at 1h in March, September and Equinox, at 2h in January and the year,

[†] The seasons are defined for this purpose as follows:—Winter, January, February, November, December; Equinox, March, April, September, October; Summer, May, June, July, August.

at 3h in June, at 23h in October and at 24h in February and winter. There is thus an unmistakable tendency for disturbance to deepen the minimum occurring near

midnight so that it becomes the principal minimum.

There is a seasonal variation in the hour of occurrence of the principal maximum in H. It appears in the forenoon in the winter season, and in all its constituent months, except November q days and February d days. It appears in the afternoon in all the inequalities for the year, equinox and summer, and in individual months from April to November inclusive on q days, from March to October inclusive on q days, and from February to October inclusive on q days. Disturbance thus seems to have little effect on the result. At the same time it appears to make the afternoon maximum come earlier. In the case of the year this appears at 18h on q days, at 19h on q days and at 17h on q days. In the equinoctial season it appears at 18h on q days, at 20h on q days and 17h on q days; while in summer it appears at 18h on q and q days, an hour earlier than on q days.

The d inequalities for individual months exhibit many irregularities of an apparently accidental character, but the d inequalities for the seasons and the year are nearly as smooth as the a. The main features of the diurnal inequality are usually prominent even in the d inequalities for individual months. A principal maximum, for example, is recognisable between 16h and 18h in seven individual months.

for example, is recognisable between 16h and 18h in seven individual months.

Tables 1, 2 and 3 contain miscellaneous data. The n.c. changes have been already discussed. The data ascribed to the year in the case of D are the arithmetic means of the monthly values taken algebraically. As the mean daily fall o'·II given by both a and q days is thrice what we should expect from the known secular change, there

was presumably a small instrumental drift even in the D magnetograph.

In the case of D the range and the A.D. (average departure from the mean) in every single month and season are larger for the a than the q days. In the case of the inequality for the whole year the excess of the a range is only 8 per cent. But if we take instead the arithmetic mean of the ranges for the individual 12 months, the a quantity is 24 per cent. the larger. If instead of the range we take the A.D. in the diurnal inequality for the year, the a value is 35 per cent. in excess of the q.

In the case of H the a range is again in general decidedly larger than the q range; but in August, September and November the excess is small, and in October there is a small deficiency. As regards the A.D. there are two months in which the a value is the smaller, and several in which its excess is trifling; while in the case of the year and the equinox the a value is slightly the smaller. The greater homogeneity of the

quiet days probably is accountable for these results.

In every case, in D and H alike, the range and A.D. are much larger for d than for a or q days. In the case of D the d range stands to the q range roughly in the ratio 30: 10 in winter and 20: 10 in equinox, but only 13: 10 in summer. The A.Ds. make the excess of movement on d days somewhat less relatively in winter, but larger in equinox and summer.

In the case of the seasonal diurnal inequalities in H the d ranges and A.Ds. are roughly double the q; but in some individual months, e.g. October, when the selected disturbed days were more than usually disturbed, the excess of the d ranges

and A.Ds. is much larger than this.

It will be noticed that though the disturbed days were identical for D and for H, except in November, there is no approach to constancy in the ratio borne by the D range on d days to the corresponding H range in individual months. For example, the D range on d days was 26 per cent. larger in July than in June, whereas the H range was 77 per cent. larger in June than in July. The extent to which disturbance manifests itself is often widely different in D and H.

In giving inequalities for a, q and d days the practice adopted at Eskdalemuir has been followed. Decided irregularities, however—easily recognised if curves be plotted—present themselves in the a days inequality for H in winter at 2h and 2oh. The occurrence of such irregularities in so quiet a year raises a doubt whether it might not be better to replace inequalities from all days by inequalities from ordinary days, omitting from the latter the five monthly international disturbed days.

INEG	ANGES QUALI' YEA	TIES	MEAN FOR T ID SE	HE N	IONTE	IS,	THE		DIVII	PART OUAL OF T		UES	NO	N-CYCL	IC CH.	ANGE	(24 h.—0	h).†
1. Ler	wick.				1	923.	2.	Lerwi	ck.		19	923.	3. L	erwick.				1923.
Month and Season.	" Al Day	-	Qu Ďa			urbed iys.		All " iys.		iiet iys.	Distu Da	ırbed ys.	" A Da			uiet Lys.		urbed iys.
Season.	D.	H.	D.	H.	D.	H.	D.	н.	D.	н.	D.	Н.	D.	H.	D.	Н.	D.	н.
Jan Feb Mar April June July Aug Sept Oct Nov Dec	, 5.65 6.58 8.34 10.27 8.72 9.63 9.13 10.05 9.34 8.39 5.43 4.61	γ 10·0 18·8 28·3 46·6 52·6 54·5 40·4 41·3 35·3 23·4 13·6 9·0	3·11 3·55 6·44 8·87 8·34 8·97 8·50 9·77 9·05 4·96 2·90 2·91	y 5·9 17·0 20·5 44·1 45·9 43·4 35·9 40·1 35·0 24·3 13·5 5·6	, 10·12 11·32 14·19 14·05 13·57 11·33 14·24 12·03 19·65 17·75 9·18 9·94	γ 18 2 68·1 110·7 65·3 109·8 109·0 61·5 50·7 114·4 144·8 18·7 15·9	, 1·15 1·69 2·18 2·56 2·33 2·55 2·36 2·30 2·31 1·86 1·21 1·06	γ 2·0 4·7 6·7 10·8 10·8 12·7 9·2 .10·0 7·9 6·2 2·6 1·8	, 0.77 0.83 1.29 1.94 2.01 2.26 1.93 2.13 1.99 1.15 0.74 0.69	7 1·2 4·1 5·1 10·6 10·0 10·5 8·5 9·1 6·2 2·9 1·5	2.09 3.12 3.55 3.18 3.89 3.29 3.52 3.16 4.45 5.14 2.49 1.80	7 3·4 12·6 20·3 14·4 23·1 23·8 14·5 21·8 28·5 3·9 3·6	, -0·12 -0·37 -0·02 -0·03 -0·15 +0·08 -0·16 -0·16 +0·05 -0·14 -0·17 -0·19	7 + 6·4 + 7·2 + 5·5 + 7·2 + 13·6 + 19·8 + 32·6 + 28·7 + 18·1 + 18·9 + 35·4 + 52·9	, -0·19 -0·93 +0·04 -0·54 +0·31 -0·12 +0·04 +0·27 +0·12 +0·27 -0·69 +0·04	7 + 9·4 + 9·7 + 7·8 + 10·8 + 15·9 + 24·1 + 37·2 + 28·8 + 18·2 + 25·4 + 28·0 + 55·1	+0·23 -1·12 +0·89 -1·04 -2·86 +0·50 -1·08 -0·08 +0·39 +0·77 -3·82 -0·27	γ + 4·6 + 0·6 - 3·4 - 8·2 - 3·8 + 14·1 + 21·1 + 29·9 + 17·8 + 15·4 + 58·8 + 28·9
Year	6.69	28.8	6.21	26.4	10.45	47.9	1.90	6.2	1.41	6.3	2.78	11.8	-0.11	-	-0.11	-	-0.62	_
Winter	5.46	12.6	2.91	9.8	8.72	20.8	1.27	2.6	0.75	2.2	2.16	4.8	_	_	_	_	-	_
Equinox	8.34	32.4	7:33	30.1	14.69	77:3	2.20	7.0	1.57	7.6	3.49	17.8		-	_	_	-	_
Summer	9.30	46.0	8.78	40.8	11.51	76.1	2.35	10.3	2.04	9.6	3.36	17.6		_			-	

^{*} The ranges are those shown in Tables 6 to 11, in the preparation of which the non-cyclic change has been eliminated. † The non-cyclic changes shown under H. are mainly of instrumental origin. See p. 26.

ABSOLUTE DAILY RANGES OF MAGNETIC DECLINATION.

4. Lerwick.

1923.

Month	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	
Day 1 2 3 4 5	6·95 9·65 20·07	, 24·51 10·04 18·72 25·67 12·16	8.69 13.12 12.93	11·19 12·16 12·74	10·04 23·74 23·35	11.30	9·84 9·84 9·84	, 13·51 11·19 24·32 15·05 8·69	16·41 13·70	6.75	47·29 13·51 4·83	5.98	Day 1 2 3 4 5
6 7 8 9	4·05 10·23	11·58 19·30 9·07 5·21 15·83	16·60 5·02 6·75	17.18	9·46 13·51 9·46	12·16 10·42 10·61	9·84 8·49	15·44 11·58 11·19 13·12 12·16	9·84 12·35 23·93	6·75 8·30 16·21 16·79 14·09	25·28 7·72 6·95	5·79 5·02 21·23	6 7 8 9 10
11 12 13 14 15	11.00		10·04 11·00 21·04	17·76 33·77 18·72	8·30 11·77 13·90	9·46 37·63 28·76	15·63 9·07 10·61	9·84 12·55 19·30 12·93 13·51	11·58 15·25 13·90	17·37 16·79 10·23 23·93 57·51	23·74 16·98 6·56	6·18 12·93	11 12 13 14 15
16 17 18 19 20	9·65 4·83 4·44	12·93 27·02 8·88 10·81 7·53	13·90 21·62 12·55	12·74 13·12 13·90	38·99 31·65 15·05	12·16 11·77 17·37	12·93 17·18 11·77	9·84 12·35 8·88 12·16 14·47	9·07 9·84 6·18	73·34 65·43 32·23 23·55 9·84	5·79 3·47 5·40	4·05 9·84 5·60	16 17 18 19 20
21 22 23 24 25	20·84 18·91	8.88	22.58	22·19 20·27 23·16	8·69 9·46 11·58	11·97 8·49 9·07	13·51 31·07 9·84	11·97 11·97 15·63	10.04	8·69 5·60 8·49	4·44 19·11 12·35 9·46 4·63	4.05	21 22 23 24 25
26 27 28 29 30	5.40		16·41 16·02	9·26 11·19 15·44	12·93 9·65 31·85	11·77 17·76 12·55	16·02 9·26 11·77	7:53 12:16 12:35 9:84 11:19	34·74 16·60	12·74 17·95 5·98 6·37 6·75	17·56 20·27 18·72	19·30 20·46 8·11	26 27 28 29 30
31	6.95	_	10.23		11.77		11.77	13.90		23.16		6.18	31
Mean	11.38	16.92	18.78	15.76	14.24	15.56	12.62	12.76	19.36	17.55	11.30	11.93	
No. of Days used	31	28	31	30	31	30	31	31	30	31	30	31	

MEAN MONTHLY & ANNUAL VALUES OF MAGNETIC DECLINATION, INCLINATION AND HORIZONTAL FORCE.

Means of the results of absolute observations made on the dates shown below.

Inclination

5. Lerwick.

Declination

1923.

Horizontal

Mont	h.	(West).		(N	forth).	Force.	
			,,	- 0			
Jan.		15 50 3	39	72	33.42	14664	L
Feb.	•••			72	33.11	14659	•
	•••		54	72	33.53	14664	
Mar.	•••		6	•		14652	
April	•••		56	72	33.90	14668	
May	•••		58	72	34.05	14655	
June	•••		14	72	34.00	14649	
July	•••	, , .	34	72	33.50	14655	
Aug.	•••	15 44	I	72	33.89		
Sept.	• • • •	3 13	8	72	33.57	14648	
Oct.	•••		58	72	34 · 37	14645	
Nov.	•••	15 41 2	28	72	33 47	14654	
Dec.	•••	15 39 3	35	72	33.27	14645	5
Year		15 44 3	3	72	33.65	14655	<u> </u>
Date	es or	which Ab	solu	te Obs	servation	s were m a	$\frac{de}{}$
				- 6		1, 6, 8, 9,	12
Jan.	• • •	1, 6, 8, 9,			9, 12,15,		
		15, 17,	- 1		23, 25,	15, 17,	-
ļ			31.		31.	25, 29,	-
Feb.	•••	2, 6, 9, 12,	15,		9, 12, 15,	2, 6, 9, 12,	15,
		19, 22.			22.	19, 22.	
Mar.	•••	1, 3, 5, 7,	12,		5, 7, 12,	1, 3, 5, 7,	
1		15, 21,	23,		21, 23,	15, 21,	23,
1		28, 30.			30.	28, 30.	- 6
April	•••	3, 5, 9, 12,	16,		9, 12, 16,	3, 5, 9, 12,	
1 -		19, 24,	26,	19,	24, 26,	19, 24,	20,
1		30.		30.		30.	
May		3, 7, 10,	14,	3, 7,	10, 14,	3, 7, 10,	14,
		21, 24,		21,	24, 26,	21, 24,	26,
		28.		28.		28.	
June		1, 4, 7, 10,	12,	1, 4,	7, 10, 12,	1, 7, 10,	12,
June		17, 21,		17,	21, 23,	17, 23,	26.
		26.	J,	26.		ı	
July		5, 10, 13,	16.	5, 10	, 13, 16,	5, 10, 13,	16,
وسارا	•••		28,		24; 31.	21, 24,	31.
ŀ		31.	,		, ,,		
Aug.		_	14,	2, 7,	10, 14,	2, 7, 10,	14,
mug.	•••		27,		23, 27.	17, 23,	27,
		28.	-,,	-7.	, 3, ,	28.	
Cont			17,	4, 5,	11, 17,	4, 5, 11,	17,
Sept.	•••	20, 24.	٠,,		24.	20, 24.	•
Oat		1, 4, 8, 20,	24		8, 20, 24,	1, 4, 8, 20,	24.
Oct.	•••				29, 31.	29, 31.	•
NT			31. 16,	5, 7,		5, 7, 13,	16,
Nov.	•••	J, 1, J.		3, /, 19,		19, 22,	26.
		<i>z</i> ′'	26.	6, 10		4, 6, 11,	13,
Dec.	•••	1 2	13,			18, 21,	29.
l		18, 21,	29.	21	, 29.	10, 21,	

DIURNAL INEQUALITIES OF THE MAGNETIC DECLINATION.

Departures from mean of the day adjusted for non-cyclic change.

Month	1	I.	G.M.T. 2.	3⋅	4.	5-	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24
and Season	١.	6.	Lerw	ick.				Ι	ECLI	[NAT]	ION ((All L	ays e	хсерt	Feb.	7, 15,	Арr.	23).						19	923.
		_o·71	_o·23	_o·58	_o·33	-0.33	_o·48	-0.33	-0.29	-0.31	+0.62	+1.39	+2.30	+2.66	+2.32	+1.81	+1.37	+o·95	+0·46	-o·33	_o·83	1·95	2.99	-2·74	
Peb. Mar.	•••	-1.18	-1.04	-1.51	-1·62	-1.66	-1.39	-0.42	-0.41	-0.14	+1.22	+2.22	+3.38	+4.13	+3.82	+2·49 +3·71	+2.07	+0.95	+0.02	-0.41	-1.20	-2.22	-2.24	-2·45	-2 -2
April		-1.39	-1.24 -1.01	-2.41	-1.01	-1·95	-2.62	-3.44	-1.74	-1·20 -2·01	+0.40	+2.74	+4.01	+6.56	± 4.94 ± 6.08	+3.71	+3.11	+1.25	+0.03	+0.10	-0.09	-1.02	-2.51	-2·14	_I
J ay		-1.35	-1.13	-2.18	-2.87	-3.46	-3.73	-3.84	-3.25	-2.18	-0.39	+2.15	+4.06	+4.88	+4.67	+3.91	+3.31	+2.45	+1.32	+0.90	+0.30	-0.30	-0.63	-o·78	3 1
une		-0.95	-1.66	-1.00	-2.82	-3.82	-4.28	-4.81	-4.54	-3.46	- I ·O2	+1.81	+4.03	+4.79	+4.82	+4.57	+3.61	+2.91	+1.79	+1.02	十0.73	+0.54	-0.27	-0.27	/ -C
uly ug.	•••	I · 69	-1.09	-2.59	-2.77	-3.01	4·00	-4·17	-3.76	-2.59	-0.91	+1.30	+3.00	+4.74	+4.96	+4·34 +3·64	+3.07	+1.83	+1.71	+1.18	+0.00	+0.09	-0.03	- I · 26	-1
. ~		-3.60	-2.42	-2.52	- 1·98	-1.44	- I·59	-3.92	-2.21	-1.05	+0.04	+3.23	+5·32	+5.74	+4.62	+3.60	+2.42	+1.53	+0.32	-0.09	-0.40	-0.70	-1.90	-2.81	-2
Oct.		-2.38	-2.04	-1.74	-0.77	-o·35	+o·o8	-0.28	-0.72	-0.44	+1.00	+2.76	+4.34	+4.73	+4.28	+3.18	+1.33	-o.18	+0.62	-0.55	-2.11	-2.95	-3.66	-2.50	1-2
lov.		-1.32	-0.41	-0.54	-0.52	-0.23	-0.43	+0.11	-0.01	-0.19	+1.05	+2.01	+2.42	+2.37	+1.85	+1.44	+1.19	+1.16	+0.79	+0.13	-0.68	9.17	-3.01	-2.97	
ec.		1.39	-0.37	-0.19	 	-0.17	-0.14	-0.07	-0.02	+0.01	+0.91	+1.50	+2.20	+2.44	+2.27	+1.78	+0.95	+0.32	4.0.17	-0.40	-1.00	-211		1 9 0	
ear		— I·54	-1.35	-1.66	1·68	-1.82	-2.04	-2:13	−1. 98	-1.30	+0.34	+2.23	+3.90	+ 4 ·56	+4.15	+3.26	+2.27	+1.32	+0.40	+0.13	o·58	-1.22	1.85	1.95	5 -
Vinter		-1.15	-o·59	-0.40	-0.60	−0.60	-0·61	-o·18	-o·18	-0.13	+0.92	+1·8o	+2.60	+2.90	+2.56	+1.88	+1.40	+0.84	+o·36	-0.34	-1.13	-2.06	-2 ·56	-2.53	3 -:
Quinox		-2.26	-1·08	-2.08	-1.65	-1.38	-T·48	-2.02	-2:10	- I ·40	+0.21	+2.78	+4.00	+ 5.67	+4.08	+3.80	+2.37	+1.04	+0.41	-0.13	- I ·04	-1.71	-2.67	-2.54	ļ_:
	1			·		[Ĭ							l	ł	1	}	1	1	1		1	1
ummer		-1.53	-1.49	-2.50	-2.80	-3.47	-4.03	-4·19	-3.67	-2.37	-0.41	+2.10	+4.22	+5.11	+4.90	+4.13	+3.04	+2.00	+1.32	+0.83	+0.43	+0.13	-0.34	-0.79	<u>'</u>
7. L	erw	ick.								DEC	CLINA	ATION	I (Qu	iet Da	ıys).									19	923
		,	· /	, ,	,	· /	, ,	1 ′		i ,	, ,		, ,	1 ′	,	,	, ,	1		<u>'</u>	1 ′	<i>'</i>	,	1	
an.		-0.76	-0.59	-o·43	0.03	0.30	-o·51	-0.63	0.67	o·88	-0.03	+0.80	+1.77	+1.96	+1.75	+0.94	+0.84	+0.61	+0.34	+0.19	-0.38	0.90	-1.13	-1.15	-
eb. Iar.	•••	-0.08 -0.76	-0.56	-0.71	-0.91	-0.91	-1.18	-1.25	- I ·O2	-0.79	+0.21	+1.14	+1.87	+2.30	+2.07	+1.41 +2.38	+0.37	+0.21	+0.21	+0.17	-0.03	-0.14	-0.41	-0.53	2 -
pril		-1.28	- I · 57	-1.65	-1.63	-2.38	-2.56	3.27	-3.75	-2.83	-0.26	+ r · 84	+4.06	+5.12	+4.40	+3.00	+2.00	+1.32	+o.88	1+0.32	+0·22	-0.18	-0·15	-0.78	5
Iay		-0.30	-0.06	- I · 63	-2.65	-3.10	3.00	4-20	-3.66	-2.71	0.80	+2.02	+ 2.72	1 + 4 ⋅ 14	+3.64	1 + 2.85	十2.17	+ 1 ·86	+ I ·69	+I:32	1+0·13	+0.14	1+0.40	1+0.00)
	1	+0.03	-0.00	-2.00	- 3.14	- 3.75	4.20	-1.21	-4.43	- 3.51	- T ·67	+ T :07	1-3.3T	1-1.17	± 4.54	1+ 2.70	+2.83	I+ I · 59	1+0.97	1+0.72	1+0.45	1+0.27	1+0.00	1+0.97	/ -
uly .ug.		-0.40	-0.97	-1.35	-2.16	-3.13	-3.80 4.90	3.96	-3.80	-2.14	-0.79	+1.18	+3.53	+4.54	+4.27	+3.38 +3.35	+1.03	+1.10	+0.71	+0.09	+0.16	+0.13	+0.03	-0.70	
ept.)	-1.31	T : 4 T	- I · 52	- I · 70	-2.TA	-2.62	- 2.17	3.55	2.47	T · T 4	1 T OT	1-4·8T	1-45.50	1.77	1-3.17	1 + 1.00	+0.8I	1+0.02	1+0.49	40.00	-0.33	-0.40	1-0.77	71-
Oct.		- I · O I	-0.82	-0.72	-1.07	T · T 3	-T-12	- T.6T	-1.71	T · AA	1+0.50	1+2.33	+3.10	1-43-25	+2.11	+ I.O3	1-0.22	+0.29	1+0.59	4-0.55	40.01	-0.11	-0.43	-1.05) -
Jov. Jec.		-0.00	-0.60	-0.17	-0.10	0·50	-0.75	-0·83	i — ∩·93	~ 0.73	1-0.37	- T - 40	1.97	I + 1 ⋅83	± 1.06	+0·73 +0·74	1-+0.54	1+0.00	十0.51	140.00	0.23	-0.75	-0.07	1-0.02) —
ec.		-0.07	-0.32	0.30	-0.43	-0.21	-0.57	-0.09	-0.57	-0.30	+0.32	+1.24	+1.71	+1.0%	+1.24	T 0 /4	7.0 40	1 0 40	1040		- /1		'	- /	1
*.o.w			~ 0 =			_ 00			0.40	0	0	- (-				+2.23	1.7.00	L0:70	+0.24	+0.37	+0.01	-0.11	-0.34	0:40	
ear		-0.72	-0.92	1.11	-1.40	-1.99	-2.27	-2.49	-2.49	-1.78	-0.28	+1.02	+3.10	+3.12	+ 3.24	+2-23	71 29	70 /9	1 0 34	1 9 37	,			- 49	1
Vinter		-0.70	-0·52	-0.42	-0.39	o·55	-0.75	-o·85	_o·8o	-0.69	+0.22	+1.17	+1.83	+1·98	+ 1·53	+0.96	+0.54	+0.46	+0.29	+0.06	-o·35	o·55	−0.75	-0.79	-
						1	1	t		1	1		1	1	l	+2.40		1	1		1	1		1	
	i		!			ł	i	1	i	Į.		1	i	i			1		!	1		1			1
ummer		-0.38	-0.88	-1.71	-2.00	-3.30	-4·o5	-4·10	-3.82	-2.46	-0.40	+1.79	+3.85	+4.68	+4.34	+3.34	+ 2.21	7 34	1009	1 77	1 0 33	1 0 39	0 30	011	
8. L	erwi	ick.							1	DECL	INAT	ION	(Distr	irbed .	Days)									19	923
		′			′	,	,	'	,	,	ı '	,	,	· /	,	1 , , ,,,,	1	,	1,	1	1	,,,,,,	6,06	6.40	
an. eb		-0.30	0 : 4 4	4.22	- 4.00	- 2.24	1. 2.45	O.O.T	1 T.OO	1 0.74	1 4.50	1 4	1	1 63 • '7' 7	ユーエ・スク	+3·70 +2·01	1-4-3·40	10.00	3.10	1 OO	1 2 33	- 33	1 5 45	-4 UI	
eb. .ar.																									
pril		-2.00	T.TO		_ 2.c×	1 0.67	T ./7	2.11	2.00	2.17	0.41	1 2.02	1 6.42	1'7.Us		1 - U.U.3	1-+ 3.07	1-0-5/	T-0 /0	0 20	. ~ ~.)				,,
ay	1	2.27	7.40	4.80	62.112		5.00	68	4.50	T	1 1 0	1 2	1 6×	1 1 6 · XX		1-1-7-54	()·()()	5 74	T 1 70	1 1 40	009	1 1.19	000	1 17	, –
ine	- 1	-2.39	-4.50	-6.80	-4.42	-5.29	-3.67	-3.61	-2.86	-1.79	-0.15	+3.03	+5.02	+4·73	+4·71	+5.89	+4.17	+3.24	+3.28	+1.62	+1.18	+0.79	+1.18	-0.73	3 -
uly ug.	- 1	T • 77 T	T +O 4	2 · 2 T	2.54	4.774	5.00	F .O.T	2.16	0.40	1 1 x	1 1 4.60	1 6.51	1 6.04	L 5.62	1-62	1 + 2.01	1 - 1 - 70	T T 1 / 1	T 1 U)	- 0 92	5 00	2 0.3	- 2 94	_
ept.		_11.56	- 5.40	- 2.02	r · S ɔ	1-2.OI	LACOT	-0.2T	110.05	1.1 1.16	1 2.72	116.01	1 7.01	ı.⊥.g.∩a	1 5 · X7	1-6.00	14.01	-+ 4.40	-0.07		- 4 10		-5 1/	TT .00	,
ct.		c · XX	4 · X 2	2.07	上つ・こん	1 - 2 - 0.7	1-6.22	1 - 5.63	1 - 2 · 4 ×	1-2.60	1.2.48	1.166	1. 1. 6. X7	上ん・ます		I - h·XII	1-1.50		1-0.34	7 29	9 14	10 91	70 00		SI —
ov. ec.		1 2.TV	0.~1	2.05	1.20	0.87	1 0.22	1 1 0.80	1 1 7	110.06	1 7.50	110.60	1 0.50	1 2.82	1 2.00	+3·18 +3·29	1-1-2:20	12.72	1 + 2 4 5		0 02	1 4 .)7	0 00	4 / 1	· -
			}		ļ		ļ																		
ear	•••	-3.19	-1.96	-2.98	-2.22	-1.35	- I·34	-1.14	-o·81	-0.26	+1.29	+3.45	+5.25	+5.97	+5.20	+5.12	+3.73	+2.13	+0.90	-0· 4 7	-2.28	-3.19	-4·2 9	4·48	-
		-1.33	-o·13	-1.70	-1.13	-o·80	0-0.51	+1.28	+1.07	+0.92	+1.01	+2.65	+3.42	+ 4 ·05	+3.29	+3.05	+2.44	+1.27	+0.30	_o·86	-2.90	4.04	-4·67	-4·53	-
Vinter																									
	τ	-5.21	-2.96	-3.27	- r·08	+1.34	1-10	+o.10	-0.07	+0.00	+ I .OU	1·57	+6·X∩I	/·nn	+0"/		T4 00	1 0 00	_	1	1 3	7 7/1	- 10		í
Vinter Equino x Summer			-2.96													+6·08									

DIURNAL INEQUALITIES OF THE HORIZONTAL MAGNETIC FORCE.

Departures from mean of the day adjusted for non-cyclic change.

Month	Hour.	G.M.T. 2. 3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.
and Season.	9.	Lerwick.		Н	ORIZ	CONT	AL F	ORCE	E (All	Day	s exce ₁	bt Fel	. 15,	Αþr	23, N	ov 21-	-26, 2	8, 30)	•	1	1	1	923.
Feb Mar April May June July Aug Oct Nov	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccc} - & 6 \cdot 1 & - & 2 \\ - & 5 \cdot 7 & - & 5 \\ + & 3 \cdot 7 & + & 1 \\ - & 4 \cdot 5 & 0 \end{array} $	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1 + 3.6 1 + 5.4 1 + 0.4 1 - 1.0 1 + 4.6 1 + 4.5 1 + 5.2 1 + 5.2	+ 8.6 + 5.9 + 7.4 - 0.2 - 2.7 - 1.0 - 0.3 + 3.8 + 5.7	+ 7·3 + 4·4 + 2·8 - 5·0 - 5·0 - 5·9 + 1·6 + 7·8 + 4·9	+ 3.8 + 0.4 - 5.5 - 11.6 - 14.1 - 10.8 - 12.8 - 4.2 + 1.6 + 1.7	- 1.9 - 5.8 -15.7 -18.6 -21.0 -16.4 -19.3 -11.9 - 7.2 - 4.3	- 8.8 - 13.5 - 26.9 - 24.0 - 27.9 - 19.5 - 25.2 - 18.8 - 11.8 - 6.7	-9.2 -17.1 -30.5 -24.8 -29.8 -19.8 -12.5 -7.9	-10.2 -14.7 -25.9 -19.3 -23.2 -17.6 -19.2 -16.0 -9.2 -5.6	- 6.9 - 9.5 - 17.7 - 12.9 - 13.1 - 10.2 - 10.9 - 9.3 - 4.6 - 3.0	- 1.5 - 3.4 - 6.8 - 5.1 - 2.7 - 3.2 - 1.3 - 0.4 - 0.9	+ 1.6 + 4.4 - 1.1 + 2.7 + 9.5 - 0.5 + 4.3 + 7.1 + 0.7	+ 3·8 + 8·1 + 3·1 + 8·4 + 15·5 + 5·1 + 7·4 + 10·4 + 0·3	+ 5.0 +11.2 +11.4 +17.9 +23.0 +10.6 +10.7 +12.5 +10.1 + 1.2	+ 5.5 + 8.7 + 14.3 + 27.8 + 24.7 + 17.6 + 13.7 + 15.5 + 10.9 + 1.9	+ 4·8 + 9·9 +16·1 +23·4 +22·2 +20·6 +15·7 +12·6 + 6·3 + 2·1	+ 1·3 + 8·9 + 15·5 + 17·4 + 19·4 + 18·4 + 15·7 + 12·9 + 2·7 + 2·2	+ 3.6 + 5.9 + 12.4 + 12.6 + 14.8 + 13.8 + 11.1) + 9.5 - 1.3 + 2.2	6 + 1.6 $0 + 4.1$ $1 + 12.5$ $0 + 9.4$ $0 + 8.6$ $0 + 8.6$ $0 + 10.4$ $0 + 9.2$ $0 + 6.6$ $0 + 6.6$ $0 + 6.6$	γ 4 + 0·2 5 - 1·2 5 + 7·2 4 + 7·2 6 + 7·2 6 + 4·5 6 - 10·5 1 - 0·6	7 4 - 7.9 4 - 7.9 4 + 7.2 4 + 1.1 4 + 5.8 5 + 4.3 5 + 6.6 0 + 1.4 8 - 8.0 6 - 0.3
Winter	– o·8	- 2·0 - I - 3·3 - I - I·4 - I	.3 + 1.	+ 4.4	+ 6.3	+ 5.5	+ 3.1	- I·4	- 4·8	— 6 ·3	_ 6·o	- 3·7	- o·4	+ 1.3	+ 1.8	+ 2.0	+ 1.9	+ 1.9	+ o·3	3 + 1.4	+ o·3	3 - 0.6	6 - 2.6
Summer	+ o·8	- I·2 - o	·4 - o·	+ 0.7	- 1 ·1	— 6·o	-12.3	—18·8	-24.2	-25.0	19.8	— II·8	- 3.1	+ 4.0	+ 9.1	+15.5	+21.0	+20.5	+17.7	+13.1	+ 9.4	1 + 7.	7 + 4.4
HORIZONTAL FORCE (Quiet Days). 10. Lerwick.													923.										
Feb. Mar. April May June July Aug. Sept. Oct. Nov. Dec.	+ 3·2 + 6·1 + 3·0 + 2·1 + 2·1 + 4·3 + 6·5 + 3·8 + 0·5 - 2·4 + 2·7 - 0·3 + 4·9	+ 4.4 + 4	·0 + 2· ·8 + 3· ·8 + 3· ·9 + 5· ·3 + 2· ·2 + 5· ·2 + 3· ·7 + 3· ·5 + 3· ·7 + 3· ·1 + 4·	1 + 3·3 1 + 3·7 0 + 5·8 5 5 + 2·4 4 + 4·1 8 + 2·4 2 + 3·3 9 + 2·9 4 + 2·5 1 + 3·5 3 + 2·9 3 + 4·5	+ 5·3 + 5·3 + 4·5 + 1·9 + 1·1 - 2·2 + 2·1 + 5·7 + 4·6 + 2·8 + 3·0 + 3·8 + 4·6	+ 5·2 + 5·3 + 1·2 - 2·4 - 3·4 - 5·9 - 1·8 + 2·9 + 3·7 + 1·6 + 0·8 + 3·3 + 2·5	+ 2·2 + 2·8 - 7·8 - 8·9 - 9·4 - 10·1 - 7·5 - 3·7 - 2·4 + 1·8 + 1·3 - 2·8	- 3.5 - 2.4 - 17.9 - 16.2 - 15.1 - 17.3 - 15.6 - 11.0 - 10.1 - 5.1 - 0.5 - 9.6 - 2.4 - 10.4	- 8·5 - 7·7 - 26·5 - 22·1 - 23·7 - 19·8 - 22·8 - 20·5 - 14·3 - 6·3 - 0·1 - 14·6 - 4·4 - 17·2	-11·7 -14·3 -12·6 -25·9 -27·1 -19·7 -25·2 -23·5 -18·6 -0·3 -17·1 -6·0 -20·7	-11·0 -15·2 -24·3 -23·0 -23·2 -14·7 -23·6 -21·4 -15·5 -7·0 -2·6 -15·2 -5·8	- 8.7 - 12.0 - 15.8 - 13.9 - 15.9 - 8.0 - 14.5 - 15.2 - 8.5 - 2.2 - 10.0	- 4·8 - 7·2 - 6·8 - 6·8 - 7·9 - 2·8 - 6·0 - 8·4 - 2·5 - 0·7 - 4·9 - 1·8	- 1.5 - 1.8 + 0.6 - 0.4 + 1.0 - 0.8 - 0.1 - 3.7 - 3.3 + 0.1 + 1.4 - 0.7 + 0.1 - 2.0	+ 0·7 - 0·7 + 6·6 + 7·4 + 0·8 + 6·2 - 1·6 - 1·6 + 1·8 + 2·3 + 0·8 + 1·1	+ 3·2 + 2·1 + 9·8 + 10·5 + 14·1 + 5·8 + 11·7 + 3·4 + 4·1 + 2·1 + 2·5 + 5·8 + 2·1 + 4·8	+ 3.9 + 2.6 + 12.0 + 16.3 + 16.3 + 10.1 + 13.2 + 6.5 + 6.5 + 1.7 + 7.8 + 2.5 + 6.9	+ 4·6 + 3·9 + 15·5 + 20·0 + 15·5 + 15·6 + 14·0 + 7·9 + 1·0 + 9·3 + 2·7 + 9·0	+ 4.3 + 4.8 + 14.0 + 15.8 + 15.8 + 14.9 + 11.4 + 7.5 + 2.5 - 0.4 + 8.8 + 1.5 + 4.5	8 + 4:2 8 + 5:0 9 + 11:5 8 + 12:5 1 + 13:1 1 + 11:9 1 + 12:5 1 + 7:5 1 + 1:3 1 + 7:5 1 + 1:3 1 + 8:5	2 + 3:2 2 + 3:2 5 + 9:7 7 + 9:7 7 + 9:8 5 + 9:3 7 + 11:5 6 + 6:4 3 + 1:2 6 + 8:5	2 + 2··································	7 + 1·8 9 + 4·5 1 + 6·4 2 2 + 6·4 2 2 + 6·4 2 2 + 6·5 5 + 7·4 7 + 8·7 3 + 5·3 4 + 4·4 1 + 0·1 1 + 6·7
11. Lerw	ick.						HOR	IZON	TAL	FOR	CE (I	Disturl	oed D	ays).							-	1	923.
Mar April May June July Aug Sept Oct Nov Dec	0.0 -50.0 + 1.8 - 30.4 - 9.0 - 9.9 + 4.7 -65.7 - 15.2 - 2.3 + 4.3	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	9 + 1··· 1 0··· 3 - 14··· 5 - 10·· 9 - 8·· 5 - 12·· 5 - 10·· 4 - 1·· 5 - 2·· 3 + 4·· 5 - 2·· 3 + 4·· 5 - 2·· 5 - 10·· 5 - 2·· 3 + 4·· 5 - 2·· 5 - 10·· 5 - 2·· 5 - 10·· 5 - 2·· 5 - 10·· 5 - 2·· 5 - 10··	0 + 10·8 8 - 7·0 0 - 5·3 9 - 9·8 7 - 4·0 7 - 8·1 3 + 5·3 6 + 2·3 7 + 8·7 7 + 7·4	+11.4 + 5.7 + 8.2 - 5.8 - 6.6 + 2.3 - 1.1 + 5.9 + 8.4 + 7.4	+6.5 $+0.8$ $+0.8$ -14.2 -20.5 -5.4 -15.0 $+8.5$ $+22.0$ $+7.5$	$\begin{array}{c} + \ 3 \cdot 2 \\ - \ 3 \cdot 0 \\ - \ 10 \cdot 4 \\ - \ 23 \cdot 4 \\ - \ 26 \cdot 9 \\ - \ 13 \cdot 9 \\ - \ 23 \cdot 2 \\ + \ 10 \cdot 9 \\ + \ 17 \cdot 7 \\ + \ 6 \cdot 3 \\ + \ 7 \cdot 2 \end{array}$	$\begin{array}{c} -7.3 \\ -8.2 \\ -18.8 \\ -34.2 \\ -31.0 \\ -19.4 \\ -20.6 \\ +5.2 \\ +8.3 \\ -3.2 \\ +5.3 \end{array}$	-22·2 -16·1 -28·5 -36·7 -39·7 -19·1 -26·0 - 3·8 + 7·4 - 8·9 - 3·9	- 8·8 - 18·0 - 36·7 - 29·6 - 38·9 - 17·9 - 27·7 - 4·8 + 15·4 - 10·0 - 8·2	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	+ 1.7 + 0.8 - 15.1 - 6.3 - 12.6 - 11.4 - 7.0 + 6.4 + 31.7 - 4.5 - 5.3	+ 8·3 +10·4 + 3·5 +12·9 + 4·6 4·0 + 4·8 +22·2 +30·2 2·7 3·3	+ 12·0 + 32·6 + 4·5 + 24·8 + 34·4 + 2·2 + 8·2 + 47·4 + 1·5 - 1·3	$ \begin{array}{r} + 19 \cdot 3 \\ + 45 \cdot 9 \\ + 9 \cdot 1 \\ + 20 \cdot 6 \\ + 47 \cdot 5 \\ + 12 \cdot 1 \\ + 7 \cdot 2 \\ + 27 \cdot 3 \\ + 53 \cdot 0 \\ - 0 \cdot 9 \\ - 0 \cdot 5 \end{array} $	+24·2 +60·7 +28·6 +48·1 +66·5 +18·5 +11·2 +48·1 +42·6 - 1·4 - 4·4	+22·2 +34·4 +25·6 +73·1 +57·0 +34·7 +18·1 +48·7 +0·4 -0·3	+17.6 $+27.4$ $+28.4$ $+37.0$ $+31.7$ $+36.8$ $+21.0$ $+21.9$ -0.4 -2.2 -0.1	+ 5.1 $+ 23.3$ $+ 24.0$ $+ 21.4$ $+ 23.0$ $+ 26.4$ $+ 17.6$ $- 16.0$ $+ 0.6$ $- 5.0$	+ 8.6 - 1.1 +17.5 +19.6 +15.6 +18.3 +10.4 + 5.8 -33.4 + 5.4 + 1.4	+ 0.9 - 5.4 + 15.7 + 10.8 - 2.7 + 12.1 + 9.9 - 50.6 - 71.3 + 1.4 - 4.0	γ - 0·8 - 16·8 - 19·7 + 5·4 + 10·3 + 4·9 - 19·1 - 91·8 - 3·4 + 0·9	7 3 - 5·3 3 - 43·9 7 + 1·9 1 - 0·9 9 + 1·8 3 + 4·9 9 + 4·4 - 33·9 8 - 71·7 1 - 0·6 9 + 1·3
Winter	– o·8 – 32·3	-29.2 -26	·7 + o·	$\frac{1}{6} + \frac{1}{3}$	+ 8 ·7 + 4·7	+ 6·8 + 8·o	+ 6·1 + 3·8	- 0·5 - 3·4	- 8·8 -10·2	- 7·6	- 5·1	- 2·0 + 6·0	+ 1.3	+ 3·7 +28·6	+ 5·5 +33·8	+ 5·3 + 45·0	+ 4·5 +36·0	+ 3.2	+ 0·1	+ 4·0 - 2·8	- 0·4	5·o	- 12·1 - 25· 9

AURORAL LOG.

12. Lerwick.

1923.

Date.	Month.	Date.	Month.	Date.	Month.	Date.	Month.
	January.		March.		September.		November.
2 6 8 9 10 11 12 14	Moonlight. Showers. Showers.	18 <u>Ш</u> 19 20 21 <u>Ш</u> 22 23 25 26	Diffuse glow.	10 11 12 14 18 20 21 24 28	But reported to have been seen in Shetland. Moonlight. Moonlight. Moonlight. Showers.	3 4 5 6 7 9 16 19	Showers. Showers. Showers. Moonlight.
17 18 19 20 22 <u>Щ</u>	Showers. Showers. Faint glow.	3 4 5 8 兴 9 兴	April. Glow. Glow.		October.	23 25 28 29 30	Moonlight. Moonlight. Showers. Showers.
5 14 15 22 24	February. Showers. Showers. Showers.	10 W 16 17 18 22 W 23 24 26	Faint. Showers. Glow 22.00-23.00. Moonlight.	1 2 3 4 7 10 W	Showers. Glow 20·00-01·00. Faint glow.	3 4 5 8 II I2	December. Showers.
4 5 6 7 8 9 11 13 14 <u>W</u>	March. Moonlight. Showers. Showers. Showers. Showers. Bright 21.00-00.30.*	27 28 29 2 4 7 9	Moonlight. Moonlight. Moonlight. September. Reported elsewhere in Shetland, but not seen at Observatory.	10	Faint glow. Faint glow. Bright 19·00-20·30.* Showers. Moonlight. Moonlight, showers. Moonlight. Showers. Showers.	13 14 17 19 20 22 23 24 25 26 27 28 <u>Ш</u>	Rain. Showers. Moonlight, showers. Moonlight. Moonlight. Moonlight. Moonlight. Moonlight. Woonlight.

In the interests of brevity there have been omitted from the table above all dates on which the sky throughout the evening remained completely overcast and on which, therefore, no opportunity arose of determining whether or not aurora occurred. The nights on which aurora was actually seen are indicated by the symbol $\underline{\mathbf{w}}$. The nights on which aurora was not seen, despite, at least an occasional interval of more or less clear sky are indicated by the symbol ...; in the latter case also, remarks on the weather are added to assist the reader in judging how far the fact of no observation of aurora may be taken as indicating that there was not actual aurora. An asterisk (*) after any date indicates that a full description is available of the auroral phenomena observed on the date in question.

M.O. 279 (Aberdeen)

Air Ministry METEOROLOGICAL OFFICE

THE OBSERVATORIES' YEAR BOOK 1923

Comprising the results obtained from autographic records and eye observations at the observatories at Lerwick, Aberdeen, Eskdalemuir, Cahirciveen (Valencia Observatory), Richmond (Kew Observatory), and Benson.

ABERDEEN

Published by the authority of the METEOROLOGICAL COMMITTEE



LONDON:

ABERDEEN OBSERVATORY.

Latitude						57° 10′N.
Longitude						2° 6′W
G.M.T. of L				• •		12h. 8m.
	Heights	in me	tres abo	ve Sea-	Level.	
Barometer						26.8
Rain-gauge						14.0
Robinson Co	up Ane	mogra	ph			37
Dines Tube	Ânemo	graph	• •		• •	21
	Height	s in m	etres ab	ove g r o	und.	
Thermomete	er Bulb	s, Nor	th Wall	Screen	١	12.5
Sunshine Re	ecorder					20.7
Robinson Co	up Ane	mogra	ph			23
Dines Tube	Ânemo	ograph	• • •			13

INTRODUCTION.

SITE.

The Observatory which was established in 1868 is housed in the top floor of the Cromwell Tower of King's College in Old Aberdeen. The College lies on a plain gradually rising from the sea from which it is distant about I mile (I·6 km). There are no serious irregularities of surface in the vicinity excepting the two river valleys of the Don and the Dee. To the north, at a distance of about 1 km. the Don flows eastwards to the sea; the Dee flows into the sea at a distance of about 3 km. to the southeast of the College. Between the college and the sea is a golf course covered for the most part with grass. Westwards is the High Street of the Old Town and beyond this there is another street. Further west grass pasture extends for about one kilo-Southward are some open spaces beyond which the modern town is reached. The enclosure in which the Stevenson screen, the Beckley and check rain-gauges and the grass minimum thermometer are exposed, lies to the north-east of the Observatory The "North-wall" screen in which the recording at a distance of about 50 metres. thermometers are exposed is erected on the wall outside the north window of the uppermost story of the Observatory. The nature of the soil and sub-soil is loam and sand.

The plan in Fig. 6 shows the position of the Observatory relative to the City of Aberdeen, and the plan in Fig. 7 shows the arrangement of the College buildings and the positions therein of the Observatory Tower and the screen enclosure. The photographs given include:—

Fig. 8, view of the Observatory Tower, as seen from N.E.

Fig. 9, screen and rain-gauge enclosure from S.S.W.

METEOROLOGY.

The elements dealt with in the following tables are:—Atmospheric pressure, air temperature, humidity, rainfall, sunshine, wind speed and direction, earth temperature and minimum temperature on the grass, together with a diary of cloud and weather.

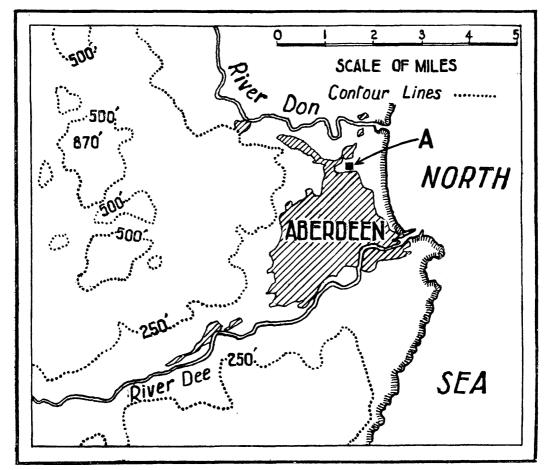


Fig. 6. A shows position of Observatory. Shaded areas represent the City of Aberdeen. Figures indicate heights in feet above M.S.L.

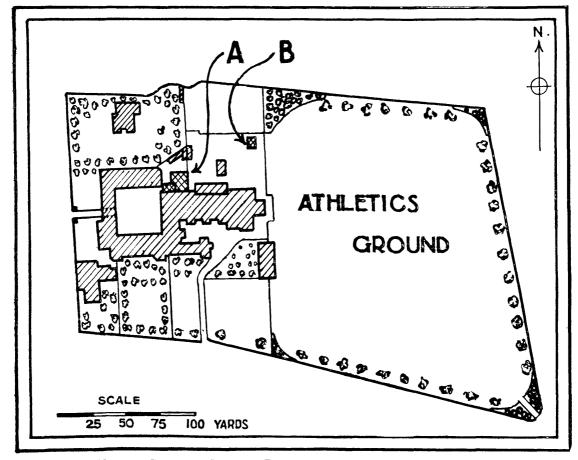


Fig. 7.—Plan of College Buildings. A is Observatory Tower. B is Stevenson Screen enclosure.

ABERDEEN OBSERVATORY.



Fig. 8. Observatory Tower (seen from N.E.)

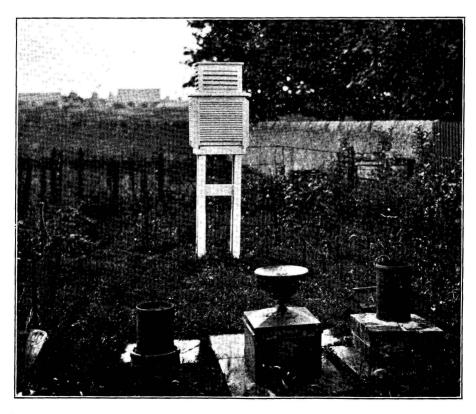


Fig. 9. Stevenson Screen and Raingauge Enclosure (seen from S.S.W.)

The instruments from which values of the above elements have been obtained and the methods of tabulating the records are described in the General Introduction to this volume. The following additional information refers especially to Aberdeen.

Pressure and Temperature.—The barograph, standard Kew barometer and thermograph are housed in the uppermost story of the Observatory (see Fig. 8). The pressure scale value of the barogram is 1 mm. on the paper = 0.85 mb., when the paper is at normal atmospheric humidity. In similar circumstances the time scale is 9.3 mm. = 1 hour. The records of the photobarograph are standardised by means of control readings taken from Fortin Standard Barometer M.O. 273.

The recording thermometers are placed in the North-wall screen already referred to. The scale value of the wet bulb thermograph record is 1° absolute = $3 \cdot 20$ millimetres on the paper; for the dry bulb thermograph the scale value varies slightly with the temperature but is approximately 1° absolute = $3 \cdot 4$ millimetres. The time scale is 1 hour = $9 \cdot 23$ millimetres. Reading of the photothermograms is done by means of glass measuring scales, the records being standardised by control readings from Standard Thermometers M.O. 1698 (dry bulb) and M.O. 1697 (wet bulb). The heights of the barometer cisterns and of the bulbs of the thermometers are given at the top of the appropriate tables.

Rainfall.—The recording instrument in use is Beckley rain-gauge No. 2 with an area of IOI I square inches (653 cm².). The procedure adopted in tabulating the records is similar to that described in the General Introduction and calls for no comment. Control is by check gauge M.O. 167.

Humidity.—On those occasions when the temperature of the wet bulb has been 273a or under, the relative humidity has been obtained from the records of a hair hygrograph (M.O. 35). This instrument is accommodated in a small louvred screen which rests on top of the Stevenson screen and is securely fixed to it. The hygrograph is II·6 metres below the level of the thermograph bulbs in the North-wall screen, and in using its records an appropriate adjustment is made.

Sunshine.—The sunshine recorder (Campbell Stokes type, M.O. 32) is exposed on the small circular tower on the Observatory roof on which the Robinson Cup Anemograph is erected. It is rigidly held by lead flaps soldered to the lead roof. The exposure is excellent, the only obstruction is a flagpole to the east, of angular diameter about 1°, which may obstruct o·I hr. record about 7h between April and September. The "possible" duration of sunshine has been computed from the mean solar declination for the four years 1849, 1850, 1851, and 1852.

Wind Speed and Direction.—The Robinson cup anemograph (M.O. 50) is erected on the top of a small cylindrical tower which rises about fifteen feet (4.6 m.) above the main square tower and about five feet $(\mathfrak{r} \cdot \mathfrak{5} \text{ m.})$ above a smaller tower at the south-west corner of the main tower. The height of the cups above this smaller square tower (which may for the purpose be regarded as the "roof" of the building) is about 4 metres. Owing to the surrounding buildings the exposure of the instrument is a very gusty one, particularly towards south and west.

There is also in use a Dines Tube Anemograph (M.O. 1011), which is mounted in a more open exposure in a field about $\frac{1}{2}$ km. east of the Observatory. The speeds given in Tables 83–94 are those obtained from the Cup Anemograph, but the directions are taken from the records of the Tube instrument, as are also the particulars of the highest gust each day and the annual table of distribution of wind speed given in Tables 95–96.

A careful analysis of simultaneous records of the two anemographs* has shown that the directions recorded by the two instruments differ only very slightly; but the values of velocity show considerable differences. Those recorded by the tube

instrument exceed those recorded by the Cup Anemograph by between 10 and 30 per cent., depending upon the direction of the wind. This fact must therefore be borne in mind in using the values entered in Table 96 giving the annual distribution of wind speed. The monthly tables of hourly values are obtained from the Cup Anemograph velocities, in order to maintain continuity with previous years' publications.

Temperature in the Ground.—This is recorded by a thermometer (unnumbered), which is kept at a depth of 124 cm. (four feet). At Aberdeen the thermometer is carried in a slot near the end of a long bar of wood, about three inches (7·5 cm.) square in section. This bar fits closely into a wooden sleeve, sunk vertically into the earth, so that the bulb of the thermometer is at the required depth. The thermometer itself is enclosed in a glass tube, and its bulb is embedded in paraffin wax so as to render the thermometer insensible to sudden changes of temperature. This allows of its being drawn to the surface and read before the temperature of the bulb has time to change appreciably. As underground temperature changes very slowly, the loss of sensitiveness, resulting from the coating of wax, does not lead to inaccuracies in the determination of the temperature of the earth. The thermometer is read at 9h each morning.

Minimum Temperature on the Grass.—The grass minimum thermometer (M.O. 17007) is exposed in the enclosure on two wooden pegs about 4 cm. above grass. It is set at 18h and read at 7h, the reading being entered to the day of observation.

13.	Aberd	een :	H_b	(heig	ght o	f bar	omet	er cis	tern	abov	ve M.	S.L.)	=2	£6·8 1	metre	es.							Ja	nuar	y, 19	23.
Ι	Day.	ı.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noor	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mea
1		mb.		mb.		mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb
[1	996∙0	996.7	997.1	997.7	998.8	999.4	1000-3	000.0	9.100	002.5	002.5	002.8	003.1	003.3	003.5	004.3	004.3	004.4	004.2	004.2	003.5	002.8	002.4	001.5	100
- [2	000.1	998.8	3 997•1	1995·c	993.2	991.6	989.8	987.9	j986∙ <u>5</u>	i 984·9	984.1	984·c	1984.3	984.1	983.7	983.1	981.8	981.4	. 980∙0	979.1	978.5	977.6	977.0	976.9	986
i	3	976.7	977:2	977.6	978-1	978.7	978.9	980.1	980.7	981.7	983.2	983.4	984∙c	984.2	984.4	985.1	986.1	987.6	988.9	990.4	991.7	993.6	995.0	996.2	997.5	984
- !	4	998.5	000.3	3001.5	002.0	004.3	005.4	1006.6	007.8	000.1	010.3	010.8	011.5	011.7	011.7	012.2	012.2	011.8	012.0	011.8	011.7	011.2	010.2	009.6	009.5	008
	5	007.2	005.8	004.0	003.7	002.9	000.1	999.3	998.7	996.8	995.9	994.5	993.2	991.9	991.4	991.6	991.7	992.7	993.4	994.2	994.9	995.9	997.0	997.8	998.3	997
İ	6	999.1	999.7	000-3	000∙€	001.0	001.2	002.2	003.1	004.2	005.1	005.5	005.9	006.6	007:3	007.7	008-3	008.3	008.3	008.2	008∙0	007.8	007.3	006.3	005.6	004
	7 8	004.7	003.7	002.6	001.1	000.0	999.4	998•4	998.6	998.6	998.7	998.8	998.3	997.6	997.5	997.1	997.1	996.5	996.0	995.6	995.5	995.3	994.8	994.2	993.4	998
		993.0	992.1	990.0	991.4	992.0	993.4	995.1	996.5	997.8	998.9	999.8	000.0	001.5	002.2	002.6	003.6	004.6	004.9	005.4	005.7	005.5	005.4	004 I	002 8	999
İ	9	001.0	999.6	995.8	994.6	993.1	991.6	991.2	99 <u>i</u> .2	991.5	991.2	990.8	989.1	987.9	986.8	986.0	985.5	985.3	985∙0	984.2	982.5	981.3	979:5	978.7	977:4	1988
	10	975.1	974.9	974:3	973.7	973:5	973.6	975.0	976.3	977.1	978.1	979.7	 981.0	982.2	984.2	985.5	986.7	987.9	990.0	991.3	991.8	991.7	992.5	992.9	993.4	1982
	11	994.2	994.6	995.2	995.4	996.0	996.3	996.9	997.1	997.2	997.0	999.2	000.3	001.6	003.2	004.5	005.7	006.7	007.5	008.6	009.4	010.1	010.7	011.5	011.9	001
<u> </u>	12	012.1	012.5	013.3	013.2	014.1	014.8	015.3	016.0	016.4	016.6	017.5	017.7	017.9	018.0	018.2	018.7	010.0	019.2	019.6	020.0	020.0	019.8	019.7	019.6	016
Level	13	019.0	019.1	018.0	0.810	017.4	016.2	016.5	016.0	014.2	013.4	011.7	010.4	009.5	000.0	008.7	008.5	008.5	008.7	008.6	008.5	008.4	007.6	007.3	006.8	012
é	. 14	005.8	005.0	003.0	001.9	000.1	000.2	000.0	002.8	004.3	004.8	005.7	006.1	006.3	006.5	007.3	007.3	007.4	007.6	007.8	008.2	008.0	008.4	008.4	008.5	00
Н	15	009.3	009-9	010.1	010.8	011.7	012.4	012.8	012.9	014.0	014.8	015.6	015.7	010.1	010.2	010.8	017.3	018.5	018.0	019.2	019.7	020 4	021.1	021.5	022.3	015
Station	16	022.7	022.8	023.2	023.6	024.0	024.3	025.0	025.4	025.7	025.7	025.9	025.5	025.3	025.1	025.1	024.9	024.9	024.7	024.9	024.8	024.8	024.5	024.5	024.0	024
:ặ	17	023.5	023.3	023.2	022.8	022.6	022.6	022.9	023.2	023.3	023.2	023.3	022.7	022.3	022.2	022.3	022.4	022.6	022.7	023.0	023.3	023.2	023.2	023.3	023.6	023
ta	18	023.8	024.5	024.5	024.4	024.8	024.9	025.3	026.2	026.7	026.9	027.1	027.2	027.0	026.8	026.2	026.4	025.7	025.0	024.9	024.6	024.1	022.9	024.0	023.7	028
S	19 20	023.8	023.8	024.0	022.8	022.4	020.8	019.6	018.4	017.2	013.8	011.2	007.7	004.3	003.0	001.7	001.9	002.4	002.6	002.8	002.5	002.5	003.0	003.3	003.5	011
	20	003.9	003.4	002.0	002.3	003.5	003.7	004.4	007.0	1009.4	011.4	012.5	013.9	015.0	010.1	017.0	010.3	019.0	019.0	020.0	020.9	020.0	020.3	020.4	02.04	012
	21										014.5															
	22	012.4	012.6	012.3	012.1	011.0	011.5	010.0	010.2	010.1	010.3	010.5	010.9	011.3	012.0	012.7	013.5	014.8	016.2	010.9	018.8	020 6	021.7	022.2	023.6	013
- 1	23										025.5															
1	24	011.3	011.5	012.1	012.1	012.9	012.0	013.2	014.5	015.2	015.8	010.0	010.2	010.2	010.5	017.1	017.0	010.2	019.9	019.9	020.2	020.0	021.1	021.5	021.7	010
İ	25	021-9	022.2	022.0	022.7	022-9	023.1	023.4	023.0	024.1	024.3	023.9	022.5	022.0	021.3	020-0	021.3	021.3	021.2	021.2	021.5	021.3	020-8	020.5	020.0	02.
	26										021.1															
1	27 28	015.2	014.5	014.3	013.0	012.0	011.5	010.8	010.2	010.3	010.3	010.1	010.0	010.5	010.8	011.0	011.5	012.0	012.8	013.0	013.6	014.1	014.2	014.2	015.0	01:
1		015.2	015.5	015.0	015.8	015.8	015.8	010.0	010.3	010.5	016.8	010.9	010.0	010.5	015.7	015.4	014.4	014.0	013.4	013.1	012.3	011.8	011.1	010.0	009.9	012
1	29 30										006·5															
1	30	012.7	012.7	0127	012 0	012 5	012 4	012 0	011.0	011 3	0111	010 0	010.3	009.7	0091	1.00 4	00, 0	007.2	0071	000 3	000.0	000 0	003 0	003 0	000 4	٥٥٥
₩	31	006.8	007:3	007.5	008.6	008.2	007.7	007.9	007.9	007.7	006.9	006.6	005.7	004.6	003.3	001.7	000.5	999.9	999:4	998.0	997:3	996.5	995.3	994.1	993.6	003
ean		1008	1008	1008	1007	1007	1007	1007	1008	1008	1008	1008	1008	1008	1007	1008	1008	1008	1008	1008	1008	1008	1008	1008	1008	10
tatio	n level)	·37	•32		∙86	.75	∙57	.74	•05	•29	.37	·41	٠16	-04	•99	•00	.20	·43	.62	.73	.76	⋅82	⋅6 8	•59	•52	<u>ا</u> ــا
ean	1\	1011									1011															
ea le		-69	·64	<u> </u>			·89	•06	•37	·6 1	•68	•72	*47	*34	•2 9	•30	.51	•74	•93	•04	.07	·13	•99l	•90		•
14.	Aberde	en:	Hb =	26.8	met	res.																	repi	ruary	, 19	23.
1											mb.															
1	-	1000.5	000.4	002.2	1002.8	002.0	00444	004.0	005.2	005.0	006.1	006.1	005.0	1005.0	اممترما	004.6	أمميرا	002.8	002.6	اح. حما	COTIO	000.0	امنععم	086.4	086.0	000

14.	Aberd	99n :	H _b =	=26 · 8	3 me	tres.												,					Fel	bruar	y, 19	923.
		l mb.	ı mb.	i mb.	mb.	∣mb.	ı mb.	mb.	mb.	l mb.	mb.	l mb.	i mb.	mb.	mb.	∣ mb.	i mb.	ı mb.	mb.	mb.	∣mb.	mb.	ı mb.	l mb.	mb.	l mb.
	I																									993.3
	2	987.2	988	3 989.	991	1 992 -	993.9	995.2	996.6	997.8	998.6	999.	1999	7000.0	000	3 000 -2	001.2	001 2	2 001 .2	2 000 0	000.6	999	998.9	998.0	997	996.8
1	3	996.0	994	994	1993-6	5 993.6	5 993.2	2 993 • 1	993.3	993.7	994.7	995	995	996.6	997.1	997:	998.9	999.8	3 000 €	001.0	001.6	002.3	003.1	1003.6	004	997.2
	4	005.5	006.	I 006+8	3007	3 008.0	3·8oo c	3 009+4	010.2	011.1	011.9	012	012.1	012.2	012.2	012.2	011.9	011.0	011.6	011	5 011 2	010.4	010.1	1009.4	008.	010.0
	5	007.6	007.	1 005.0	004.	7 003	3 002.6	000.0	000-4	998.7	999.9	000.0	998.9	998.8	998.4	1998.4	1998.1	998.2	2 998-1	997.6	5 996-8	3 996∵	995.5	994.8	994.1	000.1
	6	993.4	992	5 991 · 1	989.8	8 989.0	989.2	988-3	987.7	987.4	986.3	985.6	986.	985.9	985.7	985.6	985.1	985.3	985.3	3 984.8	984.6	984.1	983.7	983.5	983.4	987.0
	7	983.1	982 9	982.3	3 983.0	o 983 <i>∙</i> €	5 984.5	5 984.3	983.7	982.9	981.5	979.8	977:	976.1	975.0	973.7	974.0	974.0	974:5	974	1975:3	3 975.8	975.7	975.5	975:3	978.9
	8	974.7	974.7	7 974.4	1973.4	4 971 -2	970.8	970.5	970.2	969.5	968.7	969∙.	970.0	971.0	972.5	973.6	975.1	977:2	978.9	980.8	3 982.0	983.1	984.8	8 985.8	987.4	975 · 2
1	9																									997 . 7
	10	001.4	001.7	1001.2	000.0	9000.5	5000-4	000.2	000.0	999.8	999.7	999.4	999.1	1998-8	998.2	998.0	997.9	998.0	998.3	998.6	999.0	999.4	000.0	000.4	001.2	999 7
Level-	11																									004 · 3
X	12	005.9	005.7	005.7	005.6	5 005.7	006.1	006.5	007.0	007.4	007.9	008.4	008.0	009.5	010.1	010.6	011.2	012.1	012.6	013.2	013.5	014.2	014.7	015.0	015.3	009 · 5
ı	13																									019 1
	14	020.1	020.0	019.7	019.5	5019.3	8-810	8 018·8	018.7	018.9	018.8	018.8	018.6	018.3	017.9	017.7	017.3	017.2	016.9	016.0	016.8	016.2	016.3	016.0	015.6	018.2
Station	15	015.1	014.6	014.0	013.6	013.1	012.5	012.3	011.0	011.6	011.3	011.0	010.6	010.4	009.7	009.1	008.8	008.5	008.3	008.0	007.9	007.9	007.8	007.5	007.4	010.4
at	16	006.8	006.4	006-1	005.8	3 005.5	005.4	005.5	005.8	005.7	005.7	005.7	005.8	005.7	005.7	005.5	005.3	005.5	005.7	005.7	005.8	006.1	006.3	006.3	006.7	005.9
St	17																									008 · 1
1	18	004.8	003.6	002.8	001.8	3000.8	999.6	¦999∙o	998.4	998∙0	997.6	997.6	997.1	996.2	995.5	994.9	994.8	994.9	995.2	995.2	995.4	995.8	996.1	996.1	996.1	998∙0
	19	996.1	996.1	996.3	996.4	1 996.7	996.7	997.2	997.6	998.2	998.4	998.7	999.0	999.1	999.2	999.4	000.0	000.3	001.0	001.5	001.9	002.4	002.7	003.1	003.4	999 1
1	20	003.6	003.7	003.7	003.0	9004.0	004.2	004.4	004.5	004.8	005.0	005.2	004.9	004.5	004.4	003.9	003.4	003.0	002.4	001.6	001.1	000.1	999.7	998.8	998.1	003 · 1
	21	997:4	996.4	995.4	994.2	993.5	992.3	991.6	991.4	991.0	990.3	990.0	989.3	989·o	988.3	987.7	987.2	987.2	987.4	987.4	987.4	987.5	987.4	987.4	987.4	990.4
	22	987.5	987.5	987.2	986.9	986-6	986.7	986.6	986.5	986.5	986.4	986.7	986.7	986.6	986.4	986.4	986.5	986.7	986.9	986.9	986.9	986.8	986.7	986.6	986.7	986 · 8
	23	986.5	986.3	986.3	986.3	986.4	986.6	986.9	987.2	987.5	987.6	988∙1	988.5	988.5	988.7	988.9	989.2	989.6	990.1	990.6	990.6	990.9	991.0	991.0	991.0	988.4
	24	991.2	991.2	991.0	991.1	991.4	991.7	992.2	992.7	993.2	993.7	994.2	994.6	995 0	995.4	995.8	996.4	996.8	997.4	997.8	998.1	998.5	998.7	998.9	999.0	994 · 7
. !	25	999.1	999.1	999.1	999.0	999.1	999.5	999.7	999.7	999.6	999.5	999.6	999.3	998.9	998.5	998∙0	997.5	997:3	997.0	996.5	995.9	995.2	994.4	993.6	992.5	998·c
	26	991.8	991.1	990.3	989.5	989-1	987.8	986.5	986.4	985.3	984.1	983.2	981.5	979.8	978.5	977.1	975.8	974.6	973.7	972.9	971.9	971.3	970.9	970.6	970.6	981 · 1
	27	969.9	969.3	968-9	968.6	968.5	968.5	968•6	968.7	968.8	968.7	969.2	969.6	970.2	970.7	971.1	971.5	971.9	972.2	972.9	973.0	973.6	973.9	974.6	975.4	970 · 7
\	28	976.1	976.4	976.9	977:3	977.9	978.6	979.4	980∙0	980.7	980.9	981.3	981.5	981.7	982.1	982.3	982.8	983.3	983.7	984.2	984.5	985.0	985.4	985.8	986.1	981.2
Mean		996	996	996	996	996	996	996		996	9 96	996	9 96	996	996	996	996	996	996		996	996	996	996	996	996
	n level)	•66	•54		•28			•32	•46						•46	•36		•59	.76		.74	.74	•67			
Mean (Sea le	evel)	999 •9 5	999 • 83	999 • 6 9	999		999	999 •6 1	999 '75	999 •84	999 •88	999 999		999 •84	999 '74		999 •73		1000 ·05	1000 -05	1000 •03		999 •96	999 •81	999 •81	999 •85
	м.т.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.			13.			16.		18.	19.	20.	21.	22.	23.	24.	Mean

15. Aberdeen: H_b (height of barometer cistern above M.S.L.) = $26 \cdot 8$ metres.

March, 1923.

10.	Aberd	een :	\mathbf{n}_b	(neigi	It OI	Daro.	шетег	CISTE	111 aı	JOVC .	1,1,0,1	J.) —	20 0) IIICi	165.									Marc		
]	Day.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
	_	mb.	mb.					mb.												mb.			mb.			
	I 2	987.3	986.5	987·1 985·4	984.1	1 983 · 3 1 983 · 3	982.7	982.6	982.3	981.9	981.3	980.9	980.6	980.7	980.8	980.8	980.8	980.6	980·6	980.7	991·2 980·7	980.0	980.6	980.6	980.7	990·2 982·1
	3	981.1	981.3	981.6	982.2	2 982.9	983.9	985.0	986.3	987.5	988.7	989.9	991.0	991.8	992.6	993.5	994.4	995.3	996.5	997.8	998.9	000 • 2	001.2	002.6	003.0	990.8
	4 5																									005.8
	6	005:4	005:3	3 005.3	004.	7 004.6	004.0	003.8	002.0	002.7	001.0	000.7	000.0	999.2	998-2	997.4	996.4	996·0	995.9	995.5	995.2	994.8	994.4	993.7	993.5	999.9
	7 8	993.2	992.6	992.5	992.2	2 992.2	992.4	993.5	994.6	995.7	997.0	998.1	999.3	000.1	001.2	002.1	003.2	004.4	005.7	006.8	007.5	007.9	008.4	009.0	009.7	1999 6
	9	022.0	021.8	021.6	021.	1 021 3	3 021.5	021.6	021.5	021.6	021.3	021.1	021.1	020.7	020.4	019.9	019.6	019.6	019.5	019.3	019.2	018.8	018.5	018.1	017.7	017 · 1
	10	017.3	016.0	016.3	016.1	015.7	015.2	015.0	014.7	014.4	013.9	013.7	013.4	012.9	012.5	012.2	012.0	011.0	012.0	012.0	012.1	012.6	012.7	012.8	013.2	013.9
	11																									016.2
el	12 13																									012.3
Level	14	026.4	026.6	026.8	027.0	027	3 027.6	027.9	028.2	028.7	028.9	029.1	029.1	029.2	029.1	029.1	029.0	029.1	029.5	029.8	029.9	030.1	030.5	030-2	030.6	028·6 030·0
1	15	1					1		1				ł	1	ì	1	ļ	ł	ļ	1		1	}			
Station	16 17	029.3	029.1	1 028·7 3 030·6	028.2	4 028·5	031.0	028.9	031.4	029.4	030.0	030.0	030.0	029.8	032.1	029.4	029.4	029.5	029.8	030.1	030.3	030.6	030.8	030·9 033·0	031.1	029·6 031·8
tat	18	032.0	032.7	032.6	032.7	4 032.4	1032.5	032.5	032.2	032.2	032.5	032.3	032.3	032.1	031.6	031.5	031.3	031.1	031.1	030.9	030.2	030.3	030.2	030.3	030.1	031 8
S	19 20																									027.5
	21	021.4	021.0	020.7	020.3	3 020-1	020-1	020.1	020.1	020.0	020.0	010.7	010.6	010.4	010-1	010.1	o18∙o	018-0	018-0	010.1	010.3	010.3	010.2	010.1	010.1	019.7
	22	019.1	018.0	9/018/8	018.7	7 018∵	5 018.7	018.9	018.9	018.9	018.7	018.2	018.0	017.6	017.4	016.9	016.7	016.5	016.4	016.4	016.4	019.1	015.9	015.2	015.3	017.6
1 1	23 24	011.3	011.1	010.8	010.7	1 010-2	010.2	010.1	010.0	009.8	009.3	009:3	009.0	009.0	009.1	009.2	009.4	009.9	010.0	010.7	011.1	011.4	011.0	012.0	012.3	013.3
	25	012.3	012.5	012.6	012.8	3012.8	013.1	013.3	013.5	013.6	013.5	013.2	013.5	013.1	013.0	012.7	012.7	012.9	013.0	013.2	013.5	014.3	014.9	015.6	015.7	013.3
	26	016.6	017.5	018.6	019.0	019.7	020.1	020.6	021.0	021.3	021.9	022.0	021.7	021.6	021.3	020.6	020.6	020.7	020.1	020.2	020.1	019.8	019.4	019.0	018-5	020.0
	27 28	017.6	010.0	010.4	015.0	015.1	014.7	014.5	014.0	014.5	014.0	014.5	014.0	013.4	012.6	012.3	012.0	011.8	015.4	011.0	016.2	016.6	016.8	017.4	017.6	013.8
	29 30	018.0	018-2	018.5	018.6	019.2	019.6	020.3	020.5	020.7	021.0	021.4	021.5	021.7	021.8	021.7	021.8	021.9	022.2	022.9	023.2	023.6	023.7	024.1	024.2	021 · 1
1 1	_	1			1									ĺ	ĺ	1	1	i	1	1	1	1	ļ	1	1	1
Ψ	31	·		.		-	-]			-		·						·	017.4
Mean (Stat	ion level)	1014		1014	1014 ·21	1014	1014	1014 ·65	1014	1015	1015	1015	1015	1015	1015	1014	1014	1014	1015	1015	1015	1051	1015	1015 ·55	1015	1014
Mean						1017	1017	1018	1018	1018	1018	1018	1018	1018	1018			1018	1018					1018	1018	1018
																					i	1 0-	0.0			
1	level)	.90	.78	•63	.57	61	.74					•59				1.13	.11	•20	42	·64	.74	J ·8 ₅	∙88	90	1 .88	
1	level)	·90 00n :	H_b	= 26	·8 m	etres	·74	.01	.22	42	·57		· 5 5	45	•32) '42	1 .64	.74	1 .85	.88	Apr	il, 19	923.
(Sea	Aberd	een:	H _b	= 26	· 8 m	mb.	mb.	mb.	mb.	mb.	.57 mb.	mb.	mb.	mb.	mb.	mb,	mb	mb.	mb.	mb.	mb.	mb.	mb.	Apr mb. 020.5	il, 19)23.
(Sea	Aberd	90 mb.	78 Hb	= 26 mb. o14·3 o21·5	-57 -8 m	mb.	mb.	mb.	mb.	mb. 015.7	mb.	mb. 016·0	mb.	mb.	mb. 016-8	mb. 016·9	mb 017·0	mb.	mb.	mb.	mb. 019·0	mb. 019·5	mb. 019·9	Mb. 020·5	il, 19	mb. 016·7
(Sea	Aberd I 2 3	mb. o15.0 o21.0 o20.5	mb. o14.8 o20.1 o11.6	-63 = 26 mb. o14·3 o21·5 o19·8 o11·2	-57 -8 m	mb. 014.7 022.1 010.0	mb. 015·1 022·5 019·1	mb. 015.4 022.8 019.0	mb. 015·5 023·1 018·8	mb. 015.7 023.3 018.8	mb. 015·8 023·6 018·4	mb. 016·0 023·5 018·2	mb. 016·2 023·5 017·8	mb. 016·6 023·3 017·4	mb. 016·8 023·2 017·1	mb. 016·9 023·0 016·6	mb 017·0 023·0 016·1 008·0	mb. 017·3 022·8 015·6 007·9	mb. 017·8 022·6 015·2 008·1	mb. 018·5 022·4 014·9 008·3	mb. 019·0 022·3 014·8 008·5	mb. 019·5 022·1 014·3	mb. 019·9 021·8 013·7 008·7	mb. 020·5 021·6 013·4 008·7	mb. 020.8 020.9 012.8	mb. 016·7 022·5 017·3
(Sea	Aberd I 2 3 4 5	mb. 015.0 021.0 020.5 012.0 008.6	mb. 014·8 021·3 020·1 011·6 008·6	mb. o14·3 o21·5 o19·8 o11·2 o08·4	mb. o14.6 o21.8 o19.5 o10.4 o08.3	mb. 5 014.7 8 022.1 5 019.3 4 010.0 8 008.4	mb. 015·1 022·5 019·1 009·8 008·8	mb. 015·4 022·8 019·0 009·7	mb. 015·5 023·1 018·8 009·5	mb. 015·7 023·3 018·8 009·3	mb. 015·8 023·6 018·4 009·2 009·9	mb. 016·0 023·5 018·2 009·1	mb. 016·2 023·5 017·8 009·0 010·0	mb. 016·6 023·3 017·4 008·8 010·1	mb. 016·8 023·2 017·1 008·8 010·2	mb. 016·9 023·0 016·6 008·6	mb 017·0 023·0 016·1 008·0 010·2	mb. 017·3 022·8 015·6 007·9 010·2	mb. 017·8 022·6 015·2 008·1 010·5	mb. 018·5 022·4 014·9 008·3	mb. 019·0 022·3 014·8 008·5	mb. 019·5 022·1 014·3 008·6 011·5	mb. 019·9 021·8 013·7 008·7 011·8	mb. 020·5 021·6 013·4 008·7 012·2	mb. 020.8 020.9 012.8 008.6 012.4	mb. 016·7 022·5 017·3 009·4 010·0
(Sea	Aberd I 2 3 4 5	mb. 015.0 021.0 020.5 012.0 008.6	78 Hb mb. 014·8 021·3 020·1 011·6 008·6	-63 = 26 mb. 014·3 021·5 019·8 011·2 008·4 012·3	-57 -8 m	mb. 5 014.7 8 022.1 5 019.3 4 010.0 8 008.4	mb. 015·1 022·5 019·1 009·8 008·8	mb. 015·4 022·8 019·0 009·7 009·1	mb. 015·5 023·1 018·8 009·5 001·6	mb. 015·7 023·3 018·8 009·3	mb. 015·8 023·6 018·4 009·2 009·9	mb. 016·0 023·5 018·2 009·1 010·1	mb. 016·2 023·5 017·8 009·0 010·0	mb. 016·6 023·3 017·4 008·8 010·1	mb. 016·8 023·2 017·1 008·8 010·2	mb. 8016·9 9023·0 916·6 8008·6	mb 017·0 023·0 016·1 008·0 010·2	mb. 017·3 022·8 015·6 007·9 010·2	mb. 017·8 022·6 015·2 008·1 010·5	mb. 018·5 022·4 014·9 008·3 010·7	mb. 019·0 022·3 014·8 008·5 011·2	mb. 019·5 022·1 014·3 008·6 011·5	mb. 019·9 021·8 013·7 008·7 011·8	mb. 020·5 021·6 013·4 008·7 012·2	mb. 020.8 020.9 012.8 008.6 012.4	mb. 3016·7 3022·5 3009·4 3000·5
(Sea	Aberd 1 2 3 4 5 6 7 8	mb. 015.0 021.0 020.5 012.0 008.6 012.3 007.6 014.6	78 Hb mb. 014·8 021·3 020·1 011·6 008·6 012·3 007·3	-63 = 26 mb. 014·3 021·5 019·8 011·2 008·4 0012·3 007·1 0015·1	mb. 014.6 021.8 019.5 010.4 008.3	mb. 5 014.7 8 022.1 5 019.3 4 010.0 9 007.1 5 015.0	74 mb. 015·1 022·5 019·1 009·8 008·8 0011·5 007·1	mb. 015·4 022·8 019·0 009·1 011·6 007·5 017·0	mb. 015·5 023·1 018·8 009·5 009·5 011·6 007·8	mb. 015·7 023·3 018·8 009·3 001·6 007·9 017·7	mb. 015·8 023·6 018·4 009·2 009·9 011·6 007·9	mb. 016·0 023·5 018·2 009·1 010·1 011·3 008·1	mb. o16·2 o23·5 o17·8 oo9·0 o10·0 o11·0 o08·3	mb. o16·6 o23·3 o17·4 oo8·8 o10·1 o10·5 oo8·5 o18·6	mb. 016·8 023·2 017·1 008·8 010·2 010·1 008·9	mb. 8016.9 023.0 016.6 8008.6 010.2 009.7 009.3	mb 017·0 023·0 016·1 008·0 010·2 009·4 009·7 018·6	mb. 017·3 022·8 015·6 007·9 010·2 009·0 010·2 018·6	mb. 017·8 022·6 015·2 008·1 010·5 009·0 010·9 018·7	mb. 018·5 022·4 014·9 008·3 010·7 009·0 011·7 018·9	mb. 019·0 022·3 014·8 008·5 011·2 008·9 012·3 019·1	mb. 019·5 022·1 014·3 008·6 011·5 008·5 012·8 019·1	mb. 019·9 021·8 013·7 008·7 011·8 008·3 013·3 019·1	mb. 020·5 021·6 013·4 008·7 012·2 008·2 013·7 019·1	mb. 020.8 020.9 012.8 008.6 012.4 007.8 014.2 019.0	mb. 016·7 022·5 017·3 009·4 010·0 010·5 009·3 017·6
(Sea	Aberd 1 2 3 4 5 6 7 8 8 9	mb. 015.0 021.0 020.5 012.0 008.6 012.3 007.6 014.6 019.0	78 Hb mb. 014·8 021·3 020·1 011·6 008·6 012·3 007·3 014·9 018·8	-63 = 26 mb. 014·3 021·5 019·8 011·2 008·4 0012·3 007·1 0015·1 018·7	-57 -8 m	mb. 5 014.7 8 022.1 5 019.3 4 010.0 9 007.1 5 015.0 5 018.3	74 mb. o15·1 o22·5 o19·1 o09·8 o08·8 o011·5 o07·1 o16·4 o18·2	mb. 015·4 022·8 019·0 009·7 009·1 011·6 007·5 017·0 018·2	mb. 015·5 023·1 018·8 009·5 009·5 011·6 007·8 017·5 018·1	mb. 015·7 023·3 018·8 009·3 001·6 007·9 017·7 018·1	mb. 015·8 023·6 018·4 009·9 011·6 007·9 017·9	mb. 016·0 023·5 018·2 009·1 010·1 011·3 008·1 018·2	mb. o16·2 o23·5 o17·8 o09·0 o10·0 o11·0 o08·3 o18·4	1 mb. 016·6 023·3 017·4 008·8 010·1 010·5 008·5 018·6 017·1	mb. o16·8 o23·2 o17·1 oo8·8 o10·2 o10·1 oo8·6 o18·7	mb. 3016·9 023·0 016·6 3008·6 010·2 009·7 009·3 018·7 016·4	mb 017·0 023·0 016·1 008·0 010·2 009·4 009·7 018·6	mb. 017·3 022·8 015·6 007·9 010·2 009·0 010·2 018·6 015·7	mb. 017·8 022·6 015·2 008·1 010·5 009·0 010·9 018·7 015·5	mb. 018·5 022·4 014·9 008·3 010·7 009·0 011·7 018·9 015·4	mb. 019·0 022·3 014·8 008·5 011·2 008·9 012·3 019·1 015·2	mb. 019·5 022·1 014·3 008·6 011·5 008·5 012·8 019·1 014·8	mb. 019·9 021·8 013·7 008·7 011·8 008·3 019·1 014·4	mb. 020·5 021·6 013·4 008·7 012·2 008·2 013·7 019·1 013·8	mb. 020.8 020.9 012.8 007.8 014.2 019.0 013.1	mb. 8016·7 022·5 8017·3 1009·4 1010·0 1010·0 1010·0 1010·0 1010·0 1010·0
(Sea	Aberd 1 2 3 4 5 6 7 8 9 10	mb. 015.0 021.0 020.5 012.0 008.6 012.3 007.6 014.6 019.0 012.6	mb. 014·8 021·3 020·1 011·6 008·6 012·3 007·3 014·9 018·8 011·8	-63 = 26 mb. 014·3 021·5 019·8 011·2 008·4 015·1 015·1 018·7 011·2	mb. o14.6 o21.8 o19.5 o10.4 o08.5 o12.0 o06.6 o15.5 o10.5	mb. 5 014.7 8 022.1 5 019.3 4 010.0 8 0011.6 9 007.1 5 015.0 5 016.0	mb. vo15·1 vo22·5 vo19·1 vo09·8 vo08·8 vo11·5 vo7·1 vo16·4 vo16·4 vo08·9	mb. 015·4 022·8 019·0 009·7 009·1 011·6 007·5 017·0 018·2 009·0	mb. 015·5 023·1 018·8 009·5 009·5 011·6 007·8 017·5 018·1 008·5	mb. 015·7 023·3 018·8 009·3 009·9 011·6 007·9 017·7 018·1 008·4	mb. 015·8 023·6 018·4 009·2 009·9 011·6 007·9 017·9 008·0	mb. 016·0 023·5 018·2 009·1 010·1 011·3 008·1 018·2 017·7 008·0	mb. 016·2 023·5 017·8 009·0 010·0 011·0 008·3 018·4 008·0	mb. 016·6 023·3 017·4 008·8 010·1 010·5 008·5 017·1 008·0	mb. 016·8 023·2 017·1 008·8 010·1 008·9 016·8 008·1	mb. 8016·9 9023·0 9016·6 8008·6 9010·2 909·7 909·3 918·7 916·4 908·2	mb 017·0 023·0 016·1 008·0 010·2 009·4 009·7 018·6 015·9 008·4	mb. 017·3 022·8 015·6 007·9 010·2 009·0 010·2 018·6 015·7 008·9	mb. 017·8 022·6 015·2 008·1 010·5 009·0 010·9 018·7 015·5 008·9	mb. 018·5 022·4 014·9 008·3 010·7 009·0 011·7 018·9 015·4	mb. 019·0 022·3 014·8 008·5 011·2 008·9 012·3 019·1 015·2 010·1	mb. o19·5 o22·1 o14·3 oo8·6 o11·5 o08·5 o12·8 o19·1 o14·8 o10·2	mb. 019·9 021·8 013·7 008·7 011·8 008·3 013·3 019·1 014·4 010·2	mb. 020·5 021·6 013·4 008·2 013·7 019·1 013·8 010·3	mb. 020.8 020.9 012.8 008.6 012.4 007.8 014.2 019.0 013.1 010.3	mb. 8016·7 922·5 8010·3 8009·4 9100·5 9009·3 917·6 916·9 9009·5
(Sea 16.	Aberd 1 2 3 4 5 6 7 8 8 9 10 11 12	900 mb. 015.00 021.00 008.60 012.30 007.60 012.60 009.8	78 Hb mb. 014.8 021.3 020.1 011.6 008.6 012.3 007.3 014.9 018.8 011.8	-63 = 26 mb. 014·3 021·5 019·8 011·2 008·4 015·1 018·7 011·2 008·6 003·2	mb. o14.6 o21.8 o19.5 o10.6 o15.5 o10.6 o10.6 o10.6	mb. 5014.7 8 022.1 5019.3 4 010.0 8 007.1 5 018.3 5 010.0	mb. 7015·11 022·5 019·11 0009·8 0001·5 007·1 0016·4 008·9 0007·5	mb. 015·4 022·8 019·0 009·7 009·1 011·6 007·5 017·0 018·2 009·0 007·5	mb. o15·5 o23·1 o18·8 o09·5 o11·6 o07·8 o17·5 o18·1 o08·5	mb. 015·7 023·3 018·8 009·3 009·9 011·6 007·9 018·1 008·4	mb. 015·8 023·6 018·4 009·2 009·9 011·6 007·9 017·9 008·0	mb. 016·0 023·5 018·2 009·1 010·1 011·3 008·1 018·2 017·7 008·0	mb. o16·2 o23·5 o17·8 o09·0 o10·0 o11·0 o08·3 o18·4 o17·4 o08·0	mb. o16·6 o23·3 o17·4 oo8·8 o10·1 o10·5 oo8·5 o18·6 o17·1 oo8·o	mb. o16·8 o23·2 o17·1 o08·8 o10·2 o10·1 o08·6 o08·1	mb. 3016·9 023·0 016·6 009·7 009·3 018·7 016·4 008·2 005·9	mb 017·0 023·0 016·1 008·0 010·2 009·4 009·7 018·6 015·9 008·4	mb. 017·3 022·8 015·6 007·9 010·2 009·0 010·2 018·6 015·7 008·9 005·6	mb. o17·8 o22·6 o15·2 oo8·1 o10·5 o09·0 o10·9 o18·7 o15·5 oo8·9	mb. 018·5 022·4 014·9 008·3 010·7 009·0 011·7 018·9 015·4 009·5 005·5 992·8	mb. 019·0 022·3 014·8 008·9 012·3 019·1 015·2 010·1	mb. 019·5 022·1 014·3 008·6 011·5 012·8 019·1 014·8 010·2 005·5 991·4	mb. 019·9 021·8 013·7 008·7 011·8 008·3 019·1 014·4 010·2	mb. 020·5 021·6 013·4 008·2 013·7 019·1 013·8 010·3 005·5 989·7	mb. 020.8 020.9 012.4 007.8 014.2 019.0 013.1 010.3 004.9 988.5	mb. 0020:5 0020:5 0010:0 0
(Sea 16.	Aberd 1 2 3 4 5 6 7 8 9 10 11 12 13 14	mb. 015.0 021.0 020.5 012.0 030.6 012.3 007.6 014.6 019.0 012.6 009.8 004.6 987.5	78 Hb mb. 014·8 021·3 020·1 011·6 008·6 012·3 007·3 014·9 018·8 011·8 009·2 003·7 986·2 087·4	-63 = 26 mb. 014·3 021·5 019·8 011·2 008·4 012·3 007·1 015·1 018·7 011·2 008·6 003·2 985·1 087·2 087	-57 ·8 m mb. o14·6 o21·8 o19·5 o10·4 o08·3 o12·6 o06·9 o18·2 o18·2 o18·3 o18·3 o19·3 o18·3 o19·3	mb. 5014.7 8 022.1 5019.3 1010.0 5007.1 5015.9 5010.0 1008.0 1008.0	mb. o15·1 o22·5 o19·1 o09·8 o07·1 o16·4 o16 o16·4 o16·4 o16·4 o16·4 o16·4 o16·4 o16·4 o16·4 o16·4 o16·4 o16 o16·4 o16 o16·4 o16 o16·4 o16 o16·4 o16 o16 o16 o16 o16 o16 o16 o16 o16 o16	mb. 015·4 022·8 019·0 009·7 009·1 011·6 007·5 017·0 018·2 009·0 007·5 001·0 982·5	mb. 015·5 023·1 018·8 009·5 007·5 011·6 007·8 018·1 008·5 007·4 000·6 982·7 982·7	mb. 015·7 023·3 018·8 009·3 011·6 007·9 017·7 018·1 008·4 007·3 000·2 983·4 088·8	mb. o15·8 o23·6 o18·4 oo9·2 oo9·9 o11·6 oo7·9 o17·9 oo8·o o999·1 983·8 o88·8	mb. 016·0 023·5 018·2 009·1 010·1 011·3 008·1 018·2 017·7 008·0 006·5 998·3 984·0 088·0	mb. o16·2 o23·5 o17·8 o09·0 o10·0 o11·0 o08·3 o18·4 o17·4 o08·0 o06·6 997·7 984·1 o80·6	mb. o16·6 o23·3 o17·4 oo8·8 o10·1 o10·5 oo8·5 o17·1 oo8·0 oo6·4 997·3 984·3 o80·8 o80·8 o80·8 o80·8 o80·8 o10·1 o80·0 mb. 016.8 023.2 017.1 008.8 010.2 010.1 008.5 018.7 016.8 008.1	mb. 016.9 023.0 016.6 008.6 010.2 009.7 009.3 018.7 016.4 008.2	mb 017·0 023·0 016·1 008·0 010·2 009·4 009·7 018·6 015·9 008·4 005·7 994·9 985·0	mb. 017·3 022·8 015·6 007·9 010·2 009·0 010·2 018·6 015·7 008·9 005·6 993·6 993·6 993·6 993·6	mb. 017·8 022·6 015·2 008·1 010·5 009·0 018·7 015·5 008·9 005·6 993·1 986·0 991·7	mb. 018·5 022·4 014·9 008·3 010·7 009·0 011·7 018·9 005·5 992·8 986·8 992·4	mb. o19·0 o22·3 o14·8 o08·5 o11·2 o08·9 o12·3 o19·1 o15·2 o10·1 o05·5 992·1 987·4 993·2	mb. o19·5 o22·1 o14·3 o08·6 o11·5 o08·5 o12·8 o19·1 o14·8 o10·2 o05·5 991·4 987·5	mb. 019·9 021·8 013·7 008·7 011·8 008·3 019·1 010·2 005·5 990·5 987·4 994·7	mb. 020·5 021·6 013·4 008·7 012·2 008·2 013·7 019·1 013·8 010·3 005·5 989·7 989·6	mb. 020.8 020.9 012.8 008.6 012.4 007.8 014.9 013.1 010.3 004.9 988.5 995.6 995.6	mb. 8016·7 0022·5 8017·3 8009·4 010·0 8010·5 009·3 0017·6 016·9 009·5 006·8 997·4 985·2	
(Sea 16.	Aberd 1 2 3 4 5 6 7 8 9 10 11 12 13 14	mb. 015.0 021.0 020.5 012.0 030.6 012.3 007.6 014.6 019.0 012.6 009.8 004.6 987.5	78 Hb mb. 014·8 021·3 020·1 011·6 008·6 012·3 007·3 014·9 018·8 011·8 009·2 003·7 986·2 087·4	-63 = 26 mb. 014·3 021·5 019·8 011·2 008·4 012·3 007·1 015·1 018·7 011·2 008·6 003·2 985·1 087·2 087	-57 ·8 m mb. o14·6 o21·8 o19·5 o10·4 o08·3 o12·6 o06·9 o18·2 o18·2 o18·3 o18·3 o19·3 o18·3 o19·3	mb. 5014.7 8 022.1 5019.3 1010.0 5007.1 5015.9 5010.0 1008.0 1008.0	mb. o15·1 o22·5 o19·1 o09·8 o07·1 o16·4 o16 o16·4 o16·4 o16·4 o16·4 o16·4 o16·4 o16·4 o16·4 o16·4 o16·4 o16 o16·4 o16 o16·4 o16 o16·4 o16 o16·4 o16 o16 o16 o16 o16 o16 o16 o16 o16 o16	mb. 015·4 022·8 019·0 009·7 009·1 011·6 007·5 017·0 018·2 009·0 007·5 001·0 982·5	mb. 015·5 023·1 018·8 009·5 007·5 011·6 007·8 018·1 008·5 007·4 000·6 982·7 982·7	mb. 015·7 023·3 018·8 009·3 011·6 007·9 017·7 018·1 008·4 007·3 000·2 983·4 088·8	mb. o15·8 o23·6 o18·4 oo9·2 oo9·9 o11·6 oo7·9 o17·9 oo8·o o999·1 983·8 o88·8	mb. 016·0 023·5 018·2 009·1 010·1 011·3 008·1 018·2 017·7 008·0 006·5 998·3 984·0 088·0	mb. o16·2 o23·5 o17·8 o09·0 o10·0 o11·0 o08·3 o18·4 o17·4 o08·0 o06·6 997·7 984·1 o80·6	mb. o16·6 o23·3 o17·4 oo8·8 o10·1 o10·5 oo8·5 o17·1 oo8·0 oo6·4 997·3 984·3 o80·8 o80·8 o80·8 o80·8 o80·8 o10·1 o80·0 mb. 016.8 023.2 017.1 008.8 010.2 010.1 008.5 018.7 016.8 008.1	mb. 016.9 023.0 016.6 008.6 010.2 009.7 009.3 018.7 016.4 008.2	mb 017·0 023·0 016·1 008·0 010·2 009·4 009·7 018·6 015·9 008·4 005·7 994·9 985·0	mb. 017·3 022·8 015·6 007·9 010·2 009·0 010·2 018·6 015·7 008·9 005·6 993·6 993·6 993·6 993·6	mb. 017·8 022·6 015·2 008·1 010·5 009·0 018·7 015·5 008·9 005·6 993·1 986·0 991·7	mb. 018·5 022·4 014·9 008·3 010·7 009·0 011·7 018·9 005·5 992·8 986·8 992·4	mb. o19·0 o22·3 o14·8 o08·5 o11·2 o08·9 o12·3 o19·1 o15·2 o10·1 o05·5 992·1 987·4 993·2	mb. o19·5 o22·1 o14·3 o08·6 o11·5 o08·5 o12·8 o19·1 o14·8 o10·2 o05·5 991·4 987·5	mb. 019·9 021·8 013·7 008·7 011·8 008·3 019·1 010·2 005·5 990·5 987·4 994·7	mb. 020·5 021·6 013·4 008·7 012·2 008·2 013·7 019·1 013·8 010·3 005·5 989·7 989·6	mb. 020.8 020.9 012.8 008.6 012.4 007.8 014.9 013.1 010.3 004.9 988.5 995.6 995.6	mb. 0020:5 0020:5 0010:0 0	
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Station Level	Aberd I 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mb. 015.0 020.5 012.0 008.6 012.3 007.6 019.0 012.6 009.8 004.6 987.5 987.5 995.9 006.0 016.1 010.7 012.7 012.7 012.7 012.7 013.9 005.9 011.6 000.0 981.7 997.9 005.1 000.3 000.8	78 Hb mb. 014.8 021.3 020.1 011.6 008.6 012.3 007.3 014.9 018.8 011.8 009.2 003.7 986.2 987.4 016.3 017.6 010.5 010.5 010.8 012.6 013.4 005.3 012.1 998.0 981.3 998.9 005.0 000.2 000.7 100.7	-63 = 26 mb. 014·3 021·5 019·8 011·2 008·4 012·3 007·1 015·1 018·7 011·2 098·5 006·5 010·1 011·0 012·5 095·5 095·5 095·5 000·2 000·4 000·4 0006 000·4 0006	mb. oli-16 oli-	mb. 5 014.7 8 022.1 9 000.1 9 000.1 1 000.2 1 000.2 1 000.2 1 000.2 1 000.2 1 000.2 1 000.2 1 000.3 1 010.3 2 987.2 2 987.2 3 000.3 3 000.3 3 000.3 3 000.3 4 000.3 5 000.3 6 000.3 6 000.3 7 000.3 7 000.3 8 001.8 8 001.9 9 000.1 9 9 9 7	mb. 7015·11 022·5 019·11 009·8 008·8 0011·5 007·11 016·4 018·2 008·9 007·5 001·4 0997·6 011·8 012·2 005·6 012·5 988·3 981·7 002·6 004·9 000·1 999·7 1006	mb. 015·4 022·8 019·0 009·7 009·1 011·6 007·5 017·0 018·2 009·0 007·5 001·0 982·5 987·8 998·0 008·2 018·0 016·3 009·6 011·2 011·8 986·6 982·4 004·9 000·3 999·4 1006	mb. 015·5 023·11 018·8 009·5 009·5 011·6 009·5 018·1 008·5 009·6 018·2 009·6 011·2 011·8 009·6 011·2 006·9 013·2 984·7 982·6 000·3 999·4 1006	mb. 015·7 023·3 018·8 009·9 011·6 007·9 017·7 018·1 008·4 007·3 000·2 983·4 988·5 999·2 009·4 018·7 011·9 007·5 013·5 983·6 983·0 004·3 000·4 999·2 1006	mb. 015·8 023·6 009·2 009·9 011·6 007·0 999·1 983·8 989·7 010·0 019·2 011·6 008·5 013·5 983·3 983·4 004·6 003·8 000·5 999·2 1006	mb. o16 cc o23 · 5 co o18 · 2 co o18 · 2 co o19 · 1 co o10 · 1 co	mb. o16·2 o23·5·5 o17·8 o90 o10·0 o11·0 o16·2 o08·3 o18·4 o17·4 mb. o16·6 o23·3 o17·4 o16·5 o18·6 o17·1 o16·5 o18·6 o17·1 o16·5 o16·6 o17·1 o16·5 o16·6 o17·1 o16·5 o16·6 o17·1 o16·5 mb. o16 · 8 o23 · 22 o17 · 11 o o8 · 6 o18 · 7 o16 · 8	mb. 016·9 023·0 016·6 008·6 010·2 009·7 016·4 008·2 005·9 995·4 984·7 990·2 013·4 009·6 011·4 012·6 009·5 009·4 011·7 982·6 985·5 004·0 001·4 000·4 998·1 1006	mb 017.0 023.0 016.1 008.0 010.2 009.4 009.7 018.6 015.9 008.4 005.7 994.9 985.0 990.6 012.3 019.2 013.0 009.6 011.8 012.6 009.2 009.2 011.1 982.3 986.2 003.8 000.9 000.6 997.4 1006	mb. o17:3 o22:8 o15:6 o07:9 o10:2 o09:0 o10:2 o09:0 o10:2 o09:0 o12:7 o12:5 o09:0 o12:9 o10:0 o12:9 o10:0 o12:9 o10:0 o12:9 o10:0 o12:9 o10:0 mb. o17.8 o17.8 o22.6 o15.2 o08.1 o10.5 o09.0 o10.9 o18.7 o15.5 o08.9 o05.6 993.1 986.0 o91.7 o2.8 o13.0 o19.2 o12.2 o09.8 o12.1 o13.0 o09.9 982.0 989.8 o04.5 o00.4 o00.7 995.9 loo6	mb. 018·5 022·4 014·9 008·3 010·7 009·0 011·7 018·9 015·4 009·5 992·8 986·8 992·4 003·4 013·7 019·1 012·4 013·3 008·7 982·1 991·3 004·5 000·2 001·1 995·0 1006	mb. o19·0 o19·0 o19·0 o19·1 o15·2 o10·1 o15·2 o10·1 o15·2 o10·1 o15·2 o10·1 o15·2 o10·1 o1	mb. o19·5 o22·1 o14·3 o08·6 o11·5 o12·8 o19·1 o14·8 o10·2 o05·5 991·4 987·5 994·0 o14·1 o10·9 010·5 o12·6 o14·1 o06·9 982·3 o04·9 o00·7 o01·4 o06·9 994·8 o00·7	mb. o19·9 o21·8 o13·7 o08·7 o11·8 o08·3 o19·1 o14·4 o10·2 o05·5 990·5 987·4 994·7 o05·0 o15·3 o19·0 o11·7 o10·5 o12·9 o14·2 o07·5 o11·2 o05·7 982·3 995·2 o04·9 o00·5 o01·4	mb. o20·5 o21·6 o13·4 o08·2 o13·7 o12·2 o13·7 o13·8 o10·3 o05·5 989·7 987·6 o11·4 o12·9 o11·3 o07·2 o11·3 o05·5 o01-2 996·7 o010-6	188 188	923. mb. 6016.7 6022.5 6017.3 6017.6			
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Station Level Mean (Stati	Aberd I 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 10 10 10 10 10 10 10 10 10 10 10 10 10	mb. 015.0 021.0 020.5 012.0 008.6 012.3 007.6 019.0 012.6 019.0 012.6 099.8 004.6 987.5 987.5 995.9 006.0 016.1 018.0 011.1 010.7 012.7 013.9 005.9 005.9 001.6 000.0 981.7 997.9 005.9 1000.3	78 Hb mb. 014·8 021·3 020·1 011·6 008·6 012·3 007·3 007·3 014·9 018·8 011·8 009·2 003·7 986·2 987·4 016·3 017·6 010·5 010·5 010·8 012·6 013·4 005·3 017·6 013·4 005·3 019·1 998·0 000·2 000·7 1007	-63 = 26 mb. 014·3 021·5 019·8 011·2 008·4 012·3 007·1 015·1 018·7 011·2 008·6 003·2 985·1 987·2 996·5 010·1 011·0 012·5 012·5 012·5 016·4 017·0 012·5 016·1 011·0 012·5 016·1 011·0 016·1	mb. ol4 (6 ol5 ol5 ol5 ol6 ol6 ol6 ol6 ol6 ol6 ol6 ol6 ol6 ol6	mb. 1014.7 3022.1 1019.3 4010.6 1019.3 4010.6 1010.6 1008.6 1008.6 1008.6 1009.5 1010.8	mb. o15:1 o22:5 o19:1 o22:5 o19:1 o20:1	mb. 015:4 022:8 019:0 009:7 009:1 011:6 007:5 017:0 018:2 009:0 007:5 001:0 082:5 098:0 006:5 012:8 986:6 982:4 004:9 000:3 999:4	mb. 015·5 023·1 018·8 009·5 009·5 011·6 007·8 000·6 982·7 987·1 008·9 018·5 016·2 009·6 011·2 011·8 012·0 006·9 984·7 982·6 000·3 999·4	mb. 015·7 023·3 018·8 009·3 009·9 011·6 007·3 000·2 983·4 988·5 999·2 009·4 011·9	mb. 015·8 023·6 018·4 009·2 009·9 011·6 007·9 017·9 08·0 07·0 999·1 983·8 989·7 010·0 019·2 015·8 009·7 011·2 011·6 08·5 013·5 983·3 983·4 004·6 008·5 999·2 1006 .83	mb. o16·c o23·5·o18·2 o09·1 o10·1 o11·3 o08·1 o18·2 o08·0 o08·0 o08·3 988·9 999·9 o10·5·o15·6 o09·6 o01·2 o11·4 o09·0 o13·6 o982·7 983·6 o04·9 988·9	mb. o16·2 o23·5 o17·8 o16·2 o23·5 o17·8 o16·2 o23·5 o17·8 o16·2 o23·5 o16·2 o23·5 o16·2 o23·5 mb. o16·6 o23·3 o17·4 o08·8 o10·1 o10·5 o08·5 o17·1 o08·0 o17·1 o08·0 o17·1 o08·0 o17·1 o10·5 o19·5 o19·5 o19·5 o19·5 o19·5 o19·5 o19·5 o10·8 o09·6 o12·6 o10·8 o09·5 o10·2 o10·3 mb. o16 · 8 o16 · 9 o16 · 016 ·	mb. 016·9 023·0 016·6 008·6 010·2 009·7 009·3 018·7 016·4 08·2 005·9 995·4 984·7 990·2 013·4 009·6 011·4 012·6 009·5 009·4 000·4 988·1 1006 -53	mb 017·0 023·0 016·1 008·0 010·2 009·4 009·7 018·6 015·9 008·4 005·7 9985·0 990·6 011·8 012·6 009·2 009·5 011·1 982·3 986·2 003·8 000·9 000·6 997·4 1008 -45	mb. o17 3 o22 8 o15 6 o07 9 o10 2 o09 0 o10 7 3 o15 7 o8 9 o15 7 o17 7	mb. 017·8 022·6 015·2 008·1 010·5 009·0 010·9 018·7 015·5 008·9 005·6 993·1 986·0 991·7 002·8 013·0 019·2 012·2 009·8 013·0 009·9 982·0 989·8 004·5 000·7 995·9 —————————————————————————————————	mb. o18·5 o22·4 o14·9 o08·3 o10·7 o09·0 o11·7 o18·9 o15·4 o09·5 o92·8 986·8 986·8 992·4 o13·7 o19·1 o12·0 o10·1 o12·4 o13·3 o08·8 o10·2 o08·7 982·1 991·3 o04·5 o00-2 o10·1 o12·0 o10·1 o1	mb. o19·0 o19·0 o19·0 o19·1 o10·1 o1	mb. o19·5 o12·10 o14·3 o10·2 o12·8 o19·1 o14·8 o10·2 o05·5 991·4 987·5 994·0 o04·2 o14·9 o19·1 o10·9 982·3 o04·9 994·8 1007 o5 1010	mb. 019·9 021·8 013·3 013·3 019·1 014·4 010·2 005·5 987·4 994·7 005·0 011·7 010·5 012·9 014·2 007·5 011·2 005·7 982·3 995·2 004·9 000·5 001·4 995·8 1007 08	mb. o20·5 o21·6 o20·5 o21·6 o20·7 o12·2 o20·3 o20·7 o12·2 o20·3 o2	mb. o20.8 6020.9 6012.8 6012.4 6019.6 6012.8 6012.4 6019.6 6012.8 6012.4 6019.6 6012.8 6019.8 6011.3 6012.8 6012.0 6012.8 6012.0	mb. 8016·7 0022·5 8017·3 8010·5 8010·5 8010·5 8010·5 8010·5 8010·6		

17. Aberdeen: H_b (height of barometer cistern above M.S.L.) = 26.8 metres.

May, 1923.

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D	ay.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noor	n 13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
1	I		mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb. 010·2	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb, 012·6	mb.	mb.	mb.	mb.	mb.	mb.
1	2	013.3	013.3	013.7	014	1 014.6	015.4	016.1	017.5	018.8	019.8	020.5	021.2	021.5	021.6	021.0	021.7	021.5	021.5	021.5	021.7	021.7	021.4	020.9	020.5	018.8
	3 4	009.2	009.1	008.8	008	5 008 -	7 008 +6	008.6	008.2	008.0	007.5	006.6	006.0	005.2	004.	1 004 0	004.3	004.7	005.0	005.4	005.6	005.5	005.6	005.5	005.3	006.4
	5	1	l	1		i		1	į				j]	1		1	l		1				1	İ	005.0
	6	002.8	002.5	002.4	002:3	3 002 . 7	003.0	003.5	004.0	004.3	004.5	005·0	004.9	005.0	005.0	005.2	005.8	005.6	006.4	007.4	008.6	009.5	011.4 010.1	010.5	011.0	005 · 3
	8	010.0	010.4	010.2	010.1	1 010.3	010.4	010.4	010.3	010.1	009.9	009.9	009.4	009 2	009	009.7	010.0	009.9	009.7	009.6	009.7	009.7	009.4	000.1	008.7	009.0
	9 10	008.2	007.8	007.6	007.2	2 006.8	006.5	004.0	005.3	004.4	003.0	001.5	999.8	997.9	996.4	993.3	990.5	989.1	986.4	985.7	984.6	984.2	983.8	983.5	983.3	005·7 997·3
	11	983.3	982.9	982.9	983.3	3 983.6	983.9	984.1	984.7	985.6	986∙0	986.4	987.1	987.6	987.8	987.8	987.9	987.9	987.9	988.4	988.5	988.5	988.4	988.5	988.5	986 - 2
1	12 13																									990·0
Level	14 15	993.2	993.4	993.8	993.8	993.7	993.7	994.2	994.3	994.6	994.8	994.7	994.7	994.6	994.7	994.7	994.7	994.7	994.9	995.3	995.7	995.8	995.9	996∙1	996.3	994·6 995·8
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Station	16 17	999•6	999.9	999.7	999.1	1998-6	998.4	998.0	998.4	999.2	000.3	001.0	001.8	002.6	003.3	004.1	004.8	005.5	005.6	006.9	008.2	000.1	009.8	010.3	010.2	996·3
Sta	18 19																									011·6
ĺ	20	000.0	999.7	999.4	999.2	999.0	998.8	998•6	998.3	997.8	997.2	996.7	995.9	995.4	994.7	993.8	992.9	992.1	991.8	991.8	992.0	992.4	992.3	992.3	992.5	995.8
	21	993.0	993.2	994.3	994.7	995.3	996.2	997.0	997.7	998.3	999.1	999.7	000.4	000.7	001.0	001.5	002.2	002.7	003.3	004.4	004.9	005.7	006.4	006.8	007.2	999.9
	23	013.1	012.9	012.7	012.5	012.5	012.4	012.7	013.0	013.3	013.6	013.7	013.7	013.8	014.0	014.4	014.7	014.9	015.5	015.8	016.4	016.7	016.7	016.8	016.9	014.2
	24 25																									010·2
	26	005.1	005.1	005.8	006.1	006-6	006.8	007.1	008.2	008.6	009.3	009.7	010.0	010.3	010.0	011.5	011.7	012.1	012.8	013.4	013.7	014.2	014.4	014.7	015.0	009.9
	27	015.3	015.7	016.0	016.5	017.1	017.7	018.2	018.9	019.5	020.2	020.6	020.7	021.2	021.4	021.4	021.4	021.5	021.8	021.9	021.8	021.4	021.5	021.5	021.3	019·6 023·6
	29	026.1	026.0	025.8	025.8	025.7	025.8	025.9	026.2	026.0	025.7	025.2	025.3	025.1	024.0	024.3	023.8	023.7	023.4	023.5	023.3	023.3	023.4	023.1	023.0	024 · 8
							İ																			021.7
	31					-			ļ				Í	<u> </u>	·	ļ			·							023.2
Mean (Statio	n level)	•28	.10	.18	·15	27	.39	.55	.73	∙86	.93	∙98	·96	.95	93	.82	:74	. •70	.73		• 0 9	•23	·24	22	1.16	.74
Mean (Sea le	vel)	10 0 9	1009																	1010						
				121		ı Je	.69	.84	.02	.12	·2 I	•26	.23	44	40	.09	041	90	01	·2I	.38	53	.54	.52	47	·03
18.	Aberd	een :					·	.041	102	151	-21	*20	231	42		109	021	90	01	1 -21	1 .38	.53	.54			
18.	Aberd	een :	H _b =	= 26	·8 m	etres														.21				Jun	e, 19	
18.		mb. 022·9	Hb =	= 26 · mb. o22·3	·8 m	mb.	mb.	mb. 022·1	mb. 022·1	mb.	mb.	mb. 022·0	mb. 022•0	mb. 022·1	mb. 022·1	mb. 022·5	mb.	mb. 022·9	mb. 023·6	mb.	mb. 024·5	mb. 025°0	mb.	Jun mb. 025.4	mb.	mb.
18.	1 2 3	mb. 022·9 025·7 020·2	Hb = mb. 022.7 025.7 019.6	= 26· mb. 022·3 025·8 019·3	mb. o22.3 o25.6 o18.8	mb. 3022·3	mb. 022·0 025·7	mb. 022·1 025·8 017·5	mb. 022·1 025·9 017·1	mb. 022·1 025·5 016·7	mb. 022·2 025·4 015·8	mb. 022·0 025·0 015·2	mb. 022·0 024·2 014·6	mb. 022·1 023·4 013·7	mb. 022·1 022·7 012·8	mb. 022·5 021·9	mb. 022·7 021·6 012·4	mb. 022·9 021·3	mb. 023·6 021·7 011·8	mb. 024·1 021·5 011·8	mb. 024·5 021·0	mb. 025·0 021·2 012·4	mb. 025·3 021·3	Jun mb. 025.4 021.0 013.0	mb. 025.5 020.5	mb. 023·7 023·7
18.	1 2 3 4	mb. 022·9 025·7 020·2	Mb = mb. 022.7 025.7 019.6 013.4	= 26. mb. 022.3 025.8 019.3 013.6	mb. 022:3 025:6 018:8	mb. 3022·3 0025·7 8018·5	mb. 022·0 025·7 017·9	mb. 022·1 025·8 017·5	mb. 022·1 025·9 017·1	mb. 022·1 025·5 016·7	mb. 022·2 025·4 015·8	mb. 022·0 025·0 015·2	mb. 022·0 024·2 014·6	mb. 022·1 023·4 013·9	mb. 022·1 022·7 012·8	mb. 022·5 021·9 012·7	mb. 022·7 021·6 012·4	mb. 022.9 021.3 011.8	mb. 023·6 021·7 011·8	mb. 024·1 021·5 011·8	mb. 024·5 021·0 012·0	mb. 025·0 021·2 012·4	mb. 025·3 021·3 012·5	Jun mb. 025.4 021.0 013.0 012.5	mb. 025.5 020.5 013.1	mb. 023·0 023·7
18.	1 2 3 4 5	mb. 022·9 025·7 020·2 013·3 012·1 009·5	Mb. 022.7 025.7 019.6 013.4 011.9	= 26· mb. 022·3 025·8 019·3 013·6 011·4 010·0	-8 m o22·3 o25·6 o18·8 o13·7 o11·1	etres mb. 3022·33 0025·7 013·9 1 010·9	mb. 022·0 025·7 017·9 014·1 0010·6	mb. 022·1 025·8 017·5 014·3 010·4	mb. 022·1 025·9 017·1 014·6 010·0	mb. 022·1 025·5 016·7 014·4 009·8	mb. 022·2 025·4 015·8 014·3 009·4	mb. 022·0 025·0 015·2 014·2 009·1	mb. 022·0 024·2 014·6 014·2 008·7	mb. 022·1 023·4 013·7 013·9 008·1	mb. 022·1 022·7 012·8 013·5 007·5	mb. 022·5 021·9 012·7 013·1 006·6	mb. 022·7 021·6 012·4 012·8 005·8	mb. 022·9 021·3 011·8 012·3 005·3	mb. 023.6 021.7 011.8 012.5 004.9	mb. 024·1 021·5 011·8 012·4 004·7	mb. 024·5 021·0 012·0 012·4 006·1	mb. 025·0 021·2 012·4 012·6 007·4	mb. 025·3 021·3 012·5 012·7 008·0 015·0	mb. 025·4 021·0 013·0 012·5 008·6	mb. 025·5 020·5 013·1 012·4 009·1	mb. 023.0 023.7 015.2 013.4 008.7 012.4
18.	1 2 3 4 5	mb. 022·9 025·7 020·2 013·3 012·1 009·5 015·0 006·5	Mb. 022.7 025.7 019.6 013.4 011.9 009.7 014.8 004.6	= 26· mb. 022·3 025·8 019·3 013·6 011·4 010·0 014·5 004·3	-8 m mb. 022·3 025·6 018·8 013·7 011·1	etres mb. 3022·3 5025·7 8018·5 7013·6 1010·6 2010·6	mb. 022·0 025·7 017·9 014·1 0010·6	mb. 022·1 025·8 017·5 014·3 010·4 010·8 014·7 000·6	mb. 022·1 025·9 017·1 014·6 010·0 011·3 014·7 999·8	mb. 022·1 025·5 016·7 014·4 009·8 011·5 014·7	mb. 022·2 025·4 015·8 014·3 009·4 012·1 014·2 998·6	mb. 022·0 025·0 015·2 014·2 009·1 012·4 013·6 998·6	mb. 022·0 024·2 014·6 014·2 008·7 012·6 013·4	mb. 022·1 023·4 013·7 013·9 008·1 012·8 012·9	mb. 022·1 022·7 012·8 013·5 007·5 012·9 012·4	mb. 022·5 021·9 012·7 013·1 006·6 013·1 011·8	mb. 022·7 021·6 012·4 012·8 005·8 0013·3 011·2 095·6	mb. 022·9 021·3 011·8 012·3 005·3 013·9 010·8	mb. 023.6 021.7 011.8 012.5 004.9 014.2 010.6	mb. 024·1 021·5 011·8 012·4 004·7 014·4 010·1	mb. 024·5 021·0 012·0 012·4 006·1 014·7 010·0 996·1	mb. 025.0 021.2 012.4 012.6 007.4 015.0 009.3 996.4	mb. 025·3 021·3 012·5 012·7 008·0 015·0 009·0 996·5	mb. 025·4 021·0 013·0 012·5 008·6 015·1 008·2	mb. 025·5 020·5 013·1 012·4 009·1 015·2 007·2 995·2	mb. 023·0 023·7 015·2 013·4 008·7 012·4 012·5 998·9
18.	1 2 3 4 5 6 7 8	mb. 022·9 025·7 020·2 013·3 012·1 009·5 015·0 006·5 994·8	Mb. o22.7 o25.7 o19.6 o13.4 o11.9 o09.7 o14.8 o04.6 994.0	= 26 · mb. o22·3 o25·8 o19·3 o13·6 o11·4 o10·0 o14·5 o04·3 o94·1	-8 m	etres mb. 3022·3 5025·7 7013·5 7010·5 7014·7 902·2 1994·2	mb. 022·0 025·7 017·9 014·1 010·6	mb. 022·1 025·8 017·5 014·3 010·4 010·8 014·7 000·6 995·1	mb. 022·1 025·9 017·1 014·6 010·0 011·3 014·7 999·8	mb. 022·1 025·5 016·7 014·4 009·8 011·5 014·7 998·9 996·5	mb. 022·2 025·4 015·8 014·3 009·4 012·1 014·2 998·6 997·3	mb. 022:0 025:0 015:2 014:2 009:1 012:4 013:6 998:6	mb. 022·0 024·2 014·6 014·2 008·7 012·6 013·4 997·4 998·3	mb. 022·1 023·4 013·7 013·9 008·1 012·8 012·9 997·1 998·7	mb. 022·1 022·7 012·8 013·5 007·5 012·9 012·4 996·7	mb. 022·5 021·9 012·7 013·1 006·6 013·1 011·8 995·7	mb. 022·7 021·6 012·4 012·8 005·8 013·3 011·2 995·6 000·0	mb. 022·9 021·3 011·8 012·3 005·3 013·9 010·8 995·3 000·4	mb. 023.6 021.7 011.8 012.5 004.9 014.2 010.6 995.5	mb. 024·1 021·5 011·8 012·4 004·7 014·4 010·1 996·0 000·6	mb. 024·5 021·0 012·0 012·4 006·1 014·7 010·0 996·1	mb. 025·0 021·2 012·4 012·6 007·4 015·0 009·3 996·4 000·5	mb. 025·3 021·3 012·5 012·7 008·0 015·0 009·0 996·5	mb. 025·4 021·0 013·0 012·5 008·6 015·1 008·2 995·9	mb. 025·5 020·5 013·1 012·4 009·1 015·2 007·2 995·2 998·5	mb. 023.0 023.7 015.2 013.4 008.7 012.4 012.5 998.9 997.6
18.	1 2 3 4 5 6 7 8 9	mb. 022·9 025·7 020·2 013·3 012·1 009·5 015·0 006·5 994·8 997·8	Hb = mb. 022·7 019·6 013·4 011·9 009·7 014·8 004·6 996·7	= 26· mb. 022·3 025·8 019·3 013·6 011·4 010·0 014·5 004·3 994·1 996·2	-8 m mb. 022·3 025·6 018·8 013·7 011·1 010·2 014·7 002·9 994·3	mb. 3022·3 6025·7 8013·6 1010·6 2010·6 7014·7 9002·2 1994·2 1994·2	mb. 022·0 025·7 017·9 014·1 010·6 010·6 7 014·7 001·5	mb. 022:1 025:8 017:5 014:3 010:4 010:8 014:7 000:6 995:1	mb. 022·1 025·9 017·1 014·6 010·0 011·3 014·7 999·8 995·9	mb. 022:1 025:5 016:7 014:4 009:8 011:5 014:7 998:9 996:5 995:6	mb. 022·2 025·4 015·8 014·3 009·4 012·1 014·2 998·6 997·3 994·0	mb. 022.0 025.0 015.2 014.2 009.1 012.4 013.6 998.6 997.6	mb. 022·0 024·2 014·6 014·2 008·7 012·6 013·4 997·4 998·3	mb. 022·1 023·4 013·7 013·9 008·1 012·8 012·9 997·1 998·7 993·9	mb. 022·1 022·7 012·8 013·5 007·5 012·9 012·4 996·7 999·2	mb. 022·5 021·9 012·7 013·1 006·6 013·1 011·8 995·7 999·6	mb. 022·7 021·6 012·4 012·8 005·8 013·3 0011·2 995·6	mb. 022·9 021·3 011·8 012·3 005·3 013·9 010·8 995·3 000·4	mb. 023·6 021·7 011·8 012·5 004·9 014·2 010·6 995·5 000·6	mb. 024·1 021·5 011·8 012·4 004·7 014·4 010·1 996·0 000·6	mb. 024·5 021·0 012·0 012·4 006·1 014·7 010·0 996·1 000·6	mb. 025·0 021·2 012·4 012·6 007·4 015·0 009·3 996·4 000·5	mb. 025·3 021·3 012·5 012·7 008·0 015·0 009·0 996·5 000·0	mb. 025·4 021·0 013·0 012·5 008·6 015·1 008·2 995·9 999·0 003·5	mb. 025·5 020·5 013·1 012·4 009·1 015·2 007·2 995·2 998·5 004·0	mb. 023.0 023.7 015.2 013.4 008.7 012.4 012.5 998.9 997.6
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weam ——Station Level ———————————————————————————————————	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mb. 022:9 025:7 020:2 013:3 012:1 009:5 015:0 006:5 994:8 997:8 012:1 017:4 013:9 012:7 014:8 010:0 012:7 012:5 016:8	mb. 022·7 019·6 013·4 016·7 099·7 009·7 009·7 005·6 012·4 017·7 013·4 012·6 014·2 009·9 016·7 015·4 016·7 015·4 016·7 016·7 016·7 016·7	= 26· mb. 022·3 025·8 019·3 013·6 011·4 010·0 014·5 004·5 005·5 002·5 003·5 012·7 013·2 012·8 016·6 013·1 016·7 015·3 016·8 018·8 019·4 013·3 1013	8 m mb. 022-3 025-6 013-7 011-1 010-2 014-7 994-7 996-6 021-7 0013-7 013-7 014-7 012-7 013-7 014-7 012-7 013-7 015-7 015-7 016-7 015-7 016-7 015-7 016-7 017-7 01	etres mb.	mb. 022·0 025·7 017·9 014·1 010·6 0010·6 0010·6 0096·9 0099·8 0020·4 0020·5 0012·7 0016·4	mb. 022·1 022·8 017·5 014·3 010·4 010·8 011·6 019·2 002·4 016·2 012·8 013·6 018·9 012·4 016·8 015·7 016·7 017·9 019·8 012·5 1013	mb. 022·1 025·9 017·1 014·6 010·0 011·3 014·7 999·8 995·9 995·6 012·9 018·5 002·8 017·2 012·9 013·1 013·1 013·1 017·0 015·8 016·9 018·1 019·9 012·7 1013	mb. 022-1 025-5 016-7 014-4 009-8 011-5 095-6 017-8 017-5 002-6 017-8 012-2 014-3 019-0 012-8 013-0 018-8 017-0 015-9 016-8 018-3 019-9 016-8 018-3 019-9 012-6 1013	mb. 022-2 025-4 015-8 014-3 009-4 012-1 014-2 998-6 997-3 994-0 015-1 015-8 002-1 018-4 011-7 014-9 019-2 012-6 012-9 019-6 012-4 009-9 012-6 017-2 016-0 017-2 016-0 018-0 019-9 019-6	mb. 022.0 025.0 015.2 014.2 009.1 012.4 013.6 998.6 999.0 016.4 013.9 002.9 018.7 011.1 014.9 019.3 012.5 012.8 019.7 015.0 017.1 016.3 017.0 017.1 016.3 017.0 017.8 019.6 012.7 — 1013	mb. 022·0 024·2 014·6 013·4 998·3 994·0 016·9 010·4 015·0 010·3 012·3 012·3 017·3 017·6 016·2 017·3 017·6 016·2 017·3 017·8 019·6 012·5 1017·0 016·2 017·3 017·8 019·6 012·5 1017·6 012·5 1	mb. 022·1 023·4 013·7 013·9 008·1 998·7 993·9 017·9 010·4 004·1 018·9 010·2 015·1 018·6 012·1 019·4 001·9 010·0 010·0 017·9 010·0 017·9 010·0 017·9 010·0 017·9 010·0 017·9 010·0 017·9 010·0 01	mb. 022·1 02	mb. 022·5 021·9 012·7 013·1 006·6 013·1 011·8 995·7 999·6 994·9 019·4 009·1 005·0 019·0 009·3 015·3 018·6 011·2 012·8 019·3 011·3 016·9 016·3 016·9 017·8 018·0 018·3 011·9 1012	mb. 022.7 021.6 012.4 012.8 005.8 013.3 011.2 095.6 000.0 095.6 000.5	mb. 022·9 021·3 011·8 0012·3 0005·3 0015·3 0005·3 0005·3 0005·4 0996·6 005·8 018·5 0005·8 018·5 0005·8 011·2 0011·6 0012·8 011·2 0011·6 0012·8 011·2 0011·6 0012·8 011·2 0011·6 0	mb. 023·6 021·7 011·8 021·7 014·2 010·6 997·4 021·4 008·7 007·2 018·4 001·8 011·8 016·4 015·7 017·0 018·2 018·4 017·5 017·5 017·6 018·2 018·4	mb. 024·1 021·5 011·8 012·4 004·7 014·4 010·1 996·0 021·8 008·0 018·4 009·0 015·9 011·4 013·2 018·3 011·4 012·2 018·3 011·4 015·5 017·1 018·5 018·9 017·3 012·3 1012	mb. 024:5 021:0 012:0 012:4 006:1 014:7 010:0 0996:1 000:6 000:4 022:3 009:3 016:1 016:5 012:0 013:8 016:5 015:7 017:4 018:5 019:1 017:3 012:4	mb. 025.0 021.2 012.4 012.6 007.4 015.0 009.3 996.4 000.5 001.3 022.8 008.7 009.5 018.2 010.0 016.3 016.5 012.6 017.2 011.1 013.7 016.9 015.7 017.6 019.1 019.2 016.6 019.2	mb. 025·3 021·3 012·5 012·7 010·5 015·6 013·6 017·7 019·3 019·1 016·6 013·0 11013	Jun mb. 025·4 021·0 013·0 018·1 098·2 999·0 003·5 019·1 016·9 013·0 015·5 016·2 016·2 016·2 016·2 016·2 016·2 013·0 016·2 016·2 013·0 016·2 013·0 016·2 016·2 013·0 016·2 013·0 016·2 013·0 016·2 013·0 016·2 013·0 016·1	mb. 025.5 o120.5 o13.1 o12.4 o15.2 o14.5 o15.6 o15.6 o15.6 o15.6 o15.6 o15.6 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.5 o15.6 o15.6 o15.5 o15.6 o	mb. 023.0 023.7 015.2 013.4 008.7 012.4 012.5 998.9 997.6 997.1 015.5 014.1 005.1 017.8 012.4 013.3 018.0 012.1 010.8 012.7 014.9 016.4
Mean (Station Mean)	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 177 18 19 20 21 22 23 24 25 26 27 28 29 30 n level)	mb. 022:9 025:7 020:2 013:3 012:1 009:5 015:0 006:5 994:8 012:2 016:5 012:1 017:4 013:9 012:7 014:8 010:0 012:7 014:8 010:0 012:7 014:8 010:0 012:7 014:8 010:0 012:7 014:8 010:0 012:7 014:8 010:0 012:7 014:8 010:0 012:7 014:8 015:4 017:0 014:5	mb. 022·7 019·6 013·4 011·9 009·7 014·8 094·0 996·7 005·2 012·4 017·7 013·4 012·9 016·6 019·1 019·1 019·1 019·5 014·10 01016	= 26· mb. 022·3 025·8 019·3 013·6 011·4 010·0 014·5 004·3 096·2 005·5 003·5 012·7 017·9 013·2 012·8 016·6 013·1 016·7 015·3 016·8 019·4 013·3 07 1016 1016·1	8 m mb. 022-3 025-6 018-8 011-1 010-2 0994-1 0996-0 012-1 013-7 016-0 012-1 016-0 018-0 016-7 018-0 019-1 016-0 018-0 019-1 018-0 019-0 0	etres mb. 3022-33 5025-7 5018-5 7013-5 7014-7 902-2 904-2 904-2 904-2 904-2 904-3 904-4 904-2 904-6 904-	mb. o22·0 o25·7 o17·9 o10·6	mb. 022·1 025·8 017·5 014·3 010·4 010·8 014·0 995·1 996·6 011·6 019·2 002·4 016·2 013·6 014·0 018·9 012·8 013·0 018·2 012·4 016·3 016·7 016·7 017·9 019·8 012·5 1013	mb. 022·1 025·9 017·1 014·6 010·0 011·3 014·7 999·8 995·9 995·6 012·9 018·5 002·8 017·2 012·9 014·1 018·5 010·2 014·1 018·5 010·2 014·1 019·9 018·1 019·9 012·7 1013 -28	mb. 022-1 025-5 016-7 014-4 009-8 011-5 096-5 095-6 014-3 017-5 002-6 017-8 012-3 012-3 012-3 012-3 012-3 012-5 010-9 012-6	mb. 022-2 025-4 015-8 014-3 009-4 012-1 014-9 998-6 997-3 994-0 015-1 018-4 011-7 014-9 019-2 012-6 012-6 012-4 009-9 012-6 012-6 017-2 016-0 017-2 016-0 017-2 016-0 017-2	mb. 022.0 025.0 015.2 009.1 012.4 013.6 999.6 6 999.0 016.4 013.6 099.6 012.5	mb. 022.0 024.2 014.6 014.2 008.7 012.6 013.4 998.3 994.0 016.9 012.2 003.7 019.0 010.4 015.0 019.0 017.3 017.6 015.1 017.0 009.8 019.6 015.1 017.0 016.2 017.3 017.8 019.6 012.5 1012.5 1012.5 1012.5 1012	mb. 022·1 023·4 013·7 013·9 008·1 999·1 998·7 993·9 010·4 004·1 018·9 010·2 015·1 013·0 019·4 011·9 010·0 015·2 016·6 017·5 017·8 019·1 012·2	mb. 022·1 022·1 022·7 012·8 013·5 007·5 012·9 099·2 0994·1 018·9 009·6 015·2 018·8 019·3 010·3 010·3 010·3 010·3 010·3 010·3 011·5 016·4 016·7 017·9 018·0 018·5 016·4 016·7 017·9 018·0 018·5 011·9 018·0 011·9 018·0 011·9 018·0 011·9 018·0 011·9 018·0 010·7 017·9 018·0 018·5 011·9 018·0 011·9 018·0 011·9 018·0 011·9 018·0 011·9 018·0 011·9 018·0 011·9 018·0 011·9 018·0 011·9 018·0 011·9 011·0 018·0 011·9 018·0 011·9 011·0 018·0 011·9 011·0 018·0 011·9 011·0 018·0 011·9 011·0 0	mb. 022·5 021·9 012·7 013·1 006·6 013·1 011·8 9995·6 994·9 019·4 009·1 005·0 019·0 009·3 015·3 018·6 011·2 012·8 013·0 015·9 016·3 016·9 017·8 018·0 018·3 011·9 1012	mb. 022.7 021.6 012.8 005.8 013.3 011.2 0995.6 000.0 015.3 018.8 009.0 015.3 018.0 019.1 011.0 012.9 011.0 012.9 011.0 015.3 018.2 0	mb. 022·9 021·3 011·8 012·3 0005·3 0015·8 012·3 0005·3 0005·4 0996·6 005·8 016·5 010·6 011·9 016·9 017·9 018·2 017·8 011·9 016·9 01102 63 1015	mb. 023·6 021·7 011·8 012·5 004·9 014·2 010·6 997·4 008·7 007·2 018·4 008·9 015·8 017·2 010·7 012·9 018·6 011·8 013·8 017·2 018·4 017·5 011·8 011·8	mb. 024·1 021·5 011·8 012·4 004·7 014·4 010·1 996·0 021·8 008·0 018·4 009·0 015·9 016·9 011·4 013·2 013·3 011·4 012·2 013·7 016·4 015·5 017·1 015·5 017·1 018·5 017·3 012·3 1012 1016	mb. 024:5 021:0 012:0 0012:4 006:1 014:7 010:0 000:4 022:3 000:4 022:3 000:1 08:7 018:2 009:3 016:1 016:5 012:0 011:2 012:2 01	mb. 025.0 021.2 012.4 012.6 007.4 015.0 009.3 996.4 000.5 001.3 022.8 008.7 009.5 018.2 010.0 016.3 016.5 012.6 014.6 017.2 017.6 019.1 019.2 016.6 019.1 019.2 016.6 012.9 01013	mb. 025:3 021:3 021:3 012:7 008:0 015:0 009:0 099:0 002:5 002:7 007:9 010:5 016:6 015:8 017:7 019:3 017:0 01	Jun mb. 025·4 021·0 012·5 008·2 095·9 0995·9 0995·9 0995·9 010·7 016·2 015·5 015·5	mb. 025.5 o20.5 o13.1 o12.4 o09.1 o15.2 o995.2 o04.7 o17.4 o17.2 o14.5 o12.9 o16.5 o15.6 o10.3 o12.8 o15.5 o17.4 o15.2 o13.3 o19.4 o15.2 o	023. mb. 023.0 023.7 015.2 013.4 008.7 012.4 012.5 9987.6 997.1 015.5 014.7 017.8 012.4 013.3 018.0 012.1 010.8 012.7 014.9 016.4 016.4 016.4 017.6 018.5 018.6 012.7 1013
Mean (Station Tevel	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 177 18 19 20 21 22 23 24 25 26 27 28 29 30 n level)	mb. 022:9 025:7 020:2 013:3 012:1 009:5 015:0 006:5 994:8 997:8 012:2 016:5 012:1 017:4 013:9 012:9 016:7 014:8 010:0 012:7 012:5 015:4 017:0 019:2 019:4 017:0 019:2 019:4 017:5 019:4 017:5	Mb = mb. 022·7 025·7 019·6 013·4 011·9 009·7 014·8 004·6 994·0 996·7 015·4 017·7 013·4 012·9 016·6 019·1 016·7 015·4 019·5 014·0 014·0	= 26· mb. 022·3 025·8 019·3 013·6 011·4 010·0 014·5 004·3 096·2 005·5 003·5 012·7 017·9 013·2 012·8 016·6 013·1 016·7 015·3 016·8 019·4 013·3 07 1016 1016·1	8 m mb. 022-3 025-6 018-8 011-1 010-2 0994-1 0996-0 006-1 0013-9 0014-0 013-9 011-1 0010-1 0014-0 012-0 012-0 016-9 012-0 016-9 012-0 016-9 012-0 016-9 012-0 016-9 012-0 016-9 012-0 016-9 012-0 016-9 012-0 016-9 012-0 016-9	etres mb. 3022·3 3025·7 3018·5 1010·9 2010·9 2010·9 3002·1 3002·	mb. o22·0 o25·7 o17·9 o10·6	mb. 022·1 025·8 017·5 014·3 010·4 016·2 013·6 018·9 012·8 013·0 018·2 012·4 016·2 013·6 015·7 016·7 017·9 019·8 012·5	mb. 022·1 025·9 017·1 014·6 010·0 011·3 014·7 999·8 995·9 995·6 012·9 018·5 002·8 017·2 012·9 014·1 018·5 010·2 014·1 018·5 010·2 014·1 019·9 018·1 019·9 012·7 1013 -28	mb. 022-1 025-5 016-7 014-4 009-8 011-5 096-5 095-6 014-3 017-5 002-6 017-8 012-3 012-3 012-3 012-3 012-3 012-5 010-9 012-6	mb. 022·2 025·4 015·8 014·3 009·4 012·1 014·2 998·6 015·1 018·4 011·7 014·9 019·2 012·6 012·9 019·6 012·4 009·9 012·3 014·6 017·2 016·0 016·8 019·9 012·6 1013 ·18	mb. 022.0 025.0 015.2 009.1 012.4 013.6 998.6 999.6 994.0 016.4 013.9 012.5 012.5 012.1 009.7 011.7 01	mb. 022.0 024.2 014.6 014.2 008.7 012.6 013.4 998.3 994.0 016.9 012.2 003.7 019.6 011.7 009.8 012.6 011.7 009.8 012.6 012.5 017.3 019.6 012.5 017.8 019.6 012.5 017.8 019.6 012.5 017.8 019.6 012.5 019.6 019.6 012.5 019.6 019.6 012.5 019.6 019.6 012.5 019.6 019.6 012.5 019.6 019.6 012.5 019.6 019.6 012.5 019.6 019.6 012.5 019.6 019.6 012.5 019.6 019.6 012.5 019.6 019.6 012.5 019.6 019.6 012.5 019.6 019.6 012.5 019.6 01	mb. 022·1 023·4 013·7 013·9 008·1 999·1 998·7 993·9 010·4 004·1 018·9 010·2 015·1 013·0 019·4 011·9 010·0 015·2 016·6 017·5 017·8 019·1 012·2	mb. 022·1 022·7 012·8 013·5 007·5 00	mb. 022·5 021·9 012·7 013·1 006·6 013·1 011·8 995·6 994·9 019·4 009·1 005·0 009·3 015·3 018·6 011·2 012·8 019·3 016·3 016·3 016·3 016·3 016·3 016·3 016·3 016·3 016·3 016·3 016·3 016·3	mb. 022.7 021.6 012.8 005.8 013.3 011.2 0995.6 000.0 015.3 018.8 009.0 015.3 018.0 016.1 016.2 016.2 016.2 016.2 016.3 017.9 0	mb. 022·9 021·3 001·8 012·3 005·3 013·9 013·9 005·3 003·9 005·4 0996·6 0220·9 008·6 005·8 015·5 017·5 010·6 012·8 011·6 012·8 011·2 011·6 012·8 011·9 016·9 018·2 017·8 011·9 016·9 011·9 018·2 017·8 011·9 018·2 017·8 011·9 018·2 017·8 011·9	mb. 023·6 021·7 011·8 012·5 011·8 016·4 017·5 011·8 011·8 011·8 011·8 011·8 011·8 011·8 011·8 011·8 011·8 011·8 011·8 011·8 011·8 011·8 011·8 011·8 01	mb. 024·1 021·5 011·8 012·4 004·7 014·4 000·6 999·0 021·8 008·0 018·4 009·0 011·4 013·2 018·3 011·4 012·2 013·7 016·4 015·5 017·1 018·1 018·1 01	mb. 024:5 021:0 012:4 006:1 014:7 010:0 0996:1 000:4 022:3 009:1 008:7 018:2 009:3 016:1 016:5 012:0 011:2 012:2 012:2 012:2 013:6 018:5 017:4 018:5 017:4 017:3 017:4	mb. 025.0 021.2 012.4 012.6 007.4 015.0 009.3 996.4 000.5 001.3 022.8 008.7 009.5 018.2 010.0 016.3 012.6 017.2 011.1 012.7 016.9 015.7 017.6 019.1 019.2 011.1 019.2 011.1 019.2 015.7	mb. 025:3 021:3 021:3 012:7 008:0 015:0 009:0 002:5 000:5 010:7 016:6 013:0 017:7 016:6 013:0 017:0 01	mb. 025·4 021·0 013·0 013·0 013·0 012·5 008·6 015·1 008·2 995·9 999·0 003·5 011·1 016·9 012·7 016·2 015·9 010·7 013·0 015·5 019·5 019·5 019·5 019·5 019·5 019·5 019·5 019·5 019·5 019·5 019·5 019·5 019·5 019·5 019·5 019·5 019·5 019·5 019·5	mb. 025.5 020.5 020.5 020.5 020.5 020.7 020.7 020.7 020.7 020.4 020.7 02	023. mb. 023.0 023.7 015.2 013.4 008.7 012.4 012.5 998.9 997.6 997.1 015.5 014.1 005.1 017.0 011.8 014.7 017.8 012.4 013.3 018.0 012.1 010.8 010.8 01

19. Aberdeen: H_b (height of barometer cistern above M.S.L.) = 26.8 metres.

July, 1923.

19.	Aberde	en :	\mathbf{H}_b (heigh	tof	baron	neter	ciste	rn at	ove 1	M.S.L) =	20.0	meu	es.									• • • •	y, 1	J.U.
Da	ay.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.			13.	1	15.	16.	17.	18.	19.	20.	21.	22.	23.	'	Mean
<u></u> ↑		mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb. 012:0	mb.	mb.
1																										013.7
																										016.7
.	6	020.0	020.0	020.0	020.0	020.2	020.5	020.5	020.9	021.1	021.1	021.1	021.0	020.8	020.8	020.8	020.7	020.6	020.6	020.6	020.7	020.7	020.8	020.4	020.2	020.6
.	7 .	019.7	019.5	018.9	018.5	017.9	017.8	017.6	017.5	017.3	016.7	010.5	011.8	015.0	015.0	014.9	014.0	014.2	011.5	011.0	013.3	013.4	014.2	014.7	014.9	012.1
	_	O T # . 1	0 7 7 . 0	0.7.5.0	OTELO	OTCO	OTELO	OTE	OTh.O	017.2	OT7.2	OT7.2	017.2	IOT 7 · 4	1017:0	1017.7	101710	017.7	1017.7	0.010	010.0	0100	010 9	019 1	019 1	O1/ 1
	10	018.8	018.7	018.7	019.1	019.3	019.5	019.6	019.8	020.0	019.8	020.6	020.1	020.2	018.5	018.5	018.2	018.0	018.3	018.0	018.7	010.5	010.4	010.7	010.5	019 1
.	11	018-2	018-1	018.2	018.0	018.3	018.1	018.0	018.5	019.7	018.3	017.9	017.8	018.4	018-4	018-6	018.6	018-4	018-4	018-4	018.6	018.8	o18·8	o18·8	018.8	018.4
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Station Level	-6	000.0		008.8	008.6	008.5	008.6	008.8	000.0	000.3	000.5	000.7	000.7	000.0	000.0	000.0	000.0	999.9	999.6	999.7	999.8	000.2	000.3	000.1	000.5	999.5
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tat	18	1 ~ ~ ~ 6		LOOT.O	1000.0	1000.5	1002.0	1002.5	1004.2	004.7	005.2	1005.0	1005 · 8	10000.0	1000014	1007.1	10077.5	100770	1000.2	1000	OOG I	1009	1009 01	009 0	1009 4	005.7
Ϋ́	19 20	003.6	009.2	003.8	008.4	003.1	005.6	007.0	007.7	008.4	009.0	004.9	009.7	010.2	010.4	010.5	010.7	010.6	010.2	010.2	010.2	010.1	010.0	010.1	010.1	008.2
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	Aberde	mb.	H _b =	= 26·	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	Haa8+3	1998.7	998.7	1999:5	999.8	000.5	000.9	mb.	mb.	mb.	mb.
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20. A Station Level	Aberde 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 on level)	mb. 989.7 1 1 1 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1	Hb = mb. r999.1 1003 1003 1006 1006 1006 1006 1006 100	= 26· mb. 990·5 003·8 981·9 013·3 010·2 007·7 010·6 007·1 011·3 016·6 021·4 011·5 014·6 002·6 991·8 005·3 992·6 985·4 995·9 991·1 007·8 0988·8 002·4 992·5 002·0 1002 .80	mb. 990-90 988-90 992-6 002-0 11002 -838-8	mb. 991.7 994.3 904.3	mb. 992 · 2 004 · 1 1 986 · 2 015 · 7 017 · 2 016 · 3 006 · 2 011 · 4 026 015 · 6 011 · 9 012 · 3 092 · 1 092 · 2 006 · 7 003 · 0 093 · 4 1002 · 98 1006	mb. 992·9 004·6 987·8 016·0 016·8 010·1 005·8 012·3 006·9 012·4 018·1 020·8 0012·3 0015·7 013·8 012·3 996·6 992·5 006·9 004·9 986·5 997·5 991·6 008·6 008·6 002·7 1003 112	mb. 993.7 989.1 016.2 016.3 010.0 005.1 012.4 006.8 012.2 013.6 012.2 013.6 014.9 007.4 004.9 985.4 004.9 987.7 003.1 094.7 003.2	mb. 994·5 004·4 990·5 017·4 010·1 004·6 012·5 006·9 013·1 018·4 019·9 009·2 016·3 013·2 012·2 995·0 993·9 907·5 005·0 983·7 986·9 999·0 992·2 008·6 991·7 987·9 991·4 003·1 995·4 003·4	mb. 995.4 004.2 992.5 017.1 015.9 009.9 004.2 012.8 007.0 013.6 019.0 019.8 008.7 0012.1 994.3 995.1 007.7 004.8 982.4 987.3 998.7 992.9 008.3 991.5 988.0 992.1 002.7 003.7 1003 -44	mb. 996·1 993·9 017·9 015·6 004·0 012·9 007·2 013·4 019·3 019·7 008·1 016·2 012·4 011·9 993·8 996·1 008·0 004·9 981·1 987·6 993·8 992·8 992·8 003·8 003·8 1003 1006	mb. 996.4 995.2 018.3 014.9 009.2 003.9 012.7 007.5 013.6 019.6 018.9 008.3 016.0 011.7 993.3 090.7 993.3 980.1 987.9 999.5 995.4 006.9 998.6 993.5 001.8 997.1 003.8	mb. 997-2 997-0 018-7 014-3 009-5 004-0 012-7 007-9 014-0 020-0 018-3 008-1 016-0 011-0 992-9 998-3 008-0 04-6 979-5-9 98-3 999-1 996-8 006-1	mb. 998 c 2099 8	998·3 000·1 000·5 018·4 013·5 009·5 0019·6 011·0 011·0 092·3 999·4 004·2 1003 -72	998·7 999·0 002·0 018·7 013·1 009·3 004·4 011·9 008·4 013·9 020·7 016·9 008·9 015·4 010·7 992·4 000·6 008·0 003·7 980·4 990·0 998·6 000·4 003·2 989·7 987·6 996·6 999·1 1003 •78	998.7.5 997.6 997.6 997.6 903.7 019.2 002.9 005.1 011.2 008.4 014.2 020.9 016.7 009.8 015.1 011.1 010.5 992.1 981.5 998.4 000.9 001.9 989.6 987.5 998.4 004.6 004.6 005.1 004.6 006.1 004.6	999.5 995.3 995.3 905.3 0012.7 008.9 005.2 011.0 008.6 014.6 021.2 016.2 010.5 010.5 992.0 001.9 007.6 002.8 982.1 991.2 997.9 001.7 000.9 989.4 987.6 998.2 997.7 000.5	999.8 993.2 993.2 993.2 993.2 006.1 019.6 012.3 008.8 006.0 010.6 009.2 014.8 021.4 015.8 011.6 010.0 002.4 007.5 002.7 982.4 991.9 997.5 003.2 999.6 989.4 987.7 998.8 989.7 998.8 900.9 004.8 1003	000·5 991·8 007·6 019·7 012·2 008·9 006·6 019·3 015·5 015·3 012·2 015·3 017·2 009·5 992·1 007·7 002·3 983·5 997·2 004·2 998·5 989·5 987·8 999·8 999·8 999·8 999·8	000.9 990.5 008.5 019.8 010.5 015.8 021.4 015.2 015.3 011.2 008.9 992.1 003.9 007.3 001.5 983.4 994.1 001.6 005.2 1004.2 1004.2 1007.2	mb. 001.9 989.0 009.2 019.9 011.5 009.2 008.0 008.7 010.9 015.8 021.8 014.7 013.4 015.3 011.3 008.1 1992.1 004.4 007.3 000.7 984.7 993.6 994.9 006.0 996.4 988.9 988.1 001.1 995.3 1004.4 1007.3	mb. oo2·3 987·0 oo2·3 9887·0 oo2·3 9887·0 oo3·9 oo19·7 oo11·1 oo3·0 oo8·8 oo8·4 oo11·3 oo16·2 oo22·1 oo14·0 oo13·9 oo15·2 oo11·3 oo7·2 990·4 soo7·1 999·8 985·2 oo6·3 995·0 988.8 988·2 oo10·7 oo5·5 loo4 oo1·7	mb. 002-69 85-20 10-8 008-8 009-0 008-2 011-4 016-4 016-4 016-1 011-4 006-3 991-8 005-2 985-5 994-5 994-5 993-8 001-7 993-8 001-7 993-8 001-7 993-8 001-7 993-8 001-7	mb. 996·1 999·5 995·7 017·1 014·9 0006·0 011·1 008·2 013·5 019·3 018·5 010·5 010·5 995·5 997·4 7 007·1 003·9 985·2 988·8 997·2 004·3 8 997·2 1003 8 997·1 1003 7 1003 7 1003

21. Aberdeen: H_b (Height of barometer cistern above M.S.L.) = 26.8 metres.

September, 1923.

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1	5	013.4	012.9	011.9	011.0	010.3	1009.9	009.8	009.6	009.0	010.2	010.2	010.4	010.7	011.0	011.5	012.0	012.1	012.8	013.0	013.7	013.9	014.2	014.7	015.0	101
1	6								016.7																	
1	7	009.3	009.4	010.7	011.4	011.9	012.5	013.0	013.7	014.2	015.0	015.3	019.1	016.4	017.1	017.7	018.4	018.8	019.5	020.0	020.6	021.1	021.5	021.7	022.0	01
i	8	022.1	022.3	022.0	021.6	021.5	021.1	021.0	021.0	020.6	020.0	018.9	018.1	017.5	010.0	015.4	014.4	013.4	013.1	013.0	012.7	012.1	012.0	011.6	010.0	10
1	9								005.4																	
1	10	010.3	010.0	009.9	009.9	1009.9	010.0	010.3	010.9	011.4	011.4	011.5	011.4	011.1	011.3	011.8	011.7	011.8	011.9	011.9	011.8	011.5	011.3	010.8	010.2	101
! ⊣	11	009.3	008.2	007.4	006-5	005.7	004.8	004.3	003.5	002.6	001.6	000.6	999.4	998.6	998-1	997.0	996.3	996.6	995.4	995.0	994.5	993.5	993.4	993.6	993.3	3
Level	12	992.7	992.3	991.7	991.8	992.0	992.2	992.3	992.5	992.8	993.1	993.4	993.5	994.3	995.6	997.0	998.3	999.7	001.4	002.5	003.8	004.6	005.7	005.7	006.3	99
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Ħ	15	994.1	993.9	993.5	993.4	993.1	993.3	993.4	993.5	993.5	993.2	992.8	992.5	992.4	992.1	992.3	992.3	992.5	993.1	993.9	994.4	994.3	994.3	994:3	994.2	199
Station	16	994.0	994.1	994.1	994.2	994.5	994.9	995.4	995.9	996.5	997.1	997.6	998.4	998.9	999.6	000 · 2	000.7	001.5	002.1	002.7	003.3	003.5	003.4	003.5	003.4	99
ď	17	003.1	002.6	002.0	001.2	000.2	999.7	999.0	998.0	997.3	996.3	995.5	994.7	993.7	992.7	991.9	991.1	990.3	989.5	989.1	988.8	987.9	987.2	98 7∙0	986.8	3 99
Ž									988∙0																	
	19	992.6	992.8	993.2	993.8	994.6	995.2	995.7	995.8	995.7	995.4	995.4	995.5	995.4	994.8	993.7	993.3	992.7	992.3	992.0	991.9	991.9	992.2	992.2	992.6	99
	20	992.7	992.7	992.5	992.4	992.1	992.3	992.6	993.1	994.0	994.7	995.6	996.4	997.0	997.2	997.6	997.7	998.2	998.5	998.3	998.1	997.6	997.2	996.5	996.0	99
ŀ									994.4																	
	22	993.9	992.7	992 · I	991.3	990.5	989.6	988.4	988.4	988.4	988.6	988.5	988.3	988∙o	987.7	987.3	987.2	987.6	988∙0	988.4	988.5	988.5	988.5	988.6	988.5	9
Ì	23	988.4	988.4	988.3	988.3	988.4	988.7	989∙0	989.6	989.9	990∙1	990.5	990.9	991.2	991.6	992.0	992.5	993.4	994.3	995.1	995.8	996.1	996.6	997.0	997.5	99
									001.4																	
	25	997:5	996.4	995.0	993.8	992.9	992.1	991.4	990.5	990.1	989.4	988.9	988.9	988.9	988·8 	988.7	988.8	989.2	989.4	990.2	991.0	991.7	992.5	993.5	994.5	9
	26	995.8	997.0	997.6	998.8	000.1	001.3	002.3	003.4	004.4	005.2	oo6∙o	006.8	007.8	008.6	009.1	009.6	010-2	010.9	011.6	011.8	012.1	012.1	012.2	012.6	50
	27	012.8	012.0	012.5	012.6	012.6	012.2	012.0	011.6	011.3	010.9	010.3	009.9	009.0	008.6	008.0	007.5	007.3	007.1	007.0	006.6	006.3	005.9	005.4	004:5	5 0
	28	004.2	003∙8	003.5	003.9	004.5	005.2	007.1	009.8	011.1	012.7	013.6	014.4	015.2	015.8	016.4	017.3	017.7	018.5	018.9	019.4	019.3	020.0	020.1	010.0) (0
1	29	020.0	019.8	019.7	020.0	020.0	020.2	020.9	021.4	021.9	022.1	022.3	022.3	022.0	022.2	022.0	021.5	021.3	021.0	020.7	020.1	019.5	018.9	018.3	017.8	3 0
∤ 	30	017.4	016.6	016.2	015.8	015.5	015.4	015.2	015.5	015.1	014.8	014.7	014.0	013.2	012.8	012.3	011.8	011.2	011.5	011.4	010.8	010.4	010.3	009.3	009	30:
an		1004	1003	1003			1003		1004	1004	1004	1004	1004	1004	1004	1004	1004	1004	1004	1004	1004	1004	1004	1004	1004	Ire
	n level)	.13	.92	•73	.63	.59	•68	∙87	•03	•20	.18	.16	•17	•16	.19	•14	•09	.21	•37	•59	·74	-60	.61	•49	1 ⋅3€	<u> </u>
an	1								1007																	
a lev	7 e ɪ)	.39	.18	•99	89	-85	.94	.13	.28	.44	·4I	•39	•39	ા ∙વ8ો	·4I	•36	.31	·44	·60	-83	.99	·85	·86	•75	•62	۷.

22. Aberdeen: $H_b = 26.8$ metres.

October, 1923.

22.	Andru		110		O III	circs.																	·	Otono	.,	
		mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	l mb.	mb.	mb.	mb.	ı mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.
	I	009.3	009.3	009.1	009.1	009.3	009.5	010.2	010.4	010.9	010.9	010.8	010.7	010-3	010.3	010.4	010.2	010.4	010.4	010.2	010.0	009.3	008.6	007.9	∞6.8	009 · 8
1	2	005.6	004.6	003.3	002.2	001.5	002.6	004.0	004.7	006.0	007.0	007.3	008.1	007.9	008.2	008-4	1.800	008.2	008.5	5 008.4	008.0	007.8	007.3	006.7	005.9	1000.3
	3	005.0	004.3	003.4	002.6	002.1	001.0	001.7	8.100	001.0	002.1	002.5	002.9	003.3	003.8	004.4	005.3	006.0	006.0	007.7	008.4	009.2	010.0	0.110	011.8	004.6
	4	012.6	013.5	013.2	014.1	015.1	015.7	016.2	o16·5	017.3	017.6	017.8	017.5	017.4	017.2	017.3	017.0	016.0	016.0	016.7	015.9	015.2	014.2	014.1	013.4	015.5
	5	012.0	011.4	010.2	009.1	008.3	007.5	006.7	005.8	005.2	004.2	003.7	003.2	002.1	001.4	000.4	999.5	999.7	999.3	999 • 2	998.9	998.9	998.8	999.0	990.0	003.0
	6	999.0	999.0	998.8	998.4	998.4	998.2	998.1	998.3	998.4	998.3	997.9	997.7	997.9	998.2	998.3	998.7	999.3	000.0	000.5	000-8	001.1	001.3	001.4	001.2	999 • 1
İ	7	001.2	001.0	1000 - 5	1999 7	999.2	1998.0	997.2	996.5	996.0	995.4	994.6	994.4	1993.8	1993.8	994.2	994.2	994.2	994.0	1994 · I	1993.0	1993 4	993.2	1993.8	1994.4	1990.0
		995.0	995.3	995.8	996.5	997.0	997.6	998.1	998.4	998.9	999•2	999.3	999.5	999.7	999.3	999.4	999.3	998.5	997.8	3 996.6	995.4	993.9	992.5	990.0	987.6	1996 • 8
	9	985.9	984.3	982.0	982.4	982.5	982.3	982.3	982.4	982.7	982.8	983.6	984.6	984.9	985.6	986.3	987.6	989.4	991.c	992.4	993.5	994.6	995.8	996.9	997.5	987.0
l	10	997.6	997.7	997:3	997.1	997.2	990.9	990.0	996.5	995.6	995.4	994.9	994.0	993.5	993.0	992.4	992.1	992.3	992.5	992.4	992.5	992.4	992.2	992.3	992.4	994.0
1	11	992.8	992.7	993.1	993.6	994.0	994.2	994.7	995.3	995.9	996.6	997:4	997.9	998.5	998.7	998.7	999.0	998.9	999.2	999.2	998.9	998.7	998.0	997.3	996.5	996.6
	12	995.4	994.7	994.0	993·I	992.0	991.2	990.8	990.3	989.5	988.8	988·1	987.2	1986-5	1985.8	985.1	984.2	983.6	983.6	983·I	983.0	983∙0	982.7	982.0	982.0	987٠٥
Level	13	982.8	983 I	1983.2	983.4	983.7	1984.2	984.7	985.4	986.3	986.7	987.3	1987.8	988.3	988.9	080.1	1989.7	990.4	991.3	991.7	1992-2	1992.4	992.9	993.1	993.3	1902.0
e e	14	993.4	993.7	994.0	994.3	994.7	995.1	995.7	996∙0	996.4	996.8	997:3	997.7	998.2	998.9	999.3	999.9	000.4	001.1	001.0	002.1	002.4	002.0	003.1	003.2	998.0
\vdash	15	003.1	003.1	002.9	002.8	002.8	002.0	002.8	002.9	003.1	003.2	003.1	002.9	002.8	002.7	002.0	002.5	002.5	002.5	002.4	002.3	002.1	001.7	001.3	000.9	002
ជ	16	000.7	000.3	000.0	000.1	000.3	001.3	002.3	003.4	004.6	005.3	005.9	006.4	007.0	007.6	008.1	008.2	009.1	009.7	009.8	009.8	009.5	009.3	008.7	007.9	005.5
.음	17	007:3	006.5	006.4	006.7	007.7	008.5	000.3	010.3	0.010	011.6	011.7	012.0	012.2	012.3	012.3	012.6	012.8	013·I	013.0	013.1	013.1	012.9	012.8	012.2	010.9
Station	18	012.3	012.1	011.0	011.8	011.0	012.0	012.0	012.1	011.0	011.7	011.3	010.4	009.8	009.1	008.1	007.3	006.7	006.0	004.6	003.3	002.3	001.3	999.9	998.1	008.0
S	19	997.0	996.0	994.6	992.6	990.6	988.8	986.9	985.0	985.8	986.8	988.5	989.7	990.9	991.6	992.5	992.9	993.6	994.4	995.1	996.2	990.4	990.0	990.4	084.0	1992.3
1	20	990.3	995.8	995.2	994.0	994.0	994.0	994.0	994.0	993.9	993.3	993.1	992.5	992.1	991.4	991.5	1990.9	990.5	990.2	909.3	900.9	988.0	907 0	9000	904 9	992
Ì	21	983.6	982.1	980.4	978.3	976.6	974.4	972.9	971.7	971.1	971.1	972.2	973.1	973.9	974.3	974.5	974.7	974.9	975.0	974.7	974.8	975.0	975.3	975.2	975.4	975 • 4
I .	22	975.6	975.2	975.0	974.8	974.6	974.2	974.6	974.5	973.9	974.4	973.9	973.4	973·I	972.8	972.4	971.7	971.2	1970.5	1969.4	1909.0	1909.2	909.0	909.4	970.0	1972.7
	2.3	071.0	071.6	07I · Q	972.3	073.4	1073.7	1073.0	073.0	973.6	073.5	973·I	972.5	971.7	970.0	969.7	968.5	907.8	907·I	1900.0	1905.4	1904.9	1904.4	904.2	904 3	1970.1
İ	24	964.4	964.5	965.1	965.5	965.8	966.0	966.6	967.1	967.6	968∙0	968.3	968.6	969∙0	969.3	969.5	969.8	970.1	970.5	970.8	971.0	971.0	971.1	971.1	082.2	076 1
	25	971.2	971.3	971.4	971.6	971.9	972.2	972.7	973.7	974.3	975.2	976.0	976.7	977:3	977·8	978.0	978.5	979.1	979.5	979.7	979.9	900.5	900-9	901.3	902 2	9,0 1
- 1	26	083∙1	083.3	084.0	083.8	083.5	083.3	082.6	982.1	08т∙т	070.8	078.1	976.5	977.5	078.2	979.2	980.2	981.3	982.8	983.9	985 0	985.4	986.2	986.9	987.2	982 • 2
	27	1087:3	1.780	1.080 I	1984.8	1983-6	1082.5	1080.7	070.4	078.4	077.6	077.4	1978.0	1978.7	IQ78*QI	1978.3	1978.8	1979.0	1979 3	1979.4	1970.0	1970.0	9/04	9/0 0	9// 9	900)
	28	077.4	1077.2	1975.9	1975.0	976·I	077.2	1078.6	070.0	OST -2	08T-8	082.4	1983.0	1084.3	1984·81	985.8	1980.2	907.3	1987.0	1900.2	1900.0	1909.0	909.4	909 4	990 0	1903 0
	20	laaa•6i	001.5	1002.0	002.7	003.4	001.2	1004.8	005:0	006.6	007.1	007.4	007.4	1007.1	laah·8	0000	1995.8	1994.7	1994.4	1993.5	199312	1993.0	993.4	1993 4	9920	1994 4
l	30	992.5	992.2	991.3	991.1	991.2	990.9	990.9	990.8	991.3	992.0	992.7	993.1	993.7	993.9	994.2	994.4	995.0	996.1	996.6	996.8	996.9	996.9	997.5	998.0	993.5
\downarrow	31	998.4	999.0	999.7	000-3	001 •2	001.9	003.1	∞4·5	∞5·5	006.4	007.1	007.5	008·2	008-6	009-5	010.3	011.1	012.2	012.7	013.2	014.2	014.9	015.2	015.4	007 · 2
Mean		993	993	992	992	992	992	992	992	993	993	993	993	993	993	993	993	994	994		994	994	994	994	993	993
	n level)	•55	1									_										<u> </u>				
Mean	• • • • • • • • • • • • • • • • • • • •	996	1		995				1		996	996	1	996			1	997		-1		997	997	997	997	996 •76
(Sea le	vel)	<u>·79</u>	.57	-21	98	96	.90	-00	-13	.32	·48	.59	-68	-81	-89	.97	.04	-26	- 3,	•53	33	1 - 49				<u>-</u>
G.M	И.T.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
- G.II	12.1.	<u> </u>	1 2.	1 3.	· •	1 3.	· ·	<u>' /·</u>	1 0.	1 9.	, 10.	, 11.	,21001	4 -3.						· ·	his rul		- not	howe	ver a	

23. Abordson: H_b (height of barometer cistern above M.S.L.) = 26.8 metres.

November, 1923.

······································						 							N 7			<u> </u>										J.,
	Day.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.		Noon		14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
\uparrow			015 6		015.7	016.0	016.0	015.9	015.9	o15·8	015.5	014.8	014.3	013.7	013.1	012.7	012.1	011.7	011.2	8.010	010.6		009.5			013.5
l	3	989.8	986.9	983.9	981.2	980∙1	979.2	979.5	979.7	980.2	980∙1	981.1	981.1	982.1	982.7	983.5	984.1	983.8	983.8	983.6	983.3	983.1	982.9	983.0	983.2	982·8
į	4 5	983·9 991·2	984·4 992·0	984·4 992·1	985·0 992·5	985·3	985·4 993·4	986·0 993·8	986·7 994·3	987·4 994·9	988·1 995·2	988·1 995·4	988·1 995·5	988·3 995·4	988·3 995·3	988·0 995·6	988·3 995·9	988·5 996·1	988·9 996·6	989·0 996·8	989∙0 997∙0	989·6 997·2	989·8 997·4	990·5 997·7	991·0 997·8	987·4 994·9
	_		_	1 . 1		ì		1						l .												001.8
	7	003.7	004.0	004.2	004.4	005.0	005.1	006.1	006.7	006.8	006.9	007.0	006.8	oo6·8	006.6	006.3	006.2	006.3	005.7	005.2	004.9	004.2	003.1	002.4	001.4	005·3
	9	995.4	996.3	996.9	997.8	998.9	000.1	001.4	002.6	004.5	006.5	oo8∙o	009.4	010.9	012.2	013.4	015.2	016.6	0.810	018.9	019.8	020.7	021.5	022.0	022.2	009.0
		1		1		(1								_								·		1	023·1
ا	11	999:7	999.6	998.6	996.9	996.3	995.9	995.2	994.9	994.7	994.7	994.9	995.1	994.9	995.3	995.5	996.0	996.5	997.1	997.1	997.1	997.2	996.9	997.0	996.5	010·5 996·5
[مم	13	966-6	966.8	966.9	966.8	967.5	968.6	969.5	969.8	970.6	970.7	971.0	971.3	972.5	973.7	975.3	976.1	977.9	979.8	981.3	982.8	984.1	985∙0	986.4	986.9	982·3 974·1
Station I evel	15	987.9	988.5	989.0	989.4	989∙0	988.5	987.6	986·5 	985.4	983.9	981.7	979.2	976.7	974.5	972.4	970.1	967.5	965.1	962.3	961.1	960.9	960.5	961.1	962.5	976.8
24:	16 17	965·2 982·2	968.1	969.8	971·9 978·7	974.0	976.2	978.6	980·8 980·2	982·3	984·1 981·8	985·3	985·5	986·8 984·9	987·1	987.2	986·9	986·9 985·4	987·0	986·7 086·5	986·7 987·1	986·8 987·1	986·1 987·1	985·4 987·2	983·6	981·2 983·3
Ť		986.3	985.7	984.8	984.8	984.3	983.6	983.6	983.8	983.7	984.6	985.2	985.5	985.5	985.2	985.6	986∙1	987.7	988∙1	989.3	990.0	990.8	991.2	991.7	992.1	986·5 995·9
	20	996.8	996.8	997.1	993 9	997.2	997.5	998.0	998.4	998.9	999.3	999.8	000.0	000.4	000.8	001.2	001.8	002.1	002.3	002.6	002.7	002.8	002.9	002.8	002.8	000.0
	21																									003.2
	23	009.9	010.1	010.1	010.0	010.0	010.2	010.4	011.0	o11.6	011.9	012.1	012.2	012.4	012.5	013.2	013.4	013.7	014.4	014.8	015.1	015.4	015.7	019.1	016.2	008.7
	24 25																									016·0 007·4
	26	005.7	005.7	005.6	005.6	005.6	005.5	005.8	005.9	006.1	006.3	006.3	006.1	005.9	005.6	005.6	005.6	005:9	006.0	006·0	006.2	006.0	006.2	006.2	006.2	005.9
	27 28	006.1	006.2	006.4	006-3	006.4	006.7	006.8	007.2	007.5	008.0	008.1	007.9	008.1	008.1	008.1	008.3	008.5	008.8	009:4	009.6	009.8	010.0	010.5	010.3	007.9
	29	005.6	005.6	005.4	005.1	005.0	005.2	005.3	005.6	005.9	006.5	006.7	006.8	006.8	006.8	007.1	007.8	008.1	008.5	008.6	008.7	008.9	009.1	009.2	009.4	006.9
Mean		999		999	999	999	999				1000	}						999	999	999	999	999	999	999	999	·
(Stat	tion level)	·47	•50	•34	·18	•20	.29		.77	.01	•20	·23	.11	∙06		92		·8 ₅	⋅86	•67	•59	•50	•33	.27	.08	67
Mear (Sea	level)	·79	·82	1002 •66	1002 ·50	.52		1002	.003 .003				1003								1002	1002	1002	1002	41	1002
24.	Aberde	en:	\mathbf{H}_b =	= 26 ·	8 me	etres.																	Dec	embe	er, 19	923.
			mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.			mb.						mb.
i	I 2	992.4	991.4	990·7	989∙8	3 988.7	1987.8	3 986-8	985.9	984.9	984.4	983.8	3 98 3∙c	982.8	982.2	983.1	984.6	985.0	986-8	987.7	988.1	988-6	988-9	1989.4	989٠٤	987·0
,	3 4	1993 9	993.5	5 993.0	992:3	3 991 .4	1990.0	990.4	1989.6	989.4	1989.2	988.7	/ 988∙c	987.4	. 986·g	986.9	986.8	986.8	986∙g	987.0	987.4	. 988•1	988.8	989.7	990.5	1993·5 5989·4
	5	991.	991.	7 992 • 2	993.1	1993.8	995.1	1996.2	997.1	998-3	999.6	000-2	9.000	001.6	002.5	003.0	003.8	004.5	005.5	006.1	007.1	007.7	007.8	008.2	008-5	5000.3
	6	008.8	001.6	009.4	998-8	1009.7	010.0	010.6	010.9	011.0	011.1	011.1	010.0	010·6	989.0	009.6	009.3	008.9	008·4	007·8 985·1	983.0	006·4 983·1	982.6	981.7	981.0	9009 1
,	7 8 9	980.2	979	o 979∙0	1978.7	7 978 .	5 978∙3	3 978+	979.2	980.1	:lg8o∙g	981.0	982.2	1983.5	1984.6	5986∙6	988.5]990 · c	991.7	1993:5	1994.5	1990.0	1997:5	1998.0	1999:3	9 85 · 5
	IO	004.2	004.0	004.1	004.0	003.8	004 .0	004	005.1	005.8	006.2	006.5	006.8	007.2	007.4	007.6	008.0	008.6	009.1	009.4	009.0	010.3	010.4	010.7	011.0	006.9
	11	011.7	011.0	012.1	011.0	012.3	012.4	012.4	012.5	012.9	013.3	013.1	013.2	013.2	013.3	013.7	013.1	013.0	013.5	013.5	013.0	013.4	013.3	012.9	012.4	012.8
-	12 13	015	3 015-6	010.0	016.6	017:5	018.3	3/810∤8	019.8	020.0	022.3	022.6	023.1	023.6	024.1	024.8	025.2	025.7	025.9	026.1	025.3	025-1	024.9	1023.9	022.8	013.0
į) 14 15	013.	020.0	019.3	015.1	1015.3	015.5	014.3	017.3	012.1	012.4	012.8	019.6	019.3	019.3	019.0	018.6	009.0	017.7	017.2	015.6	014-8	013.9	012.7	011.3	013.4
,	13 14 15 16 17 18 19	009.2	007.9	006.6	004.0	004.5	004.8	8 005.1	005.6	005.0	004.6	004.8	3 004.7	005:3	005.2	2 005.6	006.5	007.7	008.6	008.9	009.8	010.3	010.3	011.0	011.2	007.0
• • • • • • • • • • • • • • • • • • • •	I 17	011.0	010.	7 010 9	0009.	7 0009 0	o 008∙∠	1007.0	007.6	006.8	3 006∙0	005.3	3 003.7	1003.4	1003.2	2 003.0	002.6	002.5	003.1	1003.9	004.5	1005.0	1005.0	1005.7	1005.5	006.2
Ú	n 19 20	014.	7 015:	2 015.9	010.0	016.5	2 016.7	1 016 1	015.8	015.0	016.2	016.4	1015.0	015.6	015 8	3015.3	015.2	015.7	010.2	017.2	018.5	019.4	021.5	022.9	1023.9	016·8 026·8
	21	1	1	1	1	1	i	1	1	(1	1	ł	1	l	1	1	1	ļ	j	1		i		ļ	016.5
	22	003.	7 001	5 000·0	i 998∙:	t 996∙0	994.8	3 993.7	992.9	992.6	992.9	993.0	992.4	1992.2	991.5	991.5	992.2	992.5	992.0	991.8	992.1	992.0	991.8	991.7	991.3	994 • 2
i	23	990.	909"	01900.7	900	5 995.6	995.6	5 995 ∵	995 2	995.0	997.8	9999.6	001.2	2 002 0	004.3	3 005.7	r o o6∙9	008.1	009.1	009.5	OIO.I	010.0	010.0	011.3	011.1	996.3
	24	999	999	1997		- 2	5 a - 1		MOTT .	COTTO	MOTT 2	IOTT O	0.010	. 800 l o	1007.6	0006-8	005.9	004.9	1003.8	003.1	002.5	002.1	1001.2	001.5	1001.3	1007.9
	25	011.	011.	4011.6	011.	5 011.6	011.8	1		1	1	ĺ		.i	1				Ì	-	l				05-	1
	25 26 27	001	001.	7 001 .8	0011	0011·6	6 003·3	3 003·7	004.4	004.4	005.5	006.0	005.8	001.1	000 2	999.5	999.0	998.4	997.5	996.6	996.3	995.9	995.3	995.0	995.2	003·7
	25 26	001: 001: 001: 095:	011. 001. 0001. 096.	7 001 · 8 1 001 · 2 0 996 · 8 5 021 · 6	0011: 002: 001: 001:	2 002·6 5 001·6 5 998·5 2 022·5	5 001 · 8 5 003 · 3 5 001 · 7 5 099 · 8	3 003·7 7 001·8 5 000·9	004.4	004.4	005·5 002·3 006·6	006.0	005.8	001·1	000 • 2	999·5 012·1 022·1	999·0 013·3 021·4	998·4 014·1 021·1	997·5 015·2 020·3	996·6 016·1	016.3 019.3	995·9 017·1 018·7	995·3 017·8	019·6 016·8	020·6 015·9	999·7 007·8 021·4
	25 26 27 28	001: 001: 001: 095:	011. 001. 0001. 096.	7 001 · 8 1 001 · 2 0 996 · 8 5 021 · 6	0011: 002: 001: 001:	2 002·6 5 001·6 5 998·5 2 022·5	0011.8 003.3 0001.7 5 999.3	3 003·7 7 001·8 5 000·9	004.4	004.4	005·5 002·3 006·6	006.0	005.8	001·1	000 • 2	999·5 012·1 022·1	999·0 013·3 021·4	998·4 014·1 021·1	997·5 015·2 020·3	996·6 016·1	016.3 019.3	995·9 017·1 018·7	995·3 017·8	019·6 016·8	020·6 015·9	1999 • 7
	25 26 27 28 29	001: 001: 001: 095: 021: 015:	011. 001. 0001. 0996. 0021. 0014.	7 001.8 1 001.2 0 996.8 5 021.6	0011: 002: 001: 001: 002: 012:	0011.6 002.6 001.6 5 998.5 0 022.5 0 011.2	0011.8 003.3 0001.7 0999.3 022.6	3 003·7 7 001·8 5 000·9 6 023·1 8 010·2	7 004·4 3 002·4 9 002·5 1 023·4	004·4 002·2 004·8 023·8	005·5 002·3 006·6 024·2	006.0	005.8	001.1	000.2	999·5 012·1 022·1 011·2	999·0 013·3 021·4 011·9	998·4 014·1 021·1 012·0	997·5 015·2 020·3 013·1	996·6 016·1 019·7	014·4 019·3 016·9	995·9 017·1 018·7 014·9	995·3 018·3 017·8 015·8	995.0 019.6 016.8 016.5	995·2 020·6 015·9 016·8	999·7 007·8 021·4
Mea (Sta	25 26 27 28 29 30 31	011··· 001·· 001·· 995·· 021·· 015·· 016··	011·2 001·2 0001·2	7 001 · 6 7 001 · 8 1 001 · 2 0 996 · 8 5 021 · 6 1 013 · 4 3 017 · 7	3 002 · 2 001 · 3 997 · 3 002 · 2 0012 · 0 1	2 002 · 6 5 001 · 6 5 998 · 5 2 022 · 5 0 011 · 2 7 017 · 7	5 0011·8 5 003·5 5 001·7 5 999·5 6 022·6 4 010·8	3 003·2 7 001·8 5 000·9 6 023·1 8 010·2 1005	7 004·4 3 002·4 9 002·5 1 023·4 1 010·4 1 010·5	004·4 002·2 004·8 023·8 010·3	005·5 002·3 006·6 024·2 010·4	006.0	005.8	001.1 010.0 023.0 010.6 015.4	000.2	012.1	999·0 013·3 021·4 011·9 013·8	998·4 014·1 021·1 012·0 013·9	997·5 015·2 020·3 013·1 014·0	016·1 013·5 014·0 1006	996·3 016·9 014·4 014·0	995·9 017·1 018·7 014·9 014·1	995·3 018·3 017·8 015·8 014·0	016·8 016·5 014·1	015·9 016·8 014·4 1006	999·7 007·8 021·4 012·5 015·7
(Sta	25 26 27 28 29 30 31 in tion level)	001: 001: 001: 995: 021: 015: 016: 1005	0011. 0011. 0001. 0021. 1014. 7017. 1005	7 001.6 7 001.8 1 001.2 0 996.8 5 021.6 1 013.4 3 017.7 1005 1 .58	3 002 · 2 001 · 3 002 · 2 001 · 3 002 · 2 001 · 3 002	2 002 · 6 5 001 · 6 5 998 · 5 0 011 · 2 7 017 · 7 1005 11008	5 001 · 8 5 003 · 3 5 001 · 7 5 999 · 5 6 022 · 6 4 010 · 8 7 017 · 2 1005 · 20	3 003·7 7 001·8 5 000·9 6 023·1 8 010·2 1005 1005	7,004·4 3,002·4 002·5 1,003·4 1,010·4 1,005 -51	004·4 002·2 004·8 023·8 010·3 017·0 1005 -69	1005·5 2002·3 3006·6 3024·2 3010·4 0016·6 1006 ·05	006·0 002·3 008·0 024·1 010·6 1006·1	005.8	001·1 010·0 023·0 010·6 015·4	000·2 011·1 022·5 010·9 014·7 1005	999·5 012·1 022·1 011·2 014·1 1006 •08	999.0 013.3 021.4 011.9 013.8 1006 -29	998.4 014.1 021.1 012.0 013.9 	997·5 015·2 020·3 013·1 014·0 1006 ·65	996.6 016.1 019.7 013.5 014.0 1006 .75	996·3 016·9 019·3 014·4 014·0 1006 ·81	995.9 017.1 018.7 014.9 014.1 1006 .79	995·3 018·3 017·8 015·8 014·0 1006 ·80	995.0 019.6 016.8 016.5 014.1 1006 .71	995·2 020·6 015·9 016·8 014·4 1006 ·53	999·7 007·8 021·4 012·5 015·7 1006 •06
Mea (Sea	25 26 27 28 29 30 31 mtion level)	011: 001: 001: 995: 021: 015: 016:	0011. 0011. 0001. 0021. 1014. 7017. 1005	7 001.6 7 001.8 1 001.2 0 996.8 5 021.6 1 013.4 3 017.7 1005 1 .58	1008	2 002 · 6 5 001 · 6 5 998 · 5 0 011 · 2 7 017 · 7 1005 11008	5 0011·8 5 003·3 5 001·7 5 999·5 6 022·6 4 010·8 7 017·5 1005 1008	3 003·7 7 001·8 5 000·9 6 023·1 8 010·2 1005 1005	7,004·4 3,002·4 002·5 1,003·4 1,010·4 1,005 -51	004·4 002·2 004·8 023·8 010·3 017·0 1005 -69	005·5 002·3 006·6 0024·2 0016·6 1006 005	006·0 002·3 008·0 024·1 010·6 1006·1	005.8 001.5 008.9 0023.5 010.7 1006 08	1006 1009	000·2 011·1 022·5 010·9 014·7 1005 '94	014·1 1006 1009	999.0 013.3 021.4 011.9 013.8 1006 -29	998·4 014·1 021·1 012·0 013·9 	997·5 015·2 020·3 013·1 014·0 1006 ·65	996.6 016.1 019.7 013.5 014.0 1006 .75	996·3 016·9 019·3 014·4 014·0 1006 ·81	995.9 017.1 018.7 014.9 014.1 1006 .79	995·3 018·3 017·8 015·8 014·0 1006 ·80	995.0 019.6 016.8 016.5 014.1 1006 .71	995·2 020·6 015·9 016·8 014·4 1006 ·53	999.7 9007.8 9021.4 9012.5 915.7 1006 1009 7 .40

PRESSURE AT STATION LEVEL AND AT SEA LEVEL.

ANNUAL MEANS OF HOURLY VALUES.

From readings in millibars at exact hours, Greenwich Mean Time.

25. Aberdeen: $H_b = 26.8$ metres.

1923.

G.M.T.	ı.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Station Level. 900 mb.+	mb. 105·13	mb.	mb. 104·80	mb. 104·67	mb. 104·64	mb.	mb.	mb. 104·99	mb. 105·14	mb.	mb. 105·25	mb. 105·19	mb. 105·16	mb.	mb.	mb. 105·08	mb. 105·16	mb. 105·29	mb. 105·38	mb. 105·48	mb. 105·52	mb.	mb.	mb.	mb.
Sea Level.	008.42	008.26	008.09	007.96	007.94	007.98	008-12	008.27	008-42	008.49	008.53	008.45	008:42	008.36	008.33	008.35	008.43	008.57	008.66	008.76	008-80	008.78	008.72	008.60	008.40

PRESSURE AT STATION LEVEL; MONTHLY MEANS AND DIURNAL INEQUALITIES.

The departures from the mean of the day are adjusted for non-cyclic change.

26. Aberdeen: $H_b = 26 \cdot 8$ metres.

1923.

				_																					
Month.	Mean	Hour. I.	G M.T. 2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.
Jan. Feb. Mar.	mb. 1008·27 996·54 1014·94	0.00	-0.11	-0.23	-0.34	-0·53 - 0·42	-0.71 -0.33	-0.27	-0·12	+0.01	+0.03	+0·14 +0·17	+0.00	-0·23 +0·03	−0.05	-0.14	-0.05	+0.11	+0.29	+03.1	+0.29	+0.30	+0.24	+0.11	+0.11
April May June	1006·80 1006·74 1013·10	-0.09	-0.22	0 ∙26	0 ⋅31	-0.24	0.15	-0.03	+0.12	+0.23	+0.26	+0.27	+0.23	+0.17	+0.12	-0.02	-0.14	-0.51	-0.21	-0.05	+0.08	+0.10	+0.16	+0.11	+0.02
July Aug. Sept.	1008·14 1003·53 1004·16	-0.10	—o∙3o	-0.44	-0.53	-0.45	-0.42	-0.31	-0.25	-0.11	-0·05	-0.01	-0.02	+o.081	+0.00	+0.13	十0.17	+0.21	+0.25	+0.31	+0.48	+0.49∣	+0.42	+0.29	+0.08
Oct. Nov. Dec.	993·53 999·67 1006·06	-o·39	-o·35	-o·48	-0.63	0·59	-0.49	-0.27	+0.03	+0.29	+0.50	+0.55	+0.45	+0.42	+0.30	+0.31	+0.30	+0.28	+0.30	+0.13	+0.07	-0.01	-0.15	-0.20	-0.36
Year	1005-12	+0.03	-o·14	− 0·30	-0.44	0·4 7	-0.42	-0.29	-0.13	+0.02	+0.10	+0.13	+0.06	+0.04	-0.02	-0.06	_o.o5	+0.03	+ o ·16	+0.25	+0.34	+0.38	+0.35	+0.28	+0.17

ABSOLUTE EXTREMES OF PRESSURE AT STATION LEVEL FOR EACH DAY.

Maximum and Minimum for the interval 0h. to 24h., Greenwich Mean Time.

27. Aberdeen: $H_b = 26.8$ metres.

1923.

Month.	J:	an.	F	eb.	N	Iar.	A	pril.	M	ay.	J:	une.	J,	uly.	A	ıg.	Se	pt.	0	ct.	N	ov.	1	ec.
Day.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
1 2 3 4 5	mb. 004·5 001·5 997·5 012·3 009·5	976·8 976·6 997·5	001·3 004·5	986·0 993·0 004·5	003·9 016·4	980·5 980·7 003·9	023.7	020·8 012·8 007·8		013·0 009·4 003·8	025.9	020·5 011·6 012·3	012·5 006·3 013·0	999.8	004·6 010·8 020·0	985·2 981·8 010·8	023·7 015·3	012·5 012·5 009·8	mb. 011.0 008.6 011.8 017.9 013.4		008.7	983.2	996.1	986.7
6 7 8 9 10		993·4 990·9 977·4	994·1 984·6 987·4 002·3 001·6	973·5 968·7 987·4	022.1	992·1 009·7 017·7	012·4 014·2 019·2 019·0 013·1	007·8 006·8 014·2 013·1	011·0 014·0 011·2 008·7	002.2	015·2 015·2 007·2	009·1 007·2 995·2 993·8	021·2 020·2 014·9 019·1	019·9 012·4 010·0	010·8 009·0 013·0 011·4	008·7 003·9 008·0 006·3	016·7 022·0 022·4 010·9	008·5 009·0 010·9	001·2 001·3 999·9 997·5	997·7 992·9	003·7 007·1 001·4 022·2	997·8 001·4 992·5 994·9	011.3	003.9
11 12 13 14 15	020·1 019·7	011·9 006·8 999·9	006·1 015·3 020·4 020·2 015·6	005·4 015·3 015·6	018·3 017·8 026·2 030·6 030·6	005·5 003·1 026·2	010·3 004·9 988·5 995·6 005·6	988·5 982·3 987·1	989·0 993·2 996·3	987·3 988·4 993·0	023·3 011·7 019·2	004·7 001·9 011·7	022·0 023·7 023·1	017·6 017·6 021·5 013·0 999·8	022·1 014·6 016·5	013·7 007·8 014·3	007·2 994·8	993.0 991.7 994.8 991.8 992.1	996·5 993·3 003·2		018·9 000·5 996·5 986·9 989·4	994·5 966·4 966·1	013·9 015·1 026·2 022·8 019·7	
16 17 18 19 20	026·0 024·0 027·3 024·1 020·8	022.0	005·6 003·4	005·6 994·7 996·1		030·5 030·1 025·4	015·8 019·6 018·3 011·3 013·0	015.8	010·5 013·4 007·3	997·9 007·3 000·5	019·4 014·5	012.6	001·2 009·9 009·5	998.0	006·3 005·2 008·2	991·8 991·7 005·2	992·3 995·9	986·7 986·5 991·6	013·2 012·5	000·0 006·3 998·1 985·0 984·9	987·3 992·1 997·3	978·I 983·I	011·3 011·2 014·2 023·9 029·0	004·5 002·6 002·1 014·1 023·5
21 22 23 24 25	020·4 023·6 027·2 021·8 024·3		999.0	986·3 986·2 991·0	021·6 019·1 015·3 012·3 015·7	015·3 011·6 008·8	014·5 014·3 011·5 013·6 002·3	006.6	013·9 016·9	007·2 012·2 002·0	013·2 013·8 017·1	010·3 009·3 011·7 012·0 015·4	013·6 003·4 005·9	999·6 901·8	994·5 999·5 006·4	985·4 992·4 990·7	994·3 997·5 002·9	993·6 987·1 988·2 997·5 988·7	975·7 974·0 971·2	970·8 968·8 964·2 964·3 971·1	005·8 009·9 016·2 017·2 012·1	002·4 005·8 009·8 012·1 05·5		005·6 991·3 988·6 994·9 001·2
28 29 30	017.0	010·0 009·9 005·1 005·6	992·5 975·4 986·1 — —	970·4 968·4 975·4	022·0 018·5 017·6 024·2 024·7	011·6 011·2 017·6	005·3 005·2 001·5	997·I 000·I 000·0 994·4	021·9 026·8 026·4 023·1	015·0 021·0 023·0 020·8	019·6 019·5 020·0 015·2	015·2 016·3 017·9 015·2 011·7	010·3 006·8 002·3 995·8	995·8 990·4	988·9 001·7 003·1 001·8	987·4 988·2 993·8 992·4	013·0 020·2 022·4 017·8	017·8 009·0	987·4 990·0 997·5 998·0	975·5 990·0 990·4	010·3 010·3 009·4 011·0	006·1 004·9 002·3	002·4 020·6 024·3 017·1	001·3 994·9 995·2 015·9 010·3
			1001		1018			1003	,		1016	1010	990·4 1011 ·12		1008		— 1008 '54	999 •69	998 •38	997·9 988 ·55	- 1004 •48		,	1000

28. Aberdeen: North Wall Screen on Tower: h_t (height of thermometer bulb above the ground) = $12 \cdot 5$ metres.

January, 1923.

Day.	I.	2.	3.	4.	5.	6.	7 .	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	M
	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	[a.	a.	a.	a.	a.	a.	T '
1 .	74.6	74.1	75·I	75.0	75.4	74.5	74.8	74.7	74.8	75·I	75.3	76.1	76.7	76.4	76.1	74.7	74.1	73.9	74.0	73.9	74.3		74.9	76.9	
2	77.2		77.5		78.0		78∙1		79·I			82.3									80.4				
3		78.9				78.2		77.4	77.0	77'I	78.0	78·5 78·9	70.7	70.7	78.1	77.9	77.4	77.5	78.3	77.8		78.9		78.6	
4	78.0	78.4	78.4	78.1	78.3	77.9	77.9	77.9	77.0	77.1	77.7	78.4	79.1	78.6	78.7	78.5	77.8	76.7	76.8	75.8	75.4	75.3	76.5	76.5	17
5	77.0	77.9	70.4	70.7	1	1	{	-	ł	Į	1	}	l	1	j	ļ	ļ	l			1		1	1	1
6		75.2	74.2				73.9	73.9	73.8	73.9	74.4	75.8	76·o	76.6	76·o	75.1	74.4	74.3	74.7	74.9	75.0	75.4	75.9	77.2	7
7	76.3		77.6	77.6	77.9	77.8	77.7	77.8	77.7	77.9	78.2	78.7	80.1	80.4	80.1	80.6	80.4	80.1	80.4	80.2	80.4	81.4	81.0	81.8	17
8	82.5					82.5						80.7							76.3		76.6			76.5	
9 10	77.7	76.5	76.6	76.0	76.4	78.2	78.3	77.4	78.0	70.5	76.0	76·1	77:2	77.8	77.6	77.4	77.4	77.4	77.1	77.1					
10	70.9	70.7	70.0	70.9	70.4	70.5	ľ	{	1	1	1	1	ł	1	1	1	1	1	1		ļ	1	ł	1	1
II	76.3	76.3	76.6	76.9	75.8	76.3	76.2	76·I	77.0	76.8	77.2	78.6	77:5	77.5	77·I	77.0	76.4	76.4	76.5	75.9	75.3	75.3	75.3	75.1	12
12	75.2		74.9		74.6	74.7	74.6	74.6	74.4	75.0	75·I	75.2	75.4	75.6	75·I	74.7	74.7	74.6	73.9	73.9	74.0	73.2	72.9	72.8	17
13	72.6	72.9	72.5	72.3	72.9	72.7	72.9	73.5	74.3	74.7	75.2	75.6	76.2	76.7	77.0	77.8	80.5	80.4	81.5	81.4	80.9	81.0	81.3	80.4	
14	80.3	80.2	80.9	81.0	81.0	81.1	81.0	80.5	78.8	78.4	78.5	78.9	79.3	79.0	70.5	77.4	77.3	77.8	70.0	78.1	78.4	78.4	78.9	70.0	17
15	78.3	78.5	78.4	78.7				1		1	[80.0	1		1	ł	1	ì		'	76.4	70.4	///-0	77.5	ľ
16					76.6	76.9	76.9	76.7	76.7	77.4	78·o	78.4	78.5	78.4	78.3	78.2	78.2	78.2	78∙1	78.2	78.4	78.7	78.9	78.9	17
17		78.2			78∙0	77.2	76.5	76·I	76.0	77.0	78.4	79.0	79.5	80.1	80·I	80.0	79.9	79.8	179:7	79·I	79.0	80.4	79.4	78.0	17
18	77.4		76.6					76.7	76.5	76.8	77.6	78.9	79.7	79.7	79.6	78.9	78.4	78.7	78.7	78.9	78.9	78.6		78.1	
19	79.5	79.6	80.1	79.1	78.6	78.4	78.0	78.2	78.3	80.0	80.3	80·8	01.9	05.0	04.4	04.5	02.3	01.3	74.4	79.0	70.5	75.0	7/5	75.2	1
20	76.7	70.0	70.0	70.3	1 .	1	1	1	1	i	Į.	74.7	l .	1	l	1	1		1	((T
21	75.6		75.3		75.6	75.7	75.9	76.0	76·1	79.5	81.8	82.9	83.4	84.5	84.9	83.9	83.8	83.1	83.5	83.2	82.5	83.3	83.1	83.1	8
22	83.0	82.7	82.4	82.4		83.0		82.3	82.4	83.2	83.1	80·1	79.3	78.0	76.9	77.1	76.6	76.1	76·I	75.6	76.0	76.0	76.0	76.0	12
23	75.2	75.2	75·I	75.3	75.1	75.2	75.1	75.4	75.7	76.2	76.5	76.2	76.6	78.0	78.4	78.4	77:5	77.9	78.5	83.0	82.4	82.9	82.4	82.6	12
24	83.3	84.0	84.0	84.1	84.1	83.6	83.1	82.5	82.4	82.9	83.2	83·9 83·0	82.7	82.8	82.5	83.7	82.7	82.0	82.2	81.8	81.6	82.2	82.6	82.8	18
25	101.0	80.4		}	1		1	1	J	}	1		1		1	1	1	1	i	1	i	1	[í	1
26	82.9	82.8	82.5	82.1	82.3	82.1	82.3	82.0	82.6	82.7	83.4	83.9	84.4	83.9	83.5	83.0	82.5	82.3	82.4	81.5	81.5	82.0	81.0	80.7	18
27		81.1	81.6	81.6	81.0	81.9	82.2	82.4	83.5	83.2	84.4	84.5	84.5	81.3	181.0	180.6	80.0	79.7	79·I	79.0	78.5	178.1	178.0	78.0	15
28	77.7			77.8	78.1	78.1	78.1	78·1	78·o	78·o	78.2	77.7	77.9	78·I	78.1	78.4	78.5	79.0	80.0	76.6	80.0	26.2	79.5	79.2	12
29	79.6	79.7	79.5	79·I	79.0	79.0	79.0	79.0	79.2	79.2	79.8	78.8	77:9	77.0	77.5	77.4	77.3	77.1	80.0	81.0	81.2	82.1	82.8	82.6	
30		1	i .	ł	F	ſ		í	i	l	1	78.9	l	Į.	1	1	J.	1	ì	1	1	1	1	1	- 1
31	83.1	82.0	82.4	81·o	8o·o	79.5	78.9	8o·o	79.6	79.6	80.4	80.0	80.7	80.4	81.3	82.3	83.6	83.8	82.6	82.3	82.4	84.0	83.9	83.1	8
Iean	78.2	78.2	78.3	78.2	78·o	78·I	78.0	78.0	78·1	78.4	78.9	79·I	79:3	79.5	79 ·3	79.0	78.7	78.6	78.6	78.6	78.4	78.6	78.6	78.5	1

29. Aberdeen: North Wall Screen on Tower: $h_t = 12.5$ metres.

February, 1923.

I		a.	a.	a.	a.	a.	a.												a.		a.	a.				
1		3.4	84.1	84.0	82.4	82:0	82.4	82.0	82.5	82.6	a.	82.6	a.	a. 85.2	85.5	<i>a</i> . 85⋅6	85.0	85.7		84.6		83.2	83.5	83.7	84.1	83.9
		3.9	82.6	83.2	82.5	81.5	80.6	80.2	70.4	70.3	70.5	80.4	81.0	81.1	81.7	81.1	80.8	79.8	79·I	78.4		77.9	78.1	78.8	79·I	80.4
3					79.7	79.9	79.0	78.6	79.0	80.5	81.0	81.0	82.0	82.0	82.8	82.0	79.9	79·I	78.8	70.3	70.2	1,0.1	78∙0			79.7
4			77·T	77:0	76.0	75.0	75.0	76.2	76.4	76.4	76.0	78.0	70.0	70.8	180.0	170.8	79.4	78.0	177:5	77.3	77.0	77·I	77.4	77.6	77.9	77.5
5	7	7.4	77:3	77.6	78·o	78⋅1	78.3	78.9	79.3	79.4	80.1	80.4	81.2	81.4	81·o	80.5	80.2	80.0	80.0	80.0	79.7	79.9	79.7	79.9	80.0	79.5
6	8	0.1	80.2	80·1	80.1	8o·o	8o·o	79.6	79.6	79.2	79.0	78.9	78.6	78.2	78.3	78.4	78.4	78.1	78∙0	78·0	77.9	77.5	77.6	77.3	76.9	78.8
7	7	7.2	クク・5	77.0	77.0	176.6	76.2	76.0	77.4	77.0	178.4	78.7	70.0	178·T	177·Q	178.0	179.1	179.1	179.1	179.1	1/90	1/9 3	79.3	193	100 0	78.2
8	7	9.9	79.7	79.7	79.7	79.9	80.5	80.6	80.5	80.3	80.5	80.5	80.5	79.0	77.9	77.9	78.0	78.2	70.4	77:0	78.0	77.8	70.2	70·T	70.1	79.2
9 10		7.3	76·o	75.0	75.9	75.3	75.4	75.7	70.9	70.9	77.0	78.2	79.0	79.5	79.5	79·2 78·1	78.2	78.4	78.5	78.5	78.5	78.7	78.9	78.9	79·I	78.7
10	-1'	9.1	79.1	i	1	1	1	L	1	1	1	i .	•				I .	í		,	,	,	1			1
11	7	9.2	79.2	79.0	79·I	78.9	78.5	78.5	78.4	78.3	78.2	78·o	78∙1	78.3	78.3	78.1	78∙1	78·I	78.4	78.3	78.6	78.6	78.5	78.7	78.5	78.5
12	7	8.8	78.6	17X · O	17X.X	70 · T	70.5	70.6	70.4	70 · T	17X · X	70.2	70.2	70.7	170.5	17Q · Q	170.3	170"/	170.2	1/4 3	1/4 3	1/0 -	1100	1/~/	1/00	79.0
13	17	8.5	78.6	78.4	78.2	78.3	78·I	78.0	78·o	77.8	78.0	77.7	177.6	177.4	177.7	170.0	170.0	170.0	1700	1/03	1/04	75.4	74.5	74.0	75.2	77°4 75°5
14	- 1'	- 1	•	76.0	70.0	75.7	75.7	76.0	70.1	75.3	75.3	75.4	75.1	75.7	75.4	75·5 76·6	75.4	76.7	76.8	76.7	76.9	76.9	76.9	76.9	76.8	76.3
15	17	5'4	75.5	75.0	75.4	J.	1	i e	1	1	1	L	1		1	1		l	1		1	l .	ſ	(ł	, ,
16	7	6.8	76.9	76.3	76⋅1	76.0	75.9	75.7	76.2	76.2	76·1	76.3	76.2	76·1	76.1	76.4	76.6	76.8	76.9	76.9	77.0	76.4	76.1	76.1	76.0	76.4
17						175.8	175.8	75.0	75.0	75.6	75.6	75.2	75.2	75.4	175.4	175.3	175.2	175.1	175.3	175.1	1/5 -	1/3	175	1/4 9	1/5 0	75.5
18			75°I	75.0	75·I	75.2	75.3	75.4	75.6	75.5	75.4	75.5	75.4	75.4	75.4	75.2	75.3	75.4	75.5	75.3	75.2	75.3	75.5	75.4	75.6	75.4
19 20	7	5.0	75.6	75.0	75.5	75.4	75.7	75.0	75.7	75.7	75.8	70.1	75.9	75.9	70.1	75·7 74·3	74.0	74.8	75·I	75·I	75.0	74.9		73.7		74.8
20			1		1	1	1	1	ì	ì	1	1	1	3	Į.		1		1	l	l l				l	
21	7	4.2	74.5	74.4	74.3	73.7	74.7	74.9	75.0	74.4	74.3	74.2	73.4	73.7	73.6	74.2	74.7	74.8	75.1	75.2	75.2	75.2	75·I	75.0	74.9	74.5
22	- 17	75.0 □	75.1	175.3	175.4	175.0	175.0	175.0	175.4	175.8	175.0	175.4	175.2	175.0	170.3	170.2	1701	170.0	170.1	1/00	1,00	1/~ ~	112		17	75·7 76·3
23				74.7	74.5	74.4	74.3	74.2	74.0	74.6	75.0	76.2	77.0	77.2	77.9	77.6	77.0	77.7	77.9	77.1	77·I	77.0	77.3	77.3	77.5	77.7
24 25	17	7.4	77.4	77.0	77.4	77.3	77.5	77.7	76.7	76.4	76.4	70.0	76.7	70.5	76.5	77·9 76·4	76.2	7/17	75.8	75.8	75.9	76.0				76.4
23			1	ľ	1		1		1	l .		ſ	i		1	1)	1	l	li .	l .	i	1	l .		ľ
26	7	6.7	77.6	78·o	77.9	78·1	78·1	78·1	78.2	78.3	78.2	78·1	78.0	78·o	77.9	77.8	77.6	77.5	77.3	77·I	77:5	77.9	78·I	78.2	78.2	77.8
27	17	78 · I	178.4	170.0	170.0	170.0	170.4	170.4	170.3	178.4	178°I	17X · O	17X · 4	70.0	17X · O	178.0	178.0	170'0	170.9	11/0 9	1/2/	1/	<i> - </i>		1/	78·6
28		78.8	78.8	78.9	78.8	78.8	78.6	78.3	78.3	78.3	78.2	78.2	78⋅1	78.2	78·I	77.9	77.7	77.2	77.0	/7.1	177.0	/// 5	109	104	103	1//-9
Mean	7	77:7	77.6	77.6	77.6	77.4	77.4	77.4	77.5	77.5	77.6	77.8	77:9	78·o	78.0	77:9	77.8	77.6	77.6	77.5	77:4	77:4	77.3	77:3	77.4	77.6
G.M.T.		Ι.	2.	3.	4.	5.	6.	7.	8.	9.	IO.		Noon	 -	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean

30. Aberdeen: North Wall Screen on Tower: h_t (height of thermometer bulb above ground) = $12 \cdot 5$ metres.

March, 1923.

). Aberd	1	1	1		i	1	1	ł	1	1	1	1	1	ł		1		1 .	1	i .					1
Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	<u> </u>	Noon		14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Me
1 2 3 4 5	77.6	a. 76·1 76·7 77·9 77·1 77·9	77·I	a. 76·2 77·7 77·9 76·5 77·6	a. 76·2 78·0 77·7 76·7 77·7	78.2	77·8 77·5 77·3	a. 75.6 77.8 77.4 77.1 78.0	77·7 77·5 78·0	a. 75·8 77·4 77·6 78·5 78·2	77·6 79·8	78·7 77·4 79·2	77·8 8o·o	a. 76·6 79·8 77·3 80·7 77·9	77.4 80.4	78·9 77·2	78·7 77·1 80·1	a. 76·5 78·4 77·1 79·0 80·0	a. 76·3 77·4 77·1 79·0 78·1	77·1 78·6	a. 76·3 77·6 77·6 77·6 78·8	a. 76·2 77·6 77·2 77·9 79·5	77.7	76·4 78·1 77·5 78·0	76 77 77
6 7 8 9	78·0 77·0 79·0 76·1	78·4 76·9 78·5 76·7 76·3	76.3	77·5 78·6 76·0	75.8	76·6 78·7	76·I	76.6	77·4 78·4 77·1	78·9 78·2 78·3 77·5 77·2	79·I 78·7 78·I	79·7 78·9 78·4	78·9 78·6	78·7 78·5	80·2 78·3 78·3	79·8 78·2 78·2	80·2 78·0	78·o	79·4 77·7 77·1	79·2 77·7	79·I 77·6 77·0	76.9		78·8 77·1 76·3	78 78 78 77 76
11 12 13 14	76·5 78·9 75·6	77·0 77·2 79·7 75·0 76·2	76·9 77·3 79·3 74·8 76·2	77.3	76·7 77·2 79·3 74·3 76·0	78.9	77·3 78·4		77·8 80·6	78·1 77·8 81·7 78·0 78·2	78·2 82·2	78·5 82·9	78·1 83·2	77·8 83·7	83.6	78·3 83·6	77·9 83·1		78·0 80·6	79.4 78.0	77.0 78.2 78.2 77.2 77.4	76.3		79·0 75·6	
16 17 18 19 20	74·3 76·4 75·7	76·6 73·9 76·6 74·7 77·1	73·6 76·6 74·3	73.5	73.8	76·6 76·0 76·2 74·1 76·0	76·7 76·1 74·2	76·6 73·9	78·6 77·2 74·4	77·7 79·0 78·5 76·0 78·0	78.9	79·8 78·9	79·3	79.2	79·5	79·I	78·6	78·5 78·1 76·8	76·9 77·4 76·3	77·1	78·3 76·0 76·9 76·3 78·1	75·9 76·4 76·6	76.1	76·3 75·9 77·0	77 76
21 22 23 24 25	1.0	74·2 77·6	74·7 77·5	75·0 77·5	75·0 77·7	77.8	74.3	77.8	77.9	78·8 76·0 78·1 78·0 80·3	78·9 78·4	79·6 79·0	80·1 79·2	79.6	79·5 79·1	79.1	79.1	78·6 79·1	78·5 79·0 78·8	78·4 78·3 79·0 78·6 80·9	78·3 78·9 78·5	77·9 78·8 78·2	, .	77.4	72 78 78
26 27 28	80.9	79·4 81·1	79 · 4 81·1	l C	79·4 80·6	80.5	79·1 80·6	79·6 80·5	80·1	81·4 80·7 80·5 81·0 78·4	81·0 81·4	80.5	81·4 81·7	82.6 81.4 82.6	81 · 2 82 · T	83·2 80·7	82·6 80·6 83·1	82·0 80·1	81·4 79·7 81·2	80·9 79:4 80·8	80·6 79·6	80·9 79·7 79·6	79·4 81·0 79·8 79·0 78·0	80.6 80.0 78.8	80 80 8 0
29 30	78.6	78.6	78.6	78.9	100	, -																			
29 30 31	78.6	78.6	78·6	77.6	77.5	77.4	77.4	77.7	77.8	78·0 78·4	77.9												77.8	77.7	7
29 30 31	78·6 78·0 77·4 deen :	78.6	77.6	77.0	77·5 76·9	77·4 76·9 on T	77·4 77·0	77·7 77·3	77·8 77·8 = 15	78·4 2·5 m	77·9 79·0	79.3	79.4	79-5	79-6	79.5		78·9	78·4	78·3	78·0	78·0	77·8 Apr	77·7	7 ⁸
29 30 31 ean	78·6 78·0 77·4 deen : 2. 78·5 78·6 78·6	78·6 77·7 77·3 Nor a. 78·3 78·6 78·7	78.6 77.6 77.2 Th W	77.6 77.0 78.0 78.6 78.6	77.5 76.9 creen 78.0 78.6 78.5	77.4 76.9 on T	77.4 77.0 ower a. 78.0 78.8 78.4	77.7 77.3 7: ht	77.8 77.8 = 15 a. 78.4 79.0 78.6	78.4	77.9 79.0 netres 8.2 79.1 78.9	79·3 6. 78·1 79·1 79·7	a. 78·0 79·2 79·5	79·5 a. 78·0 79·3 79·0 81·0	79·6 a. 78·1 79·2 79·1	79·5 a. 78·2 78·9 79·3	a. 78.0 78.7 79.3	78·9 a. 78·0 78·6 78·9 88·0	78·4 a. 77·9 78·4 78·7	78·3 a. 78·1 78·4 78·9	78·0 a. 78·3 78·4 78·9 79·4	78·0 a. 78·3 78·4 78·7 79·3	77·8 Apr a. 78·5 78·5 78·5 79·1	77.7 il, 19 78.6 78.6 78.5 78.8	78
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19 20	79·5				81.0	81.4	81.9	82.3	82.9	83.3	83.0	83.1	82.7	83.1	83.7	83.9	85·o	85·o	85.0	83.7				80.3	8
21	8o·o	79.6	79.4	79.2			81.4	81.4	82.0	81.8	81.6	82.0	83.1	84.0	84.6	83.6	84.3	83.7	81.7	80.3	79.6	79.0	78.6		
22	77.7					78.7	78.9	79.3	79.0	79.2	79.9	80.5	81.1	81.0	81.1	80.8	80.9	80.3	80.3	80·0	78.6		76·2	75·I 78·o	
23	74.4						78.3	78.6	78.1	78.9	85.7	81.2	82.0	84.4	85.0	85.2	84:0	84:0	84.2	83.0				79.7	
24	77.1						80.4	81.8	03.3	81.0	81.1	84·4 79·6	70.8	78.8	70.0	78·T	78.2	77.5	77.8	78.1	78.7			78.9	
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26	78.5						78.4	78.7	81.1	80.1	80.4	81·0 82·5	87.7	83.0	82.3	82.2	82 · T	81.6	80.0			1.			- 1 2
27	80.0	1,		1		79.5	70:0	80.3	80.3	80:0	81.8	81.3	81.5	81.6	81.6	82.1	81.6	81.7	80.5	79.6	79.7		78.6		
28 29	79·2 77·9					79.4	79.7	80.0	80.4	81.5	82.9	82.6	82.5	82.8	83.0	83.4	83.1	82.9	82.4	82.0	81.4	81.0	80.9	80·0	8
30	80.0					79.6	80.7	81.2	81.1	81.4	81.0	80.8	79.9	80.0	79.4	79.9	79.6	79.5	80.0	79.9	79.5	79.3	79.1	79.2	8
31	79.5	79.8		1	1	1	l	l	l	Í		81.7			.	·	·		-		-	.	79.1	-	- -
ean .	· 78·5	78.3	78.2	78.2	78.4	79.1	80.0	80.4	80.7	81.2	81.6	81.9	81.8	82·0	81.9	81.7	81.7	81.4	80.9	80.3	79.8	79.3	78.9	78.6	8
		1	<u> </u>	!		<u> </u>		!	<u> </u>		1			1			<u> </u>	<u>-</u>		<u>' </u>	·		<u> </u>	<u>-</u>	
. Abe	rdeen :	No	rth W	all S	creen	on T	ower	: h <i>t</i>	= 12	2·5 n	netres	S.										• •	Jun	18, 19)2
	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	<i>a</i> .	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.		Ī
I	79.0	79.9				81.4	82.1	83.1	84.9	86·o	86.6	86.5				85·o	85.4	84.3		81.1	80.7	80.1			
2	80.8	80.7	80.5	80.4	80.4	80.7	81.2	82.1	82.7	84.4	85·o	86·o	87.5		88.8	90.2	91.9	85.4	83.9	87.3	86·3	84·9 78·9	83.9	83·6 78·2	8
3	83.9	83.6	83.2	83.1	83.1	83.4	83.6	83.6	83.1	83.9	84.1	83.4	83.4	84.4	83.0	82.7	82.4	81.3	81.0	79.4	70.0			79.4	
4	78.6	79·I	79.2	79.2	79.4	79.5	79.8	79.9	80.8	81.0	81.4	81.4	82.0	01.8	02.2	01.7	02.2	82.0	82.0	81.7	80.1				

		_									· · · · · · · · · · · · · · · · · · ·					1 0	1 0	1 0	a.	\overline{a} .	a	a.	a.	a.	Mean
	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	82.7	81.1	80:7	80.1	80.6	81.1	82.0
I	79.0	79.9	80·I	80.4	80.7	81.4	82.1	83.1	84.9	86.0	80.0	86·5	80.4	80.7	00.0	05.0	05.4	04 3	82.0	87.2	86.2	84:0	82.0	82.6	84.4
3	83.9	83.6	83.2	83.1																					
4	78.6	79·I																							
5	79.2	79.2	79.6	79.7	79.4	80.7	82.4	83.1	83.7	83.8	84.1	84.6	84.4	83.6	83.7	82.7	82.2	82.9	83.0	01.7	90.1	00.2	79.3	70.9	01.0
,	, -	, -																							
6	78.4	78·o	77:3	77.0	78.6	79.6	8o·o	80.4	80.9	81.6	81.6	82.3	82.9	83.4	83.9	84.0	81.1	81.2	81.3	81.0	80.1	79.9	79.4	79.1	80.2
i			78.7	78.3	80.2	182.0	1×2.6	1 × 4 · 4	1×2.3	1X6.2	1XX	1 X X . 2 1	ıxx∙∩	100.7	10111	101.2	141.7	191 0	109 4	100 =	· · / -	100 -	1-3	1-3-	3 /
		0																							85.8
		1 ~ ' '	1~	10.	0																84.5	84.5	83.7	84.4	86.6
9	94.3	87.4	87.6	86.0	85.4	86.7	86.4	87:0	86.0	87.2	87.8	87.9	88.5	88.2	87.6	87.1	87.1	86.4	85.4	84.8	84.0	82.8	82.4	81.8	86.2
10	05.3	07.4	87.0	00.9	05.4	00 /	00 4	0,0	00 9	0/2	0,0	0/9	00 3		, -	-, -	'	i .						İ	
	0	000	80.0	0	80.5	80.4	80.8	81.5	82.2	82.0	82.2	84.6	8=.=	85.2	86.2	83.0	85.3	84.4	83.9	84.0	83·o	82.0	82·o	81.6	82.8
ΙΙ	01.3	00.9	90.9	01.0	30.5	80.4	00.0	01.7	82.2	80.8	03.2	84·6 83·1	85.8	88.0	80.0	00.1	80.0	00.1	89.6	89.2	87.9	87.9	87.4	86.9	85.3
12	81.1	81.3	01.2	91.0	01.7	02.9	03.1	03.0	02.9	02.0	03.0	86·1	05.0	85.7	85.77	86.T	84.5	84·T	83.2	82.9	82.4	81.7	81.7	81.5	85.3
						07.2	00.1	00.0	00.0	00.4	00.2	00.1	05.9	05.1	80.6	82.7	82.1	82.0	82.0	81.0	80.0	79.4	78·9	78∙₄	81.0
14	81.2	80.6	80.0	79.8	80.1	80.3	80.0	80.0	79.8	81.0	81.3	82·0 83·0	82.1	03.0	02.0	02.7	80.0	80.6	80.3	80.2	80·1	80.0	70.0	70.2	80.2
15	78.2	77.1	76.7	76.4	77.2	79.7	80.1	81.9	81.2	81.0	82.0	83·0	82.7	82.8	02.0	01.5	80.9	000	00 2	_			100	1,3 -	~
			ļ										_				0	00.4	82.0	81.6	80.4	80.6	80-т	7014	80.8
16	77.9	77.2	77.0	77.9	78.2	79.7	80.4	81.2	81.3	81.6	82.0	82.9	83·0	83.5	83.2	83.0	82.5	02.4	02.0	87.5	87.2	87.2	81.6	87.8	87.0
17	79.4	79.4	79·I	79·I	79.0	79.6	8o·8	81.4	81.5	82.1	83∙1	82.9	82.9	82.7	83.0	82.2	82.2	91.0	01.7	01.2	85.0	84.4	84.0	82.4	86.0
18	81.6	81.9	82.0	82.1	82.8	83.6	85.1	86.2	88·o	88.88	88.9	83.6 89.0 86.8	89.9	89.6	90.6	90.2	89·I	88.9	87.3	00.4	05.9	04.4	04.0	03.4	00.3
19	83.4	83.8	83.9	83.4	83.7	84.1	85.1	85.1	85.3	85.8	86·1	86.8	85.7	86.4	84.6	85.4	85.6	85.2	84.3	93.0	02.4	01.5	91.0	00.4	04.3
20	80.4	80.5	80.6	80.7	80.8	8i·o	81.5	82.0	82.2	81.9	83.3	85·0	86.3	86.6	86.3	86.4	85.8	85.7	85.7	84.6	84.1	83.9	85.0	80.2	83.5
20	~ 4	, ,		,	i	ì	"			_	33	١		1	_	İ						0.5	0.5		
2.	87.2	86.7	85.6	85.4	87.0	87.6	87.8	87.7	87.3	88.2	80-т	89·o	80.4	90.0	89.6	89.5	88.6	88·o	87.2	86.7	86.4	86.5	86.2	86.0	87.6
21	86.4	86.2	86.5	86.1	86.4	86.0	86.0	88.4	80.5	00:0	01.0	91·4	01.0	01.0	00.2	89.9	88.9	88.3	88·o	88∙o	87.9	87.8	87.7	87.7	88.4
22	00.4	87.0	87.5	88.2	80.2	00.3	OTIT	03:3	03.1	03:0	02.6	93.9	03.2	04.4	03.4	93.2	93.0	92.2	91.4	90.5	89.9	89.6	89.1	89.2	91 1
24	00.2	00.7	00.7	67.0	07.1	02.0	01.9	01.6	82.0	02.0	01.0	81·2 84·6	85.4	85.6	85.4	85.6	84.7	84.0	83.2	82.6	81.9	81.3	8o·4	79.4	82.5
25	79:9	79.9	80.2	179.0	00.9	01.0	01.2	01.0	03.0	03.0	04.4	04.0	05.4	05.0	054	050	,	- 7	"]					
_	١			-0.0	0- 0	000	0.	0	0.0	0	0	86.1	96.5	86.6	86.6	86.0	87.2	86.0	85.3	84.4	83.4	83.0	82.9	82.7	83.5
26	78·4	77.6	78.0	78.8	80.8	02.5	\ose 3.4	03.2	93.8	04.9	05.4	86·1	00.5	00.0	0.0	84.7	85.7	84.6	84.5	84.4	84.1	83.9	83.9	84.1	84.3
27	93.1	02.0	02.9	02.9	02.9	03.0	04.4	02.2	02.1	00.0	05.9	90.1	05.3	04 1	04 0	00 0	80.0	80.8	87.6	87.0	86.3	85.6	85.2	85.1	87·T
28	84.0	84.0	84.1	84.2	84.7	85.6	87.4	80.0	87.3	88.9	09.0	90.0	91 4	09 3	00 -	0-	87.4	87.2	87·T	85.6	85.7	85.2	85.1	84.8	86·0
29	05.0	04.9	04.7	04'4	04.1	104.9	05.2	05.0	100.0	100.4	100.4	00.2	87.8	88.2	88.5	87.4	07.4	0,2	85.T	84.6	83.8	83.4	83·T	82.7	84.6
30	83.5	83.6	83.4	83.9	84.5	83.2	84.8	85.5	85.4	85.0	84.6	86∙1	86.8	86.7	85.9	84.2	04.9	04.0	05 1	J4 5		3 4			-40
		l— - —		- -	-	-	·			-			l	-	-		0.6	0	0	84.2	82.5	82.7	82.8	82.6	84.2
Mean	82.3	82.3	82.2	$82 \cdot 1$	82.4	83·1	83.6	84.0	84.5	85.0	85.5	85.9	86.3	86.4	86.3	86.1	80.0	05.4	04.7	3	3 3	3 1	<u> </u>	1	4 2
			·	-						-							1	18.	19.	20.	21.	22.	23.		Mean
G.M.T.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	10.	19.	20.	1	-2.	-3.	-4.	
	l		l	1	1	1	1		I	1	1	1	l	l	<u> </u>	<u> </u>	<u> </u>	<u> </u>			<u>. </u>	<u>'</u>		·	

34. Aberdeen: North Wall Screen on Tower: h_t (height of thermometer bulb above ground) = 12.5 metres.

July, 1923.

4. Aberd		Nor	tn vv	an So	reen	on 1	ower	. 11;	(neig.		then		LCI L			7		_ 12	J 11K	Julius.				y, 18	
Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Me
	$\frac{1}{a}$.	a.	<u>a.</u>	a.	<u> </u> a.	a.	a.	1 a.	a.	$\frac{1}{a}$.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	l a
I	82.9	82.6	82.4	82.6	82.9	83.2	83.5	83.5	84.8	84.8	85.1	86.2	84.3	85.0	85.1	84.4	84.4	84.6	84.1	84.0	83.8		83.6		83
2	83.5	83.4	83.0	82.7	83.1	83.7	85.5	87.5	88.6		91.5	92.9				90·I	89.2		88.6			86.4		86.4	
3	86.4	85.6	86∙1	85.6	85.8	85.9	86.4	88·o	89.4	89.4	88.9	89.7	91.0	93.9	93.5	93.9	94.0	93.0		88.1			86.5	86·o	
4	85.5			83.7	86.8	88.4	87.2	88∙1	89.5	89.3	90.0	89.7	91.1	90.3	90.7	89.0	89.0		90.6	89.2	88.6	88·o	87.3	86.2	88
5	85.4	85.7	86·o	86.1		87.3	87.7	89.9	90·I	91.3	90.4	91·I	91.0	90.2	90.8	91.6	91.2	91.1	89.9	89.5	89.4	86.6	86.9	86.2	88
6	86∙1	86·o	86·o	86∙0	86.5	88·o	86.7	89.0	88.3	89.0	89.0	90.0	90.2	88.6	87.5	87.2	88.4	88.8	87.8					86∙1	
7	86∙0	85.6	85.1	85.3	86.0	86.6	87.6	87.7	88.5	88.2	88.6	88.5	87.7	88.4	89.9	88.4		87.2		87.4			86.7		8
8	88·o			87.3		87.4	88·o	86.6	88.5	88.5	88·o	87.9	90.9		87.8	91.1	93.7	91.2	90·I	89.1	87.9		87.2		88
9	86.2	85.7				86.0	86.9	88·o	88.6	89.1	90.4	90.9	91.7	92.9	90.7	91.7	91.2	90.4	88.3	88.8				85.9	
10	86.2	86.7	86.1	86.1	86.2	86.9	87.9	88.1	89.0	89.7	89.0	88.1	89· o	88.6	88.2	88.6	88.7	87.4	86.5	86.9	87.4	86.9	86.4	85.9	8
11	85.9	86·o	85.7	86·o	86.1	86.6	87.1	87.4			88.9			88.5	87.7		88.3		87.8		87.8	87.3		86.5	
12		85.7	85.7			80.3	00.0	03.0	94.8	94.3	95.1	95.3	95.9	98∙0	99·I	95.6	93.0	90.4	90.4	90.0		88.1			
13	88·1	87.2		86.4		88·o	88.4	88.6	88.8	88.9	89.1	88.8	88.9	87.7	87.2	87.1	87.0	86.6	86.3	86.3		86.1	86.0	85.4	8
14		85.0	84.7	85.4	85.8	86·o	86.8	87.0	87.9	88.2	88.2	88∙o	88.2	88.8	89.1	88.8	88.9	88.4	88.0	87.2	86.9	86.7			
15		86.2	86.2	86.2	86.4	87.1	87.6	87.9	88.4	87.9	88.4	88·o	88.4	88.9	90.1	90.9	91.2	90.4	90.6	90.2	89.7	89.1	88.9	88.5	8
16	88.2	87.7	87.5	87.1	87.6	88.5	89.2	90.1	90.4	90.1	89.4	90.1	89.4	88·o	87.7	88.1	88·o	91.2	90.3	89.2	87.9		86.1		8
17	84.9		84.0		84.4	86.6	86.7	87.0	87.9	80·1	188.6	90.4	80.0	90.0	90.9	91.0	90.1	91.2	88.8	87.9	86.4			84.0	
18	83.4			84.0			85.9	86.9	87.4	87.9	89.0	89.6	87·0	87.3	86.8	86.4	86.3	86.3	86·o	85.2	85·o			84.6	
19	84.4			83.3	82.6	84.0	84.4	84.0	84.0	85.6	85.0	87.0	86.4	87.2	188.7	90.0	89.0	94.0	94.0	91.9		89.1			1.
20	87.7	88.1	88.6	88.4	89.0	89.3	90.2	89.8	90.0	90·I	91.1	91.7	92.4	93.I	92.6	93.0	92.1	90.6	90.0	88.7	88.2	87.8	87.4	87.1	8
21	86.8	87.1	86.9	85.8	86.9	87.6	89.6	89.9	90.6	90.4	92.5	92.4	92.2	91.9	91.8			90·I	89.7		89.0	88.7		88.1	
22	87.8			86.9		87.5	87.8	88.1	88.4	80.0	lgg•g	03.6	04.5	04.1	93.7	93.1			91.0		90.0		89.2	89.3	9
23	88.7	88.3	88.0	88.0	80.0	80.0	00.0	01.2	00.3	00.2	00.3	00.1	80.8	180∙0	00.0	8 9 ·6	88⋅1	88.1	86.5	85.8	85.6		84.9		8
24	84.2	84.0	84.1	84.0	84.2	84.7	85.1	85.9	86.7	86.6	87.6	88∙1	88·o	88·o	88.6	88∙1	87.7	87.1	85.3	85.3		84.9			
25	84.7	84.1	83.9	84.0	84.2	84.8	86∙0	88.1	89.3	90.5	91.0	91.4	90.6	90.3	90.3	91.1	89.4	89.1	89.0	87.0	85.6	85.2	85.1	85·o	8
26	84.6	84.0	83.0	83.6	83.6	84.7	85.4	85.9	86.4	86.1	87.2	85.9	83.7	84.2	84.4	85.2		86.3	86.1	85.1	84.7	84.3	84.1	83.5	
27	83.1	82.3	82.4	82.6	82.6	83.6	84.9	85.3	86.3	86.6	87.0	87.9	85.9	85.5	85.4	85.1	85.2	84.5	84.2	84.1	84 1	84.1			
28		84.2	84.2	84.2	84.0	83.0	83.8	83.0	84.0	84.0	84.1	84.0	84 ∙0	84.3	84.2	84.0	84∙0	83.9	83.6	83.6	83.4	83.4	83.4	83.4	8
29	83.2	82.2	82.2	82.2	83.2	83.6	83.8	l83·0	84.2	84.1	84.1	84.2	84.1	83.6	83.1	82.9	82.9	83.4	83.8	83.9	84.0	84.1	83.9	83.7	8
30	83.7	83.6	83.7	83.7	84.0	84.0	84.2	85·o	86.1	86.4	87.0	87.6	87.1	86.5	86.8	87.5	86.9	85.9	85.2	85.3	84.5	84.4	84.1	84.1	8
31	84.1	83.5	83.5	83.8	84.0	84.1	84.3	84.5	84.9	85.1	85.9	86.2	86· 3	85.8	85.8	85.4	85.8	85.8	85.3	85.0	85.2	85·o	85.1	85·o	8
ean	85.5	85.3	85.2	85.1	85.5	86.2	86.8	87.5	88·1	88.3	88.8	89.2	89.2	89.0	88.9	89.0	88.8	88.6	88·o	87.4	86.9	86.4	86.1	85.8	8
35. Aber	deen :	Nor	th W	l Iall S	Creer	ı on	Towe	er: h	t =	12.5	meti	res.	<u> </u>	1	1			<u>!</u>	1			,	lugus	st, 19)
															1 0			1 a	1 a	a.	a.	a.		a	1
ī	84:0	a.	a.	a.	a.	84.6	a. 85∙ĭ	a. 85:3	a. 86:2	87·I	87.6	88·2	a. 88·3	a. 86∙9	85.0	86·9	$\begin{array}{c c} a. \\ 88 \cdot 2 \end{array}$	<i>a</i> . 88⋅1	a. 88∙1						8
1	04 9	104 0	104 0	104 4	104 4	154 0	127 1	1~23	100 2	17/ 1	10,0	1	12" 3	96	12.7	10	0-	lo .	8	10	10	10	10-0	10	I٥

	1 a	1 0	1 0	1 0	1 0	1 0	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	l a.	l a.	a.	a.	a.	a.	a.	a.	a.
	a. 84·9	a. 84.6	a. 84.6	84.4	84·2	84:6		85.2	86.2	87.1	87.6	88.2	88.3	86.0	85.0	86.9	88.2	88.1	88.1	87.0	86·o	85.1	84.7	84.7	86 ⋅ 1
2	84.9		82.1	82.2	82.1	84.6	85:0	85:0	85.5	85.8	86.0	85.9	85.4	86.0	86.5	85.7	85.4	85.1	85.4	85.1	85.7	05.7	85.3	85·o	85.0
2	85.1		85.4	85.9	86·o	86.4	86.0	87.8	88·T	88·I	87.4	88·o	87.9	88.1	87.9	87.6	87.4	86.7	87.2	86∙0	85.4	85.2	84.9		86.7
3	85.1	84.0	84.6	84.8	85.1	85.7	87:0	87.2	87.8	88.2	80.1	89.0	80.8	00.0	90.5	90.2	89.0	88.8	87.0	85.8		85·o	84.9	84.5	87.1
4	84.1	84·T	84.3	84.2	84.8	85.0	85·T	86.6	87.0	88.1	87.1	87.3	88.6	89.0			88.2	87.4	86.9	86.5	86∙1	86·o	86·o	85.9	86.5
3	i .		1	1	1	1	1	1	1 '	1	1 '	-	ł	1	1 '	-		' '							
6	86.0	86·T	85.0	85:0	84.8	86∙т	80.0	80.0	90.6	90.8	92.0	91.9	92.0	92.6	90.7	90.0	90.1	90.0	90.1	88.7	87.7	87.1	86.9	86.9	88.8
7	86.8	86.4	86.0	86.0	86.3	86.0	186.0	1X6+2	186.7	187.5	187·Q	180.0	101.0	102.0	102.0	189.5	100.0	190.3	109.2	100	00 1	10/1	0,0	100 0	100.0
8	86.3	86.0	85.4	85.0	84.9	85.2	85.7	86.6	87.0	86.5	87.1	88.2	87.2	187.0	187·I	180.2	100.0	86.4	86.2	86∙1	86.0				86.4
9	87.1	88.3	88.0	8.88	88.5	88·a	8a·1	80.6	01.6	92.8	94.1	94·I	94.6	92.6	90.0	90.9	90.9	92.3	91.8	190.0	88.2	87.0	86·1	85.4	90·I
10	85:0	85.4	85.0	85.3	86.2	87.1	87.6	80.0	90.3	89.9	90·I	91.0	91.0	92.0	91.9	91.0	90.3	90·I	89∙0	88·o	87.6	87·o	86.7	86∙1	88.4
	1	1	1		1	1	1	1		1	i	i	ı		1				1					_	
11	85.9	85.6	84.9	85.4	86·o	87.6	87.6	87.6	88.7	89.2	89.5	90.0	90.4	90.9	90.9	89.9	89.9	88.8	87.3	87.1	86.8	86.0	85.2	84.9	87.8
12	84.0	83.0	83.0	82.8	82.6	84.0	84.7	86.6	88.4	89·I	90.0	90.6	90.7	101.0	100.2	1.00	100.5	100.0	00.7	100.0	87.7	88·o	88.1	88.1	87.3
13	8 ∮ ∙o	88·o	87.9	187.5	187.5	87.0	188 - т	IXX.T	187.6	IXX-T	180.2	OI·I	103.U	03.0	105.5	95.6	95.6	95·I	92.4	91.0		88.3		86.7	
14	86∙т	85.2	83.0	84.5	84.7	85.0	87.0	88.4	89.7	90.4	91.2	91.3	90.6	90.0	89.4	90.0	88∙1	188·I	86.7	86.6	86.0	85.9	85.5	85.0	
15	84.0	83.9	83.6	82.8	82.2	83.9	85.3	86.6	87.6	88.6	89∙1	88.7	88.9	87.7	87.4	87.7	86.2	86.1	86∙0	85.6	84.6	84.3	84.1	84.0	85.8
· ·	•	i		i .	1	ı	1			ì	i		1	1	1			_			0 0	0.6	0.0	0	0.6
16	84.0	83.6	84.0	83.8	83.2	84∙1	84.9	85.8	86.3	87.6	88.2	88.9	88.4	87.5	88.6	87.1	86·o	85.2	85.0	84.9	84.8	84.0	04:0	84.5	85.0
17	84.4	183·a	83.4	183.2	183.5	183·9	84·I	84.2	84.3															U .	1934
18		84.0	84.6	184.6	84.4	84.6	84.9	85.3	85.3	185.4	186.0	180.4	80.3	80.2	80.7	180.3	105.4	105.4	105.0	102.1	104 /	84.1	04.0		85.3
19	83.8	83.7	183.6	183.3	183·T	83.4	183.8	184.3	85.3	85.3	85.4	85.7	86·o	86·1	85.8	85.7	85.4	85.2	05.0	04.0	04.4	04.4	04.2		84.7
20	83.6	83.6	83.7	83.9	83.9	84.0	84.2	84.6	85·o	85.5	85.7	85.3	85∙1	85.8	85.5	85.8	85.8	85.4	85.2	85.3	85.2	85.2	85.2	85.2	84.9
		١.	i	1	1					1	į .					1	1	00 -	0	96.0	85.0	00	84.2	82.6	96
21	85.2	85.4	85.4	85.2	85.2	85·I	85.6	86.4	87.9	88.3	88.7	87.9	88.5	89.1	89.9	89.2	88.6	99.0	86.2	85.0	84.7	82.2	82.7	82.9	85.5
22																									85.2
23	83.3	82.3	82·I	81.3	81.9														04.0	03.9	83.5	82.7	81.0	82.0	84.2
24																									83.3
25	81.4	80.9	80.6	80.7	80.9	81.1	81.9	82.4	83.8	84.0	84.6	84.9	85.0	85.1	85.0	84.7	84.5	04.2	04.1	04.0	04 1	04 1	04 4	174 0	03.3
_		1	1	1	1				1	1				,		1	1 1					4	!		86.2
26	84.9	84.7	83.0	83:2	03.0	04.4	04.7	85·3	80.8	00.2	00.0	00.1	98.6	07.2	88.7	87.2	88·6	86.2	85.7	84.8	84·I	83.3	82.6	82.0	85.5
27	84.3	83.8	83.2	03.0	02.7	04.0	05.0	90.0	05.9	07.7	00.0	00'4	85.5	84.6	85.7	86.0	87·7	84.0	84.3	83:4	83.0	82.1	82.0	81.8	84.0
28					82.3	02.0	03.1	05.1	05.3	05.9	05.9	05.2	05.5	84.7	85.7	84.4	86·1 84·1	84 T	83.0	83.0	82.7	82.5	82.0	82.3	82.8
29	81.0	80.0	79.4	79.0	78.6	90.0	82.3	03.3	04.0	04.0	05.0	04.9	94.0	92.4	82.7	82.1	83·o	82.7	82.8	82.6	82.4	82.3	82·1	82·I	82.4
30	82.0	82.3	82.0	81.9	02.0	02.0	02.1	02.0	91.9	02.0	02.2	02.0	03.1	03.4	03.1	03.1	03 0	02 /	02 0	.	4	- 3	02 -	-	.
	82.0	87.8	87.8	81.7	81.6	8T.E	81.7	82.0	84.2	84.4	84.2	85.2	80.8	85.8	85.7	85·T	84.9	83.0	83.2	82.2	81.2	80·1	79.9	79.0	83.0
31	02.0	01.0	01.0	91.7	01.0	<u> </u>	01.7	9	94.3	04'4	04.2	05 2	05.0	-50			-73								
Mean	84.5	84.3	84.0	83.9	83.8	84.6	85.2	86∙ o	86.7	87.2	87.6	87.9	8 8·2	88.2	88·1	87.8	87.4	87·0	86· 5	85.8	85.2	84.9	84.7	84.5	86∙0
	<u> </u>		<u> </u>			<u> </u>					<u></u> -	<u> </u>													
G.M.T.	1.	2.	3.	4.	5.	6.	7.	8.	9.	IO.	II.	12.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
	<u> </u>		l	<u> </u>																	!			!	

36. Aberdeen: North Wall Screen on Tower: h_t (height of thermometer bulb above ground) = $12 \cdot 5$ metres.

September, 1923.

Day.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mear
1 2 3 4 5	82·6 78·0	82·6 77·4	77.9	a. 78·8 81·8 77·1 84·1 82·5	81·9 76·3	81·7 77·0	80.6	a. 82·7 82·4 83·3 83·0 84·8	84.4	85.3	84·5 86·0 85·0	a. 84·9 84·1 86·4 86·5 89·3	84·6 87·9 87·0	87.4	86.7	85·0 86·4 87·0	84·9 86·0 86·4	86.4	85·9 84·8	85·2 84·1	80·2 84·4 83·1	84·1 82·9	82.9	84·I 82·3	82·7 83·2 84·7
6 7 8 9	88.1	88·2 80·3	85·6 80·3	84·2 79·8	84·I 80·0	83·7 80·0	84·2 81·0 86·7	88·1 85·1 82·9 87·5 84·1	85·6 84·6 88·0	86·2 85·6 80·6	86·9 85·9	87·0 85·8 90·1	87·1 85·0 88·7	87·5 84·9 80·8	85·5 89·4	86·2 86·2 80·0	85·6 85·9 88·5	85.5	84·1 85·0 85·9	83·0 84·5 85·0	82·5 84·6 84·2	84.9	81·0 85·3 82·1	81·2 85·0 81·9	85·2 83·7 86·7
11 12 13 14	79.9	86·9 79·2	87·0 78·6 85·1 82·1	86·4 79·1 85·1 81·5	78·8 85·1 81·5	84·6 80·1 84·9 81·2	84.6 81.0 84.4 81.3	85.6 81.8 84.5 81.9	82·9 85·4 82·4	86·5 83·5 85·8 84·0	86·9 83·2 86·4 85·1	87·7 83·1 86·8 86·0	87·9 83·0 87·3 86·3	88·0 83·0 87·1 86·7	82·9 87·2 86·1	86·9 82·9 87·3 86·5	86·1 83·1 86·5 86·2	85·0 83·5 85·7 85·2	84·3 84·1 84·3 83·9	84·3 82·7	83·0 84·6 84·1 82·3	01.0	81·0 85·0 84·0 81·0	80·4 85·0 83·1 80·8	85·6 82·3 85·4 83·4
16 17 18 19 20	83·6 81·0	1 - 4	82·9 80·1 77·6	79·1 76·6	79·6 76·0	78·9 76·0	79·9 76·6	82·7 83·1 82·1 81·3 77·9	82·5 82·9 79·4	83·0 84·1 81·4	84·1 84·5 82·2	85·1 84·2 83·3	85·0 83·6 83·7	83·1 83·8	83·4 83·5	84·0 83·7	84·1 83·5	83·9 82·6	83·3 80·6	83·0 79·0	82·6 78·0	82·2 77·5	80·9 77·6	79·4 77·1	82·1 79·8
21 22 23 24 25	80.2	76·9	79·2 76·6 79·9 83·9	79·4 76·8 79·4 83·7	79·3 77·2 79·4 83·6	79·9 77·3 79·0 83·3	80·1 77·9 78·4 83·3	i	81·3 80·8 81·9 83·4	83.0 82.2 82.4 83.7	84·3 83·1 83·1 85·1	84·7 83·4 83·4 85·6	85·7 83·7 82·7 86·0	85·9 83·5 82·0 86·0	83·7 82·9 85·4	85.6 83.1 83.3 85.7	84.0 82.3 83.1 84.9	82·7 82·0 82·8 84·3	80·5 83·0 83·8	79·4 83·2 83·7	80·0 79·6 83·0 83·6	83·0 83·0	78·9 79·1 83·3 82·7	83·5 82·3	81·6 80·2 81·7 84·1
26 27 28 29 30	85·8 88·2 84·0	85.3	84·9 88·0 84·0	84·6 87·8 84·3	85·0 87·4	84·6 87·9 83·0	85·0 88·2 83·5	82·6 85·2 85·9 84·3 86·5	85·5 85·9 85·8	85·1 87·5 86·4	84·9 87·9 87·8 93·9	84·9 88·2 88·8 93·6	85·0 88·4 88·7 93·0	85.0 89.2 87.4 92.5	85·5 88·7 87·1 9 1 ·6	86.6 87.4 86.8 91.5	87.0 85.8 90.4	86·5 85·1 89·6	86·1 85·0 89·2	84·8 84·9 88·7	84·6 85·0 88·7	84·0 84·8 87·9	84·0 84·9 87·5	84·2 85·0 88·0	85·4 88·6
			82.T	81.0	81.8	81.9	82.4	83.2	84.2	85·1	85.8	86.2	86· 4	86.4	86.1	85.9	85.5	85∙0	84.3	83.7	83.5	83.1	82.9	82.7	83.9
Mean	82.4	82.2	02 1				<u> </u>		1		1		<u>'</u>	<u> </u>	<u> </u>										
	<u> </u>					T	`	. h.	10).5 m	204*00		<u> </u>	<u>.</u>	· · · · · ·							0	ctobe	r. 19	23.
Mean	leen :	Nor	th W	all S	creen						,		1 a			1 a	1 a	1 a.	\ a.	1 a.	a.	0 a.	ctobe	or, 19	23.
	a. 88·1 82·6 78·7	Nor- 87.7 82.4 78.2	a. 87.4 82.7 77.4	all Se 86.7 82.9 76.9	a. 85.0 82.7 76.6	a. 83·7 81·5 75·6	a. 83.0 81.1 75.8	a. 83.6 81.2	a. 84.8 82.1 77.9	a. 85·4 82·6 79·4	a. 86·0 83·0 81·3	a. 86·9 82·6 81·5	83·9 82·3	83·0 82·2	a. 87.6 83.0 82.1 80.7 81.7	82·8 81·1	70.4	80·8 79·9 78·8	a. 83·2 80·4 78·6 78·4 82·1	79·6 78·4 78·0	83·4 79·4 78·8 76·5	a. 83·4 79·4 79·3 74·6	a. 83·0 78·6 79·8 74·7	a. 83·0 78·3 79·7	a. 85·4 81·7 79·1 78·4
37. Aberd	a. 88·1 82·6 78·7 79·9 76·3 80·9 81·0 80·9	Nor- a. 87.7 82.4 78.2 79.1 77.2 79.8 81.1 80.2	a. 87.4 82.7 77.4 78.5 77.3 79.2 81.5 80.1	all So 86·7 82·9 76·9 78·0 81·0 81·4 79·1	a. 85.0 82.7 76.6 78.0 78.1 80.9 81.1 79.1	a. 83.7 81.5 75.6 77.7 77.7 80.8 81.1 78.8	a. 83.0 81.1 75.8 77.6 77.3 80.2 82.4 79.7	a. 83.6 81.2 76.1 78.1 77.6 80.4 83.3 80.6	a. 84·8 82·1 77·9 78·7 78·5 81·6 84·0 81·9	a. 85·4 82·6 79·4 79·0 79·1 81·6 84·7 83·0	a. 86·0 83·0 81·3 77·2 80·1 82·9 86·6 84·0	a. 86·9 82·6 81·5 79·2 79·9 84·0 86·1 84·4	87·4 83·9 82·3 80·7 79·9 85·5 85·5 84·9	87.6 83.0 82.2 80.8 81.0 85.6 86.7 84.4	87.6 83.0 82.1 80.7 81.7 85.7 86.6 84.2 85.5	87.0 82.8 81.1 80.1 81.7 85.1 85.8 83.9 84.9	85.7 82.2 80.9 79.4 81.6 84.1 85.1 83.4 83.2	84·5 80·8 79·9 78·8 82·1 82·7 84·8 82·8 83·0	83·2 80·4 78·6 78·4 82·1 81·9 84·4 82·1 82·7	83.6 79.6 78.4 78.0 81.8 81.0 83.7 82.1 82.3	83.4 79.4 78.8 76.5 81.2 80.5 83.4 81.4 82.1	a. 83·4 79·4 79·3 74·6 80·9 79·7 82·6 81·4	a. 83.0 78.6 79.8 74.7 80.1 80.7 82.6 81.8 81.6	a. 83.0 78.3 79.7 75.4 79.5 81.6 82.0 82.1	a. 85·4 81·7 79·1 78·4 79·5 81·9 83·6 81·9 83·5
37. Aberd 1 2 3 4 5 6 7 8 9	a. 88·1 82·6 78·7 79·9 76·3 80·9 81·0 80·9 82·4 81·6 78·8 80·3 78·7 77·1	Nor a. 87.7 82.4 78.2 79.1 77.2 79.8 81.1 80.2 83.0 81.0 79.1 80.3 78.6	a. 87.4 82.7 77.4 78.5 77.3 79.2 81.5 80.1 83.8 80.7 79.2 80.4 79.8 77.0	all So a. 86·7 82·9 76·9 78·7 78·0 81·0 81·4 79·1 84·1 81·0 79·3 80·1 79·4 77·0	a. 85.0 82.7 76.6 78.0 78.1 80.9 81.1 79.1 84.0 79.9 78.2 80.1 76.9	a. 83.7 81.5 75.6 77.7 77.7 80.8 81.1 78.8 83.6 81.4 78.6 80.0 77.9 75.7	a. 83.0 81.1 75.8 77.6 77.3 80.2 82.4 79.7 82.9 81.3 79.3 79.7 78.1	a. 83.6 81.2 76.1 77.6 80.4 83.3 80.6 82.9 81.2 79.9 80.4 78.9	a. 84.8 82.1 77.9 78.7 78.5 81.6 84.0 81.9 83.6 82.5 80.0 81.6	a. 85·4 82·6 79·4 79·0 79·1 81·6 84·7 83·0 84·3 80·8 82·3 80·7	a. 86·0 83·0 81·3 77·2 80·1 82·9 86·6 84·0 85·0 84·1 81·4 82·8 81·3	a. 86·9 82·6 81·5 79·2 79·9 84·0 86·1 84·4 84·5 85·1 81·9 83·4 81·2	87·4 83·9 82·3 80·7 79·9 85·5 84·9 85·0 86·0 81·8 83·7 81·8	87.6 83.0 82.2 80.8 81.0 85.6 86.7 84.4 85.5 86.1 82.0 83.5 81.2	87.6 83.0 82.1 80.7 81.7 85.7 86.6 84.2 85.5 85.7 82.6 83.1 81.2	87.0 82.8 81.1 80.1 81.7 85.8 83.9 84.9 85.0 81.8 82.7 81.7	85.7 82.2 80.9 79.4 81.6 84.1 85.1 83.4 83.2 83.7 80.8 82.4 79.4 79.6	84·5 80·8 79·9 78·8 82·1 82·7 84·8 82·8 83·0 82·1 79·9 81·0 78·8 78·4	83·2 80·4 78·6 78·4 82·1 81·9 84·4 82·1 82·7 81·1 79·0 80·0 78·6	83.6 79.6 78.4 78.0 81.8 81.0 83.7 82.1 82.3 80.4 78.8 79.6 78.2 78.5	83.4 79.4 78.8 76.5 81.2 80.5 83.4 81.4 82.1 79.7 77.9 79.4 78.1 78.4	a. 83·4 79·4 79·3 74·6 80·9 79·7 82·6 81·4 81·9 79·5 78·8 79·1 77·9	a. 83.0 78.6 79.8 74.7 80.1 80.7 82.6 81.8 81.6 79.1 78.8 78.9 77.5	a. 83.0 78.3 79.7 75.4 79.5 81.6 82.0 82.1 81.4	a. 85·4 81·7 79·1 78·4 79·5 81·9 83·6 81·9 83·5 82·2 79·9 81·0 79·3 78·5
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37. Aberd 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	a. 88.1 82.6 78.7 79.9 76.3 80.9 81.0 80.9 82.4 81.6 78.8 80.3 77.1 77.1 80.0 79.4 81.9 83.6 79.7 82.7 79.6 80.6 80.5 76.2 80.9 87.4 82.9 80.6 84.3 82.4	87.7 82.4 78.2 79.1 77.2 79.8 81.1 80.3 78.6 77.1 77.4 79.9 83.9 80.0 82.8 79.8 80.1 80.1 80.1 77.0 80.1 77.0 80.1 77.0 80.1 80.1 80.1 80.1 80.1 80.1 80.1 80	th W a. 87:4 82:7 77:4 78:5 77:3 79:2 80:0 80:7 79:2 80:0 79:2 80:0 79:0 82:4 84:0 79:7 77:7 77:7 77:7 79:3 79:3 86:0 85:7 81:4	all So a. 86·7 82·9 76·9 78·0 81·0 81·1 84·1 81·0 79·3 86·1 79·4 82·6 79·1 79·9 77·5 79·3 83·5 79·9 84·7 80·9	a. 85.0 82.7 76.6 78.0 78.1 80.9 81.1 79.9 78.2 80.1 76.9 77.9 80.1 80.0 82.2 84.2 79.4 82.5 79.4 77.1 78.5 82.2 81.6 79.4 80.7	a. 83.75 75.6 77.7 77.7 80.8 81.1 78.8 83.6 81.4 78.6 80.0 77.9 80.1 82.1 82.1 82.8 79.4 79.0 79.3 76.8 81.4 81.5 78.9 84.6	a. 83·0 83·0 83·0 80·1 75·8 77·6 77·3 80·2 82·4 79·7 82·9 81·3 79·3 79·7 78·1 77·9 79·7 80·0 83·1 79·1 79·4 77·2 79·5 82·5 82·5 82·5 83·1 84·9 80·9	a. 83·6 83·6·1 76·1 77·6 80·4 83·3 80·6 82·9 81·2 79·9 80·4 78·9 77·7 78·5 79·8 80·4 82·3 85·0 81·0 83·6 79·6 79·6 79·8 81·0 82·7 78·6 88·6 88·6 88·6 88·6 88·6 88·6 88	a. 84.8 82.1 77.9 78.7 78.5 81.6 84.0 81.9 83.6 82.5 80.0 81.6 79.2 79.2 79.8 83.1 85.6 82.0 83.9 80.4 79.8 79.9 79.9 80.6 83.0 81.9	85.4 82.6 79.4 79.0 79.1 81.6 84.7 83.0 84.3 82.3 80.4 80.9 85.2 82.7 83.8 81.0 81.1 80.4 83.4 83.4 83.4 83.4 83.4 83.4 83.4 83	a. 86.0 83.0 81.3 77.2 80.1 82.9 86.6 84.0 85.0 84.1 81.4 82.8 81.3 80.4 81.7 80.8 83.2 84.8 85.1 83.4 81.5 81.6 82.1 80.9 83.6 82.5 86.8 84.1	a. 86·9 82·6 81·5 79·2 79·9 84·0 86·1 81·9 83·4 81·2 80·3 83·4 84·0 84·8 84·0 83·6 82·2 82·4 82·9 83·6 82·2 82·3 83·4 82·3 83·6 82·2 83·6 83 83·6 83 83 83 83 83 83 83 83 83 83	87·4 83·9 82·3 80·7 79·9 85·5 84·9 85·6 81·8 83·7 81·8 81·0 85·6 84·1 85·6 84·1 85·6 84·1 85·6 84·1 85·5 84·1 85·5 84·1 85·5 84·1 85·5 84·1 85·5 84·1 85·5 84·1 85·5 84·1 85·5 84·1 85·5 84·1 85·5 86·2 86·2 86·3	87.6 83.0 82.2 80.8 81.0 85.6 86.7 84.4 85.5 86.1 82.0 83.8 80.7 83.9 84.6 84.8 83.4 83.6 82.9 83.6 83.6 83.6 83.6 83.6 83.6 83.6 83.6	87.6 83.0 82.1 80.7 85.7 85.7 85.6 83.1 81.2 80.4 83.8 80.5 84.3 83.9 84.0 84.2 83.8 83.1 82.6 82.9 82.7 80.2 83.1 82.6 83.1 82.6 83.1 83.0 84.0 83.1 83.0 84.0 84.0 84.0 85.0 84.0 85.0 85.0 85.0 85.0 85.0 85.0 85.0 85	87.0 82.8 81.1 80.1 81.7 85.1 85.8 83.9 84.9 85.0 81.8 82.7 81.1 70.2 83.0 80.7 83.3 84.1 83.0 82.0 82.1 82.6 79.9 82.1 84.9 83.3	85.7 82.2 80.9 81.6 84.1 83.4 83.2 83.7 80.8 82.4 79.4 78.6 82.0 79.3 82.3 84.0 81.9 82.0 81.1 80.7 82.0 79.6 81.1 80.7 82.0	84.5 80.8 79.9 78.8 82.7 84.8 83.0 82.1 79.9 81.0 78.8 78.4 81.1 81.7 80.9 82.9 81.4 81.7 80.9 82.0 82.1 81.7 80.9 81.6 79.3 82.8 83.6 82.8 83.6	83·2 80·4 78·6 78·6 82·1 81·9 84·4 82·1 82·7 81·1 79·0 80·0 78·6 80·9 77·1 82·7 83·2 88·3 84·0 81·6 80·9 78·6 81·9 78·6 80·9 78·6 81·9	83.6 79.6 78.4 78.0 81.8 81.0 83.7 82.1 82.3 80.4 78.8 78.5 81.1 76.8 82.7 83.1 80.9 83.9 80.4 81.6 78.3 81.6 82.7 83.1 80.4 83.7 83.1 80.9 83.9 80.4 81.6 83.9 80.4 81.6	83·4 78·8 76·5 83·4 82·1 79·7 77·9 481·1 77·2 82·3 83·4 80·6 83·4 80·6 80·0 81·5 77·9 78·9 78·9 80·1	a. 83·4 79·4 79·3 74·6 80·9 79·7 82·6 81·4 81·9 77·5 82·6 77·5 82·0 83·4 80·4 80·1 81·4 77·5 81·3 77·8 83·0 81·0 82·6	8.0.7 8.0.7 8.0.7 80.7 80.7 80.7 80.7 80.7 80.7 80.7 80.3 78.6 80.3 80.3 80.3 80.3 80.1 81.0 81.1 81.0 80.7 83.0 80.3 80.3 80.3 80.1 81.0 80.7 80.3 80.3 80.4 80.7 80.3 80.4 80.7 80.3 80.7 80.3 80.7 80.3 80.7 80.7 80.7 80.7 80.7 80.7 80.7 80.7 80.7 80.7 80.7 80.7 80.7 80.3 80.3 80.1 80.	a. 83.00 78.33 79.77 75.44 79.5 81.6 82.01 81.44 78.9 78.6 77.5 78.0 80.1 79.0 83.2 79.8 82.6 80.7 80.8 77.0 81.2 77.3 82.8 80.9 84.9 82.7 79.0 82.1 81.2 79.0 81.2 79.0 81.2 79.0 81.2 79.0 81.2 81.2 81.2 81.2 81.2 81.2 81.2 81.2	85 85 87 9 81 9 83 9 81 9 8 8 9 8 8 9 8 8 9 8 8 9 8 8 9 8 8 9 8 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 9 8 9

TEMPERATURE.

Readings in degrees absolute at exact hours, Greenwich Mean Time.

38. Aberdeen: North Wall Screen on Tower: ht (height of thermometer bulb above ground) = 12.5 metres. November, 1923.

	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
1 2 3 4 5	79·6 81·0 78·2	79·4 82·0 77·7	79.1		76.9	85.5	a. 78·0 77·7 85·0 76·6 77·0	76.9	83·8 77·0	79·4 83·4 77·9	81·o 78·1	81·3 79·0	82·0 81·4 79·7	82·1 79·4 79·1	81·8 78·9 79·5		80·0 76·6 77·7	79·7 76·9 77·5	77.5		76·7 77·2	a. 78·7 80·1 76·7 78·0 74·7	77·1 77·7	80·7 77·7	a. 79·7 79·9 80·5 77·8 77·2
6 7 8 9 10	75·3 72·4	74·9 76·1 72·7	74·2 75·4 76·0 73·0 74·6	75·1 75·7 73·7	75·0 76·4 74·5	74·6 74·9 77·0 75·5 73·6	74·7 74·4 77·4 76·1 73·4	74·6 74·1 77·6 76·1 73·4	74·3 77·4 78·0	75·2 77·7 78·9	76·3 78·1 80·3	76·7 78·8 80·9	78·6	76·8 79·2 79·9	76·1 78·3 80·8	75·9 77·3 80·3	75·4 76·6 80·3	75·4 80·3	75·3 74·3 80·0	73·6 80·1	77.8	76.6	75·3 72·4 76·7	74·7 75·7 72·1 75·0 78·6	75·4 76·3 77·4
11 12 13 14 15	86·o 78·o 78·1	85·6 77·9 77·1	78·4 85·5 78·1 77·0 72·4	85·2 77·0 76·8	84·5 76·6 77·0	76·6 84·4 76·4 76·6 71·9	85·1 76·3	84·6 76·4 76·0	76.3	84·9 77·1 76·6	84·I 77·7 77·4	83·4 77·9 78·0	83·0 78·1 77·5	82·0 78·3 76·7	81·1 78·1 75·7	78·2 75·5	80·0 78·6 75·3	80·0 79·1	79·4 79·9 74·7	78·4 80·5 74·1	78·2 81·2 74·0	84·7 77·9 80·4 73·8 77·2	78·4 73·7	78·1	82·4 78·1 76·0
16 17 18 19 20	74·9 77·4		76·2 75·0	75·I 77·7	75·2 75·7 76·6		74·7 75·1 76·2	75·9 74·0 75·9 76·4 75·3	74·5 76·0 76·2	76·0 75·1 76·4 76·4 77·1	75·5 76·9 77·7	76·o 77·5 77·4	76·1 77·9 76·6	75·9 77·9 76·8	75·4 77·9 76·5		75·7 75·7	74·6 76·1	74·9 76·4 74·9	75·I	74·4 76·2 75·0		74·I	74·0 76·9 75·0	75·6 75·2 76·1 76·3 76·3
21 22 23 24 25	74.0	72.5	76.7	74·2 72·4	72.4	76·6 73·9 72·9	73.6	75·I 75·9 73·2 72·7 76·0	76.0	75·6 76·0 73·8 73·0 76·2	76·5 76·8 73·9 73·8 77·1	77·2	75.1	76.8	75.8	75·0	73.9	74.7	77·I 74·0 74·6 7I·7 76·0	74.3	77·6 73·9 73·5 71·5 75·6	77·6 74·0 72·9 71·6 76·4	73·I	73.8	76·3 75·8 74·0 72·9 75·8
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Mean	76.1	76.2	76.2	76.1	75.9	76.0	76· o	75.9	76.2	76.8	77.4	78·o	78.0	77:9	77.6	77.0	76.8	76.6	76.4	76.4	76.3	76.1	76.1	76.0	76.6
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TEMPERATURE: ANNUAL MEANS OF HOURLY VALUES.

From readings in degrees absolute at exact hours, Greenwich Mean Time.

40. Aberdeen: North Wall Screen on Tower: h = 12.5 metres.

1923.

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7'	a. 9·74	$\frac{a}{65}$	$\frac{a}{79 \cdot 58}$	a. 79·51	79·51	a. 79·77	a. 80·07	a. 80·42	-a. 80⋅86	$\frac{a}{a}$. 81·33	a. 81·77	a. 82·12	a. 82·26	 82·28	a. 82·15	-a. 81⋅89	а. 81·61	$\frac{\overline{a}}{81 \cdot 31}$	a. 80·93	<i>a</i> . 80⋅63	<i>a</i> . 80⋅33	-a. 80∙08	a. 79·96	$\frac{a}{79 \cdot 82}$	a. 80·73

TEMPERATURE: MONTHLY MEANS AND DIURNAL INEQUALITIES.

The departures from the mean of the day are adjusted for non-cyclic change.

41. Aberdeen: North Wall Screen on Tower: $h_t = 12.5$ metres.

1923.

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	a. 278·54	a.	a.	 a.	a.	a.	-a.	<i>a.</i> −0.48	$-a. \\ -0.49$	a. 0:45	a. -0·11	$\frac{a}{a}$	$\frac{\overline{a}}{+0.56}$	-a. +o⋅8o	$-\frac{a}{0.90}$	-a. +0·69	-a. +0.43	<i>a</i> . +0·14	_a. _0.05	a. -0.07	<i>a</i> . −0.05	_a. _0·19	a. 0.00	_a. _0.09	a. -0·13
	278·54 277·60 278·15																							-0·39	-0·05 -0·53
April May June	278·51 280·21 284·19	-0·84 -1·78 -1·82	-0.86 -1.91 -1.87	-0.95 -2.02 -1.96	-1·00 -2·08 -2·02	-1·11 -1·81 -1·71	-0·77 -1·08 -1·06	-0·45 -0·24 -0·54	-0·16 +0·15 -0·12	+0·15 +0·51 +0·30	+0·52 +1·00 +0·85	+0.81 +1.42 +1.35	+ 1·22 + 1·65 + 1·74	+1·26 +1·61 +2·06	$^{+1\cdot38}_{+1\cdot76}_{+2\cdot20}$	+1·33 +1·75 +2·11	+1·12 +1·47 +1·89	+0·71 +1·51 +1·77	+0·44 +1·21 +1·21	+0·03 +0·75 +0·52	-0.23 +0.12 +0.10	-0·29 -0·42 -0·70	-0.82 -0.84 -1.19	-0·62 -1·23 -1·44	-0·75 -1·53 -1·70
July Aug. Sept.	287·32 286·01 283·94	1·77 1·59 1·41	-1·98 -1·84 -1·56	-2·09 -2·10 -1·77	-2·24 -2·21 -1·94	-1·77 -2·22 -2·03	-1.08 -1.49 -2.01	-0·52 -0·83 -1·46	+0·16 -0·07 -0·69	+0·77 +0·67 +0·34	+1.02 +1.21	+1·46 +1·61 +1·83	+1.88 +1.92 +2.29	+1·87 +2·24 +2·48	+1.69 +2.21 +2.40	+1.62 +2.11 +2.15	+1.67 +1.82 +1.91	+1·51 +1·42 +1·49	+1·29 +1·08 +1·00	+0.68 +0.56 +0.27	+0.02 -0.13 -0.29	—0·50 —0·69 —0·59	-0.96 -1.02 -0.97	1·21 1·22 1·20	-1.43 -1.38
Nov. Dec.	276.34	-0·52 -0·25	-0·43	-0.43 -0.53	-0.21 -0.11	-0.14	-0.10	-0.05 -0.04	-0.01 -0.43	+0.09	+0.10	+0.04	+0.76	+0.87	+0.79	+0.42	+0.11	-0·15	-0.25	_0·25	-0·28	-o·35	-0.40	_0·46	0.43
Year	280.73	-0 ·99	— 1 ·07	-1.15	<u></u>	-1.22	-0 ·95	− 0·65	-o·31	+0.13	+0.60	+1.01	+1.39	+1.23	+1.55	+1.41	+1.12	+o·88	+0.57	+0.19	-0·11	-0.41	—o·6 6	–o·78	-0 ·92

ABSOLUTE EXTREMES OF TEMPERATURE FOR EACH DAY.

Maximum and Minimum for the interval 0h. to 24h., Greenwich Mean Time.

42. Aberdeen: North Wall Screen on Tower: $h_t = 12.5$ metres.

1923.

42.	74501										<u> </u>		<u> </u>		f .		C-	-4	0	ct.	N.	ov.	D	ec.
Month	Ja	n.	Fe	eb.	Ma	ar.	Ar	oril.	M	ay.	Ju	ne.	Ju	ly.	Aı	ug.		pt.		Ci.	111			ec.
Day.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
1 2 3 4 5	a. 77.0 82.4 79.9 79.2 78.8	a. 73·6 76·9 76·7 74·9 76·3	a. 85·9 84·2 82·8 80·1 81·5	a. 82·3 77·8 77·3 75·6 77·1	a. 76·9 80·0 78·2 80·7 80·4	a. 75·5 76·3 77·0 76·3 77·0	a. 78·9 79·4 79·8 81·3 80·4	a. 77.9 78.3 78.3 78.4 77.9	a. 81·2 81·1 88·0 92·0 89·4	a. 78·6 77·2 76·6 81·1 82·8	a. 87·1 92·3 84·4 82·7 84·9	a. 78·2 80·4 78·2 78·0 78·9	a. 86·2 93·8 94·4 91·7 92·1	a. 82·3 82·5 85·3 83·1 85·0	a. 89·2 86·7 88·9 90·9 89·8	a. 84·1 81·6 84·6 84·4 84·0	a. 85·7 85·8 88·5 88·3 90·3	a. 78·4 78·0 76·0 82·3 82·0	a. 88·4 83·9 82·9 81·1 82·4	a. 82·8 78·3 75·4 74·2 75·4	a. 82·9 82·2 85·5 80·0 79·1	a. 77.7 77.2 76.2 76.2 74.4	a. 78·3 80·0 77·6 79·1 79·5	a 75·3 74·9 72·7 72·5 74·8
6 7 8 9	77·7 81·8 83·4 78·9 78·7	73·2 76·3 75·6 75·5 75·7	80·3 80·0 80·7 79·7 79·2	76·9 75·9 77·5 75·2 77·9	80·0 80·7 79·1 78·9 77·7	76·6 76·1 77·1 75·7 75·5	78·3 79·0 79·2 78·8 79·8	76·1 76·0 76·5 76·3 76·6	88.0 86.4 86.0 83.0 80.2	78·5 76·4 76·4 74·2 73·6	84·1 92·0 89·9 90·4 88·9	76·9 78·0 83·7 83·7 81·8	90·8 90·1 94·1 93·3 90·0	85·6 84·5 86·4 85·2 85·6	93·0 92·6 88·4 95·0 92·4	84·6 85·8 84·8 85·4 84·9	92·7 88·2 86·4 90·7 87·9	85·1 80·8 79·5 81·7 81·0	85·8 87·1 85·1 85·6 86·3	79·1 80·9 78·4 80·9 78·3	76·6 77·0 79·3 80·9 7 ⁸ ·7	74·0 74·0 72·1 72·0 73·2	76·3 78·9 79·4 75·2 81·0	73.0 74.8 73.5 72.5 75.1
11 12 13 14 15	78·6 75·6 82·2 81·6 80·2	74·6 72·5 72·3 77·3 77·4	79·2 80·0 78·8 76·3 77·0	77·8 78·0 76·0 74·4 74·4	79·1 79·0 83·8 80·1 78·3	76·7 76·3 75·6 73·7 76·0	78·7 79·9 83·8 81·0 79·1	77·2 78·0 78·9 78·7 77·6	78·8 79·4 81·6 81·8 82·0	74·1 75·5 76·1 75·7 75·8	86·4 90·3 87·6 83·3 83·2	80·0 81·1 81·4 78·4 76·1	92·1 99·3 89·4 89·3 91·4	85·4 85·2 85·4 84·6 86·1	91·3 91·4 95·7 91·4 89·9	84·8 81·9 86·7 83·8 81·9	88·4 88·4 85·1 88·1 87·0	83·0 80·4 78·4 83·1 80·7	82·6 83·8 82·2 81·5 84·0	77·9 78·6 77·4 75·4 77·1	88·2 86·6 81·2 78·4 78·5	76·0 77·8 76·2 73·3 71·5	81·4 82·1 81·0 81·1 77·6	79·2 80·6 75·9 76·1 75·2
16 17 18 19 20	79·0 80·6 80·1 85·1 77·0	76·4 75·5 75·8 76·8 73·7	77·0 76·2 75·8 76·2 75·4	75·5 74·9 74·9 75·2 72·8	79·6 79·9 79·6 78·9 79·6	75·8 73·3 75·9 73·5 75·6	80·0 80·8 79·9 80·0 80·4	77·8 77·2 76·2 77·3 76·9	81·4 80·1 80·4 86·1 85·1	75.4 75.4 75.9 79.3 80.3	83·7 84·0 91·0 87·1 86·6	76·9 78·9 81·5 80·4 80·2	91·2 90·0 94·4 93·2	85·0 83·5 83·0 83·1 87·0	89·1 89·0 86·9 86·6 86·0	83·2 83·1 83·8 83·1 83·4	86·1 84·8 85·2 84·9 84·0	78·8 78·6 79·9 78·5 75·6	81·6 84·8 84·8 86·0 84·9	76·4 78·6 81·8 79·8 79·3	76·7 76·7 78·0 77·8 79·3	74·0 73·8 73·9 74·6 74·3	84·9 83·8 79·8 76·1 75·2	76·9 78·7 74·2 72·1 71·9
21 22 23 24 25	85·0 83·4 82·6 84·5 83·9	75·0 75·3 75·0 81·2 79·9	75.4 76.3 78.0 78.7 77.5	73·2 74·7 73·8 76·7 75·5	80·2 80·2 79·6 79·8 82·9	73·1 74·1 77·4 77·4 74·0	80·0 80·1 79·0 80·0 85·0	75·1 75·1 74·1 73·2 75·6	84·7 81·7 82·6 85·4 81·2	78·0 74·8 74·4 75·9 77·3	90·3 92·0 94·6 89·2 86·1	85·1 86·0 87·0 80·0 78·9	93·0 94·6 91·5 88·9 92·2	85·5 86·9 84·3 83·9 83·3	90·1 90·1 89·4 85·4 85·6	83·6 82·1 81·1 81·9 80·4	82·4 86·2 83·8 83·6 86·3	77.6 76.2 78.0 82.3	84·3 83·6 82·9 83·8 83·6	80·0 78·6 78·8 76·3 76·2	78·0 77·8 75·3 74·6 78·3	74·4 73·7 72·4 71·4 72·5	74·4 78·3 76·6 75·6 75·0	72·4 73·2 73·6 70·4 70·9
26 27 28 29 30	84·5 84·6 80·5 79·9 83·9	80·7 77·9 77·5 76·1 76·0	78·4 79·0 78·9 —	75·8 77·7 76·2 —	82·9 83·6 82·1 83·6 79·0	76·5 79·0 80·2 78·8 78·0	81·2 82·1 82·0 84·0 83·2	75·9 74·8 73·1 75·0 78·4	81·4 83·0 82·1 83·4 81·7	78·2 79·2 77·9 77·5 79·0	87·5 86·5 91·5 88·6 87·2	77.5 82.5 83.8 84.0 82.7	88·0 87·9 84·4 84·4 87·7	83·3 82·2 83·3 82·8 83·5	89·6 89·5 87·0 85·7 83·5	82·7 82·6 81·6 78·5 81·7	87·7 88·0 89·4 89·0 94·5	81·4 84·4 83·8 82·7 84·4	81·5 83·6 83·7 84·9 87·1	76·8 77·1 80·8 78·6 82·6	77·6 75·3 78·1 77·3 76·0	72·6 72·5 72·5 73·9 73·4	74·1 75·5 76·9 75·1 77·1 81·2	70.0 72.6 72.9 70.2 74.9
31	84.3	78.5			78.8	77.1		_	82.7	78.3			86.6	83.4	86.3	79.0	87.2	80.3	84.2	78.4	79·I	74.1	78.3	74.1
Mean	81.1	76.1	78.9	76.1	80·1	76.2	80.5	76.6	83.3	77.1	87.8	80.7	90.9	84.4	89.2	83.1	87.2	50 3		/	'	/ -	1,23	/4 -

Note.—The initial 2 or 3 of the readings is omitted, i.e. 275 o degrees absolute is written 75.0.

43. Aberdeen: North Wall Screen on Tower: h_t (height of thermometer bulbs above the ground) = 12.5 metres. January, 1923.

^{*} Computed from the mean temperature and mean relative humidity.

[†] Mean of the column.

45. Aberdeen: North Wall Screen on Tower: ht (height of thermometer bulbs above the ground) = 12.5 metres. March, 1923.

45. Aberdeei	n :]	Nortl	n Wa	all S	creei	n on	Tow	er:	h_t (1	heigh	nt of	therm	ome	ter l	oulbs	abo	ve t	he g	roun	(d) =	= 12	5 m	etres	S.	Marci	h, 1923.
Day.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
1 2 3 4 5	90 80 92 97 88	% 90 85 92 97 91	90 90 87 92 97 89	% 89 88 91 96 89	% 89 89 92 96 89	% 90 91 92 95 88	% 90 91 94 94 87	% 93 88 95 94 86	% 93 89 95 91 86	% 93 92 97 86 84	% 93 92 97 77 89	9% 88 90 97 81 91	86 81 97 76 89	% 85 75 95 71 91	% 85 85 95 71 87	% 83 84 97 74 86	% 82 86 95 76 85	% 82 91 95 83 82	% 82 88 97 83 88	% 83 91 97 83 85	% 82 91 95 88 83	% 82 92 95 84 78	% 80 94 94 83 76	% 80 93 95 85 76	% 86·9 87·8 94·7 86·0 86·1	mb. 6·7 7·5 7·9 7·7
6 7 8 9 10	79 90 94 91 90	74 90 94 90 87	77 92 93 94 86	81 92 93 94 83	82 93 91 91 84	81 93 90 93 84	84 93 88 94 79	83 93 91 92 83	86 94 96 91 89	88 94 97 89 81	87 94 95 84 86	90 91 93 83 85	90 92 93 78 77	90 88 93 79 77	89 89 93 80 76	91 90 90 78 78	91 84 88 80 80	93 86 87 85 80	93 85 87 84 82	90 85 85 87 84	90 86 85 88 86	90 92 85 88 84	87 96 88 90 84	89 93 91 92 82	86·2 90·5 90·9 87·3 83·0	7·8 8·1 8·1 7·1 6·7
11 12 13 14 15	80 86 91 85 97	78 81 86 85 95	78 80 89 86 97	75 76 89 86 95	75 76 86 87 96	79 78 87 86 95	74 76 90 86 93	76 76 88 87 88	74 75 76 85 88	71 75 66 81 86	72 74 63 76 86	68 75 57 77 79	81 75 55 81 82	84 80 53 86 80	80 78 57 85 83	81 79 57 86 76	84 85 59 92 79	80 87 68 93 81	80 87 70 93 82	82 91 78 94 82	83 91 80 97 82	80 90 82 97 84	82 90 85 99 86	84 91 85 97 86	78·3 81·2 75·0 87·5 86·8	6·5 6·9 7·1 7·1 7·1
16 17 18 19 20	89 95 99 90 87	89 96 97 93 89	89 96 95 93 89	90 96 93 91 92	90 98 93 88 92	90 98 93 93 90	89 96 92 96 95	88 96 90 94 89	87 94 88 93 87	85 94 87 91 85	83 91 83 97 87	83 89 83 95 89	83 93 82 94 93	87 92 82 96 92	87 93 81 94 93	87 93 82 92 90	87 92 84 92 89	87 93 87 90 89	86 96 92 94 89	87 99 92 92 87	90 90 90 90	94 100 92 89 91	97 99 92 88 88	95 97 88 87 91	88·1 95·2 89·2 92·2 89·7	7·5 7·8 7·5 7·0 7·7
21 22 23 24 25	91 96 81 90 85	94 98 85 90 88	94 100 89 92 90	91 99 88 92 90	95 99 84 91 90	95 98 80 91 89	97 98 77 91 89	98 98 80 92 82	100 100 84 94 80	97 100 84 95 73	93 98 83 96 75	90 82 82 87 67	92 73 80 83 68	90 86 74 83 70	91 86 77 84 75	90 83 77 83 77	93 86 80 83 81	95 87 83 87 85	95 87 90 83 86	96 91 87 79 81	97 90 88 86 89	97 91 87 88 72	96 92 87 87 77	98 91 88 85 74	94·2 92·2 83·2 88·1 80·8	7·8 7·5 7·4 7·9 7·7
26 27 28 29 30	72 99 93 97 94	76 100 94 97 94	76 100 93 97 94	82 100 93 99 94	85 100 94 99 95	84 100 94 99 97	83 100 93 99 97	80 100 94 99 97	77 100 99 100 96	67 100 93 99 99	76 100 93 89 95	65 100 92 86 97	73 100 92 89 97	76 93 93 85 96	77 87 96 82 96	80 86 93 81 97	84 88 92 81 97	84 90 94 82 97	84 89 94 84 97	86 90 97 84 96	90 92 96 91 97	89 92 97 94 97	92 92 97 99 99	94 93 96 97 98	80·1 95·5 94·2 92·0 96·4	8·0 9·9 9·8 9·7 8·6
31	99	98	99	100	98	100	100	100	100	100	100	99	98	97	97	99	95	92	94	94	88	88	88	87	96.5	8.3
		·								ļ	87.2	-	84.6		ļ				l				·	mb.	88·3	†7·8
Vapour Pressure*	mb.	mb.		mb. 7.4		7.3		1	1 .		mb. 8•1	mb. 8∙1	mb. 8•1	mb. 8•1		mb. 8·2			mb. 7·8		mb. 7°7		1			
46. Aberdee	n:	Nort	h W	all S	cree	n on	Tow	ver:	ht =	= 12	·5 m	etres.													Apri	il, 1923.
1 2 3 4 5	97 97 94 91 88	90 98 94 91 86	9/0 88 100 94 93 86	% 87 98 93 91 86	% 88 98 93 93 87	% 86 100 91 87 86	% 89 98 91 86 85	% 90 97 88 82 85	% 91 97 88 82 83	% 90 97 88 84 82	% 91 94 87 84 80	% 93 94 87 84 80	% 90 94 92 84 80	% 91 93 92 86 75	% 90 93 90 88 75	% 90 94 86 88 76	% 88 94 86 89 78	% 92 93 88 88 76	95 94 91 89 78	% 97 94 93 87 78	% 94 94 91 87 75	% 96 94 93 87 75	95 94 93 87 73	% 97 94 94 88 70	% 91·0 95·6 90·7 87·5 80·5	mb. 8·0 8·8 8·4 8·5 7·5
6 7 8 9 10	67 81 80 67 74	70 82 81 66 68	71 82 81 67 71	69 78 79 65 70	70 77 79 66 75	69 74 73 66 73	72 82 71 65 77	71 81 71 64 88	71 84 67 62 89	71 85 70 63 91	71 87 67 61 89	68 86 66 63 89	77 88 66 62 86	76 88 69 62 78	74 88 72 64 74	77 87 67 63 76	75 86 69 64 76	79 86 67 67 78	87 82 70 71 79	85 81 70 73 76	77 81 72 73 80	81 82 72 78 81	81 82 69 71 83	83 82 69 74 86	74·8 83·0 71·8 66·4 79·2	6·3 7·3 6·2 5·5 7·1
11 12 13 14 15	86 98 98 91 94	88 98 99 94 94	87 99 99 96 97	86 97 97 97 96	84 94 98 97 95	83 96 100 96 95	81 95 100 96 97	87 93 100 97 97	89 94 97 97 97	92 97 89 98 96	91 99 91 99 91	94 97 84 94 91	96 97 82 92 90	94 95 87 93 91	95 94 88 93 94	97 95 94 87 94	97 97 91 89 93	98 99 86 88 95	99 89 91 95	99 94 91 95	98 100 94 92 94	98 98 98 93 94	97 93 95 95	98 98 93 98 92	92·3 96·9 93·5 93·8 94·4	8·1 8·9 9·7 9·2 8·4
16 17 18 19 20	92 93 77 65 77	92 88 81 65 65	94 91 78 62 68	94 87 81 68 68	94 89 77 63 68	94 85 68 68 76	94 83 69 66 75	94 81 67 71 65	91 77 65 68 62	94 80 67 71 62	94 76 69 63 66	96 74 71 63 70	93 73 69 62 70	90 75 68 60 76	88 71 68 60 78	90 72 68 61 91	92 71 71 67 70	92 69 68 71 68	92 72 66 68 66	93 72 67 64 64	96 71 68 68 61	97 71 66 69 61	97 74 66 65 67	96 73 67 67 63	93·2 78·3 70·2 65·6 69·1	8·6 7·2 6·2 5·8 6·0
21 22 23 24 25	68 72 79 78 66	66 69 79 84 76	65 68 78 87 87	64 73 86 88 92	66 78 90 87 92	65 80 87 86 90	63 78 82 80 92	66 77 83 73 90	68 77 72 73 91	82 70 72 71 80	75 66 71 77 71	68 71 57 56 64	65 64 77 53 65	66 62 59 56 59	69 58 55 54 57	69 59 58 54 57	72 64 71 69 62	75 76 58 67 65	76 76 65 65 70	74 82 77 66 76	77 85 76 69 78	76 85 77 67 79	72 80 79 71 81	79 75 79 71 81	69·9 72·8 73·5 71·1 75·7	6·0 6·2 5·7 5·6 7·6
	77	83 63	83 66	87 68 87	86 69 87	87 71 87	85 73 80 75	74 64 76 66	74 58 67 61	71 56 72 59	75 56 69 53	76 49 68 53	81 52 71 57 92	81 51 71 64 92	86 50 72 67 90	81 51 71 72 92	87 69 73 67 94	89 71 78 72 94	87 84 76 66 97	81 82 88 84 97	79 81 91 73 83	78 83 94 78 74	68 85 92 81 75	74 84 91 82 75	80·6 66·6 79·8 71·9 88·1	7·6 5·7 6·9 7·1 8·9
26 27 28 29 30	67 85 93 82	86 85 71	86 79 79	76 83	81 87	77 91	93	93	96	94	94	93	<u> </u>													
27 28 29 30 Mean	85 93 82 82·3	85 71 81·7	79 79 82·7	76 83 83·o	87 83 · 6	91 82·9	93 82·4	81.0	79.6	79.8	78.6	76.6	77:3	76·7	76.5				81.2			82·6	82.0	82·4	80.6	†7:3
27 28 29 30	85 93 82	85 71 81·7 mb.	79 79 82·7 mb.	76 83 83·0 mb.	87 83·6 mb.	91 82·9 mb.	93 82·4 mb.	81.0	79·6 mb.	79·8 mb.	78·6 mb.	76·6	<u> </u>	76·7 mb.	76·5 mb.	mb.	79·0 mb. 7·4	mb.	mb.	82·7 mb. 7·3	81·9 mb. 7·2		82·0 mb.	82·4 mb.		

[•] Computed from the mean temperature and mean relative humidity.

[†] Mean of the column.

[§] Mean of the row.

47. Aberdeen: North Wall Screen on Tower: h_t (height of thermometer bulbs above the ground) = 12.5 metres. May, 1923.

710014661	1	1	i	1				1	1	1			Γ		I	1 1		ı	1	ı	1			l		I
Day.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
1 2 3 4 5	% 77 96 85 70 79	% 79 95 85 63 69	% 90 97 88 65 74	90 94 85 71 79	% 88 93 85 70 82	% 87 82 87 71 80	% 86 85 83 62 77	% 83 93 80 58 72	% 86 91 75 58 72	% 84 87 65 55 68	% 82 83 72 55 58	% 84 80 64 63 53	% 86 75 63 64 61	% 83 74 53 58 65	% 89 76 63 45 63	% 87 75 60 48 63	% 89 71 65 54 66	% 91 73 56 57 67	% 90 75 70 57 69	% 91 79 59 62 71	% 93 82 56 71 71	% 94 85 61 76 73	% 93 85 62 82 76	% 93 87 62 81 77	% 86·9 84·0 70·7 62·8 70·3	mb. 8·7 7·9 8·6 9·3 10·2
6 7 8 9 10	78 66 76 81 80	80 68 76 84 83	77 68 78 86 86 84	80 66 77 81 83	79 64 78 87 79	77 64 75 81 71	71 59 68 79 72	69 53 60 76 67	62 52 58 76 62	58 50 56 65 59	51 46 55 60 60	50 47 47 70 61	47 46 47 68 63	47 49 58 82 86	46 52 67 82 87	46 62 77 92 87	46 63 70 87 88	48 54 60 84 87	51 59 66 85 86	57 63 64 85 81	61 63 72 79 86	64 67 73 78 86	64 71 77 75 84	65 73 83 73 88	61·7 59·2 67·2 79·2 77·6	8·1 6·7 7·3 7·1 6·3
11 12 13 14 15	90 91 90 84 89	91 87 89 79 92	91 88 90 76 93	91 87 88 76 97	97 84 93 71 94	90 90 88 67 93	94 90 88 63 94	89 90 91 59 93	92 87 81 59 90	97 82 91 58 92	97 80 82 57 88	93 79 75 66 80	92 80 80 74 82	91 81 73 78 77	93 78 81 77 79	91 84 76 85 79	94 82 71 79 77	94 81 77 83 88	98 80 80 85 90	93 81 83 86 89	97 81 84 85 93	91 87 87 90 91	87 90 90 91 93	88 90 90 93 94	92·5 84·5 84·1 75·8 88·6	6·8 6·9 7·6 7·0 8·2
15 17 18 19 20	92 75 83 86 93	90 83 84 86 93	90 80 84 82 90	95 79 84 83 89	92 87 86 85 92	92 81 82 83 88	86 82 78 72 87	87 81 72 67 86	85 97 66 64 85	89 96 66 61 85	92 100 64 60 86	88 94 68 62 87	81 90 76 69 91	62 90 79 62 88	62 90 82 80 86	63 87 85 82 84	71 89 82 78 77	84 82 85 84 76	89 81 82 85 63	89 82 89 82 66	84 84 87 88 74	78 84 90 88 77	73 84 87 92 68	73 86 89 92 71	83·2 85·7 80·4 78·0 83·0	7·0 7·3 7·3 9·0 9·7
21 22 23 24 25	76 84 84 73 76	74 84 84 74 78	77 87 82 73 77	76 82 85 77 76	73 78 82 73 79	69 73 76 68 80	68 66 76 62 81	69 65 77 60 86	68 64 86 59 86	72 64 78 57 79	72 56 66 57 83	70 57 56 59 90	59 55 52 64 89	58 56 54 62 88	55 55 57 61 94	65 57 60 63 97	59 56 61 65 93	57 60 56 70 92	68 60 58 71 92	73 67 68 77 96	76 73 78 80 94	79 74 76 67 99	79 80 73 74 97	83 84 71 74 95	69·5 68·2 70·9 67·4 86·9	7·6 6·3 6·6 7·4 8·2
26 27 28 29 30	93 95 72 82 86	93 93 73 85 86	93 90 73 87 86	93 94 75 82 93	91 93 70 80 92	94 91 69 77 92	96 88 72 77 85	93 90 71 80 85	83 92 73 79 89	86 91 68 72 83	88 93 68 65 85	86 88 71 68 80	90 92 72 69 87	85 86 70 68 85	90 83 72 72 90	96 74 72 68 88	94 74 70 68 90	94 73 71 72 90	93 77 75 75 84	94 80 77 77 77	95 84 77 82 86	94 81 83 85 90	96 76 82 85 93	95 76 82 86 92	91·9 86·0 73·1 76·6 87·1	9·0 9·2 7·4 8·1 8·7
31	83	77	90	94	91	86	84	83	88	83	88	90	87	88	88	90	88	87	77	90	93	89	92	94	87.9	9.3
	1			00 0	83.5	80.8	78.4	76.9	76.3	74· I	72.5	71.8	72.6	72 · 1	74.0	75.6	74.7	75.3	76·8 ——	78.3	8 o ·9	81.8	82 · 3	83.2	78 · 1	†7·9 ————
	82.7	82.5	83.4	83.8									•		ı	1 3						1				
	mb.	mb.		mb.	mb.	mb.	mb.	mb. 7·9			mb. 8•1	mb. 8•1		mb. 8·2			mb. 8•4	mb. 8·2	mb. 8·1		mb. 7•9	mb. 7·8	mb. 7·6	1	mb. §7·9	
Mean	mb.	mb. 7·3	mb.	mb.	mb. 7°4	mb. 7·6	mb. 7·8	7.9	7.9	8.0	8·1	8·1 etres.				8.5	8.4			8.0	7.9	7.8	7.6	7:5	§7·9 Jun	e, 1923.
Mean Vapour Pressure*	mb.	mb. 7·3	mb.	mb.	mb. 7·4	mb. 7·6	mb. 7·8	7.9	7.9	8.0	8·1	8.1												1	§7·9	mb. 10:4 9:9 9:7 7:7 8:9
Vapour Pressure* 48. Aberdeel	mb. 7 · 4 n :] % 94 78 79 87	mb. 7·3 Nort	mb. 7·3 h W 93 79 85 86	mb. 7·4 all S 93 81 86 83	mb. 7·4 creei	mb. 7.6 n on 86 79 82 75	mb. 7·8 Tow % 91 77 80 71	7·9 ver: % 90 73 80 76	$h_t = \frac{\%}{81}$ $\frac{74}{86}$ $\frac{86}{72}$	8·0 = 12 % 80 72 75 71	8·1 ·5 m % 81 76 76 76	8·1 etres. % 83 70 87 67	8·2 % 82 67 88 66	% 80 71 74 67	% 81 69 86 68	% 83 58 80 70	% 76 52 80 67	% 79 76 90 70	% 83 84 90	% 85 72 87	7·9 % 87 73 86 76	7·8 % 87 76 86 87	7·6 % 86 80 84 87	7.5 % 84 82 88 89	\$7.9 Jun % 85.5 74.3 83.3 75.4	mb. 10·4 9·9 9·7 7·7
Vapour Pressure* 48. Aberdeel I 2 3 4 5 5 6 6 7 8 8 9	mb. 7·4 n: 1 % 94 78 79 87 76 86 76 69	mb. 7·3 Nort % 91 78 82 85 89 76 86 78 66	mb. 7·3 h W % 93 79 85 86 86 81 83 77 67	mb. 7·4 all S % 93 81 86 83 80 84 83 71	mb. 7·4 Creei % 90 84 85 76 81 79 81 87 72	mb. 7·6 n on % 86 79 82 75 79 76 75 80 61	mb. 7·8 Tow % 91 77 80 71 95 73 73 77 56	7·9 ver: % 90 73 80 76 86 68 73 81 55	$ \begin{array}{r} 7.9 \\ \hline h_t = \\ \% \\ 81 \\ 74 \\ 86 \\ 72 \\ 79 \\ \hline 66 \\ 73 \\ 79 \\ 52 \\ \end{array} $	8·0 = 12 % 80 72 75 71 76 61 66 81 51	8·I -5 m -6 -76 -76 -66 -65 -81 -47	8·1 etres. % 83 70 87 67 75 63 68 74 50	8·2 % 82 67 88 66 77 58 72 76 51	% 80 71 74 67 83 59 65 75 51	8·4 % 81 69 86 68 78 59 .55 74 54	% 83 58 80 70 80 58 47 74 58	8·4 % 76 52 80 67 82 72 48 51 66	% 79 76 90 70 68 72 51 50 67	% 83 84 90 62 71 57 59 71	% 85 72 87 75 63 73 62 57 80	7·9 % 87 73 86 76 74 76 65 63 86	7·8 % 87 76 86 87 71 75 70 66 93	7·6 % 86 80 84 87 76 81 71 69 92	7.5 % 84 82 88 89 79 85 73 68 95	\$7.9 Jun % 5.5 74.3 83.3 75.4 78.6 71.0 68.9 72.4 65.3	mb. 10·4 9·9 9·7 7·7 8·9 7·3 10·1 10·6 10·1
Mean Vapour Pressure* 48. Aberdeel 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14	mb. 7·4 n:] % 94 78 79 87 76 86 76 69 92 62 77 80 65	mb. 7·3 Nort % 91 78 82 85 89 76 86 78 66 75 64 76 79 73	mb. 7·3 h W 93 79 85 86 86 81 83 77 67 72 64 77 73 75	mb. 7·4 all S 93 81 86 83 80 84 87 74 68 76	mb. 7·4 Creel % 90 84 85 76 81 79 81 87 72 74 76 72 66 74	mb. 7·6 1 on % 86 79 82 75 79 76 75 80 61 71 86 67 62 74	mb. 7·8 Tow % 91 77 80 71 95 73 73 77 56 64 83 70 62 71	7·9 ver: % 90 73 80 76 86 68 73 81 55 61 72 76 60 80	$\begin{array}{c} 7.9 \\ h_t = \\ \% \\ 81 \\ 74 \\ 86 \\ 72 \\ 79 \\ 66 \\ 73 \\ 79 \\ 52 \\ 63 \\ 68 \\ 79 \\ 62 \\ 81 \end{array}$	8·o 8·o 72 75 71 76 61 66 81 51 59 62 86 59 63	8·1 ·5 m % 81 76 76 66 65 81 47 57 64 85 58 56	8·1 etres. % 83 70 87 67 75 63 68 74 55 54 88 59 56	8·2 8/0 8/2 67 88 66 77 58 72 76 51 51 55 83 61	8·2 % 80 71 74 67 83 59 65 75 51 49 58 73 66 56	% 81 69 86 68 78 59 55 74 53 59 74 64	% 83 58 80 70 80 58 47 74 58 54	8·4 % 76 52 80 67 82 72 48 51 66 69 80	8·2 % 79 76 90 70 68 72 51 50 67 67 55 69	8·1 % 83 84 90 70 62 71 61 69 62 72 56	8.0 % 85 72 87 75 63 73 62 57 80 60 66 67 68 59	7·9 % 87 73 86 76 74 76 65 63 66 71 70 63	7·8 % 87 76 86 87 71 75 70 66 93 68 74 75 73 68	7.6 % 86 80 84 87 76 81 71 69 92 70 73 80 69 69	7.5 9% 84 82 88 89 79 85 66 73 68 95 66 75 77	\$7.9 Jun %5.5 74.3 83.3 75.4 78.6 71.0 68.9 72.4 65.3 63.9 67.9 74.6 67.2 64.7	mb. 10·4 9·9 9·7 7·7 8·9 7·3 10·1 10·6 10·1 9·6 8·2 10·6 9·5 6·9
Mean Vapour Pressure* 48. Aberdeel 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 15 16 17 18 19	mb. 7·4 n: 1 % 94 78 87 87 76 86 76 69 92 62 77 80 65 71 87 93 87 80	mb. 7·3 Nort % 91 78 82 85 89 76 86 75 64 76 79 73 76 88 90 88 77	mb. 7·3 h W 93 79 85 86 86 81 83 77 67 72 64 77 73 75 77	mb. 7·4 all S 93 81 86 83 80 84 84 67 74 66 76 98 88 90 71	mb. 7·4 Creei % 90 84 85 76 81 79 81 87 72 74 76 72 66 74 77 84 90 87 61	mb. 7·6 n on % 86 79 76 75 80 61 71 86 67 62 74 73 81 87 82 59	mb. 7·8 Tow 91 77 88 71 95 73 77 56 64 83 70 62 71 66 80 59	7·9 ver: % 90 73 80 76 86 68 73 81 72 76 60 80 60 71 68 76 68 76 58	7·9 ht = % 81 74 86 72 79 66 73 79 52 63 68 79 62 68 66 68 67 73 75 75	8·o 8·o 12 % 80 72 75 71 76 61 66 81 51 59 62 86 59 63 62 70 68 68 57	8·1 ·5 m % 81 76 76 76 66 65 81 47 57 64 85 56 68 66 65 69 58	8·1 etres. % 83 70 87 67 75 63 68 74 50 55 54 88 59 66 67 59 64 69 55	8·2 9% 82 67 88 66 77 58 72 76 51 55 83 61 55 68 66 69 66 66 67 66 67 67 68	8·2 % 80 71 74 67 83 59 65 75 51 49 58 73 66 67 53 70 66 63	8·4 % 81 69 86 68 78 59 74 53 59 74 64 68 68 68 68	8·5 % 83 58 80 70 80 58 47 74 58 54 77 66 63 54 77 73 69 64	8·4 % 76 75 52 80 67 82 72 48 51 66 69 80 74 77 60 74 72 64	8·2 % 79 76 90 70 68 72 51 50 67 67 55 69 67 79 58 78 73 69	8·1 % 83 84 90 70 62 71 57 59 61 62 72 72 72 76 84 65 77 81	% 85 72 87 75 63 73 62 57 86 66 66 67 79 79 73 86	7·9 % 87 73 86 76 74 76 65 63 86 77 70 63 75 81 78 84	7·8 9% 87 76 86 87 71 75 70 66 93 68 74 75 73 80 84 82 81	7.6 %6 86 80 84 87 76 81 71 69 92 70 73 80 69 81 85 87 79 80	7.5 %4 84 82 88 89 79 85 73 68 95 66 75 82 65 71 83 90 84 88 88 88 88 88 88 88 89 85 86 86 87 87 88 88 88 88 88 88 88 88	\$7.9 Jun %5.5 74.3 83.3 75.4 78.6 71.0 68.9 72.4 65.3 63.9 67.9 74.6 67.2 64.7 72.8 72.4 77.8 68.9	mb. 10·4 9·9 9·7 7·7 8·9 7·3 10·1 10·6 10·1 9·6 8·2 10·6 9·5 6·9 7·4 7·6 8·5 11·6 9·2
Mean Vapour Pressure* 48. Aberdeel 1 2 3 4 5 5 6 7 8 9 10 10 11 12 13 14 15 15 16 17 18 19 20 20 21 22 23 24	mb. 7·4 7·4 7·4 7·4 7·6 87 92 62 77 80 65 71 87 93 87 87 93 87 67	mb. 7·3 Nort % 91 78 82 85 89 76 86 77 79 73 76 88 90 88 87 85 80 79 70 68	mb. 7·3 h W 93 79 85 86 86 81 83 77 72 64 77 73 75 77 90 87 88 87 87 87 87 87 86 87 87 87 86 87	mb. 7·4 all S % 93 81 86 83 80 84 83 71 74 68 71 66 76 79 88 85 90 71 84 82 72 72	mb. 7·4 Creei % 90 84 85,76 81 79 87 72 74 76 72 66 74 77 84 90 87 75 76 97 75	mb. 7·6 n on % 86 79 82 75 79 76 67 62 74 73 81 87 82 59 76 71 75 64 89	mb. 7·8 Tow 91 77 80 91 77 80 71 95 73 73 77 756 64 83 70 62 71 66 80 77 80 77 80 77 80 87 87	7·9 ver: % 90 73 80 76 86 68 73 81 72 76 60 80 60 71 68 76 63 67 77 77	7·9 ht = % 81 74 86 72 79 66 73 79 52 63 68 79 62 81 66 68 66 73 71 61 59 58 66	8·o = 122 % 80 72 75 71 76 61 66 81 51 59 62 86 88 68 67 75 60 60 60 59 71	8·1 ·5 m % 81 76 76 66 65 81 47 57 64 85 58 66 65 69 58 66 65 69 78	8·1 etres. % 83 70 87 67 75 63 68 74 50 55 54 88 59 64 69 55 62 51 58 57 89	8·2 9% 82 67 88 66 77 58 76 51 55 68 56 69 66 67 57 57 59 88	8·2 % 80 71 74 67 83 59 65 75 51 49 58 73 66 67 53 70 66 63 59 49 61 53 90	8·4 %6 81 69 86 68 78 59 74 54 53 59 74 64 52 68 55 68 66 68 59 53 63 63 63 63 63 63	8·5 % 83 58 80 70 80 58 47 74 58 54 77 66 63 54 77 73 64 58 58 58 58 58 58 58 58 58 58	8·4 % 76 52 80 67 82 72 48 51 66 69 80 74 72 64 62 57 65 54 86	% 79 76 76 70 68 72 51 50 67 67 55 79 68 66 67 68 78 86	8·1 % 83 84 90 70 62 71 57 59 71 61 62 72 58 84 65 77 81 73 68 63 69 69 69 68 88 88 88 88 88 88 88 88 88	8·0 % 85 72 87 75 63 73 62 57 80 60 66 67 68 79 69 79 69 69 75 67 69 61 73	7·9 % 87 73 86 76 74 76 65 63 86 63 75 81 81 70 69 77 70 63 77	7·8 9% 87 76 86 87 71 75 70 66 93 68 74 75 73 80 84 81 77 71 63 80	7.6 %6 86 86 80 84 87 76 81 71 69 92 70 73 80 69 81 85 87 79 80 75 75 77 87 87 77 87 87 87 87 87 87	7.5 %6 84 82 88 89 79 85 73 66 65 71 83 90 84 80 81 75 76	\$7.9 Jun \$5.5 74.3 83.3 75.4 78.6 71.0 68.9 72.4 65.3 67.9 74.6 67.2 64.7 72.8 72.4 77.8 76.8 76.8 68.6 61.8 78.8	mb. 10·4 9·9 9·7 7·7 8·9 7·3 10·1 10·6 10·1 9·6 8·2 10·6 9·5 6·9 7·4 7·6 8·5 11·6 9·2 9·0 10·7 12·8 9·6
Mean Vapour Pressure* 48. Aberdee 1 2 3 4 5 5 6 7 8 9 10 10 11 12 13 14 15 15 16 17 18 19 20 20 21 22 23 24 25 26 27 28 29 30	mb. 7·4 7·4 94 78 87 86 76 69 92 62 77 80 65 71 87 93 87 88 81 71 76 77 88 86 65 83 73 88	mb. 7·3 Nort %91 78 82 85 89 76 86 78 66 75 64 76 79 73 76 88 90 88 87 85 80 79 70 68 74 89 66 84 75 90	mb. 7·3 h W 93 79 85 86 86 87 77 72 64 77 73 75 77 90 87 88 87 74 69 74 88 65 79 90	mb. 7·4 all S % 93 81 86 83 80 84 83 83 71 66 76 79 88 85 90 71 84 84 82 72 80 87 65 86 84 91	mb. 7·4 Creel % 90 84 85 76 81 79 81 87 72 74 76 72 66 74 77 77 84 90 87 61 78 75 79 83 67 79 83 67 86 93	mb. 7·6 1 on % 86 79 82 75 79 76 62 74 73 81 87 82 59 76 71 75 64 89 81 78 82 90 83	mb. 7·8 Tow % 91 77 80 71 95 73 73 77 56 64 83 70 62 71 66 80 77 80 79 79 79 100 75	7·9 ver: % 90 73 80 76 86 68 73 81 555 61 72 76 60 80 60 71 68 76 75 81 66 59 88 90 68	7·9 ht = % 81 74 86 72 79 66 73 79 52 63 68 79 62 81 66 67 71 61 59 58 66 71 66 66 71 84 70	8·o 8·o 12 % 80 72 75 71 76 61 66 81 51 59 62 86 68 57 75 60 660 59 71 67 67 67 67 67 67 67	8·1 ·5 m % 81 76 76 66 65 81 47 57 64 85 56 68 66 65 58 66 65 78 65 42 64 59 88 76	8·1 etres. % 83 70 87 67 75 63 68 74 50 55 54 88 59 66 67 59 64 69 55 62 51 58 57 89 63 47 63 57 91	8·2 %2 67 88 66 77 58 72 76 51 55 68 56 69 66 67 57 57 59 88 88 88 68 69 66 67 57 57 59 88 88 88 88 88 88 88 88 88 8	8·2 % 80 71 74 67 83 59 65 75 51 49 58 73 66 63 59 49 61 53 79 65 74 65	8·4 % 69 86 68 78 59 555 74 54 54 52 68 66 80 59 53 63 557 47 74 69 66 75	8·5 % 83 58 80 70 80 58 47 77 66 63 54 77 73 69 64 58 55 62 55 62 58 89 59 49 49 49 49 49 49 49 49 49 4	8·4 % 76 76 52 80 67 82 72 48 51 66 69 80 53 78 60 74 72 645 57 65 54 88 88	8·2 % 79 76 90 70 68 72 51 50 67 67 55 79 58 78 73 69 65 61 69 67 67 86 70 49 71 64 87 85	8·1 % 83 84 90 70 62 71 57 59 71 66 66 77 81 73 76 80 71 54 77 81	8·0 % 57 87 77 75 63 73 62 79 79 79 79 73 86 75 67 69 79 73 86 75 67 69 79 73 73 73	7·99 %87 73 86 76 76 65 63 69 71 70 63 75 81 81 77 75 63 77 75 81	7·8 % 87 76 86 87 77 86 87 77 80 84 82 81 77 71 71 75 85 85	7.6 %6 86 80 84 87 76 81 71 69 92 70 73 80 69 69 81 85 87 79 80 75 74 72 68 79 80 65 75 76 80 80 80 80 80 80 80 80 80 80	7.5 9% 84 84 88 89 79 85 73 66 67 78 78 76 77 78 78 78 78 78 78 78 78	\$7.9 Jun %5.5 74.3 83.3 75.4 78.6 71.0 68.9 72.4 65.3 63.9 67.6 67.2 64.7 72.8 72.4 76.8 68.9 71.3 65.1 68.6 61.8 78.8 71.6 63.7 68.6 63.7 68.6 72.9 79.8	mb. 10·4 9·9 9·7 7·7 8·9 7·3 10·1 10·6 10·1 9·6 8·2 10·6 9·5 6·9 7·4 7·6 8·5 11·6 9·2 9·0 10·7 12·0 12·8 9·6 8·5
Mean Vapour Pressure* 48. Aberdee 1 2 3 4 5 5 6 7 8 9 10 10 11 12 13 14 15 15 16 17 18 19 20 20 21 22 23 24 25 26 27 28 29 30	mb. 7·4 7·4 94 78 87 86 76 69 92 62 77 80 65 71 87 93 87 88 81 71 76 77 88 86 65 83 73 88	mb. 7·3 Nort %91 7882 85 89 76 866 75 64 76 79 73 76 88 90 88 77 85 80 79 70 68 84 75 90 79 79 70 79 70 79 70 70 70 70 70 70 70 70 70 70 70 70 70	mb. 7·3 h W 93 79 85 86 81 83 77 67 72 64 77 73 75 77 90 87 88 71 85 83 77 74 69 74 88 65 85 79 90 79·3 mb.	mb. 7·4 all S % 93 81 86 83 80 84 83 87 74 68 71 66 76 79 88 85 90 71 84 82 72 72 80 87 65 86 84 91 mb.	mb. 7·4 Creel % 90 84 85 76 81 79 81 87 72 74 76 72 66 74 77 77 84 90 87 61 78 75 79 83 67 78 93 88 78 99 mb.	mb. 7·6 n on %86 79 82 75 79 76 75 80 61 71 86 67 74 73 81 82 59 76 71 75 64 89 81 78 76 76 82 90 83 76·4 mb.	mb. 7·8 Tow % 91 77 88 80 71 95 73 77 56 64 83 70 62 71 66 80 77 80 87 79 79 100 75 74·2 mb.	7·9 Ver: 9% 90 73 80 76 86 68 73 81 5561 72 76 60 60 71 68 76 87 67 77 75 81 66 59 68 71 66 59 68 71 66 71 66 71 66 71 66 71 66 71 67 75 81 66 67 71 66 68 71 66 69 68 71 66 69 68 71 66 69 68 71 66 69 68 71 66 69 68 71 66 69 68 71 66 69 68 71 66 69 68 71 66 69 68 71 66 69 68 71 66 69 68 71 66 69 68 71 66 69 68 71 68 69 68 71 60 68 71 60 68 71 60 68 68 71 60 68 68 71 60 68 68 71 60 68 68 71 60 68 68 71 60 68 68 71 60 68 68 71 60 68 68 71 60 68 68 71 60 68 68 71 60 68 68 71 60 68 68 71 60 68 68 71 60 68 68 69 68 68 71 60 68 68 71 60 68 68 68 69 68 68 69 68 68 69 68 68 68 69 68 68 68 69 68 68 68 69 68 68 68 69 68 68 68 68 68 68 68 69 68 68 68 68 68 68 68 68 68 68 68 68 68	7·9 ht = % 81 74 86 72 79 66 73 79 62 81 66 68 73 57 71 61 59 58 66 71 66 66 71 84 70 69 69 mb.	8·o 8·o	8·1 ·5 m % 1 76 76 66 65 81 47 57 64 85 58 65 68 65 69 58 65 53 59 60 78 66 42 66 42 66 66 66 78 66 66 78 76 66 78 76 66 78 76 76	8·I etres. % 83 70 87 67 75 63 68 74 50 55 54 88 59 66 67 59 64 69 55 62 51 58 57 89 63 47 63 57 67 65 65 mb.	8·2 % 82 67 88 66 77 58 72 76 51 55 68 56 69 66 67 57 57 59 88 88 45 63 55 88 45 63 63 63 64 65 66 67 67 67 67 67 67 67 67 67	8·2 % 80 71 74 67 83 59 65 75 51 49 58 73 66 63 59 49 61 53 90 57 48 77 65 64·8 mb.	8·4 % 69 86 68 78 59 555 74 54 54 52 68 66 80 59 53 63 557 47 74 69 66 75	% 83 58 80 70 80 58 47 74 58 54 77 66 63 54 77 73 66 64 58 55 80 60 47 78 66 63 58 66 47 78 66 64 64 64 66 66 66 66 66 66 66 66 66	8·4 % 76 76 52 80 67 82 72 48 51 66 69 80 75 74 72 64 62 57 65 54 88 67 0 mb.	8·2 % 79 76 90 70 68 72 51 50 67 67 55 79 58 78 73 69 65 61 69 57 86 70 49 71 64 87 85 68 68 68 68 68	8·1 % 83 84 90 70 62 71 57 59 61 66 69 62 72 72 73 68 63 69 58 80 71 54 72 73 77 81 70·4 mb.	8.0 % 85 72 87 75 63 73 62 57 86 66 67 69 69 79 73 86 75 69 61 73 73 62 72 86 75 69 60 75 60 60 75 60 60 75 60 60 60 75 60 60 75 60 60 60 75 60 60 75 60 60 60 75 60 60 75 60 60 75 60 60 75 60 60 75 60 60 75 60 60 75 60 60 75 60 60 75 60 60 75 60 60 75 60 60 75 60 60 75 60 60 75 60 60 75 75 60 60 75 60 75 75 75 75 75 75 75 75 75 75	7·99 % 87 73 86 76 76 65 63 76 77 75 63 77 75 63 77 mb.	7.8 %6 87 76 86 87 71 75 70 66 93 68 77 71 71 63 80 77 77 71 75 85 76 76 77 77 77 77 77 77 77 77	7.6 %6 86 86 88 87 76 81 71 69 92 70 73 80 69 81 85 79 80 75 74 72 68 75 76 88 77 77 77 77 77 77 77 77 77	7.5 % 84 82 88 89 79 85 73 66 75 82 65 77 83 68 80 81 75 76 71 63 76 83 65 83 65 75 82 75 76 77 78 78 78 78 78 78 78 78 78	\$7.9 Jun %5.5 74.3 83.3 75.4 78.6 71.0 68.9 72.4 65.3 63.9 67.9 74.6 67.2 64.7 72.8 72.4 77.8 68.6 61.8 78.8 71.6 63.7 68.6 63.7 68.6 72.9 79.8	mb. 10:4 9:9 9:7 7:7 8:9 7:3 10:6 10:1 9:6 8:2 10:6 9:5 6:9 7:4 7:6 8:5 11:6 9:2 9:0 10:7 12:0 12:8 9:6 8:5

^{*} Computed from the mean temperature and mean relative humidity.

49. Aberdeen: North Wall Screen on Tower: h_t (height of thermometer bulbs above the ground) = $12 \cdot 5$ metres.

July, 1923.

49. Aberdeen		101 (1	IVVa	III SC	16611	011	IUW	er .	117 (1.	reigi	11 01	them		rer r	Juins	abo	VC U	IC 81	Oum	1) —	14	0 111		•	oui	y, 1920.
Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
1 2 3 4 5	% 91 87 86 66 77	% 91 88 88 68 75	% 93 91 87 73 72	% 93 92 87 76 76	% 91 91 86 67 73	% 91 91 87 62 70	% 87 82 85 70 71	% 86 78 83 72 66	% 79 77 77 63 65	% 79 73 77 65 63	% 78 66 78 60 67	% 74 61 77 69 66	% 87 59 72 63 66	% 85 68 49 64 72	% 88 74 46 60 71	% 92 69 45 70 67	% 91 74 44 69 67	% 90 72 43 70 69	% 89 77 47 70 74	% 86 77 70 77 80	% 85 79 74 79 80	% 84 83 65 79 87	% 85 82 66 73 87	% 88 85 66 75 91	% 86·9 78·2 70·6 69·0 72·7	mb. 11·2 12·9 12·7 11·8 13·1
6 7 8 9 10	91 85 94 96 93	90 87 96 94 92	91 90 94 92 95	90 90 96 95 95	89 88 96 88 95	86 87 95 89 90	86 83 95 84 88	80 82 97 79 87	77 79 96 79 84	75 80 98 79 87	75 82 99 73 89	71 78 96 70 96	71 82 89 69 93	78 80 89 67 93	81 77 90 73 96	82 81 88 72 92	78 79 79 71 85	76 87 78 76 86	80 83 80 83 93	80 93 89 81 94	82 95 90 88 95	82 95 94 90 97	85 93 94 93 96	82 94 94 90 99	81·8 85·2 91·9 82·2 91·9	13·5 14·0 16·1 14·2 15·0
11 12 13 14 15	93 79 92 88	99 92 85 90 88	92 86 91 90	99 95 86 94 90	99 94 86 90 91	96 87 82 92 88	98 80 79 86 87	96 64 78 87 86	94 60 74 84 84	92 66 73 79 86	91 65 72 79 84	89 63 74 79 85	82 59 75 75 83	85 53 81 71 80	90 51 85 71 78	89 64 84 72 76	86 71 84 71 78	87 75 84 74 85	90 75 86 75 83	91 80 88 79 84	92 82 86 82 87	95 78 87 83 90	94 78 89 84 90	94 81 92 85 92	92·9 75·2 82·1 82·0 85·4	15·3 15·5 13·3 13·1 14·8
16 17 18 19 20	91 78 72 86 85	92 81 69 87 84	93 76 68 82 79	92 78 69 86 80	91 81 76 79 79	89 73 65 77 76	86 72 69 79 73	79 69 67 78 56	75 65 65 84 55	73 60 62 82 53	81 60 60 86 50	78 55 56 79 50	80 55 70 84 46	85 55 69 82 44	86 49 79 78 49	83 53 85 75 47	80 53 80 79 52	52 48 82 57 58	57 54 82 55 62	65 61 88 61 72	69 61 90 66 78	70 64 90 75 82	71 67 91 77 84	76 69 92 81 83	79·3 64·2 74·4 77·5 65·7	13·8 10·5 11·0 12·5 12·6
21 22 23 24 25	82 76 87 80 84	79 79 91 83 86	79 88 92 81 85	81 89 90 77 84	73 89 77 78 85	64 88 78 79 83	62 87 63 77 80	55 89 59 71 74	53 90 54 71 77	57 85 53 67 71	51 79 54 64 70	53 60 63 61 60	54 53 59 69 59	55 57 62 69 59	57 65 55 64 57	59 68 61 67 48	65 67 72 71 54	66 74 69 76 55	68 78 82 83 54	70 73 81 84 53	72 76 80 83 63	70 73 78 82 63	70 80 77 84 64	76 79 77 85 67	65·6 76·7 71·5 75·1 68·5	12·3 14·9 12·6 11·0
26 27 28 29 30	72 79 84 85 97	75 82 85 85 97	68 81 85 86 97	69 81 85 84 97	71 82 88 84 97	69 82 90 78 97	63 72 91 77 97	62 64 91 79 94	62 64 91 82 87	63 63 92 82 84	62 62 93 87 81	67 62 90 85 83	83 69 89 86 86	85 72 85 88 88	83 74 85 92 87	76 77 87 97 82	62 75 86 98 81	64 77 86 95 89	63 78 87 92 92	72 79 88 96 89	69 83 87 100 93	73 82 84 99 95	77 83 85 98 96	84 84 85 97 97	70·2 75·3 87·4 88·6 90·9	9·7 10·2 11·3 12·9
31	99	99	99	97	100	99	100	100	97	98	90	91	91	89	90	95	90	90	95	92	85	88	88	88	93· 9	13.1
Mean	85.6	86.4	86.3	86 · 9	85.6	83.2	8 o ·9	77.7	75.6	74 · 7	7 3 · 8	72.3	72.8	72.8	73.6	74.3	73.9	73.9	76.4	79 · 8	81 · 6	82.5	83.3	84 · 8	79· I	†12.8
Vapour Pressure*	mb. 12•4	mb. 12·3	mb.	mb. 12·1	mb. 12•4	mb. 12•4	mb. 12·6	mb. 12·8	mb. 12·9	mb. 13·0	mb.	mb. 13·2	mb. 13·3	mb.	mb.	mb. 13·3	mb.	mb.	m b.	mb. 12·9	mb. 12·9	mb.	mb.	mb.	mb. §12·8	
50. Aberdee	n:	Nort	h W	all S	creei	n on	Tow	ver:	h <i>t</i> =	= 12	·5 n	netres.			<u> </u>					i				<u> </u>	Augus	t, 1923.
I	% 88	% 91	% 91	% 87	% 87	% 84	% 80	% 83	%	% 73	% 70	% 68	% 70	% 80	% 92	% 89	% 85	%	% 82	% 87	% 88	% 89	% 88	% 82	% 82·8	mb.
2	78 94	85 95	91 94	84 89	91 86	81 84	78 79	79 74	73 84 73	77 75	78 74	80 69	84 70	88 67	84 64	87 65	90 68	77 88 71	85 65	94 68	91 73	90 68	90 70	92 69	85·2 75·6	11.8
4 5	70 87	71 87	73 84	72 86	73 89	70 88	63 88	62 83	73 58 82	59 74	57 82	55 80	56 75	55 73	54 78	55 72	60 77	57 82	76 81	79 85	83 91	83	81	84	66·6 83·0	10·6 12·7
6	90	89	89	89	90	88	84	79	77	72	62	54	60	56	69	72	71	72	69	76	81	86	87	88	77·I	1
7 8	89 89	90 88	91 87	95 89	94 88	97 87	97 82	98 79	96 79	95 83	95 80	94 77	78 78	77 80	74 83	89 84	90 84	86 86	93 89	93 89	95 92	94 93	88 95	92 94	90·7 85·6	13·7 15·4 13·0
10 9	95 76	94 73	91 75	93 74	94 72	91 75	89 69	87 62	77 57	74 56	58 55	57 52	53 53	67 50	79 47	76 54	72 53	59 57	58 61	60 6 5	67 64	69 65	73 66	74 66	75·7 62·5	14·6 10·8
11 12 13 14	67 87 85 72 76	69 88 84 77 75	74 88 83 79 78	70 88 85 79 80	69 87 85 78 82	65 86 85 69 76	64 84 85 68 70	64 78 86 65 64	62 74 93 61 61	59 71 89 57 57	58 62 88 55 57	54 63 78 59	51 64 70 61 57	55 62 76 67 72	54 66 47 68 67	58 66 45 65 63	59 76 45 75 72	70 76 49 77 75	81 78 55 81 73	79 84 61 82 72	78 84 70 87 75	84 85 65 76 75	87 84 65 72 76	84 84 71 71 77	66·9 77·7 73·0 70·9 70·3	11·2 12·6 14·1 11·6
16	77 90	80	77	78	82	76	74	69 96	66	60	59	57 88	59 81	67 78	63 88	75 89	78	92	89	89	90	92	91	92	76·o	11.0
17 18 19	90 92 90	91 91	93 91 91	92 91 92	93 93 92	92 92 91	96 89 88	89 89	96 90 83	93 92 75	93 88 79	85	85	80	81 75	84 75	90 85 78	93 85 77	93 82 78	93 84 79	95 83 85	91 87 84	91 87 86	92 88 86	87·3 82·9	13·0 12·3 11·3
20	90	91	91	90	9 1	92	92	90	83 88	75 84	86	74 88	75 88	75 87	91	91	91	92	95	95	95	96	96	98	90.9	12.6
21 22	98 78 58	96 78	99 78 64	98 79	98 81	98 76	95 72	95 70 58	92 58	86 54	82 49	85 50	82 49	78 55 58	61 54	58 54 62	60 52	59 59 68	58 61	55 62	59 66	66 69	66 61	75 65	79·6 64·0	9·3
23 24 25	58 93 83	64 95 86	64 95 89	69 95 85	67 93 86	65 93 85	57 96 78	58 96 81	56 95 68	52 96 66	51 91	51 89	52 93 63	58 90 67	61 86 71	82	52 65 85	84	71 82	85 82	92 86	91 78	95 79	93 82	66·3 89·2	10·1 6·3
25 26	96		92	90	86	82	82	84	78	71	67 72	67 69	75	86	78	77	83 67	90 76	94 74	94 80	94 87	97 87	95 87	93	81.4	12.2
27 28	84 85	93 86 85	88 87	88 88	91 84	84 86	82 86	77 76	73 76	71 74	69 72	69 84	64 75	61 85	69 79	77 72	69 68	78 74	76	80	84	82	8 ₅ 7 ₅	85 72	78·0 78·7	11.3
29 30	76 93	82 95	8r 95	86 93	82 96	75 95	73 96	72 96	67 94	65 93	66 93	69 94	77 96	78 93	73 95	79 97	79 93	82 93	74 85 92	75 86 93	75 89 95	76 86 96	92 97	95 96	78·5 94·5	9·4 11·1
31	95	95	95	96	94	96	96	92	84	83	85	79	73	71	72	76	77	78	86	91	93	97	93	97	87.2	10.6
Mean	84.5	85.6	86 · 3	86 · 1	86 · 3	8 4 · o	81 · 7	79 · 8	76.5	73 · 7	72 · 0	70.9	89 · 9	72 · 1	71.7	73·o	74 · 1	76.2	78·o	80·5	83.5	83.5	83.5	84 · 3	79·I	†11.8
Vapour. Pressure*		mb.	mb.	mb. 11·1	mb.	mb. 11·4	mb.	mb. 11·8	mb.	mb.	mb.		mb.	mb. 12·4	mb.	mb.	mb.	mb.	mb.	mb. 11·8	mb.	mb.	mb.	mb.	mb. §11·7	
Hour G.M.T.	l		3.	4.	5.	6.	 7·	8.	9.	10.	II.	Noon.			- 		17.			20.						
11001 0.11.1.	Ι.	2.	3.	7.	۱ .	٠. ا	/.		9.	10.	1 * * *	110011.	13.	14.	13.	10.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	_

^{*} Computed from the mean temperature and mean relative humidity.

[†] Mean of the column.

51. Aberdeen: North Wall Screen on Tower: h_t (height of thermometer bulbs above the ground) = 12.5 metres. September, 1923.

			-																						P.0	er, 1923.
Day.	r.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.			14.	15.	16.	17.		19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
1 2 3 4 5	% 97 93 88 97 80	% 94 92 92 99 83	% 96 96 88 99 84	96 92 91 99 87	96 90 90 99 87	% 96 92 94 95 90	93 88 89 93 87	% 86 89 84 92 86	81 86 81 85 85	% 75 77 67 76 86	% 77 72 70 65 85	% 79 71 67 59	% 86 65 66 56 64	89 60 62 57 64	93 58 64 61 69	% 95 60 77 60 69	% 91 60 78 61 68	% 91 63 73 63 68	% 95 70 72 69 71	% 93 79 77 66 73	% 93 85 85 73 75	94 86 87 76 75	97 86 90 74 79	% 96 87 95 80 79	% 90·8 79·2 80·1 77·6 77·6	mb. 10·5 9·4 9·9 10·6 11·6
6 7 8 9 10	80 89 79 89 77	77 85 82 88 76	79 87 81 89 79	79 83 83 88 79	83 73 81 90 83	87 68 83 84 77	80 65 79 82 72	77 63 70 78 68	75 64 66 74 63	69 59 65 72 59	65 57 65 69 58	66 60 65 70 57	66 54 73 81 55	64 56 76 63 61	69 60 73 56 61	75 59 69 52 63	77 63 70 57 63	82 63 75 59 69	87 67 80 62 73	84 74 85 67 78	82 71 86 71 74	87 75 89 76 71	91 76 88 81 71	90 79 88 78 74	77·7 69·0 76·9 74·2 69·3	13·6 9·7 9·8 11·5 9·1
11 12 13 14 15	76 85 82 95 82	78 80 83 94 87	81 70 86 94 87	84 61 86 92 86	85 61 87 91 83	86 62 85 90 83	79 60 85 85 83	80 52 84 76 78	75 50 81 72 81	71 52 76 69 76	81 52 85 67 76	69 49 88 62 73	72 49 93 60 73	69 49 94 59 73	68 51 91 59 76	73 53 93 58 66	77 55 99 60 61	77 63 97 65 64	81 65 99 70 70	84 70 99 78 76	81 70 100 85 75	84 75 99 83 79	86 77 96 83 80	87 80 96 85 78	78·2 62·3 89·8 76·6 77·1	11·5 9·0 10·5 11·0 9·6
16 17 18 19 20	79 83 88 76 87	82 79 88 81 84	83 82 89 80 87	82 82 93 85 88	85 82 95 80 87	90 79 91 87 86	86 76 90 82 85	81 76 87 78 81	69 79 82 73 75	68 80 77 67 70	67 86 69 63 62	67 85 65 65 58	64 79 64 74 57	64 83 65 86 59	64 82 63 86 62	69 90 66 84 61	67 88 68 83 61	68 88 74 83 69	74 86 75 91 78	74 83 80 91 84	79 86 81 89 83	81 87 79 75 85	83 91 81 80 87	83 92 81 81 87	75·3 83·3 79·0 80·0 75·8	9·0 9·7 9·7 9·2 7·5
21 22 23 24 25	88 90 91 92 90	87 88 92 90 92	88 90 93 87 87	91 90 93 89 87	91 94 94 86 92	91 95 94 86 88	94 97 92 90 91	93 94 95 84 95	92 89 89 77 95	88 80 83 76 95	84 70 82 73 91	78 68 81 71 86	78 65 79 73 82	76 61 80 83 81	77 67 79 80 85	79 65 86 76 86	83 74 91 86 89	84 91 93 86 91	87 93 93 86 91	89 93 94 86 91	89 92 93 87 92	90 91 94 89 93	91 90 94 90 96	91 93 92 96	86·5 84·1 89·5 84·0 90·0	8·5 9·3 9·1 9·4 11·8
26 27 28 29 30	92 90 93 75 95	92 92 95 70 94	88 91 91 70 95	90 92 91 69 96	87 92 94 71 96	87 92 81 76 94	88 91 77 75 98	87 92 88 73 95	79 88 85 69 87	78 95 63 67 77	70 96 63 62 61	68 99 63 59 68	70 99 65 64 71	82 100 54 75 70	84 96 56 75 74	86 97 63 77 72	82 96 58 76 75	83 95 59 91 80	81 94 59 90 79	88 94 70 93 80	80 96 69 95 78	89 93 70 95 81	91 93 70 91 84	90 93 70 92 78	84·0 93·9 73·3 76·6 82·7	11·5 13·9 11·6 11·0 14·5
Mean	86 · 6	86.5	86.6	86.8	86 · 8	86.3	84.4	82 · 1	78.2	73.8	71 · 4	69 · 5	6 9 ·9	70.5	71.3	7 2 ·6	73.9	76.9	79·6	82.4	83 · 2	84.3	85.6	86 · 1	79.8	†10.4
Vapour Pressure*	mb. 10·2	1	mb.	mb. 9·8			mb. 9·8					mb. 10·5					mb.							mb. 10·3		
52. Aberdee	n : :	Nort	h W	all S	cree	n on	Tow	er:	$h_t =$	= 12	·5 m	etres.												(Octobe	r, 1923.
1 2 3 4 5	% 79 79 78 82 84	% 82 82 80 85 78	% 83 81 82 88 81	% 85 81 83 87 80	% 68 88 83 89 75	% 65 83 88 87 79	% 70 83 87 91 84	% 68 74 89 87 85	% 65 69 81 82 82	% 60 61 76 82 85	% 61 57 71 88 85	% 58 65 67 82 87	% 51 55 63 64 90	% 50 58 64 60 86	% 50 59 68 62 85	% 53 59 71 63 87	% 60 63 72 68 89	% 64 66 82 76 91	% 72 71 86 79 92	% 70 76 88 79 92	% 70 76 87 89 91	% 68 77 89 89 88	% 70 79 89 89 90	% 71 81 87 88 89	% 66·5 71·6 79·5 80·6 85·6	mb. 9·5 8·0 7·4 7·2 8·3
6 7 8 9	91 76 77 95 65	87 80 73 92 70	89 79 73 91 73	79 82 77 87 72	80 85 78 64 77	83 88 78 59 70	90 89 75 61 72	89 87 72 66 77	85 85 70 59 73	90 85 65 56 69	87 79 61 55 68	81 82 60 61 65	64 84 57 55 65	62 81 59 52 59	61 65 65 47 61	62 69 68 48 60	66 77 68 58 65	69 76 73 56 70	74 70 75 56 72	76 73 74 61 71	77 75 88 60 73	82 81 91 63 72	77 81 93 67 73	73 76 93 68 75	78·4 79·3 73·1 64·6 69·3	8·9 10·0 8·3 8·2 8·0
11 12 13 14 15	69 79 94 81 92	71 81 94 82 88	69 81 85 81 88	66 86 90 80 78	71 88 93 79 79	68 88 92 85 79	65 90 97 84 81	65 89 94 81 78	66 83 96 78 78	61 76 85 77 76	60 77 79 80 73	57 79 74 85 66	60 79 67 80 67	57 77 70 77 66	56 81 77 80 67	60 85 78 81 70	67 86 81 82 74	69 86 88 84 78	77 93 87 83 77	75 91 87 84 76	79 96 86 86 78	77 96 84 85 84	81 96 80 84 84	82 96 78 83 85	67·7 85·5 85·2 81·6 77·5	6·7 9·1 8·1 7·3 7·9
16 17 18 19 20	88 76 85 95 83	89 76 88 95 81	86 81 84 95 86	85 87 86 95 82	86 94 87 97 82	90 94 89 96 79	86 . 86 90 96 81	87 81 90 97 77	89 73 87 94 75	84 67 86 81 73	75 65 79 58 71	74 63 86 61 76	75 58 83 56 80	76 62 88 55 73	75 63 84 58 84	73 68 88 61 85	81 69 88 68 83	86 69 89 71 79	87 74 93 74 78	89 74 91 76 77	87 78 93 78 82	84 79 96 79 81	83 82 100 79 78	82 83 97 81 81	83·3 75·1 88·3 79·3 79·5	8·0 8·5 10·7 9·9 9·2
21 22 23 24 25	80 83 71 97 86	79 82 73 93 86	81 82 75 91 88	87 89 69 93 88	93 85 76 94 91	93 86 75 96 89	93 90 77 94 89	91 89 82 94 85	90 85 82 88 78	79 84 85 78 74	67 80 84 75 71	66 77 81 67 66	65 72 83 65 67	61 71 81 63 66	58 66 83 66 73	65 71 89 69 77	70 75 95 77 75	74 79 95 78 78	76 86 95 84 85	81 88 97 83 86	80 86 95 84 86	81 76 96 82 84	82 70 97 81 82	76 70 97 82 81	77.9 80.2 84.1 82.6 80.5	9·2 8·4 8·9 8·3 8·1
26 27 28 29 30	78 92 87 92 96	81 92 87 87 96	83 92 83 91 92	81 92 84 85 96	86 89 92 82 95	84 93 88 84 93	89 94 86 85 92	92 94 88 88 88	90 94 83 87 89	90 95 86 83 87	93 93 83 82 79	96 88 82 83 71	86 92 81 77 74	82 89 79 82 75	80 83 80 92 65	78 84 80 95 68	78 85 81 94 70	77 84 78 97 71	86 84 83 98 76	85 86 84 96 78	85 84 84 95 78	88 84 86 96 79	89 82 87 97 76	91 86 87 95 72	85·1 88·9 84·1 89·1 82·0	8·2 10·0 9·8 9·9 11·3
31	74	79	80	83	84	84	80	78	72	74	67	59	бо ——	59	58	64	70	72	74	76	82	82	76	77	73.4	8.3
							84·7					I					75·3					1			79·3 mb.	†8· ₇
Vapour Pressure*	mb. 8·6		8.6	mb. 8·7	8.5	8.4	8.6	8.7	mb. 8 ·8	9.0	mb. 8·9	mb. 9·0	mb. 8·7	mb. 8·7	mb. 8·6	8.7	mb. 8·7	8.6	mb. 8·6	8.5	8.6		8· 5		§8·6	
Hour G.M.T.	I.	2.	3.	4.	5•	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	_

^{*} Computed from the mean temperature and mean relative humidity.

[†] Mean of the column.

53. Aberdeen: North Wall Screen on Tower: h_t (height of thermometer bulbs above the ground) = 12.5 metres. November, 1923.

Day. I. Z. 3. 4. 5. 6. 7. 8. 9. 10. 11. Noon 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. Mean. Pres 1
4 60 71 71 71 70 74 75 75 74 75 75 74 75 75 74 75 75 74 75 75 75 74 75 75 75 75 75 75 75 75 75 75 75 75 75
8 99 94 87 99 90 87 84 89 95 96 97 100 93 98 88 89 02 88 83 97 75 63 68 63 74 79 76 82 83 85 84 80 99 10 96 96 96 94 95 96 97 100 93 98 88 83 77 88 76 81 73 78 78 81 80 81 78 78 78 81 80 81 78 78 78 81 80 81 78 78 78 81 80 81 78 78 78 81 80 81 78 78 78 81 80 81 78 78 78 81 80 81 78 78 81 80 81 78 78 81 80 81 78 78 81 80 81 78 78 78 81 80 81 78 78 78 81 80 81 78 78 78 81 80 81 78 78 81 80 81 78 78 81 80 81 78 78 81 80 81 78 78 81 80 81 78 79 81 81 81 81 81 81 81 81 81 81 81 81 81
112 78 81 82 84 88 86 77 81 82 77 87 87 82 82 77 76 66 66 77 77 1 71 64 67 67 67 67 67 67 72 73 73 73 73 74 74 13 74 74 77 79 85 89 90 92 95 87 87 88 84 88 86 84 93 94 95 95 95 99 90 90 90 97 97 99 90 90 90 97 97 99 90 90 90 90 90 90 90 90 90 90 90 90
17 91 89 86 85 84 82 86 88 89 88 78 77 77 1 69 67 68 89 90 88 89 90 90 92 90 80 80 80 90 90 92 90 80 80 80 90 90 92 90 80 80 80 80 90 90 92 90 80 80 80 90 90 92 90 80 80 80 90 90 92 90 80 80 80 90 90 92 90 80 80 80 90 90 91 80 93 94 96 92 92 80 80 80 80 90 91 80 93 94 96 92 92 80 80 80 80 90 91 80 93 94 96 92 92 80 80 80 80 90 91 80 93 94 96 92 92 80 80 80 80 80 90 91 80 93 94 96 92 92 80 80 80 80 80 80 80 80 80 80 80 80 80
21
27
Vapour Pressure* $\begin{array}{ c c c c c c c c c c c c c c c c c c c$
Pressure* $6 \cdot 3 \mid 6 \cdot 4 \mid 6 \cdot 4 \mid 6 \cdot 3 \mid 6 \cdot 4 \mid 6 \cdot 3 \mid 6 \cdot 4 \mid 6 \cdot 3 \mid 6 \cdot 4 \mid 6 \cdot 5 \mid 6 \cdot 5 \mid 6 \cdot 5 \mid 6 \cdot 5 \mid 6 \cdot 5 \mid 6 \cdot 6 \mid 6 \mid$
1 % % % % % % % % %
1 91 90 91 91 90 89 90 85 89 84 80 80 81 82 85 94 95 95 97 92 93 95 89 3 90 90 90 90 90 90 90
3
6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$
16
21
26 92 92 92 93 93 93 94 94 94 93 92 90 90 90 91 92 92 92 92 93 93 93 93
28 29 30 94 96 95 95 93 93 88 77 82 75 82 83 84 87 87 88 89 88 89 91 91 91 90 89 85 85 81 79 77 79 76 77 77 78 91 91 96 97 98 98 98 98 98 98 98
28 29 30 94 96 95 95 95 93 93 88 77 82 75 82 82 83 84 87 87 88 88 89 91 91 91 91 90 89 92 92 94 97 98 97 98 99 97 97 97 97 97 97 97 97 97 97 97 99 97 97
28
28

^{*} Computed from the mean temperature and mean relative humidity.

[†] Mean of the column.

[§] Mean of the row.

HUMIDITY: ANNUAL MEANS OF HOURLY VALUES.

From the monthly means for exact hours, Greenwich Mean Time.

55. Aberdeen: North Wall Screen on Tower: h_t (height of thermometer bulbs above the ground) = 12.5 metres.

1923.

G.M.T.	1.	2.	3.	4.	5.	6.	7.	8.	.9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
Relative Humidity .	. 83·9	% 84·0	% 84·3	% 84·6	84.7	83.6	% 82·7	% 81·5	% 80·0	% 78·2	% 76·7	% 75·3	74.9	% 74.9	% 75·7	% 76·8	% 77 ^{.8}	% 78·9	- % 80·2	% 81·3	82·4	% 82·9	% 83·4	% 83·8	% 80·5
Vapour Pressure, in mil	8.4	mb. 8·3	mb. 8·3	mb. 8⋅3	mb. 8·3	mb. 8·3	mb. 8·4	mb. 8·5	mb. 8·6	mb. 8·7	mb. 8·8	mb. 8·8	mb. 8·8	mb. 8·9	mb. 8·9	mb. 8∙9	mb. 8·8	mb. 8·8	mb. 8·7	mb. 8•6	mb. 8·6	mb. 8·4	mb. 8·5	mb. 8·4	mb. 8·6

RELATIVE HUMIDITY: MONTHLY MEANS AND DIURNAL INEQUALITIES.

The departures from the mean of the day are adjusted for non-cyclic change.

Aberdeen: North Wall Screen on Tower: $h_t = 12.5$ metres.

1923.

Month.	Mean.	Hour.		3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.
Jan. Feb. Mar.	83.2	0.0	-0.5	-0.7	-1.0	0.0	-1.1	-o·8	-0.5	-0.4	-o·6	-1.0	-0·2 -0·6 -3·4	$-\mathbf{r} \cdot \mathbf{r}$	$ -1 \cdot 1 $	0.0	+0.3	+0.3	+1.1	+0.6	+0.9	+1.2	$+2\cdot 2$	+1.9	+0.6
April May June	80·6 78·1 72·2	+1·5 +4·9 +6·6	+1·0 +4·6 +7·0	+2·0 +5·5 +7·1	$+2 \cdot 3 +6 \cdot 1 +7 \cdot 7$	+2·9 +5·6 +6·7	+2·2 +2·8 +4·1	+1·8 +0·5 +2·0	+0·4 1·1 -0·7	-1·0 -1·7 -2·6	-0·8 -3·9 -4·9	-2·0 -5·5 -5·8	-3·9 - 6·3 -6·6	-3·2 -5·5 -7·4	-3·9 -6·0 - 7·4	-4·0 -4·1 -6·6	-3·3 -2·6 -5·7	-1·5 -3·5 -5·1	-0·7 -3·6	+0·7 -1·5 -1·7	+2·2 0·0 -0·6	+1·5 +2·6 +1·6	+2·2 +3·5 +4·0	+1·6 +3·9 +5·5	+2·1 +4·8 +6·3
July Aug. Sept.	79·1 79·1 79·8	+6·5 +5·6 +6·5	+7·2 +6·7 +6·5	+7·2 + 7·3 +6·5	+7·7 +7·2 +6·8	+6·5 +7·3 + 6·8	+4·1 +5·0 +6·3	+1·8 +2·7 +4·5	-1·5 +0·8 +2·1	-3·5 -2·5 -1·7	-4·4 -5·3 -6·1	-5·3 -7·0 -8·4	-6·8 -8·2 -10·3	-6·3 - 9 ·2 -9·9	-6·3 -7·0 -9·3	-5·5 -7·4 -8·4	-4·8 -6·1 -7·1	-5·1 -5·0 -5·8	-5·2 -2·9 -2·8	-2·7 -1·2 0·0	+0·7 +1·4 +2·8	+2·6 +4·3 +3·6	+3·4 +4·3 +4·7	+4·2 +4·3 +6·0	+5·7 +5·1 +6·6
Oct. Nov. Dec.	79·3 81·8 84·1	+4.0 +1.6 + 1.8	+4·2 +1·8 +1·3	+4·3 +2·3 +1·1	+4·4 +3·0 +1·2	+4·8 + 3·0 +1·7	+4·7 +3·0 +1·8	+5·4 +2·9 +1·2	+4·6 +2·9 +1·5	+1.6 +2.0 +0.9	-1·6 +0·1 -0·2	-5·1 -3·4 -1·6	-6·3 - 6 ·7 -3·2	-9·2 -6·3 - 4·6	-10·3 -6·1 -4·0	-9·9 -4·0 -3·0	-7·4 -1·3 -2·2	-4·0 -0·9 0·0	-1·7 +0·2 +0·6	+1·2 +0·8 +0·2	+2·0 +0·5 +0·6	+3·5 +o·5 +o·7	+3·9 +1·3 +o·9	+3·7 +1·4 +1·4	+3·4 +1·7 +1·7
Year	80.5	+3.4	+3.5	+3.8	+4.1	+4.2	+3.1	+2.2	+1.0	-o·5	-2.3	-3 ⋅8	-5.2	-5.7	-5.6	-4.8	-3.7	-2. 8	-1.6	-0.4	+0.8	+1.0	+2.4	+2.8	+3.3

RAINFALL: ANNUAL TOTALS OF HOURLY VALUES.

Amounts, in millimetres; durations, in hours, for periods of sixty minutes between the exact hours, Greenwich Mean Time.

Aberdeen: $H_r = 14.0$ metres + 0.6 metres.

1923.

G.M.T.			o to I	to 2	to 3	3 to 4	4 to 5	5 to 6	6 to 7	7 to 8	8 to 9	9 to 10	to II	to Noon.	Noon. to 13	13 to 14	14 to 15	15 to 16	16 to 17	17 to 18	18 to 19	19 to 20	20 to 21	2I to 22	22 to 23	23 to 24	o to 24
Amount	• •	••	mm. 35·0				mm. 49·1							mm. 34.0				mm. 54·4	mm. 46·0	mm. 47·0	mm. 33·8		mm. 44°3			mm. 37·5	mm. 944 4
Duration	••		hr. 33·0	hr. 26·9	hr. 24·8	hr. 28·2	hr. 34·5	hr. 33·1	hr. 33·6	hr. 31·8	hr. 32·5	hr. 28·7	hr. 28·1	hr. 28·8	hr. 27·4	hr. 32·0	hr. 34·2	hr. 38·1	hr. 36·3	hr. 40·5	hr. 36·3	hr. 30·4	hr. 30·0	hr. 31·6	hr. 34·8	hr. 36·6	hr. 772·2

58. Aberdeen.

NOTES ON RAINFALL.

1923

(1) Notable Falls and Wet Periods :-

5.—Fall of 15 mm. between o8h. and 19h. Jan.

6-8.—Desultory occasional rain, 50 mm. in all, followed by 13 mm. on the 10th, altogether 63 mm. in 5 days. Feb.

25-28.--Intermittent rain, 29 mm. Feb.

(February was an exceptionally wet month—129 mm. in all fell.) -19 mm. fell, most ly between 04h. and 20h.

May.

(May was also a very wet month—119 mm. fell.) May

3.—19 mm. felt, most by between opt. and 2011.

11-17.—Intermittent rain, 66 mm. in all, 19 mm. of which fell on 11th.

25-26.—More or less continuous rain, 39 mm. in all.

7.—Thunderstorm; 14 mm. of rain fell at a rate of 7.2 mm. per hour; 5 mm. fell in 18 minutes.

10.—Thunderstorm; 16 mm. of rain fell at a rate of 7.6 mm. per hour; 5 mm. fell in 5 minutes. July July 29-30.—Continuous fall 19h. on 29th to 17h. on 30th, 30 mm. in all. 21-29.—Intermittent rain, 63 mm. in all.

Aug. Oct.

Nov.

15-19.—Intermittent rain, 50 mm. in all. 29-30.—Nearly continuous rain, 19 mm. in all. Dec.

(2) Dry Periods :-

13-31.—No rain for first 9 days, and only 2.5 mm. for 18 days. 2-6.—No rain for 5 days. Mar.

May

May 27-July 6.—No fall reached 5 mm., the total fall being 24 mm. in 41 days.

5-12.—In these 8 days the total fall was only 0.8 mm.

(19889)

Amounts in millimetres, for periods of sixty minutes, between the exact hours, Greenwich Mean Time.

59. Aberdeen: H_r (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + h_r (height of receiving surface above ground) = $14 \cdot 0$ metres + $0 \cdot 6$ metres. January, 1923.

Day.	o-I	I-2	2-3	3-4	4-5	5-6	6-7	7-8	8–9	9–10	1011	11–12	12–13	13–14	14–15	15–16	16–17	17–18	18–19	19–20	20-21	21-22	22-23	23-24	0-24	Dura- tion. 0-24
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	Į.	ì	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	hr.
1 2		1.3	1.8										1.0		:::		•••								6.0	5.0
3																				7					1.0	0.9
5	:::						(.1)		•8	1.1	1.9	3.1	1.1	•8	.3	1.9	2.0	1.3	•6	.1					15.1	9.7
6 7		2.4	1.0													•6		•4	• 5					:::	9.0	10.9
8			•••														•••							···	0.9	0.7
9 10	:::										1.1	1.1	•3	•2				•2	•2						3.1	3.2
II	 				.1	.1					.2	.1	٠ı						•1			}			0.7	1.2
12												···													0.4	0.2
13	:::					.8	•6		•4	٠															1.8	0.9
15	***		•••		""					•••							•••				•••					'''
16 17	:::					.1	:::								:::	:::		:::	•1						0.1	0.2
18												•••										:::			:::	:::
19 20	:::					• 5		(.4)	(·5)									·I	·ī						1.9	(2.3)
21	}												 ·6												1.8	1.9
22 23													•••					•••	•••							
24 25																						:::			:::	:::
26															•••										}	
27 28												(·r)	•••	·9	1.1	· 1			 I						2.7	2.8
29							٠	•6	• • • 5	• 2	.1	• 2	• 2	.3	•1	•4	•8	•6	• 5	•4	.2	.1		.1	5.6	7.2
30	.1	• 2	• 5	.3	.3		.1	·2	.1					•3	1.1	1.2									4.3	5.7
Sum.	1.4	3.9	3.3	2.4	1.0	2.0	1.0	1·8	2.4	1.3	4.0	5.8	3.4	3.0	3.3	4.2	3.6	2.7	2.2	1.3	0.7	0.2	0.4		<u> </u>	55.8
Total	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	h r .	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	
Dura- tion.	1.6	2.2	3.0	2.8	2.4	2.3	2.4	2.6	2.5	1.3	3.2	3.3	3.4	3.6	3.2	3.1	2.7	2.9	3.3	1.5	1.0	0.3	0.2	0.3	55.8	
60.																										
	Aber	deen	: H _r	= 14	·0 me	etres -	+ 0.6	3 met	res.											 					ry, 19	
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm. •6	mm. •6		ry, 19	hr.
I 2										mm. 	mm. 	mm.	mm.	mm. 	1	ł	ł			1		1	mm.	mm.	mm. 1·7	hr. 1·5
ı	m m .	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	•••			•••	•••			•••					·6 	mm. •6 •2	mm. • 1 • 1 • 1	mm. 1·7 o·3	hr. 1·5 o·8
I 2 3	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm. 				 	•••	•••						 	·6 ·3	mm. ·6 ··· ·2 ···	mm. · I · · I · · ·	mm. 1·7 0·3 	hr. 1·5 0·8 0·6
1 2 3 4 5	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.				3.3	4.2	1.0	•6	1·4					·6 	mm. •6 •2	mm1 -1 -1 -1 -1	mm. 1·7 0·3 0·4	hr. 1·5 o·8
1 2 3 4 5	mm.	mm.	mm.	mm.	mm.	mm	mm.	mm.	mm.						1·0 2·2	•6 1·8	1·4	1·2	··· ··· ··· ··· ··· ··· ···	·2	·2	·6 ·3 ·7 	mm. ·6 · ·2 · ·6 · ·1	mm,	mm. 1·7 0·3 0·4 17·7 11·4 21·1	hr. 1·5 0·8 0·6 13·0 4·8 8·2
1 2 3 4 5	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.				3·3 3·4	 4.2 3.4	 I.O 2.2	 •6 1.8	1·4	 I·2		·2	·2 ·1 ·9	·6 ·3	mm626	mm, · · · · · · · · · · · · · · · · · · ·	mm. 1·7 0·3 0·4	hr. 1·5 0·8 0·6 13·0 4·8
1 2 3 4 5 6 7 8 9	mm	mm.	mm.	mm	mm.	mm	mm	mm	mm	 3.0 	···· ··· ··· ··· ··· 3.4	··· ··· ··· ··· ··· ··· ··· ··· ··· ··	3·3 3·4 ·1 	 4.2 3.4 .4 	 1.0 2.2	•6 1·8	1·4	1·2		·2	·2	·63 .7	mm. ·6 ··· ·2 ··· ·6 ··· ·6 ···	mm, · · · · · · · · · · · · · · · · · · ·	mm. 1·7 0·3 0·4 17·7 11·4 21·1 0·1 12·2 6·1	hr. 1·5 0·8 0·6 13·0 4·8 8·2 0·4 12·8 7·8
1 2 3 4 5 6 7 8 9 10 11 12	mm	mm	mm	mm	mm	mm 1.6 .1	mm	mm	mm 5.0	 3.0 	 	··· ··· ··· ··· ··· ··· ··· ··· ··· ··	3·3 3·4 ·1 1·5	 4.2 3.4 1.5	 1.0 2.2 1.3	•6 1·8 .9	 i.i	 1·2 	 	·2	.2 .1 .9 .1 	·6 ·3 ·7 ·1	mm. ·6 ··· ·2 ··· ·6 ··· ·6 ··· ·1	mm. · i · · · · · · · · · · · · · · ·	mm. 1·7 0·3 0·4 17·7 11·4 21·1 0·1 12·2	hr. 1·5 0·8 0·6 13·0 4·8 8·2 0·4 12·8
1 2 3 4 5 6 7 8 9 10 11 12 13 14	mm	mm.	mm	mm	mm	mm	mm.	mm	mm	 3.0 	 3.4 	··· ··· ··· ··· ··· ··· ··· ··· ··· ··	3.3 3.4 1.5	 4.2 3.4 .4 1.5	 1.0 2.2 1.3 	•6 •6 •8 ··· ·9 •7 ···	 i.i i.i 	 	···· ··· ··· ··· ··· ··· ··· ··· ··· ·	·2 ··· ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	.2 	·6 ·3	mm. ·6 ··· ·2 ··· ·6 ··· ·6 ··· ·1 ··· ··· ··· ··· ··· ··· ··· ··· ··· ··· ···	mm. · I · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · ·	mm. 1·7 0·3 0·4 17·7 11·4 21·1 0·1 12·2 6·1 7·5 2·8 1·9	hr. 1·5 0·8 0·6 13·0 4·8 8·2 0·4 12·8 7·8 4·6 5·1 2·4
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	mm	mm	mm	mm	mm	mm	mm	mm	mm	 3.0 	 	···· ··· ··· ··· ··· ··· ··· ··· ··· ·	3.3 3.4 1.5	 4.2 3.4 1.5 	1.0 2.2 1.3 	•6 •6 •8 ··· ·9 •7 ···	 	 	··· ··· ··· ··· ··· ··· ··· ··· ··· ··	·2 ··· ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	·2	·6	mm. -6 -6 -1	mm. · 1 ·	mm. 1·7 0·3 0·4 17·7 11·4 21·1 0·1 12·2 6·1 7·5 2·8 1·9 1·1	hr. 1·5 0·8 0·6 13·0 4·8 8·2 0·4 12·8 7·8 4·6 5·1 2·4 1·2
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16	mm	mm	mm	mm	mm	mm	mm	mm	mm	 3.0 	 3.4 7	··· ··· ··· ··· ··· ··· ··· ··· ··· ··	3.3 3.4 1.5	 4.2 3.4 .4 1.5	 1.0 2.2 1.3 	•6 •6 •8 ··· ·9 •7 ···	 i.i i.i 	 	···· ··· ··· ··· ··· ··· ··· ··· ··· ·	·2 ··· ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	.2 	 	mm661111111111111111111111111111111111	mm. · · · · · · · · · · · · ·	mm. 1·7 0·3 0·4 17·7 11·4 21·1 0·1 12·2 6·1 7·5 2·8 1·9	hr. 1·5 0·8 0·6 13·0 4·8 8·2 0·4 12·8 7·8 4·6 5·1 2·4
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1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	mm	mm.	mm	mm	mm	mm	mm	mm	mm	3.0	 	 	3·3 3·4 ··· ··· 1·5 ··4 ··· ··· ··· ··· ··· ··· ··· ··· ·	4.2 3.4 1.5		 	 	 	 1.5 	·2 ··· ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	.2 	·6	mm62611111	mm. · 1 ·	mm. 1·7 0·3 0·4 17·7 11·4 21·1 0·1 12·2 6·1 7·5 2·8 1·9 1·1 7·9 0·1 (1·7)	hr. 1·5 0·8 0·6 13·0 4·8 8·2 0·4 12·8 4·6 5·1 2·4 1·2 12·1 0·3 (3·6)
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1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	mm	mm	mm	mm	mm	mm 1.6	mm	mm	mm 5.0	3.0			3·3 3·4 ··· 1·5 ··· ··· ··· ··· ··· ··· ··· ···	4·2 3·4 1·5	I · · · · · · · · · · · · · · · · · · ·	 			 (·I) 	·2 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	 		mm626111	mm.	mm. 1·7 0·3 0·4 17·7 11·4 21·1 12·2 6·1 7·5 2·8 1·9 1·1 7·9 0·1 (1·7) (3·2) 1·7 0·1 0·9 7·2	hr. 1·5 0·8 0·6 13·0 4·8 8·2 0·4 12·8 4·6 5·1 2·4 1·2 12·1 0·3 (3·6) (8·1) 1·6 0·3 0·8 10·8 7·3 7·4
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1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 Sum. Total Dura-	mm	mm	mm	mm	mm	mm	mm	mm 3.5	mm 5.0 (·3) (·1) 6.6 hr. 3.8				3.3 3.4 1.5 1.5	4·2 3·4 · 1·5 · · () ·3 · · · · 7·6	I · 0 2 · 2 I · 0							.6	mm626111	mm.	mm. 1·7 ··· 0·3 ··· 0·4 17·7 11·4 21·1 12·2 6·1 7·5 2·8 1·9 1·1 7·9 0·1 ··· (1·7) (3·2) 1·7 0·9 7·2 8·6 6·5 6·8 129·0 hr. 121·1	hr. 1·5 0·8 0·6 13·0 4·8 8·2 12·8 7·8 4·6 5·1 2·4 1·2 12·1 0·3 (3·6) (8·1) 1·6 0·3 0·8 10·8 7·3 7·4 5·6

Amounts in millimetres, for periods of sixty minutes, between the exact hours, Greenwich Mean Time.

61. Aberdeen: H_r (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + h_r (height of receiving surface above ground) = $14 \cdot 0$ metres + $0 \cdot 6$ metres. March, 1923.

			-											1 0	6 mei	.103.								Marc	,	
Day.	0-I	1-2	2-3	3-4	4-5	5-6	6-7	7-8	8-9	9-10	10-11	11-12	12-13	13-14	14-15	15–16	16–17	17–18	18–19	19-20	20-21	21-22	22-23	23-24	0-24	Dura- tion. 0-24
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	1	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	hr.
I 2		·1				· · I	1.0	1.2	.1		.2	·2									•••				3.1	1·8 2·8
3	.5	•3			.1	.3	•2	.9	·8	1.6	1.7	1.9	1.7	1.3	2.4	1.6	2.2	1.3	•6	· 1	•••				19.4	13.8
5				:::							·1	(.5)	·1					••2	•4						0.5	0.2
6												l	.1			· 1									0.2	0.4
7				•1																			1.1	2.6	3.8	1.9
8 9										1.3	·2		l :::				. 1	•••		• • • • • • • • • • • • • • • • • • • •				:::	3.8	3.3
10	•2								.1		.4								•••			.6			1.3	1.3
11																								.1	0.1	0.1
12		· I								:::							1.3	2.0	.3	1.5	2.3	· 2			7.9	4.0
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2I 22	(≡€)	(≡€)	(.1)	(≡:)	(≡:)	(.1)	(≡€)						:::												0.2	(1.0)
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30											•••	:::								• • • • • • • • • • • • • • • • • • • •		:::			:::	:::
31			l									 							l		l					
Sum.	1.3	1.1	0.6	0.5	0.1		·			-	-	-[-	- 	-	3.9			ļ	ļ	0.8	- 	-		ļ- <u>-</u> -
	<u> </u>	<u> </u>			 	0.5	1.5	3.0	2.5	3.2	3.0	2.8	2.1	1.3	2.4	1.7	9.9	3.4	1.3	1.7	2.4	-	1.1	2.7	45.2	36.6
Total Dura-	hr. 1·5	hr.	hr.	hr. 0.6	hr. 0·3	hr.	hr. 2·1	hr. 3·0	hr.	hr.	hr. 2.4	hr. 2.6	hr.	hr.	hr.	hr.	hr. 1 · 8	hr. 2·3	hr. 1.6	hr.	hr.	hr.	hr. 0.8	hr.	hr. 36·6	
tion.	l	[1			-		'		1	1	1	}	}	1		-				1	İ	i	1	1
62.	l Aber	deen	 : H _r	= 14	l •0 m	etres	+ 0.	6 me	tres.	1	1 -	1	<u> </u>	}	}	-					<u> </u>	<u> </u>		Apı	l ·il, 19	23.
62.	Aber	mm.	mm.	$= 14$ $\mid mm.$	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	1		1	mm.	mm.	l .		. mm.		mm.	mm.	hr.
62. I 2										mm. 	mm.	mm. '4 	mm. '3	mm. · 5	mm.	mm. ·8 	mm. •9 	mm. ·7 ·1	mm. 1·0 ·2	mm. 2·4 ·1	mm. 1·9 ·1	. mm.	mm.	mm.		
62.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.		•••	·4 	·3 ···	· 5 	 1.0	·8		·7 ·1	I · 0 · 2 	2·4 ·1	1.9	mm. ·8 	.9	mm.	mm. 11·7 1·5	hr. 10·7
62. I 2	mm. •••	mm. .5	mm.	mm. 	mm. 	mm.	mm.	mm. 	mm. 		•••				1.0	8		.7	1.0	2:4	1.0	mm. ·8 ···		mm.	mm. 11·7 1·5	hr. 10·7 2·7
1 2 3 4	mm. • I • · ·	mm. .5 	mm. • 1	mm.	mm.	mm. • 1 •	mm. • I •	mm. • I •	mm.			·4 ···	·3 	· 5		·8	.9	.7 .1 	1.0 .2 	2·4 ·I 	 	mm. ·8 ··· ···	·9 	mm. · I · · · · · ·	mm. 11·7 1·5	hr. 10·7 2·7
1 2 3 4 5 6 7	mm.	mm5	mm	mm.	mm.	mm	mm	mm	mm.				·3 	·5	···	·8			1·0 ·2 	2·4 ·1 	 .1	. mm		mm. · I · · · · · · · · · · · · · · · ·	mm. 11·7 ···5 ···	hr. 10·7 2·7
1 2 3 4 5 6 7 8 9	mm	mm5	mm	mm.	mm.	mm	mm	mm	mm.			·4 	·3 	·5		·8			1·0 ·2 	2·4 ·1 ··· ···	1·9 ·1 ··· ···	. mm8		mm	mm. 11·7 1·5 	hr. 10·7 2·7 0·9 0·2
1 2 3 4 5 6 7 8	mm	mm5	mm	mm.	mm.	mm.	mm.	mm	mm.				·3 	· 5		·8		·7 ·1 ··· ··· ··· ···	······································	2·4 ·1 ·1 	1·9 ·1 ··· ··· ··· ··2 ···	. mm8		mm. · I · · · · · · · · · · · · · · · ·	mm. 11·7 1·5 	hr. 10·7 2·7 0·9 0·2
1 2 3 4 5 6 7 8 9 10 11	mm	mm ·5	mm	mm.	mm.	mm	mm	mm1	mm.				·3 	· 5	1.0			·7 ·1 ··· ··· ··· ··· ··· ··· ···	1·0 ·2 ·1 	2·4 ·1 ·1 	1·9 ·1 ··· ··· ··· ··· ··· ···	. mm		mm. · I · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · ·	mm. 11·7 1·5 0·5 0·2 2·8	hr. 10·7 2·7 0·9 0·2 3·8 3·3
62. 1 2 3 4 5 6 7 8 9 10	mm · · · · · · · · · · · · · · · ·	mm ·5	mm	mm	mm.	mm	mm1	mm1	mm						 	.8	 	·7 ·1 ··· ··· ··· ··· ··· ··· ···	1·0 ·2	2·4 ·1	1·9 ·1	. mm8		mm. · I · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · ·	mm. 11·7 1·5 0·5 0·2 2·8 5·5 1·5	hr. 10·7 2·7 0·9 0·2 3·8
62. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14	mm. ··· ··· ··· ··· ··· ··· ···	mm	mm	mm	mm	mm	mm	mm	mm 1 · 2 2 · 4	 		·4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··			 	.8	 	.7 .1	1.0 .2 	2·4 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ··	1·9 -1	. mm8		mm.	mm. 11.7 1.5 0.5 0.2 2.8 5.5 1.5 2.5 0.5	hr. 10·7 2·7 0·9 0·2 3·8 3·3 1·0 (2·2) 0·7
62. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15	mm. ··· ··· ··· ··· ··· (≡ ;)	mm	mm	mm	mm	mm	mm. ··· ··· ··· ··· ··· ··· ···	mm	mm 1 · 2	 		·4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··				.8 i.5	 	.7 .1 	1.0 .2 	2·4 ·1	1·9 ·1	. mm8		mm. · · · · · · · · · · · · · · · · ·	mm. 11.7 1.5 0.5 0.2 2.8 5.5 1.5 2.5 0.5	hr. 10·7 2·7 0·9 0·2 3·8 3·3 1·0 (2·2) 0·7
62. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16	mm. ··· ··· ··· ··· ··· ··· ···	mm	mm	mm	mm	mm	mm	mm	mm 1.2 2.4	 		·4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··			 	.8	·9 ··· ··· ··· ··· ··· ··· ··· ··· ···	.7 .1	1.0 -2	2·4 -1	1·9 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ·	. mm8		mm.	mm. 11.7 1.5 0.5 0.2 2.8 5.5 1.5 2.5 0.5 0.5	hr. 10·7 2·7 0·9 0·2 3·8 3·3 1·0 (2·2) 0·7 I·2
62. 1 2 3 4 5 5 6 78 8 9 10 11 12 13 14 15 16 17 18	mm (≡ ;)	mm5 (≣i)	mm.	mm (≡i)	mm	mm	mm	mm	mm 1 · 2	 		·4 ··· ··· ··· ··· ··· ··· ··· ··· ···			 	.8	 	.7 .1	1·0 -2	2·4 -1	1·9 ·1	. mm. ·8 ··· ··· ··· ··· ··· ··· ··· ··· ···		mm.	mm. 11.7 1.5 0.5 0.2 2.8 5.5 1.5 2.5 0.5	hr. 10·7 2·7 0·9 0·2 3·8 3·3 1·0 (2·2) 0·7
62. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17	mm	mm5 (≡;)	mm	mm (≡;)	mm	mm	mm	mm	mm 1 · 2 2 · 4			·4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··			 	.8	 	.7 .1	1.0 -2	2·4 ·I ··· ··· ··· ··· ··· ··· ··· ··· ··	1·9 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ·	. mm8	 	mm.	mm. 11.7 1.5 0.5 0.2 2.8 5.5 1.5 2.5 0.5 0.5	hr. 10·7 2·7 0·9 0·2 3·8 3·3 1·0 (2·2) 0·7 1·2
62. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	mm (\equiv i)	mm5 (≡;)	mm.	mm (≡;)	mm	mm	mm (≡;)	mm	mm I · 2 2 · 4		··· ··· ··· ··· ··· ··· ··· ··· ··· ··	·4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··				·8	 	.7 .1	 	2·4 ·1	1·9 ·1	. mm8	 	mm.	mm. 11.7 1.5 0.5 0.2 2.8 5.5 1.5 2.5 0.5 0.5	hr. 10·7 2·7 0·9 0·2 3·8 3·3 1·0 (2·2) 0·7 1·2 0·6
62. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	mm (\equiv i)	mm (≡:)	mm	mm	mm (≡;)	mm (·1)	mm (童:)	mm	mm	 	··· ··· ··· ··· ··· ··· ··· ··· ··· ··	·4			 	.8	 	.7 .1	 	2·4 ·I ··· ··· ··· ··· ··· ··· ··· ··· ··	1·9 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ·	mm8 .		mm.	mm. 11.7 1.5 0.5 0.2 2.8 5.5 1.5 2.5 0.5 0.5 0.5	hr. 10·7 2·7 0·9 0·2 3·8 3·3 1·0 (2·2) 0·7 1·2 0·6 0·6 0·2
62. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	mm (\equiv i)	mm5 (\equiv i)	mm	mm (≡i)	mm.	mm (·I)	mm (≡;)	mm	mm I · 2 2 · 4		··· ··· ··· ··· ··· ··· ··· ··· ··· ··	·4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··			 	.8	 	.7 .1	 	2·4 ·I ··· ··· ··· ··· ··· ··· ··· ··· ··	1·9 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ·	mm	 	mm.	mm. 11.7 1.5 0.5 0.2 2.8 5.5 1.5 2.5 0.5 0.5 0.5 0.6 0.1 (2.5)	hr. 10.7 2.7 0.9 0.2 3.8 3.3 1.0 (2.2) 0.7 0.6 0.6 0.2 (4.1)
62. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	mm (\equiv i)	mm5 (≡;)	mm (·1)	mm (≡;)	mm	mm	mm (≡;)	mm	mm		··· ··· ··· ··· ··· ··· ··· ··· ··· ··	·4			 	.8	 	.7 .1	 	2·4 ·1	1·9 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ·	mm		mm.	mm. 11.7 1.5 0.5 0.2 2.8 5.5 1.5 2.5 0.5 0.5 0.5	hr. 10·7 2·7 0·9 0·2 3·8 3·3 1·0 (2·2) 0·7 1·2 0·6 0·6 0·2
62. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	mm (≡;)	mm5 (≡;)	mm (·1)	mm (≡•)	mm	mm (·1)	mm (≡;)	mm	mm			·4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··				.8		.7 .1	 	2·4 ·1	1·9 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ·	. mm	 	mm.	mm. 11.7 1.5 0.5 0.2 2.8 5.5 1.5 2.5 0.5 0.5 0.5 0.6 0.1 (2.5) (1.1)	hr. 10·7 2·7 0·9 0·2 3·8 3·3 1·0 (2·2) 0·7 0·6 0·6 0·2 (4·1) (2·1)
62. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	mm	mm (≡;)	mm	mm (≡i)	mm (≡;)	mm (·1)	mm	mm	mm		··· ··· ··· ··· ··· ··· ··· ··· ··· ··	·4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	 		 	.8	 	·7 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ··		2·4 ·1	1·9 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ·	mm8 .		mm	mm. 11.7 1.5 0.5 0.2 2.8 5.55 1.55 2.5 0.5 0.5 0.5 0.6 0.1 (2.5) (1.1) 6.3 2.4	hr. 10.7 2.7 0.9 0.2 3.8 3.3 1.0 (2.2) 0.7 0.6 0.6 0.2 (4.1) 6.0 3.5
62. I 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	mm (≡;)	mm	mm	mm (≡i)	mm	mm	mm (≡:)	mm	mm		··· ··· ··· ··· ··· ··· ··· ··· ··· ··	·4	·3 ··· ··· ··· ··· ··· ··· ··· ··· ···		1·0	.8	 	.7 .1		2·4 ·I	1·9 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ·	mm. -8		mm.	mm. 11.7 1.5 0.5 0.2 2.8 5.5 1.5 2.5 0.5 0.5 0.6 0.1 (2.5) (1.1) 6.3 2.4 2.8 1.3	hr. 10.7 2.7 0.9 0.2 3.8 3.3 1.0 (2.2) 0.7 0.6 0.6 0.2 (4.1) (2.1) 6.0 3.5 0.5 1.0
62. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mm (≡;)	mm (≡;)	mm (·1)	mm (≡;)	mm	mm (·I)	mm	mm	mm		··· ··· ··· ··· ··· ··· ··· ··· ··· ··	· 4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·				.8		·7 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ··		2·4 ·I	1·9 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ·			mm	mm. 11.7 1.5 0.5 0.2 2.8 5.55 1.5 2.5 0.5 0.5 0.6 0.1 (2.5) (1.1) 6.3 2.4 2.8 1.36	hr. 10.7 2.7 0.9 0.2 3.8 3.3 1.0 (2.2) 0.7 0.6 0.6 0.2 (4.1) (2.1) 6.0 3.5 1.0 0.5 1.0 2.7
62. I 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum.	mm	mm (≡;)	mm	mm (≡:)	mm (≡i)	mm	mm (≡i)	mm	mm		··· ··· ··· ··· ··· ··· ··· ··· ··· ··	· 4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·	 		1·0	.8	 	.7 .1	1.0 -2	2·4 ·I	1·9 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ·	mm. -8	·9 ··· ··· ··· ··· ··· ··· ··· ··· ···	mm	mm. 11.7 1.5 0.5 0.2 2.8 5.5 1.5 2.5 0.5 0.5 0.6 0.1 (2.5) (1.1) 6.3 2.4 2.8 1.3 1.6 46.4	hr. 10.7 2.7 0.9 0.2 3.8 3.3 1.0 (2.2) 0.7 0.6 0.6 0.2 (4.1) (2.1) 6.0 3.5 0.5 1.0
62. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mm (≡;)	mm (≡;)	mm (·1)	mm (≡;)	mm	mm (·I)	mm (≡;)	mm	mm		··· ··· ··· ··· ··· ··· ··· ··· ··· ··	· 4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·	·3 ··· ··· ··· ··· ··· ··· ··· ··· ···		1.0	.8		·7 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ··		2·4 ·I	1·9 ·1 ··· ··· ··· ··· ··· ··· ··· ··· ·			mm	mm. 11.7 1.5 0.5 0.2 2.8 5.55 1.5 2.5 0.5 0.5 0.6 0.1 (2.5) (1.1) 6.3 2.4 2.8 1.3 1.6	hr. 10.7 2.7 0.9 0.2 3.8 3.3 1.0 (2.2) 0.7 0.6 0.6 0.2 (4.1) (2.1) 6.0 3.5 1.0 0.5 1.0 2.7

RAINFALL.

Amounts in millimetres, for periods of sixty minutes between the exact hours, Greenwich Mean Time.

63. Aberdeen: H_r (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + h_r (height of receiving surface above ground) = 14·0 metres + 0·6 metres.

May, 1923.

Day.	0-1	1-2	2-3	3-4	4-5	5–6	6-7	7-8	8-9	9-10	10-11	11-12	12-13	13-14	14-15	15-16	16–17	17-18	18–19	19–20	20-21	21-22	22-23	23-24	0-24	Dura- tion. 0-24
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	1	mm.		mm.	mm.	mm.	mm.	mm.	mm.	mm. 0·7	hr. 1·2
I 2				· I									 I													
3 4																							•••			
5				•••														•••	•••			•••	""	•••	•••	•••
6 7																	·1		•••						0.8	0.6
8 9															:::	.8	1.4		ı						2.8	1.0 0.9
10		.1	•••											•6	.6	•6	.3		.1	***		•••	•••		2.3	2.2
11 12						· · ɪ	·6	(.1)			2.6	3.6	I · 2		:::		I·2	8	2.3	1.4	1.4	•6	1.5	2.3	6.0	5·I
13	• 5					2.2	•6	4														· I	1.4	.2	7·2	4.4 0.2
14 15			••2	1.7	2.4	1.2	• 5	1.3	•1									1.6	• 7	.4	.7	.9	.7	•2	13.2	10.1
16	٠1	.2	• 1	·6					 1·6	4.0	3.6	1.0	·1	 I·2			· · · · · · · · · · · · · · · · · · ·		· I				•••	•••	3·9 16·5	4·1 7·9
18			:::		.1							· I	 		·2	.1	.3	1.1	• I		·			·	0·6 2·6	3.2
19 20												•4						·I		•••		•••	•••		0.0	1.9
21												• 1													0·1	0.4
22 23																					1.6				0.3	0.5
24 25								• 4					• 7	1.7	2.7	2 · I	I·2	2.5	2.0		1.9	1.9	1.3	.9		13.3
26	1.0	1.2	.1			•6	1.3	1.0	•т	.3			.2	.3	.3	2.6	•1	.9	٠ı		•8	4.4			16·3 0·2	0.5
27 28									•••																	
29 30		}					···				•••														0.1	o·8
31	l		 			 					•															•••
Sum.	3.3	2.3	0.7	2.8	3.1	4.6	3.7	3.3	3.3	6.5	8.4	7.8	5.3	4.1	4.5	8.9	4.8	7.2	5.7	4.0	6.5	8.5	4.8	4.7	118.8	84.5
Total	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	
Dura- tion.	2.8	2.1	1.0	2.4	1.6	2.5	3.6	2.4	2.4	4.4	3.2	4.5	3.7	3.6	3.1	5.7	4.3	4.4	4.4	4.3	4.3	4.7	4.6	4.3	84.5	
1 61011.	1	Ī	1 1		i					į į			l			<u> </u>			<u> </u>	1	<u> </u>	<u> </u>	<u> </u>		<u> </u>	
	Aber	deen	: Hr	= 14	·0 m	etres		6 met	res.									<u> </u>	<u> </u>	1	!	<u> </u>	1	Jun	' 10, 19	23.
64.	Aber	deen	: H _r	= 14	·0 m	etres	+0.0		res.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	, 19	23.
							+0.0			mm. 	mm.						mm.							mm. 	mm.	hr.
64.	mm.	mm.	mm.	mm.	mm.	mm.	+ 0 · · · · · · · · · · ·	mm.	mm.										··· ··· ·4 ···	···				mm. .1	mm. 1.6	hr 3.1 1.0
64. I 2 3	mm.	mm.	mm.	mm. 	mm.	mm.	+ 0 · · · · · · · · · · · · · · · · · ·	mm.	mm.			 ·2	 .3			·	•••		 .4	···				mm	mm 1.6 0.1 3.9	hr 3·1 1·0 5·1
64. I 2 3 4 5 6	mm.	mm.	mm.	mm.	mm.	mm.	+ 0 · · · · · · · · · · · · · · · · · ·	mm.	mm. .1			 ·2 	 :3 	···· ··2 ···					··· ··· ·4 ···	···				mm. 	mm 1.6 0.1 3.9	hr 3·1 1·0 5·1
64. 1 2 3 4 5 6 7 8	mm	mm.	mm.	mm	mm	mm.	+ 0 · · · · · · · · · · · · · · · · · ·	mm.	mm1			···· ··· ··· ···	 .3 	··· ··2 ··· ··4	···· ··· ··· ·· ·· ·· ·· ·· ·· ·· ·· ··	··· ·I ··· ·4	 1.9	 	··· ··4 ··· ·3	···			•••	mm. 	mm. 1.6 0.1 3.9 	hr 3·1 1·0 5·1
64. 1 2 3 4 5 6 7	mm.	mm.	mm.	mm	mm.	mm.	+ 0 · · · · · · · · · · · · · · · · · ·	mm.	mm.			 ·2 	 .3 	···· ··· ··· ··· ··· ··· ···	···· ··2 ··· ··1	··· ·· ·1 ·· ·4 ···	 1·9	··· ··· ··· ··· ··· ··· ··· ···	··· ·· ·3 ··· ···	 				mm	mm 1.6 0.1 3.9 1.1 0.6	hr 3·1 1·0 5·1 3·2 0·7
64. 1 2 3 4 5 6 7 8 9 10 11	mm	mm.	mm.	mm.	mm	mm.	+ 0 · · · · · · · · · · · · · · · · · ·	mm	mm		 	 .2 			 .2 .1	··· ·· ·1 ·· ·4 ··· ·· ·· ·· ··	 1·9		··· ··4 ··· ··3	···				mm.	mm 1.6 0.1 3.9 1.1 0.6 1.1 0.6	hr 3·I I·0 5·1 3·2 0·7 I·9 2·7
64. 1 2 3 4 5 6 7 8 9 10 11 12 13	mm	mm.	mm.	mm	mm	mm.	+ 0 · · · · · · · · · · · · · · · · · ·	mm	mm			 .2 	 .3 		 	··· ·· · · · · · · · · · · · · · · · ·	 		'4 '3					mm.	mm 1.6 0.1 3.9 1.1 0.6 1.0 2.5 0.5 0.3	hr 3·1 1·0 5·1 3·2 0·7 1·9 2·7 0·4 0·5
64. 1 2 3 4 5 6 7 8 9 10 11 12	mm	mm.	mm.	mm	mm	mm	+ 0 · · · · · · · · · · · · · · · · · ·	mm	mm		 	 .2 	 .3 		 	··· ·· ·1 ··· ·4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·	 		'4 '3					mm	mm 1.6 0.1 3.9 1.1 0.6 1.0 2.5 0.5	hr 3·1 1·0 5·1 3·2 0·7 1·9 2·7 0·4 0·5 0·6
64. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	mm	mm.	mm.	mm.	mm	mm.	+ 0 · · · · · · · · · · · · · · · · · ·	mm	mm				 				 		 '4 '3 					mm	mm 1.6 0.1 3.9 1.1 0.6 1.0 2.5 0.5 0.3	hr 3·1 1·0 5·1 3·2 0·7 1·9 2·7 0·4 0·5
64. 1 2 3 4 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18	mm	mm.	mm.	mm	mm	mm	+ 0 · · · · · · · · · · · · · · · · · ·	mm	mm				 .3 		 									mm	mm. 1.6 o.1 3.9 1.1 o.6 1.0 2.5 o.5 o.3 o.6 1.2 o.8	hr 3·1 1·0 5·1 3·2 0·7 1·9 2·7 0·4 0·5 0·6
64. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	mm	mm	mm.	mm.	mm	mm	+ 0 · · · · · · · · · · · · · · · · · ·	mm	mm				 						'4 '3					mm	mm 1.6 0.1 3.9 1.1 0.6 1.1 0.6 1.0 2.5 0.5 0.3 0.6 1.2	hr 3·1 1·0 5·1 3·2 0·7 1·9 2·7 0·4 0·5 0·6 0·7 1·4
64. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	mm	mm	mm.	mm	mm	mm	+ 0 · · · · · · · · · · · · · · · · · ·	mm	mm				 											mm	mm. 1.6 0.1 3.9 1.1 0.6 1.0 2.5 0.3 0.6 1.2 0.8 0.7 0.2	hr 3·1 1·0 5·1 3·2 0·7 1·9 2·7 0·4 0·5 0·6 0·7 1·4 1·1 0·3
64. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	mm	mm	mm.	mm.	mm	mm	+ 0 · 0 mm	mm	mm				 						'4 '3					mm	mm. 1.6 0.1 3.9 1.1 0.6 1.0 2.5 0.5 0.5 0.5 0.6 1.2 0.8 0.7 0.2 0.2	hr 3·1 1·0 5·1 3·2 0·7 1·9 2·7 0·4 0·5 0·6 0·7 1·1 0·3 0·5
64. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	mm	mm	mm	mm	mm	mm	+ 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0	mm	mm				 											mm	mm. 1.6 0.1 3.9 1.1 0.6 1.0 2.5 0.3 0.6 1.2 0.8 0.7 0.2	hr 3·1 1·0 5·1 3·2 0·7 1·9 2·7 0·4 0·5 0·6 0·7 1·4 1·1 0·3 0·5
64. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	mm	mm	mm	mm	mm	mm	+ 0 · · · · · · · · · · · · · · · · · ·	mm	mm								1·9		'4 '3					mm	mm. 1.6 o.1 3.9 1.1 o.6 1.1 o.5 o.5 o.3 o.6 1.2 o.8 o.7 o.2 o.2 o.2 o.2 o.2 o.2 o.2 o.5 o.3 o.6 o.8 o.7 o.2 o.7 o.2 o.7 o.2 o.7 o.2 o.7 o.2 o.7 o.2 o.5	hr 3·1 1·0 5·1 3·2 0·7 1·9 2·7 0·4 0·5 0·6 0·7 1·4 1·1 0·3 0·5 4·3
64. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	mm	mm	mm	mm	mm	mm	+ 0 · 0 mm	mm	mm															mm	mm 1.6 0.1 3.9 1.1 0.6 1.0 2.5 0.3 0.6 1.2 0.8 0.7 0.2 0.2 2.6	hr 3·1 1·0 5·1 3·2 0·7 1·9 2·7 0·4 0·5 0·6 0·7 1·4 0·5 4·3
64. 1 2 3 4 5 6 78 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	mm	mm	mm	mm	mm	mm	+ 0 · 0 mm	mm	mm								1·9							mm	mm. 1.6 0.1 3.9 1.1 0.6 1.0 2.5 0.5 0.5 0.6 1.2 0.8 0.7 0.2 2.6 2.6	hr 3·1 1·0 5·1 3·2 0·7 1·9 2·7 0·4 0·5 0·6 0·7 1·4 1·1 0·3 0·5 4·3
64. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mm	mm	mm	mm	mm	mm	+ 0 · 0 mm	mm	mm															mm	mm. 1.6 o.1 3.9 1.1 o.6 1.1 o.5 o.5 o.3 o.6 1.2 o.8 o.7 o.2 o.2 o.2 o.2 o.2 o.2 o.1	hr 3·1 1·0 5·1 3·2 0·7 1·9 2·7 0·4 0·5 0·6 0·7 1·4 1·1 0·3 4·3 2·5
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum.	mm	mm	mm	mm	mm	mm	+ 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0	mm	mm															mm	mm. 1.6 o.1 3.9 1.1 o.6 1.0 2.5 o.5 o.3 o.6 1.2 o.2 o.2 2.6 4.1 22.0 hr.	hr 3·1 1·0 5·1 3·2 0·7 1·9 2·7 0·4 0·5 0·6 0·7 1·4 1·1 0·3 4·3 2·5
64. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mm	mm	mm	mm	mm	mm	+ 0 · 0 mm	mm	mm											 				mm	mm 1.6 0.1 3.9 1.1 0.6 1.0 2.5 0.3 0.6 1.2 0.8 0.7 0.2 2.6 4.1	hr 3·1 1·0 5·1 3·2 0·7 1·9 2·7 0·4 0·5 0·6 0·7 1·4 1·1 0·3 4·3 2·5

Amounts in millimetres, for periods of sixty minutes between the exact hours, Greenwich Mean Time.

65. Aberdeen: H_r (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + h_r (height of receiving surface above ground) = $14 \cdot 0$ metres + $0 \cdot 6$ metres. July, 1923.

											 ,				- 0.0											D
Day.	o~I	1-2	2-3	3-4	4-5	5-6	6-7	7-8	8-9	9-10	10-11	11-12	12–13	13–14	14-15	15–16	16–17	17-18	18–19	19–20	20-21	21-22	22-23	23-24	0-24	Dura- tion. 0–24
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	hr.
I 2			•3	٠ı		•••			•••	•••				•••		٠:	. I	. і		•••				-:::	0.7	1.4
3				•••		•••								•••	•••					•••						•••
4 5				•••										•••						•••		•••			0.5	0.5
·		•••	•••	•••		'''																			0.1	0.2
6 7	· I		•••		:::			:::		:::					• • • •					3.8	9.9	· I			13.8	1.8
8								1.6	• 2	•••		•5								•••					2.3	1.6
9 10											•6	· I		3.3	9.9	1.7									15 6	2.4
								.5	.3					l							 				o·8	0.8
11 12				:::																•••						
13 14								•••																		
15							•••											•••		•••		.5	.1	·I	0.4	2.8
16						.3														• • • •					0.3	0.2
17 18	•••		•••			•••										1.7									3.7	2.7
19																				•••					0·I	0.2
20	•••	•••				•••	•••								•••	•••		•••		•••		.1		•••	0.1	0.2
21																									2.4	2.0
22 23			• 3	1.2															·I						0.9	1.4
24	٠ı																								1.0	1.4
25	•••		•••																						2.9	1.8
26 27				:									1.2					:::								
28	•••				.1	•5	•6	.6				· 1						· I		.3					3.3	3·6 2·1
29 30	•••														•6	· i									1.0	0.8
31	٠1		.2		.1		.2	(.1)																	0.4	(1.4)
Sum.	0.3	0.5	1.0	1.3	0.9	1.0	1.2	2.8	0.8	0.0	0.7	0.7	1.4	4.0	11 · 6	4.0	0.4	1 · 2	1.4	4.8	10.6	0.4	0.1	0.6	51.7	29.7
Total	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr. 2.0	hr. 1 · 2	hr.	hr.	hr.	hr. 1 · 8	hr.	hr.	hr.	hr.	
Dura- tion.	0.7	0.2	1.2	1.1	1.1	1.3	1.4	2.4	1.0	0.0	0.5	0.8	0.9	1.0	2.0	2.0	1.2	1.0	1.0	2 3	1 0	1 4		1 3	1 7	
tion.		I	ı	1	I	1	<u> </u>	, ,	<u> </u>		<u> </u>	<u> </u>			<u>' </u>	·										
66.	Aber	deen	: H _r	= 14	- -0 m	etres	+ 0.	6 met	res.			<u>. </u>				·				·	·			Augu	st, 19	23.
66.	Aber	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	i i	1	mm.	mm.	mm.] hr.
										mm.	mm.	mm.	mm. 	mm.	mm. 2 · I 	mm. • 5	mm.	mm.	mm.	mm 	mm.	mm.			mm. 2·6 6·8	hr. o·8 3·5
66. I 2 3	mm. .6	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.						2·I 	· 5 			···	 .3		···	mm.	mm. 2·8	mm. 2·6 6·8 0·6	hr. 0·8 3·5 0·7
66.	mm. 	mm.	mm. 	mm.	mm.	mm. 	mm. 	mm. 	mm. 						2·I								mm.	mm.	mm. 2·6 6·8	hr. o·8 3·5
1 2 3 4 5	mm. .6 	mm.	mm.	mm.	mm.	mm.	mm,	mm.	mm.						2·I	· 5 			···	 .3		··· 7	mm. 2.0	mm. 2·8	mm. 2·6 6·8 0·6	hr. 0·8 3·5 0·7
1 2 3 4 5 6 7	mm. .6	mm.	mm.	mm.	mm.	mm.	mm.	mm	mm 2.7				 		2·I			 	 .9 I·2	 .3 	·		mm 2 · 0 · 1 · 1	mm. 2 · 8	mm. 2·6 6·8 0·6 0·5	hr. o·8 3·5 o·7 I·I 7·2
1 2 3 4 5 6 7 8	mm6	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.						2·I	 				···	···	 .7 .2	mm 2 · 0 · 1	mm. 2 · 8 · 1	mm. 2·6 6·8 0·6 0·5	hr. o·8 3·5 o·7 i·i
1 2 3 4 5 6 7	mm6	mm.	mm.	mm.	mm.	mm.	mm	mm 1.6	mm 2.7	 			 		2·I			 	 .9 I·2			72	mm. 2:0 :I	mm. 2 · 8 · 1	mm. 2·6 6·8 0·6 0·5 IO·3 0·3	hr. o·8 3·5 o·7 1·1 7·2 o·2
66. I 2 2 3 4 5 5 6 7 8 9 10 II	mm6	mm.	mm.	mm	mm	mm 4	mm	mm	mm 2.7	 			 		2·I				 .9 I·2 				mm. 2.0 1 1	mm. 2 · 8 1	mm. 2·6 6·8 0·6 0·5 10·3 0·3 1·5	hr. o·8 3·5 o·7 1·1 7·2 o·2 1·3
66. I 2 3 3 4 5 5 6 7 8 9 10 11 12	mm6	mm.	mm.	mm.	mm.	mm.	mm	mm 1.6	mm 2.7	 i.g			 		2·I			 	 .9 I·2				mm 2.0	mm. 2 · 8 1	mm. 2·6 6·8 0·6 0·5 Io·3 0·3 I·5 	hr. o.8 3.5 o.7 1.1 7.2 o.2 1.3
66. I 2 3 4 5 5 6 7 8 9 10 11 12 13 14	mm	mm	mm.	mm	mm	mm.	mm	mm	mm 2.7	 3.2	 				2·I			···	 .9 I·2 	 	 		mm. 2.0 1 1	mm. 2 · 8 1 ·	mm. 2·6 6·8 0·6 0·5 10·3 0·3 1·5 0·1	hr. o·8 3·5 o·7 1·1 7·2 o·2 1·3 o·2 2·5
66. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	mm6	mm	mm.	mm	mm	mm.	mm	mm	mm 2.7	 	 				2·I				 .9 	 .3 .4 	 		mm 2:0	mm. 2 · 8 1	mm. 2·6 6·8 0·6 0·5 10·3 0·3 1·5 0·1 6·3 0·8	hr. o.8 3.5 o.7 1.1 7.2 o.2 1.3 o.2 2.5 o.6
66. 1 2 3 4 4 5 5 6 6 7 8 8 9 10 11 12 13 14 15 16	mm6	mm.	mm.	mm	mm	mm	mm	mm	mm 2.7	 3.2	 				2·I			···	 .9 I·2 	 	 		mm. 2.0 1 1	mm. 2 · 8 1 ·	mm. 2.6 6.8 0.6 0.5 10.3 0.3 1.5 0.1 6.3	hr. o·8 3·5 o·7 1·1 7·2 o·2 1·3 o·2 2·5
66. I 2 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18	mm6	mm.	mm	mm.	mm	mm	mm	mm 1.6	mm 2·7	 1·9 3·2 	 				2·I	 	 	 	 .9 		 		mm 2.0	mm 2·8	mm. 2·6 6·8 0·6 0·5 10·3 0·3 1·5 0·1 6·3 0·8	hr. o.8 3.5 o.7 1.1 7.2 o.2 1.3 o.2 2.5 o.6 1.4 10.0 o.5
66. I 2 3 4 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17	mm6	mm	mm	mm	mm	mm	mm	mm	mm 2.7	 3.2	 				2·I	.5 	 	 	 .9 		 		mm 2.0	mm 2·8	mm. 2·6 6·8 0·6 0·5 10·3 0·3 1·5 0·1 6·3 0·8	hr. o.8 3.5 o.7 1.1 7.2 o.2 1.3 o.6 1.4 10.0
66. I 2 3 4 4 5 5 6 7 7 8 9 10 11 12 13 14 15 16 17 18 19 20	mm6	mm	mm	mm.	mm	mm	mm	mm	mm 2.7 I.3	 3.2 					2·I	 		 	 .9 		 		mm 2.0	mm. 2 · 8 1	mm. 2·6 6·8 0·6 0·5 10·3 0·3 1·5 0·8 2·4 12·6 0·3 0·9	hr. o.8 3.5 o.7 1.1 7.2 o.2 1.3 o.6 1.4 10.0 o.5 2.2
66. I 2 2 3 4 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	mm6	mm	mm	mm	mm	mm	mm	mm 1.6	mm 2.7	 3.2 	 		 	 	2·I	 					 		mm 2.0	mm 2·8	o.1 6.3 o.8 2.4 12.6 o.3 o.9 o.2 7.1	hr. o.8 3.5 o.7 1.1 7.2 o.2 1.3 o.6 1.4 10.0 o.5 2.2 o.5 5.9
66. I 2 3 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	mm6	mm	mm	mm	mm	mm	mm	mm	mm 2.7 I.3	 3.2 				 	2·I	 	 	 	'9 I · 2				mm 2.0	mm 2·8	mm. 2·6 6·8 0·6 0·5 IO·3 0·3 I·5 0·1 6·3 0·8 2·4 I2·6 0·3 0·9 0·2 7·1 II·2 2·3	hr. o.8 3.5 o.7 1.1 7.2 o.2 1.3 o.6 1.4 10.0 o.5 2.2 o.5 5.9 4.1 3.0
66. I 2 3 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	mm6	mm	mm	mm	mm	mm	mm	mm	mm 2.7	 1·9 3·2 			 		2·I	 					 		mm 2.0	mm 2·8	mm. 2·6 6·8 0·6 0·5 IO·3 0·3 I·5 0·1 6·3 0·8 2·4 I2·6 0·3 0·9 0·2 7·I II·2	hr. 0.8 3.5 0.7 1.1 7.2 0.2 1.3 0.2 2.5 0.6 I.4 I0.0 0.5 2.2 0.5 5.9 4.1
66. I 2 3 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	mm6	mm	mm	mm	mm	mm	mm	mm 1.6	mm 2.7	 3.2 	 		 		2·I	 	 				 		mm 2.0	mm 2·8	mm. 2·6 6·8 0·6 0·5 10·3 0·3 1·5 0·1 6·3 0·8 2·4 12·6 0·3 0·9 0·2 7·1 11·2 2·3 2·9 3·6	hr. 0.8 3.5 0.7 1.1 7.2 0.2 1.3 0.6 1.4 10.0 0.5 2.2 0.5 5.9 4.1 3.0 3.2 1.2
66. I 2 3 3 4 5 5 6 7 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	mm6	mm	mm	mm.	mm	mm	mm	mm	mm.	 3.2 			 	 	2·I	 		 			 		mm 2.0	mm 2·8	mm. 2·6 6·8 0·6 0·5 IO·3 0·3 1·5 0·1 6·3 0·8 2·4 12·6 0·3 0·9 0·2 7·1 II·2 2·3 2·9 3·6 0·1 I·5	hr. 0.8 3.5 0.7 7.2 0.2 1.3 0.6 1.4 10.0 0.5 2.2 0.5 5.9 4.1 3.0 3.2 1.2 0.1 0.8
66. I 2 3 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	mm	mm	mm	mm.	mm	mm	mm	mm	mm.	 3.2 				 	2·I	 							mm 2·0	mm 2·8	mm. 2·6 6·8 0·6 0·5 10·3 0·3 1·5 0·1 6·3 0·8 2·4 12·6 0·3 0·9 0·2 7·1 11·2 2·3 2·9 3·6 0·1 1·5 5·2	hr. 0.8 3.5 0.7 7.2 0.2 1.3 0.6 1.4 10.0 0.5 2.2 0.5 5.9 4.10 3.2 1.2 0.8 4.66
66. I 2 3 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mm6	mm	mm	mm	mm	mm	mm	mm 1.6	mm 2.7	3.2				 	2·I	3·I					 		mm 2.0	mm 2·8	mm. 2·6 6·8 0·6 0·5 10·3 0·3 1·5 0·1 6·3 0·8 2·4 12·6 0·3 0·9 0·2 7·1 11·2 2·3 2·9 3·6 0·1 1·5 5·2	hr. 0.8 3.5 0.7 7.2 0.2 1.3 0.6 1.4 10.0 0.5 2.2 0.5 5.9 4.1 3.0 3.2 1.2 0.1 0.8
66. I 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	mm	mm	mm	mm	mm	mm	mm	mm	mm 2·7	3.2				 	2·I	3·I							mm 2·0	mm 2·8	mm. 2·6 6·8 0·6 0·5 10·3 0·3 1·5 0·8 2·4 12·6 0·3 0·9 0·2 7·1 11·2 2·3 2·9 3·6 0·1 1·5 5·2 24·5	hr. 0.8 3.5 0.7 7.2 0.2 1.3 0.6 1.4 10.0 0.5 2.2 0.5 5.9 4.1 3.0 3.2 1.2 0.8 4.6 16.1 1.4
66. I 2 3 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mm6	mm	mm	mm	mm	mm	mm	mm 1.6	mm 2.7	3.2				 	2·I	3·I							mm 2.0	mm 2·8	mm. 2·6 6·8 0·6 10·3 0·3 1·5 0·1 6·3 0·8 2·4 12·6 0·3 0·9 0·2 7·1 11·2 2·3 2·9 3·6 0·1 1·5 5·2 24·5	hr. 0.8 3.5 0.7 7.2 0.2 1.3 0.6 1.4 10.0 0.5 2.2 0.5 5.9 4.1 3.0 3.2 1.2 0.8 4.6 16.1 1.4
66. I 2 3 3 4 5 5 6 6 7 8 8 9 10 11 12 13 13 14 15 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Sum. Total Dura-	mm	mm	mm	mm	mm	mm	mm	mm	mm 2·7	 			 	 	2·I	3·I				·3 · · · · · · · · ·			mm 2·0	mm. 2·8	mm. 2·6 6·8 0·6 0·5 10·3 0·3 1·5 0·1 6·3 0·8 2·4 12·6 0·3 0·9 0·2 7·1 11·2 2·3 2·9 3·6 0·1 1·5 5·2 24·5 1·5 106·1	hr. 0.8 3.5 0.7 7.2 0.2 1.3 0.6 1.4 10.0 0.5 2.2 0.5 5.9 4.1 3.2 1.2 0.8 4.6 16.1 1.4
66. I 2 3 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Sum. Total	mm	mm	mm	mm.	mm	mm	mm	mm	mm 2·7	3.2					2·I	3·I							mm. 2 · 0	mm.	mm. 2·6 6·8 0·6 0·5 10·3 0·3 1·5 0·8 2·4 12·6 0·3 0·9 0·2 7·1 11·2 2·3 2·9 3·6 0·1 1·5 5·2 24·5 1·5 106·1 hr. 73·1	hr. 0.8 3.5 0.7 7.2 0.2 1.3 0.6 1.4 10.0 0.5 2.2 0.5 5.9 4.1 3.2 1.2 0.8 4.6 16.1 1.4

RAINFALL.

Amounts in millimetres, for periods of sixty minutes, between the exact hours, Greenwich Mean Time.

67. Aberdeen: Hr (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + hr (height of receiving surface above ground) = 14.0 metres + 0.6 metres.

September, 1923.

Day.	O-I	I-2	2-3	3-4	4-5	5-6	6-7	7-8	8–9	9–10	10–11	11–12	12–13	13–14	14–15	15–16	16–17	17–18	18–19	19–20	20-21	21-22	22-23	23-24	0-24	Dui tion
	mm.	mm	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	Į.	mm.	h
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4	3.3	1.9	2.2	.7	1.8	2.1	1 . 3	•6		•••														:::	13.8	7.
5		•••			•••	• • • •																			1	1.
6																•••			.6						0.7	0.
7 8	•••	•••			•••						:::															
9														.1				• • • • • • • • • • • • • • • • • • • •			•••				0.1	0.
10		•••				•••		• • • •	•••	•••								• • • • • • • • • • • • • • • • • • • •			•••				'''	"
ΙΙ																	•••	• • • • • • • • • • • • • • • • • • • •		• • • •		•••		•••		1:
12		•••			•••			•••	• • • •	•••				1.1			3.0	1.3		• • • 2	4	• • 2			10.8	10
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16					.4	.7																			14.9	
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29 30																							•••	•••		
ım.	4.3	2.0	4.1	2.9	7.9	6.8	4.7	2.7	2.2	3.0	6.5	3.4	2.4	3.0	6.8	5.8	7.2	4.7	3.3	1.4	1.1	1.3	3.7	3.0	94.2	62
tal ıra-	hr.	hr.	hr.	hr. 2·8	hr.	hr. 4·2	hr. 3·2	hr. 2·6	hr.	hr.	hr. 1 · 8	hr. 2·8	hr.	hr.	hr. 3·3	hr. 2·9	hr. 2·8	hr.	hr.	hr. 1 · 8	hr.	hr. 2·3	hr. 2·6	hr. 3·3	hr. 62•1	
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68.	Aber	deen	$: H_r$	= 14	·0 m	etres	+ 0.	6 met	tres.														(Octob	er, 15	923
68.	Aber	mm.	: H _r			etres	mm.			mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm	}	mm.	mm.	mm.	1
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Amounts in millimetres, for periods of sixty minutes, between the exact hours, Greenwich Mean Time.

69. Aberdeen: H_r (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + h_r (height of receiving surface above ground) = $14 \cdot 0$ metres + $0 \cdot 6$ metres. November, 1923.

Day.	0-І	1-2	2-3	3-4	4-5	5-6	6-7	7-8	8-9	9–10	10–11	11–12	12–13	13–14	14-15	15–16	16-17	17–18	18–19	19-20	20-21	21-22	22–23	23-24	0-24	tion. 0-24
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19	1.3	1.6				(·I) ·I	•6			·6	· I		I · 4	·8		.5					2.7			1.3	13.4	8·6
20	·I				i.	` ′	•••							.2											0.7	1.2
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26																										
27 28						1.4						···								•4					4.0	3.9
29 30						· i	· 1																1.1		0.3	1.0
Sum.	5.1	5.9	3.3	1.8	1.7	2 · 2	2.2	2.0	4.3	3.0	1.1	0.8	2.5	2.9	2.7	5.7	4.6	4.1	4·I	1.6	4.7	3.1	5.6	4.3	79 · 2	65·o
Total	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr. 2·0	hr.	hr.	hr. 65·0	
Dura- tion.	3.3	4.5	1.8	2.8	1.6	1.8	2.6	3.1	4.4	3.2	1.8	0.7	2.2	3.3	1.4	3.4	3.4	2.9	2.4	1.7	2.8	2.0		3.7	<u> </u>	<u> </u>
70.	Aber	deen	: H _r	= 1	4 · 0 m	etres	+ 0	·6 me	tres.										1	1	Imm	mm.	De	ecemb	er, 19	923.
																	mm.	mm.								
1	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm. 	mm.	mm.	mm.			mm.	mm.	mm.					
1 2 3		1	1	1	1	1		1	mm. 2·4	mm. 4.0	mm. ·8	···	1		1										 12·4 	6·6
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2 3 4 5 6 7 8 9 10	 I.4 I.4				1.4	1.9		 	 2·4 1·0 · 	4.0		 				 .3 	 1.0 2.2 .1 	 2·3 			 2·I 	 	 	 I.2 	 12·4 2·5 2·2 8·9 2·3 3·2 4·5	 6·6 4·4 2·1 6·2 2·3 3·3 4·1 5·6
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2 3 4 5 6 7 8 9 10 11 12 13 14 15			 		 1·4 1·4 	1.9		 	 2·4 1·0 2·3 	4.0		 			 		 1·0 2·2 ·1 	2·3			 2·I 	 	 	 	12·4 2·5 2·2 8·9 2·3 3·2 4·5 7·8 1·6 1·8 0·4 1·1 (0·9) (6·5) 1·3	 6·6 4·4 2·1 6·2 2·3 3·3 4·1 5·6 1·5 2·7 2·0 1·2 (1·7)
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20			 (·i)	 (·1)	1·4	 1·9 3·0 (·1)	 (·1)		2·4 1·0	4.0		 			 I.3	 	 1·0 2·2 ·I 	2·3		 	 2·1 	 	 	 	12·4 2·5 2·2 8·9 2·3 3·2 4·5 7·8 1·6 1·8 0·4 1·1 (0·9) (6·5) 1·3 3·5 11·4	6·6 4·4 2·1 6·2 2·3 3·3 4·1 5·6 1·5 2·7 2·0 1·2 (1·7) (5·8) (1·7) 4·9 8·2
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23			 (·1) 2·0	 (·1) (·1)	I'4 I'4 i'1 (-1) (-2) 2·1	 1.9 3.0 (.1)		I.I	2·4 1·0 1·0	4.0					I.3	 	 1·0 2·2 ·1 	 2·3 		 	 2·1 				12·4 2·5 2·2 8·9 2·3 3·2 4·5 7·8 1·6 1·8 0·4 1·1 (0·9) (6·5) 1·3 3·5 11·4 0·3 0·3	6·6 4·4 2·1 6·2 2·3 3·3 4·1 5·6 1·5 2·7 2·0 1·2 (1·7) (5·8) (1·7) 4·9 8·2 2·1 (0·7)
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20			 (·I) 2.0	 (·1) (·1)	I'4 I'4 i'4 (-1) (-2) 2·I	 1·9 3·0 (·1)	 (·I)		2·4 1·0 1·0	4.0		 				 	 1·0 2·2 ·I 	 2·3 		 	2·I				12·4 2·5 2·2 8·9 2·3 3·2 4·5 7·8 1·6 1·8 0·4 1·1 (0·9) (6·5) 1·3 3·5 11·4 0·3 (0·9)	6·6 4·4 2·1 6·2 2·3 3·3 4·1 5·6 1·5 2·7 2·0 1·2 (1·7) (5·8) (1·7) 4·9 8·2 2·1 (0·7) (2·8)
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26					I'4 I'4 (-1) (-2) (-2)	1·9	'7		2·4 1·0 1·0	4.0						 	1.0 2.2 .1	 2·3 			 2·1 				12·4 2·5 2·2 8·9 2·3 3·2 4·5 7·8 1·6 1·8 0·4 1·1 (0·9) (6·5) 1·3 3·5 11·4 0·3 0·3 (0·9) (2·5) 4·0	6·6 4·4 2·1 6·2 2·3 3·3 4·1 5·6 1·5 2·7 2·0 1·2 (1·7) (5·8) (1·7) 4·9 8·2 2·1 (0·7) (2·8) (5·4) 3·9
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28			 (·i) 2·0		I · 4 I · 4 (·1) (·2) (·2)	1.9			2·4	4.0							 1.0 2.2 .1 	 2·3 		 					12·4 2·5 2·2 8·9 2·3 3·2 4·5 7·8 1·6 1·8 0·4 1·1 (0·9) (6·5) 1·3 3·5 11·4 0·3 0·3 (0·9) (2·5) 4·0 4·1 (5·1)	6·6 4·4 2·1 6·2 2·3 3·3 4·1 5·6 1·5 2·7 2·0 1·2 2·1 (0·7) (2·8) (5·4) 3·9 2·4 5·5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27					I'4 I'4 I'4 ('1) ('2) ('2) ('2)	I · 9			2·4	4.0							1.0 2.2 .1	 2·3 	 		 				12·4 2·5 2·2 2·3 3·2 4·5 7·8 1·6 1·8 0·4 1·1 (0·9) (6·5) 1·3 3·5 11·4 0·3 0·3 (0·9) (2·5) 4·0 (4·1) (5·1) (5·1) (14·2)	6·6 4·4 2·1 6·2 2·3 3·3 4·1 5·6 1·5 2·7 2·0 1·2 (1·7) (5·8) (1·7) 4·9 8·2 2·1 (0·7) (2·8) (5·4) 3·9 2·4 5·5 23·0
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29					1·4	1·9			2·4 1·0 1·0	4.0							1.0 2.2 .1								12·4 2·5 2·2 8·9 2·3 3·2 4·5 7·8 1·6 1·8 0·4 1·1 (0·9) (6·5) 1·3 3·5 11·4 0·3 (0·9) (2·5) 4·0 (4·1 (5·1) (14·2) 1·7	6·6 4·4 2·1 6·2 2·3 3·3 4·1 5·6 1·5 2·7 2·0 1·2 (1·7) (5·8) (1·7) 4·9 8·2 2·1 (0·7) (2·8) (5·4) 3·9 2·4 5·5 23·0 3·5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30					1·4	1·9 3·0 (·1) 1·0 1·2 (·2) (·8)			2·4	4.0							1.0 2.2 .1								12·4 2·5 2·2 8·9 2·3 3·2 4·5 7·8 1·6 1·8 0·4 1·1 (0·9) (6·5) 1·3 3·5 11·4 0·3 0·3 (0·9) (2·5) 4·0 4·1 (5·1) (14·2) 1·7	6·6 4·4 2·1 6·2 2·3 3·3 4·1 5·6 1·5 2·7 2·0 1·2 (1·7) (5·8) (1·7) 4·9 8·2 2·1 (0·7) (2·8) (5·4) 3·9 2·4 5·5 23·0
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Summarria (Control of Contro					1·4	1·9			2·4 1·0 1·0	4.0				 			1.0 2.2 .1								12·4 2·5 2·2 8·9 2·3 3·2 4·5 7·8 1·6 1·8 0·4 1·1 (0·9) (6·5) 1·3 3·5 11·4 0·3 (0·9) (2·5) 4·0 (4·1 (5·1) (14·2) 1·7	6·6 4·4 2·1 6·2 2·3 3·3 4·1 5·6 1·5 2·7 2·0 1·2 (1·7) (5·8) (1·7) 4·9 8·2 2·1 (0·7) (2·8) (5·4) 3·9 2·4 5.5 23·0 3·5 113·6
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Total					1·4	1·9 3·0 (·1) 1·0 (·8) hr.		1·1	2·4 1·0	4·0							1.0 2.2 .1								12·4 2·5 2·2 8·9 2·3 3·2 4·5 7·8 1·6 1·8 0·4 1·1 (0·9) (6·5) 1·3 3·5 11·4 0·3 0·3 (0·9) (2·5) 4·0 4·1 (5·1) (5·1) 1·7 105·4 hr. 113·6	6·6 4·4 2·1 6·2 2·3 3·3 4·1 5·6 1·5 2·7 2·0 1·2 (1·7) (5·8) (1·7) 4·9 8·2 2·1 (0·7) (2·8) (5·4) 3·9 2·4 5.5 23·0 3·5 113·6

71. Aberdeen: h_s (height of recorder above ground) = 20.7 metres.

71. <i>A</i>	Aberd	een :	hs (heigh	t of r	ecord	ier at	ove g	groun	(d) ==	20.7	met	res.					Jar	nuary,	1923.
Day.	3 to	4 to 5.	5 to 6.	6 to	7 to 8.	8 to 9.	10.	11.	Noon	Noon to 13.	14.	15.	16.	16 to 17.	18.	18 to 19.	20.	20 to	for Day.	Per cer of Possibl
1	hr.	hr.	hr.	hr.	hr.	hr. 	hr. •7	hr.	hr.	hr. 1·0	hr. •9	hr. 	hr.	hr.	hr.	hr.	hr.	hr.	hr. 4·6	% 69
2	_		_												_		_			
3			_	_	_		• 1	I.0 I.0		1.0	···	• I	•••	_	_				1·2 4·7	18 69
4 5	_	_	_									·5	•••					-		•••
								1.0	1.0	1.0	1.0								4.2	62
6 7			_										•••	_		_			4.3	
7 8					_		•8	1.0	1.0	.8	1.0	.8	•••				_		5.4	78
9 10	_	_	_	_	_		·8	1.0	1.0	1.0				_	_			_	4·I	59
										1					-					
11 12	_		_	_			• • • • • • • • • • • • • • • • • • •				···	.1	•••						2.0	28 4
13	-	_			 —					•5	•6	•5	•••				_		1.6	22
14	-	_	_	_	-	•••	·8 ·8	1.0	1.0	1.0	•7	•••	•••			_	_		4.2	63 19
15	-				_	•••		.3		'4	•••	•••	•••		_				^ 4	19
16	-	—	-	-	-	•••	•••				•••	•••	•••		_	—		_		•••
17 18		_			_		.3	I.0 I.0	1.0	I.0 I.0	·2 ·6			_	_		=		3·5 4·5	47 61
19	l —			—					·ı	٠ı	•1	•••	•••						0.3	4
20		_	_			•••	•1	.1	.3	.3	• I	•••	•••	-		_		_	0.9	12
21								.6	•2	•4	1.0	1.0	٠3					_	3.2	46
22	<u> </u>	-	_		_	.3	1.0	•5					•••					_	1.8	23
23 24	_	_	_					••2	1.0	···	•••		··6		_		_	_	3.2	 41
25		_		-		.3	1.0	1.0	1.0	1.0	•8	.3	.3	_		_			5.7	72
26																				
	_	_	_	_	_		•••				•••	•••					_			
27 28	-	 		—	-		•••		• • • •		•••	•••	• • • • •	-	—			_	•••	•••
29 3 0			_	_			•••				•••		•••	•••	_	_		_		•••
-																				
31					•••		•••													
Sum.	_			—		0.6	8.3	11.8	10.7	11.6	9.1	4.3	1.2	•••					57.5	
						0.6	8.3				•29	•14			_				1.85	25
Sum. Mean.				20		•02	•27											_		25
Sum. Mean. 72.	Aberd	leen :	hs			·02	•27	.38	•35	*37							 hr.	Febr	uary,	²⁵ 1923 .
Sum. Mean. 72.	Aberd	leen :	hs)·7 m	etres.	·27	-38	1.00 hr.	.37	•29	•14 hr.	•04	•••	hr.	hr.	hr.	Febr	uary,	²⁵ 1923 .
Sum. Mean. 72.	Aberd	leen :	hs	hr.	 0.7 m	•o2	•27	-38	'35	hr. 1:0	·29	hr. 1.0 1.0	·04	hr.		_	hr. -	Febr	1.85 uary, hr. 4.7 7.5	25 1923. % 57 89
Sum. Mean. 72. 1 2 3	Aberd	leen :	hs)·7 m	etres.	·27	-38	1.00 hr.	.37	•29	•14 hr.	•04	hr.	hr.	hr.	hr.	Febr	1.85 uary, hr. 4.7 7.5 4.6 7.2	25 1923. % 57 89 54 84
Sum. Mean. 72.	Aberd	leen :	hs	hr.	 0.7 m hr. 	• • • • • • • • • • • • • • • • • • •	·27	-38	hr. 1.0 1.0	hr. 1:0 1:0 :5	hr. 1.0 1.0 .8	hr. i.o i.o ·2	·04	hr.	_	_	hr.	Febr	1·85 uary, hr. 4·7 7·5 4·6	25 1923. % 57 89 54 84
72. 1 2 3 4 5	Aberd	leen :	hs	hr. - -	 0.7 m hr. 	etres.	hr.	hr. 6 1.0 7 1.0	hr. 1.0 1.0 1.0	hr. 1:0 1:0 :5 1:0	hr. I·0 I·0 ·8 I·0	hr. 1.0 1.0 2 1.0	•••4 hr. ••7 	hr			hr.	Febr	1.85 uary, hr. 4.7 7.5 4.6 7.2	²⁵ 1923.
72. 1 2 3 4 5	Aberd	leen :	hs	hr.	hr	etres. hr. .8 .5 .6	·27	·38	hr. 1.0 1.0 1.0 1.0 1.0	hr. 1:0 1:0 2:5 1:0 4	hr. I·0 I·0 ·8 I·0	hr. 1·0 1·0 ·2 1·0	•04 hr76	hr			hr.	Febr	1.85 uary, hr. 4.7 7.5 4.6 7.2 0.8	25 1923. % 57 89 54 84 9
72. 1 2 3 4 5 6 7 8	Aberd	hr.	hs	hr.	 hr. 	etres. hr8 .5 .6	·27	·38	hr. 1.0 1.0 1.0 1.0	hr. i.o i.o ·5 i.o ·4	hr. 1.0 1.0 .8 1.0	hr. 1.0 1.0 2 1.0	hr76	hr			hr.	Febr	n.85	25 1923. % 577 89 54 84 9
72. 1 2 3 4 5 6	Aberd	leen :	hs	hr.	hr	etres. hr. .8 .5 .6	·27	·38	hr. 1.0 1.0 1.0 1.0 1.0	hr. 1:0 1:0 2:5 1:0 4	hr. I·0 I·0 ·8 I·0	hr. 1·0 1·0 ·2 1·0	•04 hr76	hr			hr.	Febr	n. 4.7 7.4.6 7.2 0.8	25 1923. % 577 89 54 84 9
72. 1 2 3 4 5 6 7 8 9 10	Aberd	hr.	hs hr.	hr.	 hr. 	etres. hr8 .5 .6	hr.	-38 hr6 1.0 -7 1.0 -2 1.0	hr. 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.	hr. 1.0 1.0 .5 1.0 .4 1.0	hr. 1.0 1.0 .8 1.0 1.0	hr. I·0 I·0 ·2 I·0 I·0	hr76	hr			hr.	Febr	n. 4.77 7.2 0.8 6.4	25 1923 % 577 89 54 84 9 72
72. 1 2 3 4 5 6 7 8 9	Aberd	hr.	hs hr.	hr.)·7 m	etres. hr8 .5 .6	·27	-38 hr6 1.0 .7 1.0 .2 1.0	'35	hr. 1:0 1:0 :5 1:0 :4 1:0	hr. I.0 I.0 .8 I.0 I.0	hr. 1.0 1.0 2 1.0 1.0 1.0	·04	hr			hr.	Febr	1.85 hr. 4.77 7.5 4.6 7.2 0.8 6.4 1.0	255 1923. % 577 89 54 84 84 9 72 11
72. 1 2 3 4 5 6 7 8 9 10 11 12 13	Aberd	hr.	hs	hr.)·7 m	etres. hr	·277 hr. ·1 1·0 ·9 1·0	-38 hr6 1.0	hr. 1.0	hr. 1.0 1.0 2.1 1.0 2.1 1.0 2.1 1.0 2.1 1.0 2.1 1.0 2.1 1.0 2.1 1.0 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	hr. 1.0 1.0 1.0 1.0 1.0 1.0	hr. 1·0 1·0 ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·	hr	hr			hr.	Febr	n. 4.77 7.2 0.8 6.4 1.0	25 1923. % 577 89 54 84 84 9 72 11
72. 1 2 3 4 5 6 7 8 9 10 11 12 13 14	Aberd	hr.	hs	hr.	hr. hr.	etres. hr8 .5 .6	·277 hr. ·11 ·0 ·9 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0	-38 hr6 1.0 -7 1.0 -2 1.0	'35 hr. 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.	hr. 1:0 1:0 25 1:0 4 1:0 1:0	hr. I · o I · o · · 8 I · o · · · · · · · · · · · · · · · · · ·	hr. I·0 I·0 ·2 I·0 I·0 I·0	· · · · · · · · · · · · · · · · · · ·	hr			hr.	Febr	1.85 hr. 4.77 7.5 4.6 7.2 0.8 6.4 1.0	25 1923. % 577 89 54 84 84 9 72 11
72. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	Aberd	hr.	hs hr.	hr.	hr	etres. hr	·277 hr. ·11 1·0 ·9 1·0 ·9 ·9	-38 hr6 1.0 -7 1.0 -2 1.0	hr. 1.0 1.0 1.0 1.0 1.0 1.0 1.0	hr. 1 · 0 1 · 0 · 5 1 · 0 · 4 1 · 0 1 · 0	hr. I · o I · o I · o I · o I · o I · o	hr. I·0 I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0	hr	hr			hr	Febr	1·85 hr. 4·7 7·5 4·6 7·2 0·8 6·4 1·0	255 1923. % 577 89 544 84 9 72 11
72. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	Aberd	hr.	hs	hr.	0·7 m	etres. hr	·277 hr. ·10 ·9 1·0 · · · · · · ·	-38 hr6 1.0	'35 hr. 1.0	hr. 1.0 1.0 1.0 2.1 1.0 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	hr. 1·0 1·0 ·8 1·0 1·0	hr. 1·0 1·0 ·2 1·0	hr76	hr			hr.	hr.	1.85 hr. 4.77 7.56 4.60 7.22 0.8 6.4 1.00	25 1923. % 57 89 54 84 9 72 11
Sum. Mean. 72. 1 2 3 4 5 6 7 8 9 10 11 11 11 11 11 11 11 11 11 11 11 11	Aberd	hr.	hs hr.	hr.	hr	etres. hr	·277 hr. ·11 1·0 ·9 1·0 ·9 ·9	-38 hr6 1.0 -7 1.0 -2 1.0	hr. 1.0 1.0 1.0 1.0 1.0 1.0 1.0	hr. i.o i.o -4 i.o i.o i.o i.o i.o i.o i.o i.o i.o i.o i.o i.o	hr. I · 0 I · 0 · 8 I · 0 · I · 0 · I · 0 · I · 0 · I · 0 · I · 0 · I · 0 ·	hr. 1·0 1·0 ·2 1·0 ·	hr76	hr			hr.	Febr	n. 85 hr. 4.77 7.56 4.67 7.80 6.4	25 1923. % 57 89 54 84 9 72 11
72. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	Aberd	hr.	hs	hr.	hr.	etres. hr	·277 hr. ·1 I·0 ·9 I·0 ·9 · · · · · ·	-38 hr6 1.0 -7 1.0 -2	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	*37	hr. I · o I · o I · o I · o I · o	hr. 1·0 1·0 ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·	hr	hr			hr.	Febr	1·85 uary, hr. 4·77 7·5 4·6 7·2 0·8 6·4	25 1923. % 577 89 54 84 9 72
Sum. Mean. 72. 1 2 3 4 5 6 7 8 9 10 11 11 11 11 11 11 11 11 11 11 11 11	Aberd	hr.	hs hr.	hr.)·7 m	etres. hr	·277 hr. ·1 1·0 ·9 1·0 ··· ··· ··· ··· ··· ··· ··· ··· ···	-388 hr6 1.0	hr. 1.0	hr. i.o i.o ·5 i.o ·4 i.o i.o	hr. 1·0 1·0 ·8 1·0 ·· ·· ·· ·· ·· ·· ·· ·· ·	hr. I·0 I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	hr76	hr			hr.	Febr	1·85 hr. 4·7 7·5 4·6 7·2 0·8 6·4	25 1923. % 577 89 54 84 9 72 11
Sum. Mean. 72. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	Aberd	hr.	hs hr.	hr.	hr	etres. hr	·277 hr. ·1 1·0 ·9 1·0	-388 hr. -6 1.0 -7 1.0 -7	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0		hr. 1.0 1.0 1.0 1.0 1.0	hr. 1·0 1·0 ·· ·· ·· ·· ·· ·· ··	hr	hr			hr.	Febr	1·85 uary, hr. 4·7 7·8 4·6 7·2 0·8 6·4	25 1923. % 577 899 544 844 9
Sum. Mean. 72. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	Aberd	hr.	hs	hr.	0·7 m	etres. hr	·277 hr. ·1 1·0 ·9 1·0	-388 hr6 1.00	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	hr. i.o i.o i.o i.o i.o i.o i.o	hr. I · 0 I	hr. I·0 I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0	hr	hr			hr.	Febr	1·85 hr. 4·7 7·5 4·6 7·2 0·8 6·4	255 1923.
Sum. Mean. 72. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	Aberd	hr.	hs	hr.	0·7 m	etres. hr	·277 hr. ·10 ·9 · · · · · · · · ·	-388 hr6 1.00 .7 1.00 .	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	hr. I·0 I·0 ·4 I·0 I·0 I·0 I·0 I·0	hr. I · 0 I · 0 · 8 I · 0 · I · 0 · I · 0 · I · 0 ·	hr. I·0 I·0 ·2 I·0 ··· ··· I·0 ··· ··· ··· ··· ··· ···	hr	hr			hr.	Febr	1·85 hr. 4·7 7·5 4·6 7·2 0·8 6·4	255 1923. % 577 899 544 844 99 11
Sum. Mean. 72. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	Aberd	hr.	hs	hr.	hr. hr.	etres. hr	·277 hr. ·10 ·9 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0	-388 hr. -6 1.0 -7 1.0	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	*37	hr. I · o I · o I · o I · o I · o	hr. I·0 I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0 ·· I·0	· · · · · · · · · · · · · · · · · · ·	hr			hr	Febr	1·85 hr. 4·7 7·5 4·6 7·2 0·8 6·4	255 1923. % 577 899 544 844 99 11
Sum. Mean. 72. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	Aberd	hr.	hs	hr.	0·7 m	etres. hr	·277 hr. ·10 ·9 · · · · · · · · ·	-388 hr6 1.00 .7 1.00 .	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	hr. I·0 I·0 ·4 I·0 I·0 I·0 I·0 I·0	hr. I · 0 I · 0 · 8 I · 0 · I · 0 · I · 0 · I · 0 ·	hr. I·0 I·0 ·2 I·0 ··· ··· I·0 ··· ··· ··· ··· ··· ···	hr	hr			hr.	Febr	1.85 hr. 4.75 4.6 7.2 0.8 6.4	255 1923. % 577 89
Sum. Mean. 72. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	Aberd	hr.	hs	hr.		etres. hr. .8 .5 .6	·277 hr. ·10 ·9 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0	-388 hr. -6 1.0 -7 1.0 -1	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	hr. i.o i.o i.o i.o i.o i.o i.o i.o i.o	hr. I · o I · o · · · · · · · · · · · · · · · · · ·	hr. I·0 I·0 ··2 I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 I·0	hr	hr			hr.	Febr	1·85 hr. 4·7 7·5 4·6 7·2 0·8 6·4	255 1923. % 577 89 54 84 84 9
Sum. Mean. 72. 1 2 3 4 5 6 7 8 9 10 11 11 11 11 11 11 11 11 11 11 11 11	Aberd	hr.	hs hr.	hr.	hr	etres. hr	.277 hr110 .99	-388 hr. -6 1.00 -7 1.00 -2	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	*37	hr. I · o I · o I · o I · o I · o	hr. I·0 I·0 I·0 I·0 I·0	hr	hr			hr.	Febr	1·85 uary, hr. 4·7.5 4·6 7·2 0·8 1·0	25 1923. % 577 89 54 84 9 72
Sum. Mean. 72. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	Aberd	hr.	hs	hr.		etres. hr. .8 .5 .6	·277 hr. ·10 ·9 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0 ·0	-388 hr. -6 1.0 -7 1.0 -1	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	hr. i.o i.o i.o i.o i.o i.o i.o i.o i.o	hr. I · o I · o · · · · · · · · · · · · · · · · · ·	hr. I·0 I·0 ··2 I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 ··· I·0 I·0	hr	hr			hr.	Febr	1·85 hr. 4·7 7·5 4·6 7·2 0·8 6·4	25 1923. % 577 89 54 84 9 72

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8 to

7 to 8.

6 to

7.

 ${\bf Mean.}$

Hour. L.A.T. 4 to

5.

5 to

3 to

·19 ·19 ·19 ·15

•06

9 to 10 to 11 to Noon 13 to 14 to 15 to 16 to 17 to 18 to 19 to 20 to 17.

Total Per cent.

Possible.

for

Day.

73. Aberdeen: h_s (height of recorder above ground) = 20.7 metres.

March, 1923.

73. <i>F</i>	berde	en :	hs (h	eignt	or re-	corde	rabo	ive gi	ouna) == 2	0·7 n	netres	S.					141	arch,	1020.
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75. <i>I</i>	Aberd	een :	hs (ł	neight	t of re	ecord	er ab	ove g	round	$\mathbf{i}) = \mathbf{i}$	20.7	metre	es.		•				May,	1923.
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Sum.		4.4	10.0	11.0	11.0	12·4	10.9	11.4	10.1	9.8	8.9	9.6	9.6	9.6	8.4	6.8	2.6	0.1	146.6	
Mean.		•14	•32	•35	.35	·40	•35	•37	.33	•32	•29	.31	.31	.31	.27	.22	.09	•00	4.73	29
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76.	Aberd	96n :	h _s =		7 met	res.											<u> </u>		June,	
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77. Aberdeen: h_s (height of recorder above ground) = 20.7 metres.

July, 1923.

77. 4	~ NOI W		115 (1	iicigii	COLL	ccorc	cr ab	0,08	Tourn	-,		metr	.						,	1923.
Day.	3 to	4 to	5 to 6.	6 to	7 to 8.	8 to 9.	9 to	io to	11 to Noon	Noon to 13.	13 to	14 to	15 to 16.	16 to	17 to 18.	18 to	19 to 20.	20 to	for	Per cent. of Possible.
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7 8	:::		·5		1					•4	•1		7						1.3	7 46
9		•6	•5	• 2	.1	·I	·I	.3	.9	1.0	1.0	• 2	• 2	'9	1.0	.9	•••		8.0	46
10	•••	• • • •	•6	1.0	1.0	.9	•5	•••	• • • •		•••	'''		'4	•••	•••	•••		4.4	25
11										•6	•8			•7	•5	•2			2.8	16
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13		•••				*							•6	.7	•4	•2			1.9	11
15		•••	•••	•••				•••	• • • •	.1	. 1	1.0	.6	.1		•••			1.9	11
16			·I			.3			.8	·r	•6	• 5	.6	1.0	.9	•4	∙8	.3	6.4	37 64
17		•8	.8	.7	•5	.9	.9	:4	.6	• 7	•9	.3	.8	·8 ·4	1.0				3·1	18
18			•5							:::		1.0	1.0	.4	.9	-8			4.3	25
20		•6	· 1	.1	⋅8	•6	1.0	1.0	8	.9	•8	1.0	1.0	•5	•••	•••			9.2	54
21		•4	.7	.9	.9	.8		.6	-8	.2									5.3	31
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23 24			• I	·8 ·2	1.0	·1	.7	·1						4					1.4	8
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26		•2	.5	.5	.8	.9	.8	.8					.5	1.0	.7	.3			7.0	42
27		.1	•5	.9	.5	•5	•2	.1		1.0	• 5			•1					4.4	27
28		•••	•••		•••	•••	•••			:::				•••						
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Sum.		3.9	6.3	7.6	11.3	8.9	9.3	9.5	10.7	11.6	10.6	7.9	9.5	10.0	8.9	5.7	2.4	0.2	134.6	
Mean.		•13	•20	.25	•36	•29	•30	.31	•35	·37	•34	•25	•31	•32	• 29	•18	•08	.02	4.34	25
70	A boud	<u> </u>															·		·	
		oon .	h	- 20 ·	7 me	tres												Α	ugust.	1923.
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1 2 3 4 5 5	hr	hr '4 '4	hr. 1·0 	hr. .4 r.o	hr5 I.0 I.0	hr. '4 '1 1.0 1.0	··· ·· ·· ·9 ·8 ·6 ··		·7 ·7 	·I ·2 ·5 ·2 ·8	 .2 .1	 .5 1.0	 .8 .8	.5 .2 .5	·3 ·3 ·8	 1.0 .6	·1 · ·4 ·6	hr	hr. 2·8 2·0 3·3 11·1 6·8 6·7 1·7	%0 17 12 20 69 43 42
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1 2 3 4 5 5 6 7 8 9 10 11 12 13	hr	hr '4 '4 ' ' ' '	hr 1·0 ·6 1·0 ·5 ·9 1·0	hr '4 1.0 '3 1.0	hr5 1.0 1.05 1.05 4	hr. '4 '1 1:0 1:0 3 '4 -8 -9 -6 -1	 .1 .9 .8 .6 .2 .9 .3 .6 .2	 	'7 '7 '3 '3 .4 .8 I.0	·12 .5 .2 .8 .2 I.0 .5 .8 .5 I.0	 .2 .1 .8 .3 .3 .9 .7 .8	 	 .8 .8 .2 .7 .7 .7 .7	.5 .2 .5 .7 .4 .3	.3 .8 .3 .3 .3 	.7 1.0 .6 .3 .7 	'1 '4 '6 '6 '	hr.	hr. 2·8 2·0 3·3 11·1 6·8 6·7 2·1 7·6 7·6 3·6 7·2	% 17 12 20 69 43 42 11 13 48 49 49 49 47
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1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15	hr	hr '4 '1	hr I·06 I·0	hr 1·0 .3 1·0	hr2 .5 I.0 I.05 I.0 I.0 I.0	hr. '4 '1 1.0 1.0 1.0 3 '4 .8 .9 .6 .1 '7	 ·1 ·9 ·8 ·6 ·9 ·3 ·6 ·2 ·9 ·3 ·6 ·2 ·9 ·8	 	·7 ··· ·7 ··· ·3 ··· ·8 ·1·0 ·5 ·1·0 ·6	·1 ·2 ·5 ·2 ·8 ·2 I·0 ·5 ·8 ·5 I·0 ·1 ·4	 .2 .1 .8 .3 .3 .9 .7 .8 .7 .6 .1	 	 .8 .8 .2 .7 .7 .7 .3 .4 1.0 .6	.5 .5 .7 .4 .3 .5 .3	.3 .8 	.7 1.0 .6 .7 .7 	·1 ·4 ·6 ·6 ·6 ·6	hr.	hr. 2·8 2·0 3·3 11·1 6·8 6·7 1·7 2·1 7·6 7·6 7·6 3·6 7·9 8·3	% 17 12 20 69 43 42 11 13 48 49 49 23 47 39 55
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1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	hr	hr '4	hr 1.0 1.0	hr 1.0	hr.	hr. '4 '1 1.0 1.0 .3 '4 .8 '9 .6 .1 '7 1.0 .2			'7 '7 '3 '3 '4 .8 I.0 '5 I.0 '6	·I		 	 	.5 .2 .57 	·3 ·3 ·8 · ·3 ·8 · ·3 · ·3 · ·1 ·3 · ·1 ·3 · ·1 ·1 ·3 · ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1	.7 1.0 .63776	·1 ·.4 ·6 · ·4 · ·6 · · · · · · · ·	hr	hr. 2·8 2·0 3·3 11·1 6·8 6·7 1·7 2·1 7·6 7·6 3·6 3·2 5·9 8·3 3·1 0·4 1·1 0·1 4·1 10·2	% 17 12 20 69 43 42 11 13 48 49 23 47 39 55 21 1 3 7 1
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	hr	hr41	hr 1.0 1.0	hr 1·0 1·0	hr25 I.00 I.0 I.0 I.0	hr. '4 '1 1.0 1.0 1.0 3 '4 .8 '9 .6 .1 '7 1.0 '3 '1 '4 1.0 '4			'7 '7 '3 '3 '4 .8 I.0 '5 I.0 '1	·I				.5 .5 .7 	.33 .831 .31 .3	.7	·1 ·.4 ·6 · ·4 · ·6 · · · · · · · ·	hr	hr. 2·8 2·0 3·3 11·1 6·8 6·7 1·7 2·1 7·6 3·6 7·6 3·6 7·6 3·1 0·4 1·1 0·1 4·1 10·2 8·1 0·2 4·6	% 17 12 20 69 43 42 11 13 48 49 49 23 47 39 55 21 1 3 7 1 1 28 69 55 1 32
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 117 18 19 20 21 22 23 24 25 26	hr	hr414	hr 1.0 1.0 1.0	hr 1·0 3 1·0	hr.	hr. '4 '1 1.0 1.0 1.0 3 '4 8 '9 6 1 '7 1.0 '3 '4 1.0 '4 1.0			·7 ·3 ·3 ·4 ·8 I·0 ·5 I·0 ·1 ·6 ·1 ·9 I·0 ·5 ·3	·1				·5 ·· ·2 ·5 ·7 ·· · · · · · · · · · · · · · · ·	.3 .3 .3 .3 .3 .3 .3 .3 .3 .3 .3 .3 .3 .	.7	·1 ·.4 ·6 · ·4 · ·6 · · · · · · · ·	hr	hr. 2·8 2·0 3·3 11·1 6·8 6·7 1·7 2·6 7·6 7·6 3·6 7·6 3·6 1·1 0·4 1·1 10·2 8·1 0·2	% 17 12 20 69 43 42 11 13 48 49 49 23 47 39 55 21 1 3 7 1
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	hr	hr '4 '1 '4	hr6 1.059 1.029	hr 1·0	hr.	hr. '4 '1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.			'7 '7 '3 '3 '4 .8 I.0 '5 I.0 '1 '6 '1 '9 I.0 '5 '3 '3 '3 '4 '5 I.0 '5 I.0 '1 '5 I.0 '1 '1 '1 '1 '1 '1 '1 '1 '1 '1 '1 '1 '1	·1 ·2 ·5 ·2 ·8 ·5 ·1 ·4 ·4 ·7				.5 .5 .7 	.3331 .3	.7	·1 ·.4 ·6 · ·4 · ·6 · · · · · · · ·	hr	hr. 2·8 2·0 3·3 11·1 6·8 6·7 1·7 2·6 7·6 7·6 3·6 7·2 5·9 8·3 3·1 0·4 1·1 0·1 4·1 10·2 8·1 10·2 8·6 1·9	% 17 12 20 69 43 42 11 13 48 49 49 23 47 39 55 21 1 3 7 1 28 69 55 1 32 49 60 13
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	hr	hr '4	hr6 1.059 1.02 .9	hr 1·0 1·0	hr	hr. '4 '1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.			·7 ·7 ·3 ·3 ·4 ·8 I.0 ·5 I.0 ·1 ·6 ·1	·I				·5 ·· ·2 ·5 ·7 ·· · · · · · · · · · · · · · · ·	·3 ·3 ·8 ·8 · ·3 ·8 · ·1 ·3 · ·1 ·3 · ·1 ·3 · ·1 ·3 · ·1 ·1 ·3 · ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1	.7	·1 ··4 ·6 ·· ·4 ·· ·6 ·· · · · · · · · · ·	hr	hr. 2·8 2·0 3·3 11·1 6·8 6·7 1·7 7·6 7·6 3·6 7·6 3·6 1·1 0·1 1·1 1·1 1·1 1·1 1·1 1·1 1·1 1·1	% 17 12 20 69 43 42 11 13 48 49 49 23 47 39 55 21 1 3 7 1 28 69 55 1 32 49 60
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 117 18 19 20 21 22 23 24 25 26 27 28 29 30	hr	hr '4	hr 1.0	hr 1.0	hr.	hr. '4 '1 1.0 1.0 1.0 '4 .8 .9 .6 .1 '7 1.0 '3 '4 1.0 '4 1.0 '9			·7 ·3 ·3 ·4 ·8 I.0 ·5 I.0 ·1 ·6 ·6 ·1 ·9 I.0 ·5 ·8 ·2 ·5	·I				·5 ·· ·2 ·5 ·7 ·· · ·4 ·3 · · · · · · · · · · · · · ·	.3 .3 .831 .31 .3	.7	·1 · ·4 ·6 · ·4 · ·6 · · · · · · · ·	hr	hr. 2·8 2·0 3·3 11·1 6·8 6·7 1·7 2·6 7·6 7·6 3·6 7·2 5·9 8·3 3·1 0·4 1·1 0·1 4·1 10·2 8·1 10·2 8·6 1·9 6·2	% 17 12 20 69 43 42 11 13 48 49 49 23 47 39 55 21 1 3 7 1 28 69 55 1 32 49 60 13 44
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	hr	hr '4	hr6 1.059 1.02 .9	hr 1·0	hr.	hr. '4 '1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.			·7 ·7 ·3 ·3 ·4 ·8 I.0 ·5 I.0 ·1 ·6 ·1	·1				·5 ·· ·2 ·5 ·7 ·· · · · · · · · · · · · · · · ·	.33 .8	.7	·1 ··4 ·6 ·· ·4 ·· ·6 ·· · · · · · · · · ·	hr	hr. 2·8 2·0 3·3 11·1 6·8 6·7 1·7 7·6 7·6 3·6 7·2 5·9 8·3 3·1 0·4 1·1 10·2 8·1 0·2 4·6 7·0 8·6 1·9 6·2	% 17 12 20 69 43 42 11 13 48 49 49 23 47 39 55 21 1 28 69 55 1 32 49 60 13 44
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	hr	hr414	hr	hr 1.0	hr	hr. '4 '1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.			'7 '7 '3 '3 '4 .8 I.0 '5 I.0 '1 '6 '1 '9 I.0 '5 I.0	·I				·5 ·· ·2 ·5 ·7 ·· ·4 ·3 ·· ·1· ·6 ·7 ·1 ·· ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1	·3 ·3 ·3 ·3 ·3 ·3 ·3 ·3 ·3 ·1 ·3 ·3 ·1 ·3 ·1 ·3 ·1 ·3 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1	.7	·1 · ·4 ·6 · ·4 · ·6 · · · · · · · ·	hr	hr. 2·8 2·0 3·3 11·1 6·8 6·7 1·7 2·16 7·6 7·6 3·6 7·2 5·9 8·3 3·1 0·4 1·1 10·2 8·1 10·2 8·1 10·2 8·1 10·2 8·1 10·2 8·1 10·2 8·6 1·9 6·2 8·9	% 17 12 20 69 43 42 11 13 48 49 49 23 47 39 55 21 1 3 7 1 28 69 55 1 32 49 60 13 44 64
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Sum.	hr. :::	hr4	hr 1.0	hr 1.0	hr	hr. '4 '1 1.0 1.0 1.0 3 '4 8 9 6 1 '7 1.0 2 '3 '4 1.0 '3 11 9 '4 1.0 '3 11 9 '9 12.9			.7733 .4 .8 1.0 .5 1.0 .6 .6	·I				·5 ·· ·2 ·5 ·7 ·· ·4 ·3 ·· ·1· ·6 ·7 ·1 ·· ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1	·3 ·3 ·3 ·3 ·3 ·3 ·3 ·3 ·3 ·1 ·3 ·3 ·1 ·3 ·1 ·3 ·1 ·3 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1	.7	·1 · ·4 ·6 · ·4 · ·6 · · · · · · · ·	hr	hr. 2·8 2·0 3·3 11·1 6·8 6·7 1·7 2·16 7·6 7·6 3·6 7·6 3·6 7·2 5·9 8·3 3·1 0·4 1·1 0·1 4·1 10·2 8·1 10·2 8·1 10·2 8·6 1·9 6·2 8·9 148·9 4·80	% 17 12 20 69 43 42 11 13 48 49 49 23 47 39 55 21 1 3 7 1 28 69 55 1 32 49 60 13 44 64
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Sum.	hr. :::	hr4	hr 1.0	hr 1.0	hr	hr. '4 '1 1.0 1.0 1.0 '4 .8 '9 .6 .1 '7 1.0 '3 '4 1.0 '4 1.0 '9 '9			.733 .4 .8 1.0 .5 1.0 .6 .6	.1				·5 ·· ·2 ·5 ·7 ·· ·1 ·4 ·3 ·· ·1 ·0 ·5 ·3 ·· ·1 ·0 ·6 ·7 ·1 ·· ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1	.3331 .3	.7	·1 ··4 ·6 ·· ·4 ·· ·6 ·· · · · · · · · · ·	hr	hr. 2·8 2·0 3·3 11·1 6·8 6·7 1·7 2·16 7·6 7·6 3·6 7·6 3·6 7·2 5·9 8·3 3·1 0·4 1·1 0·1 4·1 10·2 8·1 10·2 8·1 10·2 8·6 1·9 6·2 8·9 148·9 4·80	% 17 12 20 69 43 42 11 13 48 49 49 23 47 39 55 21 1 3 7 1 28 69 55 1 32 49 60 13 44 64 — 32

79. Aberdeen: h_s (height of recorder above ground) = 20.7 metres.

September, 1923.

Day.	3 to	4 to	5 to 6.	6 to	7 to 8.	8 to 9.	9 to	io to	11 to Noon	Noon to 13.		14 to	15 to 16.	16 to	17 to 18.	18 to	19 to	20 to	Total for Day.	Per cent. of Possible.
	4. hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	% 38
I 2	=	=	·	.0	1.0	1.0	1.0	1.0	.1	·4 ·9	1.0	1.0	1.0	1.0	•8	•6	_		5·3	72
3	—		•2	1.0	1.0	1.0	1.0	1.0	1.0	1.0	.7	•4	• • • 2					_	6·7 5·0	49 36
4 5		_							.3	.3	.5	•3	_		•••				1.3	10
6				.9	1.0	1.0	1.0	1.0	1.0	1.0	1.0	.9	.2	•2			_		9.2	68
7 8	-	_	•1	1.0	1.0	1.0	1.0	.3	.I I.0	1.0	1.0	1.0					_	_	10·1 2·5	75 19
9	_		• 2		.3	.8	1.0	1.0	1.0	• 5			∙8	·6	·I		_	_	7·1 7·8	53
10	-	_	•••	.8	1.0	1.0	1.0	1.0	.9	.9	.0		•••	.0	•••	•…	-			59
I I I 2		_			1.0	1.0	.3	1.0	1.0	 I·0	1.0	1.0	I.0	I.0	.3		_		10.3	8 79
13	=							•••					 •8	 ·8	• • • •	•••		_	 8·7	 67
14	_	_				1.0	1.0	.0	I.0 I.0	1.0	1.0	·5 ·8	.7	.9	·4 ·6			_	7.3	57
16	_					.7	.3	.2		.8	•4	• 5	.7	.9	.3				4.8	3 8
17	_				•••	• • • •					•••								0.1	 I
18	_	=							·1				• 1					_	4.1	33
20	-			•6	1.0	1.0	1.0	1.0	I . O	٠9	.9	•6	.9	1.0	•6		_	_	10.5	85
21												•1	1.0 .1	.3	•••		_	_	0·4 3·4	3 28
22 23	_	_							·4 ·8	·4 ·1	• 1		• 1		•2		-		1.3	11
24 25	_	_	_			 I .0		·6	.7 1.0	I · O · I	1.0 .1	·4 ·4	·9			_	_		6·3 4·2	53 35
									• 1	.1		.1	.1					_	0.7	6
26 27			_					•••						.1	• • • • •	_			0·1 5·1	I
28 29	_	_	_		 I·O	1.0	·5	1.0	I.0 I.0	·9 ·4	1.0				:::	_		_	5.7	44 49
30			-		.6	٠9	1.0	1.0	•6	·I	•••	• • • •		•••	.3				4.4	38
Sum.		_	0.6	7.0	12.3	15.4	16.1	16.1	16 · 4	14.6	12.7	9.3	9.5	8.8	3.8	0.4			143.3	
Mean	_		•02	•23	.41	.51	• 54	• 54	. 55	•49	•42	.31	.32	•29	•13	.02		-	4.78	38
															1	<u> </u>		<u> </u>	<u> </u>	
80.	Aberd	ieen :	hs =	= 20 ·	7 met	tres.													tober,	
_	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr. •9	hr.	hr. 1 · o	hr. 1 · o	hr. •7	hr. •4	hr.	hr.	hr.	hr.	hr. 5·8	% 50
I 2	_					1.0	1.0	•6	•9	•5	·8 ·8	• 7	•9	.1	• • • •	_	_		7·4 4·0	65 35
3 4	_		_	•••			•2	·8	1.0	1.0	.6	1.0	.1			-		-	3.7	33
5	-		-		•••	•••	•••	•••	•••	• • • •	•••	•6	•4	.1	•••				1.1	10
6	_	-	-		•••				.3	.7	·6	1.0		· I		_	_		3.4	31 21
7 8	_	_	_				• 4	1.0	·4 ·9	1.0								_	5·0 9·5	46 88
9 10	_		_		1.0	1.0	1.0	1.0	1.0	1.0 1.0	1.0	·8	1.0	.7		_	_	_	7.0	65
					.8	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	.5					9.3	87
11 12	_	_	_		.5	1.0	1.0	1.0	.9	•6	1.0	• 2				_	_	_	6·2 5·2	58 50
13 14	_	_	_		_I	1.0	·4 ·9	.6	·7 ·8	·6 ·8	·8 ·8	·8 ·7	·6 ·2						5.9	57
15			-	•••		•••	.2	•6	.7	٠2	•…		•••		•••	_	-		2.0	19
16	_						.5	.8	•9	1.0	.8	.8	1,0	•4		_			6·2 4·6	60 45
17 18	_	_					1.0	·8 ·2	.9							_		_	0.6	6
19 20	_		_	_	· · I	···	1.0	1.0	1.0	·1	1.0	1.0	1.0		_		_	_	7·4 4·1	74 41
		}									.2	.9	1.0	.5		_	_	_	4.8	48
2I 22	_	_	_	_		•6	·8	• • 5	·5	1.0	1.0	1.0	•4	•••		_		_	6.2	63
23 24	_	_	_	_		···	• 3	1.0	1.0	1.0	···8		• 5		_		-		5.4	56
25						•4	.7	1.0	1.0	1.0	•8			•••		-			4.9	52
26	—	_	_						•••	• 2	.7	•5	.5	.1	_	_	_	_	2·0 0·1	21 Î
27 28	=		_					•••		 ·7	1.0	• 1		•••		-	-	_	1.0	20 20
29 30	_	_		_			·6			·1	1.0 .1	1.0	1.0		_	_	_	=	3.6	39
	_	_					1.0	1.0	1.0	1.0	•5	1.0	1.0	•1		-	_		7.5	82
Sum.	_			0.1	4.7	10.8	14.3	17.9	18.5			16.0	13.1	5.4	0.3				139.0	
Mean.							ļ						.42	•17		_			4.48	44
· MAAAA	I —			.00	.12	.35	•46	•58	•60	.03	•59	. 52	42]		
Mean.																				Per cent.
Hour L.A.T.	3 to	4 to	5 to 6.	6 to	7 to 8.	8 to	9 to	10 to	11 to Noon	Noon	13 to	14 to	15 to 16.	16 to	17 to	18 to	19 to	20 to		Per cent. of Possible.

For periods of sixty minutes, between the exact hours of Local Apparent Time.

81. Aberdeen: hs (height of recorder above ground) = 20.7 metres.

November, 1923.

01. A	berue		113 (11	eigit	01 16	corde	abc	ove gi	ound	y = 2	20.7 1	пепе	J.		***			Nove	mber,	1923.
Day.	3 to	4 to	5 to	6 to	7 to	8 to	9 to	10 to	11 to	Noon	13 to	14 to	15 to	16 to	17 to	18 to	19 to	20 to	Total for	Per cent.
	1 hr.	5. hr.	6. hr.	1 7. 1 hr.	8. hr.	9. 1 hr.	10. hr.	11. hr.	Noon hr.	to 13.	14.	15.	16.	17.	18.	19.	20.	21.		Possible.
1			III.		111.		I.O	I.O	I · O	hr. 1.0	hr. 1.0	hr. 1 • 0	hr. •5	hr.	hr.	hr.	hr.	hr.	hr. 6·9	% 77
2	-	-		-		.8	1.0	1.0	1.0	1.0	1.0	.9	•2	• • •					6.9	77 78
3 4	_	_	_	_		1.0	1.0	•6	1.0	I.0 I.0	1.0	1.0	•2	•	_	_	_	_	6.9	78 56
5	—			—				• 3									_	_	4·9 0·3	3
6			_		 	.4	.7	.8	.7	.,	1.0	1.0	.9						6.4	-
7 8		-	_	-		-6	1.0	1.0	1.0	Ι·ο	1.0		.3					_	5.9	74 69
8 9		_	_								1.0	·8	•2				_		3.0	35
10	—	-		_		•2												_	0.4	5
11	l						`													
12		—	_		<i></i>										_	_		_		
13 14	_	_		_		 ·6	1.0	1.0	1.0	 •4			•••		_	_	_	_		
15	_													_	_				4.0	49
16							.6	1.0	1.0	1.0										
17		_	_						.3	.9	·4 ·7			_	_	_			4.0	51 34
18		-		_							1				-				0.1	I
19 20		=	_	_			1	•3	.4		·			_	_	_		_	0·8 0·9	10 12
	ļ																			
2 I 2 2		_	_		_				.3	·6	••2				_				1.2	14 20
23		-					•2	•••	1.0	.8	• 5	.9			'		_		3.4	45
24 25		_	_	_				1.0	1.0	·1 I·0	1.0			_	_	_			5.4 0.1	73 I
	1	١.,]]							Ů 1	
26 27	_	_						·4	1.0	1.0		· · I		_		_	_	_	3.4	47
28	-													_	_			_		
29 30		_	_	_	_	•••		1.0	1.0	I.0 I.0	1.0	1.0	. 1	-					3.1	44
						•••			ļ]	.7								. 3.9	55
Sum.			_		0.5	4.0	8.0	10.2	13.6	15.3	12.6	9.7	3.2			-			77:4	
Mean.					.01	.13	.27	.35	•45	· 51	.42	.32	•12						2.58	32
82.	Aberd	leen :	hs =	= 20.	7 me	tres.												Dece	mber,	
	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	%
I 2		-					•••	•4	.9	1.0	1.0	∙8					—	-	4.1	58
3	_	_	_					•4	•4	••2	···	· · · I	•••	_	_	_	_		0·0 2·5	o 36
4		-	_				•••	•••	•••		•••		• • • •	_				-		
5		_		_	_	•••	•••	•••	•••		•••	.1	•••			_		_	0.1	ı
6		-			_	•••	•5	1.0	1.0	1.0	•7		•••						4.3	61
7 8	_				_			•••			•••			_	_			_		
9		_				•••	•8	1.0	1.0	1.0	1.0		•••	_				-	4.8	72
10			_	_		•••	•••	•••				.1	•••		_			_	0.1	I
11		-					•••	•••	•••				•••			_		_		
12 13	_	_		_			···	 I·0	1.0	1.0	1.0	•4		_	_			_	 4·8	72
14														_	_					
15	-	_		_		•••	•••	•3	.7	∙8	.9	.3	•••		-				3.0	45
16	-				_			•4	•2	•4									1.0	15
17 18		_	_	_			·		1.0	I · O · I	·1		•••	_	_		_	_	0.2	3 52
19	_	-		_			.3	• 5	•8	.7	1.0	••2		_	_			_	3·4 3·5	53 28
20	-			-	_		•3	•5	٠6	•4	•••		•••	-			_		ĭ · 8	28
21			_	-	<u> </u>			•••												
22 23	_	_	_	_	=	•••		•4	1.0	1.0	•9	• 1	•••	_					3.4	52 66
23 24	=	=	_		=		•2		.6	I.O I.O	·8	·6 ·7		_	_			_	4·3 3·3	50
25	-	_		_	-			•••	···		•••	'	•••		-					
26	_	_								 						_				
27 28	_							•••		• • •						-				
28 29		_	_		_				3					_	_	_	_		1.8	27
30	-	_	_												_			_		
31	_	_															_			
	<u> </u>								•••											
Sum.							3.3	7.7	10.1	11 · 4	10.4	3.4							46.3	
Mean.	<u> -</u>				<u> </u>		.11	.25	.33	.37	•34	.11				\		_	1.49	22
Annual Totals.	0.3	12.6	38.8	16.0	77.7	89.0		T22 5	1				0_ 0						1051.6	
Locais.	0.3	13.6	20.0	46.0	1,1,1		111.2	133.2	141 4	140.9	133.9	106.9	07.8	01.4	30.0	24.3	11.7	1.1	1254.9	
			i					1	. •	1	1	ı	1	i .	I	1	1	t		
Annual								_	l			1	1	l	ł	1	1		_	-0
Annual Mean.		.04	.11	•13	•19	•24	.31	•36	.39	.39	.37	•29	• 24	.17	.11	.07	.03		3.44	28
Mean. Hour.	3 to	4 to	5 to	6 to	7 to	8 to	9 to	10 to	II to	Noon	13 to	14 to	15 to	16 to	17 to	18 to	19 to	20 to	Total	Per cent.
Mean.	ļ						<u></u>	10 to	II to	l	13 to		ļ		ļ				Total for	

† Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$): *Speed in metres per second.

83. Aberdeen:

 H_a (height of an emograph above M.S.L.) = Height of ground above

Day.		I.		2.		3.		4.		5.		6.		7.		8.	,	9.	10	о.	1	ı.	No	on.
		m/s.	- 0	m/s.	-	m/s.	-0	m/s.	- 0	m/s.	- 0	m/s.	•	m/s.		m/s.	0	m/s.		m/s.	0	m/s.	0	m/s.
1	290	2.3	280	2.6	280	5.2	290	4.9	290	4.9	270	2.6	240	1.6	260	2.6	260	3.3	280	4.3	260	3.9	270	3.9
2	190	4.6	190	5.9	180	6.6	18o	7.2	190	7.2	190	6.2	180	5.9	190	5.6	200	5.6	200	5.9	210	6.2	240	6.2
3	220	7.2	230	8.5	230	9.8	220	9.2	230	7.5	240	6.6	230	4.3	220	4.3	210	3.9	210	6.6	210	6.2	220	4.6
4	310	7.5	300	6.9	310	7.9	310	6.9	310	6.9	310	6.9	310	6.2	310	6.2	290	2.6	270	2.3	290	3.0	290	3.6
5	190	3.3	190	5.2	190	3.9	180	3.9	190	3.3	170	6.2	170	6.9	160	6.6	170	6.9	160	6.9	160	7.9	170	6.9
6	280	2.0	_	1.3	_	1.3	230	2.0	_	1.3	250	1.6	270	2.3	270	2.0	250	2.6		1.3	260	2.0	260	2.0
7	220	5.9	210	3.9	210	3.9	200	4.3	200	4.9	210	4.6	210	5.5	220	4.3	220	4.6	230	2.0		1.0	_	0.3
8	200	5.6	200	5.6	200	6.9	220	6.6	220	5.9	250	5.2	270	3.9	240	3.0	230	3.9	250	3.3	250	4.6	260	3.3
9	190	5.2	180	4.3	180	7.5	190	7.5	190	6.2	200	5.2	210	5.9	240	5.2	240	5.6	230	6.9	210	7.2	220	9.2
10	220	11.8	210	9.5	210	8.9	210	7.2	220	5.6	260	6.9	260	7.2	260	5.6	270	4.9	280	10.2	300	12.1	300	11.5
II	300	9.8	300	7.5	300	8.9	310	9.8	310	9.8	300	9.8	300	9.8	300	8.2	290	7.5	300	12.5	330	6.6	340	4.6
12	310	3.0	300	2.6	300	3.6	300	2.6	320	2.3	320	3.6	320	3.6	300	3.0	310	3.3	310	3.3	320	4.3	320	3.3
13	270	1.6		1.3		0.7		1.3	<u> </u>	0.7		1.0	_	1.3		0.7	210	2.3	210	2.6	210	4.9	210	4.9
14	220	5.3	220	6.9	220	4.6	210	4.9	210	5.2	230	5.2	280	6.6	290	6.6	290	5.9	290	5.2	290	7.9	280	5.9
15	290	12.8	300	12.5	240	13.1	300	9.8	290	9.5	300	7.2	290	8.2	300	11.8	300	8.9	300	8.9	300	6.9	300	6.2
16	310	2.0	320	2.6	-	1.3	_	1.3		1.3		1.3	310	1.6		0.7		0.7	_	1.0	220	1.6	220	2.6
17	210	2.6	200	2.0	210	1.6	190	1.6	210	3.3	210	2.0	_	1.3		1.0	_	1.3	220	3.0	220	3.9	220	3.9
18		1.0	280	1.6	290	2.0	280	2.6	280	1.6	280	2.0	290	3.0	300	3.0	300	3.6	290	3.3	300	5.3	260	1.6
19	200	1.6	230	2.0	240	1.6	240	2.0	220	1.6	210	1.6	200	2.6	220	3.3	200	3.0	220	6.6	200	7.2	210	8.2
20	290	6.9	290	6.9	300	9.5	300	9.8	310	8.9	310	7.5	310	10.5	350	8.9	350	7.9	340	6.6	340	9.8	330	8.5
21	270	1.6	260	3.0	240	3.3	240	2.3	230	2.0	210	2.6	210	4.9	210	4.6	220	2.6	250	2.3	270	4.3	270	5.2
22	280	7.2	290	5.6	270	6.6	270	5.2	260	6.2	260	5.9	260	5.6	260	7.2	270	5.2	280	6.2	300	5.6	330	6.6
23	290	3.3	300	2.6	280	2.0	260	3.3	260	2.6	250	2.6	230	3.6	230	3.0	220	5.6	230	4.9	220	3.0	200	3.6
24	270 260	4.9	280	5.9	280	6.6	270	7.9	270	6.9	270	6.6	250	4.6		0.7	260	2.6	260	3.0	290	3.9	280	3.3
25	200	4.6	230	2.3	250	3.0	240	2.6	240	3.0	210	3.6	220	3.6	230	4.6	260	5.2	230	3.9	240	3.0	250	6.2
2 6	260	5.9	260	5.9	270	4.9	250	2.6	240	4.9	230	4.3	230	3.6	230	4.3	240	5.2	250	5.6	250	5.6	260	4.6
27	_	1.3	240	2.6	250	3.6	260	3.3	260	4.9	250	4.3	210	2.6	230	3.0	240	3.6	270	3.6	280	5.2	290	5.2
28	280	2.3	250	1.6	280	1.6	-	1.0	280	1.6		1.0	_	1.0	330	2.3	320	2.3	300	2.0		1.3		0.7
29	220	3.0	230	2.3		0.7	_	0.3	_	0.7	_	1.0	_	1.0		1.3	310	2.0	310	2.3	330	2.6	40	4.6
30	140	6.2	150	5.6	160	4.3	170	3.3	180	3.9	190	3.0	190	3.6	190	4.3	190	3.3	200	3.9	200	3.3	190	3.3
31	300	3.6	240	3.6	270	1.6		1.3	250	2.6	260	2.0		1.0	240	1.6		1.0	230	2.0	220	2.3	180	2.3
Mean	_	4.7		4.5	_	4.7	_	4.5		4.4		4.2		4.3		4.2		4.1		4.6		4.8	_	4.7

84. Aberdeen: $H_a = 14 \text{ metres} + 23 \text{ metres}$.

3 26	240 260 210	m/s. 8·9 4·3	250	m/s.	260	m/s. 8·9	-6-	m/s.	_ '	m/s.		m/s.		m/s.		m/s.		m/s.		m/s.		m/s.	ſ	m/s.
3 26	60	- 1				0.01	260	7.2	260	9.8	260	5.9	270	5.6	260	7:5	260	7.2	250	7:5	250	8.2	250	7.2
1 3 1 -	OI		250	5.6	270	6.2	300	10.8	290	9.5	280	6.9	28o	8.5	260	5.6	260	5.6	260	5.6	260	5.9	260	6.6
1 30		4.3	220	2.6	240	2.6	250	3.3	240	5.9	250	6.9	240	5.6	250	6.6	260	7.2	250	7.5	260	7.9	270	5.6
	00	2.0	300	3.3	300	3.6	290	2.6	290	3.0	290	3.6	280	2.6	280	3.3	290	3.9	290	3.0	300	2.3	290	3.0
5 22	20	5.9	210	5.6	200	4.6	200	5.6	190	5.9	190	4.9	190	6.9	200	6.9	220	6.6	220	6.9	220	2.6	240	6.2
															ľ	ĺ	1		i	1	l		1	
6 19	90	6.9	190	5.6	190	6.6	190	7.2	180	8.5	190	5.2	190	6.9	190	6.2	180	8.2	180	10.2	180	9.5	190	8.9
	90	4.6	180	6.6	190	5.2	210	5.9	210	3.6	210	3.3	200	2.6	180	5.2	170	6.9	160	10.2	150	10.2	150	15.4
8 17	70	6.9	170	9.5	170	6.9	160	6.9	140	8.5	160	10.3	150	9.5	150	9.2	150	8.5	160	11.8	170	8.9	170	6.6
9 21	IO	1.6	220	1.0	220	1.6	220	2.0	220	1.6		1.3	210	1.6	200	2.0	230	1.6	220	2.6	210	1.6	200	1.6
10 14	40	8.5	140	10.2	140	10.2	140	10.8	140	9.8	140	12.5	140	11.8	140	14.4	140	13.4	140	12.1	140	14.1	140	13.4
	1	ı											i i		l				l		l		i	
: I	• 1	11.1	140	9.5	140	9.8	- 1	10.2	130	11.8	130	12.5	130	13.1	130	12.5	130	15.1	130	12.1	130	13.4	130	12.8
	30 1	12.1	-	10.8	130	12.1	130	9.5	150	7.2	150	5.6	150	5.3	150	4.6	150	3.9	150	3.9	160	3.0	170	2.6
1 -	40	9.2	140	8.2	140	8.2	140	7.9	150	7.5	150	7.9	140	8.9	140	8.2	140	II.I	140	8.5	140	10.2	150	7.9
	3 -	8.2	150	7.2	150	7.9	150	7.2	150	6.9	150	6:2	150	6.9	150	6.9	160	5.9	150	4.9	150	6.6	150	6.2
15 16	60	5.6	160	5.2	150	5.6	150	5.2	150	5.2	150	4.9	150	5.2	150	5.3	150	5.2	150	5.9	150	7.9	150	6.6
													l		1.		l	0				- 0		
	50	9.2	150	7.9	150	9.5	140	9.8	140	10.8	140	8.9	150	10.2	150	8.5	140	11.8	140	9.8	140	10.8	140	8.9
1 2 1		9.5	140	8.2	150	9.2	140	7.3	140	8.5	140	7.5	140	7.9	140	7.2	130	8.9	130	7.2	140	8.9	140	7.9
		9.5	170	8.2	170	9.8	150	9.8	160	10.5	160	10.8	150	12.5	150	10.8	150	10.2	150	12.5	160	10.8	160	11.1
	50	7.5	100	6.2	160	6.2	160	5.9	160	5.2	170	5.6	160	4.9	160	4.3	160	5.2	170	4.6	170	4.3	170	3.0
20 16	60	2.3	170	3.3	170	2.6	170	3.3	170	3.3	170	3.3	170	4.3	170	3.9	180	3.9	180	3.9	210	3.3	200	2.3
			-6-				-6-																	
		7.5	160	9.5	150	9.2	160	9.8	170	7.9	_	11.2	140	12.1	150	10.3	150	11.1	150	10.2		10.2	150	12.5
1	- 1	8.5	140	8.2	140	6.9	140	7.2	140	7.5	140	7.2	150	6.6	140	8.2	140	7.9	140	7.9	150	7.5	150	7.5
	40	1.6	330	2.3	330	2.6	330	2.6	310	3.3	310	3.3	300	3.3	290	2.0	290	1.3	290	1.6	300	1.6	_	0.7
	90	5.2	90	5.9	90	4.3	90	4.3	80	2.6	120	3.6	140	3.6	140	4.3	140	3.6	110	5.6	110	5·2 8·2	110	5·6 8·2
25 13	30	6.6	140	7.9	130	6.9	130	7.9	120	8.5	130	7.9	130	7.9	120	8.5	120	9.5	120	9.2	120	0.2	130	0.2
26 12	20	آ ہے		ا ا	T.40	4.0		2.0	* 40	2.0	700	2.6	100	.	7.00	6.6	7.00	10.2	120	10.2	110	12.8	7.10	12.1
· 1	20	9.8	130	5.9	140	4.9	140	3·9 9·8	140	3.9	120	2.6	120	7.2	130		120	10·2 12·8	110	10.8		10.8	110	9·8
1 4		13.8	80	10.5	110 80	12.1	110 80	-		11.8	110 80	9·8 8·2	100 80	8.9	100 80	10·2 6·6	100 80		80	, ,	80	1 1	80	
20 (00 1	10.5	0U	7.5	80	9.2	80	5.9	90	9.2	80	0.2	80	0.9	80	0.0	80	5.9		5.2	- 00	5.2		5.2
Mean		7.2		6.9	_	6.9		6.8		7.1		6.7		7.2		7.0		7.6		7.6	_	7.6	_	7.4
																				<u> </u>				
CMT		Ī		J		j		1				_		I				1					3.7	
G.M.T.	I.	.	2	2.	3	3.	4	<u>ا</u> ا		5 . [(5.	7	, l	8	3.	ç	9. ∤	1	ю.	I	I.	No	on.
<u> </u>						<u>l</u>		1						1										

[†] Directions obtained from records of the Dines Tube Anemograph. * Speeds obtained from records of the Robinson Cup Anemograph.

WIND: DIRECTION AND SPEED.

Averages for periods of sixty minutes centred at the exact hours, Greenwich Mean Time.

M.S.L. $+ h_a$ (height of anemograph above ground) = 14 metres + 23 metres.

January, 1923.

3	13.	1	4.	I	5.	I	6.	1	7.	1	8.	1	9.	2	o.	2	ı.	2	22.	2	3.	2	4.	Mean	Day.
	m/s.		m/s.	0	m/s.	- 0	m/s.		m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	m/s.	
280	4.3	260	3.6	270	2.6	250	2.3	250	1.6		1.3		1.3	220	1.6		1.3	190	2.0	210	2.0	190	3.6	2.9	I
230	3.0	210	4.3	210	4.6	190	5.6	200	6.6	200	6.9	190	6.2	190	7.9	200	6.6	210	6.9	220	7.5	220	7.2	6.0	2
220	5.6	220	5.6	220	4.9	220	3.0	250	2.6	290	3.6	300	5.6	300	5.6	310	7.5	310	6.9	310	7.2	300	6.6	6.0	3
280	2.6	270	2.3	240	2.3	230	2.3	240	2.0	240	2.3	240	1.6	230	2.3		0.7	220	2.3	200	5.3	210	3.0	3.9	4
170	6.9	180	6.2	190	4.3	210	3.3	290	5.5	320	4.9	320	3.3	320	3.0	310	2.6	290	2.6	290	2.3	290	2.6	4.8	5
260	3.0	260	2.0	_	1.3	\	1.3	210	1.6	220	1.6	220	2.0	210	1.6	200	3.3	210	3.3	210	3.0	230	5.6	2.1	6
250	2.3		0.3		1.3	220	2.3	200	1.6	200	2.0	200	2.0		0.3	180	2.6	190	2.6	180	3.0	200	3.6	2.9	7 8
260	3.9	280	3.3	260	5.2	260	4.6	260	4.3	230	3.3	210	2.6		1.3	_	1.3	220	1.6	180	2.0	200	3.6	3.9	i
230	9.2	220	10.2	230	10.2	220	9.2	210	9.5	220	8.2	210	8.9	210	7.5	200	11.1	210	11.1	210	11.1	210	10.2	7·9 9·4	9
310	12.1	320	12.8	320	12.1	320	11.1	320	11.8	320	6.9	310	8.5	310	9.2	310	11.5	310	7.9	310	10.2	300	8.9	9.4	10
320	5.6	320	4.9	320	3.9	320	4.9	320	4.3	320	4.3	320	3.6	320	4.3	310	3.3	320	3.6	310	3.0	320	3.3	6.5	11
310	4.3	300	3.3	300	2.3	300	2.0	290	2.3	300	2.6	300	2.6	300	2.3	300	2.3		1.3		1.0	250	2.0	2.8	12
220	4.6	210	2.0	210	2.3	220	2.6	270	3.3	290	3.0	300	2.0	280	3.0	280	2.0	250	6.6	230	7.9	220	6.2	2.8	13
280	7.2	270	5.9	270	7.5	280	6.9	270	6.9	280	7.2	270	7.5	280	7.2	280	8.5	280	7.5	290	11.2	290	10.5	6.8	14
290	5.2	300	8.9	310	5.9	290	4.6	300	4.3	290	4.3	310	4.9	310	5.9	300	3.6	320	3.9	310	3.6	330	2.3	7:4	15
210	2.6	200	2.6	210	3.3	210	2.3	210	3.3	220	3.3	210	3.3	210	3.0	210	3.0	210	2.3	190	3.0	190	3.3	2 · 2	16
210	3.3	210	2.0	230	2.0	250	2.0	270	1.6		1.3		1.3	300	2.0	_	1.3	290	3.3	300	3.3	310	2.0	2 · 2	17
270	3.0		1.3	220	1.6	230	2.3	220	2.0	230	2.6	220	1.6	240	2.3	240	3.0	230	3.6	250	2.3	260	2.6	2 3	
220	7.5	250	7.9	260	8.2	270	9.2	280	11.1	280	12.5	300	15.1	300	13.4	310	15.1	310	11.8	300	11.8	300 280	6.9	7.1	19 20
340	9.8	330	9.5	340	8.2	330	6.9	330	6.6	330	5.9	320	5.2	290	3.3	290	3.3	290	3 3	260	2.3	200	3.0	7·1	20
260	3.6	290	4.9	290	7.5	260	6.2	270	4.9	270	6.2	280	4.9	290	5.9	280	4.3	280	3.9	290	7.2	290	8.5	4.3	21
330	6.6	330	6.9	320	8.9	320	7.2	320	5.9	310	8.2	320	7.5	320	9.2	320	8.2	330	7.2	330	8.2	330	4.9	6.8	22
200	4.9	210	3.9	230	6.9	230	8.9	220	6.2	200	3.0	180	3.6	250	9.2	260	6.6	260	6.6	260	7.9	260	8.2	4.8	23
270	3.6	290	5.6	290	5.2	290	6.2	270	3.3	290	2.3	290	3.9	290	4.3	240	3.0	270	4.9	250	4.3	250	3.0	4.5	24
230	3.3	240	3.0	260	6.2	260	5.2	260	3.9	250	4.6	250	3.9	250	3.9	250	5.3	260	6.6	260	7.2	260	0.2	4.3	25
260	5.2	230	2.6	210	2.3	250	4.3	250	4.9	260	6.6	260	4.9	250	6.6	240	4.9	240	3.6	230	3.9	210	2.3	4.7	26
310	4.3	320	3.0	330	3.6	330	4.3	330	3.0	330	3.9	320	3.6	320	3.9	310	3.0	310	2.6	300	2.3	300	2.3	3.5	27
_	0.0		0.7	160	2.0	200	3.6	220	3.0	230	3.3	240	3.3	270	3.0	260	3.9	240	3.0	210	3.3	210	6.0	2.1	20
70	5.2	70	4.9	70	4.6	80	4.6	90	6.2	110	6.6	110	7.9	110	8.5	120	9.8	120	7.5	120	8.9	140 280	2.6	4·2 3·0	30
	1.3	220	2.0	210	2.0		1.3		0.7		0.7	250	1.6		1.3	_	1.3	260	3.9	270	4.6	200	2.0	135	35
200	3.3	190	2.3	190	2.3	220	5.2	230	5.6	220	4.6	210	5.6	200	3.6	220	2.3	230	8.2	240	9.5	230	6.9	3.4	31
	4.8	_	4.5		4.7	_	4.7		4.5	-	4.2	-	4.2		4.7	-	4.7	_	4.9	-	5.4	-	4.9	4.6	

February, 1923.

260 260	m/s. 4·3 5·6	250 260	m/s. 4·6 5·6	280 260	m/s. 2·3 4·3	240 260	m/s. 4·6 3·9	250 260	m/s. 6·9 3·6	230 210	m/s. 6·9 2·3	230 220	m/s. 6·2 1·6	220 220	m/s. 5·2 1·6	210 220	m/s. 3·9 2·0	210 200	m/s. 4·6 3·3	230 200	m/s. 5·6 3·0	250 200	m/s. 6·6 2·3	m/s. 6·5 5·1	I 2
290 220	3·3 6·2	310 290 210	3·9 3·3 6·2	280 250 200	3·3 2·0 4·9	320 230 190	4·3 2·3 4·6	300 230 210	2·3 3·6 5·2	310 240 180	2·3 3·6 4·3	320 240 190	3·9 4·9	300 230 190	3.3	310 210 190	3·3 3·0 5·2	300 210 210	3·0 3·3 6·2	310 210 200	4·3 5·9 5·9	310 220 190	3·9 4·6 5·6	3·2 5·4	3 4 5
190 170 280 210 140	7·2 11·5 5·9 2·3 12·8	320 190	7·2 14·8 5·9 3·0 12·5	190 170 320 180 140	5·9 10·2 3·9 2·6 12·8	190 180 320 160 140	7·2 8·9 3·3 3·0 11·8	190 180 310 160 140	7·2 5·2 2·3 1·6 13·1	180 190 300 160 140	7·2 5·2 1·6 3·0	180 190 270 140 140	6·2 4·9 2·0 2·3 12·1	180 190 150 140	7·2 5·6 1·0 5·6	180 190 240 150 140	4·9 4·6 2·3 8·2 13·4	180 190 230 150 140	6·2 3·9 3·0 8·5	190 180 230 140 140	5·9 4·9 2·3 7·9	200 170 220 140 140	4·3 6·6 2·0 9·5 10·5	7·0 6·9 5·9 3·1 12·0	6 7 8 9 10
130 170 150 150 150	12·8 3·3 8·2 6·6 6·6	130 170 150 150 160	10·8 3·3 8·5 5·9 6·6	130 150 150 150 150	12·8 3·6 8·9 6·2 8·2	130 150 150 150 150	10·5 3·0 7·9 5·6 7·2	130 150 150 150 160	12·1 1·6 8·2 6·6 8·2	130 130 150 150 150	9·8 2·3 8·2 4·6 7·2	130 120 150 160 150	11·5 5·2 8·5 5·2 7·9	130 140 150 170 150	10·5 7·2 7·9 4·3 8·5	130 140 150 160 150	7·9 9·2 5·6 9·5	130 140 150 160 150	10·5 5·2 8·5 5·2 7·5	130 140 150 150 150	11·5 6·9 8·5 7·2 9·2	130 140 160 150 150	7·5 7·2 4·9 7·9	11·7 5·8 8·5 6·3 6·7	11 12 13 14 15
150 150 150 170 220	9·2 8·5 Io·5 3·9 2·3	150 150 150 160 220	7·5 7·2 12·5 3·6 2·6	150 150 150 170 220	8·5 8·2 12·8 3·6 3·0	150 160 150 160 190	6·9 7·2 11·1 3·3 2·6	150 160 150 160 200	6·9 8·2 10·2 3·3 2·6	150 160 150 160 180	6·6 6·2 11·1 3·9 4·3	140 160 150 160 170	7·5 7·9 10·2 3·9 5·6	140 160 150 160 160	7·9 8·2 9·8 3·3 6·6	140 160 150 170 170	10·2 8·2 9·2 3·0 6·2	140 170 150 160 160	8·9 7·5 7·9 3·3 7·5	140 160 150 160 170	11·5 9·2 8·5 3·9 6·2	140 160 150 160 170	9·2 8·2 8·2 3·6 7·9	9·0 8·1 10·4 4·5 3·9	16 17 18 19 20
150 150 — 120 130	11·1 6·9 0·3 7·9 9·2	150 150 120 130	10·5 7·2 1·0 6·6 7·2	150 150 80 120 120	11·5 6·6 2·0 7·2 8·9	150 140 — 120 130	10·8 6·2 1·3 7·5 7·5	150 150 150 120 130	10·5 5·9 1·6 6·9 9·5	150 130 150 110 120	9·8 6·2 3·0 6·6 8·5	150 130 130 110 120	9·8 7·2 4·3 6·6 9·8	150 120 120 110 120	9·8 6·2 4·3 6·6 9·2	150 130 120 110 120	9·8 5·2 3·9 7·5 10·2	150 100 120 120 120	8·2 4·6 5·2 8·2 9·5	150 90 100 120 120	9·5 4·9 3·9 7·5 11·8	150 80 90 120 120	9·2 2·3 4·6 6·9 II·I	10·1 6·8 2·5 5·8 8·6	21 22 23 24 25
110 80	15·7 10·8 4·3	100 90	13·4 9·2 3·6	90 80	14·8 12·1 5·2	110 90 80	14·8 10·2 4·6	110 80 70	17·0 13·8 6·2	110 80 70	15·7 11·5 5·2	110 80 60	18·0 11·5 6·9	110 80 60	14·8 9·8 5·6	110 80 60	16·7 11·8 6·9	90 60	12·5 11·8 4·9	110 90 50	14·1 11·5 6·2	90 40		6·5	26 27 28
_	7·1		6.9		7.0	_	6.5		6.8		6.4		6.9		6.7		7.3		6.8		7.5		6.9	7.0	
1	3.	1	4.	1	5.	1	16.	1	7.	I	8.	I	9.	2	o.	2	Ι.	2	22.	2	3.	2	4.	Mean	Day.

[†] Directions obtained from records of the Dines Tube Anemograph. * Speeds obtained from records of the Robinson Cup Anemograph.

WIND: DIRECTION AND SPEED.

† Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$): *Speed in metres per second.

Aberdeen:

 H_a (height of anemograph above M.S.L.) = Height of ground above

Day.	1	.	2		3	3.		4.		5.		6.		7.		3.	,	9.	1	ю.]	ı.	No	oon.
	0	m/s	٥	m/s	0	m/s	۰	m/s	°	m/s	۰	m/s	۰	m/s	i °	m/s	•	m/s	0	m/s	•	m/s	i °	m/s
1	50	5.9	40	4.6	40	6.2	40	4.3	30	4.3	20	2.3	340	2.3	350	2.3	350	2.0	350	2.0		1.3	30	3.3
2	110	4.3	110	5.9	120	6.2	110	7.9	110	7.9	110	7.5	140	4.6	130	5.6	120	6.6	110	6.9	110	8.2	150	3.3
3	180	1.6		1.3	170	1.6	170	1.6	_	1.0		0.3		0.3		0.7		0.3		0.3		0.3		0.3
4	340	2.3	330	2.3	310	2.3	300	3.0	300	3.0	310	3.3	310	3.9	310	3.3	310	3.0	320	3.9	320	4.9	330	3.0
5	190	2.6	180	2.6	180	3.6	200	2.3	170	4.3	170	5.2	170	5.2	180	5.5	180	6.2	180	4.9	180	6.6	180	6.2
6	230	4.3	230	3.9	220	3.0	210	2.0	200	2.0	200	2.0	200	1.6	210	3.9	200	3.3	180	3.9	170	3.3	180	3.6
7	140	1.6		1.3		1.0		1.0		1.3	-	1.0		1.0	340	1.6	340	2.0		1.3		1.3	10	2.3
8	350	4.9	350	3.6	360	4.3	350	3.9	350	4.6	350	4.9	360	4.3	360	4.3	360	3.0	20	2.6	20	3.0	20	3.6
9	310	3.0	320	2.0	320	3.3	310	2.0	310	2.6	320	2.6	320	2.0	330	2.3	340	2.3	10	2.3	40	3.0	80	2.3
10	200	1.6	170	1.6	170	1.6		1.3		1.0		1.0	140	2.6	130	3.9	150	3.0	150	4.3	160	3.6	170	3.3
II	140	6.6	140	7.2	140	5.6	150	6.2	150	5.6	150	4.9	150	5.2	150	5.2	160	4.3	160	4.9	160	5.6	160	4.9
12	160	6.2	160	5.9	160	7.5	160	6.9	160	7.9	160	6.6	160	8.5	160	7.5	160	8.2	160	7.5	160	8.9	160	7.9
13	180	6.6	180	6.9	180	7.5	200	4.3	200	2.6	210	3.0	210	2.6	230	2.6	260	2.6	290	5.2	290	5.9	290	5.2
14	280	2.0	290	2.3	280	2.6	280	1.6	280	2.0	290	2.3	290	2.6	290	2.6	290	2.3		1.0	_	1.3	70	2.0
15		0.3		0.7		0.7	_	I.0	320	1.6	320	1.6	40	2.0	70	3.9	70	3.9	90	4.9	90	4.6	80	5.2
16	00	2.0	100	2.0	100	2.0	00	2.2	100	2.6	100	1.6	90	1.6	100	1.6	110	2.6	100	2.0	_	1.3		4.3
	90	3.0	100	3.0	100 310	3.0	90 310	2.3		1.0		0.3	90	0.7		0.3		0.7	80	2.6	100	2.3	120	2.6
17 18		1.3	310	2.3	310	I O	310	0.7		1.0		1.0	170	1.6	l	1.0		1.0		1.3	130	2.6	160	2.6
19		0.7		1.0		0.3		1.0	230	1.6		1.3	1/0	1.0		0.7		0.0		0.3	100	1.6	90	1.6
20		0.7		0.7	_	0.7		1.3		1.3		1.3		0.0	90	1.6	90	2.6	100	2.6	90	1.6	90	2.6
		,		,					1															
21		0.7	_	0.7	_	1.0		0.7		1.3	290	1.6	290	2.6	300	2.6	300	2.0		1.3	100	1.6	110	3.0
22	300	2.3	290	2.6	290	2.3	290	1.6	290	2.3	300	2.6	300 80	3.0	300 110	3.0	300 80	3.6	300	2.3	20 90	2.0	40	3.0
23	40	1.6	50	2.0	240	0.3	240	0.3	80	2.3	90	2.3		2.6			320	6.6	310	6.2	300	7.5	90 300	9.5
24	350	1.6	350	2.3	340	2.3	340	2.6	330 270	3.6	320 250	1.6	320	4·9 0·7	320	1.0	320	0.3	190	2.6	180	3.0	180	3.6
25	240	2.3	_	1.0		0.3		1.3	2/0	1.0	250	1.0				1 0		0 3	190	20	100	, ,	100	3 0
26	240	5.6	200	2.0	210	2.3	200	3.6		1.3	250	2.3	250	1.6	230	1.6	140	1.6	180	3.0	150	3.6	170	3.6
27	170	2.3	170	3.0	180	2.3	160	2.3	160	3.0	150	3.6	160	3.9	150	2.6		1.3	170	2.0	170	2.3	80	1.6
28	—	1.3	—	1.0	160	2.0	150	2.6	[1.3	160	1.6		1.3	_	1.0	_	1.0	100	2.0	120	3.0	110	2.6
29		0.3	_	1.3		1.0		0.3	_	0.3		1.0		0.7		1.0		0.7		1.0	160	3.6	160	3.3
30	170	2.3	180	2.0	170	1.6	_	1.3	130	2.0	140	3.0	170	2.0	170	1.6	160	2.0	170	3.0	170	2.3	160	2.3
31		1.3		1.3	170	1.6		1.0		1.3		1.0		1.3	_	1.0		1.3	130	2.3	140	3.6	140	2.6
Mean		2.6		2.6		2.6		2.4		2.6		2.6		2.5		2.7		2.6		3.0		3.4		3.4
Mean		2.0	_	2.0		2.0		~ -≖		2.0		2.0		- 3		~ /				ا		JŦ		3 1

86. Aberdeen: $H_a = 14 \text{ metres} + 23 \text{ metres}$.

G.M.T.	1		2		3		4		5	•	6		7	•	8		9		10).	I	r.	No	on.
Mean	_	4.2		4.3		4.4		4.4		4.4	_	4.6	_	4.6	-	5.2	_	5.3	_	5.4	_	5·I		5.3
29 30	270 —	1.9	210	3.0	260 —	3.0	250 —	2·3 0·3	240 —	0·3	240	3·6 0·3	260 120	2.0	270 140	3·6 2·6	260 120	3.0	270 110	3.0	270 110	3.6	270 110	2.0
26 27 28	210 320 290	3·9 8·2 3·6	200 320 290	3·9 5·6 2·6	210 310 270	3·0 4·9 1·6	200 300 	3·0 4·3 1·0	210 290 270	2·0 5·2 1·6	230 290	2·3 6·2 0·7	290 300 —	2·3 6·6 1·0	300 300 160	2·6 7·9 2·6	330 300 150	7·2 3·3	330 290 160	1·6 6·6 5·2	110 280 170	2·0 5·2 4·6	280 170	5·9 4·9
25	180	6.2	160	6.9	150	8.2	150	9.2	160	9.2	160	8.9	160	8.5	170	6.2	200	4.9	210	3.3	210	3.9	220	4.3
23 24	250 300	2·6 7·2	310	3.6	280 300	3·3 5·2	300 290	5·9 4·9	300 300	5·2 5·2	300 300	4·6 7·5	340 300	4·6 7·2	350 300	5·2 7·9	330 300	8.2	360 300	5·6 6·6	330 340	5·6 5·6	330 330	5.2
2 I 22	360 330	5·6 3·0	330	7·2 3·0	10 320	7·2 2·6	10 320	7·2 3·0	10 330	6.6 3.6	10 340	6·9 2·0	10 330	7·5 3·3	20 330	3.6	20 330	3·3	50 340	3.0	50 20	3.3	50 40	3.6
20	10	2.3	50	3.0	30	2.0	_	1.3	350	1.6	340	2.0	360	1.6	20	3.0	360	3.0	10	3.9	10	4.6	20	4.6
18 19	140 130	3.6	140 110	3.3	140 110	1·6	140 90	1·6 4·6	130 80	4.6	120 110	4·3 3·6	110	4·9 3·9	120 90	5.9	120 90	6·6 4·6	120 100	5.9	120 110	3.3	120 120	3·6
16 17	 180	1.0	 180	1.3	 180	1.3	 200	1.3	— 190	0.7	_	1.0	 180	0.3	 170	3.3	 160	0·3 5·2	80 170	1·6 4·6	160 170	2·6 4·6	150 170	3·9 4·6
15	_	0.3	-	1.0	50	2.0	90	1.6	80	2.3	50	1.6	40	1.6	30	1.6	40	3.0	60	3.0	60	3.0	50	4.3
13 14	30	3.3	40 130	3.0	40 130	3.9	60 130	3.0	130 120	3·0 5·6	130 130	3·6 5·6	160 130	3.6	190 120	3.3	200 130	3.0	200 120	3.9	110	3.6	180 130	4.3
11 12	120	5·9 0·7	110	4.9	100	1·3	100	5.6	110 40	6.9	110 30	7.2	120 40	7·2 3·3	120 40	8.2	120 40	7.5 3.0	110 40	7·5 3·3	100 60	3.3	110 80	7.2
10	60	9.8	60	11.5	60	10.2	50	10.2	50	9.8	40	12.1	50	13.4	60	12.8	60	10.2	80	9.8	100	8.5	110	7.2
8 9	130 130	8·2 5·9	130	6·9 5·6	130 130	7.5	130 140	7·9 5·2	130 140	3.3	140 130	7.2	140	4.6	140 120	5.6	140	5.9	120	6.2	120	5.6	011	5.9
7	120	8.5	110	7.9	120	6.6	120	7.2	130	5.9	120	6.6	130	4.9	120	8.2	120	6.9	120 140	6·9 8·5	120 140	7·5 8·2	130 140	7·5 8·9
6	130	8.2	130	6.6	130	7.9	130	6.9	120	7.5	120	7.2	120	8.2	120	9.5	130	8.5	130	8.2	120	7.5	130	7.5
4 5	140 150	3.0	150 160	4·6 3·3	150 150	4·9 3·9	140 140	3·9 5·6	140 140	3.9	140 140	5.6	160 140	3.9	140 140	4·6 6·9	140 130	5·9 6·2	140 130	7.9	140 130	6.6	140 130	6·9 7·2
3	160	3.3	160	4·9 3·3	150 170	3.3	140 180	3.6	170	2.3	170	2.6	180	3.0	180	3.3	170	3.3	170	4.6	170	4.3	170	3.6
I 2	120 150	8.9	120 150	9.2	120	8.9	120	9.2	120 150	9.2	120 150	8·9 3·9	120 140	8·2 3·0	120 140	7·9	120 140	3.6	130 150	3.9	130 140	7.5	130 140	7.5
	٥	m/s.	°	m/s.	°	m/s.	٥	m/s.	٥	m/s.	٥	m/s.	°	m/s.	°	m/s.	•	m/s.	°	m/s.	°	m/s.	°	m /s.

[†] Directions obtained from records of the Dines Tube Anemograph. * Speeds obtained from records of the Robinson Cup Anemograph.

Averages for periods of sixty minutes centred at the exact hours, Greenwich Mean Time.

M.S.L. $+ h_a$ (height of anemograph above ground) = 14 metres + 23 metres.

March, 1923.

				[.			Ι.	8.			2	o.		ι.	2	2.	2				Mean	Day.
	13.	I.	4.	I,	5.	16	э.	I	7∙	'	0.	I	9.	2	J.	2	•	4.		2,	3.	2.	1 ·	Mean	Day.
0	m/s.	0	m/s.	50	m/s.	° 80	m/s. 1·6	90	m/s.	90	m/.s	80	m/s.	100	m/s.	120	m/s.	110	m/s. 3·0	120	m/s. 3·0	120	m/s. 3·6	m/s. 3·0	1
40 220	3.3	40 190	3·3 2·6	50 160	3.3	140	3.0	140	4.3	140	2.3	_	1.3	140	1.6	140	2.0		1.3		1.3	140	1.6	4.3	2
320	0.0	330	3.0	320	3.0	330	0.3	_	0.7		0.3	_	0.7	340	2.0	320	2.3	320 210	1.6	340 220	2.6	330 190	2.6	1.0	3 4
180	8.2	190	3.6	190	3.6	200	3.0	220	2.3	260	4.9	280	3.3	260	3.3	230	2.6	240	2.3	240	2.0	200	2.6	4.0	5
180	4.3	170	3.6	180	4.3	190	3.0	190	3.0	180	2.6	190	2.0	180	1.6	180	2.0	170	2.0	200	2.3	170	2.0	2.9	6
30 40	4.3	40 60	4.6	30 50	4.6	30 50	3.6	360 60	3·6 4·9	350 70	3.3	350 70	3.6	340 80	3.3	330 80	3.0	340	4·6 0·3	340 350	1.6	350 —	3.9	3.7	7 8
60	3.0	60	3.0	70	2.3	70	2.6		1.3	_	1.0	130	2.0		6.9	160 140	2·0 6·6		1·3 8·9	190 140	7.9	180 140	2·0 8·2	2·2 4·0	9
170	3.6	160	3.6	160	3.6	150	4.9	150	4.6	150	5.3	150	5.2	140		•		140		'		'			
150 160	7.2	150 160	6.2	160	5·2 8·2	150 160	5·9 6·6	150 160	7·2 8·2	160 160	5·9 7·2	160 160	6·6 7·5	160 150	5·6 8·9	150 150	7·2 8·5	150 160	5·6 7·2	150 160	7·9 7·5	150 160	5.6	6·0 7· 5	11
310	4.9	320	4.9	320	3.9	340	2.3	340	2.0	330	2.3		1.3	_	0.7		1.3		1.0		1.3	290 —	2.0	3.5	13
80 80	3.9	100 60	3.6	70	2.6	120 80	2·3 4·6	120 80	2.3	 80	4.6	150 70	3.3	8o	3.0	140 70	3.3	 80	3.3	90	3.0	90	3.3	3.0	14 15
110	2.6	110	2.6	110	3.0	120	3.0	130	2.6	130	1.6	140	2.0	140	1.6		1.3		0.7		0.3		1.0	2 · I	16
110	2.6	110	3.0	120	2.3	120	2.6	130	2.0	120	2.0	120	2.0	<u> </u>	1.3	_	1.3		1.0		0.7	130	1.6	1.7	17
150	1.3	140 80	3.0	150 120	3.3	150 110	2.6	150	2·6 1·6	160 120	2.0	170 120	1.6	_	1.3		1.0	_	0.7	_	0.7	_	1.3	1.7	18 19
70	2.3	_	1.3	70	2.3	80	2.3		1.3		0.7		1.0	140	2.0		1.0	150	1.6	140	3.3		1.3	1.6	20
110	3.3	110	2.6	110	3.3	110	2.3	_	1.3	_	1.0		0.7		0.7		0.7	_	1.0	300	2.3	300	3.0	1.7	21
40	3.6	50 —	1.3	50 60	4.9	50 60	3.3	50 30	3·6 2·0	60 40	3.9	50 30	2.0	20	2.3	50 40	2.0	30	0.7	360	2.3	350	1.0	2.6	22 23
300	9.8	300	8.5	300	7.5	290	6.2	300	5.6	310	4.3	300	5.9	290	4.9	260	3.3	250	2.0	240 200	3.0	240	2·6 6·6	5·0 2·3	24
180	3.6	160	3.3	180	3.0	180	3.0	170	1.6	160	2.6		1.3	210	3.0	200	2.6	220	5.5		2.0	230			25
150	3.9	140	4.9	160	4.9	160 180	4.6	140	2.6	160 180	3.3	190	2·0 1·3	180	3·0 0·7	180	2·6 0·3	180	2·0 0·3	180	2.0	160	2.3	3.0	26 27
110	3.0	170	3·3 2·3	190	1.3	60	3.9	170 80	2.3		1.3	_	1.0		1.3		1.3	'	1.0	_	1.0	_	0.0	1.6	28
140 150	3.6	140 150	3.3	130 150	3.3	170 160	2·0 3·0	170 160	2.3	 160	2.6	 160	2.3	170	2.6	140	1.6	150 170	1.6	160 170	1.6	170	2.0	1.5	29 30
	-			ľ					_								5.6		6.6	130.	7.2	140	5.9	3.1	31
130	3.0	140	3.9	140	3.6	140	4.6	150	4.3	150	3.9	140	4.3	130	4.9	140		130				<u> </u>			
-	3.6	-	3.4	-	3.2		3.2		3.0		2.7	-	2-5	_	2.5		2.6	_	2.4	_	2.6	_	2.6	2.8	

April, 1923.

. 0	1 - 10	0	l m/c	0	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.		m/s.	, ,	m/s.	۰	m/s.	1 0	m/s.	0	m/s.	m/s.	Ī
	$ \mathbf{m}/\mathbf{s}. $ $8 \cdot 2$	7.00	m/s.	140	7.9	140	7.9	140	8.5	130	7.2	140	7:5	140	7.9	140	6.9	140	6.6	140	4.6	150	5.6	7.7	l r
130		130	7.9	140	1 -	140	1 -	150	4.9	150	4.3	150	4.3	150	3.9	150	3.9	150	3.3	140	3.9	150	3.0	4.2	2
150	4.9	140 160	4.6	140	4.9	160	3.9	160	3.9	160	3.3	150	3.6	160	3.0	160	3.6	150	3.6	160	3.9	150	4.3	3.5	3
170	3.9		3.6	150	3.9	140	5.6	160	3.3	170	3.3	160	3.0	150	4.6	160	3.3	160	3.3	160	3.0	150	4.3	4.7	4
140	5.2	150	3·9 6·6		6.2	130		130	7.5	130	7.5	130	9.5	140	7.9	140	8.2	140	7.5	140	8.2	140	7.5	6.5	5
130	7.2	130	0.0	130	0.2	130	7.5	1 130	13	130	13	130	93	140	1 9	1,40		1 - 4 -	' '	- 4-		l '	, ,	ľ	
700	7.0	120	8.9	120	8.2	120	9.2	120	8.5	130	8.2	130	8.2	130	8.9	130	8.9	120	9.2	120	8.2	110	8.9	8.2	6
120	7.9	•	1	130	6.9	130	6.6	130	7.5	130	7.2	130	6.9	140	7.5	140	5.9	130	7.2	130	7.5	130	8.2	7.2	7
130	7·9 8·5	130	7·9 8·2	140	7.2	140	6.9	130	6.6	140	6.2	130	6.6	140	4.6	130	5.6	130	5.9	130	5.9	130	5.6	7.2	8
140	1 -	140	5.2	100	5.6	90	5.6	80	5.9	80	5.2	60	5.9	50	6.6	50	7.2	50	8.2	60	8.9	60	9.2	5.8	9
110	5.6	110	6.9	130	6.2	130	6.9	130	6.2	140	5.9	140	5.6	140	6.2	130	4.9	130	4.9	130	6.6	120	5.9	8 ⋅4	10
120	0.9	120	0.9	130	0 2	130	0 9	150	0 -	140	1 9	-40	ا ت	-4-	-	-5-	7	- 3 -	' '	,			" -	l	i
120	5.0	120	6.2	130	4.0	140	3.9	130	3.3	130	3.0	130	3.0	140	2.6		1.3		0.7		0.7		1.0	5.0	11
120	5·9	130 60	2.3	70	4.9	140	1.3	70	1.6	90	2.0	-55	1.3		0.7		0.7	10	1.6	20	2.3	30	3.0	Ĭ·9	12
ì	_	160	1 -	170	4.6	210	3.0	200	2.3	180	3.0	170	2.6		1.0	_	1.0	_	0.7	140	2.6	130	2.3	3.0	13
170	4.9	120	3.9	120	4.3	130	4.9	140	3.6	140	3.9	140	3.0	140	3.3	160	3.0		1.0		1.0	130	1.6	3.9	14
60	3.9	60	3.0	50	2.3	50	2.3	40	2.0	30	2.0	50	2.6	40	1.6	30	2.0		1.0		1.0		1.0	2.0	15
00	2.0	00	3 0) 30	2 3	٦٠	~ 3	7"		,		J-				,									1
T40	4.2	140	3.9	150	4.3	140	4.9	150	4.9	140	4.6	150	4.3	150	3.6	170	3.0	160	2.6	170	3.0	170	3.0	2.5	16
180	4.3	170	3.9	160		170	4.3	160	3.6	160	4.3	150	4.3	140	3.6	140	3.3	140	3.9	140	3.3	140	3.3	3.2	17
100	5.6	100	5.9	100	4·9 5·6	100	4.3	130	4.6	130	3.6	120	3.9	130	4.3	130	4.3	140	3.9	130	3.9	120	4.3	4.4	18
100	3.0	90	3.9	90	4.3	80	3.3	80	3.0	100	4.6	110	3.0	110	2.0		1.0	50	2.0	60	3.3	60	2.0	3.5	19
20	5.2	50	5.9	40	6.9	40	8.9	30	6.9	20	7.5	10	5.2	10	4.9	10	6.2	10	6.6	360	5.9	360	5.6	4.4	20
20	5 2	30	39	40	0 9	40	0 9	J 3°	0 9		/ 3		J -		7 /					Ŭ.	0 -			` '	
50	10.2	50	11.1	50	10.5	50	10.5	50	8.2	50	8.5	40	7.9	30	6.6	360	4.3	350	3.3	330	3.0	330	2.6	7.8	21
50	3.6	10	3.3	340	3.0	J.	1.3	120	1.6	_	1.3	210	1.6		1.3		1.0	250	1.6	270	2.0	270	2.3	2.6	22
350	7.2	330	7.5	340	7.5	330	6.6	310	7.5	320	8.2	320	7.2	300	6.6	300	6.6	300	7.2	300	6.6	300	6.9	5.9	23
330	5.9	330	3.9	310	4.3	240	2.6	170	3.3	160	3.6	150	3.6	140	3.9	170	3.9	170	4.9	180	4.9	170	5.9	5.2	24
310	6.2	220	5.6	220	5.2	220	5.6	210	4.9	200	4.6	200	3.6	190	3.3	200	2.6	210	3.9	200	3.3	200	3.3	5.2	25
220	0.2	1 -20	ر ا		, , ,] "	_10	4 9		' '	-30	ا ` ` ا	- ,0	3 3								_		
_	1.3	120	1.6	340	3.3	310	6.9	320	9.8	330	7.9	340	8.9	330	7.2	330	8.9	330	8.5	320	8.2	310	8.2	4.2	26
280	4.9	280	4.3	300	3.9	290	4.3	300	5.9	300	3.6	310	3.6	300	2.3	310	3.6	280	2.6	290	3.6	280	1.6	5·1	27
	5.2	170	5.6	180	4.3	180	4.3	180	4.9	200	3.3	210	3.6		1.0	,	0.3		0.7		1.0		0.7	2.8	28
170	2.6	120	1.6	130	3.0	80	1.6	330	4.6	310	3.9	300	1.6		0.7		0.7		1.3		1.3	_	1.3	2.4	29
110	2.6	120	3.0	150	2.3	140	2.6	160	3.3	170	1.6	110	2.0		1.0	250	4.9	260	4.6	260	3.9	260	5.2	2.2	30
110		120					!I			-,-						<u> </u>									
_	5.2	_	5.2		5.1	_	5.1	_	5.1	-	4.8	—	4.6		4.1		4.0		4·1	_	4.3	_	4.3	4.7	
	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	1				1		<u> </u>		<u> </u>	<u> </u>		1	l I	J	<u> </u>			<u> </u>
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1	3∙	1.	4.	1 ^	<i>J</i> .	1 1	٠.	l *	′			l '	7.	1 ~		ΙĨ		1		l .	-	1	-		
l		<u> </u>		<u> </u>		<u>'</u>						<u></u>		<u> </u>		<u>' </u>									

† Directions obtained from records of the Dines Tube Anemograph. * Speeds obtained from records of the Robinson Cup Anemograph.

WIND: DIRECTION AND SPEED.

† Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$): *Speed in metres per second.

Aberdeen:

 H_a (height of anemograph above M.S.L.) = Height of ground above

Day.	1		2		3		4	ļ.	5	j.	6		7	.	8		9		10	0.	1	ı.	No	on.
	0	m/s.	0	m/s.	0	m/s.	- 0	m/s.		m/s.		m/s.		m/s.	0	m/s.	0	m/s.	-0	m/s.	•	m/s.	0	m/s.
I	260	4.6		1.3	350	2.0		0.7		1.0	330	1.6	340	1.6	30	2.3	60	2.0	80	2.6	80	2.6	80	3.3
2	210	0.7	200	0.7	210	0.3	200	0.7	290 210	4.6	290 210	4.6	320 210	5·9 4·6	10 210	6.6	20 210	3·3	30 220	3.0	50 190	5·6 2·6	60 200	3.0
3 4		3.0	200	2.3		1.0		3.3		0.7		0.3		0.7		1.3		1.3	110	2.0	110	3.0	80	3.0
5	200	3.3	210	3.3	180	2.6	210	4.6	210	4.6	210	3.0	190	3.6	200	3.9	190	4.3	180	3.6	220	5.6	220	5.6
6	_	1.3	290	2.0	290	2.6	_	0.7	ļ '	0.7		0.7	300	2.0	-	1.0	230	2.6	270	3.3	270	3.9	260	4.3
7	-	1.3	l —	1.3	-	1.0	210	2.0	220	2.3	260	3.0	250	4.9	260	5.2	260	4.9	260	4.9	240 280	5.3	240	5.9
8	220	2.0	230	3.0	220	1.6	220 200	3.0	240 190	2.0	260 —	2.0	240 190	3.0	260 150	3·3 5·6	250 150	3.3	260 150	5·6 3·6	140	4.9	270 130	3.6
9 10	290	3.0	290	2.6	300	4.6	300	5.6	280	3.9	290	4.9	280	3.6	250	3.6	250	1.6	220	3.3	180	4.9	170	6.6
II	_	1.3	_	1.3	290	2.3	300	2.3	280	3.0	330	2.6	10	5.6	30	9.8	20	10.5	10	10.2	10	10.5	360	7.9
12	320	7.9	320	8.5	320	9.8	320	8.9	320	8.2	310	9.2	310	8.5	300	10.8	300	10.2	300	12.5	300	11.2	300	12.1
13	280	3.6	280	3.9	280	3.6	290	4.3	300	4.6	280	3.5	290 280	5·9 6·2	310	3.6	330	5.9	340 290	5.9	340 220	4.9	350 160	3.6
14 15	300	9.2	300	7.2	290 70	7°5	280 70	3.9	290 100	7.2	290 120	5.6	90	3.0	290 110	3·3	290 100	3.3	90	2.6	110	3.3	130	3.9
16	310	5.9	310	6.6	310	5.6	310	5.2	300	6.6	300	7.9	300	7.9	300	10.5	300	10.5	300	10.5	300	8.9	310	8.2
17	290	8.9	280	7.2	280	7.9	280	9.5	280	11.5	280	14.8	290	12.1	300	14.1	300	14.1		11.8	290	9.8	310	8.5
18	300	7.2	290	6.2	300	4.9	300	6.2	310	4.3	300	4.9	300	6.9	310	5.9	300	4.6	300	4.6	310	3.6	290	3.0
19	_	0.7	200	1.6	_	0.7	210	1.6	210	2.6	210	1.6	280	3.6	290 210	5.9	290 220	4.3	280 220	3.6	290 210	4.9	280 210	3.3
20	_	0.3		0.7		0.7		1.3		0.7		1.3	-	1.3		2.3	220	4.9		[]				1
21	290	7.5	300	7.2	270	5.9	270	4.9	270	6.6	270	6.6	270	5.6	280	7.5	290	6.6	280	7·2 6·6	280	7:9	290	7.2
22		1.3		1.3	330	3.3	330	3.3	330 250	3.9	330 270	4.9	330 300	6.2	330 300	4.6	330 300	5·6]	300 310	5.6	320 330	4·6 3·9	320 320	3.9
23 24	280	1.3	280	1.3	260	0.7	230 240	1.6	240	3.3	230	3.6	230	4.3	230	2.6	240	4.6	230	4.3	240	3.6	240	3.9
25	260	3.3	260	2.3	250	2.3	270	2.6	290	4.9	290	5.9	310	5.9	310	6.2	330	5.2	320	6.2	320	5.6	320	5.6
26	340	6.2	340	5.6	350	3.6	340	3.3	340	4.3	340	3.9	360	3.9	20	5.2	10	6.6	350	5.2	10	6.2	360	6.2
27	20	4.9	20	4.6	20	4.3	20	5.2	20	4.3	20	4.9	20	4.6	20	5.9	20	6.2	30	5.9	40	5·2 8·9	40	6.2
28	350	4.9	350	4.3	360	4.6	350	3.9	350	5.2	10	7.2	10	8·5 5·2	10 350	3·9	10 340	3.9	360 340	3.9	10 350	3.3	360	7.5
29 30	340 340	3.3	340 330	2.3	340 330	2.0	340 350	3.0	340 350	3.0	350 350	4·3 2·6	350 350	2.6	330	4.3	340	5.5	360	4.9	20	5.2	40	5.3
31	340	1.6	340	2.3	320	2.6	310	1.6	320	2.6	330	3.0	330	2.6	340	2.6	360	3.9	10	4.9	50	4.9	50	4.6
Mean		3.4		3.2		3.2		3.5		3.8		4.2		4.7		5.3		5.3	_	5.4		5.3		5.3

Aberdeen: $H_a = 14 \text{ metres} + 23 \text{ metres}$.

1 300 2-0 320			m/s.		l m/s	0	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	•	m/s.	·	m/s.	0	m/s.	0	m/s.	0	m/s.
2 330 3:3 330 4:6 330 5:2 330 3:3 330 3:3 330 3:3 330 3:3 330 6:2 330	т .	220		220	m/s.	220				200		200	,			310		310		320		320		310	
30		_	,			-			- 1																
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\$\frac{1}{5}\$ \$\frac{1}{300}\$ \$\frac{1}{2}\cdot 0 \frac{1}{270}\$ \$\frac{1}{1}\cdot 6 \frac{280}{280}\$ \$\frac{1}{2}\cdot 0 \frac{1}{1}\cdot 0 \frac{280}{200}\$ \$\frac{1}{1}\cdot 0 \frac{280}{200}\$ \$\frac{1}{3}\cdot 0 \frac{1}{3}\cdot 0 1		-				-								-	1	_	1 -		h :	~	4.9	_			
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8 20 3-9 200 2-3 20 5-6 100 4-3 180 4-3 200 4-9 200 7.2 210 9.2 210 8-9 210 7.5 210 8-9 210 7.5 210 8-9 210 3-9 180 210 3-9 230 6-9 230 8-9 220 7-9 220 6-0 220 4-9 220 7-5 220 8-9 220 8-5 220 11-5 220 12-1 230 9-5 11 280 8-9 280 9-2 280 10-5 290 13-1 290 14-1 300 9-8 310 8-5 310 10-5 310 10-5 310 10-5 310 10-5 310 10-5 310 10-8 310 12-1 12 260 2-6 240 1-6 210 1-6 220 2-3 210 1-6 210 2-3 20 3-6 8-5 200 3-6 200 3-6 200 3-9 190 3	7	_						J00		-				J			1.0								
9 180 2:3 220 5:6 210 4:6 210 3:6 240 4:9 250 7:5 220 8:9 220 8:5 220 11:5 220 12:1 230 9:5 11 280 8:9 220 8:9 220 8:5 220 11:5 220 12:1 230 9:5 11 280 8:9 220 8:9 220 8:5 220 11:5 220 12:1 230 9:5 11 280 8:9 220 8:9 220 8:5 220 11:5 220 12:1 230 9:5 11 280 8:9 220 8:9 220 8:5 220 11:5 220 12:1 230 9:5 11 280 8:9 220 1:6 210 1:6 220 2:3 210 1:6 210 2:0 2:3 210 1:6 210 1:0 2:0 2:3 210 1:0 2:0 2:0 3:0 3:0 2:0 3:0 3:0 3:0 3:0 1:0 3:0 1:1 8 3:0 1:1 8 3:0 1:1 8:0 1:1 8:0	: <u> </u>				1			100				200	1	200		210	9.2	210		210	7.5	210	8.2	210	
10 210 3.0 230 6.9 230 8.9 220 7.9 220 6.6 220 4.9 220 7.5 220 8.9 220 8.5 220 11.5 220 12.1 230 9.5 11 280 8.9 280 9.2 280 10.5 290 13.1 290 14.1 300 9.8 310 8.5 310 10.5 310 10.5 310 13.1 310 10.8 310 12.1 12 260 2.6 2.6 1.6 210 1.6 220 2.3 210 1.6 210 2.3 210 3.0 200 3.6 200 3.6 200 3.6 200 3.9 190 3.9 170 4.3 13 230 4.3 320 3.0 250 3.6 280 4.9 250 5.0 250 4.6 280 8.5 290 13.1 280 9.8 290 11.8 300 12.5 300 11.6 300 2.6 290 2.0 260 1.6 280 1.6 - 1.3 1.0 - 1.0 - 7.2 320 7.9 320 7.9 320 7.5 330 8.2 320 7.9 320 7.5 330 8.2 320 7.9 320 7.9 320 7.5 330 8.2 320 7.9 320 7.5 330 8.2 320 7.9 320 7.9 320 7.5 320 8.2 320 7.9 320 7.5 320 8.2 320 7.9 320 7.9 320 7.5 320 8.2 320 7.9 320 7.9 320 7.5 320 8.2 320 7.9 320 7.					1 9									1		240	7.2	250	6.6	240	6.2	260	6.2	260	3.9
11			_							1							8.9	220	8.5	220	11.2	220	12.1	230	9.5
11			3 ,	-5			_		, ,				' '	l				l							-
12	11	280	8.9	280	9.2	280	10.5	290	13.1	200	14.1	300	9.8	310	8.5	310	10.5	310	10.2	310		310	10.8	310	12.1
14	12	260	2.6	220	1.6	210		220		210	1.6	210	2.3	210	3.0			200							4.3
14	13	230	4.3	250	3.6	280	4.9	250	5.6	250	4.6	280	8.5	290	13.1	280	9.8	_				-	١		10.5
15	14			320		320	8.2	320	7.9	320	7.5	330	8.2	320	7.2	320		_	1 1						1 - 1
17 320 3.3 320 2.3 300 2.6 320 3.7 320 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.		300	2.6	290		260	1.6	280					1.0		1.0		0.7	110	3.3	150	3.6	150	4.6	160	3.3
17 320 3.3 320 2.3 300 2.6 320 3.3 320 3.3 320 3.3 320 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.				1		Ì		l		ł		İ		1				•							
18	16	320	3.0	310	3.3	320	3.3	320	3.3	320	3.9	320	3.9						- 1						
19	17	320	3.3	320	2.3	300	2.6	320	3.3	320	3.0	310	5.2	310		_									
20	18	220	1.6	<u> </u>	0.3				0.3			i		_				_							
21	19	340	2.0	330		330		300	3.0	-	5.9	-	1										1 .		
22	20	300	3.6	310	4.6	320	4.9	320	5.9	320	5.2	320	5.6	320	6.3	320	7.2	320	0.2	320	7.2	330	0.0	320	7.2
22														.0-	- 6	200	6.6	200	2.2	200	2.0	200	6.0	280	7.0
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30		310		i .		320		320				320			1						4.9	320	5.2	-	
Mean 3·2 - 3·4 - 3·7 - 3·5 - 3·6 - 4·2 - 5·0 - 5·3 - 5·6 - 5·6 - 6·0 - 5·6 - 5·6 - 6·0 - 6·0 - 5·6 - 6·0 - 6		3.0	1	1 -	1 1		1 -												"	320		310	4.3	330	
G.M.T. I. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. Noon.			- 3										7 -			<u> </u>	<u></u>	<u> </u>							
5	Mean	-	3.3		3.4		3.7	_	3.2	_	3.6	-	4.3	-	5∙0	-	5 ·3	-	5.6	_	5.6	_	6.0	_	5.6
5	0.34.57	 	-	<u> </u>	<u>`</u>		<u> </u>		<u>.</u>		·		1				.	·		7.	,	,	т.	No	, n
	G.M.T.	'		2	2.	3	;.	4	. 1	5	.	6	.	7	•		·	٩	'		- '	•		1,100	
+ Directions obtained from records of the Dines Tube Anemograph.	1	!		<u> </u>											!		!	<u>'</u>							'

[†] Directions obtained from records of the Dines Tube Anemograph. * Speeds obtained from records of the Robinson Cup Anemograph.

Averages for periods of sixty minutes centered at the exact hours, Greenwich Mean Time.

M.S.L. $+ h_a$ (height of an emograph above ground) = 14 metres + 23 metres.

May, 1923.

M.S	S.L	⊢ ha ((heigl	it of	anemo	ograp	lı abo	ve gr	ound) == 1	.4 me	tres -	- 23 :	metre	es.								IM	ay, 1	923.
I	3.	1	4.	,	5.		6.	1	7.	1	8.	1	9.	2	0,	2	I	2:	2.	2	3.	2.	4.	Mean	Day
00	m/s 3·3	90	m/s	90	m/s	0 110	m/s 3·0	0 120	m/s	100	m/s 1.6	000	m/s 2·0	-	m/s 1 · 3	0 110	m/s	-	m/s		m/s 0·7	-	m/s 0·7	m/s 2·1	,
70	3.9	80	3.3	90	3.3	100	3.0	110	3.0	130	2.6	140	2.0	160	2.0	190	2.6	210	2.3	210	2.0	200	2.6	3.1	1
220	3.0	210	3.3	230	3.9	210	3.0	200	2.3	250	2.6	200	2.6	230	2.6	220 180	2.0	230	2.0	 170	2.3	190	0.7	3.0	
40 170	3.6	20 170	2·6 5·2	220 170	3.6	240 160	4.9	240 170	3.3	240 180	5.9	240 180	3.0	200 190	2.3	210	2.3	190	0.3	-	0.7		3.3	3.2	
240	4.3	250	5.2	250	5.6	240	7.2	240	6.2	250	4.9	240	6.6	260	3.6	270	3.9	260	3.0	250	2.6	240	1.6	3.3	١,
250	6.2	230	5.9	240	5.6	240	4.9	240	4.6	230	5.6	220	4.3	170	2.0	210	4.3	230	5.2	220	3.0	210	2.6	4.0	
290	4.3	300	6.6	310	5.2	310	4.9	310	5.9	320	4.6	310	2.0	330	2.0		0.0		0.3		1.0	230	2.0	3.2	
90	2.6	350	3.3	330	4.3	310	4.6	360	6.2	360	5.9	340	4.6	10	5.6	330	3.6	340	3.6	320	3·9 1·6	310	3.0	3'4	ı
180	5.2	190	5.2	180	6.2	180	6.9	190	6.2	190	5.9	200	3.6	260	2.3		1.3	_	1.0	270	1.0	_	1.3	4.0	
350	6.9	340	7.2	340	7.5	330	7.5	330	8.2	330	7.5	330	6.6	330	7.2	330	6.9	330	7.5	330	8.5	330	6.9	6.4	1
300	11.5	290	11.5	290	10.5	300	12.5	290	8.2	290	7.5	280	6.9	290	5.9	290	5.2	280	5.2	290	4.3	280	5.2	8.9	I
330	5.2	350	5.6	340	5.2	360	4.3	350	4.6	320	6.2	320	5.6	300	5.2	290 220	4·6 2·6	310	6.9	300	9.3	300	0.3	5.3	I
150 150	3.9	150 210	3.9	140 290	4.9	140 300	4.9	150 240	3.3	180 250	2.3	180 290	3.0	190 310	2·6 5·2	310	4.3	300	3.6	300	3.0	310	5.3	2.9	ī
-				l	7.2	310	9.2	300	9.5	310	8.5	310	8.2	310	6.6	300	7.5	300	9.2	290	9.5	290	9.2	8.2	1
310 310	8.5	320 310	9.5	310	12.1	310	10.2	310	10.5	320	10.3	320	9.2	310	7.5	310	8.5	310	7.2	300	7.9	300	6.6	10.1	1
270	2.0	310	1.0	150	1.6	170	2.6	170	2.6	180	2.3	180	2.0	180	2.0	200	2.3	210	1.6	210	2.0	-	1.0	3.7	1
320	3.9	260	3.0	100	3.3	110	2.6	120	2.3	150	2.0	—	0.7	_	1.0		0.7		1.0		0.0		0.0	2.3	1
200	4.3	200	3.9	200	3.6	200	4.3	210	4.3	240	5.3	260	4.9	290	5.9	270	3.9	250	2.6	230	3.6	270	3.6	3.0	2
290	7.2	300	8.9	310	7.2	300	7.5	320	7.2	330	6.6	340	4.9	340	6.9	340	4.6	340	5.2	330	3.0	330	3.6	6.4	2
330	4.6	340	5.2	340	3.9	350	3.9	340	3.9	340	3.0	30	2.6	10	2.6	350	1.6		1.3	280	2.0	270	1.3	3.7	2 2
340	3.9	320	4.6	320	5.3	300	4.9	320	4.3	320	4.9	320 210	3.6	320 230	3·0 5·6	310 280	3.0	280 270	1·6 5·2	270 250	2.6	260	3.0	3·2	2
10 20	4·6 5·6	220 330	5.9	220 330	7.9	220 320	5·2 9·8	210 320	5.6	210 320	5.6	320	5·9 8·2	320	6.6	320	7.2	330	6.6	340	5.9	360	4.9	6.2	2
10	5.9	20	6.9	10	5.9	360	5.6	360	6.6	360	4.9	360	4.6	360	3.6	360	4.6	360	3.9	10	3.6	20	3.9	5.0] 2
40	6.6	40	7.2	40	7.9	20	5.6	350	5.6	350	5.9	350	4.9	340	4.3	350	4.3	350	4.3	350	4.6	340	3.9	5.3	2
io	9.8	360	6.9	360	6.9	360	6.9	360	6.6	360	5.6	360	4.3	ΙO	4.3	360	3.3	340	3.3	340	3.0	340	3.0	5.8	2
36 0	3.6	350	3.9	340	3.6	350	3.3	360	3.3	360	3.6	360	3.0	350 10	3.0	350 10	1.6	350 350	2.3	360 350	2.6	330	3.0	3.3	3
50	6.2	40	5.6	40	4.9	40	4.3	40	4.9	30	4.3	20	3.6	10	3.3	10		1	1	1	ì	1		1	1
50	3.6	60	4.3	60	4.9	·60	5.6	50	3.3	50	4.3	40	3.0	20	1.6		0.0	320	2.3	300	2.6	300	2.3	3.1	-[
	5.2		5.5		5.5	-	5.5	-	5.3	-	5·1	-	4.3	-	3.9	-	3.2	_	3.4	-	3.3	_	3.3	4.4	
																							Ju	ine, 1	923
0	m/s		m/s	1 0	m/s	1 °	m/s	0	m/s		m/s	· °	m/s		m/s	l °	m/s	1 °	m/s	•	m/s	1 °	m/s	m/s	Ī
330	4.3	330	6.2	340	5.2	340	4.3	340	3.9	360	4.3	350	3.6	340	3.9	330	3.3	310	2.3	320	5.2	330	3.3	4 1	ŀ
180	3.6	180	3.0	180	2.6	230	4.3	320	6.2	360	3.9	110	2.6	320	3.6	310	6.2	300	4.9	300	4.9	310	4.6	3.8	
10	7.2	320	8.2	330	5.6	340	5.6	330	5.6	350	3.9	350	4.3	10	4.6	360	3.0	340	2.6	330	3.6	320	3.0	5.5	
30	5.2	330	4.3	330	4.6	330	4.6	350	4.9	340	4.3	340	4.9	320	3.6	330	3.0	320	2.3	240	1.3	340	3.9	2.0	
:60	3.0	_	0.7	_	1.3	_	1.3	-	1.0	300	2.3	310	6.2	340	4.9	350	4.6	340	3.9	340	3.9	1			
340	3.6	340	4.3	330	3.0	290	3.6	130	3.3	140	2.3	140	2.0	140	2.0	160	1.6		1.3		1.3	200	2.6	3.7	
70	2.6	190	3.0	240	4.3	260	4.6	260	3.9	240	3.9	230	5.5	210	3.3	210	4.3	200	3.9	210	4.3	200 190	1.6	2·8 5·9	1
210	6.6	220	7.9	210	7:5	210	7.2	230	8.5	250	8.2	240	4.6	230	3.6	220 180	3.3	210 180	4·6 2·6	190 160	2.3	190	2.0	3.7	
270	2.6	250	3.3	240	8.9	230	9.8	200 260	2.0	190 270	9.5	210 280	2·0 6·2	280	1·3 6·2	280	6.2	280	6.2	280	6.2	280	7.5	8.0	1
:30	10.2	240	10.2	250	3.9	250	9.0	200	9.5	1 2/0	9.3	200	0 2	1 200	~ 1	200				i			1	-	
310	11.5	210	0.8	310	10.8	300	9.8	300	7.2	290	6.6	290	8.9	290	4.9	300	3.9	280	3.6	280	3.3	260	2.3	9.0	1

				-							/-			. 0	· /c		1 /-		m/c	0	m/s	0	m/s	m/s	1
	m/s		m/s		m/s		m/s		m/s	-6-	m/s		m/s		m/s	1	m/s	310	m/s	320	5.2	330	3.3	4·I	
330	4.3	330	6.2	340	5.2	340	4.3	340	3.9	360	4.3	350	3.6	340	3.9	330	3.3	I ~		300	4.9	310	4.6	3.8	2
180	3.6	180	3.0	180	2.6	230	4.3	320	6.2	360	3.9	110	2.6	320 10	3.6	310 360		300	2.6	330	3.6	320	3.0	5.5	3
310	7.2	320	8.2	330	5.6	340	5.6	330	5.6	350	3.9	350	4.3	320	3.6	330	3.0	340 320	2.3	330	1.3	J	1.3	4.0	4
330	5.2	330	4.3	330	4.6	330	4.6	350	4.9	340	4.3	340	4·9 6·2	_	4.9	350	4.6	340	3.9	340	3.9	340	3.9	2.9	5
260	3.0	_	0.7		1.3		1.3	_	1.0	300	5.3	310	0 2	340	4 9	350	4 0	340	3 3	340	, ,	31	3 -	_	
2.0	2.6			222	2.0	200	2.6	120	2.2	140	2.3	140	2.0	140	2.0	160	1.6		1.3		1.3	200	2.6	3.7	6
340	3.6	340	4.3	330	3.0	290 260	3·6 4·6	130 260	3.3	140 240	3.9	230	5.3	210	3.3	210	4.3	200	3.9	210	4.3	200	4.3	2.8	7
170 210	6.6	190 220	3·0 7·9	240 210	4·3 7·5	210	7.2	230	8.5	250	8.2	240	4.6	230	3.6	220	3.3	210	4.6	190	2.3	190	1.6	5.9	8
270	2.6	1	, -	240	2.0	230	1.6	200	2.0	190	2.6	210	2.0	-3-	1.3	180	1.6	180	2.6	160	2.3	190	2.0	3.7	9
230	10.2	250 240	3.3	250	8.9	250	9.8	260	9.5	270	9.5	280	6.2	280	6.2	280	6.2	280	6.2	280	6.2	280	7.5	8·o	10
230	10 2	240	10 5	1 250	"	-50	9 0		, ,	-,-	1 , 3			l								i			l
310	11.5	310	9.8	310	10.8	300	9.8	300	7.2	290	6.6	290 .	8.9	290	4.9	300	3.9	280	3.6	280	3.3	260	2.3	9.0	11
200	3.9	240	4.3	290	3.3	290	7.9	280	7.2	290	5.6	300	3.9	300	3.6		1.3		1.0	_	1.3	200	2.3	3.3	12
300	12.1	300	10.2	300	9.2	300	10·8	310	9.5	320	10.2	310	9.8	310	8.9	320	10.5	320	9.5	320	8.5	320	9.2	9.0	13
320	7.9	320	8.2	320	7.5	320	6.6	330	5.6	340	5.2	340	5.2	340	4.3	330	3.3	320	3.3	300	3.3	300	3.6	6.7	I 4
170	4.3	180	3.6	170	3.6	160	3.3	150	2.6	150	2.3	120	2.3	90	3.0	70	2.6	40	2.6	36 0	5.3	330	2.3	2.6	15
1	' '			l ′						_	-			l				i i	1						
340	6.9	340	6.2	340	6.9	330	5.9	340	5.9	340	5.2	340	4.6	330	4.3	330	5.2	330	3.9	320	3.3	320	3.9	4.8	16
100	4.3	140	3.3	150	3.9	170	3.6	170	2.6	180	3.9	180	3.6	190	4.3	170	2.3	170	2.3	200	1.6		1.3	3.3	17
180	4.3	190	5.2	190	4.3	190	4.3	190	3.9	200	2.3	-	1.0	340	4.9	350	2.3	350	2.3	350	2.0	340	1.6	2'4	81
310	5.2	310	6.2	310	3.3	320	4.3	310	4.3	300	5.2	310	6.2	310	5.6	320	4.9	330	3.6	330	4.3	310	4'3	4:7	19 20
320	7.9	320	6.9	320	5.6	320	5.2	310	3.6	290	2.0		1.0	180	1.6	190	2.6	210	2.0	240	2.6	200	2.0	4.8	20
ļ.,		_															- 0		7.0		1.0		1.3	3.9	21
290	6.2	280	6.2	280	6.9	290	6.9	290	6.2	- 310	3.9	290	4.6	290	3.3	280	1·0 6·2		1.0	290	4.9	280	5.6	6.0	22
280	8.9	280	8.9	290	8.2	290	8.9	290	9.5	290	7.5	290	8.5	290	6.9			290 260	4.6	240	2.0	240	2.6	5.8	23
270	7.2	270	6.6	270	7.5	270	8.2	280	10.2	280	8.9	270	6.2	260	3.9	250	3·9 3·6	300	3.9	290	5.6	290	3.9	4.0	24
330	3.6	340	3.3	350		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		310	3.0	310	3.6	300	4.3	290	3.9	300	3.0	300	1.3	290	1.0		1.3	3·1	25
330	4.3	330	3.9	350	4.3	330	2.0	180	2.3	170	2.3	180	2.0	170	2.0		1.0		. 3					١	,
	6.0	0.00		240	٠.,	320	6.2	240		240	2.0	220	2.0	220	2.6	310	2.3	290	2.6	280	2.3		1.3	4.2	26
340	6.2	350	5·2 2·6	340 120	5·2 2·0	330 130	2.0	340 160	5·2	340	3.0	330	3.9	330	3.6	310	0.3		0.7	_	0.3		1.3	1.5	27
140	3.0	120	2.3	130	2.6	160	1.6	140	1.6	130 320	3·0 4·6	170 300	4.6	300	5.2	310	4.9	310	7.2	300	4.9	310	5.9	3.1	28
350	3.3	120		130	1.6	210	2.3	220	2.3	220	1.6	300	1.0	300	0.7	200	1.6	220	2.0		0.3		0.3	3.6	29
320	4.6	320	3.3	160	2.6	210	2.0	240	1.6		1.3	340	2.0	320	2.6	310	3.6	310	1.6	300	3.0	310	2.6	2.5	30
310	3.6	350	2.0	100		210		240			1 3	340		320	2 0	3.5									
	5.6	_	5.3	-	4.9	-	5.1		4.8		4.4		4.5	_	3.9	_	3.2	-	3.3		3.1	-	3.1	4.4	
<u></u>	<u>!</u>			! 	<u>. </u>							<u>'</u> '		 	<u> </u>	<u> </u>		 I				1		Mean	Day.
13	3.	I	4.	ı	5•	10	6.	1	7•	1	8.	I	9.	2	о,	2	I.] 2	2.	2	3.	2	4.		Duy.
1		<u> </u>		<u></u>										<u> </u>		<u> </u>		<u> </u>					!		<u></u>
																	nomoo								

[†] Directions obtained from records of the Dines Tube Anemograph. * Speeds obtained from records of the Robinson Cup Anemograph.

† Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$): *Speed in metres per second.

89. Aberdeen:

Ha (Height of anemograph above M.S.L.) = Height of ground above

Day.	1	Ι.	2		3		4		5		6		7		8		9		10). 	1	I.	N	oon.
	°	m/s.		m/s.	0	m/s.	,	m/s.	l °	m/s.	l °	m/s.	l °	m/s.		m/s.	<u> </u>	m/s.	l °	m/s.	<u> </u>	m/s.	-	m/s
1	-	0.7	300	3.0	290	2.0	290	2.0	290	2.0	290	2.3	310	3.3	290	3.6	320	3.9	320	3.6	330	2.0	350	3.0
2		0.3	_	1.0		1.0	-	0.3	_	0.0		0.3		0.3	-0-	0.7		1.3	210	2.3	230	3.3	220	5.
3	200	4.3	200	4.6	190	3.3	190	5.2	190	4.6	190 180	1.6	190	4.3	180	3.9	190	3.3	190	4.3	170	3.9	180	4.
4 5	250	1.3	240	1.0		0.7	_	0.7	_	0.7		0.7	150	0.3	170	1.9	170 170	2.3	130 180	3.3	150	3.0	190	3.
6		0.3		0.7		0.3		0.3		0.0	_	0.3		1.3		1.3	120	2.6	140	3.6	140	3.6	140	2.
7	150	3.0	140	2.0		1.3		1.3	170	3.3	170	2.6	150	3.0	130	2.3	130	2.6	120	3.9	130	3.6	120	3.
8	220	2.3	220	2.3	_	0.7		0.3		0.7		0.7	-	0.3	170	2.3	_	1.0	-	0.7	130	2.0		0.
9 10	110	2.0	150	0.3		1.3	170	0.3	_	0.7	160	0.7	140	1.0	180 80	2·6	170 80	2·6 1·6	180	3.0	180	3.9	160	3.
11	_	1.0		0.3		1.0	36 o	1.6	_	1.3	340	3.0	320	2.3	340	3.3	20	1.6	330	3.3	330	2.6		1.
12		0.7		1.3		0.7		1.0	-	1.3		1.3		1.0	200	2.6	210	3.6	190	3.3	170	3.0	170	2.
13		1.3		1.3	280	1.0	290	2.3	l —	1.3		1.0	10	1.6	70	2.0	70	2.6	70	2.3	80	3.0	80	3.
14	.00	0.7		0.3		1.0		0.3		0.6		1.3	140	2.0	140	3.3	140	3.0	130	3.0	130	3.6	130	2.
15	180	3.0	190	2.3	190	3.6	200	3.3	200	2.6	200	3.0	200	3.3	200	3.9	190	4.3	190	3.9	200	3.9	190	3.
16		0.3		0.7		0.3		1.0		0.0		ó.3		0.7		0.3	40	1.6	330	1.6	130	1.6	130	3.
17 18	220	2.0	220	3.0	220	3.6	220	2.0	220	3.0	210	3.0	220	4.3	210	3.9	210	5.2	210 280	5.2	210	4.9	220	4.
19		0.7	270	2.6	260 260	2.6	260	1.9	240	2.3	250 240	3.3	270 220	2·6 3·0	220	3.6	280 220	5·2 3·9	210	2·3 4·6	260 200	3.3	270	5.
20		1.0	_	1.0	250	2.6	250	4.9	250	3.0	250	2.6	270	4.6	280	4.9	270	6.6	280	5.9	280	2.9	270	4.
21		1.0	250	2.3	250	2.0		1.3	250	2.6	270	3.3	240	3.3	260	4.3	260	2.6	230	3.3	250	5.9	250	5.
22	210	1.6	190	2.0		1.0		1.0		0.3		1.3		0.7	180	1.6	160	2.0	210	2.3		1:3	230	2.
23	200	2.3	210	2.0	230	2.0	250	1.6	280	3.0	260	3.0	280	3.0	310	4.3	290	5.9	270	5.9	290	5.2	290	6.
24 25	290	3.0	_	0.7	270	2.6	280	1.9	270	2.3	270	2.6	280	3.3	290	5.2	290 150	3.0	300 170	3.3	290 200	2.3	310 300	3.
_	120		220				2.0		'		260				,					8.2	200	6.9	290	8.
, 26 27	230 320	2·3 4·6	220 310	2·3 4·6	240 300	2·6 3·6	240 300	3.0	200 310	3.6	260 320	3·6	280 320	5·9 3·6	300 320	7·2 3·6	290 330	7·9 3·0	300 330	2.0	300 330	1.6	130	2.
28	140	3.3	150	3.9	140	3.3	130	4.6	130	6.2	130	5.2	130	5.6	120	6.9	120	5.6	120	6.2	120	6.2	110	4.
29	100	2.6	110	2.3		1.3	130	1.6		1.3	150	2.3	150	2.3	160	2.6	170	2.3	170	2.3	180	2.6	170	3.
30		0.7		0.0		0.3		0.3	_	0.7	_	1.0	Ť	0.7		1.0	320	2.3	10	1.6	30	1.6	90	2.
31	70	2.6	50	3.0	30	3.3	30	3.3	30	3.0	40	3.6	30	3.3	30	3.3	20	3.3	40	4.3	40	5.3	50	4
Mean		1.8		1.8		1.7		1.8		1.8		2 · I		2.5		3.0	_	3.3		3.5		3.2		3.

90. Aberdeen: $H_a = 14 \text{ metres} + 23 \text{ metres}$.

		m/s.	0	m/s.	, ,	m/s.]	0	m/s.	0	m/s.	0	m/s.	0	m/s.		m/s.	0	m/s.		m/s. I	0.	m/s.	0 -	m/s.
I	340	3.6	340	3.0	330	2.3	340	3.0	320	3.0	320	3.3	320	4.3	320	3.3	320	3.9	320	3.0	310	3.3	350	3.3
2		1.3	_	0.3		1.0	<u> </u>	1.3		0.3	_	0.7		0.3	120	1.6	_	1.3	130	2.3	170	3.0	170	2.6
3	170	6.6	180	5.9	200	3.3	260	5.2	270	6.6	270	5.6	270	6.6	280	6.9	290	6.9	280	7.5	290	7.9	290	8.9
. 4	270	5.2	260	3.9	270	4.3	250	4.6	260	3.3	270	3.9	290	7.5	300	8.5	290	6.6	300 160	9.8	290	3.6	310	5.9
5	_	1.3	140	2.0	150	2.3	170	1.6	170	2.3	170	2.6	170	2.6	170	2.0	150	4.3	100	3.3	170	3.0	150	3.3
6		1.3		1.3	_	1.0		1.0		0.3		0.3	_	1.0		1.0	180	2.0	210	3.6	210	4.9	220	5.6
7		1.3	160	1.6		1.0	160	1.6	18o	2.0	170	2.0	180	2.0	190	3.3	200	3.0	190	2.0	180	2.3		1.3
8	320	3.3	320	2.6	300	4.6	310	3.3	300	2.6	300	3.0	300	2.6	330	1.6	80	1.6	130	2.6	140	2.3	160	2.6
9	170	2.3	200	2.0	200	2.6	210	3.3	220	3.0	220	2.6	240	3.0	210	2.6	230	3.3	210	3.0	280	2.6	260	2.6
10	220	2.0	220	3.3	220	3.0	210	3:3	220	3.0	230	3.3	230	3.6	250	4.3	240	3.9	26 0	2.6	260	4.6	260	4.6
11	240	3.3	240	3.0		1.3	250	2.6	260	1.6	270	2.6	280	3.3	280	5.2	280	4.6	310	5.6	320	4.6	300	4.6
12		1.0	290	1.6		1.3	280	2.0		1.3		1.0		0.3		1.0	160	2.0	180	3.3	180	3.6	170	3.3
13	200	2.0	190	2.6	190	2.0	180	1.6	210	2.6		1.0	*******	1.3	210	3.9	210	3.6	210	2.0	200	2.0	240	3.0
14	260	1.0		1.3		1.0		1.3	210	1.0	210	2.3	220	3.6	250	3.3	240	2.0	260	3.0	250	1.6	170 280	3.3
15	240	2.0	280	1.6	260	1.6		0.7		1.0	210	2.0	230	3.0	240	2.6	240	3.9	270	3.9	290	5.9	200	4.9
16	280	3.9	290	4.6	290	3.6	270	2.0	260	1.6	270	2.6	270	3.0	280	4.6	280	5.2	290	5.6	300	5.6	290	5.2
17	220	1.6	200	2.0	190	2.0	170	3.3	170	3.9	170	4.6	170	5.2	180	4.9	190	3.3	210	3.3	200	1.6	210	2.0
18	—	1.0	300	2.6	300	4.3	300	3.3	300	3.6	300	4.3	310	4.9	310	4.9	20	4.3	40	5.9	50	4.6	40	5.2
19	l —	1.0	300	1.6	300	1.6	290	1.0	290	2.0	290	1.6	290	1.6	290	1.6		1.0	30	2.0	T.40	1.3	140	1.6
20		1.3		0.7		0.7		0.7		1.3	150	1.6	140	2.6	130	3.0	130	3.3	140	3.9	140	3.3	140	3.6
2 I	130	5.2	140	6.6	150	4.9	160	5.2	170	6.6	170	5.2	180	3.9	180	5.2	190	6.2	180	5.6	18o	6.2	180	6.6
22	210	3.9	230	5.2	230	4.6	220	3.6	220	3.3	230	4.9	230	5.2	220	4.6	250	5.6	260	7.9	260	7.2	260	6.9
23	250	3.9	250	4.3	240	3.9	230	3.3	230	2.0	230	3.0	250	4.6	250	3.0	250	3.3	280	4.3	290	4.3	200	1.6
24	190	2.3	190	1.0		0.7		0.7	_	0.7	l —	1.0		1.0		1.3		1.3	10	4.3	10	6.6	360	6.9
25	300	4.9	290	3.6	290	2.6	300	4.3	280	3.0	260	3.0	280	3.3	290	2.3	270	1.6		1.0	220	2.3	160	3.3
26	210	2.6	220	3.6	220	3.6	230	3.9	240	3.0	230	4.3	210	3.3	200	3.6	210	4.9	220	4.9	210	3.3	200	4.6
27	190	2.3		1.0	210	2.0	250	2.6		1.0	210	3.3	200	2.6	180	3.0	200	4.3	210	3.9	190	4.9	180	3.6
28		1.3	_	1.3		1.0	_	0.3		1.0		1.0	270	1.6	280	4.3	290	3.6	310	3.9	310	4.6	310	3.6
29	220	2.6		1.0	-	0.7		0.3	240	2.6	250	2.6		1.0		0.7	140	2.3	140	4·3 6·6	160	4.3	100	4.3
30	40	3.3	30	4.9	350	4.6	340	3.6	320	5.3	330	4.6	320	6.6	320	5.9	300	5.9	300	0.0	300	7.2	310	4.9
31	_	0.7		0.7	_	1.0		0.7	en contra de	1.3	300	1.6	300	2.0		0.7		1.0	100	3.0	120	2.0	130	3.3
Mean	_	2.6		2.6		2.4		2.4		2.5		2.8	_	3.1		3.4		3.2		4.1		4.1	-	4·I
G.M.T.	I		2			3.	4		5	•	6	•	7		8	3.	9		10	o.	r	ι.	No	on.

[†] Directions obtained from records of the Dines Tube Anemograph.

^{*} Speeds obtained from records of the Robinson Cup Anemograph,

Averages for periods of sixty minutes centred at the exact hours, Greenwich Mean Time.

 $M.S.L. + h_a$ (Height of anemograph above ground) = 14 metres + 23 metres.

July, 1923.

ı	3.	r.	4.	1	5•	1	6.	I	7.	r	8.	I	9.	2	о.	2	ı,	2:	2.	2	3.	2.	‡ •	Mean	Day.
0	m/s.	° 170	m/s.	200	m/s.	210	m/s.	200	m/s.	200	m/s.	210	m/s.	200	m/s.	210	m/s.	200	m/s.	°	m/s. 0 · 7	0	m/s. o·7	m/s.	I .
200	5.6	190	3.9	200	3.9	200	3.3	200	3.3	190	3.3	200	3.3	200	3.3	200	3.9	180	3.6	210	5.2	200	3.3	2.5	2
190 170	3.3	240 170	5·2 4·3	260 170	5.6	260 180	3.3	280 190	4·6 3·9	280 190	3.3	280 170	3·0	190	3.3	210	3.0	250 230	3.3	250 200	3.0	250	2·6 1·0	3·7 2·8	3
200	3.0	190	3.0	180	3.0	180	2.6	200	3.3	180	2.0	180	1.6	200	1.6		0.7	-	1.0		0.7		0.3	1.7	5
150	4.3	110	3.0	100	3.6	130	3.3	120	2.3	130	3.3	_	1.3	120	2.0	160	3.0		1.3	150	1.6	160	2.3	2.0	6
120	3.0	120 140	3.3	140 130	2.0	120 170	3.0	140 210	3.3	120 350	1.6	150 360	1.0	140	2.3	250 310	3.9	36o	1.9	160 340	1.0	200	2·0 1·0	2·4 1·7	7 8
170	3.3	150	2.6	150	2.0	130	1.6	140	3.0	130	1.6	140	2.6	150	2.6	_	0.7	130	1.6	_	1.0 I.0		1·0 0·7	2·0 1·5	9 10
-	1.0	10	2.0	10	2.0	40	2.0	30	3.0	50	3.6	30	2.6		1.0		0.3		0.3		10				
310 140	3.0	100 220	3.3	220	3.9	350	1.0	 40	1.3		I.0 I.0	120	1.0	_	1.0		0.7	_	1.0	_	0.3		0.3	1.8	11
80	3.9	60	4.6	60	4.6	50	3.9	40	4.3	40	3.6	50	2.3	-0-	1.3		0.7		1.0		0.3		1.3	2.3	13
150 180	3.9	160 190	4·3 3·9	170 180	3.9	170 200	3.3	170 210	3.6	170 220	3.3	180 220	3·3 2·6	180 220	3.3	180	2.6	190	2.3	190 230	1·6	190	2·6 1·3	3.4	14 15
150	3.3	110	3.3	110	1.6	90	1.6		1.3	240	3.6	240	3.3	220	3.3	240	2.6	220	3.6	220	2.6	200	2.6	1.8	16
240	5.9	240	6.9	240	6.6	230	5.2	240	4.6	250	4.3	240	4.3	240	3.3	260	3.0	250	2.6	-	1.3	-	1.3	3.9	17 18
90 220	3.0	100 200	3.0	150 180	4.3	170	3.3	140 160	2.3	140 240	3.9	270	2.6	270	3.0	260	3.6	230	1.0	200	3.0	210	2.3	3.0	19
270	5.6	270	6.9	260	4.9	250	4.6	220	4.6	220	3.6	210	4.3	210	5.9		1.3	200	2.3	-	1.0	_	0.7	3.9	20
260	5.6	260	5.6	260	3.9	260	4.6	270	4.3	240	2.0	240	1.6	260	2.6	240	2.6	200	2.3	230	2.6	220	2.0	3.2	21
250 280	4·9 4·6	220 290	5.9	230 290	4·9 5·9	230 310	5·2 5·2	230 310	4·9 5·6	210 310	3.9	220 300	3.3	230 310	4.9	250 290	2.6	230 300	3.6	220 280	4·3 3·9	230 290	3.3	2·7 4·I	22
_	1.3	160	2.6	180	2.6		1.3		0.7	_	1.3	320	2.0	_	0.7	160	1.6	_	1.0	230	1.6	-	1.3	2 · I	24
310	5.6	280	6.6	280	5.9	290	6.6	270	5.6	290	6.2	280	4.6	260	3.3	250	2.3	220	2.6	210	2.3	210	3.0	3.0	25
290 120	4·6 3·6	310 120	5·2 3·6	320 130	5·6 3·9	320 130	5·2 3·6	320 130	7·2 3·9	320 140	6·9	320 140	6·6 3·6	310 140	5·6 3·3	310 140	3.3	310 140	3.9	320 140	7.9	320 140	3.3	5·6 3·6	26 27
110	5.2	110	5.9	100	5.9	100	5.2	100	5.9	90	5.6	90	3.9	80	3.9	8o	3.6	80	3.3	80	2.3	80	1.6	4.8	28
160	3.3	160 120	3.3	160 150	3.9	150 140	3.3	140 140	3.3	150 120	3.0	150	3.0	160 140	3.6	170 —	3.9	200	1.3		0.7	20	0.3	2·6 1·4	29 30
50	5.6	40	5.2	50	4.6	50	3.0	40	3.3	40	3.6	30	3.6	40	4.6	10	2.6	10	2.3	340	3.0	340	2.3	3.6	31
										<u> </u>							ļ						1.8		
-	3.9	_	4.0	_	3.8		3.3		3.4		3.2	_	2.7		2.7		2.4		2.2	_	2.1	-	1.0	2.7	

August, 1923.

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0	m/s.	0	m/s.	٥	m/s.	٥	m/s.	0	m/s.	٥	m/s.	0	m/s.	°	m/s.	٥	m/s.	٥	m/s.	°	m/s.	0	m/s.	m/s.	
130	2.0	210	2.6	200	2.6	220	2.3	220	1.6	240	2.0	240	3.0	250	2.3	250	2.3		1.0	280	1.6	280	1.6	2.7	I
140	3.0	150	4.9	150	7.2	150	6.6	130	6.6	130	9.8	130	10.5	140	9.2	140	10.5	150	7.5	160	8.2	160	9.2	4.4	2
290	11.2	290	12.1	290	11.8	300	11.2	290	9.2	280	7.9	290	8.2	280	7.9	270	6.2	280	5.6	270	3.6	270	3.9	7.5	3
310	4.6	320	5.2	320	3.9	240	2.3	160	3.0	150	2.6	100	1.6	<u> </u>	1.3	100	2.0	140	1.6	120	2.0	130	1.6	4'3	4
160	3.9	170	3.9	160	3.9	180	4.3	170	4.3	170	3.0	150	3.0	160	1.6	160	2.0	180	1.6	_	1.0		1.0	2.7	5
220	5.6	200	3.9	190	3.6	140	2.0	180	3.6	180	3.0	210	3.6	200	3.3	210	4.6	200	2.6	180	2.0		1.0	2.6	6
260	2.3		1.3		1.3	60	1.6		0.7		0.3		1.0		1.0	300	2.0	300	4.3	310	3.9	320	3.6	1.0	7
160	4.6	170	3.6	170	4.3	170	3.3	180	3.6	170	4.3	170	3.0	190	3.9	190	2.6	190	3:9	190	3.0	190	2.3	3.2	8
260	3.6	300	2.6	50	2.6		1.0	10	2.6	270	3.9	260	3.6	280	3.3		0.7	260	1.6	230	2.0		1.3	2.6	9
260	4.9	270	4.9	270	5.6	290	6.6	280	5.2	280	4.3	280	2.0	290	3.3	250	3.3	260	3.0	240	2.0	230	3.3	3.7	10
		İ												ł						1					
290	3.6	300	3.6	320 180	2.6	150 180	3.3	170	1.6	200	0.7		1.3		0.7		1.3	200	1.0	200	0.7	200	1·0	2.7	11 12
170 240	3.3	180	3.6	290	3.3	270	3.9	180 280	3.3	200 320	3.0	170	2.3	200 280	2.0	210 310	2.3	200 280	3.3	200 260	3.0	250	3.3	2.8	13
170	2.3	230 20	2.0	110	4·6 2·6	200	4.9	90	2.0	50	2.3	300	4·6 1·3	200	0.3	310	1.0	260	1.6	270	2.0	270	2.0	2.0	14
280	5.2	290	5.9	280	4.6	280	6.2	300	4.6	280	3.3	290	3.6	28o	3.9	270	1.6	270	3.3	270	2.3	270	2 · 3	3.3	15
	"	-)-	3 3		7 -			J-			3 3	-,-	J -		J /			,		′ .		1			Ŭ
300	5.6	290	3.3	340	3.3	100	1.6	160	2.6		1.0	140	2.0		1.3	170	1.6		1.3	170	1.6	180	2.0	3.1	16
	1.0	230	1.6	230	2.3	310	2.3		0.3		0.7		1.0	_	1.3		0.7	270	1.6	270	1.6	290	2.0	2.3	17
40	4.9	40	4.9	40	4.9	50	4.9	50	4.9	50	3.0		1.3	340	1.6	330	1.6	310	1.6		1.0	300	2.0	3.6	18
130	2.3	130	2.6	120	2.3	150	2.6	160	1.0	150	2.3	170	2.0		1.0		1.3		1.3	T.10	1.3	7.40	1.3	1.7	19 20
130	4.9	130	3.9	130	3.9	130	4.9	140	3.0	140	2.3	140	2.3	140	2.6	140	2.6	130	3.9	140	2.6	140	3.6	2.7	20
200	6.2	230	7.2	250	7.5	250	5.6	240	6.6	240	6.6	240	8.5	240	5.6	230	6.6	220	3.6	220	5.2	210	3.3	5.8	21
270	6.9	280	5.6	270	4.9	270	6.2	260	5.9	260	3.6	240	2.6	250	3.6	230	1.6	230	2.3	240	2.6	240	2.6	4.7	22
190	3.0	220	3.6	230	4.9	210	4.6	210	3.9	200	3.0	170	3.3	160	3.9	130	4.9	100	6.2	110	8.2	150	4.9	3.9	23
350	5.9	340	6.9	340	6.2	340	5.9	340	6.6	340	6.2	340	6.2	330	5.6	320	6.6	320	4.9	300	4.6	310	6.9	4.2	24
150	3.6	170	5.6	160	4.6	160	5.6	160	4.3	150	5.2	170	4.3	170	3.3	160	4.3	170	3.9	180	3.3	200	3.3	3.6	25
180	2.6	180	2.0	180	2.2	180	2.0	200		-0-		-0-				-0.5		210		270	2.2	190	1.6	3.3	26
200	3·6 5·6	210	3.9	190	3.3	190	3.3	200 190	3.0	180	2.3	180	2.0	190 210	2.0	180 220	2.0	210 220	2.3	210 240	3.3		1.0	3.0	27
290	4.6	310	4.3	300	5.2	310	3.3	300	3.9	190 300	3.0	210 280	3.9	280	2.6	260	2.6	260	2.3	260	2.0	270	3.0	3.0	28
150	4.6	150	5.2	150	3.9	140	4.9	140	3.3	120	4.3	110	3.3	130	2.6	120	4.9	80	6.2	50	4.6	20	3.6	3.2	29
360	2.6	350	3.0	10	2.3		I.o		1.0		1.3	_	0.3		0.7		0.7		0.0		0.3		1.0	3.3	30
														l	·									ا , ,, ا	
160	2.3	160	3.9	160	2.3	160	2.6	150	2.0		0.2		0.0		0.7	310	2.0	300	2.0	300	3.0	300	3.6	1.7	
_	4.3	_	4.3	_	4.2		4·1	_	3.7	_	3.3		3.5		2.8	_	2.9		2.9	_	2.8		2.7	3.3	
	<u> </u>	ļ					<u> </u>						<u> </u>	<u>!</u>			<u> </u>			<u> </u>	<u> </u>	<u> </u>	<u> </u>		
1	3.	1.	4.	1	5.	1	6.	r	7.	I	8.	r	9.	2	о.	2	I.	2	2.	2	3.	2.	4.	Mean	Day.
		1					-							l		I				l					

[†] Directions obtained from records of the Dines Tube Anemograph.

^{*} Speeds obtained from records of the Robinson Cup Anemograph.

WIND: DIRECTION AND SPEED.

† Direction expressed in degrees from North. (E = 90°, S = 180°, W = 270°, N = 360°); *Speed in metres per second.

91. Aberdeen:

Ha (height of anemograph above M.S.L.) = Height of ground above

Day.	I		2	i. 1	3		4	•	5	. .	6	i.	7		8	B.	9		1	0.	1	ı.	No	on.
	-0					/		1 /-	-	1 /		m/s.		m/s.	-	m/s.		m/s.	0	m/s		m/s.	-	m/s
1		m/s.	1	m/s.	1	m/s.	J	m/s.	290	m/s.	290	2.6	290	3.3	300	4.6	300	3.9	340	2.6	80	2.3	90	2.0
2	300 300	3.3	290 320	3·0 4·6	300 320	3.0	300	3.3	320	4.6	310	5.2	310	5.2	300	6.2	310	6.6	310	6.6	320	6.2	320	6.6
3	300	3.3	290	2.0	280	1.6	320 290	2.0	290	1.6	280	1.6	310	1.3	170	2.6	190	2.6	200	3.3	180	3.6	190	3.3
3 1	190	3.0	190	3.0	200	2.3	220	2.3	270	3.3	310	5.6	310	4.3	300	4.6	310	5.2	320	5.6	310	6.6	320	5.2
7	190	2.0	190	1.6	210	2.3	210	4.3	210	5.2	210	4.6	220	4.3	210	3.6	210	3.9	210	3.3	240	2.3	270	3.6
ر ا	190	20	190	1 0	1 -10	- 3	2.0	4 3	2.0	J -		7		T 3		3		3 ,	1	0.0			· ·	
6	250	2.0	240	2.0	280	2.3	220	2.3		1.0	230	1.6	230	3.0	_	1.0		1.0	210	2.0	230	3.9	220	4.9
7	210	3.0	270	4.3	330	2.3	310	4.3	300	5.2	260	2.6	280	3.3	280	5.2	290	5.9	290	8.2	290	7:5	300	5.9
8		1.3		1.3	260	2.0	220	1.6	230	1.6	—	1.3		1.3	200	1.6	190	3.0	230	3.6	210	3.6	210	5.3
9	200	3.9	190	2.6	200	3.3	180	2.6	190	3.6	200	3.9	200	3.3	210	8.5	210	6.2	220	8.9	220	8.2	220	7.9
10	240	2.6	230	2.3	230	2.0	250	2.0	290	1.6	260	1.6	260	2.3	250	3.3	300	5.6	290	5.6	290	5.9	300	4.9
i	·						ł		1														222	6.6
11	220	3.9	220	4.6	220	4.6	210	5.6	200	3.6	200	4.6	200	3.6	190	3.9	200	3.6	220	4.9	190	3.3	220	6.6
12	220	5.6	240	4.3	240	3.6	260	5.6	250	5.6	250	6.6	250	7.9	250	8.2	240	8.9	250	9.5	260	9.5	270	9.2
13	- 1	1.3	280	1.6		1.3	280	2.3	300	3.0		1.3		1.0		0.3	80	2.0	130	3.9	130	4.6	130	5.6
14	170	5.6	180	5.9	180	5.5	190	4.6	190	4.6	200	2.3	190	3.0	210	4.3	220	4.9	220	4.6	230	5.2	220	4.9
15	200	3.0	200	2.3	220	2.0	210	1.6	210	2.3	200	3.3	220	2.0	220	3.3	230	2.0	200	2.6	200	2.3	200	4.3
- 6											220	2.6		2.2	220	2.2	260	5.2	280	5.9	290	6.6	290	6.6
16	210	4.6	210	4.6	220	4.3	230	3.6	240	4.9	230 210	2.6	230	2.3	220 190	3.3	190	5.2	190	6.9	180	8.2	180	8.5
17	230	2.3	220	2.6	210	3.0	210	3.0	200	4.6	210	3.9	310	3.9	310	2.0	310	3.0	310	3.3	310	4.6	320	4.3
18	190	6.9	210	4.6	210	2.3	220	1.6	220	2.6	210	1.6	310	1.3	200	1.6	220	2.6	230	4.3	230	4.3	230	5.6
19	280	3.0	260	3·3 0·7	250	2.6	240	1.6		1.3	210	0.7	_	0.3		1.3	300	1.6	350	3.0	20	3.0	360	2.3
20		1.0		0.7		0.7	240	1.0	_	1.3		٠ <i>،</i> ا		× 3		1.3	300	1 0	330	,		J -	J	- 3
21	290	2.6	280	2.6	280	2.0		1.3		1.3		0.7		1.3	300	1.6	290	2.3	290	3.3	300	3.0	300	2.3
22		1.3	_	1.3	210	2.3	210	2.6		1.0		0.3		1.3	250	1.6	230	2.3	250	2.3	260	3.3	240	2.6
23	280	1.6	280	1.6	280	2.0	280	2.0	280	2.3	290	2.3	280	2.0	280	1.6		1.3		0.7		0.3	<u> </u>	1.3
24	200	2.6	280	3.0	280	3.3	280	3.3	270	2.3		1.3	280	2.3	280	2.3	280	3.0	310	2.0	310	2.0		1.3
25	140	6.6	150	6.6	130	6.6	140	8.2	140	9.2	140	8.2	140	7.9	130	9.2	130	8.2	140	6.2	150	3.0	160	2.6
-,	, ,		,		,		'	1	'			[.	· •		-	-							
2 6	300	3.9	300	3.6	290	4.3	280	1.6	280	1.6	250	2.0	210	1.6	200	1.6		1.0	250	2.6	280	3.6	300	3.6
27		0.7		1.0	210	2.3	190	2.3	190	2.6	180	2.3	190	3.9	180	3.3	190	4.9	200	5.6	190	4.9	180	4.6
28	200	6.9	200	5.6	210	5.2	210	3.6	190	1.6	210	2.6	260	4.3	310	3.0	320	3.0	300	6.6	300	6.6	280	4.9
29		0.3	270	2.6	270	3.3	240	3.6	240	4.3	280	2.0	250	2.0	220	2.3	220	3.3	230	2.3	240	2.3	230	2.0
30	210	2.3	200	2.6	-	1.0	-	1.3		0.3		0.7		0.3		0.7		1.0		1.3	190	2.6	180	3.6
Mean		3.1		3.1		2.9		3.0		3.0		2.7		2.9		3.4		3.8		4.4	_	4.4		4.5
mican		3.1		3.1		2.9		١٠		3 ~		~ /		~ "		3 4		3 -		77		7 7		1 3

92. Aberdeen: $H_a = 14 \text{ metres} + 23 \text{ metres}$.

		mia	0	m/s.	0	m/s. (0	m/s.	•	m/s.	0	m/s.	0	m/s.		m/s.	0	m/s.	0	m/s.	•	m/s.	•	m/s.
1		m/s.		1.3	150	2.0	310	2.0	300	3·6	270	3.3	250	3.0	220	2.3	250	1.6	260	4.3	220	3.6	260	5.9
2	210	3.9	200	3.0	200	4.3	190	3.0	230	4.6	300	7.5	300	8.5	300	8.2	300	7.5	290	6.6	280	8.5	290	7.2
3	240	2.3		0.7	270	1.6		1.3	280	i · 6	290	2.0	300	2.6	300	2.6	300	2.6	310	3.3	350	3.0	360	3.0
4	330	4.6	320	3.3	310	3.3	310	4.9	330	3.9	320	4.3	320	3.0	310	3.0	330	3.3	330	3.3	330	5.6	310	3.6
5	_	1.3	220	1.6		1.3	200	2.3	200	3.3	200	3.9	180	3.6	200	3.6	200	5.2	200	4.9	210	4.9	200	4.6
ő	240	3.3		1.0	230	2.3	220	3.3	220	3.3	210	3.0		1.3		1.0	230	2.0	230	4.6	220	3.3	240	3.6
7	220	3.0	220	3.3	200	3.0	190	3.3	190	3.0	180	3.0	200	4.6	200	5.2	200	4.3	200	5.6	210	6.6	210	5.2
8	270	3.0	270	3.0	260	3.3	230	3.3	230	2.6	230	3.0	240	3.6	240	4.3	250	3.3	270	4.3	270	4.9	280	4.9
9	180	4.6	200	3.6	200	5.9	220	4.6	250	5.6	240	7.9	240	8.2	240	8.5	240	10.2	250	12·I	250	11.5	250	11.1
10	250	3.6	240	5.3	250	5.2	240	3.6	200	1.6	240	3.9	230	3.3	230	3.6	230	5.6	230	6.9	240	6.9	240	5.9
11	250	3.9	260	5.6	260	5.6	260	4.9	250	3.9	260	4.6	260	5.2	270	6.6	280	8.9	280	9.2	280	8.2	280	8.5
12	220	5.6	230	4.6	230	4.6	230	2.0	220	2.0	220	2.6	210	3.3	210	4.6	200	2.6	200	4.3	190	3.6	180	3.3
13		1.0	100	2.6	011	3.0	40	2.3	300	3.0	300	4.9	300	4.3	300	4.6	320	3.9	330	4.3	350	4.9	340	5.6
14	280	3.3	270	3.0	200	2.0	270	2.6	250	2.3	240	1.6	260	2.6	280	3.9	280	6.2	300	5.9	310	7.2	310	6.9
15		1.3		1.0		1.3	240	2.3	220	2.0	210	2.0	_	1.0	230	2.6	230	2.6	210	3.3	230	3.0	230	3.6
16	_	0.7		1.0	240	2.0	240	2.0	310	2.0	350	3.9	330	2.6	320	3.9	330	3.3	320	4.3	310	5.9	320	6.2
17	210	3.6	200	3.6	210	2.6	240	2.6	260	1.6	l —	1.3		1.0	260	3.0	280	4.6	260	3.0	270	4.6	270	3.6
18	190	1.6	180	2.0	190	1.6		1.3	180	2.3	200	2.0	200	2.3	210	3.3	210	3.3	200	3·3 8·5	180	3.3	190	3.6
19	180	5.6	170	4.9	160	5.9	160	5.9	150	7.9	160	7.9	160	7.9	160	8.5	190 210	6.6	220	8.5	250 210	7.2	230	7.5
20	190	2.6	220	2.3	240	1.6	200	3.9	210	4.3	200	5.6	200	5.3	200	4.9	210	4.6	210	0.5	2.0	' -	200	′ -
21	160	7.9	160	7.9	160	7.9	160	7.2	160	7.9	150	9.2	170	7.2	170	7.2	180	6.6	210	5.2	260	4.9	250	4.9
22		1.0	200	1.6		1.0		1.0	200	2.3	220	4.3	200	1.6	210	2.3	200	4.6	210	3.3	210	3.9	210	3.9
23	260	5.2	260	4.9	250	5.6	260	4.9	230	2.6	240	2.6	230	1.6	-	0.3	_	0.7	220	3.0	210	2.0	190	2.6
24	280	2.6	270	3.6	270	3.3	270	3.3	240	2.6	240	3.0	250	1.6	240	1.6	240	2.6	260	4.3	250	3.9	260 240	4.3
25		1.0		0.0		0.7		1.0		0.7		1.0		1.0		1.3	240	2.6	230	3.3	240	4.3	240	4 3
26	230	4.6	220	4.6	220	3.9	190	3.0	190	1.6		0.7	170	5.2	150	2.3	150	6.2	140	5.2	100	6.2	190	5.9
27		1.0		0.3		0.7	140	3.6	140	6.6	130	6.9	130	8.9	130	10.2	130	10.8	140	9.2	170	6.9	190	3.9
28	160	7.2	150	8.2	150	9.5	150	8.2	180	4.3	200	4.3	190	4.6	190	3.3	190	4.6	190	5.9	200	6.6	210	5.9
29	240	2.0	260	1.6		1.3	240	2.6	240	3.0	230	2.6	220	2.3	200	2.3	190	2.0	200	3.3	200	3.0	210	3.9
30	190	3.3	100	2.3	190	3.6	190	4.6	190	3.3	190	3.9	180	2.0	210	4.3	210	5.2	220	4.3	250	4.9	220	4.9
31	230	5.9	200	2.3	200	3.6	200	4.3	180	2.0	200	3.0	210	3.0	220	3.6	210	3.0	230	3.0	250	5.2	260	5.2
Mean	_	3.3	_	3.0		3.3		3.4		3.3		3.9	-	3.7		4.1		4.6	_	5.2	_	5.3	-	5.2
G.M T.	-	Ι.	2	·	3			' <u>'</u>	5		6			7.		8.		9.	10).	11	.	No	on.
							-	·	3											į)	

[†] Directions obtained from records of the Dines Tube Anemograph. * Speeds obtained from records of the Robinson Cup Anemograph.

Averages, for periods of sixty minutes centred at the exact hours, Greenwich Mean Time.

 $M.S.L. + h_a$ (height of anemograph above ground) = 14 metres + 23 metres.

September, 1923.

1	3.	1.	4.	1	5.	16	i.	1	7.	18	3.	19).	20).	21	ι.	22	2.	23	3.	24	ļ.	Mean	Day.
110	m/s. 3·o	120	m/s. 1·6	- 	m/s. 0·7	-	m/s.	-	m/s. o·3	310	m/s. 1·6	340	m/s.	320	m/s.	310	m/s.	300	m/s. 2·3	300	m/s. 4·3	300	m/s. 3·3	m/s. 2·6	I
320 200 310	5·2 3·6 4·6	320 220 300	5·9 3·3	320 210 290	5·9 4·3 3·9	330 180 280	5·2 3·9 2·3	330 190 290	4·3 3·3 3·0	340 190 260	3.3	320 210 260	3.3	290 200 260	1·6 2·6 3·0	270 210 240	3.0	290 210	2·3 3·6 1·3	280 210 200	1.6 2.0 1.6	190	1·0 2·6 1·3	4.4 2.8 3.4	2 3 4
290	5.3	280	5.3	280	4.9	270	4.9.	290	6.9	290	4.3	260	4.3	250	3.3	260	2.6	260	2.0	250	2.0	_	1.3	3.7	5
210 280 220	5·2 6·6 5·9	210 300 200	5·9 4·3	300 210	5·6 5·9 4·3	300 210	4·9 5·6 4·3	300 210	5·9 4·9	210 290 200	4·3 3·9 4·6	300 180	3·6 3·3 3·6	220 260 170	4·6 2·0 3·0	300 200	7.5 2.3 3.3	300 200	7·2 2·3 3·9	220 — 200	5·2 4·3	220 290 200	3.9 1.6 3.0	3·7 4·4 3·2	6 7 8
240 280	6·9 5·9	250 290	5·6 6·2	250 280	6·6 4·6	260 280	6·6 4·3	270 280	4·6 4·6	280 290	3.3	270 290	1.6	260 210	2·3 1·6	240 230	2·0 1·6	230	2.6	220	1.3	240 220	3.3	4·6 3·4	10 9
220 270 130 230 200	4·9 9·5 5·6 4·6	220 280 160 220 190	4·9 9·2 4·3 5·9 4·6	230 290 150 210 190	5·9 9·2 4·3 3·9	220 280 140 230 210	7·5 6·9 6·6 4·6 4·3	210 290 140 210 220	4·6 5·9 6·6 3·3 4·9	210 300 140 200 220	6·9 4·3 6·2 3·0 4·3	210 290 150 190 220	6·2 4·3 5·2 2·6 2·6	220 280 160 190 220	4·3 2·6 4·9 2·3 3·6	230 290 160 190 230	8·2 3·6 3·6 3·3 3·9	220 270 170 190 250	7·9 3·0 4·6 3·0 3·0	210 290 180 200 220	6·9 2·3 4·3 3·9 3·3	210 280 170 210 220	6·2 1·6 5·6 2·0 3·6	5·2 6·2 3·7 4·2 3·2	11 12 13 14 15
290 180 320 210 330	7·5 9·2 3·9 4·9 3·6	300 180 320 190 320	6·9 7·9 3·0 3·3 3·6	300 190 320 190 320	6·9 7·9 3·6 5·2 3·3	290 180 320 190 330	4·9 8·5 2·0 2·6 2·6	300 180 320 180 320	4·9 8·9 1·6 2·0 2·3	280 180 — 190 —	4·9 10·5 1·0 2·6 0·0	280 180 260 200	3·0 9·2 2·0 2·6 0·7	270 180 — 210 —	2·6 7·5 1·3 2·3 1·0	270 180 270 270 270	2·6 9·8 2·0 2·3 1·6	300 180 280 290 280	1.6 8.5 2.0 2.6 2.3	 190 290 	0·7 8·5 2·6 1·3	240 190 290 250 290	1·6 8·2 3·3 1·6 1·6	4·3 6·7 2·8 2·9 1·7	16 17 18 19 20
280 230 110 110 180	2·0 3·6 2·3 3·0 3·6	320 230 — 100 170	2·0 3·9 1·3 2·6 4·6	210 140 120 170	1.0 3.6 1.6 3.3 3.3	 220 150 170	1·3 4·6 1·0 3·3 2·3	280 — 170 180	1·3 2·6 1·3 3·3 2·3	220 — — 180 190	3.6 1.0 3.6 1.6	220 — 290 170 180	2·6 0·3 1·6 3·6 1·6	220 — 290 170 —	2·6 0·7 2·0 3·3 1·0	230 280 180 	2·3 1·0 2·6 4·3 1·3	240 — 280 170 300	2·3 1·0 3·0 4·6 1·6	240 	1.6 1.3 3.6 4.6 2.0	280 150 300	1·3 2·3 5·6 3·3	2·0 2·0 1·8 3·0 4·7	21 22 23 24 25
180 300 180 200	1.0 4.3 4.6 2.3 3.3	180 280 200 200	1·3 3·9 3·6 2·3 3·3	150 290 — 180	1·3 2·6 2·6 1·3 3·0	170 260 — 200	1.0 2.0 2.0 1.3 3.9	190 270 150 200	0·7 3·9 2·6 2·3 3·9	180 280 170 190	0·7 3·0 1·6 2·0 1·6	140 270 180 170	0·7 2·0 2·3 3·0 1·6	200 150 240 180 180	1.6 3.3 1.6 2.3 2.3	220 160 250 200	3·9 3·0 2·6 1·3	21 0 200 250 200 —	3·3 4·6 2·0 2·6 1·3	210 200 — 210 190	2·6 5·2 1·3 3·3 1·6	200 210 — 210 30	3.6 6.6 1.0 2.0 1.6	2·2 3·4 3·5 2·4 1·9	26 27 28 29 30
_	4.7	_	4.4	_	4.3		3.9		3.8	_	3.2	_	2.9	_	2.6		3.2	_	3.1		2.9	_	2.9	3.2	

October, 1923.

																								•	
•	m/s.	۰	m/s.	۰	m/s.	•	m/s.	0	m/s.	•	m/s.	۰	m/s.	0	m/s.	°	m/s.	0	m/s.	ı °	m/s.	٥	m/s.	m/s.	1
270	5.6	270	5.6	260	5.2	270	3.6	270	3.0	250	3.3	230	2.0	210	2.6	210	1.6	210	2.0	220	2.6	220	3.6	3.0	I
310	6.9	300	6.2	300	6.6	280	5.2	280	4.3	280	4.9	240	2.0	230	2.6	240	2.3	190	2.3		1.3	230	2.0	5.0	2
350	3.3	340	3.6	350	4.3	340	4.6	320	3.9	320	3.9	300	4.6	300	5.2	310	4.3	310	4.6	320	4.3	330	3.6	3.5	3
340	4.9	340	3.9	340	3.6	340	2.3	330	2.3		1.3	300	1.6		0.2	_	1.0	280	2.0		1.0		1.3	3.0	4
200	3.9	200	2.0	210	0.2	210	5.6	220	3.9	230	2.6	200	2.0		1.0	250	2.6	240	2.0	-	0.7	250	2.3	3.1	5
300	4.9	280	5.2	290	3.9	270	3.6	270	3.3	270	2.6	250	2.6	240	2.6	230	2.6	210	2.0	230	3.0	230	3.6	3.0	6
200	5.9	200	4.3	240	3.0	260	3.0	230	1.6	230	3.0	210	3.3	210	3.6	210	3.9	200	3.3	250	3.6	280	4.9	3.9	7
270	3.3	270	4.3	240	2.0	240	1.6	190	1.6	190	2.3	200	3.0	190	3.3	200	4.6	200	4.9	180	4.3	180	6.2	3.5	8
250	10.2	250	11·8	260	11.1	270	11.5	270	11.8	270	8.2	270	7.9	270	6.6	270	8.2	260	7.9	260	5.2	240	2.6	8.3	9
230	6.2	250	6.2	250	6.2	240	6.2	260	4.6	250	5.6	250	3.6	260	3.0	250	4.3	250	5.6	250	4.6	250	4.9	4.8	10
280	.	280	7.2	280	6.2	270		260	2.2	240	2.6			220	2.2			200	7.6		7.3	270	2.6	4.0	l
280	7.2	280 170	7.2	170	3.3	270 180	4·3 3·0	260 170	3.3	240 240	2.6	300	2.6	220	1·3		0.7	200 280	2.0	290	1.9	210	0.3	3.0	11
340	5.9	330	6.2	330	5.2	320	5.6	310	4.9	310	4.3	300	5.2	300	4.3	300	5.6	280	3.9	270	3.3	280	3.9	4.2	13
310	6.9	310	6.2	310	5.2	290	3.9	270	2.0	260	1.6	280	3.0	280	2.6	290	2.0		1.3	250	1.6		0.7	3.6	14
240	3·ó	250	3.3	240	2.6	250	2.0	240	2.0	220	2.3	220	2.6	230	3.3	230	3.9	230	2.6	230	2.6		1.0	2.4	15
							1 1							_		_		_			1				_
320	6.9	320	4.9	310	4.6	320	3.3		1.3		1.0		1.0	_	1.3	220	2.0	210	2.0	210	2.3	200	2.0	2.9	16
260	3.6	210	1.6	250	2.0	250 180	2.3	240	2.6	210	2.3	200	1.6	190	1.6	190	2.6	200	2.3	200	3.3	190	2.6	2.6	17
190	3.3	180	3.3	190	4·6 8·2	230	3.3	170 230	3.6	160 220	3.6	150	4.9	160	5.2	160 210	5.6	170	4.3	170	4.9	160 200	4·6 3·6	3.3	18
180	4.6	230 190	7·9 5·6	230 170	4.9	180	5.2	180	5.6	180	4.3	230 180	3.9	220 170	4·3 5·2	170	5.6	200 170	3·9	210 170	4·9	170	7.5	5.2	20
100	4 0	190	J	1,0	7 7	100	3 -	100	4 3	100	J 9	100	~ ~	1,0	3 -	1,0	0 2	1,0	0 9	1,0	0 9	~,"	' '	J ~	
250	4.6	230	3.3	230	5.2	210	4.6	210	5.2	210	5.9	220	7.2	210	5.6	210	3.3		1.3		1.0	270	2.0	5.7	21
220	3.9	230	3.6	220	3.6	210	4.3	200	5.2	200	4.3	210	4.9	230	3.9	220	3.6	230	4.3	250	5.9	260	6.2	3.4	22
180	2.3	170	3.6	180	3.3	170	3.3	150	3.9	150	3.6	130	2.6	130	2.6	110	1.6		1.3	320	1.6	290	2.0	2.9	23
260	3.9	250	4.9	250	3.0	250	2.3	230	2.3	230	2.0	220	1.6	230	1.6	240	1.6		1.3		1.3		1.3	2.7	24
250	3.9	230	3.6	230	2.0		0.2	200	3.3	190	2.3	200	2.0	210	3.3	210	5.2	220	4.9	210	6.2	220	6.9	2.6	25
260	5.2	260	5.2	260	5.2	260	4.6	250	3.6	260	3.3		1.3	230	3.0	230	2.3	220	1.6		1.3	_	1.3	3.8	26
220	3.3	180	2.6	140	4.3	150	3.3	160	4.6	170	5.9	160	6.2	150	7.9	160	8.5	160	7.9	160	8.2	160	7.9	5.7	27
230	5.6	240	4.3	210	3.0	210	2.3	200	3.0	200	3.0	210	2.6	210	3.3	210	3.3	220	2.6	230	3.6	230	2.3	4.8	28
210	4.3	200	4.3	190	3.3	170	4.3	180	3.9	180	5.6	200	5.2	200	3.9	200	3.9	200	3.9	180	2.6	210	3.6	3.3	29
220	4.6	220	4.3	230	5.6	220	7.5	210	7.2	220	5.6	230	4.6	230	6.2	220	7.9	220	8.9	220	6.9	220	6.2	5.0	30
26.5		260	4	260	3.0	260	2.6	230	2.0	220	2.6	222								ا مور ا	0.6	220	2.6	3.4	21
260	4.6		4.9	200	3 0						2.6	230	3.6	230	2.6	200	2.0	220	2.3	220	2.6			3.4	31
-	4.8		4.9	_	4.5	-	4.0		3.8	_	3.6	-	3.4	_	3.4		3.7		3.2	-	3.4	_	3.4	3.9	
13).	1	4.	ı	5.	1	6.	1	7.	1	8.	1	9.	2	:o.	2	1.	2	2.	2	3.	2.	4.	Mean	Day.

[†] Directions obtained from records of the Dines Tube Anemograph. * Speeds obtained from records of the Robinson Cup Anemograph.

WIND: DIRECTION AND SPEED.

† Direction expressed in degrees from North. ($E = 90^{\circ}$, $S = 180^{\circ}$, $W = 270^{\circ}$, $N = 360^{\circ}$); *Speed in metres per second.

93. Aberdeen:

Ha (height of anemograph above M.S.L.) = Height of ground above

Day.	1		1	2.	3	3.	4	ļ .		5.	(5.	7	7.	}	3.	ç).	1	о.	I	I.	N	oon.
	•	m/s.	°	m/s.	°	m/s.	°	m/s.	°	m/s.	°	m/s.	0	m/s.	•	m/s.	•	m/s.	·	m/s.	0	m/s.	°	m/s.
. I	230	3.3	230	3.6	230	2.6	220	2.6	200	1.6	200	1.6	220	2.0	l —	1.0	210	2.6	220	2.6	220	3.6	220	3.3
2	250	2.0	250	2.3	270	2.0		1.3	290	2.0	290	2.6	290	2.3	280	2.6	290	2.0	260	3.6	260	3.6	260	3.9
3	200	3.6	210	4.5	210	6.2	220	6.9	230	2.5	260	8.2	260	9.8	260	9.8	270	7.5	280	7.5	280	8.5	270	11.2
4	280	6.6	280	9.8	290	7.9	270	8.5	270	5.3	260	5.2	200	3.3	150	1.6	260	3.3	300	7.5	300	7.5	290	8.9
5	300	5.6	290	3.9	310	4.3	300	3.9	290	3.9	290	2.6	290	3.9	290	3.9	290	3.3	300	4.3	310	3.3	330	3.3
6	310	4.9	300	4.9	310	5.2	310	3.9	310	5.2	320	5.9	340	4.3	310	4.6	310	5.6	310	6.6	310	6.6	300	7.9
7	300	9.2	300	8.9	300	9.8	300	6.6	300	11.1	300	8.9	300	7.5	290	5.9	290	5.6	290	5.6	300	6.2	300	6.9
8	210	5.9	210	5.2	210	5.2	200	5.2	210	3.9	210	5.6	220	4.6	230	3.0	200	1.6	260	2.3	260	2.3	270	3.0
9	310	3.9	300	3.9	300	3.9	300	3.9	350	3.0	350	3.3	360	3.9	10	4.3	110	3.9	100	5.6	110	6.6	100	9.2
10	280	3.0	280	2.0	280	2.3	270	2.0	_	1.3		1.3	250	1.6	280	2.0		1.3	250	2.3	240	2.0	240	2.3
II		1.3	230	2.0	220	2.0	220	1.6	_	1.3	230	2.0	260	2.0		0.3	260	2.0	270	1.6	_	1.0	_	1.3
I 2	230	6.9	230	6.2	230	6.2	220	6.2	220	5.6	230	3.9	240	4.6	230	3.6	240	3.0	250	3.3	290	5.9	270	3.3
13		1.3	220	2.0	210	1.6	200	2.0	210	3.0	210	2.3	210	1.6		0.7		1.3	120	3.3	120	2.6	120	3.9
14	290	6.2	280	6.6	280	6.6	280	6.2	280	6.2	270	6.6	260	6.2	250	6.9	250	7.2	240	7.9	250	9.2	260	8.2
15	250	4.9	250	4.3	230	4.6	220	3.3	240	3.0	210	1.6	210	2.0	220	2.0	200	2.3	150	6.9	150	8.5	150	10.2
16	330	13.8	330	13.8	330	14.8	320	14.8	320	14.8	310	12.1	300	10.8	290	9.2	290	7.2	280	7.2	290	6.6	280	6.6
17	190	3.6	190	3.6	210	4.6	220	3.0	220	2.6	270	3.9	290	7.5	300	6.6	300	8.2	300	8.5	300	9.2	290	13.1
18	250	6.6	260	8.9	250	6.9	260	7.2	260	7.9	270	10.8		12.8	290	11.1	300	16.4	300	15.4	310	14.1	310	13.1
19	340	5.6	340	4 3	320	4.9	320	6.2	310	4.9	320	5.6	310	5.9	310	6.6	310	5.2	320	4.9	320	7.5	310	8.2
20	300	4.6	330	4.3	330	4.6	320	2.6	320	3.6	320	3.6	310	4.6	330	3.9	35°	3.9	350	3.0	360	3.9	50	3.9
21	310	5.2	300	5.6	300	4.6	300	5.9	310	6.2	310	5.9	310	5.9	300	4.9	300	6.6	310	6.6	310	6.9	310	6.6
22	350	3.3	360	3.6	10	2.6	350	2.0	350	3.0	330	2.6	340	2.3	320	3.3	320	2.3	300	2.6	300	3.0	310	4.3
23	300	3.9	290	4.6	290	4.3	290	4.3	300	2.6	290	4.3	300	4.3	310	4.6	310	3.0	310	4.6	300	5.9	310	5.6
24	300	4.9	300	4.6	310	3.9	290	3.6	300	5.6	300	5.2	300	4.6	290	4.6	290	4.3	280	3.6	280	3.3	290	3.6
25	230	3.3	220	1.6	_	1.3	_	1.3		1.0	260	4.3	250	3.9	240	2.6	240	2.0	260	2.3	230	2.0	240	2.3
26	220	2.0	230	3.3	240	2.3		1.0	_	0.7		0.0		0.7		1.0		1.0	-	1.3	240	1.6	220	2.3
27		0.7	_	0.7	240	1.6	240	1.6		0.7		1.0	280	1.6	290	1.6	290	2.0	300	2.0	300	2.6	290	1.6
28		1.0	290	3.0	290	3.0	290	2.0	290	2.0	310	3.0	300	2.3	300	3.3	280	2.0	290	2.3	150	3.0	120	4.9
29	70	6.6	70	6.6	40	5.9	40	3.6	360	4.9	20	4.9	340	3.3	20	3.6	40	4.9	20	3.3	350	2.6	350	3.0
30	290	5.6	290	4.3	270	3.0	280	3.0	290	3.0	290	3.6	280	2.3	300	2.6	290	2.3	260	2.6	240	2.3	250	3.0
Mean		4.6	-	4.8	_	4.6	_	4.2	_	4.2		4.4		4.4	_	4.1		4.1		4.7		5·1		5.7

94. Aberdeen: $H_a = 14$ metres + 23 metres.	94.	Aberdeen	:	$H_a =$	14	metres	4	23	metres.	
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	0	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.		m/s.		m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.
I	210	3.6	210	3.3	200	1.6		0.7	240	1.6	220	1.6	230	1.6	230	2.3	230	3.0		0.3		0.7	210	2.0
2	210	2.6	200	3.0	200	2.0		1.3		1.0		1.0	-3-	1.3	190	1.6	170	2.6	170	6.2	160	6.6	170	6.2
3	290	1.6	300	2.6	300	2.3	280	2.6	290	2.0	280	2.3	290	3.9	300	3.9	310	4.3	300	3.9	310	3.3	280	1.6
4		1.3	210	2.0	220	2.0	210	1.6	200	2.3	210	1.6	_	1.0	160	2.6	160	5.6	160	4.9	170	4.6	150	5.6
5	100	8.9	90	8.5	90	8.2	90	8.9	80	7.9	79	6.9	70	8.9	60	6.9	70	7.2	50	8.2	50	6.2	60	6.9
					1								1		1				1		Ì	1	ľ	
6	300	5.2	300	4.3	300	4.9	310	6.2	310	4.9	290	4.3		1.0	<u> </u>	1.3		1.0	_	1.3	270	2.3		0.7
7	200	3.0	190	5.2	190	3.9	190	4.9	190	5.6	190	6.6	190	5.9	190	8.2	180	6.2	180	8.2	190	8.2	180	7.2
8	190	4.3	190	3.6	200	4.6	200	3.0	200	3.3	200	3.3	210	2.0	220	2.6	280	5.9	300	10.2	310	13.1	310	11.8
9	290	5.2	290	5.3	290	5.9	290	5.9	300	3.6	300	3.3	290	3.6	280	2.6	290	3.3	280	2.6	280	1.6	270	3.0
10	200	3.6	200	3.3	200	3.6	200	2.0	230	2.0	240	3.6	230	2.6	220	3.6	210	3.6	210	2.6	220	2.0	_	1.3
	.0.	- 6			210		225		* # 5.					1			700	2.2	170	2.0	200			
II	180	1.6	230	3.0	210	2.3	220	3.9	150	4:3	150	3.6	210	3.3	210	3.9	190 160	3.3	170 180.	3.0	200	4.6	200	3:9
12	200	4.3	200	1 1	190	6.6	190	4.6	200	7.2	190	6.2	200	5.6	170	3.6		2.3		3.3	200	2.3	200 280	3.0
13	300	2.3	310 220	6.6	320 200	3.6	320 190	5.6	310 210	6.2	310	5.2	310 210	1.6	200	1.0	270	10.5	300	3.9	290 220	3.0	210	2.0
14	220	4.6	290	8.2	290	4.3	300	6.9	290	5.2	200 290	3.9	1	5·2 8·2	200	4:3	240 300	6.2	240 300	3.0	280	5.9	280	5.2
15	270	4.9	290	102	290	9 2	300	109	290	0 9	290	0.0	300	0.2	310	4.6	300	0 2	300	30	200	3.9	200	2.3
16	200	2.6	220	2.3	220	2.6	240	4.6	260	5.6	270	3.9	280	6.2	280	7.2	280	7.2	270	7.9	280	7.2	280	6.9
17		0.3		0.3		1.0	-7"	1.3		0.7	240	1.6	190	2.0	210	3.0	160	1.6	260	3.9	240	3.3	250	6.9
18	280	4.9	270	5.6	270	5.9	270	6.0	280	5.2	280	9.5	290	11.1	290	11.5	280	8.2	280	10.8	290	14.4	290	15.4
19	320	7.9	320	7.9	320	8.2	310	5.6	310	6.6	310	4.3	290	4.6	290	7.9	300	8.9	310	9.5	310	10.2	310	9.8
20	340	6.9	340	6.2	330	9.2	340	6.6	330	7.5	330	7.2	330	8.2	330	6.6	340	7.2	330	8.9	330	7.9	330	7.2
	٥,	_	١ ٠٠		1 33		0 '		55	' '	33	,	33.		33	1	٥,	'	""		55	' '	33	,
21	330	6.6	320	5.6	310	5.6	320	4.9	330	4.6	340	4.6	330	4.3	320	3.3	310	4.3	310	3.3	320	2.6	310	2.6
22	200	3.6	200	3.6	200	3.0	210	3.0	220	3.3	230	2.6	240	2.3	280 -	2.0	320	6.9	320	5.2	310	6.2	310	8.9
23	300	8.2	290	10.8	290	11.1	300	11.8	300	12.8	310	11.1	310	10.5	310	10.8	320	9.8	320	11.5	310	11.1	310	10.5
24	280	4.6	260	4.3	240	4.6	280	4.9	280	4.9	290	5.9	290	4.3	300	6.2	310	7.5	330	4.6	350	4.6	30	8.5
25	290	3.3	280	3.6	290	6.2	290	3.9	280	3.6	290	2.6	290	4.3	290	3.0	280	2.6	280	3.0	280	2.0		1.3
	1		[-	(l	l	ł	1								
26	30	1.6	_	1.3	340	2.3	30	3.3	20	1.6	310	2.6	320	2.3	320	2.3	310	2.6	300	3.3	280	1.6	290	2.3
27	130	4.9	160	1.6		0.3		0.3		0.3		1.0	-	1.0	300	1.6	_	1.0	290	1.6		1.0	230	1.6
28	300	3.3	300	3.6	320	3.6	320	3.3	320	3.3	340	3.6	40	6.2	50	8.5	50	7.2	40	3.9	330	2.6	320	3.0
29	290	3.3	290	3.0	290	3.6	290	3.0	280	2.6	270	1.6	260	1.6	280	2.3	290	1.6	290	2.3	760	1.3		0.3
30	170	3.6	170	4.6	170	5.2	170	6.6	100	6.6	160	7.5	150	9.2	150	9.5	150	8.5	160	9.8	160	9.8	160	8.2
31	190	4.2	200	3.6	210	3.6	210	2.2	210	T. (.	200	0.0				0.0		0.7		1.0		0.3		0.3
31	190	4.3	200	3.0		3.0	210	3.3	210	1.0	220	2.3		1.3		0.0		0.7		1.0				0.3
Mean		4.1		4.4		4.5		4.4		4.3		4.3		4.4		4.5		4.9		5.2	l —	5.0	_	5.0
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			İ		1		 I			1	r <u>'</u>		<u>'</u>		<u>'</u>	<u>'</u>	1		<u> </u>		Ī		Ī	
G.M.T.		Ι.	i :	2.	1 :	3.	4	١.	ء	5.		5.		7.		8.		.	1	ο.	1	ı.	No	on.
			l		1						Ì		1 '	,	l i		1 '		l		1		l	

[†] Directions obtained from records of the Dines Tube Anemograph. * Speeds obtained from records of the Robinson Cup Anemograph.

Averages for periods of sixty minutes centred at the exact hours, Greenwich Mean Time.

M.S.L. $+ h_a$ (height of anemograph above ground) = 14 metres + 23 metres.

November, 1923.

I	3.	I	4.	1	5∙	1	6.	1	7.	1	:8.	1	9.	2	œ.	2	21.	2	2.	2	3.	2.	4.	Mean	Da
0	m/s.	0	m/s.	0	m/s.	٥	m/s.	0	m/s.	٥	m/s.	0	m/s.	٥	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	m/s.	i –
230	3.9	230	4.9	220	3.0	220	3.6	220	3.3	230	4.3	240	3.0		1.0		I.3		0.7		1.3		1.3	2.6	1
250	3.3	240	3.6	230	2.3	230	3.0	210	2.0	200	2.6	210	4.6	220	5.6	220	6.9	210	4.6	210	4.3	200	4.3	3.5	1 :
280	9.8	260	8.5	260	7.5	260	7.2	250	7.5	240	6.9	240	5.2	250	7.5	250	6.9	250	5.9	200	7.2	270	8.2	7:3	
280	6.6	270	5.9	270	6.2	280	4.6	270	2.0	270	4.9	270	5.9	270	5.2	270	4.9	290	6.2	290	6.6	290	6.2	5.9	
330	3.6	330	3.6	350	2.6	320	2.3	320	3.3	320	4.3	310	3.6	310	3.9	310	4.3	310	4.6	300	3.9	310	4.9	3.8	
00	7.2	290	7.2	300	8.2	290	5.9	280	7.5	280	5.9	290	7.9	300	8.2	290	9.8	290	9.5	300	10.5	300	8.9	6.7	
00	3.9	280	3.0	280	1.6	_	0.7		1.0	220	1.6	230	2.3	220	2.6	200	2.3	200	3.9	200	4.6	200	4.9	5.3	į .
8 o	2.0	290	3.0	270	2.0	260	2.3	270	1.6		1.3		1.3	290	2.3	300	2.0		1.3	300	3.6	300	3.0	3.1	l
10	4.9	80	5.9	90	8.5	90	7.2	80	6.2	80	5.9	90	4.9	80	4.3	50	2.6	300	2.6	290	2.6	290	3.0	4.7	1
-	1.0	_	1.3	_	1.0	_	1.0		1.0	<u> </u>	1.3	210	1.6	190	1.6		1.0	230	1.0	210	2.0	210	2.3	1.7	
	1.3	200	2.3	210	4.3	200	2.6	200	2.0	210	3.6	200	3.0	200	3.3	240	8.5	220	4.6	220	4.9	220	6.6	2.6	
70	3.9	290	6.6	290	5.6	280	4.6	280	4.6	280	3.9	280	5.9	270	4.3	210	2.0	220	2.3	230	2.6	220	2.3	4.6	Ì
30	3.3	140	4.3	130	3.3	140	3.0	130	3.6	120	3.9	110	4.3	90	4.3	130	2.6	220	1.6	270	2.6	280	3.6	2.7	1
70	7.5	270	7.2	280	6.9	280	6.2	280	7.2	270	6.2	280	7.5	280	6.2	270	5.9	260	5.6	270	5.2	270	4.3	6.7	1
50	9.8	140	11.2	120	12.5	110	13.1	90	12.1	70	14.8	60	14.4	40	11.8	360	7.5	340	8.5	340	10.2	320	13.4	7.9	1
60	4.6	240	3.0		1.3	210	2.6	200	2.0	200	2.0	180	1.6		1.0	130	1.6	180	2.6	160	2.6	180	2.3	6.8	
70	5.9	260	4.9	250	4.9	250	6.2	260	6.9	260	4.9	260	4.9	270	4.6	260	5.2	260	3.3	240	4.9	240	4.9	5.6	1
00	13.8	300	14.8	310	14.4	300	14.8	300	12.1	300	12.1	300	9.8	300	8.5	310	7.9	300	6.6	310	4.3	320	4.3	10 · 4	1
10	7.2	320	8.2	320	6.6	310	5.9	300	5.9	300	7.5	310	8.2	300	8.9	300	6.9	300	6.2	310	5.2	300	4.3	6.3	
70	4.9	60	4.3	70	4.6	20	3.0	340	2.3	320	3.0	300	3.3	300	4.3	310	4.3	300	4.6	300	4.9	300	2.5	3.9	1
20	6.9	320	4.9	330	4.6	350	4.3	330	5.9	330	4.3	330	4.6	340	2.3	350	4.6	350	3.6	20	3.3	360	3.3	5.2	1
30	3.9	320	3.0	310	3.6	300	3.9	310	3.6	300	3.9	290	3.3	290	4.3	310	3.0	290	4.6	290	4.3	300	3.6	3.3	
io	4.9	310	5.9	320	3.6	310	4.3	310	4.9	310	4.3	340	3.9	350	3.3	320	3.9	290	3.6	320	4.3	310	3.9	4.3	1
80	2.3	280	2.3	290	3.3	270	2.3	290	2.0	-	1.0	-	1.3	280	3.0	250	2.0	260	2.0	240	3.3	230	3.6	3.3	
40	1.6	240	2.3		1.0	240	1.6		1.3		1.3	_	0.7	-	0.3		1.0		0.4		1.0	1 -	1.3	1.8	
0	3.0	220	3.6	210	2.6	220	2.3		1.3		1.3	_	1.3		1.3		1.0	_	1.3		1.3	250	1.6	1.6	
90	2.3	290	1.6	290	2.6	290	2.0		1.0	l —	1.3		0.7	l	1.0	<u> </u>	1.3	_	1.3		1.3	l —	1.3	1.5	ı
10	5.6	120	6.6	120	7.5	130	4.6	110	7.5	100	5.2	90	7.5	100	6.9	90	7.9	90	7.2	80	7 · 2	70	7.5	4.6	1
20	3.6	310	4.3	310	5.2	300	5.2	300	4.6	300	4.6	300	4.9	300	4.9	290	4.3	290	4.6	290	3.9	290	4.9	4.6	
10	2.0		0.7	210	2.0	210	2.0	200	2.0	210	3.6	220	2.6	210	4.3	220	5.6	220	5.9	210	3.9	210	3.6	3.5	
	4.8		5.0		4.8		4.4		4.3	l		l	4.5	l	4.4	ļ ———	4.3	_	4.1		4.3	1	4.4	4.5	1

December, 1923.

																							COLLIN	er, it	,20.
0	[m/s.	۰	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	°	m/s.	0	m/s.	0	m/s.	m/s.	
230	2.3	240	3.3	220	2.0	200	1.6	210	2.6	240	2.3	200	2.3	220	2.3	220	1.6	210	2.3	_	1.3		1.0	2.0	I
180	4.6	190	2.6	260	2.6	270	2.6	220	2.6	230	1.6	210 260	1.0	28o	1.0	260	2.0		0.7		1.0	220	1.3	2.5	2
290	2.3	280 150	2·3 6·6	250 150	1.6	260 130	2·3 8·5	270 120	9.2	250 120	3·0 10·5	110	11.1	110	2·6 9·5	110	8.5	120	9.2	110	9.8	230 90	10.5	2·3 5·7	3 4
30	4.6	40	3.0	330	2.0	350	3.0	350	3.0	330	3.3	340	3.3	350	3.0	300	3.9	290	4.3	300	4.6	300	5.2	5.8	5
]]-	-	Τ-		33		33		33		33	0.0	٥,					0 ,	-	, -			_			
220	2.0		1.3	_	1.3		1.3		0.3	220	1.6	200	2.0	200	2.0	220	3.9	210	3.9	200	2.6	210	3.6	2.7	6
180	9.2	180	7.9	180	7.5	190	6.9	180	8·2 9·2	180 320	8·2 9·2	180 300	7.9	170 300	6·6 7·2	180 300	7·5 5·6	180	6.6	180 - 290	6·2 4·6	190 290	4·3 4·6	6·7	7 8
260	3.6	310 250	3.6	310 230	3.0	310 220	2.0	310 220	3.3	220	5.2	220	7.5 5.2	220	4.9	210	4.9	210	4·9 4·3	210	4.9	210	5.2	4.0	9
210	1.6	210	2.0	220	3.0	220	3.6	210	3.3	210	3.6	220	3.6	220	3.6	190	2.3		1.3		1.3	180	1.6	2.8	10
													_					-0-				100	- 6		
200	5.9	200	4.9	200	3.6	200	4.6	200	6.9	200	4.9	190	5.9	200 220	4.6	200	4·9	180 220	3.6	190 210	5·2 1·6	190	5.6	3.8	11 12
220	2.3	220	3.9	210 280	5.6	220 260	3.3	210	3.3	210 220	4.3	220 240	2.3	220	2.6	220 220	2.0		1.3	210	5.2	220	1·3 5·6	2.5	13
210	3.0	290 210	4.9	240	3.3	290	5.9	280	4.6	280	4.3	270	4.3	260	6.9	270	5.6	280	6.2	280	5.2	280	5.2	5.4	14
270	2.3	280	3.0	280	3.0	260	3.6	240	2.6	250	3·ŏ	230	3.0	240	4.3	230	3.9	220	3.9	210	3.3	200	3.3	4.6	15
													. 6	220		200	2.0	220	2.0		7.2		T. 2	F.,	•6
280	8.9	290	9.8	290 220	9.2	310	7.9	320	5·6	320 290	4·6 6·2	310 330	4·6 5·2	320 320	4·3 5·6	300 200	3.3	320 280	3.9	260	2.3	290	1·3 5·9	5·3 3·5	16 17
300	16.1	240 300	5.9	300	15.4	230 300	13.8	270 300	13.8	310	9.5	310	9.8	310	7.5	300	7.2	310	8.2	310	9.5	310	8.9	1Ŏ Î	18
310	11.8	310	11.1	310	11.8	300	10.2	310	10.2	320	7.2	340	6.9	340	5.6	350	6.9	360	4.3	360	3.9	320	4.9	7.9	19
330	7.5	320	7.9	320	6.9	320	6.9	320	6.9	310	5.6	310	4.9	320	5.6	330	5.9	330	4.3	330	5.9	340	7.2	6.8	20
200	2.6		2.6	200	2.0			400	2.6	200	2.0	250	1.6		1.3		1.0	200	1.6	200	2.3	200	3.3	3.4	21
300	2.6	310 320	3·6 9·8	300 320	3.0	300 320	2.3	290 310	2.6	290 310	2·0 9·5	250 300	9.5	300	6.6	300	6.2	290	5 2	290	3.9	300	$6 \cdot 2$	6.0	22
320	9.2	320	10.2	310	6.6	300	6.6	280	3.3	250	2.6	270	3.9	270	4.3	280	3.9	290	5.9	290	5.6	280	4.9	7.8	23
40	8.9	20	5.6	350	3.0	340	3.0	290	3.3	300	3.3	290	3.6	290	4.6	290	3.9	290	3.6	280	3.9	280	3.3	4.8	24
-	1.3	250	1.6	_	0.3		0.3		1.3	150	3.0	170	3.0	160	3.6	160	3.0	150	4.3	100	3.0		1.3	2.8	25
_	1.2	290	2.0	300	2.6	290	2.6	290	2.3	300	2.0	300	2.6	300	3.0	290	1.6	300	2.6	300	2.3	110	2.6	2.2	26
	1.3	290	1.0	240	2.0	240	2.3	230	1.6	300	1.0	J	0.7	300	0.3		1.0	310	1.6	310	2.3	310	2.6	1.4	27
320	2.6	310	3.6	310	3.6	310	3.0	300	3.0	300	3.3	310	3.6	310	3.9	310	3.9	300	4.9	300	3.6	290	2.3	3.9	28
_	1.3	220	2.0		1.3	200	2.3	210	2.3	200	2.3	200	2.6	210	2.3	200	2.3	200	2.0	200	2.3	190	3.6	2.2	29
170	8.9	170	9.2	170	8.5	170	8.2	170	7.2	170	5.2	170	6.2	180	5.2	180	4.6	190	5.2	190	4.6	190	3.6	6.9	30
	0.3		0.3		1.3		0.7		0.7	_	0.7	_	1.0	260	2.6		1.3		0.7		0.3	280	2.0	1.4	31
_	5.3		5.3		4.8	_	4.7	_	4.6	_	4.4	_	4.3		4.2	_	3.9		3.7	_	3.7	_	4.0	4.2	
	1				<u> </u>	<u> </u>	<u> </u>			<u> </u>			l	<u> </u>			<u> </u>	<u> </u>		<u> </u>	1	<u>. </u>	<u> </u>	!	
i	3.	1	4.	1	5.	,	16.	1	7.	1	8.	,	9.	. 2	о.	2	I.	2	22.	2	23.	. 2	4.	Mean	Day.

[†] Directions obtained from records of the Dines Tube Anemograph. * Speeds obtained from records of the Robinson Cup Anemograph.

HIGHEST INSTANTANEOUS WIND SPEED RECORDED EACH DAY BY THE DINES TUBE ANEMOGRAPH.

95. Aberdeen: $H_a = 8$ metres + 13 metres.

1923.

	J. AI	701 UCC1	1 . 110	a = 0	metre	5 + 13	men	CS.									_		_				192	J.
	Ј	an.	F	eb.	М	ar.	A ₁	pril	М	ay	Jı	ine	J	uly	A	ug.	Se	ept.	С	Oct.	N	ov.	D	ec.
Day.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Tim of Gus
1 2 3 4 5	m/s. 10 17 20 12 18	h. m. 3 40 5 10 3 40 3 40 9 30	m/s. 20 17 17 12	h. m. 3 10 4 5 9 10 23 55 9 20	m/s. 9 14 4 8	h. m. o 50 9 25 3 10 9 55 12 45	m/s. 16 12 9 14 15	h. m. 2 50 0 5 14 45 10 15 22 55	m/s. 11 13 11 13 11	h. m. o I 7 45 5 55 16 5 12 25	m/s. 11 12 16 13	h. m. 14 55 21 40 13 40 11 55 19 15	m/s. 7 13 13 11 8	h. m. 9 55 23 15 15 20 14 35 10 15	m/s. 9 11 24 17	h. m. 8 30 19 55 13 20 9 55 15 0	m/s. 8 13 11 12	h. m. 8 15 10 55 14 0 10 45 16 50	m/s. 15 18 11 14 13	h. m. 12 20 11 15 14 45 4 30 11 30	m/s. 9 13 25 23 11	h. m. 13 5 19 30 12 30 1 50 1 0	m/s. 9 15 8 19 18	h. n o 3 io 3 8 5 i9 2 2
6 7 8 9	8 11 12 21 25	23 40 1 5 4 20 21 35 14 5	22 30 24 16 25	10 25 12 40 9 40 23 40 11 35	10 10 10 6 15	13 30 23 50 1 25 11 0 21 40	17 15 15 14 22	22 15 0 30 3 25 23 40 6 45	16 14 13 15	15 50 13 40 14 0 19 50 15 40	13 11 18 17 21	8 25 16 15 18 0 7 0 10 5	10 9 9 9 7	12 45 20 45 16 55 10 45 18 10	13 8 10 13 14	12 25 23 10 19 30 18 15 16 0	14 15 11 17 13	21 0 8 50 13 10 10 0 12 30	28	13 25 11 10 23 55 14 45 15 40	16 17 15 15	22 45 3 15 0 35 13 0 7 55	11 20 21 11	3 5 17 4 10 4 22 4 0 2
11 12 13 14 15	22 7 13 24 23	10 5 6 45 22 10 23 30 2 30	15	7 25 I 5 2I 50 I 30 23 20	16 19 18 5 8	23 0 8 45 2 45 18 30 11 20	13 5 10 9	7 20 10 0 8 40 5 55	20 19 15 16 8	10 15 10 45 13 0 0 40 12 35		8 50 16 40 7 5 11 35 11 30	7 9 7 9	10 55 14 15 14 0 14 40 13 5	8	8 40 14 50 15 5 16 15 16 25	14 12	17 40 12 25 18 5 13 35 21 5	13	11 45 1 25 13 45 12 25 11 55	14 8 20 23	21 5 13 35 13 40 13 20 19 15	15 15 11 24 16	18 3 5 3 4 9 3 3
16 17 18 19 20		17 40 12 15 21 50 19 5 7 45	22 15	23 25 23 5 5 35 1 20 22 55	6	0 35 14 10 13 50 14 45 11 25	9 11 9 9 14	18 45 10 50 12 45 5 30 15 40	24 11 11	12 45 7 50 1 15 12 40 19 55	14 11 11 13	10 50 6 35 14 40 13 5 12 55	12 15 9 12 16	18 10 13 40 8 55 16 35 14 10	11 10 5	11 5 7 10 9 20 15 0 13 25	21 18 10	10 25 18 15 0 20 11 55 12 35	13 12 21	12 40 11 25 19 50 8 50 11 45	28 14 25 18 12	3 0 10 10 15 55 1 15 12 15	20 16 29 20 18	13 3 12 1 12 5 13 4 5 2
21 22 23 24 25	21	23 30 19 20 20 15 4 45 8 40		6 55 0 25 22 0 22 30 22 45	5 16	12 30 13 45 17 55 12 10 22 15	19 8 18 15	9 10 11 5 15 5 9 0 5 55	* 12 14	15 15 * 16 20 20 40 17 10	15 19 23 12	11 50 9 30 16 20 2 50 14 15	15 12 13 10 14	12 30 12 55 13 50 9 50 17 30	16 13	16 0 10 35 22 40 12 35 0 10	10 { 5	18 0 12 35) 15 15) 22 40 23 50 7 25	15	5 45 24 0 0 50 12 40 23 15	12 10 10 11 8	16 0 2 40 11 55 5 30 6 5	14 19 21 15	1 30 15 30 4 3 12 20
26 27 28 29 30	15 13 8	12 45 12 5 16 25 21 10 1 35	ł	17 50 0 50 0 30	11 9 5 7	0 15 15 45 12 25 12 35 15 40	19 14 12	21 5 1 25 17 5 17 25	15 13	9 15 21 35 11 15 *	14 6	10 20 17 40 22 15 1 20 7 25	17 10 12 9	20 45 0 5 6 20 12 40 13 45	11 12 12 11	14 5 13 45 16 15 21 35 11 35	9 12 16 8	1 40 22 35 0 55 4 45 16 30	14 21 19	8 40 9 0 3 0 19 15 21 15	15	2 15 16 10 15 30 5 15 21 20	* * 13 7 21	* * 7 4. 17 2. 9
31	19	22 55		-	13	22 45	-	-	9	10 55	-		9	13 20	9	12 45		-	14	0 40	_	-	10	1 5

^{*} Defective Record.

DISTRIBUTION OF WIND SPEED: EXTREME VELOCITIES AS RECORDED BY THE DINES TUBE ANEMOGRAPH.

		1	DISTRIBU	TION O	F WIND	SPEED.					4	EXTRE	ME VEL	OCITIES.			
Month		More than 1	7 ·1 m /s.	10·8 to	7·1 m/s.	5·5 to 10·7 m/s.	1.6 to 5.4 m/s.	Less than 1.6 m/s.	No Record.	н	lighest Ho	urly Wind		Н	ighest G	ust.	
	•	Dates of Occurrence.	Duration.	No. of Days.	Duration.	Duration.	Duration.	Duration.	Duration.	Veer from N.	Speed.	Mi Tin		Speed.		Da te	
Jan	•••	_	hr.	5	hr. 16	hr. 287	hr. 396	hr. 45	hr.	° 300	m/s. 13	day.	hour. 19	m/s. 26	day.	h. 19	n
Feb		10th, 26th	9	18	200	302	156	5		110	19	26	$\begin{Bmatrix} 18 \\ 19 \end{Bmatrix}$	30	7	12	4
Mar	•••	decourse		2	7	114	469	154	-	150	12	12	20	19	12	o 8	4
April			. —	6	30	349	284	57		60	14	10	8	22	10	o 6	4
May		-		5	21	307	346	70		10	14	11	10	24	17	07	5
June		-	_	4	28	261	381	50		220	13	10	11	23	13	07	О
July		-	-			146	449	149		310	9	26	21	17	26	20	4
Aug	•••		-	2	9	202	456	77		140	14	2	20	24	3	13	2
Sept		-		3	19	184	453	64	-	180	13	17	19	23	12	12	2
Oct			-	6	21	256	417	50		260	15	9	15	28	9	14	4
Nov			_	6	36	272	357	55		330	16	16	1	28	16	оз	0
Dec				8	42	267	380	55		300	15	18	13	29	18	12	5
Yea r.		2 days	9	65	429	2,947	4,544	831		110	19	Feb. 26	{18 ₁₉ }	30	Feb. 7	12	49

97. Aberdeen.

Readings, in degrees absolute, at 9h., Greenwich Mean Time.

1923.

Day.	Jan.	Feb.	Mar.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.
I	78·5	78·o·	77.8	79.0	79.7	8 o · 8	83.1	85.1	84.9	83.6	81.7	78.6
2	78.4	78 · 1	77.8	79.0	79.7	80.9	83.2	85.1	84.9	83.6	81.7	78.4
3	78 · 3	78·1	77.8	79.1	79.8	0.18	83.3	85.1	84.8	83.7	81.7	78.3
4	78.2	78.2	77.8	79.2	79.9	81.1	83.3	85.1	84.7	83.7	81.6	78.3
5	78.2	78.3	77.9	79.2	8o·o	81.2	83.4	85·o	84.7	83.6	81.5	78.1
_	•		,,,				-3 4	-,,	94 /	03.0	01.3	78.1
6	78.2	78.3	77.9	79.3	80.1	81.2	83.6	85.0	84.7	83 4	81.4	78.1
7	78·1	78.2	77.9	79.3	8o·3	81.3	83.7	85·o	84.6	83.4	81.3	78·o
7 8	78·1	78.2	78.0	79.3	80.6	81.4	83.8	85.0	84.6	83.3	81.1	77.9
9	, 78∙o	78.2	78.0	79.3	80.6	81.4	84.0	85.1	84.6	83.3	81.0	
10	, 77·9	78.2	78·o	79.2	80.6	81.6	84.1	85.1	84.6	83.1	80.8	77.9
	11 >	/	,,,,	192	00 0	01 0	04 1	05.1	04.0	03.1	00.0	77.8
11	77.9	78.3	78·1	79.2	80.7	81.7	84.3	85.2	84.6	83.1	80.6	0
12	77.9	78.2	78·I	79.2	80.8	81.7	84.4	85.2	84.6	82.9	80.4	77.8
13	77.9	78.3	78·I	79.2	80.7	81.8	84.6	85.3	84.5	82.8		77.8
14	77.9	78.3	78.1	79.2	80.6	81.0	84.5		84.5		80.3	77.8
15	77.8	78.3	78.2	79.2	80.6	82.0	84.7	85.4	84.4	82.8	80.3	77.8
*3	// 0	70 3	70.2	/9-2	30.0	02.0	84.8	85.5	84.4	82.7	80.3	77:9
16	77.8	78.3	78.2	79.3	80.5	82.1	84.9	85 5	84.4	82.6	80.2	
17	77.8	78.3	78.2	79.3	80.4	82 1	85.0	85.5	04.4			77.9
18	77.8	78.2	78.3	79.4	80.5	82.1	85.1	85.5	84.4	82.4	80·1	78·1
19	77.8	78.2	78.3		80.5	82.2		85.5	84.3	82.3	79.9	78·1
20	77.8	78 2		79:4			85.2	85.4	84.3	82.2	79.8	78·1
20	77.0	76-1	78.3	79.4	80.5	82.2	85.2	85.4	84.2	82.2	79.6	78.2
21	77.8	78.0	78.3	79.5	80.4	82.2	85.2	8	8	82.2		-0
22	77.8	77.9	78.4	79.6	80.5	82.3	85.2	85.4	84.1	82.2	79.4	78 · 1
23	77.8	77.9	78.4	79.6	80.6	82.4		85.3	83.9		79.4	78.0
~2 ₄	77.8	77.8	78.5	79.6	80.6		85.3	85.3	83.9	82.2	79.3	78·o
25	77.8	77.8	78.6		80.6	82.4	85.3	85.3	83.8	82.2	79.2	77.8
23	77.0	// 0	78.0	79.6	90.0	82.6	85.3	85.3	83.7	82.1	79.1	77.8
26	77.8	77.7	78.6	79.6	80.6	82.8	8	85.0	82.6	00.7		
	77.8	77.7	78.6	79.6	80.6	82.8	85.4	85.2	83.6	82.1	79.1	77.8
27 28	77.8	77.8	78.7				85.4	85.2	83.2	81.9	78.9	77.7
	77.8	77.8		79.7	80.7	82.8	85.3	85.1	83.4	81.9	78.8	77.6
29 30	77.0		78·8 78·9	79:7	80.7	82.9	85.2	85.1	83.4	81.8	78.7	77.4
30	77:9		70.9	79.7	80.7	83∙0	85.2	85∙0	83.5	81.7	78.6	77.4
31	78·o	_	78.9	_	80.7		85.2	85·o		81.7		77.2
Mean	77:9	78⋅1	78.2	79.4	80.4	81.9	84.6	85.2	84.3	82.7	80.2	77.9

MINIMUM TEMPERATURE "ON THE GRASS" DURING THE INTERVAL 18h. TO 7h.

98. Aberdee	n.			Rea	adings, in	degrees a	bsolute.					1923.
Day.	Jan.	Feb.	Mar.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
I 2	a. 68·6 68·6	a. 78·0 77·4	a. 74·7 73·0	a. 76·9	a. 75·2	a. 74 · I	a. 81·4	a. 83·3	a. 75.9	a. 79·3	a. 72·1	a. 72·1
3 4	74·7 73·6 69·1	71·9 71·3 74·1	73.0 74.1 72.4	77.4 78.0 76.3	76·3 71·9 71·9	78·0 81·3 75·2	78·7 84·8 75·2	74·6 83·5 79·7	78.6 71.8 82.1	77·6 72·0 75·4	71·4 78·1 73·4	72·9 71·4 66·7
5 6	66 · 3	78.6	71.9	75·2 75·8	74·7] 75·8	76·3 74·1	79·7 84·0	76·9 79·0	76·2 79·6	70.7	73.7	75·5 70·2
7 8 9 10	70·2 70·8 68·6 74·1	73.0 78.0 69.7 72.4	71·3 77·4 73·0 71·9	74·7 76·3 74·7 73·0	67·4 .70·2 69·1 69·7	71·3 75·8 80·8 83·0	81·3 82·0 80·7 81·2	80·6 82·8 85·3 76·9	77·9 72·7 78·5 72·8	72·4 73·6 79·2 73·1	73.0 72.4 68.3 68.6	69·2 77·4 69·0 73·6
11 12 13 14	74·1 70·2 66·9 74·7 75·2	77:4 77:4 76:9 74:7 73:0	75·8 75·2 75·2 70·2 74·7	73·6 77·4 75·8 79·1 71·3	70·2 74·1 74·1 72·4 70·8	78·0 75·8 83·0 77·4 69·1	85·0 81·8 83·6 79·5 85·3	78·6 77·6 85·1 75·6 73·1	80·9 82·2 73·1 83·2 77·9	74·1 70·9 76·4 69·1 73·4	70·8 81·1 74·7 73·6 65·4	74·5 79·8 76·8 70·4 73·0
16 17 18 19 20	74·1 72·4 69·7 73·0 73·0	74·7 74·7 74·1 74·7 73·6	75·2 69·7 74·7 68·0 73·6	77.4 73.6 70.2 74.1 73.6	75·2 73·0 73·0 75·8 77·4	73.0 76.3 79.7 77.4 77.4	82·1 77·8 75·0 79·2 85·1	77·9 82·1 82·8 81·8 79·6	77 · 4 72 · 9 80 · 2 72 · 8 69 · 4	74·1 70·4 77·6 82·6 74·7	73·8 68·3 70·9 73·6 73·1	74·4 73·4 75·4 69·1 70·7
21 22 23 24 25	71·3 79·1 70·2 75·8 73·6	72·4 73·6 72·4 73·0 75·2	70·2 70·2 73·6 77·4 68·6	74·7 72·4 71·3 69·7 74·7	73.0 70.2 66.3 68.6 75.8	79·7 84·1 84·1 81·9 75·8	79·2 85·4 85·9 79·6 76·4	84·4 76·5 73·4 82·4 75·2	72·4 73·0 73·1 71·9 81·4	81·2 73·2 74·9 78·2 70·6	72·6 73·8 71·4 69·7 66·4	70·1 71·9 72·2 69·9 67·4
26 27 28 29 30	76·9 73·6 73·6 76·3 75·2	74·7 76·3 78·0 —	70·2 75·8 75·2 75·2 72·4	77·4 70·8 66·9 68·0 74·7	76·3 78·6 76·3 71·3 78·0	73.0 79.1 82.4 82.4 81.9	77·4 79·1 82·6 81·6 81·8	77·6 75·7 75·7 70·3 80·9	75·7 80·8 83·6 79·0 79·2	73·2 70·9 79·2 73·7 82·3	67.8 68.5 69.8 73.6 69.3	70·5 69·7 72·2 68·2 73·5
31	73.6		76.9		78.6		78.6	79.9		75.4		74.9
Mean	72.5	74.7	73 · 2	74.2	73·3	78·o	81.0	79.0	76.9	74.9	71.7	72 · 1

⁻⁽¹⁾ The initial 2 or 3 of the readings is omitted, i.e., 275.0 degrees absolute is written 75.0.
(2) The minimum "on the grass" refers to the interval from 18h. the previous day to 7h. on the day to which it is entered.

99.	Aberdeen.	

		Cloud Forms.					Am Forn						Weat	her.			
Day.	7h	13h	18h	7h	9h	13	h 15	h	8h 2	2 I h	7h	9h	13h	15h	18h	21h	Remarks.
1 2 3 4 5	Nb. A. Cu. Nb.	Nb. St. Cu. Ci. St. : Ci. Cu. Nb.	CiSt. St. Cu. St. Cu. Ci. St.: St. Cu. Nb.	- IO 2 - IO	I 10 2 I 10	- 10 9 2 10	10 7 1		6 1 2	10 5 10 7	1	□ • · · · · · · · · · · · · · · · · · ·	 •° 		• [:.]	• • • • • • • • • • • • • • • • • • •	b $\sqcup a : b \text{ to } bc \equiv^0 \square p : c \equiv^0 \text{ to } o \equiv^0 n :$ $\bullet \equiv^0, \bullet^0 g \equiv^0 a : \bullet^0 \equiv^0 \text{ to } bcq p : bcq n :$ $b, b \text{ to } o a : o \text{ to } bp : b \text{ to } o \bullet n :$ $\bullet^0 \text{ to } ba : b, b \sqcup \equiv^0 p : c \equiv^0 n :$ $c \text{ to } o \bullet, \bullet^2 q \equiv^0 a : \bullet \& \bullet^2 \equiv^0 p : \bullet \text{ to } o n :$
6 7 8 9 10		Ci.: St. Cu. Cu.: Fr. Cu. St. Cu. Ci.: Cu.Nb.: Fr.St.	Ci. St. Nb. — St. Cu. : Fr. St. Nb.	- 10 5 1 8	- 10 5 2 9	8 2 1 10	10 1 6	10	8 1	10 10 - 10 5	□ •	<u>j</u> :: : : : : : : : : : : : : : : : : :			p ●		$[to o \stackrel{\bullet}{=} n:]$ o to b \coprod \equiv 0 to b $a: b \equiv$ 0 & $\equiv p: b \equiv$ 0 o \bigoplus 0 to c $a: c$ to o \equiv 0, \bigoplus p: \bigoplus to o o \equiv 0 to b & bc $a: b \not = n:$ $[\equiv 0 \ n:]$ b to p \bigoplus q to bq $a: b \otimes b$ cq $p: c \otimes c$ qcp c $\otimes c \otimes c$ q. \bigoplus \bigotimes \bigotimes a: bc \bigotimes oqp \bigoplus p \bigotimes n: $[\bigoplus$ 0 n:
11 12 13 14 15	St. Cu. St. Cu. : Cu. Nb. Ci. St. Nb. St. Cu.	Cu.: Cu. Nb. Ci.: St. Cu. Ci. St.: St. Cu. St. Cu. St. Cu.	St. Cu. CiA. St. St. Cu. St. Cu. St. Cuf.	1 5 10 10	8 7 10 2 3	5 5 2 1 8	2 I I	1	2 I I	1 – 10 – 1	 p ★º- 	::: = :::		 p ●°		 ப 	b to cq, p
16 17	St. Cu.	St. Cu. : St. A. CuSt. Cu.	St. Nb.	10	10	9				8				•	 • 0		$ \begin{array}{l} o \equiv^{0} \& \equiv a : o \bullet^{0} \equiv^{0} \text{ to c } p : c \equiv^{0} n : \\ \text{bc, b} \equiv^{0} \text{ to } \equiv a : \text{b to o } \equiv^{0}, \bullet^{0} p : \bullet^{0} \text{ to } \\ \vdash c n : \end{array} $
18 19 20	St. Cu. St. Cu. Cu. Nb.	Ci.: St. Cu. A. St.: Cu.: Fr.Cu. Cu. Nb.	A. St. ————————————————————————————————————	2 10 7	1 10 6	2 10 8	8	-	- -	8 -	 * P		 ₩° ▲ °p		 *º▲º p		b \sqcup early, b a : b to o \equiv 0 p : c $\overset{\land}{\circ}$ o \equiv 0 n : o \equiv 0 to oq a : oq to bq p : bq n : p \not , \not \not q a $\overset{\hookleftarrow}{\circ}$ p : b n :
21 22 23 24 25	St. Cu. St. Cu. A. Cu.: St. Cu. Ci. St.: St. Cu. St. Cu.	Ci. Cu. : St. Cu. Nb. Cuf. A. St. : St. Cu. CiCi. St. : Cu. Ci. St. : Cu.	St. Cu. St. Cu. St. Cu. Ci. St. : St. Cu. Ci. CuCi. St.	10 1 7 3 2	9 1 9 5 3	3 10 10 5 6	10	5 2	1 5 2	- 2 2 2 6			•	 • 		 Ü	b to o $a : c \equiv^{0}$ to b $p : b n :$ b $a : o \bigoplus$ to b $p : b n :$ c & o \equiv^{0} $a \& p : b \equiv^{0} n : \bigoplus$ 19h. b & bc $a, p \& n :$ b & bc $a, p \& n :$
26 27 28 29 30	Ci. : St. Cu. A. St. : St. Cu. St. Nb. Nb.	Ci.CuA.St.: St.Cu. St. Cu. : St, Nb, Nb. Nb.	Nb.	10 10 10	10 10	6 10 10 10	10	10	0 I	0	 •0 •0	 • ° • °	 •°	 • • 0 • 2	 •	 •	b & c a, p & n: c & o a:
Mean Claud	St.	Nb.			10		-	- -	- -	<u>I</u>		=	•				$o \equiv^0$, $\equiv to \bullet a : p \bullet p : bq n :$
Cloud Am'nt			<u>'</u>	5.8	5.1	6.3	6.3	3/5.	6 5	.8							
100.	Aberdeen.		3		·						-		'		1		February, 1923.
1 2 3 4 5	Ci.: St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.	Ci.: St. Cu. St. Cu. A. St.: St. Cu. Ci. St. Cu.: Fr. Cu.	St. Cu. St. Cu.: Fr. Nb. Ci. St. Nb.	I - I 2 IO	1 - 7 1 9	1 1 5 1 8	7 1	8	8 1	- 8 0					 b ● ₀	• 	b $a & p : b$ to o, o \bigcirc , p \bigcirc n: q early, fine throughout. b & cq $a : cp \bigcirc$ p \bigcirc n: b $a & p : b$ to o n: oq $a : c & oq$, \bigcirc p: \bigcirc n:
6 7 8 9	A.St. : St.Cu. : Fr.St. Cu. Nb. St. Cu. Nb.	Nb. Nb. Nb. Fr. St. Nb.	A.St.: Fr.St. : Fr.Nb. St. Cu. St. Cu.	I IO 2	10 10 7	10 10 1 1	10	10	0 I	1 0 0	 •] •°	 • 2 	● ² ★ ² .:	• 2 ··· ··· ··· ···	··· ··· • ···	• • °	$\begin{array}{c} \text{oq, } \bullet^2 a: \bullet^2 \text{ to } \bullet p & n: & [b \equiv^0 n: \\ \bullet \text{ early, b to o, } \bullet \& \bigstar^2 a: \bullet^2 p: \text{ oq to } \\ \bullet \& \bullet^2 \text{ q } a & p: \text{ oto o} \bullet^0 n: & [\equiv^0 p & n: \\ p \bullet^0 \text{ early, b} \sqsubseteq \bullet^0 \& c \equiv^0 a: b & \infty \text{ to o} \\ \text{oq, } \bullet^0 \text{ to } \bullet^2 \swarrow^1 \text{ q } a: \bullet \swarrow^p : \bullet \text{ q } n: \end{array}$
11 12 13 14 15	Nb. Nb. St. St. Nb. Cuf.	Nb. St. Cu. : Fr. St. Nb. Nb. Cuf. Nb.	St. Cu. ; Fr. St. Nb. Nb.	01 01 01	10 10	10 6 10 10	9 10 10	10	9 0 0 10	9	●° ●° … *°	 • 0 • 0 • 0	 •° •°	•	 • • •	• 0 • • 0 • 0	$ \begin{array}{l} $
16 17 18 19 20	Nb. St. Cu. : St. St. Cuf. St. Cuf. St. Cuf. St. Cu. : St. Cuf.	Nb. St. Cuf. St. Cuf. St. : St. Cuf. Nb.	St. Cuf. St. Cuf. St. Cu. : Cu.	10 10	10 10	10 10	10 10	10	O 10 O 10 O 10 O 10	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	• 	• *	●° *°	● *° p		* °	● q \equiv ⁰ throughout. ● early, oq, p \bigstar a : o \equiv ⁰ p \approx n : Dull and squally throughout. o \equiv 0 a : p \star 0 p : o \equiv n : p \star 0 $\stackrel{\circ}{\star}$ * \star 0 $\stackrel{\circ}{=}$ 0 throughout. $\stackrel{\smile}{\star}$ trace.
21 22 23 24 25	Nb. Nb. St. Cu. : Fr. St. St. Cu. : St. St. Cu. : Fr. St.	Nb. Nb. St. Cu. : St. St. Cu. : Cu. Nb.	A. St. : Cu. Nb. Nb. Cuf.	10 3 10	10 4 10	10 9 9	10	10	O I O I O I O I O	0 9 10	 •° 	* • ° · · ·	₩° ··· ··· ··· ··· ··· ··· ··· ··· ··· ·	*° p •°	*° p ●°	• ° · · · · · · · · · · · · · · · · · ·	$\begin{array}{l} & & & & & & & & & & & & & & & & & & &$
26 27 28	St. Nb. Nb.	St. Nb. Nb.	Nb.	10		10	10	10		0	 •° •°	• ° • ° • ° • ° • ° • ° • ° • ° • ° • °		•	 • _W	● _ш ● 0 ···	$\begin{array}{ll} \bullet \text{ early to } 0 \equiv^0, \ \bullet \ q \equiv^0 a : \bullet \ \downarrow q \equiv^0 \\ \bullet \ q \equiv^0 a \text{ \& } p : 0 \equiv^0 \text{ g to } \bullet^0 n : \ p \text{ \& } n : \\ \bullet^0 \equiv^0, \ \bullet \ a \text{ \& } p : \bullet^0 \equiv^0 n : \end{array}$
Mean Cloud Am'nt				7.9	8·5	8·3	8.	5 8	.96)·2							
7	7h	.13h	18h	7h	9h	131	151	h I 8	8h 2	1 h	7h	9h	13h	15h	18h	21h	Remarks.
Day.		Cloud Forms.			Clou (A		Amo						Weat	her.			

4	01	A	h	01	rd	۵	^	n
1	u	A	U	ш	w	u	u	Н

		Cloud Forms.			Clou (A)		4mc						Wea	ather.			Remarks.
Day.	7h	13h	18h	7h	9h	13h	15h	18	h 21	t h	7 h	9h	13h	15h	18h	21 h	Remarks.
1 2 3 4 5	Nb. Nb. Nb. St. Cu. : St. St. Cu. : St.	A.St.: Nb.Cuf. A. Cu.: Fr. Cu. Nb. Cu.: Cu. Nb. Nb.	A. St. : St. Cuf. St. Cu. Nb. St. Cu. St. Cu. : Nb. Cuf.	10 10 8 10	10 10 5	10 7 10 6	10 7 10 7 2	10	2 10	9 7 0 8 5	• ° · · · · · · · · · · · · · · · · · ·	•°		 • 	•		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
6	A. Cu. St. Cu. : St.	A. St. : Fr. St. Ci. : St. Cu. : Cu.	A. St. : A. Cu. St. Cuf.	4 10	9	3	3			0					d ::		bc to $o \equiv^0$, \bullet^0 $a : p \bullet^0$, $b \equiv^0 \frown p : [b \equiv^0 n : p \bullet \text{ early, o to } b \equiv^0 a : b \text{ to } o \equiv^0 p : [o \equiv^0 n : b \bullet o \equiv^0 p : b \bullet o \equiv^0 n : b \bullet o \equiv$
8 9	St. : Fr. St. St. Cu.	Nb. St. Cu. : Cu.	Nb. St. Cu. : Cu.	10 10	10	10 2	10	1	3 I	0		•	•°	•0		•	
10	St. Cu. : St.	A. St. : St. Cuf.	St. Cu. : St. Cuf.	10	10					0					 p●▲º	P●	
11 12 13 14 15	St. Cu. : St. Cuf. St. Cu. A. St. : Fr. St. Ci. Cu. : Ci. St. St.	St. Cu. : St. Cuf. A. St. : Fr. St. Fr. Cu. Ci. St. Cu.	Nb. Cuf. Nb. St. Cu. St. St. Cuf.	10 3 3 10	10 1 1 2 10	6 10 1 1	10 2 -	10	0 I 2 7 I	0 0	 					• • • •	oq $\equiv a : \bigoplus^{0} q \equiv^{0}$ to $\bigoplus^{0} p \not \subseteq n :$ o early, $b \equiv^{0} a : by p : b n :$ b \sqsubseteq , $\equiv^{0} a : b, c \equiv^{0} p : o \equiv : n :$ Dull throughout.
16 17 18 19 20	St. St. St. Cuf. Ci. St. St.	Fr. St. : St. Cuf. St. Cuf. St. Ci. St. : Fr. St. St.	St. Cuf. St.: Fog St.	10 9 9 2 10	10 9 1 5 8	6 5 1 5	4 1 10	I	5 I - I	7	 =	 ≡⊕ 	 		= 	=	o to be $a: bc & c p & n:$ $o \equiv 0 \ a: bc, \equiv : p & n:$ o to $b \equiv 0 \ a: b \equiv 0 \ p & n:$ $b \equiv a: bc \equiv to o p: o \equiv 0 \ n:$ $c \& o a: o - b p: b \equiv 0 \ n:$
21 22 23 24 25	St. St. St. Nb. Ci.: A. Cu.: St.	Fr. St. CiCi. Cu. St. Cu.: St. Cuf. St.: Fr. St. Ci.: Ci. Cu.	A. Cu. : St. Cuf St. Cuf. St. : Fr. St. Ci. : St. Cu.	10 10 10	1 - 10 10 4		6 8	I	7 1 0 1 9	 10 10 6 2		 ≡i •°	∷ ⊕ ∷ ∷				$b \equiv^{0} \text{ to } \equiv, \equiv^{0} a : b \equiv^{0} p $
26 27 28 29 30	Ci. Wet Fog St. Cu. : Nb. Fog St. : Fog	Ci. St.: Fog A. Cu. St.	Ci.: St. CiCi. Cu.: A. Cu. St.: Fog Ci. St.: Fog	2 10 10 10		9	10	5	I I	5 6 10 10	 =: =: =: =: =:	=		⊕ 	 =:	 = =:	1
31 Mean	Fog	Fog.	St.	10	10	10	10		0	10	<u>≡i</u>	<u>≡</u> :	=:		-		$\equiv a \otimes p : 0 \equiv^0 n :$
Cloud Am'nt				8.3	7.2	6.	06.	0 6	0.2	7.3				-			
102.	Aberdeen.				1						1	1	1	1	1	1	April, 1923.
1 2 3 4 5	St. Cu.: St. Cuf. Nb. St. A. Cu.: St. Cu. Ci.St.A.St.:Fr.St.	Nb. St. St. A. Cu.: St. Cuf. Ci.:A.Cu.:St.Cuf.	Nb. Nb. Ci.:Ci.Cu.:St.:Fr.St. St. Ci.: St. Cuf.	10	10	10	10		7	10 10 5 10 6	 •° 				• • • • • • • • • • • • • • • • • • •	• 0 ····	$ \begin{array}{l} \operatorname{op} \bigotimes^{0} a : \bigoplus \& \bigoplus^{2} \cong^{0} p \otimes n : \\ \bigoplus, \bigoplus^{0}, \operatorname{o} \equiv^{0} a : \operatorname{o} \equiv^{0} p : \bigoplus^{0} \equiv^{0} n : \\ \operatorname{o} \equiv^{0} a \otimes p : \operatorname{bc} \equiv^{0} n : \\ \operatorname{c} \& \operatorname{o} \equiv a, p \otimes n : \\ \operatorname{Mainly bc} \& \operatorname{c} \equiv^{0} \operatorname{throughout} \end{array} $
6 7 8 9	St. Cu.: St. Nb. St. Cu.: St. Cuf. St. Cu. Nb.	Nb. : St. St. Cu. : St. Cuf. St. Cu. Cu. : Fr. St.	St. Cuf. : Fr. St. St. St. Cuf. Cu. Ci. : Ci. Cu. : Cu.	10 10 10 10	10 10 9	8	10	3 1		10 10 9 - 8	 p●⁰ •	•° ···	P●°				oq, $p 0^0$, $p 0^0 0^0$ a, $p 0^0$ n: op $ 0^0$, $p 0^0 0^0$ a: $o 0^0$ $p 0^0$ n: c & o throughout. o a: c & o p: b & bc n: bc, $ 0 0^0$ to c a: b & bc $ 0 0^0$ bc.
11 12 13 14 15	St. Cu. : Fr. St. St. Wet Fog St. Cu. : St. St.	Nb. St. Ci.: Cu. St. St.	St. Nb. Ci. St.: St. Cu. Ci.: St. Cu.: Fr. St St.	10 10 10 10 10	10 8 10	2 8	10		0 I 4	10 10 - 5 10	 ≡ : ≡	• • 0 	•°	• ° · · · · · · · · · · · · · · · · · ·	 •° ····		
16 17 18 19 20	St. St. A. Cu. : St. Cuf. St. Cu. St. Cu.	Nb. St. Cu.: St. Cuf. Cu. St. Cu. St. Cu. St. Cu.: Fr. St.	St. Cu. : St. St. Cu. : Cu. St. Cu. : Cu. Cu. : St. Cu. St.Cu.:Cu.Nb.:Fr.St	10 10 2 7 10	9 2 7	7			2	10 2 10 8 9	 		•°				$p \bullet 0 \equiv 0$ $a : c to b p \Leftrightarrow n :$ b early, b & bc $a \Leftrightarrow p : b to o n :$ c & o throughout. c & o $p \bullet $ & $p \bullet A$ $a, p \Leftrightarrow n :$
21 22 23 24 25	St. Cu. St. Cu. Ci. : Nb. Cuf, Cu. Nb. Nb.	St. Cu. : Cu. Nb. St. Cu. : Cu. St. Cu. : Cu. Nb. Ci. : Cu. A. St. : A. Cu. : Cu.	Nb. Cuf. St. Cu. Cu.: Cu. Nb. St. Cu.: Cu. Nb. A. Cu.: St. Cu.: Cu.	8 9 6 1	10 5 9	2 3	10	5 1	2 4	8 10 3 10	 p●° 	p X °		P*			c & o, q, p
26 27 28	St. Cu. : Fr. Nb. Ci. Ci. : Ci. Cu.	A. St. : Nb. Ci. : St. Cu. Ci. St. : Cu.	Nb. St. Cu. : Cu. Nb. Ci. St. : St. Cu. : St.	10 1 3	4	8	3 8		0 9 8	8 7 5		●° … ⊕	●° … ⊕	•°	p ● 0	p ● 0	• throughout, q at night. b to cy $a & p : c & op • n :$ • early, bc & $c \equiv a & p : c, o •$, bc $n :$ • $\oplus 9^{-1}3^{h}$
29 30	St. Cu. Nb.	Cu. Nb. St.	Ci. St. : St. Cu. Nb.	I 10	6				7	10	 •°	 •°		p⊕▲ ●°	⊕ •°		early, bc & c, v $a : \operatorname{cp} \bullet \blacktriangle p : o n :$ $\bullet^{0} \equiv^{0} a \otimes p : \operatorname{b too} n : \qquad [\oplus 18h]$
Mean Cloud Am'nt	•			8.1	8.6	7.	68.	2 7	. 8	7 • 4							
Day.	7 ^h	13h	18h	7 ^h	9h	1		\perp		21 h	7h	9h	13h	15h	18h	21h	Remarks.
Ì		Cloud Forms.					Orn						Weath	er.			

103.	Aberdeen.			_												May, 1923.
		Cloud Forms.					Amo orm					Wea	ther.			
Day.	7 ^h	13h	18h	7h	9h	13h	15h	18h	21 h	7h	9h	13h	15h	18h	21 h	Remarks.
1 2 3 4 5	St. Cu.: St. Cuf. St. Cuf. CiCi. St.: St. Cuf. Ci. Cu.	A. Cu. : Fr. Cu. Ci. : St. Cu. A. CuA. St. : St. Cu. Ci. : Ci. Cu. Ci. St. : St. Cu. : Cu.	St. Cu. : Fr. Nb. CiCi. Cu. A. Cu. lent. Ci. : St. Cu. A. St. : St. Cu.	10 4 4 - 2	9 10 5 - 5	4 4 9 1 7	10 1 10 1 6	9 1 7 1 9	10 1 5 1	 ⊕ 	P ● 0 ● 0 		p●0			Mainly c & op \bigoplus ⁰ $a & p : o n :$ bc to $o \bigoplus$ ⁰ to bc $a : b p & n :$ bc to $o a : o p : bc n : \bigoplus 7h$ b, by, b $a, p & n :$ b & bc $a & p : o \equiv$ ⁰ $n :$
6 7 8 9 10	A. Cu. : St. Cu. St. Cu. : St. Cuf. St. Cu. : St. Cuf. Ci.	A. Cu.: St. Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. A. St.: Fr. St.	Ci.: St. Cu.: Cu. St. Cu.: Cu.: Cu.Nb. St. Cu.: Cu. Nb. Nb. Cuf. Nb.	8 - 6 5 1	9 1 6 6 10	7 6 9 9	8 7 9 10 10	2 5 4 9 10	7 4 9 8				 0	 	 •0	c & o $a & p : b \ n :$ b $a : bc & cp \infty p : c & o \ n :$ bc, $p \infty {}^0 A^0 a : c & op \infty p : bc \ n :$ \Box , bc & $cp \infty {}^0 a : op \infty, \star {}^0 p : \bullet^0 n :b & bc a : o \star, \star \triangle, \bullet^0 \equiv {}^0 p : \bullet^0, c \equiv {}^0$
11 12 13 14 15	St. Cu. : Nb. Cuf. Nb. A. Cu. : St. Cu. : Nb. Ci. : Cu. Nb.		Nb. A. St. : St. Cuf. Ci.St.:Cu.Nb.:Nb.Cuf A.St. : St.Cu. : Fr.St. Nb.	10 7 1	10 8 6 10	10 9 10 7	10 8 8 10	10 9 7 9 10	10 9 9	p ★ • ° · · · · · · · · · · · · · · · · · · ·	• 0 ···	* 	•°	•	• · · · · · · · · · · · · · · · · · · ·	$\begin{array}{c} n:\\ \bigstar \equiv^0 \ a: \bullet \equiv^0 \ p \ \& \ n:\\ \circ \bullet^0 \neq a: c \ \& \ oq, p \bullet^0 \ p: o, \bullet^2 \ later \ n:\\ c \ \& \ op \bullet \ \& \bullet^2, p \bullet \bigwedge \ a \ \& \ p: c \ \& \ op \bullet^0 \ n:\\ o \ to \ b \ to \ o \ a: c \ \& \ op \bullet^0 \ p \ \& \ n: \oplus \ 13h\\ \bullet^2 \equiv^0, \bullet^0 \ a: c \ \& \ op \bullet^0 \ p: \bullet \equiv^0 \ n: \end{array}$
16 17	Ci. St. : St. Cuf. Nb.	A.St.: A.Cu.: Cu.Nb. Nb.	Nb. Cuf. St.Cu.: Fr.Nb.Cuf.	9	9	8 10	8	9	8 8	 p●º	•0	 •²		 P●0		$ \bigoplus_{0}^{n} \bigoplus_{0}^{n} (\mathbf{q}, \mathbf{p}) \bigoplus_{0}^{n} (\mathbf{p}) \bigoplus_{0}^{n} (\mathbf{q}, \mathbf{p}) \bigoplus_{0}^{n} (\mathbf{q}$
18 19 20	Ci, Cu. : St.Cu. : Cu. St. Cu. : Cu. St. Cu. : Nb.	St. Cu. : Nb. Cuf. Cu. Nb. Nb.	St. Cu.: Fr. Nb. St. Cu.: Cu. Nb. Cu.	5 9 10	9 9 10	10 7 10	9 6 10	8 9 9	8 9 3	 •°	 •0	•° 	P● ⁰ P● ⁰	• o p • o		bc to $0 \oplus 0$ $a : c \& op \oplus 0$ $p \& n :$ bc & op \oplus throughout. $\bullet 0 \equiv 0$ all day, b later.
21 22 23 24 25	St. Cu. : Cu. St. Cu. : Cu. Ci. : Ci. St. : St. Cu. Ci. St. : St. Cu. Ci. : St. Cuf.	A. Cu.; Cu.; Cu. Nb. St. Cu.; Cu. Cu. A. St.; Cu.; Nb. Nb.	CiCi. Cu. ; Cu. St. Cu. St. Cu. ; Cu. A. St. ; St. Cu. Nb.	3 4 4 5 6	8 10 10 6 10	9 5 10	6 6 6 10	3 5 8 10	5 1 6 5 10	 ⊕ 	 • p•	 •° p•		 		b, c & op
26 27 28 29 30	Nb. St. St. Cuf. St. Cuf. St. Cu.: Nb. Cuf.	Nb. Cuf. St. St. Cuf. St. Cu. : Cu. Nb. Cuf.	Nb. St. Cuf. St. Cuf. St. Cu. : Cu. St. Cu. : Nb. Cuf.	10 9 8 10	10 10 8 10	10 6 10	3	4 2 9	10 10	• 	 	p ● 0 	• • 0	 	•2 ··· ···	$ \begin{array}{ccccc} \bullet, o, p & \& p & \& & a: & p: & \& & \bullet^2 & n: \\ p & \bullet^0 & \text{early, c & o } & a: & \text{bc } p & \& & n: \\ \text{bc & cq} & a: & \text{bq} & p: & c & & o & n: \\ \text{oq, o} & a, p & \& n: \\ p & \bullet^0 & \text{early, } & \bullet^0 & a, p & \& n: \end{array} $
31 Mean	St. Cu.	St. Cuf.	St. Cuf.		10	<u> </u>	-				•0		ļ			● ⁰ , ○ a:c&o p:b n:
Cloud Am'nt				6.4	8.2	8.2	7.9	7.0	7.0							
104	Aberdeen.	1			1		1	1	1	· · · · · · · · · · · · · · · · · · ·		1	1	1	1	June, 1923.
1 2 3 4 5	St. St. Cuf. St. Cu .: St. St. Cu .: St. St. Cu .: St. A. Cu .: Cu.	St. Cuf. Ci. : Ci. Cu. Nb. Cu. A. St. : Nb.	A. Cu. : St. Cuf. Ci. St. : St. Cu. Nb. Ci. Cu. : Cu. Nb.	10 10 10 10	8 4 10 8 10	3 10 10	8 7 10 9	7 10 9	10		 •0 	 •° p•	 •° 	 •° 		c & o a & p : b n : o to b a : c, c & o p & n : ov, ● a : ● p & n : c & o a & p : p ● n : c & o a : ● & ● p & n :
6 7 8 9	Ci. : Cu. St. Cu. A. St. : St. Cuf. A. Cu. : Cu. St. Cu. : Cu.	Cu. Ci. St. : Cu. A. St. : St. Cuf. A. Cu. : Cu. A. Cu. : Cu.	St. Cu. : Cu. A. Cu. : St. Cu. A. Cu. : Cu. Nb. St. Cu. : Cu. Nb.	2 9 10 8 6	7 10 10 6 2	7 9 10 10	3 8 8 10 8	7 4 7 10 8	2 10 8 10 9			 ⊕ 			 • 0	b, b & bc a : bv p : c, b & bc n : $0 \equiv^0 a$: c & bc p : bc to o n : \bigoplus III-I4h $p \bigoplus \text{early, oq, } p \bigoplus^0 a \bigotimes p : \text{cq } n$: bc & c, qy a : o, \bigoplus 0 p : op \bigoplus 0. \bigoplus 0 \equiv 0 n : b & bcq a : cq p : c & o n :
11 12 13 14 15	Ci. Cu. : Fr. Nb. A. St. Cu. Nb. Cuf. A. Cu.	Ci.: Ci. Cu.; Cu. A.St.: St.Cu.: Fr.Nb. St. Cu.: Cu. Cu. A. Cu.: St. Cu.	Cu. Nb. A.Cu. lent : Fr.Cu. St. Cu. : Cu. Nb. Ci. Cu. A. St. : Nb.	7 10 8 7 8	6 10 4 9 7	3	4 10 10 4 10	8 8 9 1	1 9 10 8 10	P● P●°	P ● 0 P ● 0		 			bc & cp \bullet 0 q $a & p : b n :$ b to o , \bullet 0 \equiv 0 $a : c & o p : o n :$ p \bullet 0 early, cq $a : oq$, p \bullet 0 $p & n :$ c & oq, p \bullet $a : bcq$, b $p : c n : \oplus 15^{h}$ bc & c $a : o p : o \bullet$ 0 \equiv 0 $n :$
16 17 18 19 20	Ci. Cu. : St. Cuf. St. Cu. : Cu. St. Cuf. St. Cu. St. Cu. : St. Cuf.	A. Cu. ; St. Cu. ; Cu. Ci. ; Ci. St. ; Cu. Ci. ; Cu. ; St. Cu. Cu. Nb. A. Cu. ; Cu.	St. Cu. : Cu. St. Cu. Ci. St. : St. Cu. St. Cu. : Cu. Nb. St. Cu.	7 4 10 4 10	6 9 7 5	6 5 6 9 4	3 9	5 10 4 9 10	7 9 1 9			 ⊕ p•°	 ∞ 	 		bc & cp
21 22 23 24 25	A, St. ; St. Cu. St. Cuf. Ci. ; A. Cu. ; St. Cu. Nb. St. Cuf.	A. Cu.: A. St.: St. Cu. St. Cu. lent ; Cu. Ci. Cu. : St. Cu. : Cu. Nb. Ci. St.: St. Cu.: Fr.Cu.	St. Cu. : Cu. Cu. A. Cu. : St. Cu. St. Cu. : Fr. Nb. Cu.	10 10 10 10	7 7 10 8	9 10 8 10 8	10 5	10 9 6 9 6	10 9 1 10	 •°	 		•			o, oy, o a, p & n: [⊕ 9h p ● 0 early, c & oq, y a : oq, o p & n: c & oq, y a : b & bc qy p : c to o n: e = 0q a : ● = 0 p : o to b n: e & b & bc, o, cy a & p : b n: ⊕ 13h
26 27 28 29 30 Mean	Ci. : Ci. St. : Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. : Fr. St.	Ci. Cu. lent St. Cu. Ci. A. Cu. : St. Cu. St. Cu. : Fr. St.	A. Cu. St. Cu. Ci.: A. Cu.: Cu. St. Cu.: St. Nb. Cuf.		8 10 2 10	3 10 2 8 9		3 9 4 10	5 10 7 10 8							b & cqy a : byq p : bc n : \oplus Ioh Dull throughout. c to by a : by, by bc p : c n : Mainly dull, \equiv 0 later. c, $o \bullet$ 0 a : \bullet 0, \bullet , c $p \otimes n$:
Cloud Am'nt	1	1		7.8	7.7	7 · 7	7.5	7.6	7.4							
Day.	7 ^h	13h	18h	7h		<u> </u>		1	2I h	7 ^h	9h	13h	15h	18h	21h	Remarks.
		Cloud Forms.					Amo orm	unt s).				Wea	ther.			

July, 1923.

105.	. Aberdeen.															July, 1923.
		Cloud Forms.						noun ms)				Wea	ather.			
Day	7h	13h	18h	7 ^h	9h	13	h 15	h 18	h 211	7h	9h	13h	15h	18h	2 I h	Remarks.
1 2 3 4 5	Nb. St. Cu. A. Cu.: Fr. St. Ci.: St. Cu. St. Cu.	Nb. Cuf. Ci.: A. Cu.: Cu. Cu. Ci.: A. Cu.: Cu. St. Cu.: Fr. Nb.	Nb. St. Cu. St. Cu. A. Cu.: St. Cu. A. Cu.: St. Cu.	7 7 4 10	9 9 6 6 9	5 7 4	6	7 3	10 1 3	•°		•° ··· ··· ··· •°	●°	 		
6 7 8 9	St. Cu. Ci. Cu. St. Cu.: Cu. Nb. Ci.: St. Cu. A. Cu.	Ci. Cu. Ci. St.: A. St.: Fr.Cu A. Cu.: St. Cu. Ci.; St. Cu. St. Cu.: Nb.	CiCi. Cu. : A. Cu. St. Cu. A. St. : Cu. Nb. Ci. St.	4 1 10 6 1	3 1 10 8 3	9 5 4	77	7 9	10 2	 T•	 	 	 			bc \equiv^0 to b ∞ $a:$ bc ∞ $p:$ c \equiv^0 $n:$ b \equiv^0 to $0 \equiv^0$ $a:$ c $\&$ $0 \equiv^0$ $p:$ R \bigoplus $\&$ \bigotimes \cong $n:$ \bigoplus , T , R \bigoplus , O \cong O
11 12 13 14 15	St. St. Cu. lent. Cu. St. Cu. St.	A. Cu.: Fr. St. A. Cu.: St. Cu.: Cu. Cu. St. Cuf. Fr. St.	A. Cu.: St. Cu. Cu. St. Cu. St. Cu. St. Cu.: St. Nb.	10 8 9 10	10 8 7 10	9 1 10	4	7 8 1 9	9 10 10		•°			 		o≡ ⁰ , $\[\] \] \$ $\[\] \] \$ o≡ ⁰ , $\[\] \] \$ o= ⁰ , $\[\] \] \$ o= ⁰ , $\[\] \] \$ o box o= ⁰ $\[\] \$ o cos o= ⁰ $\[\] \] \$ o a: b & bc $\[\] \] \$ o a: b & bc $\[\] \] \$ o a: b & bc $\[\] \] \$ o a: bc to o● ⁰ ≡ ⁰ $\[\] \] \$ o a: bc n:
16 17 18 19 20	St. Cu. Ci. CuA. Cu. A. St.: St. Cu.: Nb. A. St.: St. Cu. Ci. CuA. Cu.: Cu.	Cu. A, Cu.: St. Cu.: Cu. A. Cu.: Cu. Nb. A. St.: Fr. Nb. Ci. CuA. Cu.: Cu.	St. Cu. : Cu. Cu. Nb. St. Cu. : Cu. Nb. St. Cu. : Cu. St. Cu.	10 6 10 10 6	7 5 9 10 7	7 9 10	9	5 4	7 9 5	 •° 		 •°				c&o
21 22 23 24 25	Cu. Nb. Cu. St. Cu.: Cu. St. Cu.	Cu.: St. Cu. A.Cu.: St. Cu. lent: Cu St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu.	A. St.: St. Cu. A. Cu.: St. Cu. St. Cu.: Cu. Nb. Nb. St. Cu.: Cu. Nb.	2 10 2 8 10	6 10 7 9 7	9 10	7	7 4 7 10	9 8	 •° 	 p●°			 ••		bto oqy $a:o p \otimes n$: • oto o, y $a:o p:op \bullet o n$: •, c & o, p • o & p • a, p & n: c & o, p • o a:o, • o p: •, o n: c & o, cp • o a:c p:b n:
26 27 28 29 30	Cu.: St. Cuf. Ci.: Cu. Nb. St. Cu. Nb. Fog.	Nb. Ci. Cu.: St. Cu.: Cu. A. St.: Nb. St. Cuf. A. Cu.: Cu.: St. A. CuSt. Cu.: Fr. St	Ci. Cu. : Cu. St. Cu. : Cu. Nb. Nb. Nb. A. Cu. : St. Cu. : Nb.	8 4 10 10 10	10	3 10 10	10) IC 0 IC 0 IC	10 10 10 8	 • •°	 •° 	• • 0 		 •• •• ••	 •0 =:	bc $p \bullet^0 a : o \bullet$, o to bcq $p : c \& o$, bc &c $a : b$ to $o p : o n : [p \bullet^0 : n : o \bullet \equiv^0, \& \bullet^0$ throughout. o $a : \bullet^0 \equiv^0 p : \bullet \equiv^0$ to $o \equiv n : o \& \bullet^0 \equiv^0$ to $b : a : b$ to $o \bullet \equiv^0 p : o \otimes^0 n : $
Mean Cloud		A. Cu5t, Cu F1. 5t	St. Cu.	-	-	- -	28.	- -	1 7.	-				-	-	$p \bullet^0 \text{ early}, \equiv \stackrel{\cdot}{,} o \equiv^0 a : c \& o \equiv^0, \bullet^0$ $[p : o n :$
106				<u> </u>	<u> </u>					<u> </u>	1	<u> </u>	<u>!</u>	<u> </u>	<u> </u>	August, 1923.
ı	St. Cu. : St.	St. Cu. : Cu.	St. Cu. : Cu. Nb.	10	8	9	10	8	I	T	T	T	•	T	T	c&o a:p $ \bullet p$:b n: [p $ \bullet ^2 $, $ \bullet \equiv ^0 n$:
2 3 4 5	A. Cu.: St. Cu. St. Cu.: Fr. Nb. Ci.: St. Cu. Ci.: Ci.Cu.: Fr. St.	A. St. : Nb. Cu. A. Cu. : Cu. Ci. StA, St. : A. Cu.	A. St.: Nb. Ci. CuA. Cu.: Fr. Cu Ci.:Ci.Cu.:A.Cu.:St.Cu Ci. Cu.: A. Cu.:St.Cu	. 4	9 9 3 4		10 8 1	10 9 4		 •°				•	 	bearly, c to $o \equiv^0 a : o p \bigoplus^0 \equiv^0 p :$ • to oq $a : cq p : o to b n :$ Mainly fair. bc & $c \equiv^0 a & p : o \bigoplus^0 \equiv^0 n :$
6 7 8 9	Nb. A. Cu. : St. St. Cu. St. Cu.	A. Cu. : St. Cu. A. Cu. : Cu. A. Cu. : A. St. : Cu. CiCi. Cu. : Cu. St. Cu. : Cu,	A. Cu.: St. Cu.:Fr.St. St. Cu.: Cu. Nb. St. Cu.: St. Ci.: Ci. Cu.: Cu. Ci.:Ci. St.: Cu.: St.Cu	10 9 10	9 10 10 6 5	7 7 10 3 8	9 10 8 6	7 10 6	9 10 -	 •° 	•				 p⊕⁰ 	$b \equiv^{0} to o \equiv^{0} a : c & o p : o to b n:$ $\bullet \equiv^{0} a : c & o p \bullet T, c p : p \bullet^{2}, p \bullet^{0} n:$ Dull all day; $\bullet^{0} n :$ $\bullet \text{ early, o to by } a : bc & c p : b n:$ $bc & c a, p & n:$
11 12 13 14 15	Ci.: St. Cu. lent. A. Cu.: St. Cu. St. Cu. Ci.: Ci. St.: A. Cu. A. Cu.	Cu. Ci. : Ci, Cu. : A. Cu. Cu. St. Cu. : Cu. St. Cu. : Cu.	Cu. A. Cu. : A. St. : Nb. Ci. : Cu. Ci. Cu. : Cu. Nb. Ci. Cu. : Cu. Nb.	3 8 10 6 1	7 8 10 5 1	6 6 3 9 9	7 10 2 5 7	10 1 8	IO I		•			•°		b & bc a :ctoo p :otob n : c a :ctoo
16 17 18 19 20	St. Cu. : Cu. Nb. St. Cu. : St. St. Cu. : Nb. St.	St. Cu.: Cu. St. Cu.: St. St. Cu.: St. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: St.	Nb. St. Cu.: Nb. St. Cu.: Cu. A. Cu.: St. Cu.: Cu. A. St.: St.	8 10 9 9		8 10 9 9	8 10 10 7 10	9 4 9		 •° 	•°		•	•	 •° ∞	c $a: cp \bullet^0$, $o \bullet =^0 p: \bullet$, $o =^0 n:$ $\bullet^0 = a \circ p: \bullet^0 n:$ $p \bullet^0$ early, $o : a: o t o b o p: c, o : n:\bullet^0 early, o : a \circ p \circ n:\bullet^0 early, o : a \circ p: o =^0, \bullet^0 : n:$
21 22 23 24 25	Nb. CiCi. Cu. : A. Cu. Ci. : Cu. St. Ci. St. : St. Cu.	A. St. : A.Cu.: Fr.St. Ci. : Cu. Ci. : A. Cu. : Cu. Nb. Ci. : A. Cu. : St. Cu.	St. Cu. : Cu. Ci. : Cu. A. St. : St. Cu. A. Cu. : Fr. St. Nb.	10 4 1 10 9	9 4 2 10 9	9 5 7 10 4	4 5 10 10	3 10 7	- 1 10 8 10	•°	 •0	 	 •°		 •	
26 27 28 29 30		A. St. : St. Cu. : Cu. Nb. A. Cu. : St. Cu. : Cu. Cu. Nb. A. Cu. : Cu. Nb.	St. Cu.: Cu. Ci.: St. Cu.: Cu. Nb. St. Cu.: Cu. Nb. A. St.: St. A. St.: Fr. Nb.	7 4	4 4 8 3 10	9 6 9 9	7 6 9 9	6	7 7 4 10	: id :•		 	 			
31 Mean Cloud	St. Cu.	Cu.	Ci.: St. Cu.	6 7·1	<u>2</u> 6·9	<u>3</u>	7.4	-	1 6·3						٩	$p leftharpoonup early, bc, b \equiv^0 a \otimes p : b \triangle n :$
Am'nt	7h	13h	18h			<u> </u> 	- 	<u> </u>	21h		9h	13h	15h	18h	21h	
Day.		Cloud Forms.			lou	d A	mo	unt				Wea				Remarks.
- 1		Cloud Porms.			(A	ll F	orn	ıs).				wea	mer.			

107.	Aberdeen.		DI	11(1		_						¥				September, 1923.
		Cloud Forms.				ud A		unt s).				Wea	ther.			Demonte
Day.	7 h	13h	18h	7h	9h	13h	15h	18h	21 h	7h	9h	13h	15h	18h	21 h	Remarks.
1 2 3	St. Cu. St. Cu. : St. Ci.	Cu. Nb. : Cu. Cu. Ci : Ci. St. : Ci. Cu.	St. Cu. : Cu. Nb. St. Cu. A. St.	1 8 1	1 7 1	6 4 4	10 4 9	8 1 10	6 _ 10	b : b	p		P ● 2			b \triangle , b, cp \bullet $a : c \& o p \bullet2, \bullet \equiv0 p : bc \bullet early, cp \bullet0 a : bc p : b n : [\equiv0 n : b b \equiv0 a : bc to o p : o \bullet \equiv0 n : \oplus IIh & [15h$
4 5	Nb. A. St.	Cu. St. Cu. : Cu.	Ci. : Ci. St. : St. Cu. Cu.		8 10	4 9	7	8 9	10 3	•					p ● 0	
6 7 8 9	A. St. St. Cu. Ci. St. : St. Cu. Ci. CuA. Cu. : Cu. Ci. Cu.	A. Cu. : Cu. A. Cu. : Cu. St. Cu. : Fr. Nb Cu. Nb. Ci. : Ci. St. : Cu.	Nb. St. Cu. : Cu. A. St. : St. Cu. A. Cu. : Cu. A. Cu. : St. Cu. : Cu.	1 1 8 6 2	1 4 5 3	1 3 10 10	2 3 10 4 9	9 2 9 3 8	8 1 2 1 10	þ :⊕: þ	 	 p • 0 p • 0		• ° · · · · · · · · · · · · · · · · · ·		b \triangle , b a : bto o, \bigcirc 0 p : \bigcirc 0 , c n : b & bc a, p & n : c & bc, o a : \bigcirc 0 \equiv 0 o \equiv 0 p : b n : \bigcirc 7h— bcq a : p \bigcirc 0 , b & bc p : b n : bto bcq a : c & o p & n : \bigcirc 14h.
11 12 13 14 15	Ci. St. : St. Cu. : Cu. St. Cu. St. Cu. Ci. St. : St. Cu. A. StA. Cu.	A. St. : St. Cu. Fr. Cu. Nb. Ci. : Cu. Cu. : Fr. Cu.	Ci.CuA. St. : St.Cu. Cu. Nb. Ci. St. St. Cu.	10 1 10 6 8	6 1 9 4 9	10 1 10 3 2	10 6 10 5 3	9 6 10 3 1	7 - 10 2 -	•••		•	 •° •	•	•	o, bc, $p $
16 17 18 19 20	St. Cu. A. Cu : A. St. : St.Cuf St. Ci. Cu. : St. Cu. Ci.	St. Cu : Cu : St. A. St. : Fr. Nb. A. St. : Fr. Cu. A. St. : Nb. Ci. : Cu.	Ci.: St. Cu.: Cu. Nb. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu.	1 10 10	10	8 10 10 10	7 10 10 10 2	5 10 8 9 1	- 10 2 9	 		 •••	 • • 0	• • • • • • • • • • • • • • • • • • • •	•	cp
21 22	Nb. St. Cu. : Cu. Nb.	St. Cu. : Fr. Cu. St. Cu. : Cu.	St. Cu.: Cu. Nb. Cu. Nb.	10	9 7	9 7	8	7 8	I 2	•	•°		p.●°			
23 24 25	St. Cu. St. Cu. Nb.	St. Cu. : Cu. St. Cu. ; Cu. Nb. A. Cu. : Cu.	St. Cu. : Cu. Nb. St. Cu. : Fr. St. Cuf. Ci. : St. Cu. : St. Cuf.		8 1 10	7 8 2	7 4 5	6 9 4	1 8 10	<u>•</u>		•••			 •0	$ c & o \ a : cp $
26 27 28 29 30	St. Cu. A. St. : St. Cu. A. St. : Fr. Nb. Ci. Cu : A. Cu. Ci.	St. Cu. Nb. Ci. Cu. : Cu. A. CuSt. Cu. : Cu. A. Cu.	St. Cu. CiCu. : St. Cu. : St. A. CuSt. Cu. lent. Nb. St. Cu.	6 10 10 2 1	9 10 4 1	8 10 2 9 7	7 10 9 10	10 7 9 10 9	8 10 10	:: ::: d		•	 •0	= •°		bc to $0 \equiv 0$ $a : c \& 0 \equiv 0$ to $0 \equiv p : 0 \equiv 1$ to $0 \equiv 0$ to 0
Mean Cloud Am'nt				6.1	5.4	6.5	7.2	6.9	5.6							
108	. Aberdeen.							,			1		1	T		October, 1923.
1 2 3 4 5	A, Cu.; St. Cu. St. Cu.; Fr. Nb. A, St. St. Cu.; Cu. Nb. A, St.; Nb.	Ci. St. : Cu. St. Cu. : Cu. Nb. Ci. : Cu. Cu. Nb. St. Cu. : Fr. Nb.	Ci. : Cu. St. Cu. Ci. : St. Cu. St. Cu. Ci. : St. Cu. : Fr. St.	9 5 9 7	7 2 9 9	1 3 6 7 10	3 4 7 5 7	1 4 1 8 8		 	 p ●°	•••				c & o, bc $a : b \ p : b to o \equiv^{0} n :$ p \bullet^{0} early, b & bc q $a, p \& n :$ c, o, bc $a : c, b \& bc \ p : b \& bc p \bullet^{0} n :$ c & o p $\bullet^{0} a : bc \ p : b n :$ b, o $\bullet^{0} \equiv^{0} a : c \equiv^{0} p : b n :$
6 7 8 9	A. Cu. ; St. Cuf. St. Cu. ; Fr. Nb. St. Cu. St. Cu.	Ci, : St. Cu. : Cu. St. Cu. : Fr. Nb. Ci. CuA. Cu. : Cu. Cu. CiCi. Cu : Cu.	Ci. St. : St. Cu. : Cu. St. Cu. A. St. : Fr. St. St. Cu.	10 9 3 - 4	9 4 - 3	4 7 6 1 2	3 8 9 1 4	4 9 10 - 1	7 8 10 -		•°	 •0 			•	bc, o $lack o$ \equiv 0, c a : b & bc p : c n : c & o $lack o$ 0 a : cp $lack o$ 0 & p $\not o$ p $\not o$ n : o to b & bc y a : bc y to o \equiv 0 p : $lack o$ o to bq a : bq & bc p o p : bq n : b & bc a : bc p o 0 p : b n :
11 12 13 14	Cu. Nb. Ci. : St. Cu. A. St. : St. Cu. St. Cu. St. Cu.	St. Cu. : Cu. Nb. Cu. Cu. Nb. Cu. Nb. A. St. : St. Cu.	St. Cu. Nb. Cuf. Cu. Nb. A. St. : St. Cu. A. St. : St. Cu.	1 4 10 1 8	I 2 10 I 8	5 5 8 8	7 5 5	1 10 6 8 9	- 10 - 10 10			 p ●º		 • ° ° ° ° · · · · · · · · · · · · · · ·	• · · · · · · · · · · · · · · · · · · ·	b, bq b $a, p & n :$ b & bc $\equiv^0 a : bc, c \equiv^0, \bullet^0 p : \bullet \equiv^0 n :$ o \bullet to bc $a : bc & cp \bullet p : b n :b a : cp \bullet^0 p : c & o \bullet^0 n :c^0 \equiv a : c, o \equiv p : o \equiv^0 \bullet^0 n :$
16 17 18 19	St. Cu. : Nb. Cuf. A. St. : St. Cu. Ci. St. : St. Cu. Nb. Ci. Cu.	Cu. : Cu. Nb. St. Cu. lent. St. Ci. : Cu. Ci. St. : A. St.: St.Cuſ	A. Cu. St. Cu. St. Cu. St. Cu.	10 7 7 10 4	8 7 8 4	2 2 10 2 9	1 8 10 1 9	1 10 6 - 8	8 10 10 1 3							$\begin{array}{l} \bullet^0 \text{ early, o to b } a: b \& \text{ bc } p: \text{ b to c} \equiv^0 n: \\ \bullet^0 \equiv^0 \text{ early, c t} \bullet b \ a: b \text{ to o} \equiv^0 p: c \& o \\ c \equiv^0 a: \text{ o to bc } \equiv^0 p: c, o \equiv^0 n: \\ c \& \text{ oq } \bullet^0 \ a: \text{ bq } p: b \ n: \\ \text{ bc, oq } a: c \& \text{ oq } p: b \ n: \end{array}$
2 I 2 2	Nb. St. Cu. : St. Cuf. St. Cu.	A. StA. Cu. : Cu. Cu. St. Cu. : Fr. St.	St. Cu. A. St. : Nb. Nb.	10 7 8	8 4 8	6 2 9	3 2	4 10 10	3 -							
23 24 25	Nb. St. Cu.	A. Cu. : Cu. St. Cu. : Cu.	Ci. : A. Cu. St. Cu.	9 7	10 5	6	3 6	3	1 8	●° 						
26 27 28	A. St. : St. Cuf. Nb. St. Cu. : Cu. Nb.	St. Cu. : Cu. Nb. Nb. St. Cu. : Fr. Cu.	St. Cu. St. Cu. St. Cu.	10	01 01	7 10 2	4 9 5	1 7 5	- 5 8	•	•	p ● 0				$o \equiv^{0}, \bullet, cp \bullet^{0} a : bc & c p : b n : \square 24h.$ $co \bullet \equiv^{0}q a : \bullet \equiv^{0} to c p : bc & c \equiv^{0}n :$ $\bullet^{2} early, bc & op \bullet a : b & bc p : c & o,$ $co \bullet \equiv^{0}q a : \bullet c \circ p : bc \circ c \circ p : c \circ c \circ c \circ c \circ c \circ c \circ c \circ c \circ c \circ c$
29 30	St. Cu Cu.	Ci. St. : A. Cu. : Cu. Ci. : St. Cu. : Cu.		-	2		l	10	-			•••	•0	•		$b \equiv^{0} \text{too } a : \bullet^{0} \equiv^{0}, \bullet p : \bullet \text{too } \equiv^{0} n :$ otob $a : b \neq \otimes n :$
31 Mean		Cu.	St. Cu.		I	I	I	4_	_	•••						b, by $a \otimes p : bc, b \equiv^0 n :$
Cloud Am'nt				6.6	6.1	2.1	5.2	5.2	4.8							
Day.	7h	13h	18h	[!	I			18ь	21 h	7 ^h	9h	13h	15h	18h	21 h	Remarks.
		Cloud Forms.		'		ad A all F		unt is).				Wea	ther.			

109.	Aberdeen.															November, 1923.	
				Clou (A	ıd A						Wea	ther.					
Day.	7h	13h	18h	7 ^h	9h	13h	15h	18h	21 h	7 ^h	9h	13h	15h	18h	2 I h	Remarks.	
1 2 3 4 5	St. Cu. St. Cu. St. Cu. St. Cu. : Cu. Nb. Ci. : Cu. Nb.		A. St. St. Cu. Cu. Nb. Ci. St. A. St. : St. Cu.	4 1 5 5 4	1 - 6 7	- 1 3 9	- I 2 2 9	1 8 1 1 9	I IO - - -			 ••			•	bc, b $a:b \equiv^{0} p \otimes n:$ $\bullet^{0} \text{ early, b } a \otimes p:c \equiv^{0} \text{ to } 0 \oplus \equiv^{0} n:$ oq to b & bcq $a:b$ & bc p $\bullet^{0} p:b$ $n:$ b & bc $a:bq$ $p:b$ $n:$ cp $\cancel{*}^{0}$, \bullet^{0} $a:op\bullet^{0}$ $p:o$ to b $n:$	
6 7	St. Cu. : Cu. Nb. Ci. : St. Cu.	Cu. Nb. Ci.	St. Cu. A. St.	5 8	1	I I	8	7 6	10							cp $lackbox{0}$ to b a :b p :cq to o $\not\approx$ 0, $\not\ll$ n : $\not\approx$, $\not\ll$ early, cq to b a : b to o \equiv 0 p : [bc \equiv 0 n :	
8 9 10	St. Cu. : Nb. St. Cu. : Cu. Nb.	False Ci.: Cu. Nb. St. Cu.: Cu. Nb. A. St.	St. Cu. Cu. A. St.	10	10 10 2	1 6 10	2 7 8	1 1 3	- 8	●° **° ···	 ப						
11 12 13 14 15	St. Cu. A. St.: St. Cu. Nb. — Ci. StA. St.	Nb.: Fog Ci.Cu.:St.Cu.:St.Cuf. St. Cu.: Nb. St. Cu. Nb.	St. Cu. A. St. : Fr. St. Nb. Nb.	10	9 10 1	9	10 8 10 10	10 8 10 -	10 10 -	 • ° · · · · · · · · · · · · · · · · · ·	 • ≡	•= •° 	 • *	 •°	•	c, $o \equiv^0$ to $o \equiv a : o \equiv to o \equiv^0 p : o n : o, o to c a : c p : c \& o \equiv^0 n : o to b to o a : p \bigstar \equiv^0 to b p : b \equiv^0 n : b c \equiv^0 to o o \equiv c p \bigstar o \equiv^0 to b o \equiv c p \bigstar o \equiv^0 to o \equiv c p \bigstar o \equiv^0 to o \equiv c p \bigstar o \equiv^0 to o \equiv c p \bigstar o \equiv^0 $	
16 17 18 19 20	St. Cu. Nb. Nb. St. Cu. : Cu. Nb. Cu.	Ci.: St. Cu. Ci. St. A. St. Cu. Nb. Ci.:St.Cu.:Cu.Nb.:Cu	A. St. : St. Cu. St. Cu. Nb. St. Cu. : Nb. Cu. : Cu. Nb.		3 10 10 5 7	1 9 10 6	9 2 10 10	8 1 10 9 1	10 - 10 8 -	··· 本 ···	··· *	•	 •° •		•	$\begin{array}{l} $	
21 22 23 24 25	A. St.: Cu. Nb. St. Cu. Ci. St. A. St.: Cu. Nb. St. Cu.	Ci. St.: St. Cu.: Nb. St. Cu.: Cu. Nb. St. Cu.: Cu. Nb. Ci.: Cu. Nb. St. Cu.	St. Cu.: St. Cuf. St. Cu. Cu.: Cu. Nb St. Cu.	8 10 6 9 8	9 7 2 9	9 7 6 3 8	9 6 10 1 8	10 4 7 - 8	9 5 2 - 6	:::] :::		•°	p*		::: ::: ::: :::	o	
26 27 28	A. St. St. Cu. Ci. St. : Fr. Nb.	Ci. St. Cu. : Fr. St. Nb. Cuf.	St. Cu. St. Cu. St.	3 9 8	3 6 10	2 10 10	5 10 10	8 10 9	8 5 10]]B	≝ ⊔ ≡ 	 = •°	 ≡		=	bc $\equiv^0 \sqcup$, \equiv , b $\equiv^0 a$: bc, c $\equiv^0 p$: c $\equiv^0 n$: c $\equiv^0 \sqcup$, bc \equiv to o \equiv a : o $\equiv p$: bc $\equiv n$: \bigstar early, c \equiv^0 , o \equiv , p $\triangleq^0 a$: o $\triangleq^0 p$:	
29 30	Nb. St. Cu.	Ci.: St. Cu.	St. Cu. Ci. St.	10	8	I	3	I 2	3	P▲ ⁰	 ப			1	<u></u>	[c & op	
Mean Cloud Am'nt				6.4	l	1	1	1	5 · 2								
110	. Aberdeen.															December, 1923.	
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6 7 8 9	— Nb. A. St. : St. Cu. Cu. St. Cu.	Ci. Nb. Nb. St. Cu. St. Cu.	Nb. A. St. A. St.	- 10 3 1	I 10 9 I	10 10 1 9	1 10 10 3 5	- 10 9 10 -	9 10 - 10 -	□ °	□ °	 •° 	 • • • · · · · · · · · · · · · · · · · ·	•	•	$\begin{array}{ll} \mathbf{b} \sqcup_{\bullet} \equiv_{\bullet}^{0} \ a \& p : \mathbf{b} \equiv_{\bullet}^{0} \sqcup_{\bullet}^{\bullet}, \mathbf{o} \mathbf{later} n : \\ \bullet^{0} \equiv_{\bullet}^{0} \mathbf{q} a \& p : \bullet =_{\bullet}^{0} \mathbf{q} n : \\ \mathbf{b} \& \mathbf{op} \bullet a : \bullet^{0} \equiv_{\bullet}^{0} \mathbf{q}, \bigstar p : \mathbf{b} n : \\ \mathbf{b} a \& p : \mathbf{b} \mathbf{to} \mathbf{o} \bullet \equiv_{\bullet}^{0} n : \\ \bullet \mathbf{early}, \mathbf{o} \equiv_{\bullet}^{0} a : \mathbf{bc}, \mathbf{b} \equiv_{\bullet}^{0} p \& n : \end{array}$	
11 12 13 14 15	St. Cu. St. Cu. : St. Cuf. Nb. St. Cu. Cu. Nb.	A. St. : St. Cuf. St. Cuf. Ci. A. St. : Nb. Ci. St. : St. Cu.	St. St. — A. Cu. A. Cu.	10 10 10 10	1 -	10 10 1 10 2	10 8 1 10 3	10 - 1 5	10 - - -			 •° 	•	 		$ o \equiv^{0} a, p \otimes n : o \equiv^{0} a : c & o \equiv^{0} p : o \equiv^{0} n : \bullet early, b \equiv^{0} a, p \otimes n : c & oq, \bullet^{0} \equiv^{0} a : \bullet to b p : b n : bq, p \bullet^{0} a : b & bc p : o, \bullet later n : $	
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21 22 23 24 25	St. Cu.: Nb. Nb. Cu. Nb. Cu. Nb. Ci. St.	St. Cu. Cu. Nb. Cu. Nb. Cu. St. A. St.	St. Cu. St. Cu. — — — — Cu. A. St. : St.	8 10 8 1	9 8 6 4 6	10 1 2 1 10	10 1 3 10	10 2 - 1 10	10 8 6 - 10	P * ⁰ *° U	 b ● 0				* *°	cp\(\bar{N}\), o $a: o \ p: \ \ \ \ n: \ \ \ \ \ \ \ \ \ \ \ \ \ \$	
26 27	St. Cu. : Cu. Nb. St. Cu. : St.	A. St. St. Cu. : St. Cuf.	A. St. : St. Cu. Nb.	8	-	10		10						=	*	\bigstar early, be & $o \equiv^0 a : o \equiv^0 \text{ to } \equiv p :$ $[\equiv \text{to } \bigstar \equiv^0 n : \boxed{\Xi \text{ 20 mm.}}$ $p \bigstar \text{ early, } o \equiv a : o \equiv^0, \bullet p : \bullet, o \equiv^0 n :$	
28 29	Nb. A. Cu.	St. Cu. A. CuSt. Cu. Nb.	St. Cu. St. Cu. Nb.	10	10	1	3	3	_ IO	•		 ≅⊔			□	to b a: b p: b i, p \bigstar ⁰ n: b i ≡ a: o ≡ p: o ≡ o, \bigstar o to \bigstar n: • & \bigstar o, q a, p & n:	
30	Nb. St.	Nb. : Fog	Nb.		10	10		10	10	•	●° =	● 0 =	=	• • • • • • • • • • • • • • • • • • • •		$\bullet^{0} \text{ to } \equiv a \& p : \bullet^{0} \equiv^{0} n :$	
Mean Cloud Am'nt				6.6	6.5	6.6	6.8	6.5	6.9								
Day.	7h	13h	18h						21 h	7h	9h	13h	15h	18h	21h	Remarks.	
		Cloud Forms.						Cloud Amount (All Forms.)				Wea	ther.				

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M.O. 279 (Eskdalemuir.)

Air Ministry METEOROLOGICAL OFFICE

OBSERVATORIES' YEAR BOOK 1923

Comprising the results obtained from autographic records and eye observations at the observatories at Lerwick, Aberdeen, Eskdalemuir, Cahirciveen (Valencia Observatory), Richmond (Kew Observatory), and Benson.

ESKDALEMUIR

Published by the authority of the METEOROLOGICAL COMMITTEE



LONDON:
PRINTED AND PUBLISHED BY HIS MAJESTY'S STATIONERY OFFICE

ESKDALEMUIR OBSERVATORY.

Latitude	• •			55° 19′N
O		• •		3° 12′ W
G.M.T. of Local Mean No	oon	• •		12h 13m.
Heights in n	netres a	bove Se	a-Level	
Barometer				237:3
Rain-gauge				242.0
Dines Tube Anemograph	n		••	250
Heights in n	netres a	bove gr	ound.	
Thermometer Bulbs				0.9
Sunshine Recorder				1.5
Dines Tube Anemograph		• •		15

INTRODUCTION.

SITE.

Eskdalemuir Observatory, some $3\frac{1}{2}$ miles $(5\frac{1}{2}$ kilometres) north-north-west of Eskdalemuir Parish Church in the county of Dumfries-shire, is situated on a rising shoulder of moorland which is bounded on the east by the road which leads north to Ettrick and Selkirk, on the west by the small Davington Burn, and at the southern

extremity by the small hamlet of Davington.

The hillside in the immediate vicinity of the Observatory slopes generally from the north-west to south-east. The mean height above sea level of the Observatory site is about 800 feet (244 metres). Cassock Hill, slightly more than a mile distant to the north-west is 1,205 feet (367 metres), while the bench mark at Davington School ½ mile (0.4 km.) to south-east is 699 feet (213 metres) above M.S.L. To the east the ground slopes fairly rapidly to the valley bottom, the level of the Ettrick road at a point about ½ mile (0.4 km.) east of the Underground Magnet House being 682 feet (208 metres). The River White Esk is rather less than $\frac{1}{2}$ mile (0.8 km.) to the east. Immediately beyond the river, and almost due east of the Observatory, Dumfedling Hill rises to a height of nearly 1,200 feet (366 metres) above M.S.L. Some 4 or 5 miles (8 km.) to the north is a high ridge, following approximately the boundary between Dumfries-shire and Selkirkshire, the highest point of which is Ettrick Pen (north-north-west) 2,200 feet (670 metres) above M.S.L. Rather more than half a mile (0.8 km.) to the west, and beyond Davington Burn, the ground rises to 1,040 feet (317 m.), and reaches nearly 1,200 feet (366 m.) half a mile (0.8 km.) further on. To the south and south-south-east the Observatory commands a view of the White Esk valley as far as Hartmanor, 4 miles (6½ km.) distant, and beyond that the upper slope of Cauldkine Hill, about 10 miles (16 km.) distant, is visible. surrounding country is bare and wild and there are but few trees to relieve the monotony of the grass covered hills and moorland.

Within the Observatory grounds the soil is peaty and in many places is more or less boggy at all seasons. Some two feet, or less, below the surface a clay-like substance containing soft rock is encountered. The local geological formation is described as "rock of the Tarannon Llandovery series traversed by igneous dykes."

The selection, in the early years of the century, of this isolated site for the Observatory was dictated by the desire to reduce to a minimum the possibility of artificial magnetic disturbance due to electric traction and power circuits, and in this connection it may be noted that there is no town, industrial centre, or point of railway within a radius of q miles ($14\frac{1}{2}$ km.) from the Observatory.

The general features of the immediate surroundings and the lay-out of the buildings may be seen from the accompanying photographs, plan and map.

Although the Observatory as such has been in operation since 1909, no particulars of the general lay-out have been published hitherto. The following brief descriptive notes serve as an index to the accompanying site plan (Fig. 11).

There is a narrow belt of trees—chiefly conifers, with a few birch and rowans—around the greater part of the Observatory enclosure. These trees were planted shortly after the building of the Observatory and subsequently. They are largest to the south, but few of them exceed 20 feet (6 metres) in height.

A is a water reservoir, from which water is distributed to the various buildings. The reservoir is fed from a spring on Cassock Hill by means of a pipe line.

B, B are two similar double-walled wooden huts in which absolute observations of the magnetic elements are made. The space between the inner and outer wooden shells is packed with non-conducting material. Lighting is provided by windows in the north sides and by skylights.

C is the underground magnetograph house, constructed throughout of nonmagnetic material. Within the outer shell of stone and concrete, and separated therefrom and from each other by corridors and vaultings, are two similar rooms of which the approximate internal dimensions are:—Length, 25 feet (7.6 m.); width, 20 feet (6·1 m.); height, 10 feet (3·0 m.). The ceilings of the rooms are just below the undisturbed level of the surrounding ground. The roof portion of the outer containing shell is covered with a thick layer of earth, thus forming the mound shown in Fig. 10. The super-structure which is visible in the photograph is part of the ventilation system. The east room contains the standard magnetographs and the photographic barometer. Other magnetographs have been set up from time to Acetylene gas is used as illuminant. time in the west room.

D is the Beckley self-recording rain-gauge, and E the standard 8 inch rain-gauge; each is surrounded by a low wall or dyke of turf. F is an auxiliary 8 inch rain-gauge but is not artificially screened. G is a snow-gauge of the Hellmann pattern, made by Fuess. It was not installed in the position shown until 1925.

H is the Campbell-Stokes sunshine recorder.

J is a concrete pillar, 4 feet high, on which a pilot-balloon theodolite may be mounted. The pillar is surrounded by a wooden seat of convenient dimensions.

K is the pit from which observations of the electric potential at I metre above the surface of the ground are made. The dimensions of the brick-lined pit are 4 feet $(\mathbf{I} \cdot \mathbf{2} \, \mathbf{m})$ by 3 feet $(\mathbf{o} \cdot \mathbf{9} \, \mathbf{m})$ by 3 feet. The lid which consists of a fixed and a hinged portion is covered with zinc, is provided with a small glass window, and is flush with the level of the approximately circular lawn indicated on the plan by the dotted circle.

L is a stone pillar formerly used as a support for an Ebert ion-aspiration apparatus but latterly to support a Besson Comb nephoscope.

M is a large louvred hut which contains the standard dry and wet bulb thermometers, the photographic and pen thermographs, and maximum and minimum thermometers. The hut, of which the general features may be seen on reference to Fig. 10, is painted white inside and out. Until recently, when electric light was introduced, acetylene gas was the illuminant for the photographic thermograph

N marks the position in which the grass minimum thermometer is exposed between 18h and 9h G.M.T.

O is a screen in which is exposed a hair hygrograph.

P is the main building, two-storied, and containing offices, workshop, laboratory, seismograph and photographic rooms. Q indicates the position of the mast of the Dines tube anemograph and R the position of the jet of the Kelvin water-dropper electrograph.

S, T are residences.

U is the acetylene gas generating house.

V is a block containing the garage, the electric lighting generating set and the accumulator batteries. The electric lighting equipment, which was installed in 1924, provides for continuous illumination for photographic recording instruments in M and P and for occasional general lighting in P, U and V. The voltage on the lighting circuits is restricted to 8 volts. Connection between the battery room in V and buildings M and P is by underground cable which is insulated, lead covered, and armoured. All precautions have been taken to guard against leakage of current to earth.

METEOROLOGY.

The elements dealt with in the following tables are:—Atmospheric pressure, air temperature, humidity, rainfall, sunshine, solar radiation, wind speed and direction and minimum temperature on the grass. There is also a diary of cloud and weather.

Notes on Instruments.

Brief descriptions of the recording instruments and of the methods of tabulating the records with notes on the information contained in the Tables are given in the General Introduction to the Tables. The following particulars, which refer specially to Eskdalemuir, are to be regarded as amplifying the information contained therein. References to full accounts of other instruments used at Eskdalemuir appear below.

Pressure.—The standard mercury barometer, Kew pattern (M.O. 1320), is situated in a north window embrasure on the ground floor of the main building.

Towards the end of 1922 the cistern of the barometer of the photographic barograph was broken, and the instrument was not available again until early in 1924. Throughout 1923, therefore, the records obtained from a Dines float barograph were utilised.

The particular float barograph (M.O. 1004) used is one of the instruments designed by Mr. W. H. Dines, F.R.S., in 1912. So far as is known a description of this type of barograph has not been published hitherto; but the following brief account, in conjunction with the accompanying Fig. 14, may serve to indicate sufficiently well, for the present purpose, the general features of the instrument.

The float A, in the shape of a small inverted bell-jar, rests on the mercury in the lower and open limb of a syphon barometer, a number of small steel balls forming a bearing between the glass float and the walls of the cistern. From a small cross piece at C fixed near the upper end of the vertical steel rod B, which is fixed to the float, two fine platinum wires pass partly around and are attached to the central portion D of an aluminium pulley wheel. The axle of the pulley wheel is supported at two points on two bevelled rollers and the tapered ends of the axle pass through two narrow vertical slots in the vertical portion of a brass carriage. A bifilar suspension of fine platinum wire attached to the outer rim of the pulley wheel carries a long glass rod E, to which is attached the recording pen F. The movements of the float are thus transmitted to the pen, which records on a suitably ruled chart wrapped round a clockwork drum H. The diameter of the outer rim of the pulley is four times that of the inner portion, so that fourfold magnification of the float displacements is secured. Base lines are obtained on the chart by means of two fixed pens G. The upper and lower cylindrical cisterns are large in diameter compared with the remainder of the tube, so that capillary effects are reduced to a minimum. Compensation for temperature changes is secured by adjusting the quantity of air within the float A. The requisite quantity of air under standard conditions may be determined from knowledge of the dimensions of the instrument, due allowance being made for the effect of temperature changes on the transmission system (steel rod, suspension wires and pulley wheel). A small ivory pointer J is adjusted in position so that its tip indicates the level at which the mercury should stand in the float when the appropriate quantity of air is contained in the latter.

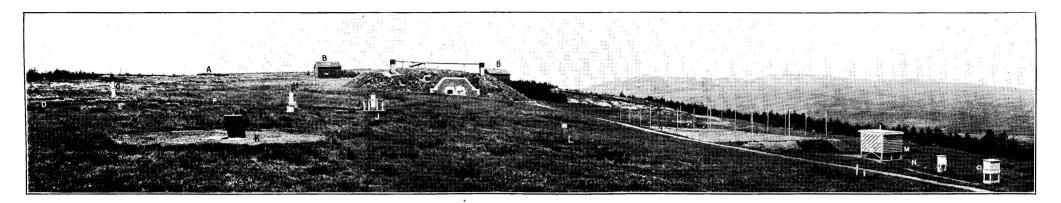


FIG. 10. GENERAL VIEW (NORTH-WEST TO NORTH-EAST) FROM MAIN OBSERVATORY BUILDING.

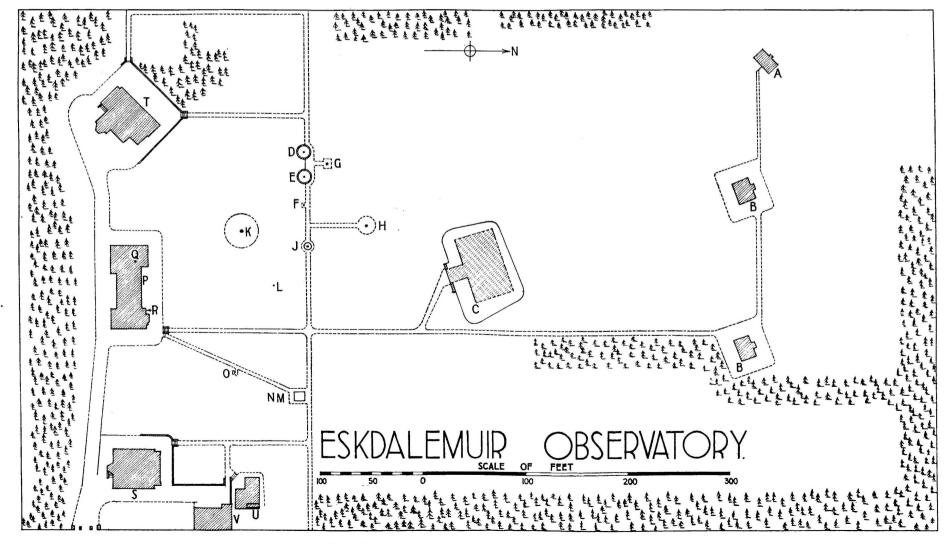


Fig. 11. Site Plan (for explanation see page 93).

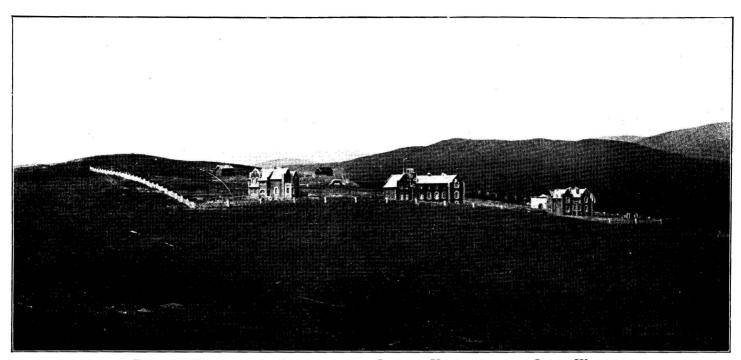


Fig. 12. Eskdalemuir Observatory.—General View from the South-West.

The Office Block is the middle one of the three buildings in line; the Superintendent's house is on the left, the Assistants' quarters on the right. The two huts in the background are the wooden magnetic huts for "absolute" observations. In front of the right-hand hut is seen the mound of the underground magnetic chamber, with the stonework of the top of the porch.

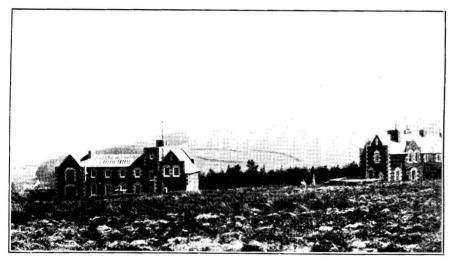


Fig. 13. View from West Magnetic Hut, showing proximity of Superintendent's House to the Anemograph on Main Observatory Building.

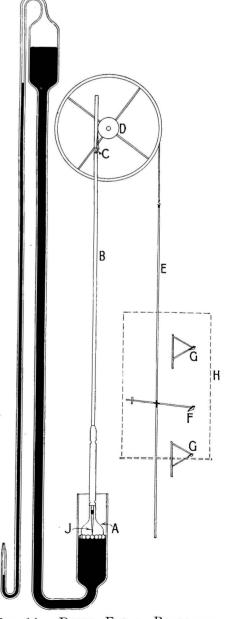


Fig. 14. Dines Float Barograph (for explanation see page 94).

The scale of the records of the Dines float barograph is very approximately From determinations made in December, 1922, it was found that for the Eskdalemuir instrument I millimetre on the paper = .632 millibar. The time scale

of the record is $15 \cdot 2$ millimetres on the paper = 1 hour.

Unfortunately the behaviour of the instrument was not entirely satisfactory during 1923. On many occasions there was evidence of sticking. This was probably due to the corrosion of certain of the moving parts, the instrument having been exposed to the damp atmosphere in the Underground Magnet House since September, In the continued absence of the photographic barograph it was considered inadvisable entirely to dismantle the float barograph for cleaning. throughout 1923 each day's record was treated on its merits and tabulated with reference to the eye readings of the standard barometer at 7h, 9h, 13h, 15h, 18h, and 21h. On occasions of defective record hourly values were obtained from the weekly records of a Richard barograph, pen recording, situated in the main building.

Temperature.—The photographic thermograph and the standard mercurial thermometers, dry bulb (M.O. 19123) and wet bulb (M.O. 1695), are situated in a wooden hut, provided with louvred sides and double roof, which is some 200 feet (60 m.) north-north-east of the Main Building (see Fig. 10). The installation is similar to that described on p. 12 except that a special enclosure is provided inside the hut to accommodate the optical and photographic arrangements.

The scale values of the thermograph records are 1° absolute = 2.79 millimetres and 2.44 millimetres on the paper for the dry and wet bulb records respectively,

while the time scale is I hour = 9.20 millimetres.

As auxiliary recorders of temperature there are, in the same louvred hut:—

- (a) A psychrograph, pen recording, which is in effect a bimetallic spiral thermograph with two spirals, one of which is kept dry and the other wet. The records are of 24 hours duration.
- (b) A bimetallic spiral thermograph (Short and Mason, M.O. 184), of which the record is changed every week. It is described in the Meteorological Observer's Handbook.

Humidity.—In addition to the dry and wet bulb thermograph described above there is a Richard hair hygrograph (M.O. 59) which is situated in a Stevenson screen about midway between the louvred hut and the Main Building.

As is stated on p. 16, the records from this instrument are utilised when the wet bulb reading does not exceed 273a. On the records obtained in 1923 a change of 10 per cent. in relative humidity is represented by about 0.8 centimetre, the time scale being I hour = 3 millimetres.

Rainfall.—The recording instrument is a Beckley self-registering rain-gauge (No. 4), which is described on p. 12. The time scale of the record is 1 hour = 9.24millimetres on the paper and the rain scale has a magnification of 3.35. instrument has been in use at Eskdalemuir since 1908 and was originally installed at Fort William in July, 1890.

The conical part of the gauge funnel is surrounded by a cylindrical copper casing lined with asbestos on the inner side and of diameter equal to that of the funnel, viz. 11.27 inches (28.6 cm.). Within the enclosure so formed is a gas jet, and a flame of suitable dimensions is maintained, as circumstances dictate, to melt snow which may be collected.

The gauge is surrounded by a circular turf wall or dyke, the top of which is on a level with the rim of the gauge; the external and internal diameters of the dyke

being II·5 feet (3·5 m.) and 7 feet (2 m.) respectively.

A standard 8 inch (20·3 cm.) rain-gauge (M.O. 391) is situated some 24·5 feet (7.5 m.) to the east of the Beckley gauge and is surrounded by a turf dyke of similar Readings of amounts of rain received in the 8 inch gauge are made at 7h and 18h G.M.T. It is customary to adjust the indications of the recording gauge to agree with the readings of the standard check gauge.

Sunshine.—The record of sunshine is obtained from a Campbell-Stokes recorder (M.O. 99) described on p. 13.

The recorder is fixed on a stone pillar and has a reasonably free exposure, the chief obstacles being hills to east and west. The elevation of hills between 70° and 110° east of south varies from $2 \cdot 5^{\circ}$ to 5° , while between 50° and 135° west of south the high ground varies in elevation from 3° to $4 \cdot 4^{\circ}$, being generally about $3 \cdot 5^{\circ}$. As sunshine can be recorded when the sun is 3° above the horizon only in the most favourable circumstances, it appears that the loss of record occasioned by the neighbouring high ground is of relatively small extent and is confined mainly to a possible defect of record at the beginning of the day during a few weeks centred about the equinoxes.

Solar Radiation.—Measurements of the intensity of radiation received from the sun by a surface which is normal to the line drawn from the instrument to the sun are effected by means of an Ångström compensating pyrheliometer* (No. 116). The intensity of radiation is expressed in milliwatts per square centimetre (1 mw. per sq. cm. = 0.01435 gramme calorie per sq. cm. per minute). In addition the value is given of the function (p/p_0) sec Z, in which p is the barometric pressure at the observatory in millibars at the time of the observation, p_0 is 1000 millibars, and Z is the zenith distance of the sun. This affords a measure of the mass of atmosphere which the solar radiation has had to penetrate before reaching the earth. Entries in the column headed "Sky" are intended to show the presence or absence of haze, mist or cloud in the direct path of the solar radiation recorded.

Wind.—A Dines tube anemograph (M.O. 1015), furnished with direction recorder, is situated in the Main Building. The vane-head is 15 metres above a tangent plane to the slope of the hillside and approximately 7 metres above the general level of the roof of the building. A description of the speed recorder will be found on p. 14.

The records of speed and direction are obtained on the same chart. The recorder in use throughout 1923 was provided with a Munro-Rooker single-pen direction recorder. In this arrangement the lower end of a long vertical rod, rigidly attached at its upper end to the freely moving vane, is connected to the vertical axle of a short solid brass cylinder which consequently rotates with the vane. In the curved surface of the cylinder is cut a helical channel in which runs a short roller projecting from the side of a pivoted pen arm. The helix forms a nearly complete turn, and the upper and lower ends are connected by a steep cam. As the recording pen reaches the upper North line on the chart it is rapidly forced by the connecting cam to the bottom North line, or conversely if the wind direction is changing from east of north to west of north. For some years prior to the introduction, in June, 1922, of the Munro-Rooker recorder a Dines twin-pen recorder was in use.

Apart from the surrounding hills, the exposure of the vane-head is tolerably free in all directions save to the west where at a distance of some 130 feet (40m.) is a rather large building (see Fig. 13) of which the height is somewhat greater than that of the Main Building. With winds from nearly due west the direction records show markedly greater turbulence than with other winds.

Minimum Temperature on the Grass.—The thermometer (M.O. 13) used for readings of grass minimum temperature is of the spirit type with index; and when exposed, between 18h and 7h G.M.T., is supported at a height of one or two inches (4 cm.) above close-cropped grass a few metres from the louvred thermometer hut.

Notes on Results.

Diurnal Variation of Atmospheric Pressure.—The values of the mean diurnal inequalities for the several months are given in Table 124, p. 127. The inequalities for February and August are somewhat irregular and in each case the range is smaller

^{*} For description see The Observer's Handbook, 1921, Ed., Meteorological Office, London; Astrophysical Journal, Vol. IX, 1899; Actes de la société royale des Sciences d'Upsal, 1893; also Geophysical Memoirs, No. 21 (1923), Meteorological Office, London.

than usual. In September, October and December the early morning minimum is very prominent in comparison with the afternoon minimum. The inequalities for April, May, July, August, September, October and November are alike in that the principal maximum occurs in the late evening and the principal minimum in the early morning. The inequality for March shows considerable regularity and that for April approximates closely to the normal type for that month.

The results of the harmonic analysis of the monthly and seasonal mean diurnal inequalities for 1923 are given in the accompanying table, along with the corresponding results for the mean inequalities for the period 1911-20. The data for the latter period have been discussed recently by Dr. A. Crichton Mitchell.* In computing the Fourier coefficients for the individual months of 1923 the unit employed was of mb.; while for the seasons and year the inequalities were taken to oor mb.

and the values of the amplitudes are also given to three decimal places.

As is apparently usual, the 24-hour term shows considerable irregularity from month to month both in amplitude and phase, although the variation in phase is comparatively small from September to December. Apart from the January value c_2 is largest in the equinoctial months, as in the "normals" for 1911–1920. The predominance of c_2 in March, 1923, is very marked. The amplitudes of the 8-hour term seem to be rather greater than usual and the transition in phase from winter to summer is less abrupt than in 1922.

HARMONIC COEFFICIENTS OF THE DIURNAL INEQUALITY OF ATMOSPHERIC PRESSURE—ESKDALEMUIR.

Values of c_{n_1} α_n in the series $\sum c_n \sin (15nt + \alpha_n)$, t being reckoned in hours from midnight, G.M.T.

Mont and			¢ ₁		α1	ļ	<i>c</i> ₂	 	α,		<i>c</i> ₃	ļ	α3		-		α
Season		1923.	1911– 20.	1923.	1911– 20.	1923.	1911– 20.	1923.	1911– 20.	1923.	1911– 20.	1923.	1911– 20.	1923.	1911- 20.	1923.	1911 20.
		mb.	mb.	0	•	mb.	mb.	•	•	mb.	mb.	۰	•	mb.	mb.	•	۰
an		.31	.094	159	343.2	.35	.235	139	145.2	•20	.125	354	335.7	.05	·046	231	201
eb.	• •	.53	.118	107 ₁₅	211.9	:07 :44	.273	151	131.7	.09	.083	334	331.6	.03	.042	103	54.
Iar	• •	·þø	.128		182.1		.304		138.9	.08≲		379	325.4	.084		4615	11.
pr	• •	.28	.205	117	89∙1	*34	.299	134	148.4	.05	.022		146.7	.04	·045	342	342
ſа́у	• •	.07	.225	251	49.5	.53	.270	138	141.0	.09	·0 <u>7</u> 5	169	150.5	.04	.032	285	317
une	• •	.24	.152	353	50.7	.18	.234	133	139.7	.07	∙084	146	151.0	.04	·018	292	312
uly	• •	.09	.171	164	66.2	.23	.211	141	134.8	.08	.077	143	146.2	.01	.023	4	287
ug.	• •	.06	.114	156	111.4	·II	.239	117	141.3	•06	.057	122	147.6	.05	.047	311	318
lept.	• •	'34	.121	189	84.5	•29	.313	141	145.2	.04	.012	57	101.1	.04	.050	343	331
ct.	• •	.63	.110	173	72.8	.35	.312	125	153.I	.10	·060	5	358.6	.02	.041	19	20.
lov.	• •	.22	.125	190	180.3	·12	.242	151	161.7	.11	.101	18	359.6	.02	.012	167	133.
Dec	• •	43 ا	.137	197	93.9	21	.213	117	140.2	12	.124	345	354.6	.05	.067	191	200
ear		162	∙085	171	87.6	233	•260	142	143.7	033 037	.020	35	32·I	012	.016	318	329
Vinter			·038	172	162.2	.183	·236	136	144.5	•126	.106	353	345.9		.023	193	176
quinox		227	·108	i67	100.7	183 353	.306	136	146.4	.0333	.021	2432	354.8	027	.044	162	356
ummer		.016	.153	304	64.0	188	·238	134	139.4	·071	.074	141	148.9	.031	•030	300	311

Note.—Winter comprises the four months January, February, November, December Equinox the months March, April, September, October. Summer the months May to August.

ATMOSPHERIC ELECTRICITY.

Notes on the Instruments.

Autographic records of atmospheric electrical potential gradient were obtained by means of an electrograph of the Kelvin water-dropper type. In all essential details the electrograph arrangements, the method of making scale and insulation tests and the method of reducing the autographic curve readings to potential gradient in the open were as described in the *Observatories' Year Book*, 1922, pp. 75–76.

^{* &}quot;On the Diurnal Variation of Atmospheric Pressure at Eskdalemuir and Castle O'er, Dumfriesshire," by A. Crichton Mitchell, D.Sc., Quarterly Journal of the Royal Meteorological Society, Vol. L., No. 210, April, 1924.

As in former years the Wulf quartz-thread electrometer, No. 3040, was used in the determination of scale values of the photographic records and in the absolute

observation of potential in the open.

By reason of adjustments to the Dolezalek electrometer of the electrograph system, chiefly between the middle of May and the beginning of August, 1923, there were various changes in the scale value of the electrograph records. From January to April the scale value was from 5 to 6 volts per millimetre, while from August to December it was about 9.35 volts per millimetre.

The values of the factor used in converting the potential recorded to the potential at 1 metre above the surface of the ground in the open are given in Table 208. The monthly factors ranged from 6.87 in March to 6.37 in August. The values from January to May were appreciably higher than the values in the months preceding or following that period. No intentional changes in the jet exposure or in the method of determination of potential in the open are known to have been introduced.

Notes on the Tables and Results.

Table 208 contains the values of electrical potential gradient at 3h, 9h, 15h and 21h G.M.T. daily, the value for a given hour representing the mean for the period of 60 minutes centring at that hour. The reduction factors used in converting the potential at the water jet to potential gradient, in volts per metre, in the open are also given.

As far as possible an electrical character figure is assigned to each day and values of potential gradient are assigned for 3h, 9h, 15h and 21h G.M.T. on all days, while values for all hours are assigned on days classified as 0a, 1a or 2a. The character figures are given in Table 210A, the significance of these symbols being as follows:—

o, denotes a day during which from midnight to midnight no negative potential was recorded.

I, denotes one or more excursions of limited duration to the negative side of the scale during the same period.

2, denotes negative potential extending in the aggregate over three hours

or more during the same period.

a, denotes that within the 25 periods of 60 minutes for which an estimate of the mean potential gradient has to be made in the process of tabulation there was in no case a range of potential gradient in the open exceeding 1,000 volts.

b, denotes that, during the same period, a range of 1,000 volts or more was reached in one hour at least but in fewer than six hours.

c, denotes that, during the same period, a range of 1,000 volts or more was reached in at least six hours.

In Table 209 are given, for oa days, (1) the monthly, seasonal and annual inequalities, (2) particulars of the number of days and of the non-cyclic changes and (3) the corresponding mean values of potential gradient. The inequalities or the mean values for the year and seasons are the means of the inequalities or means, respectively, for the appropriate months.

It should be noted that, in these tables, Winter denotes the four months January, February, November, December; Equinox the four months March, April,

September, October; and Summer the four months May to August.

Corresponding data for 1a and 2a days combined appear in Table 210.

Contrary to the practice followed in former years the mean values of potential gradient given in Table 208 are of two kinds, viz., (a) the means of all the positive values of potential in the column and (b) the algebraic mean derived from all days on which all four hours were represented. The mean values for the month as derived from the (a) and (b) values respectively, are shown in the last line. It is to be expected that the mean derived from the values at 3h, 9h, 15h and 21h, on a sufficiently large number of days will approximate closely to the mean value derived from the 24-hourly

values of each of the days. As might have been anticipated the (a) mean exceeds the (b) mean in each month of the year. Moreover, in each month, with the exception of December, the mean for 0a days exceeds the corresponding (a) mean. For the whole year the mean from 0a days was 278 v/m, that from positive values at 3h, 9h, 15h, and 21h was 235 v/m, while that from the complete days of Table 194 was 159 v/m. It may be noted that the effect of high negative potential on certain days in February was to make the (b) mean at 9h and 15h negative. On February 10th the potential was mainly negative from 1h 30m to shortly after 15h, and the mean value from 7h to 10h was approximately -2200 v/m.

The values of mean potential gradient on oa days for the year, winter and summer, are rather higher than the corresponding values for 1922. The value, 299 v/m, for July is unusually high, but there were only five oa days and the mean appears to be greatly influenced by the high potential recorded during several hours on the 4th.

8th and 12th, when fog or cloud at ground level prevailed.

The mean diurnal inequalities on oa days for the year and seasons are fairly close to the respective normal types, but there are rather more irregularities than in 1922. The range of the mean diurnal inequality for winter is greater than usual, being largely due to the high range of the November inequality. In the mean inequality for equinoctial months the secondary maximum near 7h is somewhat more prominent than usual, the effect being attributable to the March and September contributions. In each of the four summer months of 1923 the principal minimum occurs in the afternoon, but in May and July the early forenoon maximum is in excess of the evening maximum.

TERRESTRIAL MAGNETISM.

Notes on the Instruments.*

The magnetographs in use are situated in the east chamber of the Underground Magnet House and are arranged so as to record changes of the three geographical components of terrestrial magnetic force, viz., the north component, N (or + X), west component, W (or - Y), and the vertically downward component, V (or + Z).

The diurnal range of temperature in the east chamber of the magnet house is normally negligible. Temperature is ascertained daily at 9h 30m by the thermometers within the instrument cases. The daily values appear in Tables 214, 218, etc.; the monthly means of the readings so obtained during 1923, together with the mean values for the years 1911–22, were as follows:—

EXCESS	OE	MEAN	TEMPERATURE	AROVE	280a	

Month.			Jan.	Feb.	Mar.	Apr.	Мау	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
Mean 1923			4.1	3.9	3.8	3.6	3.7	4.1	5.8	7:3	7.7	7.6	7·I	5.7
Mean 1911-22	••	••	3.4	2.6	2.4	2.2	2.5	3.4	4·4	5.5	6.2	6·1	5.4	4.4

The annual range of temperature during 1923 was 4·3° C., the mean range for

the previous twelve years being also $4\cdot3^{\circ}$ C.

The north and west component instruments are of the bifilar type, by Adie. In each of these instruments the torsion of a bifilar suspension, of fine tungsten-steel wire, is utilised to bring the magnet into an azimuth approximately perpendicular to the direction of the component of which the changes are recorded. The instrument for the vertical component is a multiple magnet balance designed by the late

^{*} For more detailed accounts of the magnetographs, absolute instruments and normal methods of procedure, see *The Observatories' Year Book*, 1922, pp. 77 et seq.

Professor W. Watson, F.R.S. It was necessary to adjust this instrument on only one occasion during 1923, viz., December 21st. On that date the small magnet on the pillar which supports the balance was lowered slightly, the base line value on the

record being thereby decreased by about 110%.

As a result of an adjustment made to the west instrument on August 30th, the magnet was displaced in azimuth between 9° and 10° east of north. Most unfortunately this was not detected until the end of 1924 when it was found that the suspended magnet was inclined at 9°·7 east of north. Thus, from 1923 August 30th until the end of 1924 the records obtained from the west magnetograph were not simply of changes in W but of changes in the component W', which is given by $W' = W \cos \alpha + N \sin \alpha$; α being the inclination, measured from north through east, of the magnet to the geographical meridian. The gradual easterly drift of the magnet amounted to about 15' between September, 1923, and December, 1924, and therefore the value of α for the period August 30th to December 31st, 1923, has been taken as 9°·5. The methods which have been adopted to allow for the consequences of this error in azimuth of the west magnet are described at the end of the present section.

The constants of the magnetographs were as follows:—

			•			North.	West.	Vertical.
Time Scale				I hou	ır =	15·6 mm.		
Time marks						Every two ho	ours, beginning a	t exact hour.
Error of time mark		٠.				Not:	more than \pm 1 1	nin.
Period of vibration, s	econds					14.0	11.0	7 4
Logarithmic decreme	nt *					•369	·639	<u> </u>
Angular equivalent o	f r mm.	on pa	per, rad	ians		.00032	00032	.0003
Twist of bifilar susper	nsion	••	• •			35 ⁸	90°±5°	
Ratio length of bifilar	suspens	sion				51	66	
mean breadth o	f susper	ision	• •	• •		J.	O,O,	
Temperature coefficie						-9 γ	-2γ	+26 y
Direction of marked						West.	North.	
Azimuth of magnet						270° 8′	I° IO'	346°
Azimuth of magnet	• •	• •	• •	• •		270 8	1 10	340

^{*} Log. decr. = $\log_e a_n - \log_e a_{n+1}$; where a_n , a_{n+1} are the amplitudes of two successive swings on the same side of the zero position.

In the above table the constants for the west magnet refer to the period prior to August 30th. After that date, as has been stated, the azimuth of the magnet was approximately 9° 30′, but there were no determinations of period, logarithmic decrement or suspension constants.

The scale values of the magnetographs were determined at intervals of two weeks. In the following table are given the scale values, obtained by overlapping means, which were employed in reducing the curve readings. For the west instrument the scale values for the period subsequent to August 30th are the scale values of the component W' (see above).

Scale Values of the Magnetographs (γ per mm. on the paper).

								· • · · · · · · · · · · · · · · · · · ·	_				
Month.		Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
North Instrument		4.87	4.87	4.87	4.87	4.87	4.87		4.83				4.86
West Instrument	••	5:33	5.33	5.34	5.33	5:34	5.33	5.32	{5·30† 5·24	5.24	5.25	5.24	5.25
Vertical Instrument	•	1	į.	1	Į.		1	3.93	1	3*94	3.95	3.94	$\begin{cases} 3.92 \\ 4.18 \end{cases}$

^{† 5.30} to Aug. 30d 14h; 5.24 from Aug. 30d. 18h to Aug. 31d 24h.

^{1 3.92} to Dec. 21d 11h; 4.18 for remainder.

Absolute observations of horizontal force, declination and inclination were taken, usually twice weekly, in the east magnetic hut. Declination and horizontal intensity were determined by means of the Kew pattern unifilar magnetometer, Elliott No. 60 (collimator magnet 600 and mirror magnet 600), placed on Pier No. 5, and determinations of inclination (dip) were made with the Schulze Inductor, No. 103, placed on Pier No. 6. In the deflection experiment of the horizontal intensity determination observations were made for three distances of the collimator magnet, viz. 25, 30, 35 cms. The value of the correction, $\log_{10} \left(1 + \frac{P}{25^2} + \frac{Q}{25^4}\right)$, used in the reduction of the horizontal intensity observations was obtained for a given month by taking the mean derived from the observations obtained during the seven months including the given month as fourth of the seven. For the year 1923 the values of this correction were as follows:—

January, .00514; February, .00503; March, .00488; April, .00494; May, .00486; June, .00496; July, .00514; August, .00515; September, .00523; October, .00537; November, .00536; December, .00541.

The base line values of the magnetograph records are deduced from the results of the absolute observations, any of the latter obtained during times of considerable disturbance being excluded. The base line values finally adopted are obtained from a curve drawn smoothly through points given by the deduced values.

The results of the absolute determinations of D, I and H are summarised in the subjoined table and the values of m, the moment of collimator magnet 60a, are also given. For each set of absolute observations are shown the deduced base line values of N, W and V and, in brackets, the adopted base line values. Thus, the entry 15823 (18) signifies:—deduced base line value 15823, adopted base line value 15818. The adopted values were obtained as described in the foregoing, and therefore the base line values corresponding to dates between those given in the table may be obtained by interpolation. As has been mentioned above, the "west" magnet recorded the component W' from August 30d 18h and in the table below the base line values of W' are given from August 31st. On December 21st, between 11h and 12h, a discontinuity in the base line value of V was introduced, the base line value being decreased by 112 γ .

Absolute Determinations of D, I and H, and Base Line Values of N, W and V. Eskdalemuir. 1923.

Da	te.	De	clina	tion.		Incl	Inclination.			rizontal I	Force.	Base Line Values (deduced and adopted).			
. —		Mean Time.		D.		Mean Time.		I.	Mean Time.	H.	m.	North.	West.	Vertical.	
		h m	0	,	"	h m	0	,	h m	γ					
								- 0 .				15,000 γ +	4,000 y +	44,000 y +	
Jan.	2	14 9	16	22	54	12 53	69	38.7	11 21	16671	906.5	813 (16)	643 (44)	851 (55)	
	6	14 3	16	21	20	12 25	69	37.9	10 51	16680	907.1	821 (15)	641 (43)	866 (56)	
	9	14 13	16	22	33	15 32	69	38.9	11 6	16671	906.8	813 (14)	645 (43)	867 (57)	
	12	14 35	16	21	15	12 29	69	38.7		-				00 (6)	
	16	14 23	16	19	28	11 15	69	39.2	11 53	16680	907.2	822 (14)	639 (42)	882 (61)	
	19	14 17	16	20	38	10 45	69	38.9	11 18	16687	908.0	823 (14)	643 (42)	923 (863)	
	23	14 27	16	22	58	12 29	69	41.2	II I	16664	906.6	806 (15)	642 (42)	858 (67)	
	23		_	-			_	_	12 47	16662	906.8	803 (15)	641 (42)	850 (67)	
	26	14 30	16	22	28	12 36	69	39.0	11 9	16665	906 9	809 (15)	645 (41)	858 (70)	
	30	15 27	16	20	8	15 5	69	40.5	11 34	16649	907.2	808 (15)	639 (41)	851 (73)	
Feb.	2	14 21	16	20	15	11 36	69	38·9	12 15	16684	907.0	823 (16)	639 (41)	892 (76)	
	6	14 27	16	19	23	11 16	69	38.9	11 55	16672	907.7	819 (17)	642 (41)	886 (79)	
	9	14 23	16	19	48	11 3	69	38 8	II 37	16682	907 6	824 (17)	641 (41)	890 (81)	
	ı́3	14 45	16	20	30	11 10	69	39.5	11 47	16666	907.5	810 (18)	641 (41)	866 (85)	
•	16	14 53	16	21	8	II 12	69	38·8	11 49	16675	907 · I	823 (18)	641 (41)	893 (87)	
	20	15 13	16	23	25	11 4	69	40·I	11 38	16674	906.8	807 (18)	651 (41)	897 (88)	
•	23			_		10 59	69	40·I	_			' '	`	894 (89)	

Absolute Determinations—continued.

D-4	ło.	De	clina	tion.		Inc	linati	on.	Но	rizontal I	Force.		ase Line Val	
Dat	æ.	Mean Time.		D.		Mean Time.		I.	Mean Time.	H.	m.	North.	West.	Vertical.
		h m	•	,	•	h m	0	,	h m	γ				
Mar.	2 6 9 13 20 24 28 30	14 41 14 53 15 13 14 35 12 13 11 1 14 23 14 39	16 16 16 16 16 16 16	20 20 20 22 20 23 22 22	10 38 38 33 45 41 25 38	12 35 11 17 11 30 11 14 14 51 11 47 12 44 11 35	69 69 69 69 69 69	39·4 39·1 39·2 39·1 38·1 41·6 40·8 40·0	11 58 11 53 12 6 11 51 11 36 11 5 12 5 10 57	16655 16674 16667 16658 16657 16636 16677 16662	907·8 907·5 907·6 907·3 907·5 908·1 907·1	810 (17) 811 (16) 809 (16) 811 (16) 819 (15) 822 (15) 823 (15) 817 (15)	4,000 y + 637 (40) 641 (40) 641 (40) 638 (40) 640 (40) 639 (40) 642 (40) 650 (40)	44,000 γ + 870 (90) 871 (91) 875 (92) 880 (93) 906 (894) 906 (896) 923 (897) 913 (897)
Apr.	3 6 10 13 14 17 20 24 27	14 31 15 47 14 15 — 11 23 14 17 14 29 14 21 14 55	16 16 16 16 16 16 16	22 19 20 — 20 21 18 21 19	35 53 6 43 41 16 12 58	12 27 12 15 12 28 12 41 	69 69 69 69 69 69 69	40·5 40·5 39·0 39·7 41·1 39·2 40·0 39·9	II 48 II 34 II 53 I2 5 — II 29 II 27 II 18 I2 33	16679 16672 16674 16636 — 16675 16673 16656 16668	908·0 907·5 908·0 907·8 —— 907·8 907·7 907·5	823 (15) 818 (16) 818 (16) 809 (16) 820 (17) 820 (17) 811 (16) 800 (16)	643 (40) 640 (40) 632 (40) 647 (40) 642 (40) 627 (40) 638 (39) 642 (39)	920 (898) 900 (899) 888 (901) 893 (903) 925 (04) 910 (04) 892 (05)
May	1 4 8 11 15 22 25 29	14 53 14 33 16 13 14 29 15 37 14 21 16 39 15 15	16 16 16 16 16 16 16	17 18 17 17 17 16 22	49 40 50 8 15 53 37 12	12 25 12 7 16 27 12 11 12 15 12 4 12 11 12 31	69 69 69 69 69 69	38·9 38·9 39·0 38·9 40·1 40·4 39·2 39·5	II 47 II 29 II 57 II 31 II 36 II 27 I4 46 II 48	16678 16681 16681 16655 16655 16652 16673 16691	907·5 907·3 907·7 907·7 907·4 907·5 906·9 909·2	814 (16) 823 (15) 823 (14) 812 (14) 817 (14) 807 (13) 804 (13) 833 (12)	636 (39) 641 (39) 639 (39) 634 (39) 632 (39) 629 (39) 640 (39) 645 (39)	901 (06) 929 (06) 921 (05) 888 (905) 920 (04) 878 (904) 901 (04) 1005 (906)
June	1 5 8 12 15 19 21 26 29	15 25 14 33 14 43 15 38 14 39 15 29 15 13 14 43 16 17	16 16 16 16 16 16 16	17 21 17 18 18 19 18 18	58 19 57 21 20 52 3 17 6	12 30 12 48 12 45 12 43 12 43 12 41 12 16 12 17 12 10	69 69 69 69 69 69 69	39·6 39·7 38·9 38·5 39·8 39·1 38·9 39·5 40·7	11 51 11 42 11 22 11 30 11 33 11 57 11 43 11 43 15 23	16692 16686 16667 16681 16698 16698 16682 16700 16668	907·5 907·6 906·7 906·8 907·1 908·0 907·7 907·7 906·8	819 (12) 808 (13) 808 (13) 806 (15) 803 (17) 825 (20) 821 (22) 833 (26) 806 (29)	638 (40) 644 (40) 641 (40) 643 (40) 638 (40) 642 (41) 641 (41) 644 (42) 637 (42)	913 (02) 892 (902) 881 (902) — 856 (902) 898 (902) 926 (02) 937 (02) 857 (902)
July	3 6 10 13 16 20 24 27 31	15 5 15 3 15 51 14 45 15 31 14 17 15 31 15 5 15 17	16 16 16 16 16 16 16	17 18 15 15 19 11	13 55 30 3 33 37 53 33 8	12 33 14 40 12 23 15 5 12 31 14 51 12 36 12 33 12 23	69 69 69 69 69 69 69	39·4 38·2 38·4 39·1 39·1 39·9 39·1 38·5 38·9	11 54 12 40 13 47 13 25 11 53 11 9 11 59 11 55 11 43	16689 16675 16723 16686 16704 16690 16677 16676 16692	907·1 906·0 905·9 907·0 908·4 908·0 907·6 907·1	836 (33) 829 (36) 856 (39) 836 (41) 855 (43) 854 (45) 840 (47) 844 (48) 852 (49)	643 (42) 638 (42) 648 (43) 640 (43) 649 (43) 651 (44) 641 (44) 645 (44) 647 (45)	920 (02) 906 (02) 944 (02) 911 (02) 938 (02) 939 (02) 883 (901) 896 (900) 897 (900)
Aug.	2 3 7 10 14 17 21 25 28		16 16 16 16 16 16 16	19 16 16 15 13 15 18 16	5 53 58 53 37 10 25 13	14 24 14 13 15 39 12 33 12 27 12 25 14 42 12 28 12 15 12 11	69 69 69 69 69 69 69	37·7 38·5 39·1 39·3 38·6 39·0 38·7 40·5	14 59	16649 16688 16685 16718 16687 16684 16681 16687	907·4 	850 (49) 856 (50) 848 (50) 866 (50) 842 (50) 848 (50) 848 (50) 862 (50) 852 (50)		872 (99) 900 (899) 910 (899) 919 (898) 896 (96) 923 (896) 892 (95) 894 (94) 886 (94) 931 (894)

ABSOLUTE DETERMINATIONS—continued.

Da	ate.	De	clina	tion.		Incl	linati	on.	Ho	rizontal F	orce.		se Line Val	
		Mean Time.		D.		Mean Time.		I.	Mean Time.	н.	m.	North.	West.	Vertical.
		h m	٥	,	•	h m	۰	,	h m	γ		15,000 γ +	6,000 γ +	44,000 γ +
Sept.	4 7 11 14 18 21 25 27 28	14 35 14 59 14 33 15 15 14 39 15 15 14 33 — 13 3	16 16 16 16 16 16	15 14 16 14 13 13 —	18 15 1 20 38 25 48	12 33 15 31 12 21 12 21 12 31 12 26 12 1 11 9 12 3	69 69 69 69 69 69	40·7 39·3 40·0 40·3 39·1 38·8 39·0 42·3 40·0	II 59 II 56 II 41 II 43 II 51 II 47 II 17 — II 25	16679 16664 16685 16683 16683 16677 16676	907·3 907·1 907·2 907·5 907·2 906·9 907·0	857 (50) 840 (50) 853 (50) 863 (50) 848 (50) 847 (50) 848 (50) 849 (50)	963 (61) 954 (60) 959 (60) 963 (60) 953 (59) 955 (59) 955 (59)	958 (894) 870 (94) 924 (894) 930 (894) 890 (95) 883 (96) 893 (98) 888 (98) 885 (99)
Oct.	1 2 3 3 4 4 5 9 16 19 23 26 27 29	14 31 — 15 45 14 57 14 59 15 23 15 17 14 53 11 21 11 3	16 16 16 16 16 16 16	15 	20 43 33 23 53 3 55 25	12 39 14 16 12 12 12 14 15 43 12 13 15 21 12 47 14 40 14 46 12 30 12 11 11 41	69 69 69 69 69 69 69 69	39·6 39·5 39·5 39·7 38·9 39·8 38·7 39·4 42·8 41·2 39·5 40·3	II 3I II 3I II 3I II 32 II 32 II 47 II 33 II 47 II 33 II 4	16668 	907·1 	851 (50) 851 (49) 855 (49) 855 (49) 852 (48) 860 (48) 851 (47) 844 (46) 847 (46) 845 (45)	964 (59) — 965 (59) 960 (59) 962 (59) 962 (59) 962 (59) 959 (59) 953 (59) 956 (59)	894 (900) 891 (900) 894 (900) 903 (00) 900 (00) 903 (01) 906 (01) 926 (03) 935 (06) 980 (07) 929 (09) 910 (10)
Nov.	2 6 9 13 16 20 27 30	14 39 15 11 14 27 14 49 14 21 14 37 15 9 14 29	16 16 16 16 16 16 16	13 12 13 11 10 13 12	9 0 50 8 43 43 53 16	12 13 12 21 12 11 12 21 12 24 12 24 12 11 12 9	69 69 69 69 69 69	40·3 39·5 39·7 39·6 38·6 38·6 39·7	11 39 11 41 11 31 11 43 11 45 11 45 11 26 11 27	16674 16671 16676 16676 16679 16667 16656	906·2 907·1 907·3 907·3 907·5 906·6 906·9	860 (44) 838 (43) 843 (42) 842 (40) 842 (39) 824 (37) 829 (34) 834 (32)	969 (59) 957 (58) 962 (58) 958 (57) 961 (57) 954 (56) 950 (55) 958 (55)	956 (13) 905 (15) 921 (17) 921 (18) 923 (19) 869 (920) 908 (22) 932 (23)
Dec.	5 7 11 18 22 24 28	14 49 15 11 14 33 15 1 12 19 15 7 14 13	16 16 16 16 16	10 10 9 9 12 12	14 40 43 5 40 13 23	12 25 12 21 12 2 12 35 12 4 14 43 12 15	69 69 69 69 69	39·4 39·2 39·7 38·4 38·8 39·4 39·9	II 45 II 43 II 23 II 55 II 27 I2 II II 33	16664 16691 16669 16686 16667 16648 16670	907·I 907·3 906·8 907·3 907·0 906·8 907·7	820 (29) 837 (28) 829 (25) 829 (21) 813 (19) 811 (18) 813 (17)	946 (54) 960 (53) 955 (52) 951 (51) 945 (50) 944 (50) 956 (49)	900 (25) 957 (26) 937 (27) 969 (35) 822 (38) 817 (37) 835 (35)

The hourly readings are obtained from the magnetograms, standardised as described in the foregoing, by means of a ruled glass scale. The reading for any given hour G.M.T. is that ordinate estimated to be the mean reading for 60-minutes centering at the given hour. The product of this ordinate and the scale value is added to the adopted base line value, and the sum so obtained is the hourly value printed in the tables.

In consequence of the error in the azimuth of the "west" magnet (August 30th—December 31st, 1923) it has been necessary to introduce modifications in certain parts of the normal procedure described above. To obtain the true scale values of the W' record it was necessary to multiply the values derived in the usual way, and in the belief that the magnet azimuth was correct, by $\cos 9^{\circ} \cdot 5$. For the period named,

base line values of W', not W, were computed; and in the calculations of the base line values of all three components, N, W' and V, the circumstance that W' and not W was recorded was allowed for. Hourly values of W' were tabulated, and from each such hourly value and the corresponding hourly value of N the hourly value of W was deduced, using the relation $W = W' \sec \alpha - N \tan \alpha$, i.e., $W = \text{i·oi39i}\ W' - \text{o·i6734}\ N$. The finally resulting hourly values of W showed differences mostly of the order of $\text{i}\gamma$ or $\text{i}\gamma$, but on disturbed occasions varying up to $\text{i}\text{i}\gamma$, from the values computed on the assumption that W and not W' was recorded. The algebraic mean difference over the four months amounted to $\text{o·8}\gamma$. Therefore, so far as the actual hourly values are concerned, it has been possible to eliminate the effects due to the displacement of the "west" magnet and the results published may be regarded as of the normal order of accuracy; the same consideration applies to the diurnal inequalities.

The determination of daily maxima and minima and daily ranges of W is less straightforward. If W_0 ', N_0 are the base line values of the W' and N records; w', n corresponding curve ordinates in millimetres; c', b the scale values of the W' and N records in γ per m.m., then

$$W = W_0{'} \sec \alpha - N_0 \tan \alpha + c{'} \sec \alpha \Big\{ w{'} - \frac{nb}{c{'}} \sin \alpha \Big\}.$$

For a given day W is a maximum or minimum according as $w'-\left(\frac{b}{c'}\sin\alpha\right)n$ is a maximum or minimum. In the particular case in question a typical value of $\frac{b}{c'}\sin\alpha$ is $0\cdot 152$. Theoretically it should be possible, by employing a pantagraph or similar instrument, to trace the quantity $\left(\frac{b}{c'}\sin\alpha\right)n$ beneath the W' record with

the base line of the latter as zero, and so to select and measure the largest and smallest ordinate differences between the two traces. With the apparatus available certain practical difficulties were encountered in endeavouring to trace the N curves reduced to between one-sixth and one-seventh in ordinate, and consequently this method of achieving the object in view was abandoned. Instead, the W' trace for each day was re-examined, in relation to the corresponding N-trace and in the light of the relative effects of changes in w' and n, in order to determine (I) whether the apparent time of maximum or minimum as shown by the W' curve was or was not the true time of maximum or minimum of W for its immediate neighbourhood, and if not what was the true time for that neighbourhood; (2) whether there was in any other section of the W' curve a point which when duly corrected, might possibly compete with the former local maximum or minimum. The true time of maximum or minimum having been thus ascertained, the correct value of W was computed from appropriate measurements made on the W' and N curves. It is considered that the resulting maxima and minima are very nearly of the usual order of accuracy. In nearly all cases the true time of maximum and minimum of W was found to be the same, for all practical purposes, as the apparent time shown on the W'record.

Notes on Tables.

The hourly values of N, W and V, obtained as described above, appear in three of the four monthly tables. The mean value for the day is computed according to the expression

$$x = \{\frac{1}{2} (x_0 + x_{24}) + x_1, + x_2 + \dots + x_{23}\}/24.$$

The letters "Q" and "D" denote the five quiet and the five most disturbed days as selected at De Bilt.

In the fourth table for each month are given :-

- (a) the values and times of the daily maximum and minimum and the values of the absolute daily range for each of the components N, W and V.*
- (b) the value of ΣR^2 † for each day. ΣR^2 is written for $R_N^2 + R_w^2 + R_v^2$ where R_N , R_w , R_v denote the absolute ranges for a calendar day of the north, west and vertical components.
- (c) the "characteristic ratio," ρ , which is the ratio of the value of ΣR^2 for a given day to the mean monthly value of ΣR^2 . This ratio is an index of the degree of disturbance or activity on a given day relatively to the other days of the same month.
- (d) the daily magnetic character figures, assigned according to the international scheme wherein "o," "1," "2," respectively, denote quiet, moderately disturbed and highly disturbed conditions.
- (e) the daily values of temperature in the underground magnetograph chamber.

Mean diurnal inequalities of the components N, W, V, H, D and I on "all" days and on international quiet and disturbed days are given, for the months, seasons and year, in Tables 259 to 276. In calculating diurnal inequalities the non-cyclic change has been eliminated on the assumption that its time-rate is linear. Inequality values are first calculated to 0.01γ and then rounded off to 0.1γ . The inequalities of H, D and I have been computed from those of N, W and V by means of the formulae:—

$$\delta D = \frac{180 \times 60}{\pi} \left(\frac{\delta W \cos D - \delta N \sin D}{H} \right)$$

$$\delta H = \delta N \cos D + \delta W \sin D$$

$$\delta I = \frac{180 \times 60}{\pi} \cos I \left(\frac{\delta V \cos I - \delta H \sin I}{H} \right)$$

in which δD and δI are expressed in minutes of arc, and where H, D and I for any given month are the respective mean values for that month as published in Table 280. The values of the range of the mean diurnal inequalities of the several elements on the three different types of day are brought together in Table 277, and the values of the non-cyclic change of N, W and V are given in Table 278.

The results of harmonic analysis of the monthly, seasonal‡ and annual diurnal inequalities of N, W and V are to be found in Tables 281 and 282, in which are given the values of a_n , b_n , c_n , and α_n , in the two equivalent series Σ (a_n cos 15 nt° + b_n sin 15 nt°) and Σc_n sin (15 nt° + α_n). In the former series t is reckoned in hours from midnight G.M.T., whilst the published values of α_n refer to Local Mean Time. The values of the harmonic coefficients have been computed from the unrounded values of the inequalities and have been corrected, where necessary, on account of the fact that the hourly values are not instantaneous values but are mean values. The factors by which the coefficients have to be multiplied (vide Report of the British Association, 1883, p. 98) are 1.00286 for a_1 , b_1 , c_1 ; 1.01152 for a_2 , b_2 , c_2 ; 1.02617 for a_3 , b_3 , c_3 ; and 1.04720 for a_4 , a_4 , a_5 . Finally, the values were rounded off to 0.1 α_5 .

^{*} See p. 104 for method of obtaining daily maxima and minima of W from 1923; August 30th to December 31st.

[†] See also p. 107.

[‡] The seasons are defined for this purpose as follows:—Winter, January, February, November, December; Equinox, March, April, September, October; Summer, May, June, July, August.

The mean values of the squares of the absolute daily ranges are summarised in Table 279.

In Table 280 appear for the months and year the mean values of N, W, V, D, I, H and Total Force, T. The means of the four latter elements are derived from the corresponding mean values of N, W and V, which are the means of hourly values on "all" days in the month or year.

Review of Results of Magnetic Observations.

Mean and Extreme Values of the Magnetic Elements, 1923.—The mean values are given below in Table I along with the corresponding values for the previous year. The values of N, W and V have been computed from the hourly values derived from the autographic records of "all" days, standardised by means of the absolute observations; those of H, D, I and T have been deduced from the values of N, W and V.

TABLE I.

Year.	н.	D. (West).	I.	N.	w.	v.	T.
1922 1923	γ 16680 16676	6 25·8 16 13·8	69 40·0 69 38·8	γ 15999 16011	γ 4718 4661	γ 45012 44954	γ 48003 47947

H continued to decrease, but less rapidly than in the three immediately preceding years. The increased rate of decrease of westerly declination which became noticeable in 1921 was maintained. The steady fall in W continued, the mean value of this component for 1923 being 650γ less than the value, viz., 5311γ , for 1910. The increase in N was the largest since the rise of 15γ from 1919 to 1920. Inclination decreased, the change from 1922 being larger than is usual from one year to the next. The fall in V from the previous year was somewhat larger than the fall from 1921 to 1922.

The extreme values of N, W and V recorded during 1923 are given in Table II.

TABLE II.

0		Maximu	m.				Minimu	m.			Absolute Annual
Component.	Value.	Da	ate, i	92 3.		Value.	Da	ate, 19)2 3.		Range.
North West Vertical	7 16141 4848 45104	Feb. Mar. Mar.	d 24 24 24	h 21 17 17	m 26 10 21	γ 15749 4443 44724	Sept. Sept. Sept.	d 27 27 27	h I I	m 40 36 46	7 392 405 380

The absolute annual ranges in N and W were greater in 1923 than in 1922, but the range in V was the smallest for the years for which the records are complete. The maximum value of W was almost the same as the 1922 value, recorded about twelve months earlier, although the mean value of W in March, 1923, was less than that in March, 1922, by 54γ .

Magnetic Character of the Year.—As an endeavour to obtain magnetic activity estimates free from the effects of variations in personal judgment, to which the character figures assigned in accordance with the international scheme are subject, it has been the practice in recent years to tabulate for each day two quantities which are in some measure indicative of the degree of magnetic activity. These quantities

are (1) ΣR^2 ,* the sum of the squares of the absolute daily ranges of the three geographical components; and (2), the mean of the hourly values of Σr^2 ,† the sums of the squares of the hourly ranges of these components. The magnetic character

TABLE III.

	1923.					Mear (I	·Value Jnit 100	of $\sum_{\mathbf{r^2}}$					
	-9 - 3.	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
Day. 1 2 3 4 5	••	 0·6 1·2 1·2 2·7 1·5	5·3 1·6 2·9 5·7 1·3	1·6 1·2 1·1	2·0 1·2 1·6 1·8 0·7	0·9 0·8 6·5 3·5 2·3	· 2·0 1·7 3·1 6·2 8·8	2·2 5·4 1·4 1·0 0·8	1·3 2·1 14·1 5·9 1·8	3·4 2·6 5·1 2·0 1·2	1·4 0·6 0·5 0·8 1·3	2·7 16·9 3·3 0·5 0·4	1·2 0·3 — — 0·6
6 7 8 9		 2·5 0·6 0·3 0·6 I·5	2·9 3·2 2·2 0·5 3·7	0·4 2·7 0·6 0·4 0·6	2·0 2·4 3·2 3·6 5·7	1·1 3·4 4·7 2·2 1·1	6·2 1·8 2·3 0·9 0·9	4·8 5·3 2·5 1·4 19·4	4·4 1·5 1·9 1·8 2·2	0·9 0·9 0·8 7·5 4·1	1·7 0·9 2·5 1·4 4·5	0·7 2·7 0·7 0·8 0·4	1·0 0·6 0·5 5·7 2·8
11 12 13 14 15		 0·8 0·7 5·4 2·5 0·8	1·5 0·8 0·6 5·6 0·6	0·8 1·2 1·5 4·8 9·2	10·6 10·3 9·3 6·9 2·5	1·3 0·8 1·4 2·1 2·2	18·5 7·2	8·7 2·9 1·2 0·7 1·1	1·1 2·1 9·7 5·8 3·8	2·7 1·5 2·7 4·3 1·8	6·6 — 3·7 73·1	0·7 6·0 3·1 0·6 0·3	0·8 0·8 1·4 2·5 2·7
16 17 18 19 20		 1·4 0·5 0·2 7·8	2·6 12·8 4·7 1·9 1·3	6·7 4·3 3·8 1·8 3·3	1·4 1·7 1·6 6·1	1·0 33·8 19·8 5·4 6·1	2·8 1·2 1·3 1·7 3·7	1·5 2·2 9·3 3·8 1·8	2·2 1·6 0·8 2·6 1·8	1·2 2·6 3·3 1·0 2·5	111·5 33·2 18·2 6·6 3·8	0·8 0·8 0·3 0·4 0·1	0·3 0·2 1·3 1·0 1·2
21 22 23 24 25		 8·6 6·8 5·6 3·4 0·9	1·1 1·0 0·3 1·0 51·4	2·4 1·4 0·8 104·1 50·1	15·0 19·2 13·9 6·9 1·3	3·2 1·2 2·1 1·1 2·0	9·4 2·0 1·0 1·0	0·8 3·5 7·4 0·8 0·8	1·1 3·4 1·2 3·5 3·3	0·6 1·5 2·6 3·1 1·4	1.0 1.2 0.6 0.5 1.2	1.6 3.2 1.0 0.4 0.5	0·7 0·2 5·3 3·7 5·5
26 27 28 29 30 31		 0·7 0·4 0·6 4·9 7·8 1·8	32·7 52·8 9·8 — —	24·7 7·1 5·7 3·3 3·1 2·4	0·9 — I·7 I·1	1·7 2·0 1·0 12·8 9·3 2·1	1.6 5.0 3.7 1.2 32.0	1·3 3·5 1·9 1·9 1·2 1·2	1·1 1·7 1·2 0·6 1·4 3·5	26·2 247·8 16·0 3·5 3·0	2·1 4·7 0·8 0·7 0·4 4·0	5·0 2·9 6·6 3·7	23·7 7·4 6·2 1·5 0·7 0·8
Mean	١	 2.5	7.6	8.7	4.9	4:5	4.8	3.3	2.9	11.9	10.0	2.3	2.8

figure, the value of ΣR^2 , and the value of ρ^* (the "characteristic ratio") for each day appear in the fourth table under each month in this volume. The daily means of Σr^2 are given in Table III above. Owing to the error; in azimuth of the west

^{*} See p. 105. † r_N , r_W , r_Z , denoting ranges, for the 60-minutes period centered at the exact hour G.M.T., of N, W and V, $\sum r^2$ stands for $r_N^2 + r_W^2 + r_Z^2$. Table III contains the value of $\frac{1}{24} \sum (\sum r^2)$, where—

 $[\]sum (\Sigma r^2) = \frac{1}{2} \left\{ (\Sigma r^2)_0 + (\Sigma r^2)_{24} \right\} + (\Sigma r^2)_1 + \dots + (\Sigma r^2)_{23}$

[‡] See pp. 103-104.

magnet from 1923, August 30th to December 31st, the daily means of Σr^2 for that period are not strictly comparable with the earlier values, for in tabulating hourly ranges of the "west" component during the period specified no attempt was made to allow for the circumstance that the component recorded was $W' = W \cos \alpha + N \sin \alpha$, and not W.

The monthly distribution and the mean values of the magnetic character figures, together with the mean values of ΣR^2 and of Σr^2 , are shown in Table IV.

TABLE IV.

		Magne	tic Character I	Figuces.	Mean	Mean	Mean
Month,		No. of "o" days.	No. of " I" days.	No. of "2" days.	Character Figure.	value of $\Sigma m R^2/100$.	$\begin{array}{c} \text{value} \\ \text{of} \\ \Sigma_{r^2/100}. \end{array}$
1923						γ ²	γ ²
January		21	9	I	0.35	47	2.5
February		16	9	3	0.54	124	7.6
March		18	10	3 3	0.52	*187	*8.7
April	••	17	12	I	0.47	*118	†4·9
May		19	10	2	0.45	104	4.5
June		20	8	2	0.40	†129	‡ 4 ·8
July		22	9	О	0.29	84	3.3
August		21	10	О	0.32	75	2.9
September		21	7 6	2	0.37	204	11.9
October		22	6	3	0.39	198	*10.0
November		18	II	I	0.43	56	*2.3
December		20	10	I	0.39	§ 55	*2.8
Year, 1923		235	III	19	0.41	115	5.5
Year, 1922		174	145	46	0.65	205	11.3
Year, 1921		177	145	43	0.63	255	15.6
Year, 1920		194	137	35	0.57	286	13.9

^{*} Mean for 29 days.

It will be seen that the number of days to which the highest character figure was assigned was much smaller in 1923 than in recent years and that there was a considerable increase in the number of "o" days. The mean character figure and the means of ΣR^2 and of Σr^2 were all considerably less in 1923 than in the years 1917–1922, the annual mean of ΣR^2 being smaller than in any other year since 1914; and the individual monthly means were less than the corresponding values in 1922, with the exception of the mean character figure and mean value of ΣR^2 in December.

A somewhat more detailed representation of the activity features is afforded by the data in Table V, which contains the monthly and annual mean values of ΣR^2 and Σr^2 for days to which different magnetic character figures have been assigned.

In this table the annual means are the means of the monthly mean values—i.e., in the case of "2" days the annual means are the means of the ten monthly means. For international quiet days, "o" days, and "1" days the annual means of ΣR^2 and of Σr^2 for 1923 were quite definitely smaller than in recent years. For these days, too, but with the exception of ΣR^2 for quiet days in April and December, the individual monthly means in 1923 were less than the corresponding values in 1922. In 1923 the annual means of ΣR^2 and Σr^2 on "2" days were somewhat larger than in 1922, but decidedly less than in the years 1918–1921. If equal weight is given to individual "2" days the means of ΣR^2 /100 are 914, 704, 1327, 1683, and of Σr^2 /100 are 53·4, 41·7, 97·3, 92·5 for 1923, 1922, 1921 and 1920

[†] Mean for 28 days.

[‡] Mean for 27 days.

[§] Mean for 30 days.

respectively. Of the nineteen "2" days in 1923, four, viz., March 24th, September 27th, October 15th and 16th, contributed more than 50 per cent. to the totals of ΣR^2 and Σr^2 for the year. The value of ΣR^2 on September 27th, 1923, was greater than on any day in 1922, whilst the values on March 24th and October 16th, 1923, were exceeded on only one day in 1922.

TABLE V.

			TABLE V	·				
	Q d	lays.	"o"	days.	""	days.	"2"	days.
Month.	ΣR ² 100	$\frac{\sum_{\Gamma^2}}{100}$	$\frac{\Sigma R^2}{100}$	$\frac{\sum_{\mathbf{r^2}}}{100}$	$\frac{\Sigma R^2}{100}$	$\frac{\sum_{\Gamma^2}}{100}$	ΣR ³ 100	$\frac{\sum_{\Gamma^2}}{100}$
1923. January February March April	. 16 . 25	γ ² 0·4 0·7 0·6 1·1	γ ² 19 29 41 69	γ ² 1·0 1·3 1·6	γ ² 94 117 114 167	γ ² 5·3 6·0 5·1 7·8	γ ² 218 654 1211 321	γ ² 7·8 45·7 59·7 19·2
May	· 52 · 44	1·1 0·8 1·0	51 70 51 57	1·5 1·9 1·6 1·6	147 163 167 113	5·7 8·6 7·5 5·6	400 569 —	26·8 32·0 —
September	. 23 . 10	1·0 0·5 0·4 0·4	55 38 14 15	2·0 1·5 0·6 0·8	143 152 86 89	5·9 6·9 3·7 4·6	1987 1464 476 456	137·0 72·6 16·9 23·7
Year, 1923 Year, 1922 Year, 1921 Year, 1920	47	0·8 1·5 1·3 1·5	42 64 60 78	1·4 2·5 2·1 2·6	129 221 181 242	6·1 12·5 8·5 11·4	776 720 926 1262	44·1 43·2 61·5 67·5

It may be concluded that in most respects the degree of magnetic activity in 1923, which was apparently a year of sunspot minimum, was distinctly less than in several immediately preceding years; and that if the mean annual value of ΣR^2 be regarded as sufficient criterion, 1923 was the quietest year, magnetically, since 1914 at least.

Table VI.—Mean Diurnal Inequalities of Σr^2 on International Quiet Days for Months and Seasons, 1923. Unit $1\gamma^2$.

Month a Season		ı	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	24-0 (n.c. change).	Mean Value.
January February March	••	+ 42	- 20	_ I	- 41 - 18	- 41 - 36	+ 2 -30	-47 -28	+26 +16	+ 36 + 17	+ 8 +52	+ 40 + 151	- 7 + 42 + 57 + 123	+ 25 + 48	+ 39 + 42	+78	$\frac{-2}{+25}$	-17 -16	-38 - 9	-38 -39	-30 -47	-52 -33	-33 -41	+ 4 -59	-35 -56	- 3 + 2	41 67 65 114
May June July August	••	- 8 - 51	-116 - 32 - 55 - 84	- 58 - 70	- 90 - 60	- 58 - 6	-59 + 7	-17 -53	-27 + 16	+ 26 - 3	+53 + 8	+ 76 +172	+134 +178 +119 +117	+ 20 + 26	+ 70 + 36	+98 +66	+63 + 32	+24 + 5	-24 -15	-49 -16	-42 + 13	$-51 \\ -27$	-44 -35	-47 -47	-7 -56	-36	111 107 84 99
September October November December	••	- 16 + 3	- 39	-32 + 27	- 42 + 15	— 37 — 8	-25 -13	- 8 - 8	-17 +58 +12 -24	+ 57 + 6	+48 + 5	$^{+341}_{+62}$ $^{+21}_{+17}$		十 I7 一 7	+116	+80 + 6 -13 -11	+18 -5	-38	-45 -37	-36 -30	-35 -12	-48 - 2	-27 -18	-10 + 47	-20 + 22	+10 +54	97 53 35 41
Year Winter Equinox Summer	• •	+ 25 - 39	+ 10 - 52	-10 -48	- 21 - 53	- 37 - 61	-15	-33	-3 + 16	+ 5 + 77	+ 6 +46	+ 21 + 191	+ 75 + 18 + 69 + 137	+ 14 + 38	+ 17 + 71	+ 7	-6	-10 -17	-18 -39	-14 -51	O - 54	-1 -35	- I	+24 -17	+19 -42		76 46 82 100

Daily Variation of Σr^2 .—As for the years 1920–1922 attention has been confined to the five international quiet days* of each month and the mean values of Σr^2 have been obtained for the hour periods centred at exact hours G.M.T. The results, in the form of mean diurnal inequalities for the months, seasons and year, are shown in Table VI. The mean values of the difference between the 24h and oh values of Σr^2 are also given.

The mean inequalities for the seasons and year exhibit fewer irregularities in 1923 than in the years 1920–1922, and the range of the mean inequality in winter and in summer was less in 1923 than in either of the former years mentioned. As in the earlier years the winter inequality shows maxima near midnight and noon and minima in the morning and evening. In the inequalities for equinox and summer, 1923, there is a prominent maximum near midday and there are indications of a small maximum near midnight, and minima in the early morning and late evening. The results for these seasons in 1921 and 1922 showed a rather prominent maximum near midnight.

Diurnal Inequalities.—The mean diurnal inequalities for "all" days, international quiet and disturbed days, for the months, seasons and the year, are given in Tables 259–276, and the corresponding inequality ranges in Table 277. The inequalities of N, W and V for international quiet and disturbed days are shown graphically in Plates I and II, the representation in the latter plate being in the form of vector diagrams.

(1) Ranges.

(a) All Days.—The range of the north component inequality for winter and of the west component inequality for equinox was larger than the corresponding quantity in 1922. Apart from these exceptions the ranges for all seasons and for the year, for all components, were the smallest since those of 1914. The ranges for the north component in July, for the west component in July and August, and for the vertical component in April and July were the smallest, for the respective months, of the period 1911–1923.

(b) Quiet Days.—With the exception of the range of the north inequality for the year as a whole and of the range for the vertical component in equinox the ranges for all three components for the seasons and the year were the smallest since those of 1914. The ranges of the north inequality in July, September, October and December, of the west inequality in March and July, and of the vertical inequality in January, February and August were the least, in the respective months, of the period 1911–1923.

(c) Disturbed Days.—With the exception of the west inequality range in summer, the ranges of the inequalities of all three components show a reduction from those of 1922, and in the majority of cases the ranges for the seasons and the year are the smallest during the years 1915–1923. The ranges of the vertical inequality in July, August, November and December, 1923, were noticeably small.

(2) Harmonic Coefficients.

(a) All Days.—Apart from the amplitude of the 12-hour term in winter the amplitudes of the two principal terms for the north and west components were less than in 1922, while for the vertical component the values of c_1 and c_2 for the seasons and for the year were less than in 1922. The values of c_1 and c_2 for the year, for all three components, were the smallest since 1914. The phase of the 24-hour term of each component was slightly less retarded relatively to 1922.

(b) Quiet Days.—The values of c_1 for the north component, of c_1 and c_2 for the west component, and of c_1 and c_2 (with the exception of c_1 in summer) for the vertical component were less than in 1922. The decrease in the values of c_1 and c_2 for seasons and year from 1922 was proportionately greater in the case of the west component than in the case of the north component. The value of α_1 for the north component for summer was greater than usual. For the vertical component α_1 and α_2 were respectively less than and greater than the values in 1922, except in the case of the values for winter.

^{*} The V record was defective on April 27th and therefore this quiet day was omitted.

DIURNAL VARIATION IN THE COMPONENTS OF MAGNETIC FORCE ON QUIET AND DISTURBED DAYS, ESKDALEMUIR 1923. (THE YEAR AND THE SEASONS.)

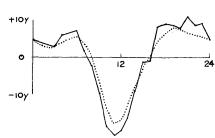
QUIET DAYS Dotted lines

DISTURBED DAYS Continuous lines._

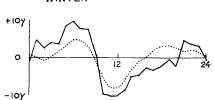
North Component.

Vertical Component.

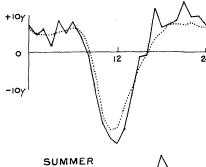


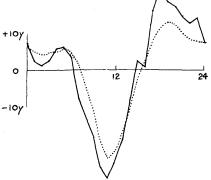




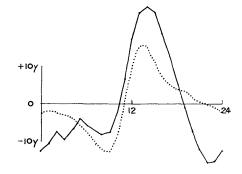


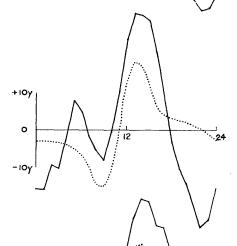
EQUINOX

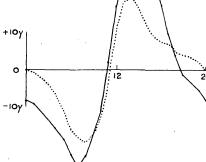




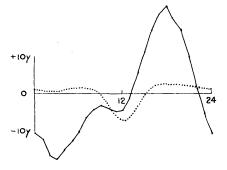
West Component.



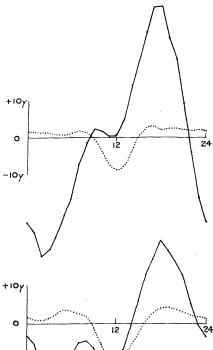


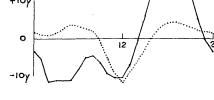


Scales; Force, Imm. = /y.
Time, 2mm. = Ihr.







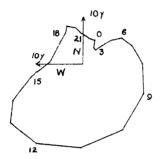


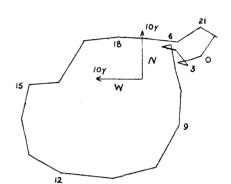
VECTOR DIAGRAMS ILLUSTRATING DIURNAL VARIATION IN MAGNETIC FORCE ON QUIET DAYS AND DISTURBED DAYS. ESKDALEMUIR 1923.

QUIET DAYS.

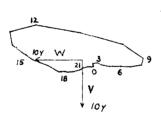
DISTURBED DAYS.

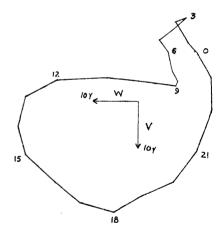
Horizontal Components.



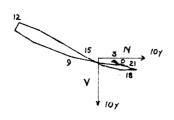


Prime Vertical Components.





Meridian Components.



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Scale, 0.05 ins. = /y.

(c) Disturbed Days.—With the exception of c_2 for the north component in winter, of c_2 for the west component for year, winter and equinox, and of c_2 for the vertical component in equinox, the values of c_1 and c_2 were smaller than in 1922. The values, for the north component, of c_1 and c_2 for year and summer, of c_2 for equinox, and the values, for the west component, of c_1 for year, winter, and summer were the smallest during the period 1916–1923. For the north and west components the values of α_1 and α_2 were less than in 1922, with the exception of α_2 in winter.

Daily Range.—The values of mean absolute daily range for the months and seasons of the year, together with the corresponding means for 1912–1922 (1914–1922 for V), are given in Table VII; the ranges are also expressed as percentages of the mean absolute daily range for the year.

TABLE VII.—ABSOLUTE DAILY RANGE. MEAN MONTHLY VALUES.

		M	lean A	bsolute.	Daily	Rang	ge.	Mea F	n Dai	ily Ra	nge ex Yearl	pressed y Mea	as n.
Month.			1923.			n 1912-	-22 * .		1923.		Mea	n 1912-	-22*.
	N. W. V.				N.	w.	v.	N.	w.	v.	N.	w.	v.
January February March April	ruary 62 59 20 1 70 67 3		ν 17 28 38 31	γ 59 60 87 93	γ 63 67 88 84	7. 34 37 58 58	% 64 107 103 121	% 76 102 119 116	% 61 100 136 111	% 73 74 107 115	% 81 86 113 108	% 69 75 118 118	
May June July August	•••	63 70 59 59	59 68 56 55	33 32 27 23	97 86 85 99	84 82 80 88	60 43 45 61	109 121 102 102	102 117 97 95	118 114 96 82	120 106 105 122	108 105 102 113	122 88 92 125
September October November December	•	70 66 40 40	68 63 44 43	37 40 16 16	93 89 66 58	86 87 67 63	61 59 40 35	121 114 69 69	117 109 76 74	132 143 57 57	115 110 81 72	110 112 86 81	125 120 82 71
Winter Equinox Summer	••	45 67 63	47 67 59	19 37 29	61 90 92	65 86 83	36 59 52	78 116 109	81 116 102	68 132 104	75 111 114	83 110 106	73 120 106
Year	••	58	58	28	81	78	49				_		

^{* 1914-1922} for V.

Whereas in 1922 the mean annual ranges differed but slightly from the means for the years 1911–1921 or 1912–1922 (or for V, 1914–1922), the mean ranges in 1923 were considerably less than the means for the eleven (or nine) year period. The mean ranges in N and in W for the seasons and year were 25 to 30 per cent. less than in 1922, but in V the relative decrease in range was somewhat greater. With the exception of the mean range in N in December, the range in each component was in every month less in 1923 than in 1922. The mean annual ranges in N and W were the smallest since those in 1913, whilst the range in V was the smallest since that in 1914.

On the days January 8th, 19th, November 18th, 20th, 24th, December 17th, 22nd, the daily range in either N or W did not exceed 21γ , and on each day the range in V was either 7 or 8γ .

The frequency distribution of absolute daily ranges recorded in 1923 is shown in Table VIII, which also contains the percentage distribution for the period 1912–1922, or 1914–1922.

TABLE VIII.—FREQUENCY DISTRIBUTION OF ABSOLUTE DAILY RANGE.

		L£	C		Per	centage I	Distribution.		
Range.	Num	ber of 1923.]	N.	,	w.		V.
γ.	Ň.	W.	v.	1923.	1912-22.	1923.	1912-22.	1923.	1914-22
0-9	0	О	41	0.0	0.1	0.0	0.1	11.4	5.2
10–19	19	8	124	5.2	2.8	2.2	1.8	34.5	18.4
20-29	37	40	118	10.1	5.7	11.0	4.9	32.9	23.9
30-39	47	59	32	12.9	7.8	16.2	7.7	8.9	14.8
40-49	76	71	II	20·8	10.1	19.5	11.5	3.1	9.1
50-59	59	57	II	16.2	13.0	15.6	13.1	3.1	5.3
60-69	41	48	2	11.2	13.4	13.2	13.3	0.6	4.8
70 - 79	31	30	4	8.5	9.5	8.2	12.1	I.I	3.2
80-89	15	17	2	4.1	8·o	4.7	7.7	0.6	2.7
9099	8	10	I	2.2	6.3	2.7	6.9	0.3	2.3
100-109	5	3 6	I	1.4	5.3	0.8	4.5	0.3	1.2
110-119	3	6	4	o·8	3.6	1.6	3.2	$I \cdot I$	1.2
120-129	9	2	0	2.5	3.0	0.2	2.6	0.0	0.9
130-139	9 2	3	2	0.5	2.4	o·8	2.0	o·6	0.0
140-149	2	Ī	0	0.2	1.4	0.3	2.2	0.0	0.6
150-159	4	· I	o	1.1	1.2	0.3	1.1	0.0	0.7
160-169	I	2	0	0.3	1.1	0.2	0.8	0.0	0.5
170–179	0	0	I	0.0	0.8	0.0	1.0	0.3	0.4
180189	О	1	o	0.0	0.7	0.3	0.6	0.0	0.5
190–199	ı	I	0	0.3	0.5	0.3	0.6	0.0	0.3
200+	5	5	5 6	1.4	3.6	1.4	2.4	1.4	2.9
ays omitted	o	o	6			_			_

TABLE IX.—PRINCIPAL MAGNETIC DISTURBANCES RECORDED AT ESKDALEMUIR, 1923.

Where the beginning of a disturbance has been marked by a "sudden commencement," the serial number is followed by an asterisk (*), and the time entered in the second column is that of the sudden commencement, estimated to the nearest minute. In other cases, the exact hour nearest the time at which disturbance may be regarded as having begun is entered in the second column. To the tabulated values of maximum and minimum the following have to be added:— N, 15000 γ ; W, 4000 γ ; V, 44000 γ .

				North	Compo	nent.			West	Compo	onent.			Vertic	al Comp	onent.	
No.	From	To.	Max.	Time.	Min.	Time.	Range	Max.	Time.	Min.	Time.	Range	Max.	Time.	Min.	Time.	Range
1 2 3 4 5 6 7* 8* 9 10	d h m Feb. 24 22 Feb. 27 6 Mar. 24 9 Apr. 20 0 May 16 21 16 May 29 10 June 3 19 10 June 12 20 28 June 30 6 July 9 14	d h Feb. 26 6 Feb. 28 2 Mar. 27 8 Apr. 24 6 May 19 8 May 31 4 June 5 20 June 15 8 July 1 8 July 12 6	7 1093 1090 1141 1074 1102 1084 1051 1091 1119 1083	d h m 25 21 41 27 22 23 24 21 26 22 18 50 17 18 12 30 17 2 4 22 46 14 18 18 30 17 28 11 18 58	934 896 944 938 963 955 932 964 946	d h m 26 o 6 27 20 9 25 2 33 22 11 30 18 1 41 30 11 14 5 11 30 13 2 55 30 18 3 10 11 43	7 203 156 245 130 164 121 96 159 155 137	7 726 710 848 719 730 726 709 732 791 728	d h m 25 21 21 27 12 59 24 17 10 21 14 22 17 14 38 29 14 28 5 4 34 13 14 35 30 17 33 10 13 42	7 592 570 479 610 598 607 624 573 624 622	d h m 25 23 14 27 20 17 24 21 26 {21 3 28 23 1 42 17 18 6 29 21 3 5 7 18 13 2 20 30 9 3 11 1 10	7 134 140 369 109 132 119 85 149 167 106	996 1004 1104 978 1027 993 957 989 1079 997	d h m 25 21 8 27 18 31 24 17 21 20 19 18 17 18 6 \$\begin{cases} 29 18 30 \\ 30 16 51 \\ 5 18 47 \\ 13 17 0 \\ 30 18 3 \\ 10 20 10 \end{cases}	914 937	d h m 26 2 26 27 23 10 25 3 24 22 24 0 18 1 55 29 12 0 5 5 8 14 2 5 30 11 43 10 2 20	7 150 96 292 86 179 75 56 75† 132 60
11 12 13* 14 15	July 22 21 26 Aug. 2 23 Aug. 12 21 2 Sept. 26 3 Oct. 14 21 Nov. 2 0 Dec. 25 12	July 23 24 Aug. 4 12 Aug. 14 8 Sept. 28 6 Oct. 17 10 Nov. 3 8 Dec. 27 6	1087 1066 1081 1097 1110	22 23 59 3 1 31 13 20 14 27 2 20 15 19 40 2 21 22 26 20 51	986 941 990 749 809 941 936	23 12 0 3 10 52 13 9 59 27 1 40 16 23 40 2 9 48 26 13 50	101 125 91 348 301 141 154	697 699 698 745 732 728 666	23 13 50 3 12 24 13 13 28 27 22 16 15 15 20 2 6 55 26 2 14	580 614 615 443 473 564 530	23 2 51 4 6 59 13 21 22 27 1 36 16 22 3 2 21 48 26 20 36	117 85 83 302 259 164 136	991 1002 993 1067 1063 973 982	23 17 30 3 20 12 13 21 14 27 17 35 15 16 28 2 16 38 26 17 0	933 941 963 724 770 931 920	23 5 32 4 4 50 14 5 30 27 1 46 16 23 42 3 1 40 27 1 14	

[†] During this disturbance the vertical component record was defective until June 13d 11h.

For both horizontal components the interval of maximum frequency was $40-49\gamma$, and in each case the range on 50 per cent. of the days fell within the interval $30-59\gamma$. Thus the range interval of maximum frequency was definitely smaller than in 1922, and the scatter of distribution was decidedly less. Rather more than one-third of the V ranges fell within the interval $10-19\gamma$, and only slightly more than 20 per cent. of the ranges in this component exceeded 29γ , the distribution of V ranges being somewhat similar to that in 1914. In 1923 there were 11 days on which the range of a horizontal component was 160γ or more; the numbers of such days in 1919, 1920, 1921, 1922, were 55, 36, 27, 32 respectively.

Principal Magnetic Storms during 1923.—Particulars of the principal magnetic storms recorded during the year are given in Table IX. The magnetograms for the most highly disturbed days are not reproduced in this volume, but photographic copies may be obtained on application to the Director, Meteorological Office, Air Ministry, Kingsway, London, W.C.2.

Remarks on the Autographic records for Terrestrial Magnetism, 1923.

January.—The month was one of the quietest of the year, and there was no outstanding disturbance. In the moderate disturbance of the 13th and 14th the largest changes occurred in W. After two of the quietest days of the month a small preliminary movement at 20d 3h 4m appears to have initiated the largest disturbance, which continued throughout the 20th and 21st. Moderately large changes in N occurred between 22h and 24h on the 20th and near 24h on the 21st; and in W between 22h on the 20th and 3h on the 21st. The degree of disturbance on 22nd and 23rd was above the average for the month. After three or four very quiet days moderate disturbance ensued on the 29th and 30th. Short period pulsations of small amplitude and a few minutes period occurred in N and W as follows:—near 6d 20h; near 8d 1h; shortly before 11d 2h; between 16d 21h and 16d 22h; and between 17d 22h and 18d 1h. A smooth bay-shaped movement in W, in which the component attained a value of about 25 γ above the undisturbed, was centred at 10d 4h 12m.

February.—During this month conditions were generally more disturbed. In a bay-shaped movement between 18h 30m and 19h 40m on the 1st W fell to a value more than 50γ below the undisturbed. Associated with this were an irregular wave movement (range 59γ) in N and a small flat peak in V. Somewhat similar associated movements, but in which a wave is superposed on the W bay, occurred between 18h and 20h on the 2nd, between 20h and 22h on the 6th, and between 20h and 24h on the 14th. During otherwise moderate disturbance on the 17th there was a prominent peak in N, centred at 19h 30m, N being then about 96γ in excess of the undisturbed value.

The last days of the month were marked by fairly considerable disturbance. The storm which began gradually after 24d 22h reached its maximum development between 25d 14h and 26d 4h. In N and W a double oscillation of some magnitude occurred between 20h and 22h on the 25th, the ranges in this interval being N, 1417; W, 1007. In V there were no particularly rapid changes; a rounded maximum at 25d 16h 50m, followed by a relatively quiet period, was repeated by another at 20h 25m and at 21h 8m by a sharp peak maximum of about the same magnitude as The fall from the peak was sharp at first but was interrupted by the two former. two periods of partial recovery, the minimum value being reached at 26d 2h 26m. During the greater part of the 26th conditions were much less generally disturbed, but the following associated movements may be noted:—N increased by 1017 between 20h 29m and 20h 36m, and decreased to approximately the undisturbed value at 21h 5m; W fell sharply 48 y between 20h 27m and 20h 32m and then in the ensuing four minutes increased by 40γ ; V decreased sharply by about 10γ between 20h 32m and 20h 36m. There was fresh onset of disturbance on the 27th, and between 18h and 23h on that day several prominent oscillatory movements occurred in N

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and W. In V the main features of the larger movements bear a considerable resemblance to those on the 25th–26th, although the range was smaller and corresponding phases occurred earlier, the minimum being reached at 23h 10m. Moderate disturbance continued on the 28th. V reached a not very prominent maximum at 17h 45m which coincided approximately with the culmination of a bay movement in W in which that element fell about 85γ below the undisturbed value. A wave movement occurred in N between 17h and 18h 30m, the range being 73γ.

March.—Mainly quiet conditions prevailed during the period 1st to 13th. Disturbance of moderate character occurred from the 14th to the 17th. Somewhat conspicuous bays in which W fell below the undisturbed value were centred at 18d 21h 50m and 20d 21h 5m.

A storm of considerable intensity began about 24d 9h, and therefore approximately 27 days after the first of the disturbances at the end of February. The maximum activity was developed between 24d 16h and 25d 6h*. Between 17h and 18h 30m and between 21h 20m and 23h prominent oscillatory movements occurred in N and W. In the former period the ranges in N and W were 1277 and 262γ. Between 21h 20m and 21h 26m N increased rapidly by 163γ, reaching its maximum value at the latter time, and then between 21h 37m and 21h 46m decreased by 175γ. During the six minutes commencing at 21h 20m W decreased by 133γ and then in the ensuing six minutes increased by 150%. W was below the normal value from 24d 18h to 25d 6h. V increased after 12h on the 24th and reached a sharp maximum at 17h 21m. In the next five minutes a decrease of 62 γ occurred and was followed immediately by oscillations, of diminishing amplitude, which continued until nearly 19h. V then decreased gradually by about 90 until shortly after 21h when there was an irregular rise of about 437 to a sharp peaked secondary maximum at 21h 26m or 27m. In the ensuing 19 minutes V decreased by 141γ. This was followed by an irregular partial recovery, lasting until 25d oh 40m, after which there occurred a further fall of 118γ in an hour, and after another temporary recovery the minimum value was reached at 25d 3h 25m. The subsequent recovery was fairly rapid at first but then more gradual. The ranges during this storm were N, 245 γ ; W, 369 γ ; V, 292 γ . Conditions continued to be disturbed on the 25th, 26th, 27th, the degree of disturbance being greater during the third than in the second 24-hour period following the beginning of the storm.

The following associated movements took place shortly after oh on the 31st in an otherwise fairly quiet period:—N increased by 33γ between oh 23m and oh 28m, remained fairly steady until 45m and then gradually decreased, reaching its undisturbed value at 1h 15m; W increased by 37γ between oh 21m and oh 30m and then gradually decreased to the undisturbed value at 1h 15m; V fell gradually by 18γ between oh 23m and 1h om, and then rose very slowly. The initial rise in N and in W was accompanied by small short period pulsations.

April.—The early days were comparatively quiet, the 5th being one of the quietest of the month. Moderately large disturbance occurred late on the 10th. There was short period agitation between 10h and 14h on the 11th which was followed by larger disturbance later that day and during the 12th, the most noticeable changes occurring between 22h and 24h on the 11th and between 16h and 22h on the 12th. Further fairly large disturbance occurred between 13d 21h and 14d 4h; between 0h 33m and 0h 55m on the 14th. N increased by 62γ and W decreased by 75γ between 22h 7m and 22h 37m on the 13th. After four quiet days disturbed conditions developed during the 20th and continued until the 24th, most activity being shown during the latter part of the 22nd and the early hours of the 23rd. Between 20h and 21h on the 24th a bay movement in W, in which W fell below the undisturbed value, was associated with a wave in N and a small flat peak in V, movements similar to those between 18h and 19h on February 25th. Apart from comparatively slight

^{*} On March 24th auroral displays were witnessed from the Hebrides, Fifeshire, Cumberland, and from the vicinity of Eskdalemuir.

disturbance near 22h on the 29th, conditions were quiet on the remaining days of the month. Small oscillations of a few minutes period are in evidence on the N and W records on several occasions during the month.

May.—After two quiet days disturbance of a moderate character developed on the 3rd. Between 3d 22h 35m and 3d 22h 46m there occurred in N a fairly sharp rise (on which were superposed small oscillations) amounting to 49 γ . This was followed by an irregular fall, of 82 γ , which continued until 23h 50m. There were periods of moderate disturbance on the 4th, 5th, 7th and 8th, but the succeeding four days were quiet.

The largest disturbance of the month was apparently initiated by a small movement, with some of the characteristics of a "sudden commencement," which occurred at 16d 21h 16m. The intervals of greatest activity were between 17d 13h and 18d 6h. It is of interest to note that there is an approximately 27-day interval between this disturbance and that which developed during April 20th. The largest movements in N and W occurred between 17d 13h and 17d 19h, and between 17d 21h and 18d 4h. The maximum value of N occurred in a sharp peak at 17d 18h 13m and the minimum value of W at 17d 18h 9m. N reached its minimum at 18d 1h 43m. In V there was a fairly sharp but not very high maximum at 17d 18h 6m and this was followed by a somewhat irregular fall to a minimum at 18d 1h 56m. The ranges during this disturbance were:—N, 182 γ ; W, 131 γ ; V, 176 γ . Somewhat disturbed conditions continued on the 18th, 19th and 20th. Small peak movements in N shortly after 18h and between 20h and 21h on the 18th resemble on a smaller scale those which occurred at approximately the same times on the 17th.

The period 22nd to 27th was quiet.

The second and smaller of the two largest disturbances of the month began at about 10h on the 29th and continued throughout that day and the following.

June.—A small and rather slow "sudden commencement" at 3d 19h 10m was followed by comparatively slight disturbance, which continued until about 5d 20h. Bay-shape movements in N and V, in which both elements fell below the undisturbed value, occurred between 3h and 5h and between 4h and 7h, respectively, on the 5th. Comparatively moderate disturbance occurred after 10h on the 6th. Conditions were quiet on the 9th and 10th.

A rather large disturbance* began with a not particularly sharp "sudden commencement" at 12d 20h 28m, and therefore 27 days after the small movement which apparently marked the beginning of the disturbance of May 17th. N and W remained above the undisturbed value for rather more than three hours after the "sudden commencement." Both N and W reached a minimum between 2h and 3h on the 13th. The interval between 3h and 11h on the 13th was marked by considerable short period fluctuations in N and W. Disturbance continued throughout the 13th and 14th, but was less on the latter day. A prominent rounded maximum in N occurred at 14d 18h 18m.

The period 16th-20th was comparatively quiet; but disturbance of a moderate character ensued on the 21st and 22nd. Quiet conditions prevailed again during the 23rd to 25th, but were followed by moderate disturbance on the 27th and 28th.

The second of the larger disturbances of the month commenced gradually shortly before 6h on the 30th. In N and W greatest activity occurred between 14h and 19h. Oscillations in N culminated in a maximum at 17h 28m, which was followed by a minimum at 18h 3m, the range between the two extreme values being 155 γ . W reached its maximum at 17h 33m; this was followed by a fall of about 55 γ in the ensuing ten minutes and between 17h 54m and 18h 4m by a sharp fall of 85 γ . The rise in V, which began at 12h and terminated in a fairly sharp maximum at 18h 3m, was accompanied by oscillations of increasing magnitude. From 18h 3m V decreased gradually, but there was no prominent minimum.

^{*} There was no V record of this disturbance until 13d 10h.

July.—A small disturbance commenced with small pulsatory movements in N and W at 1d 21h 22m and continued until about 2d 23h. The curves were moderately disturbed on the 6th and 7th, and during the afternoon of the 8th.

What was apparently another of the series of disturbances separated by intervals of about 27 days developed gradually after 9d 14h. The first prominent changes were bay-shape movements centred near 10d 2h and in the course of which N rose above, and W and V fell below, the undisturbed value; the early stages of the bay in N and W were accompanied and preceded by small short period pulsations. After a comparatively quiet interval disturbance became general from 10d 10h until 11d 6h. There was further disturbance, but of less intensity, from 11d 11h to 12d 4h.

Short period pulsations in N, and to a less degree in W, were in evidence almost continuously from 9h to 18h on the 13th.

The moderate disturbance on the 18th appears to have been initiated by a series of small short period pulsations in N and W between 21h and 22h on the 17th.

A movement, at 22d 21h 26m, which may be described as a doubtful "sudden commencement," was followed by comparatively moderate disturbance, which subsided by midnight on the 23rd.

In addition to the occasions already noted short period pulsations in one or both of the horizontal components occurred as follows:—Near 4d 9h; near 7d 13h and 7d 21h; near 11d 19h; near 15d 20h; near 16d 22h; near 18d 23h; between 21d 17h and 21h; near 24d 2h; between 27d 22h and 24h; near 30d 20h; between 31d 2h and 3h, and between 31d 21h and 24h.

August.—As in the preceding month, general magnetic activity was low. The largest disturbance commenced shortly before midnight on the 2nd and continued until the 4th, but exhibited no very conspicuous features. A "sudden commencement" occurred at 12d 21h 2m and was followed on the next day by disturbance of a very moderate character. A somewhat sharp rise of 9γ in V, between 13d 20h 25m and 20h 30m, was accompanied by falls of 67γ and 27γ in N and W respectively. A double oscillation or wave occurred between 0h and 2h 30m on the 31st.

Short period pulsations occurred in N or W or both N and W at or near the following times:—2d 2h; 5d 18h and 24h; 6d 2h; 7d 13h and 14h; 8d 20h; 9d 24h; 11d 2h; 12d 22h; 16d 20h; 18d 11h to 16h; 19d 22h to 24h; 21d 23h; 22d 23h; 31d oh to 2h.

September.—Conditions were mainly quiet until near the end of the month.

The storm which began about 3h on the 26th and continued for rather more than 48 hours, was in some respects the largest of the year. In N the largest changes occurred during two or three conspicuous wave movements between 1h and 6h on the 27th. This component reached a sharp minimum, 267 γ below the mean value for the month, at 1h 40m and then increased by 348 γ in the ensuing 40 minutes. W was considerably below the undisturbed value from 26d 21h to 27d 3h and again during the greater part of the interval 27d 18h–24h. The evening maximum in V on the 26th was only about 25 or 30 γ in excess of the undisturbed value. After 21h on the 26th V decreased with but one interruption to a sharp minimum at 27d 1h 46m. The subsequent recovery was irregular until 5h 30m, but then more rapid and smooth. The maximum in V occurred at 27d 17h 35m. A secondary minimum in V occurred at 27d 22h 30m and was preceded between 22h 0m and 22h 20m by a fall of 138 γ .

October.—Apart from very moderate disturbance on the 10th and 11th, conditions were quiet during the first half of the month.

One of the principal disturbances of the year began somewhat abruptly shortly after 21h on the 14th and continued until about 10h on the 17th. In the horizontal components the periods of greatest activity were from 15d 12h to 16d 4h and from 16d 12h to 17d 6h. N was mainly below normal from 8h to 23h on the 15th and from 10h on the 16th to 10h on the 17h. The defect of W from the normal value was most

marked during the interval 16d 17h to 17d 2h. For about 10 hours after the commencement of the storm V was slightly below normal, and then rose to a maximum at 15d 16h 28m. A minimum at 15d 23h 23m was followed by an irregular rise to a second maximum, only slightly less than that on the 15th, at 16d 16h 44m. This was followed by an irregular fall to the principal minimum at 16d 23h 42m. In the ensuing 18 minutes there was a rise of about 38γ but in the next four hours the recovery was very slow. The absolute ranges of the components during the storm were N, 301γ ; W, 259γ ; V, 293γ .

The latter part of the 17th and the 18th were moderately disturbed. A rather prominent bay-movement in N was centred at 27d 8h 30m.

November.—In some respects this was the quietest month of the year. Conditions were particularly quiet on the 18th and 20th. The character figure 2 was assigned to only one day, viz., 2nd. On that day fairly considerable disturbance between 6h and 11h was followed by a calm interval of some hours duration, but shortly before 21h there was a fresh onset of disturbance which did not subside until about 6h on the 3rd. There was disturbance of moderate character on the 12th and also, but to a less degree, during the evening hours of the 13th. A very slight disturbance, of short duration, in which N and W were mainly in excess of their undisturbed values, began abruptly shortly after 15h on the 21st and ceased abruptly about five hours later. The moderate disturbance between 22d 16h and 23d 3h was most developed in W. Conditions were moderately disturbed on 27th–30th. A fairly prominent peak in N centred at 29d 22h 43m was apparently repeated in a similar but smaller movement at 30d 20h 50m.

December.—This also was a quiet month, the highest magnetic character figure being assigned to only one day, viz., the 26th. The 17th and 22nd were very quiet days. The run of the curves during a moderate disturbance between 9d 15h and 10d 3h is somewhat similar to that during the interval November 22d 16h to 23d 3h. Fairly prominent movements in which N rose above the undisturbed value, in otherwise quiet or only slightly disturbed conditions, occurred near 1h and 24h on the 15th and near 22h on the 20th.

There was an apparently isolated period of disturbance between 18h and 22h on the 23rd; N and W being below and V above the respective undisturbed values. In this interval N fell to a value about 53 γ below the undisturbed value, W about 88 γ below the 18h value, and V rose 26 γ above the 18h value. Disturbance increased during the 24th and 25th, reached its maximum on the 26th, and subsided by the 29th.

SEISMOLOGY.

Notes on Instruments.—As in previous years the instruments in use were three Galitzin pendulums, with galvanometric registration, arranged to record earth displacements in the north, east and vertical directions. The installation is situated in ground floor rooms of the principal building of the Observatory, the pendulums being placed on massive concrete pillars which extend down to boulder clay and are independent of the floor.

For detailed descriptions of the Galitzin seismographs and for particulars of the interpretation of the records, reference may be made to Vorlesungen über Seismometrie by the late Prince B. Galitzin, to Modern Seismology by the late G. W. Walker, or to Dictionary of Applied Physics, Vol. III.

No determination of the constants of the instruments was made in 1923, but it is considered that no serious error has been introduced by using the values found in 1915 and 1916 (see *British Meteorological and Magnetic Year Book*, 1915). It may be stated that the Galitzin vertical pendulum is particularly sensitive to temperature changes, and as the temperature variation in the room is fairly considerable frequent adjustments of the pendulum are necessary. For this reason the records

from this instrument are regarded as only qualitative in certain respects. At the same time it must be noted that the vertical record is an important factor in the determination of an epicentre from the records of an earthquake at a single station.

The situation of the Observatory is such that the effect of wind produces undesirably large disturbances on the records, and on occasions the reading of an earthquake record is rendered quite impossible by the large and more or less irregular but persistent wind disturbance.

During 1923 the clockwork recording drums gave considerable trouble and in consequence of this several records were lost or spoiled.

Notes on Tables:—Earthquakes.—The Earthquake Diary, Table 283, contains the particulars of the earthquakes recorded by the Galitzin instruments. The notation employed is as follows:—

P is the time of arrival of the first phase (longitudinal waves). S is the time of arrival of the second phase (transverse waves). L is the time of arrival of the long waves (surface waves).

 PR_1 , PR_2 ... are longitudinal waves reflected once, twice... at the earth's surface, prior to their arrival at the station. SR_1 , SR_2 ... similarly denote reflected transverse waves. Any times given for reflected waves refer to the beginning of the disturbance at the observatory.

 M_1 , M_2 . . . are the times of successive maxima of the displacement of the ground, corrected, if necessary, for the lag of the instrument.

i is the sudden commencement of a phase. iP means a sudden commencement of the P phase. e means an indistinct commencement of a phase. F is the end.

T, the period in seconds, is the duration of a double oscillation (to-and-fro movement). μ represents a micron (0.001 mm.).

 Δ is the distance in kilometres of the epicentre measured along the arc of the great circle passing through the station. α is the azimuth of the epicentre (o° to 360°) measured from north through east. The distance is estimated from Klotz's Seismological Tables (Publication of the Dominion Observatory, Ottawa, Vol. III, No. 2), which are also used for computing the time at which the disturbance originated. This time of origination is denoted by the letter O.

 A_x , A_z are the amplitudes of the components of the true displacement of the ground from the position of rest, and are measured in microns. When the displacement shown by the north-south seismograph is to the north a + sign is shown; for a displacement to the south a - sign is used. Similarly + is used for displacement to the east, - for displacements to the west. When the oscillations are of a simple harmonic character no sign is prefixed to the amplitude. (For reasons mentioned in the foregoing, values of A_z are not given.)

The suffixes N, E, Z indicate that the estimates refer to the records from the north-south, east-west and vertical seismographs respectively.

Microseisms.—Microseisms are the small and often extremely regular tremors which are practically always in evidence on the seismograph records. The periods range to something more than 8 seconds, and the larger periods are generally associated with larger amplitude. At Eskdalemuir the amplitudes are usually confined to the range 0 to 8µ. These minute tremors attain their greatest development in the winter months, and on occasion render the interpretation of earthquake records exceedingly difficult and sometimes impossible. Microseisms of the type referred to are believed to arise from other than purely local causes, but the precise nature of their origin remains in doubt. Although their period corresponds with that of sea waves there is evidence that the breaking of the latter on coasts does not afford a complete and satisfactory explanation of the known facts with regard to microseismic movement. There is evidence of a relationship between the travel of cyclonic disturbances in eastern seas and microseismic movement in China and Japan*, and evidence of a somewhat similar nature has been adduced in favour of a connection between microseismic movement and atmospheric pressure gradient in Europe and Canada.

In Table 284 are given the amplitude and period of the microseisms shown by the North component Galitzin seismograph on each day at oh, 6h, 12h and 18h G.M.T. The group of waves of greatest amplitude occurring in the 30 minutes centering at the hour in question is selected, and the amplitude tabulated is the mean obtained from two or three waves in that group. The period is derived from a measurement made in the same group.

In computing the mean period occasions of zero amplitude are omitted. For reasons already mentioned there were no records on a number of days.

The mean values of amplitude and period for each month of 1923 and for the year. together with the means for the years 1911-1922, are given below.

M	icros	SEISM	s. N	MONT	HLY	AND	Anni	UAL	MEAN	s.		
	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Ī

	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	Year
1923 $\left\{ \begin{array}{l} \text{Amplitude } (\mu) \dots \\ \text{Period (secs.)} \end{array} \right.$	2·6 6·2	2·9 6·5	1·4 6·1	1·3 5·4	0·7 4·9	o·6 4·8	0·3 4·4	0·7 4·8	0·9 5·8	1·5 5·1	1·6 5·1	2·1 5·7	1·4 5·4
1911 $\left\{ \begin{array}{l} \text{Amplitude } (\mu) \dots \\ \text{1922} \end{array} \right\}$ Period (secs.)	1		1	Ì		1		ļ.	į	i			

^{*} Mean for II years only.

The occasions of the largest microseismic amplitude in 1923 were:—January 9th–1oth (6 to 7μ); January 19th–21st (7μ); February 6th–9th (6 to 7μ); February 26th–27th (6 to 7μ); October 8th–1oth (5 to 6μ). The following notes on the changes in amplitude during those occasions and on the associated meteorological changes may be of interest and exemplify the difficulties encountered in seeking to determine the primary cause of microseisms:—

January 9th-10th.—The increase in amplitude was very noticeable after 9h on 9th. The maximum amplitude occurred between 9d 18h and 10d oh. The amplitude decreased during the 10th. During the 9th a depression with a well-defined centre moved eastwards from south of Iceland. The centre passed the extreme north of Britain about 10d 1h. On the western coasts there were high westerly winds, becoming north-westerly on the 10th. There was a general, but not very marked, increase in sea disturbance at most places on the coast between 9d 7h and od 18h.

At Strasbourg the largest amplitude occurred at od 18h.

January 19th-21st.—Microseismic amplitude increased rapidly between 18h and midnight on the 19th, reaching 7 at the latter time. The amplitude remained high throughout the 20th and diminished during the 21st. In the early part of the 19th, the British Isles were under the joint influence of an anticyclone to the south-west and of the southerly extension of a deep depression between Greenland and Scandinavia. Later on the 19th, a cold north-westerly air current invaded the northern and eastern districts of the British Isles, the wind on the western coasts reaching gale force in places on the 20th. Later on that day the wind force abated. The direction became westerly on the 21st. At most coastal stations sea disturbance increased during the 19th but diminished in the north and west during the 20th.

At Strasbourg the largest amplitude during this period occurred at 12h on 20th, and there were further large amplitudes (5 to 6µ) on 21st and 22nd. According to one school of thought, the large values on 21st and 22nd might be attributed to the influence of a well-developed depression centred near Sardinia on those days.

February 6th-9th.—The amplitude of microseisms increased during the early hours of the 6th and again on the 7th, remaining high during the greater part of that day and on the 8th and 9th. The largest amplitudes measured occurred near 7d 12h, 8d 18h, and 9d oh. Throughout the 6th and 7th a large depression situated over the Atlantic influenced the British Isles and Western Europe. The wind was mainly

southerly, being high or gale force in many places. The influence of the large depression was apparently less direct on the 8th, but on that day and the following, secondary depressions developed over the British Isles and neighbouring continental districts, the wind speed being generally considerably less than on the 7th, save in the Shetland Isles. At 8d 18h and 9d 7h sea disturbance on British coasts was less generally than on the 7th. This point is of some interest, for high microseismic amplitudes were recorded during the later hours of the 8th and early hours of the 9th.

At Strasbourg the largest amplitudes occurred at 8d oh and 8d 18h.

February 26th-27th.—The amplitude of microseisms increased gradually during the 26th and reached a maximum in the early hours of the 27th. The general activity of the microseisms was less than on the two occasions noted in January. On the 26th a very deep depression moved eastward from the Atlantic to Ireland. The centre remained over the British Isles during 27th and 28th but the depression became gradually less intense. High winds and gales occurred off the British and French coasts. At most parts of the British coast sea disturbance increased between 7h and 18h on 26th.

This occasion was marked by a notable development of microseisms at Strasbourg. The amplitude (north component) increased during the 26th from 2μ to 13μ , and values in excess of 10μ were recorded throughout the 27th.

October 8th—10th.—Owing to failure of time marks, values of the amplitude are not given in Table 270 from 8d 6h to 9d 6h, but it may be stated that the amplitude increased fairly rapidly from 9d 6h, the largest values being recorded between 9d 9h and 9d 15h. During the night of the 8th—9th a depression moved eastwards from south of Iceland and increased in intensity. At 9d 7h the centre was near Faröe Islands, and by 18h on that day the centre was approaching Norway. Throughout the 9th high winds or gales, from west to north-west, prevailed over the western and northern parts of Britain.

At Strasbourg the amplitude of microseisms increased during the 9th and decreased during the 10th, the largest values occurring between midday and midnight on the 9th.

Readings in millihars at exact hours

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	11	974.2	974.6	975.2	975.8	975.8	976.5	977.2	977.6	978.1	978.1	978.1	978.4	978.0	978.3	979.2	979.9	981.6	082.5	083.6	084.4	085.0	085.4	086.2	086.4	7070
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	29 30	984.7	907.5	985.8	986.0	1904.0	984·0 986·8	986.0	984.0	087.0	088.0	088.	088.2	1983.0	082.4	982.2	982.2	982	982.6	982.8	983.0	983.4	1 983.7	7 984	984	3 984
	_		1	1	1	1	I	ţ		1	Į.	1		1	i		1	1	!	1	1		1		1	1
an	31	1		986			987·4 986		·		987.2	-		l	984.2	-	982.8	-	- 	·	-		-	-	-	
	n level)	19	-06	90	·61	•47	.37	.59	-oc	:29	52	: 51	.27	•01	1 83	·8g	99	18	24	987	5:50	987 3 ·63	3 .5	987	7 :40	987
a le	vel)	•47	.32	1010	1013	.73	1015 ·63	.85	1010	.57	1010	1010	.42	1010	1015	1010										
2.	Eskda	iemu	ir :	H _b =	₌237·	3 me	etres.																E.	h	4 <i>1</i>	102
小		mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	ı mb.	ı mb.	mb.	l mb.	ı mb.	l mb.	⊥mb.	ı mb	ımb	ımb	1 mh	Lmb	l mb	ımb	y, 19	1
	I	197919	1900-4	1900-0	901.2	1900.9	11900.4	900'2	900	1900.3	1979 7	1979:1	1978.0	1978 1	[[Q78 *0	0.077.7	077.4	1076.	1075.1	1072.0	1072.2	0.77	070.4	1060.6	1060.	
	2 3	19/0.2	9/1/	19/3 4	9/4 0	19/5 0	976·7 976·4	19/70	4700	1979.2	4774.0	11000.2	1140015	4000°	איס7סוו	ผดชดาด	$0.000 \cdot 4$	1070.0	いいての・と	(IO7X · C	コロケス・5	1077.5	1077.0	1076.	1076.	- 1000
	4	1900.4	901 4	1904 0	19033	1904 1	1905.3	1905.0	1900	1907.0	1400.7	1400.4	uuoora	10000:0	NONN C	איאאטוו	K-KKON		$(\alpha \times \alpha \times a)$	$\square \cap XX \cdot c$	ハヘスス・と	∩XX+1</td <td>1087.6</td> <td>1087.0</td> <td>1086.</td> <td>$-1 \sim 26$</td>	1087.6	1087.0	1086.	$-1 \sim 26$
l	5	986.3	985.3	984.4	982.5	982.1	981.3	980.3	979.6	979.9	979.6	979	978.4	977	976.7	976.6	977.0	976.7	975.7	975.2	975.0	974.5	973.9	973.2	972	978
	6	1	l	1	1		965.5	1	1			!	1		1	1	1	1		1	1	l.	1	l .		
1	7	1939 4	19.79 /	1900 1	1939 3	1909 0	1950	1907.0	470 1	1454.4	1451.0	1145014	แนนนาบ	1040.1	IOVO.1	איאאטו	IOAO T	10.40.2	$0.010 \cdot 0$	100000	COSTIC	OFT .T	1050.0	1050.6	10404	210 - 1
1		1949 4	1940 4	1947	1943 9	1943 3	119 44 4	1945 4	944	1943 4	1944 'C	1940.0	1947.0	1940.0	DIQAQ C	1105T-4	1053 2	1051 ·t	りのちん・エ	1057.2	1050.2	1060.2	INDT 1	1062.2	1062.4	iloso
	9 10	1994.5	1995	1900 4	1907 0	1900 9	969·3 969·3	1970.7	19715	1972.0	1973.7	1974	11974.7	1974 * 7	11074·7	1075.1	074.4	1074.5	074.7	1074 - 5	1074.0	ハクフ・エ	1072.8	072.2	072.0	1071
<u> </u>		1		1	i	Į.	1	l l		1	I .	1	l .	1	i	I	1	ŀ	ł	1	1	1	1	l	1	
Ve	11 12	971.4	971.5	971.7	971.1	971.5	971.5	971.7	972.1	972.5	972.8	972.9	973.1	973.2	973.2	973.1	973.4	973.9	974.6	975.2	975.8	976.5	976.4	977.6	978.1	973
3	13	1907 0	1900 .	11900 1	1909 3	1909 1	981.7	1990.7	990	1991 0	1991	HUUL L	יי ביטטוי	IOO1 'A	I COCI 1-V	$1001 \cdot 1$	1001.3	1001.2	חי ד סטוי	แดดบางต	ทองเกา	IOO T •O	ioo tool	IOO T • T	IOO T . T	IUU
¤.	14	1990.9	1990.0	1990.5	1990 3	990.2	1909.9	1909.0	190917	1989.7	1989.0	NOSO ·	llogo.v	IOSO·1	1088.7	1088.5	In88+2	I088+1	1088.2	·ͿດϨϨͺ·τ	ปก88 ก	ปก8วงก	087.7	087.5	087.5	080
9	15	987·3	986·8	986.3	986-1	985·3	985∙0	984.2	983-9	983.8	983.0	982.8	982.3	981.8	981.0	980.6	980.1	979.6	979.4	979.4	979.0	978.1	978.1	977.6	977.5	982
Station Level	16	977.2	976.9	976.6	976.5	976.4	976.3	976.3	976.5	976.6	976.6	976.7	977.0	977.0	976.7	976.0	976.0	976-8	977.2	977.2	977.2	977.0	977.0	977.0	976-6	076
S)	17	19/4.3	19/0 4	1915 4	1913 4	1970 0	19/00	14// 4	14//4	1470.7	10/01	1107012	uzuro	IOOO T	ലാരവം	∄080°5	IOXO+4	10X0 · 2	IOXO · A	1070.7	リヘケヘ・ヘ	リハケメ・ケ	077.0	077.0	076.7	1000
	18 19	1972.7	19/4	19/4.5	1970.0	1909.5	1900"/	1907.5	1907.1	1900.7	1900.1	1904.4	1964.5	1964	1064·5	064.7	1065.1	1064.0	1065.2	065.0	ქინნ•ნ	1067.0	067.4	067.7	067.0	067
	20	977.5	977.6	977.8	977.8	978.3	969·3 978·4	978.9	978.0	979.1	979.5	979.3	978.0	978.4	972.4	972.0	972.9	973.3	973.7	974.5	975.1	970.0	970.3	970.8	977:3	1971 1076
	4			l .	ì	1	1	ı	1	1	1	1		l	ſ	1	1	}	1		1	1			ł	
	21 22	959.4	959.5	959.4	959.2	950.0	963·0	958.0	901.0	959.8	959.1	959.1	959.1	958.9	958.8	958.7	958.8	958.9	959.1	959.1	959.2	959.2	959.2	959.1	959.3	961
l	23	959.3	959.3	959.5	959.7	960.0	960.3	960.8	959	959 0	062.1	959.1	959.1	062.5	950.5	950.4	950.4	950.5	950.0	950.0	950.0	958.8	958.9	958.9	958.9	958
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	25	971.1	9/1.1	9/0.9	9/0.9	9/0.9	970.9	970·8 	970.7	970.6	970.5	970.5	970.3	969.6	969.2	969.0	968.3	968-3	968.3	968-2	967.7	967.4	967.0	966.7	966.1	969
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Note. When pressure exceeds 1000 mb. the leading figure 1 is not printed, i.e., 1005.6 mb. is written 005.6. This rule does not, however, apply to monthly means.

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Mean

Mean

(Station level)

G.M.T.

(Sea level)

113. **Eskdalemuir**: H_b (height of barometer cistern above M.S.L.) = $237 \cdot 3$ metres.

March, 1923.

													<u> </u>													923.
	Day.	I.	2.	3.	4.	5.	6.	7.	8.	9.	IO.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
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	1 2	957.6	5 9 5 6•	6 956∙:	1 956∙	o¦956•	5 956.	9 957 9	957.6	5 957:	5 956.9	956∿	9 956-8	956-2	2 955.8	3 955.5	955.1	955.1	9551	1 954.9	954.8	954.5	954.3	954.4	954.6	956 · 0
	3	954.8	954	9 955	1 955.	2 955.	7 956.	6 957.7	7 959 2	2 960.4	1 962 1	1 963.	3 964.4	1965-6	5 966.	7 967.8	3 968-8	969.9	970.	5 972·C	973.0	974.1	975.4	976.4	977.5	964.4
	5	990.	989	3 988 8	8 987	5 986	5 986	2 985	1 984 2	2 983	5 983.0	982	3 981 3	980.8	1989 ·	5 980.5	990·1	980.8	981.4	1982.2	982.9	983.2	984.8	985.0	985·1	984.1
1 1	6	085.1	1084	0084	7 0821	5 082	0.82.	0087.		10704	078.		5 076.	075.5		5074.1	072.7	072.4	072.		070.0	070.6	070.0	077.0	077.0	077.6
	7 8	970:3	3 968+	7 968.0	6 9671	8 967.	5 967 :	2 966.9	9 967.0	0 967*/	7 968∵	5 969+	1 971 2	1972.6	974.2	2 975.6	973·7 976·8	978.3	979:3	3 980.5	5 981.5	982.4	983-2	: 984∙0	984.4	1973 • 6
	8 9	984.8	3 985.	1∣985∵	3 985	8 986•	2 986.	9¦987·9	9 988+1	ւ 988∙։	5 989 .	5 989√	8 990 1	990.	5 990 ·5	991.1	1 991 • 7	992.1	992.8	3993.3	3 993 9	994.0	994.1	994.3	994.5	989.8
	10	990.	1989	8 989	7 988	9988	8 987	8 987.7	7 987 6	5 987	5 987.2	2 986	986.8	993.	985.7	7 985.0	7 992·3 984·6	984.2	984.1	1984.2	984.3	984.6	984.7	985.0	985.2	986.7
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	12	991.1	1 990	7 990 2	2 990	1 990	0 989	5 989.4	1 989 2	1 989	1988-6	987	987.5	986.4	1985	984.3	990·1 983·8	983.0	982.5	981.6	981.5	981.4	981.2	981.2	981.7	986.3
٦	13	981.6	982	3 983.5	5 984°.	3 985.	2 986•	5 987.9	989.1	ī 990∙	5 991.8	3 991	8 992.8	993.2	994.0	994.7	1995.1	995.7	996.8	997:4	µ998∙1	998.5	999.1	999.3	999.7	991.7
ة ا	14	001	999	9 001 8	3001	6 001	6 001	5 001 6	001.6	001.	2 001 2	2001	1 000.7	000.1	999.8	999 1	999.5	999.6	999.6	999.6	999.4	999.3	999.2	999.2	999.3	000 · 5
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; t	18	004.5	004.	004.0	004.0	003.	9 003 9	9 004-1	004.1	004.5	004.4	004	3 004.4	004 1	003-4	002.9	002.7	002.7	003.0	003.0	003.2	003.2	003.1	002.8	002.4	003∙6
	19 20	996.5	996	2 995 - 8	3995	4 994	8 995	0 994 9	994.8	999.0	999.1	998	7 994 2	998.2	998.0	997.0	996.9	990·7	990.9	990.9	997.0	997.1	997.0	990.9	990.0 993.5	990.9
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	24 25	988.6	988.6	7 984.6 5 988.4	988 -	988	985·3 1988·1	3 985·3 1 988·4	985.8	988.2	988-0	986.0	985.0	988∙0 988∙0	985.9	985.9	985·9 988·5	080∙1 980•0	980·6 980·8	990.8	987.8	988·4 992·3	988.4	988.6	988.0 993.0	980·1
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	26 27	994.2	080	994.7	994.7	7 995.0 1 088.0	995.3	995.4	995.6	995.6	995.6	995.1	994.9	994·I	993.5	085.1	992·4 984·6	992·3	992 · 0 983·0	991.8	991.7	991·7 083·0	083.0	991·0	990·5	993·6 086·3
	28	984.2	984.1	984.4	984.7	985.1	i 986∙c	986.5	987.0	987.6	988.2	988.6	988.7	989∙0	989.2	989.6	989.6	990.0	990•6	991.1	991.5	991.9	992.0	992.5	992.9	988:4
	29 30	993.1	993.4	1993.6	993.8	994.0	994.4	994.6	995.2	995.2	995.6	995.4	995.4	995.3	995.2	995.0	995·0 994·9	995.0	995.3	995.8	996.0	996.2	996.3	996.7	996.8	995.0
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¥	31	993.4	992.8	992.2	991.7	991.4	991.2	991.1	990.8	990.6	989·6	989.4	988.9	988.5	988∙0	987.4	987.1	986.9	986·8 	986.4	986∙0	986·o	985.9	985.8	985.8	989 • 1
Mean		987	987	987	987	987	987	988	988	988	988	988	988	988	988	987	987	988	988	988			988	988	988	988
(Stati	on level)	-99						1 .10									89		•22							
(Sea l	evel)	1017	.27	·8g	.79	-28	.62	.55	71		1017							•04	36						·31	
444	Eskda			17.	10 17	09 17	9 .25																		1 10	
114.	Eskda	Iemui	r : E	$I_b=2$	37.3	met	res.																	Apri	1, 19	ZJ.
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114.	Eskda I 2	mb. 985.8	mb. 985·8	mb. 985·6	mb. 985·5	mb.	mb.	mb.	985.9	986.7	986.9	986.0	987.0	987.4	987.6	987.9	988.3	988.8	989.4	990.5	990.9	991.6	992.4	mb. 993·1	mb. 993·2	mb. 987·9
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Readings in millibars at exact hours, Greenwich Mean Time.

123 PRESSURE.

115. **Eskdalemuir**: H_b (height of barometer cistern above M.S.L.) = $237 \cdot 3$ metres.

May. 1923.

			r i 1.	I_b (he	ngiit	or ba	101116				ve m	.S.L.) — 2	37.3	men	es.									y, 19	
Da	ay.	I.	2.	3.	4.	5.	6.	7.	8	9	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mear
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	3	994.3	993.8	993.5	992.6	992.3	992.2	992.1	991.8	991.3	990.8	990.4	990.4	990.0	989.5	989.0	988.7	988.2	988.2	988.2	988.2	988.2	988.2	988.2	988•2	990
	4 5	983·8 983·8	98 7 ·5 98 3 ·8	987·3 983·8	987·2 983·6	986·7 983·6	980·3 983·6	983·6	983·6 983·6	98 3 ·8	983·9	983.5	984·7 983·2	984·7 982·9	982·8	982.1	981.8	981.3	980.9	980·1	979:7	904·2 979·6	979.5	979.1	979·1	982
	6	979.1	979.1	979.4	979:5	980∙0	980.5	980.9	981.3	982.4	982.7	983.1	983.4	983·6	983.7	983.9	984.4	985·o	985.7	986.2	986.7	987.5	988·o	988.3	988.7	983.
	7 8	988·9 989·4	989·1	989·5 988·8	990·0 988·5	990.4	988.1	988·1	991·5 988·1	991·7 987·8	991·5 987·8	991.3	991·1 987·6	991 · 2 987 · 0	990·9 986·7	990·6 986·6	990·5 986·5	990·3 986·2	990·4 985·9	990·5 985·6	990·8 985·6	990·8 985·5	990·1	990·5 984·9	989.8	987
]	9	983.6	983.2	982.7	982·0	981.1	980.5	980∙0	979.3	978.6	978.2	978⋅0	977·5 978·4	977:3	976.7	976.5	976.6	976.8	977.5	978.2	979.6	980.4	980.8	981.2	981.5	979
									1														i		İ	1
]	12	966.2	966.2	966.4	966•6	966.8	966.9	966.8	967.1	966.9	967.3	967.4	960·4 967·3	967.5	968.2	967.6	967.6	967.7	968·o	968.3	968.5	968.7	968.8	968.6	968.3	967
Level	13 14	967.8	967.3	966·6	966·0	965.5	965·4	965.4	965·1	965·0	965.1	965.3	965·5 971·1	965·8	966.2	966.3	967.2	967·4 970·1	967·4	968·9 969·7	969·1	969·5 969·5	969.5	970.5	969.4	907
Le	15	969.5	969.7	969.6	970.1	970.3	970.6	970.7	970.9	971.5	971.6	971.4	970.9	970.9	970.4	970.1	969.7	969.6	969.2	969.3	969·3	969.5	969.5	969.4	969.2	970
on	16	969.1	969.0	969.0	969.2	969.7	970.2	970.4	971.1	971.8	972.2	972.5	972.7	973.2	974.3	974.4	974.3	975.0	975.4	976.2	977.0	977:4	977.6	977.6	977.9	973
Station	18	986.9	987.1	987.2	987.4	988.2	988.4	988.9	989.2	989-2	989∙0	988.9	980·2 988·9	988.9	988+5	988.1	987.8	987.5	987.2	986.5	986.2	986.4	986∙1	985.5	985.0	987
St	19	983.9	983.3	982.6	982.1	981.6	981.5	981.0	980.9	980.4	980·1	979.8	979·6 974·8	979.5	979.5	979.2	979.1	979.1	979·I	979.0	979.0	979.0	979.0	978.9	978.5	980
		l							i	i	ļ	1	979.2										1	1		1
	22	982.8	983.1	983.1	983.2	983.5	984:0	984.4	984.7	985∙0	985.7	985.0	986.0	986∙0	986.3	986.3	986-6	986-6	986.7	986.4	986.8	986.8	1986.8	1986-8	1986-9	985
	24	992.4	992.4	992.4	992.4	992.4	992.6	992.6	992.3	992.2	991.4	990.6	988·4 990·0	989.9	989.5	988.7	988.1	987.0	986.2	984.7	983.5	982.3	981.7	981.1	981·0	988
	25	979.9	979.6	979.0	977.8	977.7	977.5	977.9	978.4	978.7	978.9	978.9	979.4	979.3	979.7	979.5	979.9	980·1	980.5	980·9	981.1	981.5	981·3	981.0	981.0	979
	26	980.6	980.5	981.0	980.6	980.9	981·o	982.0	982.3	982.7	983.1	983.2	983.6	984.0	985.0	985.3	985.6	986∙0	986.7	986.9	987.2	987.5	987.5	987.7	987.9	984
	28	993.7	993.4	993.4	993.2	992.9	993.4	993.4	994.0	994.3	994.5	994	991·4 995·0	995.0	995.6	995.8	996.0	995.5	995.6	995.9	997.1	997.6	998.4	1998-6	998-5	5 995 ·
	29	1998-4	998.6	998.5	998-6	998.6	998.5	1998.9	999.0	998.7	1998.3	1998-2	998·0	997.7	1997:3	1997.2	996.6	996-6	996.5	996+5	990.5	996.3	3 996.2	:1996.2	2 996·c	վեթլ.
		l			l	l	ļ	1	1			1	996.8	1			1						1	i		1
	31	990 3	982		982	982	982	982	982		982	982	982	 -		- 	982	982	982	982	983	983	·	983	i	982
Mean Statio	n level)	37	·31	.28	·26	•34	. 48	√65	.78	⋅84	∙88	3 .90	√ 89	•93	.93	.79	•68	•63	.62	.76	•00	17	25	•22	.10	• 7
Mean (Sea le	vel)	1011											1011 8 ·57		1011			34							1012	6 .6
116.	Eskda	lemu	ir : I	$\mathbf{H}_b =$	237	·3 m	etres.																	Jun	e, 19	23.
<u></u>		mb.																								
j			mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	m 5.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.
	2	996·0 999·5	996·2 999·6	996·1 999·5	995·0 999·6	995·8 999·8	995·7 000·0	996·2	996.6	996·8	996·5	996.3	996.3	996·3 998·3	996.3	996.3	996·3	996·3 996·7	996·3	996·9 996·3	997·2	997.9	998.3	998.7	999.1	1996 · 1998 ·
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	3	996·0 999·5 995·5 086·8	996·2 999·6 995·2 987·1	996·1 999·5 995·2 987·5	995·0 999·6 994·6 988·0	995·8 999·8 994·0 987·3	995·7 000·0 993·8 988·1	996·2 000·2 993·4 988·4	996·6 000·2 993·2 988·7	996·8 000·1 992·7 989·0	996·5 999·4 992·0 988·8	996·3 999·3 990·9	996.3	996·3 998·3 989·8 988·3	996·3 998·1 989·2	996·3 997·5 989·1 987·5	996·3 997·1 989·0 987·2	996·3 996·7 987·7 987·1	996·3 996·4 987·2 986·7	996·9 996·3 986·6 986·6	997·2 996·2 986·1 986·5	997.9 996.2 986.2	998·3 996·1 986·3	998·7 996·6 986·6	999·I 995·9 986·3 987·I	1996 · 1 998 · 1990 · 1987 ·
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Station Level	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	996.0 999.5 985.5 987.1 983.9 990.4 985.5 977.8 986.0 000.3 986.6 989.4 990.9 984.2 992.6 992.6 992.6	996.2 999.6 995.2 987.1 984.1 990.4 985.0 977.8 986.3 000.2 985.8 990.6 985.9 992.7 990.1 088.3	996·1 999·5 987·5 987·1 984·3 990·4 974·4 977·5 987·0 999·7 985·2 999·5 986·4 992·8 989·7 988·4	995.0 999.6 984.6 988.0 987.1 984.7 990.4 983.7 977.6 988.4 999.4 989.6 989.2 987.1 992.8 989.6	995.8 999.8 994.0 987.3 987.1 985.3 990.6 983.0 974.5 997.7 988.5 999.0 983.4 991.6 988.9 987.4 993.2 989.5	995.7 993.8 988.1 987.1 985.4 990.9 982.2 974.3 977.9 989.8 988.0 983.1 988.3 988.3 988.3	996·2 993·4 988·4 987·0 986·4 991·1 982·0 977·9 990·9 982·1 998·5 988·6 993·5 989·2 989·2	996.6 000.2 993.2 988.7 986.9 986.7 991.4 981.3 977.8 991.5 997.0 982.3 997.8 989.1 989.1 989.2	996.8 992.7 989.0 986.7 987.1 991.6 980.1 977.6 992.2 995.9 983.1 989.2 993.6 989.3 989.3	996·5 999·4 992·0 988·8 986·5 987·2 991·6 976·1 978·1 993·3 994·9 983·5 989·7 989·7	996.3 999.3 998.7 988.7 986.6 987.3 991.4 976.6 978.1 994.2 983.5 985.7 990.1 993.2 989.3	996·3 998·9 989·1 988·3 885·7 987·6 991·3 976·6 978·5 995·0 993·0 993·1 993·5 990·3	996·3 998·3 988·3 985·3 987·8 991·3 977·9 978·8 996·1 991·8 984·1 993·4 984·5 989·3	996·3 988·1 988·1 984·7 987·8 991·2 977·6 977·3 996·6 991·2 984·5 993·8 993·1 989·0 989·0	996·3 997·5 989·1 987·5 984·3 987·9 997·0 977·1 997·2 990·5 984·7 993·0 983·2	996·3 997·1 989·0 987·2 983·8 988·1 990·6 977·3 977·4 997·8 989·8 985·2 992·6 982·3 992·6 988·6 988·6	996·3 996·7 987·7 983·0 988·3 990·0 976·5 977·3 979·8 998·5 989·6 992·2 981·9 990·1 992·5 988·6 988·6	996·3 996·4 987·2 981·8 988·6 989·8 977·6·4 977·6·9 980·2 998·3 989·5 992·2 992·5 988·9 988·9	996.9 996.3 986.6 981.6 988.9 989.3 977.8 987.8 980.7 999.2 989.4 991.9 991.3 990.4 992.5 988.7 988.7	997.2 996.2 986.1 986.5 982.0 989.2 989.1 976.0 998.5 989.5 981.5 991.0 992.7 989.0 989.0	997.9 996.2 986.2 982.7 989.6 982.7 989.6 976.0 978.3 989.4 986.4 992.2 981.7 991.5 992.7 998.9 988.9	998·3 996·1 986·3 986·7 983·0 989·8 975·9 975·9 978·4 983·9 902·2 982·3 991·6 992·5 998·7 988·7	998.7 996.6 986.6 987.8 9975.4 975.4 975.4 978.4 984.3 000.3 988.7 987.9 992.1 992.2 992.1	7 999·1 995·9 986·3 987·1 983·3 996·2 975·5 978·6 985·2 000·4 987·5 988·7 991·5 988·7 991·5 998·2 998·3	996. 998. 999. 987. 995. 996. 997. 997. 994. 993. 984. 993. 984. 992. 985.
Station Level	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	996.0 999.5 986.8 987.1 983.9 990.4 985.5 977.8 986.0 936.6 989.4 990.9 984.2 990.8 988.3 991.3	996.2 999.6 995.2 987.1 987.1 984.1 990.4 975.0 977.8 986.3 997.7 985.9 990.6 985.9 990.1 988.3 991.7	996·1 999·5 987·5 987·1 984·3 990·4 984·4 977·5 987·0 985·2 999·5 989·9 986·4 992·8 992·8 992·8 992·4	995.0 999.6 988.0 987.1 984.7 990.4 997.6 988.4 999.4 983.6 990.9 989.2 987.1 992.8 989.1	995.8 999.8 994.0 987.3 987.1 985.3 990.6 974.5 977.7 988.5 993.2 989.1 989.3 989.1 993.7	995.7 993.8 988.1 987.1 985.4 998.2 974.3 977.9 989.8 998.3 991.8 988.3 988.3 993.5 989.3 993.5	996·2 993·4 987·4 987·9 980·4 991·1 997·9 990·9 982·1 988·5 988·6 988·6 988·6 988·6 988·6 988·6 988·6 988·6 988·6 988·6 988·6	996.6 000.2 988.7 986.7 991.4 991.5 991.5 992.8 989.7 989.4 994.4	996.8 000.1 988.7 987.7 987.6 987.7 997.6 992.2 993.6 992.2 993.6 987.1 989.2 993.6 987.1	996·5 999·4 992·0 998·8 986·5 991·6 976·1 978·1 993·3 994·9 983·3 994·9 983·3 994·9 989·7 998·3	996:5:999:3:999:5:988:7:988:7:988:7:998:5:978:1:9994:5:9983:5:7:9993:2:989:3:5:7:999:3:2:989:3:5:7:999:3:2:989:3:5:7:999:3:2:989:3:5:7:999:3:2:989:3:5:7:999:3:2:989:3:989:3:3:989:3:3:989:3:3:989:3:3:989:3:3:989:3:3:989:3:3:989:3:3:989:3:3:989:3:3:989:3:3:989:3:3:3:989:3:3:3:3	996·3 998·9 989·1 988·3 885·7 987·6 991·3 976·6 978·5 995·0 993·0 9983·1 993·5 989·1 999·3 999·3 999·3	996·3 3989·8 3985·3 987·9 991·3 997·9 998·9 996·1 9991·3 9	996·3 998·1 988·2 984·7 987·8 991·2 977·0 979·3 996·6 991·2 984·5 993·9 983·8 999·3 989·9 994·8	996·3 997·5 989·1 987·5 984·3 987·9 997·0 977·1 997·2 990·5 984·7 993·0 983·2 990·2 993·0 989·3 994·8	996·3 997·1 989·0 987·2 983·8 988·1 990·6 977·3 979·4 997·8 985·2 992·6 982·3 990·1 992·6 988·6 989·5 994·9	996·3 996·7 987·7 987·7 983·0 988·3 990·0 997·5 997·5 988·6 992·2 981·9 990·1 9992·5 988·6 989·2 990·1 9992·5 988·6 989·2 990·1 990·3	996·3 996·4 987·2 986·7 981·8 988·6 989·8 977·6 980·2 988·3 989·3 992·2 981·5 992·2 981·5 999·3	996.9 996.3 986.6 988.9 988.9 987.3 997.8 980.7 999.2 989.4 981.3 990.4 992.5 989.9 994.9	997-2 996-2 986-1 982-0 989-2 989-1 982-6 976-0 978-1 982-6 989-5 989-5 989-5 989-5 989-5 989-5 989-5 989-5 989-5	997.9 996.2 986.2 982.7 989.6 988.4 976.2 976.2 983.1 000.2 981.7 981.7 992.7 989.5 989.5 989.5	998·3 996·1 986·3 986·3 987·9 975·9 975·9 978·4 983·9 982·2 982·3 991·6 992·5 988·7 989·8 994·9	998.7; 996.0; 987.1; 999.0; 987.8; 975.4; 975.4; 984.3; 987.9; 982.9; 992.1; 982.9; 992.1; 988.4; 990.5; 994.3;	999:99 986:33 986:33 986:33 986:23 986:22 975:59 975:59 985:22 987:59 988:29 999:43 999:44 989:79	996, 998, 998, 998, 999, 998, 999, 998, 999, 998, 999, 998, 999, 998, 999, 998, 999, 998, 999, 9
Station Level	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	996·0 999·5 998·8 987·1 983·9 990·4 985·5 977·8 986·0 989·4 990·9 984·2 992·6 990·8 991·3 991·3 994·3 993·9	996.2 999.6 989.1 984.1 985.1 985.1 985.3 990.4 985.0 977.8 986.3 990.6 985.9 992.7 993.6 993.6 993.6	996·1 999·5 987·5 987·1 984·3 990·4 984·4 977·5 987·0 999·7 985·2 990·5 986·4 992·8 988·4 992·4 992·7 989·6	995.0 999.6 988.0 987.1 984.7 999.4 983.7 974.6 988.4 983.6 999.9 989.2 987.1 992.8 989.1 993.0	995.8 999.8 998.7 987.1 985.3 987.1 985.3 997.7 988.5 997.7 988.9 987.4 993.2 989.5 989.7 989.7 989.7 989.7	995.7 990.0 988.1 987.1 985.4 990.9 982.2 974.3 977.9 989.8 998.0 983.1 991.8 988.3 993.5 989.3 992.1 992.1 989.8 994.9	996·2 998·4 988·4 987·0 986·4 987·0 975·2 977·9 990·9 982·1 988·5 988·6 993·5 989·4 994·1 992·1 9904·3	996.6 000.2 988.7 986.9 986.7 981.3 997.8 991.5 997.0 982.3 997.8 989.1 993.7 989.2 999.4 991.8	996·8 900·1 986·7 989·0 986·7 987·1 97·6 992·2 995·9 983·1 989·2 993·6 994·7 991·9 991·9	996·5999·69992·9992·9992·9992·9991·69991·69991·69993·39994·9993·3989·79994·79991·99991·9991·9991·9991·9991·	996:5:999:5:999:5:998:7:998:7:998:7:998:7:998:7:998:7:998:7:998:7:998:7:998:7:998:7:998:7:998:7:998:7:998:7:999:7:9998:7:99888:7:99888:7:99888:7:99888:7:9988888888	996·3 998·9 988·1 988·3 988·5 997·6 997·6 997·6 993·0 993·0 993·1 993·5 993·2 989·1 999·8 991·8 991·8	996·33 998·3 988·3 987·8 997·9 977·9 977·9 991·8 993·4 984·5 993·2 993·2 993·3 993·3 993·3	996·3 998·1 988·2 988·1 988·7 987·6 977·6 979·3 996·6 991·2 984·5 993·0 983·8 990·3 9994·8 991·3 9904·8	996·3 997·5 989·1 987·5 984·3 987·9 977·1 997·1 997·2 990·5 984·7 993·0 983·2 990·2 993·0 989·3 990·9	996·3 997·1 989·0 987·2 983·8 996·8 977·3 979·4 997·8 989·8 985·2 992·6 982·3 990·1 992·6 988·6 989·9 994·9	996·3 996·7 987·7 987·7 987·7 989·1 990·3 990·3 990·1 990·3 990·3 990·3	996·3 996·4 987·2 981·8 988·6 989·8 976·4 977·6 980·2 998·3 989·5 981·5 992·2 982·5 988·9 994·9 990·3 992·3	996-9 996-3 986-6 986-6 988-9 976-0 977-8 989-7 999-2 989-4 992-5 988-7 994-9 990-5 992-9 994-7	997-2 996-2 986-2 986-5 982-0 989-2 976-0 988-6 992-0 981-5 991-0 992-7 989-2 995-1	997.5 996.2 986.6 982.7 988.4 976.5 983.1 000.2 989.4 992.2 981.7 991.5 992.7 998.9 989.9 989.9	998·3 996·1 998·3 998·7 983·0 989·8 9975·9 975·9 989·1 989·1 989·3 991·6 992·5 988·7 998·8 994·9	998.7; 998.7; 988.7; 987.1; 975.4; 975.4; 978.4; 984.5; 992.1; 982.5; 992.2; 992.1; 989.5; 993.5;	999:99 986:33:38 987:11 983:33 990:33:986:22 975:59 985:22 000:44 987:59 988:79 988:79 988:28 994:44 989:79 992:59 993:88	996 998 998 997 985 987 998 997 997 997 993 984 993 985 989 989 989 999 989 999 999
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Station Level———————————————————————————————————	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	996.0 999.5 986.8 987.1 983.9 990.4 985.5 9977.8 986.0 9936.6 989.4 992.6 992.8 991.3 991.3 991.9 991.9 991.9	996.2 999.6 998.7 987.1 987.1 985.0 977.8 986.3 980.2 985.8 990.6 985.9 990.7 993.6 989.7 993.7 993.7 993.7 993.1	996 1 999 5 995 2 987 5 987 1 984 3 990 4 977 5 987 0 999 7 985 2 999 5 989 9 986 4 992 8 992 7 989 8 992 7 989 8 992 7 989 8 992 7 992 1	995.6 999.6 988.0 987.1 984.7 999.4 983.7 999.4 998.3 987.1 988.4 998.3 987.1 989.2 987.2 989.3 992.2 989.3 992.2 989.4 993.4	995.8 999.8 998.7 987.1 985.3 999.6 983.0 974.5 997.7 988.5 999.0 987.4 991.6 992.2 989.9 991.6 994.5	995.7 993.8 988.1 987.1 985.4 998.2 977.9 989.8 998.0 983.1 991.8 988.9 988.3 993.5 989.3 992.1 989.8 992.1 991.9 992.3 990.0 991.6 994.5 994.5	996·2 998·4 987·0 986·4 991·1 982·0 975·2 977·9 990·9 992·4 998·5 998-6 998-6 998-2 992·4 992·4 992·4 992·4 992·4 992·4	996-6 000-2 988-7 986-9 988-7 981-3 977-8 991-5 997-0 982-3 989-1 999-7 994-6 992-1 990-4 990-4 991-7 994-8	996.8 900.1 986.7 989.0 986.7 991.6 987.1 991.6 992.2 995.9 983.1 989.2 994.7 991.9 990.4 990.4 990.4 990.4	996·5 999·4 988·8 986·5 987·2 991·6 978·1 993·3 994·9 998·6 989·7 994·7 991·9 991·6 994·8 992·3 992·5	996:5999:5999:5999:5999:5999:5999:5999:	996·3 998·9 988·1 988·3 988·5 997·1 976·6 978·5 993·0 993·0 993·1 993·5 993·2 989·1 991·8 991·8 991·8 991·8	996·33 9988·3 9888·3 987·3 997·3 997·3 997·8 998·1 998·5 998·3 998·3 998·3 998·3 998·3 998·3 998·3 998·3 998·3 998·3 998·3 998·3	996:3998:1998:29988:1998:2997:0997:0997:0997:0997:0997:0997:0997	996·3 997·5 989·1 987·5 984·3 987·9 997·0 977·1 997·2 990·5 983·2 993·0 983·2 993·0 989·9 989·3 991·8 991·6 990·6	996·3 997·1 989·0 987·2 983·8 988·1 990·6 976·8 987·3 997·4 997·8 985·2 992·6 982·3 990·1 992·6 988·6 989·5 994·9 990·4 991·1 992·3 993·5	996·3 996·3 996·7 987·7 987·1 983·0 988·3 999·0 976·5 987·3 999·2 9992·2 999·3 999·4 999·3 990·1 991·1 992·5	996·3 996·4 987·2 986·2 988·6 988·6 988·3 988·3 988·5 998·3 989·5 999·2 998·3 998·9 994·9 990·3 992·8 994·7 991·6 990·1	996-9 996-3 986-6 986-6 981-6 988-9 977-8 980-7 999-2 989-4 988-0 998-3 990-4 998-7 999-1 991-5 999-1 991-5 991-9 991-5 991-9 991-5 991-9 991-7 991-8 991-9 991-	997:2 996:2 996:2 986:5 982:0 989:1 976:0 978:1 976:0 998:5 989:5 991:0 991:7 991:5 991:7 993:5 992:7	997.52 996.62 986.62 988.62 988.63 978.33 988.44 976.62 989.44 981.75 988.95 989.52 989.52 989.62 999.73 991.62 999.74 999.74 999.74 999.74 999.74 999.74 999.74	998·3 996·1 986·3 988·8 987·9 975·9 975·9 978·4 983·9 900·4 982·3 991·6 992·5 988·7 989·8 991·6 992·5 994·8 991·5 990·1 992·7 994·6 992·7	998.7.998.7.998.7.998.7.998.7.998.7.998.7.998.7.998.7.998.7.999.7.998.7.999.7.	999:19 995:99 986:33 987:1 983:3 990:33 986:22 975:5 978:02 987:5 988:7 999:5	996 998 998 998 998 998 998 999 996 998 999 998 999 998 999
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Mean (Statio Mean	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 n level)	996·0 999·5 999·5 998·8 987·1 983·9 990·4 985·5 986·0 980·6 989·4 990·9 984·2 992·6 990·8 988·3 991·3 994·7 991·0 991·0 991·0 991·0 991·0	996.2 999.6 999.6 998.7 984.1 998.6 995.9 977.8 986.3 900.6 985.9 992.7 993.6 989.8 992.1 988.8 992.1 989.8 992.1	996·1 999·5 995·2 987·5 987·1 984·3 990·4 974·4 977·5 989·7 985·2 990·5 989·7 989·7 989·9 986·4 992·4 992·7 989·8 992·7 992·1 989·8 992·7 992·1 989·8 991·8 994·3 994·7 996·9 989·9	995.0 999.6 999.6 998.0 984.7 984.7 984.7 974.6 988.4 997.6 988.4 999.2 987.1 992.8 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2	995.8 999.0 994.9 998.7 987.1 985.3 987.7 988.5 997.7 988.5 999.6 989.5 989.7	995.7 000.0 993.8 988.1 987.1 985.4 990.9 982.2 974.3 977.9 989.8 998.0 983.1 991.8 988.9 988.3 993.5 989.3 992.1 989.8 994.2 991.9 992.3 990.0 991.6 994.7 989.6 990.0 991	996·2 998·4 987·0 986·4 987·0 986·4 987·0 975·2 977·9 990·9 982·1 988·5 988·6 993·5 989·4 992·4 992·4 992·4 992·4 992·4 992·4 992·4 992·4 992·4	996.6 996.6 9903.2 9988.7 986.9 986.7 981.3 977.8 991.5 997.6 982.3 992.8 989.1 993.7 989.2 990.4 991.7 994.8 999.7 994.8 999.4 991.7 994.8 999.7 994.8	996·8 000·1 986·7 988·1 998·0 986·7 987·1 976·3 997·6 992·2 995·9 983·1 989·2 994·7 991·9 990·5 992·4 991·8 994·8 994·8 994·8	996·5999·49991·699999999	996:5:999:999:999:998:7998:6:999:5:999:999:5:999:5:999:5:999:5:999:5:999:5:999:5:999:5:999:5:999:5:999	996·3 998·9 989·1 988·3 988·5 997·6 997·6 993·0 993·0 993·1 993·5 993·5 993·5 991·8 991·8 991·8 991·8 991·8 991·8 991·9 991·9 991·9	996·33 987·8 998·39 987·8 997·9 978·8 996·1 991·8 991·3 991·3 991·3 991·3 991·3 991·3 991·3 991·3 991·3 991·3 991·3	996·3 998·1 988·2 988·1 988·3 988·6 977·6 979·3 996·6 991·2 984·5 993·0 989·3 991·3 991·3 991·3 991·3 991·3 991·3 991·3 991·3	996·3 997·5 989·1 987·5 984·3 987·9 990·9 977·1 997·2 990·5 984·7 993·0 983·2 990·2 991·8 991·8 991·6 990·6 991·1 992·2 993·6 991·1 998·7 988·7 989 1018	996·3 997·1 989·0 987·2 983·8 988·1 996·8 977·3 979·4 997·8 989·6 982·3 990·1 992·6 988·6 989·9 990·4 992·0 994·8 991·1 992·3 993·5 993·0 988·7 989 •56	996·3 996·7 987·7 987·7 988·3 998·5 976·5 977·3 979·8 998·5 998·6 992·2 981·9 990·1 991·1 991·1 991·1 992·5 993·4 992·8 988·6 989·1 991·1	996.3 996.4 987.2 988.6 989.8 976.4 977.6 980.2 998.3 989.5 992.2 981.5 992.2 992.5 989.9 990.3 992.8 994.9 990.1 991.6 990.1	996-9 996-3 986-6 988-6 988-9 977-8 988-7 999-2 988-7 998-3 998-7 998-3 998-9 998-3 999-1 991-5 993-3 993-	997-2 996-2 996-2 986-2 986-5 982-0 989-2 976-0 978-1 982-6 999-8 989-5 991-0 992-7 993-5 991-7 993-5 991-7 993-5 991-7 993-5 991-7 993-5 991-7	997.5 996.2 986.6 982.7 989.6 983.1 000.2 989.4 981.5 991.5 992.7 991.5 991.6 993.7 991.6 993.7 991.6 993.7 991.6 993.7 993.	998·3 996·1 986·3 986·7 983·0 987·9 975·9 978·4 983·9 992·2 982·3 991·6 992·5 988·7 998·8 994·9 994·6 994·6 992·7 994·6 992·1 988·6 989·9 991·1 988·6	998.76 998.76 998.76 998.76 998.76 988.76 987.76 987.76 987.76 988.76 988.76 988.76 988.76 988.76 988.76 988.76 999.76 989.76 9	999:99 999:99 998:99 988:33 990:33 990:33 990:35 998:52 998:52 999:53 9	996 998 988
Mean (Statio Mean (Sea le	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 n level)	996·0 999·5 999·5 998·8 987·1 983·9 990·4 986·0 900·3 986·6 989·4 990·8 988·3 991·3 994·3 994·7 991·0 991·0	996.2 999.6 999.6 998.7 984.1 998.6 995.9 977.8 986.3 900.6 985.9 992.7 993.6 989.8 992.1 988.8 992.1 989.8 992.1	996·1 999·5 987·5 987·1 984·3 990·4 987·5 987·5 987·0 989·7 985·2 990·5 989·7 989·7 989·7 989·7 989·7 989·8 992·4 992·7 989·8 992·7 989·8 992·7 989·8 992·7 989·8 992·7 989·8 992·7 989·8 992·7 989·8 992·7 989·8 992·7 990·0 ———————————————————————————————————	995.0 999.6 999.6 998.0 984.7 984.7 984.7 974.6 988.4 997.6 988.4 999.2 987.1 992.8 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2 989.2	995.8 999.0 994.9 998.7 987.1 985.3 987.7 988.5 997.7 988.5 999.6 989.5 989.7	995.7 000.0 993.8 988.1 987.1 985.4 990.9 982.2 974.3 977.9 989.8 998.0 983.1 991.8 988.9 988.3 993.5 989.3 992.1 989.8 994.2 991.9 992.3 990.0 991.6 994.7 989.6 990.0 991	996·2 998·4 987·0 986·4 987·0 986·4 987·0 975·2 977·9 990·9 982·1 988·5 988·6 993·5 989·4 992·4 992·1 992·4 990·3 990·3 994·8 989·5 994·8	996.6 996.6 900.2 988.7 986.9 986.7 981.4 981.3 975.3 977.8 991.5 997.0 982.3 989.1 993.7 989.2 991.7 994.6 992.1 992.4 994.8 989.2 990.4 994.8 989.2 990.4 991.7	996.8 900.1 998.7 998.7 988.7 987.1 976.3 977.6 992.2 995.9 983.1 989.2 994.7 991.9 990.5 994.7 991.9 990.4 991.8 998.8	996·5999·49991·699991·69991·69991·69991·69991·69991·69991·69991·69991·69991·69991·6999111·6999111·6999111·6999111·6999111·6999111·6999111·69999111·6999111·6999111·6999111·6999111·6999111·6999111·6999111·699	996:3999:9999:9999:9989:3989:3989:3989:3	996·3 998·9 989·1 988·3 988·5 997·6 997·6 993·0 993·0 993·1 993·5 993·5 993·5 991·8 991·8 991·8 991·8 991·8 991·8 991·9 991·9 991·9	996·33 988·3 988·3 988·3 987·9 977·9 978·8 996·1 991·8 993·4 984·5 990·3 994·8 991·3 991·3 991·3 991·3 991·3 991·3 991·3 991·3 991·3 991·3 991·3 991·3	996·3 998·1 988·2 988·1 988·3 988·6 977·6 979·3 996·6 991·2 984·5 993·0 989·3 991·3 991·3 991·3 991·3 991·3 991·3 991·3 991·3	996·3 997·5 989·1 987·5 984·3 987·9 990·9 977·1 997·2 990·5 984·7 993·0 983·2 990·2 991·8 991·8 991·6 990·6 991·1 992·2 993·6 991·1 998·7 988·7 989 1018	996·3 997·1 989·0 987·2 983·8 988·1 996·8 977·3 979·4 997·8 989·6 982·3 990·1 992·6 988·6 989·9 990·4 992·0 994·8 991·1 992·3 993·5 993·0 988·7 989 •56	996·3 996·7 987·7 987·7 988·3 998·5 976·5 977·3 979·8 998·5 998·6 992·2 981·9 990·1 991·1 991·1 991·1 992·5 993·4 992·8 988·6 989·1 991·1	996.3 996.4 987.2 988.6 989.8 976.4 977.6 980.2 998.3 989.5 992.2 981.5 992.2 992.5 989.9 990.3 992.8 994.9 990.1 991.6 990.1	996-9 996-3 986-6 988-6 988-9 977-8 988-7 999-2 988-7 998-3 998-7 998-3 998-9 998-3 999-1 991-5 993-3 993-	997-2 996-2 996-2 986-2 986-5 982-0 989-2 976-0 978-1 982-6 999-8 989-5 991-0 992-7 993-5 991-7 993-5 991-7 993-5 991-7 993-5 991-7 993-5 991-7	997.5 996.2 986.6 982.7 989.6 983.1 000.2 989.4 981.5 991.5 992.7 991.5 991.6 993.7 991.6 993.7 991.6 993.7 991.6 993.7 993.	998·3 996·1 986·3 988·6 987·9 975·9 978·4 983·9 9975·9 982·3 991·6 992·5 988·7 998·8 994·9 994·6 994·6 994·6 994·6 994·6 994·6 994·6 994·6 992·1 1988·6 989 991·5	998.7; 998.7; 998.7; 998.7; 999.7; 989.7; 989.7; 989.7; 989.7; 989.7; 989.7; 989.7; 989.7; 989.7; 999.7; 989.7; 999.7; 9	999:99 999:99 988:33 986:33 986:33 986:23 975:59 978:03 987:59 988:23 991:59 988:23 991:59 988:23 991:59 988:23 991:59 988:23 991:59 9	996 998 988

PRESSURE.

Readings in millibars at exact hours, Greenwich Mean Time.

117. Eskdalemuir: H_b (height of barometer cistern above M.S.L.) = 237·3 metres.

Station level 12 91 68 63 75 76 84 79 84 79 74 75 75 75 75 74 74 66 74 74 74 75 75 75 75 75	117.	Eskdal	lemui	r : I	I_b (he	eight	of ba	arom	eter c	ister	abo	ve M	.S.L.) = 2	37.3	metr	es.								Jul	y, 19	23.
1	Da	y.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
Proc. Proc	1	.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.
1	ł	2	989·1	988.6	988·0	987.6	987·I	986.5	986.3	986·1	985.6	989·7 985·3	989·9 985·0	989·9 984·7	990.0 984.4	989:9 984:2	989.8	989.6	989·5 983·0	989·5 982·6	989·5 082·3	081.8	989.6	989∙6 081•1	989.5	989·5 980·3	989.5
5 0000-0000-0000-0000-0000-0000-0000-00		3 l	979.9	979:7	979.2	979.0	978.9	978.7	978.6	978.5	978.4	978.91	979.2	979.3	979.3	979.6	979.8	980.3	980.4	981.0	981.2	981.8	982.3	982.7	083.1	083.3	1 · 080
Description Control		4	983·4 989·6	983·7 980·6	983·9 980·6	984.0	984.3	984.5	984.8	985·3 991·3	985·4	985.4	985·5	985.5	985.8	986.3	986.6	986.6	986.9	987.2	987.9	988.3	988.5	988.9	989.2	989.4	986.0
1		1							1 1			· '					ł				1	1	Į i		1		
Sept of purpose a purpose appears beginning to the purpose appears of the purpose appears		7	995.1	994·8 992·I	994.8	994.8	994.7	994.8	994.8	994·8 990·5	994°5 980°0	994°4	994'4 080'1	994.0 080.5	088·3	993.4	088.3	088.3	992·8 088·5	992·6 088·3	088.3	088.2	993.1	993·2	993.2	992·8	993.9
1		8 1	989.0	988.9	988.6	988.6	988.6]988.5	1988.6	988.6	988.9	989·I	989∙1	989.1	989.3	989.2	989.2	1.089	989.2	989.8	989.9	990.2	:1990.6	991.1	991.2	991.3	989∙4
The contract of the contract		9 10	991·2	991.0	991.0	991.0	991.0	991.1	991.0	991·0	991.7	991.0	991.0	991.6	991.7	991.7	991.6	991.6	991.6	991.5	991.5	991.5	991.9	992.0	992.1	992.1	991.5
1												·		ĺ	1		1					l	1		l		l
1	}	12	991.9	991.7	995.5	995.5	991.9	995.6	991.9	991.9	992.4	992.9	993·0 995·7	993.0	993·0 1995·8	993·0	993.2	993.3	993.6	993.7	993.9	994:3	994∙8 005∙0	995·0	995.3	995.4	993 0
Fig. 16	vel	13	990.1	990-1	1990∙0	995.9	995.9	990∙0	1990.1	996.4	996.2	996-3	996.2	995.6	995.6	994.6	1994:5	994.5	994.4	994.6	995·I	995.5	1996.2	996·I	996.0	996.1	1995-6
Fig. 16	Le	15	987.3	986.6	985.8	985.2	985·0	984.5	983.9	983.7	983.7	982.7	982.3	981.9	981.7	981.4	980.9	980.5	990.3	990.2	989.0	989.5	989.4	989·0	988.7	988·2 978·3	992.5
21			l			1	1	1				i			l		1	i					1				
21	tio	17	1978.9	978.7	978.5	1978.3	977.9	977.7	1977:7	977:6	977.6	977.4	977.4	977:5	977:3	977.7	977.6	977.9	978.0	978.1	978.4	1978-6	979.2	979.4	979.9	980.0	978.2
21	sta	18	1980.2	980.5	1980.5	1980.7	981.1	1981.6	1981.9	982.4	982.9	984.0	984.0	984.0	1984.7	1984.8	985.2	1985.3	985.8	i986∙0	986.3	1987.1	1987.4	087.4	1987.5	087.5	lo8a ∙c
2	97	20	984.6	984.3	984.1	984.4	985.5	985.9	987.2	988.3	988.5	988.7	989.0	989.4	989.6	989.8	989.7	989.7	989.2	989.0	988.8	988.8	988.9	989·0	988.9	988.9	987.8
2			1		l .	1	1		1	l					1			i			ì					1	
31		22	1993.0	992.0	4991.9	116611.9	1991.9) 992.c	1991.9	991.9	991.8	991.7	991.4	991.3	1990.9	990.5	99 0 +6	989.8	989.2	988.8	988.0	1987.4	1986.7	1.686	1985.0	083.3	1990-2
25 979 2 977 3 977 977 977 977 977 977 977 977 9	į	23	982.5	982.1	981.4	. 980•4	979.7	979.7	979.1	979.0	978.9	978.9	978.9	978.8	979.0	979.3	979.4	1979.4	979.5	979.6	980.0	980∙c	980.4	980.3	981.0	981.1	lo8o∙c
## 25		25	979.2	978.7	978.0	977.5	977.5	977.4	977.0	976.9	976.9	977.0	976.7	976.3	976.2	975.9	975.4	975.5	975.3	975.3	975.4	976.8	976.5	976.5	976.2	976·0	976.8
27 983 3083 3084 3084 3084 3084 3084 3084 3084 3085 308			1	[1	1	(1			l	ł	l	ł	l	1	1	ŀ	l	1	Į.	1	ļ	1	!	l
\$\frac{5}{2} \text{ 3.9 } 9.97 \text{ 9.977 \text{ 9.978 \text{		27	1983.3	983.3	984 1	1984.3	984.9	984.9	985.1	985.4	985.5	985.4	985.5	985.5	985·1	985∙0	984.6	984.2	983.6	983.4	982.8	982.5	982.2	981.2	980.5	979.5	984 • 0
30 90° 70° 70° 190° 190° 190° 190° 190° 190° 190° 19		28	978.5	977.9	976.8	970.5	975.8	975.3	975.1	974.7	974.3	974.2	974.0	974.0	973.8	973.7	973.6	973.5	973.5	974.1	974.8	975.0	975.5	975.6	975.8	975.8	975 1
Mean		30	970.7	970.1	970.1	970.0	970.1	970.5	970.5	970.6	970.8	970.6	970.6	970.6	970.3	969.8	969.6	969.2	968·5	973 7 967·9	966.8	966.1	965.5	972.4 964.9	964·I	963.8	969 0
Mem Set Post Po	\downarrow	31	963.5	963.4	963.0	963.0	963-т	063.4	063.8	064.1	064.3	064.3	064.3	064.3	063.0	064:0	062.0	062.8	062:4	062.5	062.5	062:6	062.7	064.2	064.2	064.8	062.9
Station level 12 13 68 65 65 75 63 40 80 80 80 79 71 70 75 40 80 33 35 50 72 72 70 35	Mean		-		·	 																					
118. Eskdalemuir H.D. = 237.3 mctrs.	(Station Mean	n level)		91	∙68	62	•65	1 .76	84	•90	88	-88	•86	.79	-71	-67	.56	49	-36	•43	.45	.56	74	.74	.69	54	.72
mb, mb, mb, mb, mb, mb, mb, mb, mb, mb,	(Sea lev	vel)	.53	.31	.09	.03	·6 ₄	1.10	.13	.10			•89	.78	.67			•46	∙34	.48	•56						
mb, mb, mb, mb, mb, mb, mb, mb, mb, mb,	118.	Eskda	alemu	iir : 🗎	$H_b =$	237	·3 m	etres	٠.															Α	ugusi	, 19	23.
3 90 - 190 -	1			mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	l mb.
4 992 992 992 1993 993 1993 993 1993 993 1993 1	-	2	980.4	980.6	980.4	980·0	900·4 979·7	909.0	909.8	979·4 979·1	971·2 978·2	972.2	972·9 976·0	974.1	974.4	975.1	975.7	976·5	977·3 966·3	977:4 064:4	978.1	978.8	979.8	980·1	980·3	980.4	973 3
5 9937 1993 5 992 6 991 5 991 5 991 5 991 5 991 5 991 5 991 5 991 5 991 5 991 5 991 5 998 5 988 6 987 5 987 6 987 6 987 6 987 6 987 6 987 987 2 987 2 987 2 987 8 987 6 987 6 987 6 987 6 987 987 2 987 2 987 2 987 9 8 987 9 987 6 987 6 987 6 987 6 987 6 987 9 987 1 987 2 987 2 987 1 987 1 987 2 987 1 987 1 987 2 987 1 987 2 987 2 987 1 987 2 987 2 987 1 987 2 987 2 987 1 987 2 987 2 987 1 987 2 987 2 987 2 987 2 987 2 987 2 987 2 987 2 987 2 987 1 987 2		3	1902.7	1904.0	1900.3	1908.3	970∙0	1971 0	1973:4	975.0	976.3	977.5	1978.6	070.7	1080·7	1081 ·a	1083.1	1984.2	1985.5	1986.7	1987:6	lo88•⊿	ıla8a∙2	900.2	990.7	T · TOO	078.4
0		5	993.7	993.5	992.1	993.0	993.5	994.2	995.1	995.2	995·4 989·9	995·6 989·1	995·3 988·5	995·3	995·3	995.1	995.0	995·0 2 987·1	995·0 987·0	995.0	995.0	994.9	994.8	994.5	994.3	994.0	994.4
9 98.7 08.4 16.8 1.1 08.2 16.8 2.3 16.8 2.3 16.8 2.3 16.8 2.3 16.8 2.3 16.8			i	1		ì		ì		1		1		ļ	i	1	į.	1	l.	1		1		1	1	İ	1
9 980 3 990 7 997 7 997 7 997 7 9987 3 9987 5 9987 9987 9987 9987 9988 9988 1988 1 9887 1 985 6 988 1 988 7 1 985 6 988		7	1984.7	984·I	1983.1	1982.8	1982.5	982.4	1982.3	982.1	982.0	982.1	982.1	982.1	982.1	982.4	1982.4	ıl982·5	982.6	983.2	1983-8	984.4	ıl985·5	985.7	1986∙ o	la86•6	082 - 2
11		8	1986.9	987.0	987.1	987.3	987.3	3 987:5	987.9	987.9	987.9	988∙0	988∙c	988.1	988·1	1987.8	3 987.4	ı 986∙9	987.0	987.1	1986-9	986∙0	987.0	986•6	l986·8	986·4	087.3
TI		10	989.8	990.1	990.1	9901	990.2	990.7	991.2	991.6	905.3	992.5	992.5	992.5	900.5	980.7	993.2	993.1	993.2	993.2	993.9	994.4	1994.4	994.6	994.9	989.7	986.8
12 995/997/1997/0909/999-15990-4905/9905/3905/3905/3905/3905/3905/0907/0907/9907/9907/9907/9907/9907/9			1	f		1		1	1	ĺ	1	í		ì	1	ł	l	1	1	i	}	Į	1		l	1	j
13		12	1990.9	997.1	1997.0	1990-9	1996.5	5 996+4	H995·9	996.3	1995.8	995.3	994.4	994.5	994·I	993.7	1993.7	7 993.2	1992.8	992.3	991.7	991.6	991.4	991.0	990.1	000.1	004 - 3
16	ve	13	1909.0	909.0	1900.5	1907.0	907.1	. 1980-4	980·4	986.2	1986-1	985.9	986.2	1980-5	1 987•0	987.2	2 987.9	9 98819	1989:3	1989.9	990-6	991.2	991.4	992·I	992.4	992.5	lg88+5
16	Le	15	992.4	992.3	991.9	991.2	991.3	991.3	991.5	991.3	993.7	991.0	994.1	993.5	990.2	990.1	989.8	990.0	989.8	989.7	992.0	990.2	992.0	992.0	990.8	992.0	993 • 1
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20 981 3 980 8 980 3 980 1 979 9 980 0 980	tio	17	1981.4	1979 9	978.0	1976.7	974.9	973.6	972.9	972.2	971.8	971.5	071.5	971.1	971.1	970.7	070.3	3 970.2	969.9	060.0	a6a•a	070-2	1970.3	970.2	070.2	070.0	072 . 7
20 981 3 980 8 980 3 980 1 979 9 980 0 980	Sta	10	1909.9	1909.9	1909.7	4909.0	1909.4	H909 :	51969-9	970.2	970.5	971.0	971.0	971.8	972.7	973.5	1974.4	1975.0	975.9	976.6	977:3	1978-6	979.1	979.6	980.2	080.3	073 - 3
21 971 0 969 5 967 7 966 7 966 7 966 7 966 7 966 7 966 7 966 7 966 7 967 5 967 967	Ĭ	20	981.3	980.8	980.3	980·1	979.9	980.0	980.0	980.0	980.0	980.0	979.7	979.5	979 4	979 1	978.6	977.9	977.7	977.4	976.6	975.9	975.3	974.7	973.6	972.3	978.5
22 907:2906:9907:2907:3907:5907:6907:3907:5907:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6977:1977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6977:1977:6971 977:5977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6977:9971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:6971 977:5977:9971 977:5977:9971 977:5977:9971 977:5977:9971 977:5977:9971 977:5977:9971 977:5977:9971 977:5977:9971 977:5977:9971 977:5977:9971 977:5977:9971 977:5977:9977:9971 977:5977:9977:9977:9977:9977:9977:9977:			1		1	1			1	l	1					1		1	ĺ	ļ	ļ	1	1			-	ı
973-9978-978-978-978-978-978-978-978-978-97		22	907.2	1900.9	1907.0	1967:2	907:3	3 907:5	5 967.7	968.3	968.7	968.8	969.3	96g·g	970.5	970.8	3 971 2	2 971.2	971.6	972.6	973.5	974.2	974.7	975·I	975.6	975.9	070 • 4
25 9637 9837 984 2 984 2 984 2 984 1 984 0 984 5 984 3 983 8 983 2 982 5 981 8 980 6 979 8 978 5 977 3 976 0 974 5 973 6 973 1 972 6 971 9 971 6 980 2 2 2 2 2 2 2 2 2	1			1470.0	1970.5	1970.0	1970.7	7 977·C	977.1	977.5	977.6	977·I	977.3	977.2	1976.3	975.7	7 974 4	1 972 6	971.1	1969.8	968.7	1968∙0	1967.7	967.4	967.0	la66∙a	1073 • 0
26 971 7 971 2 970 8 970 4 970 4 970 0 969 9 969 8 969 2 968 8 968 5 965 5 965		23 24	1000.0	1000.0	1900.7	(1900.0	90/3			,	1-1-1	ء جيرا	1717 -	176	681.8	980.6	979.8	978.5	977.3	976.0	974.5	973.6	973.1	972.6	971.9	971.6	980.2
27 900-5		23 24	1000.0	1000.0	1900.7	984.2	984.1	984.0	984.5	984.5	984.3	983.8	983.2	982.5	1	1-									1		
29		23 24 25 26	983·7 971·7	983.8	984.2	984.2	970.4	984.0	984.5	984·5	969.8	969.2	983.2	968.6	968.5	968.5	968.2	967.5	 967∙4	967.1	967.2	967.2	966.0	966∙a	966.8	966-8	968 • 0
30 900		23 24 25 26 27	983·7 971·7 966·8	983·8 971·7 966·8	984·2 971·2 966·5	984·2 970·8 966·3	970·4 966·2	984·0 1970·4 1966·0	984·5 1970·0 965·9	984·5 969·9 965·9	969·8 965·8	969·2	983·2 968·8	968.6	968·5 965·4	968·5	ւ 965∙≎	3 965.2	l965•o	964.9	965.1	965.6	1.666	966·1	966.2	l966∙3	1965 • 8
Mean (Station level) 980 980 980 980 980 980 980 980 980 980		23 24 25 26 27 28 29	983·7 971·7 966·8 966·7 980·3	983·8 971·7 966·8 966·9 980·5	984·2 971·2 966·5 980·4	984·2 970·8 966·3 967·0 980·4	970·4 966·2 967·1	984.0 970.4 966.0 967.6	984·5 970·0 965·9 967·9	984·5 969·9 965·9 968·5	969·8 965·8 969·1	969·2 965·3 969·7	983·2 968·8 965·4 970·1	968·6 965·4 971·1	968·5 965·4 972·0 973·6	968·5 965·4 973·2	965·3 973·9 971·8	965·2 974·7 8970·6	965·0 975·8 969·5	964·9 976·7 968·2	965•1 977•4 967•1	965·6 978·3 966·3	966·1 979·1	966·1 979·8 965·3	966·2 979·9 965·3	966·3 980·3 965·8	965·8 972·2
(Station level)		23 24 25 26 27 28 29	983·7 971·7 966·8 966·7 980·3	983·8 971·7 966·8 966·9 980·5	984·2 971·2 966·5 980·4	984·2 970·8 966·3 967·0 980·4	970·4 966·2 967·1	984.0 970.4 966.0 967.6	984·5 970·0 965·9 967·9	984·5 969·9 965·9 968·5	969·8 965·8 969·1	969·2 965·3 969·7	983·2 968·8 965·4 970·1	968·6 965·4 971·1	968·5 965·4 972·0 973·6	968·5 965·4 973·2	965·3 973·9 971·8	965·2 974·7 8970·6	965·0 975·8 969·5	964·9 976·7 968·2	965•1 977•4 967•1	965·6 978·3 966·3	966·1 979·1	966·1 979·8 965·3	966·2 979·9 965·3	966·3 980·3 965·8	965·8 972·2
Mean (Sea level) 1008		23 24 25 26 27 28 29 30	983·7 971·7 966·8 966·7 980·3	983·8 971·7 966·8 966·9 980·5	984·2 971·2 966·5 967·0 980·4	984·2 970·8 966·3 967·0 980·4	970·4 966·2 967·1 979·7	984.0 970.4 966.0 967.6 979.7	984·5 970·0 965·9 967·9 7979·0	984·5 969·9 965·9 968·5 978·8	969·8 965·8 969·1 977·8 973·1	969·2 965·3 969·7 976·9 973·5	983·2 968·8 965·4 970·1 976·2 974·0	968·6 965·4 971·1 975·4 974·7	968·5 965·4 972·0 973·6 975·8	968·5 965·4 973·2 973·0 975·9	973·9 973·9 971·8 976·5	965·2 974·7 970·6 976·4	965·0 975·8 969·5 976·7	964·9 976·7 968·2 977·1	965·1 977·4 967·1 977·4	965·6 978·3 966·3 977·7	966·1 979·1 965·7 977·8	966·1 979·8 965·3 977·7	966·2 979·9 965·3 978·2	966·3 980·3 965·8 978·2	965·8 972·2 973·9 973·8
G.M.T. I. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. Noon 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. Mean	Mean (Station	23 24 25 26 27 28 29 30 31	983·7 971·7 966·8 966·8 966·8 978·2	983.8 971.7 966.8 966.9 980.5 978.1 980	984·2 971·2 966·5 967·0 980·4 968·7 978·0 980	984·2 970·8 966·3 967·0 980·4 969·4 977·9	984·1 970·4 966·2 967·1 979·7 970·2 977·9	984.0 970.4 966.0 967.6 971.1 977.9	984·5 970·0 965·9 967·9 7979·0 971·5 977·8 980	984·5 969·9 965·9 968·5 978·8 977·8 977·8	969·8 965·8 969·1 977·8 973·1 977·8	969·2 965·3 969·7 976·9 973·5 978·2 980	968.8 965.4 970.1 976.2 974.0 978.2	968·6 965·4 971·1 975·4 974·7 978·1	968·5 965·4 972·0 973·6 975·8 978·1 ———	968·5 965·4 973·2 973·0 975·9 978·3	965.3 973.9 971.8 976.5 978.3	965·2 974·7 970·6 976·4 978·5 980	965.0 975.8 969.5 976.7 978.7	964·9 976·7 968·2 977·1 978·9	965·1 977·4 967·1 977·4 979·3	965.6 978.3 966.3 977.7 979.6	966·1 979·1 965·7 977·8 979·8	966·1 979·8 965·3 977·7 980·1 980	966·2 979·9 965·3 978·2 980·2	966·3 980·3 965·8 978·2 980·4 981	965.8 972.2 973.9 973.8 978.5 980
1 3 4 5 7 6 9. 10. 11. Noon 13. 14. 15. 10. 17. 16. 19. 20. 21. 22. 23. 24. Integr	(Station Mean	23 24 25 26 27 28 29 30 31	983.7 971.7 966.8 966.7 980.3 966.8 978.2 980 •46	983.8 971.7 966.8 966.9 980.5 978.1 980 .40	971·2 966·5 967·0 980·4 968·7 978·0 980 •30	984·2 970·8 966·3 967·0 980·4 969·4 977·9 980 •25	970·4 966·2 967·1 979·7 970·2 977·9 980 •24	984·6 970·4 966·6 967·6 971·1 977·9 980 •30	984·5 970·0 965·9 967·9 971·5 977·8 980 •42	984·5 969·9 965·9 968·5 972·3 977·8 980 •55	969·8 965·8 969·1 977·8 973·1 977·8 980 ·59	969·2 965·3 969·7 976·9 973·5 978·2 980 •58	983·2 968·8 965·4 970·1 976·2 978·2 980 ·52	968·6 965·4 971·1 975·4 974·7 978·1 980 •60	968·5 965·4 972·0 973·6 975·8 978·1 980 •67	968·5 965·4 973·2 973·0 975·9 978·3 980 -73	973.9 971.8 976.5 976.5 978.3 980 .74	965.2 974.7 970.6 976.4 978.5 980 -63	965.0 975.8 969.5 976.7 978.7 	964·9 976·7 968·2 977·1 978·9 980 ·62	965·1 977·4 967·1 977·4 979·3 980 •69	965.6 978.3 966.3 977.7 979.6 980 .81	966·1 979·1 965·7 977·8 979·8 980 •92	966·1 979·8 965·3 977·7 980·1 980 •97	966·2 979·9 965·3 978·2 980·2 981 •00	966·3 980·3 965·8 978·2 980·4 981 •00	965.8 972.2 973.9 973.8 978.5 980 .60
	(Station Mean (Sea le	23 24 25 26 27 28 29 30 31 n level)	983.7 971.7 966.8 966.8 980.3 966.8 978.2 980.46	983.8 971.7 966.8 966.9 980.5 978.1 980 ·40 1008	984·2 971·2 966·5 980·4 968·7 978·0 980 •30 1008	984·2 970·8 966·3 967·0 980·4 969·4 977·9 980 •25 1008	970·4 966·2 967·1 979·7 970·2 977·9 980 •24	984.0 970.4 966.0 967.6 7979.7 971.1 980 30 1008 78	984·5 970·0 965·9 997·9 971·5 980 •42 1008 81	984·5 969·9 965·9 968·5 972·3 977·8 980 •555	969·8 965·8 969·1 977·8 973·1 977·8 980 •59	969·2 965·3 969·7 976·9 973·5 978·2 980 •58	983·2 968·8 965·4 970·1 976·2 978·2 980 ·52 1008	968·6 965·4 971·1 975·4 974·7 978·1 980 •60	968·5 965·4 972·0 973·6 975·8 978·1 980 •67 1008	968·5 965·4 973·2 973·0 975·9 978·3 980 -73 1008	965:3 973:9 971:8 976:5 978:3 980 -74 1008	978·5 978·5 978·5 978·5 980 •63	965.0 975.8 969.5 976.7 978.7 980 .63	964·9 976·7 968·2 977·1 978·9 980 ·62 1 c 08	965·1 977·4 967·1 977·4 979·3 980 •69 1008	965.6 978.3 966.3 977.7 979.6 980 .81	966·1 979·1 965·7 977·8 979·8 980 •92 1009 •33	966·1 979·8 965·3 977·7 980·1 980 •97	966·2 979·9 965·3 978·2 980·2 981 •00	966·3 980·3 965·8 978·2 980·4 981 •00 1009	965.8 972.2 973.9 973.8 978.5 980 .60

Readings in millibars at exact hours, Greenwich Mean Time.

Eskdalemuir: H_b (height of barometer cistern above M.S.L.) = $237 \cdot 3$ metres.

September, 1923.

119.	Eskda	lemu	ir : I	\mathbf{I}_b (h	eight	of ba	arome	eter c	eisteri	ı abo	ve M	.S.L.	=23	37.3	meti	es.							26bt	embe	r, it	723.
D	ay.	ı.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
		mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.
	I 2	088.4	080.1	1080.0	1000.5	001.1	ιΙοοτ •6	002:5	1003.0	003.6	004.3	004.4	1994.7	1994.8	995.1	995.3	1995 4	1995 9	1990.0	997.2	1997'9	1990.01	990.1	990.4	1990.2	983·3 994·1
-	3	1008.5	008.5	1008.5	1008.1	- 008.5	1008.5	008-4	1008.3	007.8	006.4	1006.3	005.7	005:3	004.0	994.7	994.2	1993.0	1.693	992.7	992.4	991.7	990.9	990.2	90912	1995.5
į	4 5	988.0	987.2	986.7	1986.7	7 986·7 7 990·2	7 987·2 1 990·4	987.8	988.4	989.2	991.8	991.8	991.1	993·1	993.2	993.0	993.5	992 /	993.2	993 4 994 · I	993 °	994.2	994.3	993.8	994.4	990·6 992·5
	6	004.8	005.1	005:0	005:3	005:3	005.3	005.3	005.5	005.6	005.6	005.6	004.8	004.4	994.1	993.8	992.7	992.4	992.1	991.7	991.6	990.9	990.7	989.8	989.3	993.7
	7 8	1000.	1088.5	1088.5	$\alpha \times \alpha \times \alpha$	1080.1	1000.6	COOT • 2	I COO T	1002.7	003.2	10004 • 0	ноол• г	CKIA:A	DOM: U	1005.0	IUUS S	995	1990 0	990 /	199/ 1	991	99/ 9	1990 1	1990 4	1777
	8 9	000.7	080.0	1088.6	1088.0	1087.	1087.	087.4	1087.2	087.0	087.0	lox6·f	1080.3	IOX6+2	loso o	lo8b•o	laŏ5∙a	1.000	dou.o	907.3	1907.0	1000.1	90072	900.3	900.3	995·6 987·4
	10	988.3	988.3	988-2	987.8	987.8	987.8	988-2	988.6	989.2	989.8	989-8	989.6	989.5	989.5	989.4	989.2	989.4	 989.3	909.1	909.3	909.7	909.7	909.0	909.5	1909.0
	11	988.8	988.1	987.5	986.8	986.1	986.1	985.6	985.3	985∙0	984.1	983.6	983.0	982.5	981.5	979.9	979.9	979.9	978.9	978·0	977.7	977.6	977:3	976.9	976.5	982.6
vel	* ^	1080.0	In Sair	LOST.C	JOSTIF	NOXT 10	NOSOF	IOXO+h	100004	1070.0	070.2	078.0	11075.0	077.4	1070 7	14.70.0	47/51	9/4 1	9/3/	1913 7	19/3 1	9/4 0	9/1 .)	910 9	17/ J	97 7 ·4
Le		1060.0	060.6	1060.6	1060.5	1060.5	1060.	1060.8	$0.060 \cdot 0$	070.2	070.6	1070 - 5	1070.5	070.0	1070.0	1970.5	1970.0	1970.4	1970.9	1970.9	1971.4	971.4	971.4	9/13	9/10	970·4 971·1
Station Level																										
ati																										977·8 970·5 965·3
St	-0	060.	1060.4	1062.	1060.0	1062.2	1062.5	062.7	Chart	$004 \cdot 1$	002.0	1002.0	HODATE	004.5	Q05.0	11005.0	IUO5 5	9057	1900.4	190/3	1907 9	9000	1909 0	19/03	1970 0	1000 0
	19 20	971·3	972.0	972.0	973.1	973·3 969·6	969·0	968.5	968.5	968.5	969·1	969.8	973.0	971.7	973 2	974.2	974.5	974.8	975.2	975.1	974.6	974.0	973.4	972.7	972.2	972·5
			060.=	060.0	060.2	068.0	068.8	060.1	060.2	060:4	070.5	071.1	071.5	072:0	072.4	972.6	072.8	973.0	973.3	973.5	973.9	973.7	973:3	972.7	971.2	971.4
	2 I 2 2		ACO 0	A6 m. m	1066.9	066.	1066.	067.0	067.0	067.0	000.6	のわわ・た	John h	10hh • 5	aoo	lonn.o	1005 · 0	1905.0	1405.2	1905.2	1905.5	905 4	1904 9	1904 0	1904 4	H9CC J
				0 = 4 . 0	0000	075.5	1076.6	IOTA N	077.3	1077.4	077.8	אידדטו	11077710	(177.7	10777.4	1077.7	10 /O U	19707	14/01	19/7 0	19/4 9	1917	19/20	19/1	1272 1	3 967 · c 3 975 · 7 5 064 · c
	25	968.3	966.3	965.3	964.7	964.4	964.1	964.1	963.7	903.5	903.1	903.1	903-1	903.1	903.0	902-9	903.0	903.0	903 2	903 /	904 0	900 3	900 9	,,,,,,,) 3/- \	1
	26	973.5	975.7	976.5	977.6	978.9	980.0	980.8	982.2	983∙0	984.3	985.2	985.6	986∙1	986.9	987.3	987.7	988.2	988.8	988-9	989.8	990·I	990.2	990.3	990.4	4 584·1
	27	990.3	990.3	990.1	990.0	989.9	989.8	989.5	989.7	989.8	989.5	988.7	988.1	987.4	900.7	900.4	900.0	900.4	900.0	905 9	996.7	996.7	997.1	997.1	997	2 991 · 2
																										997·6
		997.1	990.0	990.8	990-3		990-1		·					1	·				1		982	982	982	982	982	981
Mean (Statio	on level)	981 •55	.26		981	980	· 15	1 .28	981 981	.78	•от	981 •92	. ∙88	-08	.03	981 •84	981 	.89	982	. 09	.24	.23	.24	15	; °08	8 .75
Mean	911 10 (01)	1010	1010	1009	1009	1003	1009	1010	1010	1010	1010	1010	1010	1010	1010	1010	1010	1010	1010	1010	1010	1010	1010 ·88	1010	1010	1010
(Sea le		•24				·64		•08	•22	•27	*34	•30	.21	•29	•24	. •15	15	20	1 31		1 04	1 0		<u>-</u>		
120.	Eskda																				1	Land		ctobe		
1	7	.00.4	000.1	088.5	1088.3		ロヘスケ・ス	OXX · E	IOXX • E	IOXX · F	088.7	IOXX**	വരവെ	T•osoi	ioso·i	1080.2	luou-2	1000.1	1404.4	1909.3	1909.3	1900 0	1900 1	1901)	1900 -	mb. 1988 · 7
	_	00 = . =	08	082.2	108T-6	JOSO - E	ปกหลาก	IOXT •6	10X5.0	OX5 · 2	$080 \cdot T$	108b-1	1080.2	IOSO:4	1000.	ordoul.	1400.5	1900.2	1900-5	11900.3	1900 1	1905 4	1904 9	1904 0	1200	984 · 9 979 · 6 1 990 · 2
		06	087.0	OXM.b	LOXX.2	LOXX:0	IOXO.7	1000.7	100T • 2	OOT O	CHOIL: CO	(M) 1 *C	บดดาเด	K3O 1 *7	IUU I "	1001 7	1991.4	GGT 3	1991 7	1991	1990 0	1990 3	1220 -	12-2 -	10-0 "	
	5	988.3	987.4	986.5	985.7	985.0	984.5	983.9	983.4	982.8	981.9	981.0	979.0	979.5	970.9	978.0	977.8	9/7/	9///	9// 9	970 1	9703	970 3			
		978.4	978.1	977.9	977.8	977:7	977.5	977.3	977.0	976.8	977.1	977:1	977.2	977:4	977.7	978.1	978.4	978.8	979.4	979.7	979.9	980·0 973·0	980.3	980.6	980.7	7 978·3 9 976·4 3 975·7
	0	~~	075.0	075.2	076.4	ロハクハ・ち	1077.0	1077.5	1078.2	1078.2	078.5	1078:5	3U70*7	1070 3	1070.5	10//01	14//4	1470.0	19/7 6	1910	1910 4	1910 1	19100	7200 7	7-1	11/1/
	_	066.6	1066.6	1065.7	066.2	けいわフ・ク	けいいフ・ク	IODX • 5	പറവവംവ	1000.7	070.7	1071 2	5071.0	1072.7	107335	14741	14/5 4	19/59	19/0 /	19// 4	1970 -	12/2 *	1717	12 1	J	972·4 976·3
ļ				1	1		1	1	!	1		1				1	1	1	1	1	1	4	1	1	1	976.8
/el	13	957.0	957.0	957.0	957.1	957.5	958.2	959.5	900.7	901.9	902.8	903.0	904.4	075.1	075.3	900.3	907.0	976.8	977.5	978.1	978.5	979.0	979.4	979.4	979.9	974.9
Le	15	980·0	980.3	980.4	980.6	980.7	981.0	981.2	981.4	981.8	981.7	981.7	981.7	981.6	981.5	981.3	981.2	981.2	981.2	981.2	981.1	981.0	980.5	980.0	979:5	5 981·c
Station Level	16	979·3	978.9	978.5	978.3	978.4	978.6	978.8	979.2	979.9	980.2	981.3	981.8	982.2	982.9	983.5	984.1	984.7	985.5	986.4	986.4	986.4	986.7	986.5	986.2	2 982 · 1 7 989 · 1
ati	17	986.2	985.7	985.6	985.7	980.2	1980.7	088.6	088.4	088.0	088.0	087.5	086.4	1990.0 1084.8	083.2	982.0	081.0	979.9	978.9	977.6	976.9	976.3	975.7	975.1	974.1	984.1
-St		~ ~ ~ ~	A=+.0	060.0	1068.0	lobb.c	106 4 17	100 4 · X	1000.2	1007.2	002.2	$10000 \cdot 4$	11070.0	1070.0	107110	10/72:5	10/20	14/30	19/4 7	19/3	197.) 4	19/1/4	1213 3	1217 2	17/T v	969.5
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	24 25	944°4 948°1	944.0	944·9 949·1	945.1	950.3	945.7	952.2	953.2	954.4	947.2	947.3	955.7	955.9	955.9	956.2	956.5	957.3	958.5	959.3	960.0	960.6	961.2	962·0	962.6	955.1
	26	062.4	061.0	061.2	050.8	058.7	057.1	055.6	055.4	054.8	056.2	056.6	057.2	057.4	057:0	058.5	050.6	960.8	961.7	962.4	962.6	962.6	962.5	962.0	961.5	959.5
	27	960.4	957.7	950.4	954.4	953.0	951.9	951.0	952.2	952.5	953.2	953.1	953.1	952.9	062.0	063.3	063.0	951.0	951 0	950 9	965.5	966.0	966.7	968.8	969.4	1960.4
		070.4	1071.7	1077.2	1072.3	1072 U	11074.0	1074.7	1075.4	1075.0	1070.7	070.0	いいづい・ハ	いつフェ・コ	1074 5	10731	10730	9/29	9/4 9	9/20	191- 2	1713 -	12/3 -	171-1	171	7775
	30	972.9	972.9	971.0	971.0	970.3	970-2	970-2	970.5	970.8	971.7	972.4	∮ 973°3	973.7	973.9	974.0	975.2	970.0	970 7	9700	9// 1	911 3	311 9		177	7,3
\downarrow	31	979.6	980.1	980.6	981.3	981.9	982.6	983.8	984.5	985.6	986.7	987.1	987.4	987.7	988.1	988.7	989.2	989.8	990.4	991.1	991.5	991.8	992.3	992.6	992.9	986.7
Mean		971		971					971		971	971	971	971	971	971		971		972	972	1	972		972	97I 2 ·71
(Statio	on level)	·82			999		∙65 ⊎⊎⊎			999	1000	1000	1000	·8 ₅	92	≥ .84	ր ∙8Ն		1000				1000	1000	1000	1000
(Sea le	<u>.</u> .	.41				•23		•38	.74	.89	.19										95	.92	-98		7	7 .21
G.M	A.T.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mear
		l			1	<u> </u>	<u> </u>	<u> </u>	<u> </u>	1			1	<u> </u>	<u> </u>	1	1	1	<u> </u>	1	1	1	ـــــا۔		1	<u></u>

Readings in millibars at exact hours, Greenwich Mean Time.

121. Eskdalemuir: H_b (height of barometer cistern above M.S.L.) = $237 \cdot 3$ metres.

November, 1923.

Day.		oiiiaii	• 11	o (Hei	8111					abo	V C 111.	J.1.,			meur	CS.									r, 19	
		I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
<u></u>		mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.
	1	003.0	003.2	003.1	393.1	993.1	993.0	993.0	993.0	992.7	992.7	992.1	991.2	990.6	990.1	989.4	989∙o∣	988-6	988.4	988·o	987:4	987.0	986.7	986.5	980.1	990.0
	2	985.8	985.6	985.2	985·1	985.3	985.6	985.9	986.2	986.5	986.4	986.3	985·9	985.4	984.5	984.3	983.9	983·7 068·5	982·8 967·9	981.3	979·9 067·8	978.0	970.4 968.1	974.7 968.0	972.9 968.2	967.4
	4	068.2	a68∙s∣	a68∙7l¢	a68∙6	968.6	968.2	968.5	968-6	968.7	969.3	969.8	970·1	970.7	970.6	970.5	970.5	970.6	970.8	971.0	97 1·1)	970.7	970.9	971.0	971.2	909.7
	5	971.1	971.0	971.1	970.7	970.8	970.9	970.8	971.1	971.0	97Í·2	971.2	971.1	971·0	970.9	970.7	970.6	9 70 ·6	970.9	971.1	971.4	971.5	971.6	972.2	972.3	971.1
		073.3	073.0	073.	072.6	074.3	075.1	075.8	076.7	077.0	078.2	078.=	070.2	070.5	070.7	980-т	080.4	იგი-8	981.0	_{281.} ₄	081.5	₉ 8τ-6	982·0	982.0	982.1	978.1
	7	082.1	082.11	082.1	a82·1	982.3	982.7	982.8	983.44	983.21	983.1	983.1	983.1	982.9	982.8	982.6	982.5	982.5	982.5	982:2	981.9	981.7	981.0	980.2	979.0	902.4
	8	070.1	a77·61	977.0	976·0	975.0	973.7	973·I	972.7	972·I	971.6	971.3	970.9	970.6	970:3	970·I	970.0	969.9	969.9	969.7	909.7	969.3	969.3	968.6	908.0	972.2
	0	la68·51	968:4	968·sh	968·9	969.7	970.8	971.7	972.7	973.8	974.5	975.2	977:0	979.6	980.5	982.4	984.0	985.6	987.0	988.7	990.2	991.5	992.5	993.0	994'4	979.0
I	10	995.1	995.0	990.4	997'1	997.9	990.7	999.3	999.7	000-0	000-8	000.0	000-7	000.0	000-4	000 4	000 0	000 0	999.9	999 0	999 9	999 3	999 3	999 1	990 0	-
1	11	998-1	997.5	996.9	996.4	995.8	995.8	995.5	995:3	994.0	994.1	993.3	993.0	992.2	991.3	990-1	989.5	989∙0	988.3	987.8	986.7	986.4	985.7	984.5	984.4	992.0
<u>.</u>		000.4	080.01	080.71	070.8	078.5	077.4	077.4	077.46	076.8	075.3	075.5	071.2	072.0	072.0	074.4	$074 \cdot 61$	ハクエ・クロ	975·6	フクロ・ロル	075.71	075 21	075.2	074.51	u73'01	970.7
Š,	13 14	045.8	970.5	909.1	900.0 048.5	904.1	950.7	952.0	950.0	950.3	953.1	950.0	950 4 954 I	953 3 954·3	955.0	957.5	958.8	959·9	961.3	962.9	964.1	965.2	965.9	966.1	966.6	955.7
н ;	15	966.9	967.0	965.7	966·I	964.8	963.0	961.3	959.9	957.5	954.4	950.2	947.1	945.9	944.4	943.0	942.2	942.1	941.3	941.1	941 2	941.5	942.5	944.7	946.5	952 · 1
6			- 1	i		ı	i l		- 1												İ	1				
ati	T7	050.1	058·7l	058·5l	058·0	058.4	958.2	958·3	958:74	959.6	962.5	963.5	964.51	965.0	966.0	966+5	900.7	967.1	966·2 967·2	907:71	907:71	907.9	900.0	900.1	900.2	1903.31
St	т8	la68·2	967·9	967.81	967.6	967.6	967.4	967.3	967:3	967.5	967.6	967.5	967:6	967.6	967.7	967:6	967.6	967:5	967.6	367·61	968.0	968.5	908.8	909.5	970.5	907.9
	TO I	970·I	970·I	970.3	970.7	971.0	971.7	971.9	972.4	972.7	973·I	973.1	973.2	973.5	973:4	973.3	973.5	974·I	974.219	974 1	974 • 1	973:91	972.9	972.9	972.0	972.0
2	20	972.4	972.4	972.1	972.1	971.8	971.7	971.6	971.0	972.0	972.2	972.2	972.2	972.0	972.9	973.4	974.0	974.2	974.7	9/5 2	9/5.9	9700	970 1	970 /	970 /	9/3 4
2	21	976.7	977.2	977.2	977.2	977.2	977:3	977:3	977.5	978-2	978.3	978.2	978.1	978.1	978.1	978.0	978·o	978.1	978.3	978.6	978.6	978.7	979.0	979.1	979.2	978.0
2	22	070.2	070.4	979.6	070.8	0.080	080.5	08T O	081.8h	082.2	082.8	083.0	983.0	982.8	982.9	1983.0	983.1	983.31	983.06	303·71	905.7	903.0	904.1	904.1	904.2	972.2
	23	984.2	984.2	984.3	984:2 000:8	984.2	984.2	984·2	984.8	985.0	985.4	902.2	905.8	902.2	900.3	900.2	900.9	907.1	987·6 991·7	991.6	900.3	991.2	990.8	990.6	990·2	991.3
	24 25	989.8	989.4	988.8	988·5	988.0	987.4	987.1	986.8	986·7	986.7	986.7	986·1	985.6	985.1	984.8	984.3	984.3	983.8	983·6	983·2	98 3 ·1	982.9	982.6	982.3	985.9
			i	1			1 1	i			i .								1		1					
	26	982.1	981.8	981.6	981·I	080.6	981.0	981.0	981.0	981·5	981.7	981.4	981.2	082.0	980.7	082.0	980.6	980·6	980·6 982·9	183.1 (982.1	983.1	983.1	983.0	982·8	981.8
	28	082.6	082:41	о8т•иЬ	080.7	а⊗о∙т	1070·01	070·81	070.86	070.8	070.6	070·I	978.6	078.4	977.91	1977.81	977.01	977:51	977:51	۲77'7ا€	977:31	977'31	977.1	977.0	977.0	979.0
	20	076.7	976.7	070.7	976.7	1076.6	077·I	077.5	077.86	978.4	078·0	070.2	979.7	1980.0	980.21	081.3	982:21	982:5	983.516	903.0k	903.91	904.2	904.9	905.01	900.2	900.2
↓ 3	30	986.4	986•9	986.9	986.8	986.8	987.4	987.4	987.6	987.7	987.8	987.7	986-9	986.1	985.9	985.5	984.9	984.2	983.5	983.1	982.6	982.0	981.5	981.1	981.0	985.4
lean		976	976	976	976	976	976	976	976	976	976	976	976	976	976	976	976	976	976	976	976	976	976	976	976	976
station le	evel)	.64	.58	.43	•36	.27	·24	31	.46	.62	·76	.71	.57	.53	.47	.50	.54	.64	.68	.72	.62	.51	•42	·41	•40	•52
ean		1005	1005	1005	005	1005	1005	1005	1005	1005	1005	1005	1005	1005	1005	1005	1005	1005	1005	L005	1005	1005	1005	1005	1005	1005
ea level))	.91	·85	.71	.65	.57	.53	.59	.74	.85	·94	·84	-651	•59	.53	·65	.69	-85	.911	. 9 0	·89]	•791				
22. Es	skdal			-																				embei		
	- 1	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.
1	1	980.6	980.1	979.9	979:7	979.6	979.6	979.6	979.6	979.6	979.1	978.8	978.1	977:5	975·8 062·1	970.0	975.4	974.7	973·8 963·6	9/3.4	964.5	964.7	965·I	965.2	965.3	962.0
	2	065.75	obboo!	ინნაუს	ინნავ	066.2	066.7	067.6	のんお・まし	$000 \cdot T$	070 · I	070.4	070.6	070.7	071.0	071.4	971.7	972.4	972.7	972.0	9/2 /	1974.4	9/4/	9/13	9707	909.7
	4	laha•8:	obo•ol	007·6!	$000 \cdot 4$	Q05.1	1004.3	003.21	002.4	001.4	lahata	ODO: I	058.0	057.0	957.2	Q57.1	1950.91	9507	957 1	957 31	95/ 9	930 /	939 2	1939 0	900 0	DOT O
	5	961.2	961.7	962.3	963.2	964.0	965.1	965.9	967.1	968.3	969.9	970.4	971.3	972.4	973.1	974.3	975.5	970.5	977.7	970.7	979.9	900.5	901.2	901.0	901.9	971.4
	6	982.3	983.4	984.1	984.3	984.7	985.2	985.9	986-1	986.5	986.7	986.8	986.5	985.9	985.9	985.7	985.3	985·o	984.6	984-1	983.4	982.9	982.2	981.2	980.4	984•6
	7	070.3	078·0!	976.81	075.4	074.2	073.4	072.6	071.5	070.4	loho•X	1068-6	007.0	1005.2	004.0	1903.5	902.0	001.0	900.0	950.91	950 3	1957 7	193/ 4	1937 *1	951 0	190/ 1
1	х :	0.56.21	055.6	055.0	054.4	054.0	054.1	055.1	056.6	$0.5 \times .0$	1060 · T	062.2	062.5	064.7	065.8	007.2	1008.3	909.4	970·6 984·7	971.0	9731	1974.0	19/4 0	19/0 41	9/0 1	1903.0
	9	970.7	977'4 083:2	083.4	979:3 083:6	983.7	083.0	901.3	984.7	084·8	085.3	085.4	9°4'3	9°4°5	985.8	986.6	986.9	987.4	987.8	988.0	988·o	988.7	989.2	989.2	989.4	985.9
		1		i				i l			1	1	1	1				i		i i		1	1	1	l .	l .
1	11	989.4	989.7	989.9	989.9	990.3	990.4	990.4	990.3	990.7	990.5	990.9	990.9	990.7	990.7	991.2	991.4	991.2	991.4	991.3	991.1	991.2	990.7	990.7	990.7	990.0
	т э	001.2	$T \cdot T \cap \Omega$	OOT O	0.100	loot to	1002.6	002.5	004.7	006.2	1008-6	1008.0	0.00	1000.2	$1000 \cdot 2$:I000+3	1.100	1001.7	991.0	001.0	001.9	002 2	002	1002 3	OO1 4	1997 3
, VE	7 4	201.2	000.3	$\alpha \alpha \cdot x $	000.2	InnX-h	007.2	0000.7	002.2	$10000 \cdot T$	005.2	004.4	002.2	1000.5	0.000	บอออาร	1080:4	1050*3	1909.71	990.0	9900	199- 3	199~ -	199- /	1994 9	1994
Le	15	993.0	993 [.] 4	993.6	994 · 1	994.5	994.1	994.5	995.0	995.0	995.9	996.2	996.2	996.3	996.3	996.3	996.2	996.2	995.7	995.8	995.1	993.6	992.9	991.9	 	1994.8
	16	000:6	000.0	000.6	080 <i>•6</i>	080-1	080-1	080.5	080.2	080.1	080-1	088:7	088-6	088.2	088.7	088-1	087.0	 088∙0	988.7	989.2	989.9	990-1	990-2	990.1	990.1	989.3
ជ .	16	1990.0	220.7	390.0	$\alpha \times \alpha \cdot c$	HOXO+4	HOXO•T	IOXX:O	ハメメ・ケ	OXX · 4	INX7.6	コムメク・メ	IOX7+2	IOXD:b	OX5.8	SIO255*0	1004.4	1004.1	1903.0	907/	1203 3	7 7 7	777	リランファ	1201 -	1907 0
tion	1/	 990:2	00000	$000 \cdot 1$, 1		Ľ 0. –	OX 5 • 2	IOXD:0	MOX6.2	OX6.7	1087.4	1087.5	1088°C	บดลล • 7	iooa.o	1000.2	1990 0	991 3	1ツラー ノ	リフンニ T	122- 1	122~ 1	フフー フ	190/
tation	rx I	IOX 5 · TI	085.1	085.1	085.2	11085.2	'IOX4'O	985.2	905 2	1.0			i				1004.0									
Stati	18	985.1	990·3	985·1	985.2	985.2	984.9						993.7				002.5	002.0	002.8	002.5	002.3	001.0	001.2		. 7	, 0
	18 19 20	998·3 998·3	99 0·3 985·1 991·9	990·1 985·1 992·4 000·4	985·2 992·6 001·2	985.2	984.9	992.9	993·0	993.0	994.0	994.0	004.9	993.5	993.9	993.9	003.5	003.2	002.0	002 3	002 3	, 001 9		1		
	18 19 20	985·1 991·9 998·3	990·3 985·1 991·9 999·6	990·1 985·1 992·4 000·4	985.2 992.6 001.2	985.2	984.9	992.9	993.0	993.0	994.0	994.0	004.9	993.5	993.9	993.9	080.4	988.7	987.6	987.4	986.6	985.7	984.	983.7	982.3	991.9
	18 19 20 21	985·1 991·9 998·3	990·3 985·1 991·9 999·6	990·1 985·1 992·4 000·4	985.2 992.6 001.2 997.4	985.2	984.9 993.0 995.5	992·9 003·9 994·9	993.0 003.9 994.5	993.0	994.0	994.0	992.3	993:5	993.9	993.9 990.1	989.4	988.7	987.6	987·4 970·6	986.6	985.7	984.7	983·7 970·5	982·3	991.9
	18 19 20 21 22 23	985.1 991.9 998.3 999.8 980.9 970.2	990·3 985·1 991·9 999·6 979·3 970·0	990·1 985·1 992·4 000·4 998·1 970·2	985.2 992.6 001.2 997.4 976.2 970.1	985.2 993.0 996.3 974.1 970.7	984.9 993.0 902.8 995.5 972.1 7970.7	992·9 003·9 994·9 970·8 972·0	993.0 003.9 994.5 970.8 973.0	993.9 993.9 970.1 974.1	994.0 993.3 969.2 974.8	994.0 005.0 993.0 969.2	992·3 968·7 976·4	993.5 004.4 991.4 969.6 976.9	993.9 994.3 990.7 970.3	7 993.9 7 990.1 3 971.3 3 978.3	989·4 971·2 978·8	988·7 971·0 979·3	987·6 971·2 979·7	987·4 970·6 980·2 984·6	986·6 970·9 980·4	985·7 970·8 980·3	984.7 970.9 980.1	983·7 970·5 979·9 987·7	982 · 3 970 · 5 980 · 0 988 · 1	991·9 972·3 975·6
	18 19 20 21 22 23	985.1 991.9 998.3 999.8 980.9 970.2	990·3 985·1 991·9 999·6 979·3 970·0	990·1 985·1 992·4 000·4 998·1 970·2	985.2 992.6 001.2 997.4 976.2 970.1	985.2 993.0 996.3 974.1 970.7	984.9 993.0 902.8 995.5 972.1 7970.7	992·9 003·9 994·9 970·8 972·0	993.0 003.9 994.5 970.8 973.0	993.9 993.9 970.1 974.1	994.0 993.3 969.2 974.8	994.0 005.0 993.0 969.2	992·3 968·7 976·4	993.5 004.4 991.4 969.6 976.9	993.9 994.3 990.7 970.3	7 993.9 7 990.1 3 971.3 3 978.3	989·4 971·2 978·8	988·7 971·0 979·3	987·6 971·2 979·7	987·4 970·6 980·2 984·6	986·6 970·9 980·4	985·7 970·8 980·3	984.7 970.9 980.1	983·7 970·5 979·9 987·7	982 · 3 970 · 5 980 · 0 988 · 1	991·9 972·3 975·6
	18 19 20 21 22 23 24 25	985·1 991·9 998·3 999·8 980·9 970·2 979·8 988·2	990·3 985·1 991·9 999·6 998·9 979·3 970·0 978·8 988·4	990·1 985·1 992·4 000·4 998·1 970·2 978·1 988·3	985.2 992.6 001.2 997.4 976.2 976.9 988.3	985.2 993.0 996.3 974.1 970.7 975.8 988.4	984.9 993.0 002.8 995.5 972.1 7970.7 974.7 988.3	992·9 994·9 970·8 972·0 973·9 988·2	993.0 003.9 994.5 970.8 973.0 973.2 987.7	993.9 993.9 970.1 974.1 972.8 987.6	994.0 993.3 969.2 974.8 972.7 987.6	994.0 005.0 993.0 969.2 976.0 973.6	992·3 968·7 976·4 974·4 986·1	993:5 004:4 991:4 969:6 976:9 975:6	993.9 004.3 990.7 970.3 976.6 982.3	993.9 990.1 9971.3 9978.3 9978.3 980.4	989·4 971·2 978·8 980·1 978·1	988·7 971·0 979·3 981·7 975·7	987.6 971.2 979.7 983.2 974.3	987·4 970·6 980·2 984·6 972·7	986·6 970·9 980·4 985·3	985·7 970·8 980·3 986·2	984·7 970·9 980·1 986·7	983·7 970·5 979·9 987·7 987·0	982·3 970·5 980·0 988·1	991·9 972·3 975·6 1979·0
	18 19 20 21 22 23 24 25	985·1 991·9 998·3 999·8 980·9 970·2 979·8 988·2	990·3 985·1 991·9 999·6 998·9 979·3 970·0 978·8 988·4	990.1 985.1 992.4 000.4 998.1 978.1 970.2 978.1 988.3	985.2 992.6 001.2 997.4 976.2 976.9 988.3	985.2 993.0 996.3 974.1 970.7 975.8 988.4	984.9 993.0 002.8 995.5 972.1 7970.7 974.7 1988.3	992·9 003·9 994·9 970·8 972·0 973·9 988·2	993.0 003.9 994.5 970.8 973.0 973.2 987.7	993.9 993.9 970.1 974.1 972.8 987.6	994.0 993.3 969.2 974.8 972.7 987.6	994.0 993.0 969.2 976.0 973.6 987.3	992·3 968·7 976·4 974·4 986·1	993.5 991.4 995.6 976.9 975.6	993.9 990.7 970.3 976.9 982.3	7 990 · I 7 990 · I 3 971 · 3 9 978 · 3 9 980 · 4	989·4 971·2 978·8 980·1 978·1	988·7 971·0 979·3 981·7 975·7	987.6 971.2 979.7 983.2 974.3	987·4 970·6 980·2 984·6 972·7	986·6 970·9 980·4 985·3 971·8	985·7 970·8 980·3 986·2 971·1	984·7 970·9 986·7 970·5	983·7 970·5 979·9 987·7 970·0	982·3 970·5 980·0 988·1 970·4	991·9 972·3 975·6 979·0 981·9
	18 19 20 21 22 23 24 25 26 27	985.1 991.9 998.3 999.8 980.9 970.2 979.8 988.2 970.3	990·3 985·1 991·9 999·6 998·9 970·0 978·8 971·0 973·1	990·1 985·1 992·4 000·4 998·1 970·2 978·1 988·3 971·2 973·4	985.2 992.6 001.2 997.4 976.2 970.1 976.6 988.3	985.2 993.0 996.3 974.1 970.7 975.8 988.4	984.9 993.0 9002.8 3 995.5 972.1 7 970.7 3 974.7 4 988.3	992.9 003.9 994.9 970.8 972.0 973.9 988.2 975.1 974.7	993.0 003.9 994.5 970.8 973.0 973.2 987.7 975.9	993.9 993.9 970.1 974.1 972.8 987.6 976.5	994.0 993.3 969.2 974.8 972.7 987.6	994.0 993.0 969.2 976.0 987.3 979.5	992·3 968·7 976·4 974·4 986·1	993.5 004.4 1991.4 1969.6 975.6 1975.6 1979.1	993.9 990.7 970.3 977.6 976.9 982.3 975.2	993.9 993.9 990.1 971.3 978.3 980.4 979.4 2974.2	989·4 971·2 978·8 980·1 978·1	988·7 971·0 979·3 981·7 975·7	987.6 971.2 979.7 983.2 974.3 977.5 972.2	987·4 970·6 980·2 984·6 972·7 976·0 971·7	986·6 970·9 980·4 985·3 971·8 975·8 970·6	985·7 980·3 986·2 986·2 971·1 975·5 969·2	984.7 970.9 980.1 986.2 970.5 974.6	983.7 970.5 979.9 987.7 970.0 974.1 967.7 5995.3	982·3 970·5 980·0 988·1 970·4 973·7 967·6	991·9 972·3 975·6 979·0 981·9 7975·7 973·2
	18 19 20 21 22 23 24 25 26 27 28	985.1 991.9 998.3 999.8 980.9 970.2 979.8 988.2 970.3 973.3	990·3 985·1 991·9 999·6 998·9 970·0 978·8 971·0 973·1 967·0	990·1 985·1 992·4 000·4 998·1 978·1 970·2 978·1 988·3 971·2 973·4 968·6	985.2 992.6 001.2 997.4 976.2 976.9 988.3 972.6 973.6	985.2 993.0 1996.3 974.1 970.7 975.8 988.4	984.9 993.0 9002.8 3 995.5 972.1 7 970.7 4 988.3 974.3 972.8	992.9 003.9 994.9 970.8 972.0 973.9 988.2 975.1 974.7 974.7	993.0 003.9 994.5 970.8 973.0 987.7 975.9 975.5	993.0 004.2 993.9 970.1 974.1 977.6 976.5 978.0	994.0 993.3 969.2 974.8 972.7 987.6 978.7 976.2	994.0 993.0 969.2 976.0 987.3 979.5 976.1	992·3 968·7 976·4 974·4 986·1 979·4 975·7 981·3	993.5 991.4 9969.6 976.9 975.6 984.7 1975.3	993.9 990.7 970.3 977.6 976.9 982.3 975.2 984.6	993.9 9993.9 999.1 999.1 998.3 980.4 999.4 2994.2 999.4 2994.2	989·4 971·2 978·8 980·1 978·1 978·6 973·8	988.7 971.0 979.3 981.7 975.7 978.4 973.2 989.7	987.6 971.2 979.7 983.2 974.3 977.5 972.2 990.4	987·4 970·6 980·2 984·6 972·7 976·0 971·7 991·6	986·6 970·9 980·4 985·3 971·8 975·8 970·6	985.7 980.3 986.2 971.1 975.5 969.2 8 993.1	984.7 980.1 980.1 986.2 970.5 974.6 968.2	983.7 970.5 979.9 987.7 970.0 974.1 2 967.7 5 995.3	982·3 970·5 980·0 988·1 970·4 973·7 967·6	991·9 972·3 975·6 979·0 981·9 7975·7 973·2 8981·7
	18 19 20 21 22 23 24 25 26 27 28	985.1 991.9 998.3 999.8 980.9 970.2 979.8 988.2 970.3 973.3	990·3 985·1 991·9 999·6 998·9 970·0 978·8 971·0 973·1 967·0	990·1 985·1 992·4 000·4 998·1 978·1 970·2 978·1 988·3 971·2 973·4 968·6	985.2 992.6 001.2 997.4 976.2 976.9 988.3 972.6 973.6	985.2 993.0 1996.3 974.1 970.7 975.8 988.4	984.9 993.0 9002.8 3 995.5 972.1 7 970.7 4 988.3 974.3 972.8	992.9 003.9 994.9 970.8 972.0 973.9 988.2 975.1 974.7 974.7	993.0 003.9 994.5 970.8 973.0 987.7 975.9 975.5	993.0 004.2 993.9 970.1 974.1 977.6 976.5 978.0	994.0 993.3 969.2 974.8 972.7 987.6 978.7 976.2	994.0 993.0 969.2 976.0 987.3 979.5 976.1	992·3 968·7 976·4 974·4 986·1 979·4 975·7 981·3	993.5 991.4 9969.6 976.9 975.6 984.7 1975.3	993.9 990.7 970.3 977.6 976.9 982.3 975.2 984.6	993.9 9993.9 999.1 999.1 998.3 980.4 999.4 2994.2 999.4 2994.2	989·4 971·2 978·8 980·1 978·1 978·6 973·8	988.7 971.0 979.3 981.7 975.7 978.4 973.2 989.7	987.6 971.2 979.7 983.2 974.3 977.5 972.2 990.4	987·4 970·6 980·2 984·6 972·7 976·0 971·7 991·6	986·6 970·9 980·4 985·3 971·8 975·8 970·6	985.7 980.3 986.2 971.1 975.5 969.2 8 993.1	984.7 980.1 980.1 986.2 970.5 974.6 968.2	983.7 970.5 979.9 987.7 970.0 974.1 2 967.7 5 995.3	982·3 970·5 980·0 988·1 970·4 973·7 967·6	991·9 972·3 975·6 979·0 981·9 7975·7 973·2 8981·7
	18 19 20 21 22 23 24 25 26 27 28 29 30	985.1 991.9 998.3 999.8 980.9 970.2 979.8 988.2 970.3 973.3 967.6 996.4 990.1	990·3 985·1 991·9 999·6 998·9 979·3 970·0 978·8 971·0 973·1 967·8 997·0 989·3	990·1 985·1 992·4 000·4 998·1 978·1 978·1 988·3 971·2 973·4 968·6 997·2 987·9	985.2 992.6 001.2 997.4 976.2 976.9 988.3 972.6 973.6 977.5	985.2 993.0 996.3 974.1 970.7 975.8 988.4 973.6 973.6 973.6 977.8	984.9 993.0 902.8 995.5 972.1 7,970.7 4,988.3 9,973.8 5,974.3 1,972.8 8,997.9 9,85.0	992·9 003·9 994·9 970·8 972·0 988·2 975·1 974·7 975·3 998·2	993.0 003.9 994.5 970.8 973.0 987.7 975.9 975.5 976.5 998.5	993.0 004.2 993.9 970.1 974.1 972.8 987.6 976.5 978.6 998.9	994.0 993.3 969.2 974.8 972.7 987.6 978.7 979.6 998.8 998.8	994.0 993.0 969.2 976.0 987.3 9979.5 980.1 980.1 980.1 983.2	992·3 968·7 976·4 974·4 986·1 979·4 975·7 981·3 998·2 983·3	993·5 991·4 969·6 976·9 984·7 1979·1 1979·1 1983·4 1983·6	993.9 990.7 970.3 977.6 982.3 979.6 984.6 983.9	993.9 3003.9 3003.9 3003.9 3003.9 978.3 980.4 979.4 2074.2 984.6 984.6	989:4 971:2 978:8 980:1 978:1 978:1 978:0 987:9 987:9	988.7 971.0 979.3 981.7 975.7 978.4 973.2 989.7 985.7	987.6 971.2 979.7 983.2 974.3 977.5 972.2 990.4	987·4 970·6 980·2 984·6 972·7 976·0 971·7 991·6 986·5	986·6 970·9 980·4 985·3 971·8 975·8 970·6 992·3 993·7	985.7 970.8 980.3 986.2 971.1 9975.5 969.2 8 993.1 7 992.8	984.7 986.7 986.7 970.5 974.6 968.7 994.1 998.7	983.7 979.5 979.9 987.7 5970.0 5974.1 2967.7 5995.3 1991.2 5989.2	982·3 970·5 980·0 988·1 970·4 973·7 967·6 995·8	991·9 972·3 975·6 979·0 981·9 7 975·7 983·2 8 981·7 8 996·3
	18 19 20 21 22 23 24 25 26 27 28 29 30	985.1 991.9 998.3 999.8 980.9 970.2 979.8 988.2 970.3 973.3 967.6 996.4 990.1	990·3 985·1 991·9 999·6 998·9 979·3 970·0 978·8 971·0 973·1 967·8 997·9 989·3	990·1 985·1 992·4 000·4 998·1 978·1 978·1 988·3 971·2 973·4 968·6 997·2 987·9 992·5	985.2 992.6 001.2 997.4 976.2 976.9 988.3 972.6 973.6 977.5	985.2 993.0 1996.3 1970.7 1975.8 1988.4 1973.6 1973.6 1973.6 1973.6 1973.6	984.9 993.0 0002.8 8 995.5 972.1 7 970.7 8 974.7 988.3 974.3 972.8 8 997.9 7 985.0	992.9 003.9 994.9 970.8 972.0 973.9 988.2 975.1 974.7 975.3 998.2 984.4	993.0 003.9 994.5 970.8 973.0 973.2 987.7 975.9 975.5 998.5 984.0	993.9 993.9 970.1 972.8 987.6 976.5 978.6 998.9 983.7	994.0 993.3 969.2 974.8 972.7 987.6 998.6 998.8 998.8	994.0 993.0 993.0 969.2 976.0 987.3 979.5 976.1 988.1 998.5	992·3 968·7 976·4 974·4 986·1 979·4 975·7 981·3 998·2 983·3	993·5 991·4 9969·6 976·9 975·6 984·7 1979·1 1979·1 1979·1 1979·1 1979·1	993.9 990.7 970.3 977.6 976.9 982.3 979.9 983.9 992.9	993.9 9993.9 1990.1 3971.3 9978.3 9979.4 2974.2 5986.1 3996.7 992.2	989·4 971·2 978·8 980·1 978·1 978·6 973·8 987·9 996·2 985·1	988.7 971.0 979.3 981.7 975.7 978.4 973.2 989.7 995.9 985.7	7 987·6 971·2 979·7 983·2 974·3 977·5 972·2 990·4 995·5 985·7	987·4 970·6 980·2 984·6 972·7 976·0 971·7 991·6 986·5	986·6 970·9 980·4 985·3 971·8 975·8 970·6 992·3 993·7 987·4	985.7 970.8 1980.3 1986.2 1971.1 1999.2 1988.1	984.7 986.7 986.7 970.5 974.6 968.7 994.1 998.7	983.7 979.5 979.9 987.7 5970.0 5974.1 2967.7 5995.3 1991.2 5989.2	982·3 970·5 980·0 988·1 970·4 973·7 967·6 995·8	991·9 972·3 975·6 979·0 981·9 7 975·7 983·2 8 981·7 8 996·3
lean	18 19 20 21 22 23 24 25 26 27 28 29 30 31	985.1 991.9 998.3 999.8 980.9 970.2 979.8 988.2 970.3 973.3 967.6 996.4 990.1 991.2 991.2	990·3 985·1 991·9 999·6 998·9 970·0 978·8 988·4 971·0 973·1 967·8 997·0 989·3 991·9 ——— 982 •20	990·1 985·1 992·4 900·4 998·1 978·1 978·3 971·2 973·4 968·6 997·9 992·5 982 982	985.2 992.6 001.2 997.4 976.9 976.9 988.3 972.0 970.3 986.9	985.2 993.0 996.3 996.3 974.1 970.7 9975.8 3988.4 0 973.6 0 973.6 0 973.6 0 973.6 0 973.6 0 985.7 981.8 981.8	993.0 993.0 993.0 993.0 993.0 993.0 992.1 1,970.7 1,988.3 1,972.8 1,987.9 1,985.0 1,985.0 1,985.0 1,985.0 1,985.0 1,981.0	992·9 003·9 994·9 970·8 972·0 973·9 988·2 975·1 974·7 975·3 998·2 984·4	993.0 003.9 994.5 970.8 973.2 987.7 975.9 975.5 976.5 998.5 984.0	993.9 993.9 970.1 974.1 977.6 976.5 978.6 978.6 998.9 983.7	994.0 993.3 969.2 974.8 974.8 972.7 987.6 978.7 9979.6 998.8 7982.7 994.9	994.0 993.0 993.0 973.0 979.5 979.5 976.1 998.5 983.2 994.8	992·3 968·7 976·4 976·4 986·1 979·4 975·7 981·3 998·2 983·3	993.5 991.4 996.6 976.6 984.7 979.1 7975.3 983.4 997.8 983.6 993.4 	993.9 990.7 970.6 977.6 982.3 979.0 975.2 984.6 997.3 983.9 992.9 982.9	993.9 990.1 3971.3 998.3 998.3 9979.4 2974.2 9979.4 2974.2 9984.6 9992.2 982.8	989·4 971·2 978·1 978·1 978·1 978·1 978·1 978·6 973·8 987·9 996·2 985·1 982 	988.7 971.0 979.3 981.7 975.7 978.4 973.2 989.7 995.9 985.7	987.6 971.2 979.7 983.2 974.3 977.5 2972.2 990.4 995.5 985.7	987·4 970·6 980·2 984·6 972·7 976·0 971·7 991·6 986·5 991·1 982	986·6 970·9 980·4 985·3 971·8 975·8 970·6 992·3 993·7 987·4 991·0	985.7 986.2 986.2 997.1 9969.2 993.1 988.1 990.2	984.7 986.7 986.7 970.5 986.2 968.2 994.3 992.3 988.3 990.3	7 983·7 979·9 979·9 7 987·7 5 970·0 5 974·1 2 967·7 5 995·3 1 991·2 5 989·2 1 990·1 982	982·3 970·3 980·0 988·1 970·4 973·7 967·6 995·8 990·3 990·3	991·9 972·3 975·6 979·0 981·9 7975·7 973·2 8981·7 996·3 8986·0 892·5 982 55
lean Station l	18 19 20 21 22 23 24 25 26 27 28 29 30 31	985.1 991.9 998.3 999.8 980.9 970.3 970.3 970.3 967.6 996.4 990.1 991.2 ————————————————————————————————————	990.3 985.1 991.9 999.6 988.9 979.3 970.0 978.8 988.4 971.0 989.3 991.9 982	990·1 985·1 992·4 998·1 978·1 978·1 988·3 971·2 973·4 968·6 997·2 987·9 992·5 982 •05	985-2-992-6 997-4 976-2 997-6 978-6 973-6	985.2 993.0 996.3 9974.1 970.7 975.8 988.4 973.6 973.6 973.6 997.8 985.7 981 86	981 981 981 981 981 981 981 981	992.9 994.9 970.8 972.0 973.9 988.2 975.1 974.7 975.3 998.2 984.4 994.3 981 981	993.0 003.9 994.5 970.8 973.0 973.2 987.7 975.9 975.5 976.5 998.5 984.0 994.5 982 08	993.0 004.2 993.9 970.1 974.1 972.8 987.6 976.5 978.0 998.9 983.7 994.7 982 .39	994.0 993.3 993.3 969.2 974.8 9972.7 998.6 9978.7 998.8 7994.9 982 7994.9	994.0 993.0 969.2 976.0 973.6 987.3 998.5 988.2 994.8 988 00	992·3 968·7 976·4 986·1 979·4 985·3 994·0 982 -83	993·5 991·4 9969·6 976·9 975·6 984·7 9975·3 983·4 993·4 982 73 1012	993.9 990.7 970.3 977.6 982.3 979.0 975.2 983.9 992.9 983.9 982.9	993.9 1993.9 1990.1 1997.3 1998.3 1998.3 1998.4 1999.4 1992.2 1982 1982 1982 1982	989:4 971:2 978:8 980:1 978:1 978:1 978:6 973:8 987:9 985:1 992:1 982 -86	988·7 971·6 979·3 981·7 975·7 978·4 973·2 989·7 995·9 985·7 991·7 982	987.6 971.2 979.7 983.2 974.3 977.5 972.2 990.4 995.5 985.7 991.5 982 91	987.4 970.6 980.2 984.6 972.7 976.0 971.7 991.6 994.6 986.5 991.1 	986.6 970.9 980.4 985.3 971.8 975.8 970.6 992.3 993.7 987.4 991.0	985.7 970.8 980.3 986.2 971.1 8 975.5 969.2 8 993.1 988.1 988.1	984.7 970.5 980.1 986.7 970.5 968.2 968.2 988.3 990.3 982.3 1012	7 983·7 970·5 970·9 7 987·7 970·0 5 974·1 2 967·7 5 989·2 1 990·1 982 • 76	982·3 970·5 980·6 988·1 970·4 973·7 967·6 995·8 990·3 990·3 990·3	991·9 972·3 975·6 979·6 981·9 7 975·7 973·2 8 981·7 8 996·3 8 992·2 982 5 1011
	18 19 20 21 22 23 24 25 26 27 28 29 30 31	985.1 991.9 998.3 999.8 980.9 970.2 979.8 988.2 970.3 973.3 967.6 996.4 990.1 991.2 991.2	990.3 985.1 991.9 999.6 988.9 979.3 970.0 978.8 988.4 971.0 989.3 991.9 982	990·1 985·1 992·4 998·1 978·1 978·1 988·3 971·2 973·4 968·6 997·2 987·9 992·5 982 •05	985-2-992-6 997-4 976-2 997-6 978-6 973-6	985.2 993.0 996.3 9974.1 970.7 975.8 988.4 973.6 973.6 973.6 997.8 985.7 981 86	981 981 981 981 981 981 981 981	992.9 994.9 970.8 972.0 973.9 988.2 975.1 974.7 975.3 998.2 994.3 981 993	993.0 003.9 994.5 970.8 973.0 973.2 987.7 975.9 975.5 976.5 998.5 984.0 994.5 982 08	993.0 004.2 993.9 970.1 974.1 972.8 987.6 976.5 978.0 998.9 983.7 994.7 982 .39	994.0 993.3 969.2 974.8 8972.7 987.6 9978.7 998.8 7994.9 982 7994.9	994.0 993.0 969.2 976.0 973.6 987.3 998.5 988.2 994.8 983 00	992·3 968·7 976·4 986·1 979·4 985·3 994·0 982 -83	993·5 991·4 9969·6 976·9 975·6 984·7 9975·3 983·4 993·4 982 73 1012	993.9 990.7 970.3 977.6 982.3 979.0 975.2 983.9 992.9 983.9 982.9	993.9 1993.9 1990.1 1997.3 1998.3 1998.3 1998.4 1999.4 1992.2 1982 1982 1982 1982	989:4 971:2 978:8 980:1 978:1 978:1 978:6 973:8 987:9 985:1 992:1 982 -86	988·7 971·6 979·3 981·7 975·7 978·4 973·2 989·7 995·9 985·7 991·7	987.6 971.2 979.7 983.2 974.3 977.5 972.2 990.4 995.5 985.7 991.5 982 91	987.4 970.6 980.2 984.6 972.7 976.0 971.7 991.6 994.6 986.5 991.1 	986.6 970.9 980.4 985.3 971.8 975.8 975.8 975.8 975.8 975.8 975.8 992.3 993.7 987.4 991.0	985.7 970.8 980.3 986.2 971.1 8 975.5 969.2 8 993.1 988.1 988.1	984.7 970.5 980.1 986.7 970.5 968.2 968.2 988.3 990.3 982.3 1012	7 983·7 970·5 970·9 7 987·7 970·0 5 974·1 2 967·7 5 989·2 1 990·1 982 • 76	982·3 970·5 980·0 988·1 970·4 973·7 967·6 995·8 990·3 990·3 990·3	991·9 972·3 975·6 979·6 981·9 7 975·7 973·2 8 981·7 8 986·3 8 992·5 982 5 1011

ANNUAL MEANS OF HOURLY VALUES.

From readings in millibars at exact hours, Greenwich Mean Time.

Eskdalemuir: $H_b = 237 \cdot 3$ metres.

1923.

G.M.T.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Station Level	mb. 981·34	mb. 981 ·20	mb. 981. 02	mb. 980·8 9	mb. 980·85	mb.	mb. 981.05	mb. 981·21	mb. 981·34	mb. 981·44	mb. 981·45	mb. 981·38	mb. 981·32	mb. 981·26	mb. 981·21	mb. 981·18	mb. 981·22	mb. 981·30	mb. 981·42	mb. 981·51	mb. 981·58	mb. 981·59	mb. 981.56	mb. 98 1·51	mb. 981·28
Sea Level	010.33	010-20	010.02	009:89	209.85	009·85	009.98	010.03	010.16	010.51	010.16	010.04	009·96	009.89	009 ·84	009.85	009.93	010.00	010-20	010.39	010.49	010.54	010.23	010.49	.(3 010·14

PRESSURE AT STATION LEVEL; MONTHLY MEANS AND DIURNAL INEQUALITIES.

The departures from the mean of the day are adjusted for non-cyclic change.

124. Eskdalemuir: $H_b=237\cdot3$ metres.

1923.

	1	Hour.	G.M.T.								<u> </u>						<u> </u>	I				i			
Month	Mean	I.	2.	3⋅	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.
	mb.	mb.	mb.	mb.	mb.	mb.	mb.		mb.		mb.	mb.		mb.		mb.		mb.	mb.		mb.	mb.	mb.	mb.	mb.
	987.13																								
	969·92 988· 1 9		0.06	-0-42	-0·53	-0-51	-0.40	+0.00	1025	→0-41	+041	+0-40		1-0-07	-0.17	-0-30	-0-44	0-97	-0.10	1005	+0-17	40-25	+0-29	40.20	+0.28
	.25			-0.16	- 0.Z7	-0.27	-0.14	10.03	+0.19	to 35	+0.35	+0.34	+0.25	10.01	-0.23	-0.45	-0.50	-0.43	-0.25	-0.01	+0.11	+0.19	40.59	40.5	40-22
	979·61 982·74																								
	989.90																								
July	984.72	1 0.04	0.74	0.22	0.26	0.20	0.76	0.04	10.05	1 0,06	1 0.00	LOUTT	10.07	10.00	1 0,00	0.06	0.70	0.20	0.00	0:04	1.0.10	1 0.21	1 0.25	1-0.22	10.21
	980.60																								
	981.75																								
Oct.	971.71	+o·16	-0.14	-0.57	-o·84	-o·98	-1.03	-0.84	-0.47	-0.28	 +o·o6	+0.10	+0.17	+0.13	+0.20	+0.13	+0.12	+0.26	+0.47	+0.61	+0.50	+0.56	+0.58	+0.21	+0.35
Nov.	976.52	0. 06	-0.10	-0.24	-0.29	-o·36	-0.38	-0.29	—ი·i3	+0.05	+0.21	+0.17	+0.05	+0.03	-0.02	+0.03	+0.09	+0.20	+0.26	+0.31	L +0.23	+0.14	+0.06	+0.07	+0.07
Dec.	982.55	0.10	-0.55	-o·39	-o·53	-0. 66	-0.75	− 0·56	-0.42	-0.13	+0.27	+0.46	+0.28	+0.17	+0.17	+0.27	+0.26	+0.32	+0.28	+0.31	+0.30	+0.26	+0.50	+0.07	+0.06
Year	981.28	+0.08	-0.06	-0·2 6	-o⋅3 8	-0.42	o·38	-0.24	-0.04	+0.04	+0.17	+0.1	+0.16	+0.04	-0.03	-0.08	-0·1	-0.07	+0.01	+0.1	+0.21	+0.28	+0.28	+0.2	+0.51
	<u> </u>	7		3	6	39		3	7	6	1	7	. 09	1				1	<u> </u>	2.	1 (1	6	1

ABSOLUTE EXTREMES OF PRESSURE AT STATION LEVEL FOR EACH DAY.

Maximum and Minimum for the interval 0h. to 24h., Greenwich Mean Time.

125.	Eskd	alemui	ir: H	=237	·3 me	etres.																	1	923.
Month	Ja	n.	Fe	b.	Ma	ır.	Ap	ril.	Ма	y.	Jui	ne.	Ju	ly.	Αυ	ıg.	Sep	ot.	Oc	t.	No	v.	De	c.
Day.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
1 2 3 4 5 6 7 8 9 10 11 12	mb. 980·5 975·5 976·0 988·7 985·4 982·5 984·9 981·2 973·6 986·7 994·9	973·6 986·7	986·5 972·3 960·1 963·4 975·4 972·0 978·1 987·5	958·8 948·0 942·2 963·4 967·1 971·1 978·1	977.5 991.7 990.4 985.1 984.4 994.5 994.6 990.9 991.6 991.2	977.5 980.3 971.2 966.9 984.4 990.9 984.1 985.2 981.2	993.8 985.4 982.7 982.8 983.2 989.2 989.1 982.2 978.8 977.2	985·4 979·4 979·5 978·0 977·5 983·2 982·2 977·4 975·6 961·6	991·8 989·8 984·2 982·9 966·3 968·8	988·2 983·8 979·1 979·0 988·7 984·2 976·4 957·8 956·6 966·1	mb. 999 · 1 000 · 2 995 · 9 989 · 1 987 · 2 990 · 3 991 · 7 986 · 2 978 · 5 985 · 2 000 · 4	986.0 986.3 981.6 983.3 986.2 975.3 974.1 977.4 985.2 987.5	983·3 989·4 995·0 995·1 992·8 991·3 992·1 993·2 995·4 996·5	980·3 978·3 983·3 989·4 992·5 988·2 988·4 990·9 991·1 991·5 995·2	991·1 995·6 994·0 987·7 986·6 988·2 989·7 994·9 997·8 997·5	962·4 991·1 986·9 985·2 982·0 986·4 984·4 989·7	998.7 990.8 989.8 989.5 982.3	973.9	980·8 979·1 980·5 980·6 978·6 975·2	986.0 977.6 976.6 972.9 967.3 965.6 972.7 973.5 957.1	972·9 971·2 972·3 982·1 983·6 979·8 994·4 000·9 998·8 984·4	979·8 968·6 968·4 994·4 984·4 973·7	972·8 970·7 981·9 986·8 980·4 976·1 984·8 989·4	mb. 968·1 955·6 965·3 956·7 960·6 980·4 987·1 982·8 989·3 990·0
13 14 15	996.5	983·0 990·5	991.7 991.1 987.5	987·4 977·5	002.0	999·1	'	958·8 968·7	971·0 972·7 971·7	969·4 969·1	988·7 993·6 991·5	988.7	996·2 988·2	988·2 978·3	994·2 992·6	992·5 989·7		969·4 970·0	979·9 981·9	979.5	966·6 967·I	945·1 945·6 941·1	996·5	990·9 989·2 991·7
16 17 18 19 20	999.9 000.1 004.0 002.3 997.9	998·9 999·6 983·5 981·1		975·5 964·4 967·9 970·9	001·5 004·5 004·5 002·4 996·7	000·6 002·4 996·7 992·0	989·7 991·6 990·6 983·1 985·8	989·7 982·1 980·7 983·0	986·7 989·3 985·0 978·5	977·9 985·0 978·5 972·7	995.3	991·5 988·2 988·1 990·8	980·0 987·6 987·5 989·9	977 ² 980 ⁰ 982 ⁵ 984 ⁰	982·7 980·3 983·0 981·5	970·0 969·4 980·3 972·3	974·4 975·2	961·9 962·9 970·5 968·3	991·2 990·7 975·5 974·5	985.5	970·6 974·3	957.9		987·8 983·5 984·9 991·8 997·1
21 22 23 24 25	998·1 001·0 004·5 002·7 004·3	989·7 995·7 996·1	970·9 959·5 970·0 971·1	958·4 958·9 963·3 966·1	993·5 991·2 988·1 988·6 993·9	988·0 984·3 984·5 987·8	985·7 984·6 988·0 989·8 976·0	982·5 980·8 976·0 959·5	986·9 992·7 981·5	982·8 986·7 981·0 977·4	993.8	989·0 992·5 991·1	993:9 993·1 983·3 983·6 980·0	983·3 978·7 980·0	975·9 977·6 983·1	966·9 966·9 966·7	977.9	964·4 964·0 969·8	959·7 954·7 953·7 948·2 962·6	952·I 941·4 944·2	979·2 984·2 989·4 992·4 990·2	976·7 979·2 984·1 989·4 982·3	982.3	982·3 968·6 969·9 972·6
26 27 28 29 30	002·3 996·8 994·1 989·4 988·4	996·8 990·7 989·4 982·1 984·3	948·5 959·1 — —	935.3	995.6 990.5 992.9 996.8 997.5	983·7 984·1 992·9 994·1	979·I	974·6 976·5 976·7	998·7 999·0	987·9 993·0 996·0 994·0	994·7 994·9 991·7	991·5 991·7	983·4 985·6 979·5 975·9 971·2	979·5 973·4 971·2 963·8	980.5	964·9 966·3 965·2 965·8	997·2 998·3	985·1 982·2 997·1	969·4 976·3	950·2 950·4 969·4 970·1	982·3 983·2 982·8 986·2 987·9	980·5 977·0 976·5		967.6 967.5 990.3 982.6
Mean	991 · 99	982 · 45	975 · 17	965.30	992 · 15	984.41	983 · 41	976.60	986.01	979.45	992.65	987.14	987.19	982.26	984 • 90	976.11	985.73	977.67	976.49	966 · 78	981 • 40	971.60	987.98	976.9

Readings in degrees absolute at exact hours, Greenwich Mean Time.

126. Eskdalemuir: Louvred Hut: h_t (height of thermometer bulb above ground) = 0.9 metre.

January, 1923.

Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	М
	a.	$\frac{1}{a}$	a	a.	a.	$\frac{ }{ }a.$	a.	a.	<i>a</i> .	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	1
1	71.0	69.9	69.0	68·1	68·1	67.2	66.6	66.2	66.0	67.7	69.8	71.7	72.6	73.4	73·I		72.0	73.2	73.4	73.7	74.3	74.9		75.0	
2	75.1	75.7	76·o	76.0	75.9	80·o										79.7		79.8			79.3	70.0	70.2	1'.	
3	78.8	78.7	78.8	79.0	78·o	77.4	77.1	77.0	76.5	76.3	77.0	77.9										77.5		76.1	
4	75.8	75.4	75.4	75.5	75.5	75.6	75.0	75.1	74.9	76.3	77.9	78.3	79.0	78.1	76.2	74.7	74.0	73.5	73.1		74.0				
5	77.0	77:3	77.1	77.0	77.1	77.1	76.2	76.0	75.9	76.2	76.9	76.8	76.7	77.6	78.0	77.7	70.0	70.5	70.5	70.1	75.2	75.1	74.9	/4-1	ľ
6	73.7	74.0	73.9	74.0	73.6	73.0	74.0	73.3	73:5	74.2	74.7	74.9	75.3	75.3	75.0	75.1	74.9	74.9	75.1	75.0	75.4	76.0	76.7	77·I	17
7	76.4	76.4	77.0	78.0	78·T	78.5	78·0	70·1	70.5	180.0	80.4	81.7	81.0	81.8	82.1	02.0	82.0	02.0	102.0	02.0	02.7	01.0	01.4	01.7	٦,
8	81.1	81.4	81.4	81.7	82.0	81.0	80.2	80.1	79·I	79.0	79:3	179:3	79.4	78.8	70.0	178.0	77'5	177.3	170.9	75.7	170.3	170.0	170.4	1// 1	- 1/
9	77.0	77.2			77.7	76.5	75.0	75.5	75.0	75.0	75.0	175.6	75.7	175.0	175.0	174 · Q	175.2	175.0	175·I	174.9	75.2	74.2	75.0	75.3	17
10		74.4			75.0	74.8	74.5	75.4	75.9	76.8	77.4	77:9	78·o	77.5	77.8	77.0	76.2	76.3	76.4	75.7	75.2	75.6	74.6	74.2	7
			77.0	77.0	77.0	74.8	74.4	74.1	74.6	75.4	76.2	77.1	76.2	76.8	76.5	76.6	76.6	75.6	76.2	75.5	75·I	74.1	73·I	73.5	17
II	74.6	74.9	75.0	75.0	75.0	74.0	74 4	71.0	70:2	77.0	71.6	73.4	74.5	76.2	76.4	75.5	74.2	72.3	72.1	71.1	70.6	70.6	69.5	68.4	1
12	73.2	72.9	73.5	68.2	99.1	60.3	70.8	71.2	72.3	72.2	72.8	74.7	74.3	75.4	75.7	76.3	77.1	77.1	77.7	78.0	78·I	77.8	78.4	79.3	17
13		67.5	80.0	180.0	80.6	181.0	180.8	180.1	78.7	178.5	178.0	78.3	17X · 2	177.8	177.0	77.4	76.0	77.5	77.3	77.0	77.0	77·I	77.4	77:3	17
14	79.1	00.7	00.9	00.9	77.4	78.0	77.0	78:0	78.6	78.6	78.8	70.2	70.2	70.5	70.4	79.5	80.0	81.5	81.4	81.3	80.9	80.4	80.2	79.8	1/2
15	ľ		1	1	1		1		1	1	\$	i			1	1	ı			ł .			1	1	•
16	79.7	8o·o	79.9	79.7	79.6	79.6	79.2	78.9	78.7	78.2	79.0	79.0	78.6	79.0	78.8	79.0	78.6	78.6	78.5	78.3	78.4	78.2	78·I	78.1	17
17		78·o	78.4	78.2	78.0	78.1	77.8	78.0	78.0	78.3	78.2	78·I	78·I	78.2	178.1	78·o	70.0	70.0	70.0	78.0	78.8	78.0	77.9	78.0	1/2
18	77:3	77.7	77.6	76.9	77.4	78.4	77.3	77.2	77.2	77.9	78.9	79.8	78.8	78.1	70.5	78.0	70.1	77.0	77.7	70.4	70.0	70.0	7/9	76.2	1/2
19					80.0	79.5	79·I	79.0	79.1	79.5	79.4	79.0	90.8	91.3	01.9	81.7	02.1	01.0	72.0	70.8	77.7	77.5	70.8	72.7	1/2
20	76.0	75.9	75.8	75.3	1	1		1	1	1		1		ı	1	74.8		1		1	ı	i	1	1	
21	72.2	73.4	72.2	71.6	73.6	73.7	73.9	74.2	74.9	75.7	76.4	76.9	78.5	80.9	81.0	81.3	81.1	80.8	81.2	81.7	80.5	81.2	81.0	80.0	7
22	80.3	80.2	80.6	80.3	80.3	80.9	8o·6	80.4	80.1	180.0	180.8	180.3	80.7	180.4	180.3	180.3	178.9	170.7	175.5	174.0	174.0	173.4	173.0	1/2.0	-1/
23	177.5	77.2	70.8	70.0	60.3	168·0	168.4	60.5	70.7	72.7	7.1.2	174.8	75·I	70·I	75.9	76·I	170:3	70.5	77.1		77.7	78.3	78.7	79.3	7
24	lac. i	170.0	180.0	180.2	180.5	180.7	18 T · O	18r.o	80.9	!8т∙т	81.2	l8r•8	81.7	182.0	81.4	180·a	80.3	80.4	80.5	80.6	80.8				
25	8o·6	80.7	80.6	8o·8	80.3	79.8	80.2	8o·o	79.9	79.7	79.7	79.8	8ი∙ი	80·1	80·0	79.7	79.3	79.3	79.3	79.1	80.2	80.0	79.0	79.2	17
26	70::	70.2	70:2	70.2	70.2	70:0	70.8	70.0	70.0	80.1	80.1	80.1	80.2	80.2	80.1	80·o	79.7	79.8	79.3	79:5	79.8	79.7	79:3	79.4	1
26					79.5	70.6	70.8	80.2	80.6	81.0	81.3	81.0	81.8	82.1	81.0	81.3	191.3	101.2	101.2	01.0	101.0	101.0	01.7	101.7	10
27 28	0 -	79.7	0	10	Q	Q	180.0	180.6	180.6	80.4	180.8	180.0	ISO. 4	180.2	70.6	170.8	70.2	170.0	170.0	179.0	170.0	178.0	170.7	170'0	C
		1-0-	mo . o		100.8	180.8	18 x . ~	181.6	Qr.e	18 T . 6	IXT · O	82.2	1X2 · 4	182.2	182 · T	8T-8	81.5	81.1	81.2	81.1	81.2	81.0	81.1	81.0	8
29 30	81.0	81.0	80.0	80.5	80.0	80.7	80.6	80.3	80.5	80.9	80.5	80.9	81.2	81.4	81.2	82.2	82.8	82.7	82.7	82.4	82.2	82·o	82.1	82.5	8
31				1	1	1	1	Į.		1	i	ì		i		81.5	1	ſ	ſ	í	1	1	1	1	
_				1	1	!		·																	-1-
Iean	. 77·I	77.2	77.1	77·I	77.1	77·I	77·I	77.I	77.1	77.5	77.9	78.4	70.5	19.0	10.5	10.4	10.2	1,0.1	1/00	119	1// 5	1115	113	11/3	1

127. Eskdalemuir: Louvred Hut: $h_t = 0.9$ metre.

February, 1923.

	-	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	83·5	a.
1		82.3	82.2	82·0 81·4	80.3	81.0	80·8 79·7	70.0	70.0	78.8	178.8	70 · I	80·8 79·7	170.0	180.0	70.7	170.7	170.7	79.4	79.7	80.1	80.3	80.7	81.8	81.5	80.2
3			79.2	79.0	78.7	79.3	79.3	79·I	79.0	79.2	80.0	80.0	80.3	80.7	80.6	80.4	78.5	78.8	78.0	77.8	77.8	77.4	77·I	76.8	77·2 73·9	79.1
4		77·8	77.2		76·0	74.8	74·1	73·6	74 · I	74.7	75.9	77.7	78·5 78·6	79·1 78·7	78.9	78·9	77.2	75.0	78.3	78.3	78.3	78.1	78.4	78.7	78.6	77.8
5			1		1	1	[[ſ	1	(1	i	i	1	i	1	1	1	1	ł .	ł	1	1	75.7	1
6		78·3 75·7	78.1	78·3 75·7	77.6	77.6	77.4	77.7	77.6	77.0													78·I	78.0	78·0	76 6
8		77.9	78·o	78.5	79.0	79.7	79·I	80.0	79.0	77.5															73.9	76.4
9 10		74.0	74.0	74·3 77·4	74.9	75.3	76.0	76.1	75.9	76.1	77.0	77.8	77.9	78·6	79·I	77.8	78·0	78.2	78.3	78·5	78.7	78.8	79.0	78.9	77.9	77.9
10																										
II 12		77:5	77.8	77.7	78·o	17h.0	775.5	75.0	170.2	17h.X	170.4	77.1	172.0	170.1	170.1	17/01	1/3.4	1/7 9	17.7	17.)	1//	1/1 /	1/T -	1/	76.3	76.4
13			76.3	-6	Mr M	175.0	177.8	75.6	176.2	176.0	176.8	76.8	77.2	クフ・2	177.0	77.1	76.8	76.7	76.7	76.5	76.3	76.1	76.0	75.6	75·0	76·3
14		74.5	74.0	73·9 73·0	73.6	72.5	77.4	777.4	777.1	777.7	172 · T	72.2	72.2	72.5	173.9	173.0	17.4.0	1/39	1/34	1/33	1/3 ~	1/3 ~	113 -	1/3		
15																										
16		75.8	76.1	76·1 76·2	76.1	75.6	775.77	175.5	175 · T	775.4	175.0	174.0	174.8	174.7	17/4:0	17/413	1/4 1	1/4 0	1/.) /	1/.)	1/.	1/	1/- /	12	,, ,	111
17 18		72·2	72.2	72.0	72.0												72:0	72.1	72·I	72.5	72.5	72·I	72·I	72.5	73·0	71.8
19		72.7	72.9	72·9 71·0	73.0	22.0	72.0	72.0	72.0	72.0	72.0	72.0	172.X	172·0	172.8	173.0	172.0	1/2	1/1.9	1/14	1/1)	1/-	/ - -	1/		
20																										
21		69.9	69.8	70.1	70.0	69.9	69.5	68.9	69.2																73.7	73.6
22 23			73·2 73·3	73.4	73.4	73·I	72.0	70.9	70.2																73.7	
24		73.6	73.6	73.8	73·I	73.1	72.1						75·3												75.7	75.2
25				75.0				/4.0	/5.0	/5.4	75.1	75.4	/5 3	/5 0	13 7	/5 0	150	/3	,,,,	_0	78.0	78:0	77.8	77.2	77.T	76.0
26		75.0	74.9	74·9	75.0	75.0	75.0	76.0	76.2	77.5	77.5	77.5	76.7	76.8	77.2	78.2	79.4	79.0	78·9	78·4 78·0	77.9	77.6	77.9	77.7	77.8	77:7
27 28		77.7	177.3	77.1	77.7	77.7	77.3	77.2	77.4	77.6	77.6	77.6	77.6	78·o	78.6	78.4	78.5	78·I	77.9	77:9	77.5	77.0	76.1	76.7	76.8	77.6
Mean				75.8	75.6	75.5	75.4	75.3	75.4	75.6	75.9	76.2	76.5	 76·7	76.7	76.8	76.7	76.3	75.8	75.7	75.6	75.6	75.6	75.7	75.7	75.9
G.M.T.		I.	2.	3.	4.	5.	6.	7.	8.	9.	10.		Noon		14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean

TEMPERATURE.

Readings in degrees absolute at exact hours, Greenwich Mean Time.

128. Eskdalemuir: Louvred Hut: h_t (height of thermometer bulb above ground) = 0.9 metre.

March, 1923.

Day.		ı.	2.	3.	4.	5.	6.	7-	8.	9.	ıo.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
1 2 3 4 5	7 7 7	76·0 76·5 75·0	75·9 76·9 75·2		75·6 77·0 76·3	76·2 76·9 76·3	76.0	75·4 76·3 76·5	76.3	76·3 76·7 77·6	77·1 76·9	77·2 78·7	78·8 77·9	77·8 78·4 80·0	81.2	78·0 78·0 80·2	78·2 77·7 79·4	77·7 78·5	76·1 77·5 77·0	76·0 76·0 75·4	76·1 76·0 75·0	76.6	76·3 75·6 73·7	76·2 73·6	76·1 76·0 74·0	a. 76·6 76·6 76·9 76·9
6 7 8 9 10	7 7 7	8·0 77·3 75·1	78·0 76·6 74·8	76.9	77·9 77·6 74·6	77.3	77·9 77·0 74·3	78·1 76·3 74·8	77·8 76·5 75·0	78·5 76·6 75·9	79·7 77·1 76·4	79·6 77·1	79·9 77·8 77·1	80·6 78·5 76·5	79·7 78·8 77·0	79·5 78·5 77·2	77.3	78·0 77·2 75·9	78·1 76·9 75·8	78·0 76·4 75·0	77·8 76·3 75·0		77·7 75·7 73·1	77·8 75·5 73·0	77·3 75·1 73·3	78·0 78·5 77·0 75·3 74 ·3
11 12 13 14 15	7 7 7	74·3 79·0 74·8	74·0 79·1 76·0	75.0 74.0 78.6 76.3 76.0	74·2 78·6 76·2	78.7	74·4 78·3 74·3	74·7 78·1 73·9	73·9 78·1	74·1 78·8 78·8	74.7 80.7 80.0	75·7 80·7 81·2	76·2 81·0 80·4	76·7 82·2 80·7	76·7 81·7 81·0	76·7 81·2 80·2	77·0 80·5 79·3	77·3 80·6 79·0	77·5 78·0 77·4	78·1 77·0	78·8 77·1 76·8	78.6		79·5 76·3 76·0	76·1 76·1	75·6 76·2 79·0 77·4 76·0
16 17 18 19 20	7	74·8 75·0	75·2 74·8	75·5 75·8 74·7 74·0 73·9	75·8 74·8	76·0 75·3 74·5 73·8 74·8	76·5 74·9	76·5 75·2	77·3 75·7	78·0 78·3	79·0 79·4 78·0	80·0 79·9 78·0	80·3	81·3 82·0 81·3	81.0 81.0	81·2 83·6 81·4	80·5 82·7 80·2	79·9 80·6 79·1	78·7 78·3 76·6	77·4 75·6 75·0	76·I 74·I 75·0	74·0 75·5	74.4 75.7 73.4 75.0 76.0	74·7 74·7 74·8	74·3 74·7	76·8 77·6 77·3 76·5 77·3
21 22 23 24 25	7 7 7	76·3 75·7 70·8	75·3 74·4 71·0	73·7 75·1 74·1 71·4 76·0	74·3 74·0	73.7	74·3 72·9	74·0 74·3	74·8 76·2	77·4 76·9	78·5 77·7	79.2	80·1 80·0	82·4 81·1 81·1	83·5 81·7 82·5	83·3 82·1 83·6	83·1 82·0 84·2	82·0 80·9 82·5	79·1 78·1 80·5	76·0 76·1	76·0 74·5 76·7	73·8	75·8 73·4 75·1	75·7 73·1 75·1	76·7 75·6 70·4 76·0 74·0	77 · 6 77 · 6 76 · :
26 27 28 29 30	8	31·8 33·1 78·8	82·8 77·8	75·2 82·5 82·5 77·3 75·3	82·3 81·9	82·8 81·3	83·0 80·9	83·4 80·8 75·0	83·9 81·0	84·3 81·1 78·7	85·8 81·8 81·9	86·4 82·2 84·0	86·9 82·3 85·8	87·0 83·7 86·5	87·7 83·3 86·3	88·9 82·8 86·3	88·6 82·7 85·1	88·0 82·2 85·1	87·5 82·0 83·1	86·9 81·1 80·3	86·3 80·4 78·0	80·2	84·1 80·0 76·9	84.0		85.0
31						74.3		l	l			-	·	I—-—			·		ļ	l		-				1
Mean	7	75.9	75.8	75.7	75·8	75.6	75.6	75.7	76.2	77.2	78.3	79·I	79.9	80.5	80.8	80.9	80.5	79.7	78.8	77.7	77.1	76.9	76.7	76.4	76.1	77.

129. Eskdalemuir: Louvred Hut: $h_t = 0.9$ metre.

April, 1923.

1 2 3 4 5	78·6 77·2	78·5 77·1	78·5 76·3	74.6	78·5 75·6 79·8	78·3 75·9 79·9	78·3 76·1 80·1	78·6 76·7 80·1	a. 78·6 78·7 78·3 81·9 78·8	79·0 81·0 83·1	79·6 82·7 83·2	79·3 83·0 83·9	79·9 83·4 83·9	79·8 84·0 84·0	79·5 84·8 83·9	79·5 84·1 82·4	79·8 83·2 82·0	79·8 82·5 81·0	79·3 79·1 80·8	79·1 80·7	81.2	77·6 79·7 80·9	77·7 79·3 79·9	79.4	78·8 79·7 81·2
6 7 8 9 10	75·7 78·3 74·7	75·3 78·0 74·6	75·0 77·7 74·4	75·1 75·2 77·7 74·3 73·9	75·3 77·6 74·2	74·3 77·0	74·3 77·1 74·8	75·5 77·8	76·4 76·4 77·6 75·9 74·5	76·9 79·2 76·2	77·2 79·0 76·7	77·8 79·1 76·7	79·3 79·3	79.7 79.4	79.5 79.5	78·7 76·9	79·8 77·9 75·8	76·4 75·8	74·7 74·7	77·0 74·5	77·8 74·9 74·4	75·7 77·5 74·6 74·3 75·8	77·7 74·4 74·8	78·I	
11 12 13 14 15	77·5 79·9 78·2	77·2 80·0	77·I	77·3 79·6	77.9	78·0	77·9 79·5	78·0 78·3	17X・2	78·5 79·6 78·9	79·6 80·0 78·7	80·2 81·2 78·2	81·4 81·4 78·0	81·6 78·0	83·1 80·8	83·1 82·0 77·0	83·2 82·0 77·7	81.7	81·1 76·3	81·0 76·1	80.3	80.1	79·9 75·3	199.0	80·3 77·4
16 17 18 19 20	71·8 72·0 73·0	71·1 71·0	71·0 70·9 74·1	72·0 70·2 74·3	72·0 70·6 74·3	73·0 71·3 74·9	74·I 73·9 75·3	77·3 75·0 75·8	78·a	80·0 76·3 78·5	77.1 78.1	81·4 77·1 78·8	81·7 77·9	82·0 77·4 77·7	77·3 77·7	77·2 77·9	76·8 77·3	79·8 76·4 77·0	77·3 76·0 76·5	75·6 75·8	73.4 75.3 73.6	75.0	74·9 72·9	72·3 72·1 74·1 71·5 74·9	74.7
21 22 23 24 25	75·7 74·3	75·8 60·0	75.7	75·0 75·2	74·9 74·9	75·0 73·9	75·5 75·7	76·1 77·8	75·6 78·1 78·9 78·1 78·8	78·7 77·5	78·9	75·5 80·0	79·1 77·3	78·9 80·0	79·6 77·9	79·0 78·8 80·2	78·5 77·5	78·7 76·5	74·9	73·1 73·3	73·8 72·5 75·5	75·5 74·2 71·1 75·2 78·4	74·2 70·4 75·6	71·0 74·2	75·5 76·7 75·5 75·9 77·7
26 27 28 29 30	74·3 73·3 74·1	72·7 74·6	72·9 70·9 75·3	72.0 70.8	71·8 69·1 75·0	72·1 70·1 76·0	70·1 74·2 77·8	77·6 78·4	78·8 79·1	80·0 78·3	80·0 79·7	80·0 78·2 81·8	78·0 81·8	79·I	80·0 79·9	79·2 80·3 82·0	80·7 82·0	79·3 79·8 80·1	77·0 78·7 79·4	77·8 78·0	74·3 77·6 78·2	76·I 78·0	75·0 78·0	74.0	76·3 78·7
Mean	 75.2	75.4	75.3	75.1	75.3	75.5	76.5	77:4	78.4	79.0	79.4	79.7	8o o	80.1	80.2	80.1	79.9	79.2	78.1	77:3	76.8	76.3	76·1	75.8	77.6
G.M.T.	 Ι.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	l	14.		-	17.		19.	20.	21.	22.	23.	24	Mean
	 <u> </u>	1	1) TE	The i	1	1		<u> </u>			<u> </u>	<u>!</u>	<u> </u>		l a oba	<u> </u>					<u> </u>	1	<u>'</u>	<u></u>

Readings in degrees absolute at exact hours, Greenwich Mean Time.

130. Eskdalemuir: Louvred Hut: h_t (height of thermometer bulb above ground) = 0.9 metre.

May, 1923.

Day.	ı.	2.	3⋅	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	
	a.	a.	$\frac{ }{ }a.$	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	Ī
I	81.0	80.3	79.9	79.7	79.5	79.8	80.9	81.2	82.3	84.0	83.7	83.4	84.2	84.5	83.5	84.7	84.8	84.5	82.8	82.1	81.9	81.3	00.5	79.9	
2	7 8·0	76.7	78.7	78.6	77.5	78.9	80.7	81.5	82.7	83.5	84.9	85.3	85.2	80.8	83.9	04.1	03.1	01.4	85.6	79.7	80·7	70.0	70.1	78.8	١
3	78.3	78.4	78.0	77.8	76.1	76.2	77.4	80.9	83.7	85.2	80.0	86·7 84·7	98	85.0	85.7	85.7	84.2	8410	82.2	82.5	81.6	81.6	81.2	81.5	1
4	78.0	77.1	76.0	75.7	76.1	80.0	82.8	82.0	82.3	03.0	86.0	86.8	86.4	86.4	86.0	86.7	86.6	85.0	84.2	82.5	81.6	79.9	78.4	76:0	ı
5	1 -	1	1	1	1	i	1	l.	!		1	1	ı		i	i				i				ļ .	1
6	76.3	77.8	78.3	79.0	79.0	80.1	82.3	82.7	81.6	81.0	81.7	83.0	83.2	83.6	84.0	81.5	80.2	80.1	80.0	79.5	78.7	76.7	75.7	75.8	١
7 8	74.6	72.4	72.1	71.1	70.0	73.2	77.1	79.5	81.1	02.0	82.7	83.7	84.8	84.7	85.1	82.7	82:0	82.7	80.7	77:0	76.0	76· o	75.6	73.3	J
	78.9	78.0	78.3	78.6	77.0	79.1	79.7	80.7	81.3	01.5	03.3	82·2 78·0	80.4	87.7	80.0	80.3	70.8	76.T	76.3	75.4	75:0	75:0	74.8	74.3	
9	73.3	71.4	70.3	70.0	70.8	72.0	74.2	76.5	77.6	78.0	70.8	78.2	76.6	76.7	77:0	76.4	76.5	77.8	78.3	75.8	76.5	77.0	76.0	76.5	1
10	73.7	73.3	72.8	72.3	$ ^{72\cdot7}$	1	1.	1	Į.	i	ı	1	ı		ŀ	1	1	l	ł			1	1	1 .	. I
11	75.8	75.9	75.1	75.2	75.1	75.9	76.3	77.6	77.2	76.6	77.3	76.9	76.0	77.0	76.2	76.0	76·o	76.0	75.6	75.2	75.3	75.0	74.9	74.4	ľ
12		74.0	74.1	74.0	74.2	75.1	76.4	76.5	77.4	80.4	80.9	79.5	78.7	75.7	80.9	81.0	80.3	78.7	77.3	76.0	75.5	74.6	74.0	74.2	
13	74.2	73.8	74.0	73.9	74.0	171.6	75.4	76.2	178.7	70.2	180.0	81.0	182.4	01.9	02.0	100.2	100.3	01.0	100.0	70.0	77.0	77.0	77.0	77·0	
14	76·o							76.2	76.7	77.2	77.9	79.0	75.9	87.5	79.9	79.7	70.3	77.5	77.0	70.9	77.1	70.0	75.0	76.T	١
15	75.9	74.6	73.7		1	1	!	1		ì	1	79.4	1	ì	i	1	ł	1			i		i .	1	1
16	76.0	76.0	75.4	75.0	74.9	75.3	76.3	76.7	77.9	78.6	79.6	8o·8	81.0	76.1	79.1	81.5	76.6	76.1	76.3	74.8	75.4	74.9	75.0	75.0	ľ
17	75.0	74.5	74.0	73.0	73.8	77.0	75.0	77.7	77.7	77.0	70.0	170.7	IXT•O	193·I	180.9	102.3	100.1	179.7	179.0	17.7.0	70.0	70.0	74.5	79.1	ı
18			75.0	73.0	72.4		76.4	78.3	79.1	80.1	80.6	81·0 82·9	79.8	80.2	79.9	80.0	80.3	87.0	87.0	87.2	80.7	80.6	80·T	70:0	Ŀ
19	79.0	78.9	79.0	78.8	78.7	79.0	79.4	80.0	81.0	80.2	80.7	81.3	81.6	81.6	81.5	81.7	82:0	81.5	8T.5	81.0	70:0	70.4	78.0	78.6	
.20	79.9	79.9	79.8	1	l .		i	1	1	1	1				1	l .	1	1	1	1	1		1	1	- 1
21	78.7	77.9	77.8	77.4	78.2	78.2	79.1	80.0	81.0	82.0	83.0	82.7	83.0	83.3	83.2	84.5	84.1	82.0	81.3	81.3	79.6	79.1	78.8	78.7	ŀ
22	78.7	77.8	77.0	76.7	76.9	78.3	80.7	82.2	83.1	93.0	83.9	82·8 77·9	03.0	01.1	00.0	79.4	80.7	80.7	80.5	70.6	77.4	75.8	74.5	74:0	ı
23	76.3	76.0	75.9	75.3	75.3	76.4	78.8	80.1	81.0	70.3	80.9	82.4	79.5	81.0	81.2	81.1	80.0	80.1	70.8	70.8	80:0	80.0	78.7	78.6	ŀ
24	74.3	74.0	73.0	72.7	72.8	73.9	79.3	01.0	02.3	81.8	83.3	81.4	70·I	80.7	81.4	81.2	81.2	70.8	79.0	78·T	77.0	77.7	77.5	77.3	þ
25	- 1	1.	1			1		i	1	1	l.		t .	1	1	1	1	1	1	ł	t	ł	1	!	- 1
26	77.3	78·o	77.1	77.8	77.8	78·o	79.1	79.8	81.5	82.0	80.9	79.7	81.5	80.0	81.7	80.8	80.4	79.5	79.7	77.9	78.0	78.3	78·2	78.1	
27	77.8	78.2	78.1	78.1	78.7	79.5	80.4	80.3	01.3	80.7	80.5	83.6	80.3	03.0	80.1	80.7	80:0	70.T	78.7	77.7	77.2	77.8	77.4	77:4	١
28			1	I	1		190.0	I ST.O	1×2.2	1×2.0	1X 4 + O	80·2 84·1	IX2 • 5	122.0	12/2:2	103.2	102.1	10117	100.7	17417	79.2	78.9	78.7	78.3	1
29	77.0	77.1	77.0	77.0	77.0	77.7	00.0	70.4	81.4	80.7	70.7	81.7	81.8	82.4	82.8	82.5	82.0	81.7	80.7	79.6	78.9	78.4	78·I	78.0	1
30			1	į.	1	1				1	1	1		1			1	1	1		1		1	i	- 1
31	77:9	77.9	77:3	77.2	77.6	77.9	78.2	79.1	79.3	79.0	80.2	80.5	80·8 	81.6	81.9	81.4	81.7	81.1	80.3	80.1	79.8	79.4	79.4	79.1	_
an	. 77.0	76.6	76.3	76·I	76.1	76.9	78.4	79.4	80.3	80.7	81.6	81.6	81.7	81.8	82.0	82.0	81.3	8o·6	80.0	78.9	78.3	77.9	77.4	77·I	

131. Eskdalemuir: Louvred Hut: $h_t = 0.9$ metre.

June, 1923.

																		_						····		
1 2 3 4		80·6 83·8 79·0	78·9 81·8 78·1	79·1 80·5 78·2	78·7 79·1 77·5	78·7 79·7	a. 79·1 79·0 80·8 78·1 78·0	79.4 86.2	86.8	86.1	86.8	87·9 86·7	85.9	85·6 82·8	86.1	85.8	85·6 82·5	85·3 81·0	84·3 81·3	83.0	81.8	81.0	81.1	81·0 70·0	81·0	83·7 80·2
6 7		1'	1	75·5 80·7 81·7	1	1	78·7 82·1 82·0	1	1		1	1	1	1	1	1	1		1	1	1	1		•	1	
8 9 10		83.0	83.0	84.4	82.9	82.9	82·9 83·0	83.0	83.3	82.7	82.9	83.1	83.7	84.7	84.5	83.7	83.2	84.0	83.3	83.0	82.3	82.0	81.1	81.2	80.9	83.1
11 12 13 14 15		74.2	13.2	12.4	123	1/4 -	79·5 81·0 83·3 80·3 76·0	113	190	199	100 0	00 9	-	T T	1			1	"	1					ļ	
16 17 18 19 20		73.5	72.8	71.8	73.6	74.4		81.2	82.6	83.6	84.0	85.0	85.6	80.3	05.0	05.5	03:0	01.7	88.8	86:4	85.7	84.0	82.8	82.0	81.0	
21 22 23 24 25		84·8 84·1	84.0	84.8	84.7	84.3	84·7 84·9 84·4 86·1 81·0	85·0 85·2	86.8	85·6 88·6	89.8	89.7	91.4	91.7	91.8	92.0	91.9	91.7	87·8 85·6	87.3	86·4 84·1	85·6 83·8	84·9 83·7	85·0 83·6	85·0 80·7	87·4 85·6
26 27 28 29 30		75·9 81·3 85·5	75·0 80·9 84·6	74·4 81·1 84·8	74·8 81·1 85·1	76·6 81·6 85·0	80·0 82·4 85·0 80·2 82·9	84·7 83·3 86·0	85·1 84·6 86·9	86·8 86·8 88·3	87·3 87·8 90·5	87·5 89·2 89·3	88·7 89·0 90·0	88·9 89·7 91·0	89·8 88·5 91·7	89·7 87·6 91·8	88·8 87·8 92·7	89·3 87·5 92·0	88·2 86·9 90·4 88·0	86·9 86·0 89·0 87·8	85·2 85·6 87·0 85·0	84.0 85.5 84.3 83.4	83·0 85·5 83·2 82·4	82·4 85·3 81·1 82·7	82·0 85·0 80·7 82·6	83·8 85·4 87·4 85·5
Mean							81.2																		81.3	
G.M.T.	•	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean

132. **Eskdalemuir**: Louvred Hut: h_t (height of thermometer bulb above ground) = 0.9 metre.

July, 1923.

Day.	ı.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
1 2 3 4 5	83·0 84·5 84·3	a. 81·2 83·0 84·5 84·2 85·2	84.2	84·8 84·1	84.5	83.8	84·I 84·9 85·2	84·5 85·8 85·7	84·8 85·7 86·7	a. 85.8 86.0 85.1 87.5 86.8	86·7 85·7 86·0	86·o 86·8	86·2 86·3 86·7	87·9 86·2	85·5 87·9 86·0	86·o 88·o 86·o	a. 86·9 85·7 87·8 85·9 88·9	85·0 87·1 85·4	86·4 85·1	85·0 85·6 85·0	85·o	84·9 85·0	84·8 85·0	84.6	85·7 85·4
6 7 8 9	89·4 87·8 85·7	89·0 87·2 85·6	88·7 87·0 85·6	88·3 86·2 85·4	88·9 86·2 86·7	88·4 90·3 86·2 87·0 88·1	91·4 86·7 88·0	93.8	95.2	98·2 87·2	97.5	93·6 87·4	93·8 87·7	92.8	94.8	95.3	94·3	93·3	93·0 87·9	92·0 85·7	90.7	90·3 85·4	88.7	88.1	93·2 92·2 87·3 89·6 89·2
11 12 13 14 15	82·5 83·7 85·7	82·5 83·6 85·2	82.6 83.8 85.0	82·3 83·0 84·0	83·0 84·7 85·5	87·3 84·5 86·7 85·9 86·8	86·1 86·4	88·4 89·5 88·1	93·2 92·0 89·6	94·3 92·3 80·8	95·0 93·0 89·3	95·0 94·7 91·2	96·0 95·2 92·3	96·3 96·0 92·7	96·8 96·0 92·0	95·5 91·5	97·3 94·4 91·0	90·0 92·3 89·7	94·I 90·5 88·9	89·0 89·1	88·9 87·5 87·2	86·2 86·5 86·9	86·0 86·2	86·0 86·4	89·5 88·3
16 17 18 19 20	83·0 79·9 82·9	82·9 81·4 82·1	83·5 81·1 81·6	83·6 80·9 81·4	83·7 81·1 82·2	86.8 83.8 83.0 83.1 87.7	84·0 84·7 83·5	85·1 84·6 83·5	84:0	85.6	85.6	85.0	86.2	86.5	87.4	87.4	87.3	88.0	86.0	85.0	83.8	83.5	81.9	82.2	86·7 84·1 84·4 85·0 88·8
21 22 23 24 25	87·7 86·6 83·1	88·0 86·3 83·0	88·2 86·4 83·2	88·4 87·0 83·1	88·4 87·1 83·5	85·2 88·1 87·3 83·8 86·3	88·0 87·3 83·7	88·1 87·8 85·3	88·6 87·5 87·4	88·8 87·6 88·4	89·1 87·9 89·0	89·3 89·5 89·1	89·6 90·2 88·0	89·3 88·9 88·3	89·0 87·1 87·8	88·9 87·0 87·0	89·2 86·5 85·8	85·0 85·0	85·0 84·3	84·4 84·3	87·6 83·9 84·2	87·2 84·2 84·6	83·9 84·9	83.0 85.1 82.7	85·5 86·1
26 27 28 29 30	81·3 82·9 83·7	80·9 82·7 83·8	80·1 82·7 83·9	80·0 82·9 83·8	80·3 83·0 83·9	82·9 83·1 83·3 84·2 84·9	83·8 83·9 84·9	85·3 84·2 85·3	86·9 84·5 86·3	87·3 84·9 85·3	86·8 85·4 86·3	88·1 85·8 87·0	88·o 86·1 86·o	87·9 86·9	87·5 87·0 85·4	86.6	86·7 87·1 85·7	85·1 86·0 85·3	84·7 85·1 85·1	83·9 84·8 85·2	83·2 84·1	82·9 84·0 85·0	82·9 83·8 85·0	82·8 83·5 85·1	84·3 84·4 84·7 85·1 86·0
31																	·	.		-		-		-	84.9
Mean	84.9	84.9	84.8	84.7	84.9	85.5	86∙0	86.9	87.7	88.3	88.6	89.0	89.3	89.5	89.5	89.2	89.0	88.3	87.7	86.9	80.1	85.7	85.5	85.1	87.0
133. Eskda	alemu	ir:]	Louv	red F	Iut :	$h_t =$	0.9	metr	e.													1	Augu	st, 19	23.
1 2 3 4	77·2 85·0 83·5	83.0	a. 83·7 77·2 85·4 83·0 78·5	79·4 85·1 82·1	79·7 84·2 82·7	a. 84.0 81.7 84.3 83.5 82.5	83·0 84·4 84·2	84·4 83·7 84·5	85·0 83·7 85·9	84·8 84·6 86·5	85·1 85·1 88·5	84·9 85·4 89·5	85·3 87·0 90·2	85·9 87·0 90·9	86·6 86·8 90·9	88.6 86.0 87.7 89.6 89.2	86·5 85·6 87·9	85·6 86·9 87·3	85·0 86·7	84·7 84·4 85·5	83·1 84·9 83·9 83·5 87·4	85·1 83·1 81·5		84·7 83·0 80·0	a. 85·3 83·4 85·1 85·5 86·9
6 7 8 9	86·6 86·9 81·8	86·0 86·7 81·1	85·6 86·6 81·4	85·1 86·6 81·6	84·6 86·5 81·2 86·8	85·0 86·3 81·1 86·9 83·8	85·8 86·4 84·1	86·0 86·8 86·4	87·2 86·9 88·6 88·3	89·6 87·3 91·0	89·6 87·5 89·9	89·8 87·9 89·2	87·2 88·1 87·7	87·4 88·2 88·2	87·1 88·9 88·0	89·6 87·4	89·0 87·4 90·2	89·5 87·6 89·0	87·0 87·5 88·0	85·5 87·5 85·8	84.0 87.7 84.2	83·9 87·9 84·8	82·5 87·9 85·8	82·0 87·6 85·6	86·7 86·8 86·1 88·2 85·8
11 12 13 14	181.1	85.9	86.0	79.4 86.3	80·0 86·5	83·7 81·0 86·6 82·1 82·2	81·9 87·0 84·2	83·1 87·5 85·2	84·8 87·9 86·5	87·0 85·6 88·2 87·0 84·0	86·7 88·8 88·0	87·7 89·3	88·0 89·8 80·0	88·0 90·6 80·0	88·2 91·7 89·1	89.2	87·6 89·8 88·2	87·9 90·8 87·1	87·5 89·0 86·2	87·1 85·5 83·9	86·3 83·7 82·1	87.0 83.0 82.5	87·2 83·0 82·0	81·2	85·5 84·6 87·4 84·7 84·1
16 17 18 19	83.9	84.4	83.2	83·0 84·1	83·2 84·1	83·0 84·6 84·3 83·9 84·0	85·0 84·8	84·9 85·5	86·4 85·4	80.7	87·3 89·6	88·6 88·3	86·6 88·6	86·6 88·6	87·7 87·5 88·4	88.0	86·1 86·7	86·0 86·7 86·1	84·6 86·4 85·1	84·3 85·5 85·0	84·7 84·8 85·0	84·5 85·0	84·1 84·5 85·0	84·0 84·5 84·9	84·5 85·2 85·9 85·5 86·0
21 22 23 24 25	84·0 79·9 81·8 83·5 78·0	82.0	80·3 82·4	80·4 82·4	81·9 82·4 83·0	87·1 81·9 82·4 82·7 76·0	82·6 82·0 84·0	83·2 83·2 86·3	83·8 83·7 86·8	88.0	85·3 83·9 86·0	83·8 88·o	85·1 83·2 86·0	86.4	85·0 83·1 84·0	85·2 85·0 83·1 83·5 83·2	84·6 83·1 84·3	84·1 83·9 84·0	82·9 84·1 84·0	82·0 84·2 83·0	82·5 84·2 81·4	84·5 80·9	81·9 85·0 80·9	78.2	85·2 82·9 83·3 84·1 81·9
26 27 28 29	84·7 83·0 82·2 75·6 79·0	82·9 82·3	82.2	83·0 82·4 74·I	82·9 82·4 74·3	84·2 82·6 82·4 75·0 79·9	82·9 82·3	83·2 82·9	83·3 83·1 81·8	85·5 83·0 84·0	85·6 85·4 84·3	84·8 86·3 84·0	85·5 86·9	85·0 85·2 82·3	85·2 86·7 82·0	84.0 85.1 81.9	81.0	83·3 83·3	80.8	82·7 82·3 81·0	81·0 81·0	80.9	82·2 78·0 80·9	82·4 77·2 80·2	85·1 83·5 82·9 79·8 81·9
30			1	1	1	1	0-	100.0	82.2	82.0	82.4	84:0	82.0	82.2	82.5	81.8	82.1	82.1	81.0	80.2	80.1	70.0	128.T	77.2	80.9
30	79.9			 				-		-	-	-		-		·		-	-	-			-		-
	79·9 82·5			 		79·3 82·8 6.		-		-	87.0	-	87.2	-		86.8		-	-	-		83.3	-	82.5	84·7 Mean

Readings in degrees absolute at exact hours, Greenwich Mean Time.

134. Eskdalemuir: Louvred Hut: h_t (height of thermometer bulb above ground) = 0.9 metre.

September, 1923.

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Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mear
1 2 3 4 5	84.8	a. 74.9 80.7 73.2 85.1 82.0	85.3	a. 76.0 80.9 71.8 83.2 82.3	71.2	71.3	73·2 82·3	77·0 83·2	81.7	a. 85·2 84·9 83·9 85·5 85·1	85·0 86·0	85·0 87·6	85·1 87·0	a. 85.9 85.9 85.0 86.0 86.2	87.7	86·9 84·9 85·0	84·3 84·3	84·0 84·2 83·5	83.0	79·5 84·1 82·1	a. 81·4 78·3 84·1 81·5 85·3	76·2 84·3 81·3	75·7 84·1 81·8	84·5 81·8	81.9
6 7 8 9	87·5 77·6	87·5 76·0	87·0 76·1	85·7 74·9	85·8 73·8	84·2 74·3	83·0 75·0	84·0 77·5	85.7 81.1	86.0	86·0 84·0	87·0 84·7	87·7 85·1	85·9 86·0	85.0 85.0 85.2 84.3 86.1	84·9 85·9	85·5 85·0	84.9	82·6 84·4 83·0	81·1 84·5	84.7	80·0 84·7	84·4 81·6	77·9 84·5 81·7	81.4
11 12 13 14 15	85·1 78·7	78.9	85·3 79·1	79.2	85·5 79·5 82·8	85.4 80.0 82.7	84·7 80·1 82·7	83·9 80·5	83·9 80·7 83·6	82·8 81·2 84·1	84·3 81·8 84·0	85·7 82·7 85·1	85·5 84·8 85·3	84·9 85·1 84·9	84·9 84·5 84·9 85·0 83·0	84.2	83·7 85·0 83·8	83·0 85·0 82·6	82·0 85·0 81·0	81·1 85·1 80·0	80·6 85·1 79·7	79·7 85·2 80·5	80.8	78·2 85·0 80·3	83.1
16 17 18 19 20	76·8 77·0 81·0 80·0 76·0	78·8 78·8 80·0 79·8 76·3	79.8	79·1 79·4	80·5 79·1	80·9 79·2	81·2 79·5	81·8 80·3	82·5 82·1 80·7	81·1 83·8 80·0	81.6 84.5 81.2	81·9 84·7 81·8	81·2 85·9 82·0	81·2 84·1 81·9	84·7 81·2 85·0 82·3 83·9	81·3 82·9 82·6	81·1 81·5 82·5	80·8 80·5 82·5	80·7 78·1 82·2	80·9 79·0 81·5	81·3 77·9 81·0	81·5 80·0	81·9 80·0 78·4	81·7 80·6	80 · 7 81 · 2 80 · 6
21 22 23 24 25	79.1	79.8	78.6	82·1 78·0	81·6 78·7	79.1	80·9 79·0	81·5 80·1 78·0	81·5 81·2	82·6 83·8	83·0 84·4 83·0	82·8 84·0 84·5	82·9 84·0 85·0	83·1 84·9 86·0	83·0 83·1 85·0 84·9 83·8	80·7 84·8 84·0	81·4 83·0 82·7	80·9 82·1 80·2	80·2 81·2 70·3	80·0 80·7 78·3	80·1 80·3 80·5	80·1 79·0 81·3	79·9 79·2 81·8	79·5 79·5 81·2	80.0
26 27 28 29 30	85.0 86.3	82.0	84·3 86·3	84·1 86·2	84·3 86·3	84·3 86·9	84·4 86·8	84·7 85·0	84·7 85·0 84·8	84·8 85·6	84·8 85·1	85·0 87·0 85·6	85·1 86·2 86·0	85·1 86·3	86·1 85·2 86·2 86·3 87·5	85·3 85·7	85·4 84·0 86·9	85·1 82·5 87·0	85·1 82·0 87·4	85·1 82·0 87·9	85.0 82.2 87.6	85·2 82·5 87·0	85·4 83·1	86.7	84 · 9 85 · 6
Mean	81.1	81.1	80.9	80.8	8o·7	80.7	81.0	82.0	83.1	83.8	84.3	84.7	84.9	85.0	84.9	84.6	84.1	83.2	82.5	82.2	82.0	81.8	81.9	81.7	82.6
35. Eskda	alemu	ir: 1	T 01117	з т	τ	1 4	0 0															_		46	
	1 a.	a.	$\frac{1}{a}$	$\frac{1}{a}$	$\frac{1}{a}$		a.	a.	a.	\ a.	a.	a.	<i>a</i> .	a.	a.	\overline{a} .	<i>a</i> .	a.	<i>a</i> .	a.	a.) a.	ctobe	a.	a.
1 2 3 4 5	81·1 77·8	a. 84·8 81·9 78·3	a. 84·8 81·8 78·1	(a. 84·7 82·0 77·8	a. 85·1 82·7 77·4	a. 83·1 82·0 77·4	a. 83·0 80·5 77·8	a. 81·9 81·7 78·1 78·2	a. 82·7 81·1 78·4	83·0 83·0 78·8	84.0 82.8 78.8	84.5 82.2 79.1 80.8	85·1 82·2 79·0 81·0	84·2 83·0 79·1		84.0 81.2 78.3	83·1 80·5 77·9 78·9	82·I 79·0 77·7 76·0	81·1 78·0 76·1 74·0	79·6 78·7 76·1	79·2 78·2 76·3	79.8 78.3 75.9	a. 80·7 78·4 76·5	a. 81.0 77.6 76.5 71.2	83 · 6 80 · 9 77 · 8
1 2 3 4 5 6 7 8 9	81·1 77·8 76·4 71·0 80·0 81·0 80·2	a. 84·8 81·9 78·3 76·6 71·3 80·0 81·4 80·2	a. 84·8 81·8 78·1 77·2 71·8 79·6 81·6 80·0 86·6	(a. 84·7 82·0 77·8 77·3 72·4 79·9 81·5 79·5	a. 85·1 82·7 77·4 77·3 73·2 79·8 81·8 79·1	a. 83·I 82·0 77·4 76·0 73·3 80·0 82·I 79·0	a. 83.0 80.5 77.8 76.5 73.8 80.2 82.3 78.1	a. 81·9 81·7 78·1 78·2 74·2 80·9 82·4 79·9 81·8	a. 82·7 81·1 78·4 78·0 77·2 81·0 82·9 81·4	83.0 83.0 78.8 78.7 78.8 81.2 82.9 81.9	84.0 82.8 78.8 79.4 79.8 81.8 82.9 82.9	84·5 82·2 79·1 80·8 81·0 83·1 83·2 82·8 82·6	85·1 82·2 79·0 81·0 81·0 83·7 83·7 83·0 84·0	84·2 83·0 79·1 79·9 81·9 82·8 84·0 82·5 84·0	83.8 82.0 79.4 80.9	84.0 81.2 78.3 79.7 82.2 83.8 84.6 81.9 81.5	83·1 80·5 77·9 78·9 82·1 82·0 84·7 81·1 81·0	82·1 79·0 77·7 76·0 82·3 81·7 84·3 80·7 80·1	81·1 78·0 76·1 74·0 82·0 80·6 84·1 81·0 81·0	79.6 78.7 76.1 73.0 81.5 80.5 83.5 80.9 80.9	79·2 78·2 76·3 73·2 80·9 80·8 83·7 80·7 80·3	a. 79.8 78.3 75.9 72.1 80.9 80.9 83.1 80.7 81.0	80·7 78·4 76·5 71·8 80·7 81·0 81·8 83·0 80·3	81.0 77.6 76.5 71.2 80.4 81.0 81.1 84.9 80.4	83.0 80.9 77.8 77.0 78.0 81.2 82.9 81.1 82.7
6 7 8 9	81·1 77·8 76·4 71·0 80·0 81·0 80·2 85·9 80·3 79·8 74·9 74·3	a. 84.8 81.9 78.3 76.6 71.3 80.0 81.4 80.2 86.2 80.7 78.2 77.4	a. 84.8 81.8 78.1 77.2 71.8 79.6 80.0 86.6 80.7 78.3 78.2 74.1	79.9 81.5 79.5 84.9 81.0 78.1 79.5 74.3	a. 85·1 82·7 77·4 77·3 73·2 79·8 81·8 79·1 84·0 80·9 77·4 79·4 75·1	a. 83·1 82·0 77·4 76·0 73·3 80·0 82·1 79·0 82·3 81·0	a. 83.0 80.5 77.8 76.5 73.8 80.2 82.3 78.1 81.3 81.2 78.5 79.1 75.8	a. 81·9 81·7 78·1 78·2 74·2 80·9 82·4 79·9 81·8 81·5 79·2 79·2 76·2	a. 82·7 81·1 78·4 78·0 77·2 81·0 82·9 81·4 82·4 81·5 80·0 80·0 77·5	83.0 83.0 78.8 78.7 78.8 81.2 82.9 81.9 81.7 81.1 79.9 79.1	84.0 82.8 78.8 79.4 79.8 81.8 82.9 82.0 82.0 81.8 80.2 79.7	84·5 82·2 79·1 80·8 81·0 83·1 83·2 82·8 83·6 82·3 80·0 80·2	85·I 82·2 79·0 81·0 81·0 83·7 83·7 83·0 84·0 82·3 82·7 82·1 80·8	84·2 83·0 79·1 79·9 81·9 82·8 84·0 82·5 84·0 80·8 80·3 80·3	83.8 82.0 79.4 80.9 82.7 84.2 82.1 83.4	84.0 81.2 78.3 79.7 82.2 83.8 84.6 81.9 81.5 82.7 82.1 81.0 79.7 80.3	83·1 80·5 77·9 78·9 82·1 82·0 84·7 81·1 80·0 79·3 78·8	82·I 79·0 77·7 76·0 82·3 81·7 84·3 80·7 80·I 82·0 77·4 77·9 75·7 77·8	81·1 78·0 76·1 74·0 82·0 80·6 84·1 81·0 80·6 77·6 77·6 77·6	79.6 78.7 76.1 73.0 81.5 80.5 83.5 80.9 80.9 80.7 76.0 76.2 75.9	79·2 78·2 76·3 73·2 80·9 80·8 83·7 80·7 80·3 80·7 74·8 75·5 76·5 74·8	a. 79·8 78·3 75·9 72·1 80·9 83·1 80·7 81·0 79·9 75·0 74·9 73·9	a. 80·7 78·4 76·5 71·8 80·7 81·0 81·8 83·0 80·3 79·4 74·5 74·6 73·0 74·9	a. 81·0 77·6 76·5 71·2 80·4 81·0 81·1 84·9 80·4 79·4 74·1 72·0 75·1	83.0 80.9 77.8 77.0 78.0 81.2 82.7 81.3 79.0 78.4 76.6
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Readings in degrees absolute at exact hours, Greenwich Mean Time.

10.

136. Eskdalemuir: Louvred Hut: ht (height of thermometer bulb above ground) = 0.9 metre.

Day.

November, 1923.

23.

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Mean	74.3	74.3	74.1	74.0	73.9	74.0	74·I	74.1	74.7	75.1	75.6	76·I	76 ·3	76.2	75.9	75.4	74.9	74.7	74.4	74.3	74.3	74.1	74.1	74.3	74
37. Eskd	alemu	ir: 1	Louv	red H	Iut :	$h_t =$: 0.9	metr	·e.													Dec	embe	er, 19	23
37. Eskd	alemu	a. 76·0	a. 76·1	$\begin{vmatrix} a \\ 76 \cdot 5 \end{vmatrix}$	a. 75·8	a. 75°9	a.	a.	a. 75°1		a. 75.5		a. 75·4	a. 75.9 76.0		75.9	75·6	a. 75·7	a. 75·8	a. 75.7 75.3	a. 76·0	75·8	75·7	75·I	75
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TEMPERATURE: ANNUAL MEANS OF HOURLY VALUES.

From readings in degrees absolute at exact hours, Greenwich Mean Time.

138. Eskdalemuir: Louvred Hut: $h_t = 0.9$ metre.

1923.

	1.	2.	3⋅	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
-	<u>a</u> .	${a}$	a.	-a.	${a}$	${a}$	<u>a.</u>	\overline{a} .	\overline{a} .	\overline{a} .	\overline{a} .	${a}$	\overline{a} .	${a}$	a.	<i>a</i> .	\overline{a} .	a.	-a.	-a.	\overline{a} .	-a.	-a.	a.	-a
7	8.19	78.11	78.04	77 · 93	77.99	78.23	78.73	79.23	79.88	80 · 43	80.99	81 · 29	81.62	81.68	81.65	81.37	80.96	80 • 40	79.83	79 34	79.00	78.72	78· 5 9	78・37	79.61

TEMPERATURE: MONTHLY MEANS AND DIURNAL INEQUALITIES.

The departures from the mean of the day are adjusted for non-cyclic change.

139. Eskdalemuir: Louvred Hut: $h_t = 0.9$ metre.

1923.

24 (1	1,0		G.M.T			_	6	_	0				Noon.				76		-0						
Month.	Mean.	Ι.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	NOOII.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.
		${a}$	$-{a}$	<u>a.</u>	${a}$	- - -	<u>a.</u>	\overline{a} .			a.	-a.	-a.	\overline{a} .	${a}$	\overline{a} .	\overline{a} .	a.	a.	${a}$	\overline{a} .	\overline{a} .	${a}$	$-{a}$	-a.
Jan.	277.67	-0.43	-o·35	-o·39	-0.45	-o·48	-0.43	−0.50	-0.56	-o·53	-o·17	+0.30	+0.69	+0.76	+0.93	+0.83	+o·68	+0.43	+0.31	+0.20	+0.07	-0.01	-o·18	– 0∙36	-o·32
Feb.	75.91	-o.18	-o·26	-0.31	-0.35	-o·45	-0.61	-0.62	-0.53	o·33	—o·o ₇	+0.29	+0.56	+0.81	+o·86	+0.90	+0.77	+0.45	-0.03	-0.10	-0.30	-0.24	-0·20	0.09	-o·o8
Mar.	77.62	-1.40	-1.81	-1. 86	-1.83	-2.00	−2·04	-1.95	-1.40	-r40	十0.73	+1.50	+2.27	+2.89	+3.18	+3.29	+2.82	+2.11	+1.13	+0.07	−0.50	-o·78	—o∙99	-1.24	-1.21
April	77:59	-2.04	-2.14	-2.30	-2.42	-2.38	-2.10	-1.06	-o·19	+0.78	+1.44	+1.77	+2.13	+2.39	+2.55	+2.57	+2.50	+2.33	+1.55	+0.45	-0.29	-o·85	-1.27	-1.48	-1.85
May	79.16	-2.23	-2.62	-2.85	-3.10	-3.13	-2.23	-0.76	+0.19	+1.09	+1.50	+2.47	+2.47	+2.55	+2.65	+2.85	+2.86	+2.19	+1.49	+0.84	-0.29	-o·87	-1.28	-I·72	-1.00
June	83.41	-2.47	-3.03	-3.14	-3.47	-3.02	-2.19	–o·98	-0.23	+o·74	+1.45	+2.06	+2.42	+2.93	+3.02	+3.10	+2.91	+2.76	+1.94	+1.07	+0.12	-o·74	-1.31	-1.67	-2.17
July	87.01	-2.05	-2.14	-2.22	-2.33	-2.05	- I·47	-1.02	-0 ·06	+o·74	+1.28	+1.59	+1.99	+2.26	+2.54	+2.52	+2.21	+1.97	+1.27	+0.64	-o·13	-0.91	-1.31	-1.51	-1·90
Aug.	84.67	-2.31	-2.56	-2.50	-2.45	-2.26	-1.88	-1.01	-0.05	+0.80	+1.60	+2.29	+2.66	+2.55	+2.50	+2∙70	+2.16	+1.70	+1.42	+o.66	-0.23	—o⋅88	-1.31	- I · 57	-2.12
Sept.	82.61	-1.39	-ı·43	-1.58	-1.73	- I·88	-1.89	-1.24	-0.60	+o·56	+1.51	+1.68	+2.07	+2.33	+2.34	+2.51	+1.91	+1.43	+o·56	-0.18	-o·52	-o·73	–o∙95	−o ·79	- I ·08
Oct.	80.16	-1.01	-o·97	-o·8 ₃	-0.72	-0.70	-0.77	-o·68	-0.33	+0.19	+0.74	+1.19	+1.62	+1.99	+1.86	+1.63	+1.27	+0.50	-0.07	-0.4 8	-o·74	-0.73	-o·98	وورو	-1.11
Nov.	74.71	-0.43	-0.41	-0.63	-0.69	-0.78	-0.72	-0.59	-0.59	—o ∙o6	+0·39	+0.90	+1.37	+1.62	+1.51	+1.20	+0.70	+o.18	+0.03	-0.34	-0.44	-0.51	-o·66	10:58	-0·48
Dec.	74.82	-0.43	-0.13	-o·17	-0.09	-0.19	-0.13	-6.13	-0.31	-o·37	+0.00	+0.49	+o·85	+1.02	+o·88	+0.60	+0.26	+0.02	-0.22	-o·34	-0.27	-0.51	−0.3 9	0·44	-0.41
Year	279.61	-1.39	- I · 49	— 1·56	-1.64	— I·61	- I·37	-0.91	-0.3 8	+0.27	+o·85	+1.38	+1.76	+2.01	+2.07	+2.03	+1.75	+1.34	+0.78	+0.51	−0·2 8	−0 ·62	-0.90	-1.04	-1.25

ABSOLUTE EXTREMES OF TEMPERATURE FOR EACH DAY.

Maximum and minimum for the interval 0h. to 24h., Greenwich Mean Time.

140. Eskdalemuir: Louvred Hut: $h_t = 0.9$ metre.

1923.

Month	Jai	.n.	Fe	b.	Ma	ır.	Apı	ril.	Ma	ıy.	Jur	ne.	Jul	ly.	Au	ıg.	Ser	ρt.	Oc	:t.	No	ov.	De	эс.
Day.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
1 2 3 4 5	a. 75·0 81·4 79·0 79·5 78·1	a. 65·6 75·0 76·1 72·6 74·0	a. 84·0 81·9 80·9 80·0 78·9	a. 80·3 78·6 76·5 72·2 73·7	a. 77·5 78·8 78·5 81·3 81·7	a. 75·9 74·8 76·1 73·0 73·5	a. 80·3 80·1 84·9 84·1 83·5	a. 76·0 77·0 74·6 79·0 74·3	a. 85·2 87·2 89·4 86·1 87·2	a. 79·3 76·4 76·1 74·9 76·9	a. 86·8 92·7 87·2 83·7 84·4	a. 78·7 78·3 80·9 77·4 73·2	a. 88·8 87·8 88·7 87·5 90·4	a. 80·5 82·8 84·3 84·0 85·0	a. 90·9 86·9 88·4 91·4 94·6	a. 78·1 76·8 82·9 79·7 78·2	a. 86·9 88·0 85·4 88·0 86·3	a. 74 · 7 74 · 9 70 · 5 81 · 2 81 · 8	a. 86·0 84·0 79·8 81·8 82·7	a. 78·3 77·0 75·9 75·9 70·8	a. 82·0 82·1 84·1 79·7 78·7	a. 72·1 75·0 75·1 74·9 71·8	a. 76·6 78·6 76·1 73·8 76·0	a. 75.0 74.1 70.0 71.9 70.9
6 7 8 9 10	77·1 83·0 82·0 77·8 78·5	72·1 76·3 75·5 74·2 74·0	78·6 79·2 80·0 79·5 79·0	74·2 74·2 73·0 73·8 77·2	80·2 80·7 79·4 78·0 75·4	75·6 77·3 75·1 72·7 73·0	77·5 81·1 80·0 78·1 79·1	74·9 74·3 74·3 73·8 73·6	84·5 85·6 85·5 83·0 80·0	74·9 69·9 77·9 69·7 71·7	86·5 86·9 83·5 87·4 85·0	78·7 81·4 81·7 82·8 80·8	99·7 98·2 91·1 93·5 93·1	85·1 88·1 84·9 85·3 87·1	90·7 90·1 91·3 92·0 90·2	84·5 82·0 80·9 84·0 81·8	87·5 88·1 86·3 85·3 87·1	84·1 77·6 73·7 80·7 78·8	84·6 84·8 84·9 86·9 82·9	79.4 81.0 78.0 79.4 80.1	76·8 76·7 78·1 76·9 80·1	69·0 68·9 71·2 71·3 72·0	75·0 78·8 79·1 76·3 80·5	69·3 72·6 67·9 66·4 76·3
11 12 13 14 15	77.8 76.8 79.3 81.6 81.6	73·0 68·4 66·9 76·5 77·1	79.0 78.3 77.4 75.0 75.9	75·9 74·8 74·9 73·0 72·3	77·7 79·6 83·0 81·8 77·9	74·4 73·9 75·8 73·8 75·0	85·8 83·3 83·0 79·3 84·3	74·3 77·1 78·2 74·7 73·2	78·8 81·5 83·2 80·1 82·4	74·3 73·7 73·8 73·3 73·3	88·1 85·1 86·0 87·8 83·9	78·0 78·1 80·5 74·9 72·0	97·8 97·3 96·2 93·0 88·0	84·2 82·0 82·7 83·9 85·2	91·2 88·4 92·1 90·2 88·6	78·0 78·0 81·1 79·0 79·9	85·5 86·4 85·4 86·1 84·8	81·0 78·1 78·2 79·0 75·7	83·1 82·7 81·3 81·8 81·4	73·8 74·1 72·0 68·9 73·9	83·4 79·0 75·5	73·9 77·2 74·0 70·2 70·0	80·8 80·1 79·9 80·2 78·7	79·3 79·1 72·3 75·0 74·8
16 17 18 19 20	80·0 78·4 80·0 82·2 76·2	78·1 76·9 76·0 76·1 70·0	79·2 76·4 73·0 73·1 74·5	75·7 72·4 70·3 71·0 69·9	81·1 81·5 83·8 81·8 83·0	74·0 74·1 73·1 73·5 73·2	82·0 83·0 77·7 78·9 80·4	72·2 70·2 70·0 72·7 70·5	81·7 83·9 81·7 83·1 82·1	74·7 72·8 72·0 78·5 78·0	83·7 86·7 93·1 87·2 89·0	74.0 71.7 80.3 78.7 78.3	90·2 87·5 88·7 89·2 92·4	84·1 82·5 79·7 81·2 87·2	88·4 88·9 90·4 88·8 89·0	82·0 82·9 83·9 83·2 83·5	86·0 82·9 86·0 82·7 85·0	76·0 75·9 77·1 75·1	83·3 84·9 85·0 86·7 83·3	79·5 78·3 81·3 76·0 76·2		73·7 73·0 73·3 72·5 73·0	81·9 82·3 78·4 74·3 74·2	78·7 78·4 73·4 70·0 68·3
21 22 23 24 25	81·7 81·0 79·3 82·2 80·9	71·2 72·0 67·8 79·2 79·0	73.7 75.6 76.6 76.4 75.8	68·9 72·3 70·0 72·1 74·2	82·7 83·8 82·2 84·5 83·6	72·8 73·8 70·4 70·2 72·9	78·4 81·8 79·3 81·6 82·1	73·8 72·9 70·4 69·3 73·0	85·1 85·0 82·2 83·1 84·3	77·3 76·2 73·9 71·6 77·1	89·0 89·0 92·1 89·2 87·7	82·4 84·3 83·8 80·7 76·1	91·5 89·9 90·6 90·9 89·6	85·2 86·7 83·0 82·9 82·7	87·3 86·9 85·2 89·0 85·7	79·3 78·7 81·7 78·2 74·5	84·7 84·0 85·0 86·1 85·0	76·7 79·0 77·2 75·9 81·0	82·9 81·0 80·9 81·9 82·6	79·9 78·0 77·9 76·1 78·8	76·1 75·3 74·9 72·7 75·5	72·9 73·3 70·7 63·0 63·1	73·9 81·2 76·0 75·5 71·8	70·4 73·0 71·5 63·9 62·8
26 27 28 29 30	80·4 82·2 81·8 82·5 83·0	79·1 79·0 78·4 78·8 80·1	79·7 78·5 78·6 —	74·7 76·7 76·1 —	87.0 89.0 83.7 87.2 85.0	73·9 81·5 79·7 74·6 73·5	82·9 81·0 81·0 83·2 84·3	75.0 71.2 69.1 74.0 76.9	82·8 85·1 81·1 84·6 83·1	77·1 77·2 76·6 76·9 77·8	90·2 91·0 93·2 91·9 86·5	74·3 80·9 80·5 76·8 81·5	88·4 88·8 87·9 87·1 89·2	81·8 79·8 82·5 83·5 83·9	87·3 86·6 88·0 84·7 87·0	82·5 81·8 77·2 73·9 78·6	87·3 86·1 88·2 87·9 87·8	82·1 84·1 81·1 83·3 85·0	81·2 81·9 83·5 84·0 85·3	77.5 79.3 79.2 79.3 80.7		73·5 69·9 71·0 70·8 64·1	73·5 74·4 75·3 74·1 74·9	71.8 72.2 64.7 62.6 73.9
31 Mean	83·0 80·1	79·9 74·8	77.8	73.9	81.3	72.4	81.4	73.7	82.2	77.2	87.8	78.7	91.0	82.9	85.1	77·2 80·1	86.1	78.6	83.0	75·0 77·1	77.5	71.5	82·0 77·2	73.7

Note. The initial 2 or 3 of the readings is omitted, i.e., 275.0 degrees absolute is printed 75.0.

Percentages at exact hours, Greenwich Mean Time. Determined as explained on page 16.

141. Eskdalemuir: Louvred Hut: h_t (height of thermometer bulbs above ground) = 0.9 metre.

January, 1923.

										I	1			1			1	1	1	- 1						
Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
1 2 3 4 5	99 86 84 100	% 91 94 90 82 97	% 92 97 89 79 94	% 94 97 86 81 89	% 94 97 86 77 94	% 94 99 88 77 89	% 95 99 85 85 94	% 96 99 88 84 90	% 96 99 91 85 94	97 100 95 80 91	96 100 92 74 94	% 95 86 87 75 92	% 90 92 90 74 94	% 87 92 86 75 91	% 91 93 86 84 87	% 93 90 88 91 93	% 94 92 92 93 88	% 95 92 83 95 85	% 95 92 86 97 81	% 94 92 80 97 99	% 94 92 76 95 87	% 93 89 80 93 82	% 93 94 87 95 72	% 95 86 84 95 80	% 93·4 94·5 86·7 85·1 90·2	mb. 4·9 8·7 7·3 6·2 7·1
6 7 8 9	87 95 97 93 78	89 97 96 95 93	86 97 97 96 91	86 99 95 96 93	85 99 96 91 91	94 99 86 87 90	87 100 84 81 91	87 99 85 81 84	88 99 82 80 84	93 98 82 81 76	88 98 80 81 76	91 96 81 76 74	93 99 75 75 73	91 100 73 87 79	93 97 76 84 71	93 100 80 85 73	91 96 81 81 77	95 97 78 84 79	93 95 62 82 79	95 96 61 82 75	93 95 93 81 76	96 94 87 71	97 97 94 84 79	97 99 94 81 80	91·0 97·5 84·4 84·9 80·6	6·2 9·9 7·8 6·2 6·1
11 12 13 14 15	81 89 97 99 77	82 90 97 95 75	82 91 97 92 78	81 89 97 88 76	81 92 98 88 73	76 93 98 86 73	77 95 98 95 74	80 98 98 74 74	79 98 98 78 74	78 98 99 79 76	77 98 99 74 77	74 90 97 73 81	80 83 95 64 87	78 80 93 69 92	78 82 99 68 92	77 86 97 65 92	78 93 97 73 95	83 96 99 70 94	82 97 96 79 94	81 97 96 76 94	85 94 97 77 86	87 94 94 76 88	91 96 97 70 85	91 96 96 72 86	80·6 92·1 97·0 78·5 82·7	5·8 5·3 6·1 7·1 7·7
16 17 18 19 20	88 97 91 94 82	89 99 86 97 84	89 90 88 97 75	90 88 88 94 81	91 90 94 81 76	95 91 80 80 75	97 91 84 85 76	96 93 82 87 75	97 94 85 93 70	97 93 87 94 67	93 97 82 94 62	97 97 74 94 55	94 96 76 93 55	96 94 84 93 53	97 93 78 88 53	94 96 80 91 53	96 96 80 87 62	93 96 81 81 66	95 96 84 75 72	97 97 80 69 70	97 96 80 78 73	97 94 86 70 75	99 91 87 80 77	99 88 91 80 69	94·5 94·1 83·6 86·7 69·2	8·7 8·2 7·3 8·4 4·6
21 22 23 24 25	78 86 80 87 80	72 88 82 85 79	83 82 85 85 80	89 88 82 84 81	88 89 86 81 86	87 85 90 79 92	93 86 93 77 92	95 86 94 78 84	96 86 94 81 81	98 90 94 79 85	98 78 83 82 87	98 84 77 77 82	97 79 78 79 85	89 84 71 70 84	91 88 73 79	88 90 79 76 81	85 82 82 81 84	86 82 86 81 82	86 78 88 83 80	81 82 97 84 82	85 79 94 85 74	82 74 96 84 76	80 80 91 80 87	80 81 86 77 86	87·5 83·6 85·8 80·4 82·7	7·2 7·6 5·5 8·4 8·2
26 27 28 29 30	83 83 85 92 91	83 78 91 87 89	82 77 88 93 88	83 77 87 96 92	86 83 86 92 88	87 81 85 91 91	85 80 84 89 87	90 83 86 89 86	86 85 86 90 85	85 84 89 91 84	86 83 86 89 92	85 79 86 88 92	84 82 82 89 95	84 83 86 89 95	85 81 86 87 97	86 85 82 89 95	87 85 85 87 87	87 84 80 94 86	89 83 86 88 81	81 79 86 91 84	78 79 88 93 89	82 79 88 89 91	84 81 90 89 92	82 82 90 93 88	84·7 81·5 86·0 90·2 89·5	8·2 8·6 8·7 9·6 9·8
ı	92	87	88	92	92	88	82	84	92	92	88	90	96	96	97	94	93	96	96	92	93	91	87	87	91.1	10.1
31	92					ا ـ ـ ا	87.8	87.3	87.9	88.1	86.6	84.6	84.7	84.7	84.7	85.9			85.8							†7:5
Mean Vapour Pressure*	83·4 mb. 7·2	mb. 7·2	mb.	mb. 7·2	mb. 7°2	mb.	mb. 7·1	mb. 7·1	mb. 7·1	mb. 7 '4	mb.	mb.	mb. 7·7	mb.	mb. 7.7	mb. 7·6	mb. 7·6		mb. 7·5				l	7.3	‡7.4	
Mean Vapour	83·4 mb. 7·2	mb. 7·2	mb.	mb. 7·2 red H	mb. 7·2 Hut:	mb. 7 · 1 ht =	mb. 7·1 = 0·	mb. 7·1 9 m	mb. 7·1	mb. 7 '4	mb.	mb. 7·5	mb. 7·7	mb.	7.7	7.6	7.6			7.4	7.0	7.2		7.3	‡7.4	y, 1923.
Mean Vapour Pressure*	83·4 mb. 7·2	mb. 7·2	mb. 7.7	mb. 7·2	mb. 7·2	mb. 7 · 1 ht =	mb. 7·1 = 0·	mb. 7·1	mb. 7·1	mb. 7·4	mb. 7·5	mb. 7:5	7.7	mb. 7·7	mb. 7.7 96 78 66 70 84	7.6		7.6	7.5			1	7.3	7·3	† _{7·4} bruar	
Mean Vapour Pressure* 42. Eskdale	83·4 mb. 7·2 muir % 80 78 89 89	mb. 7·2	mb. 7.7 ouvr % 72 79 80 88	mb. 7·2 red F	mb. 7·2 Hut: % 79 80 82 87	mb. 7 · 1 ht = % 84 78 82 86	mb. 7·1 = 0· % 86 71 85 87	9 m % 89 76 86 88	mb. 7·1 etre. % 92 83 85 86	mb. 7·4	mb. 7·5 100 86 74 76	mb. 7.5	% 99 80 67 68	mb. 7·7	7.7 % 96 78 66 70	7·6 % 93 78 79 82 94	7·6	% 99 94 86 90	7·5 % 100 93 88 92 88	% 96 99 85 93	% 96 97 91 94	7·2 % 97 93 91 93	7·3 % 97 90 89 91	7·3 Fee % 92 93 89 92	\$7.4 bruar % 90.3 84.2 81.3 84.5	mb. 10·2 8·5 7·6 6·2
Mean Vapour Pressure* 42. Eskdale 1 2 3 4 5 6 7 8 9	83·4 mb. 7·2 muir % 80 78 89 92 81 90 84 100	mb. 7·2 : L % 69 81 77 84 90 84 89 83 100	mb. 7.7 ouvr % 72 79 80 88 95 80 89 86 99	mb. 7·2 red F % 86 81 84 87 92 99	mb. 7 · 2 Iut: % 79 80 82 87 88 80 95 90	mb. 7·1 ht = % 84 78 82 86 86 82 96 94 99	mb. 7·1 = 0· % 86 71 85 87 84 80 88 89 99	9 m % 89 76 86 88 86 80 78 86	mb. 7·1 etre. % 92 83 85 86 88 85 79 88 88 87	% 94 86 76 83 86 92 91 95 88	mb. 7·5	mb. 7·5 % 97 78 73 69 84 95 97 88 87	7.7 % 99 80 67 68 82 97 95 92 90	% 94 77 68 73 83 94 92 78	% 96 78 66 70 84 90 93 88	7·6 % 93 78 79 82 94 100 91 94	7·6 % 97 87 79 84 94 100 90 89 78	7·6 % 99 94 86 90 94 99 91 94 93	7·5 % 100 93 88 92 88 97 86 99 80	% 96 99 85 93 90 100 89 99 83	% 96 97 91 94 84 95 87 94 82	7·2 % 97 93 91 93 80 100 84 96 75	7·3 % 97 90 89 91 77 96 90 100 72	7·3 Fee % 92 93 89 92 79 90 86 93 74	\$\frac{1}{7\cdot4}\$ \$\frac{1}{9}\text{order}\$ \$\frac{9}{90\cdot3}\$ \$\frac{3}{84\cdot5}\$ \$\frac{86\cdot9}{90\cdot2}\$ \$\frac{90\cdot2}{89\cdot4}\$ \$\frac{91\cdot6}{88\cdot6}\$ \$\frac{1}{88\cdot6}	mb. 10·2 8·5 7·6 6·2 7·5 7·0 7·0 8·1 6·8
Mean Vapour Pressure* 42. Eskdale 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 14 14 15 14 15 16 16 16 16 16 16 16	83·4 mb. 7·2 muir % 80 89 92 81 90 84 1100 81 92 95 95 91	mb. 17·2 2 3 4 4 5 6 9 8 4 8 9 9 7 9 5 9 3 5 6 6 9 8 3 1 100 100 100 100 100 100 100 100 100	mb. 7.7 ouvr % 72	mb. 7·2 red F red F 88 87 99 91 88 88 91	mb. 7·2 Hut: % 79 80 82 87 88 80 95 87 91 93 91 90	mb. 7·1 ht = % 84 78 82 86 86 86 99 89 99 89 95 88 88	mb. 7·1 = 0·	mb. 7·1 9 m % 89 76 86 88 86 89 99 91 95 92 88	mb. 7·1 etre. % 92 88 85 86 88 85 79 88 89 88 87 99 88 87 92 92 88	mb. 7·4 % 94 86 76 83 86 92 91 95 88 88 94 100 88 88	mb. 7·5 % 100 86 74 76 84 92 89 97 81 87 93 100 88 88	mb. 7·5 % 97 78 73 69 84 95 97 88 87 86 84 88 87 88	7·7 99 80 67 68 82 97 95 92 90 87 92 90 84 87	mb	7.7 % 96 78 66 70 84 90 93 88 77 88 88 88 88 84 84 87	7·6 % 93 78 79 82 94 100 91 94 75 88 88 91 86 88	7·6 % 97 87 79 84 94 100 90 89 78 91 89 88 88 88	7·6 % 99 94 86 90 91 94 93 93 93 91 99 88 91	7·5 % 100 93 88 92 88 97 86 99 80 93	7:4 % 96 99 85 93 90 100 89 99 83 90 90 91	% 96 97 91 94 82 91 94 96 87 91	7.2 % 97 93 91 93 80 100 84 96 75 90 97 98 86 91	7·3 % 97 90 89 91 77 96 90 100 72 89 95 99 90 91	7:33 Fee % 92 93 89 92 79 90 86 93 74 94 100 91 91	\$\frac{1}{5}\text{order}{\frac	mb. 10·2 8·5 7·6 6·2 7·5 7·0 7·0 8·1 6·8 7·5 8·7 7·4 6·9 5·6
Mean Vapour Pressure* 42. Eskdaler 1	83·4 mb. 7·2 mb. 7·2 muir % 80 78 89 99 84 100 81 99 59 99 99 99 99 99 99 99 99 99 99 99	mb. 17·2 : L % 69 81 77 84 90 83 100 87 88 97 95 93 92 99 84 84 84 94	mb. 7.7 ouvr	mb. 7·2 red F // 73 86 81 84 87 92 99 91 88 91 92 99 95 83	mb. 7·2	mb. 7 · 1 l l l l l l l l l l l l l l l l l l	mb. 7·1 86 71 88 87 84 80 88 89 99 91 88 92 95 91 88 94	mb. 7·1 9 m % 89 76 88 86 86 89 91 95 92 88 89 92 93 97 92 94	mb. 7·11 etre. % 92 83 85 86 88 87 99 88 87 92 92 92 92 92 93 90 95 94	mb. 7·4 % 94 86 76 83 86 92 91 95 88 88 94 100 88 88 91 95 84 90 95	mb. 7·5 % 100 86 84 92 89 97 81 87 93 100 88 88 99 94 86 98	mb. 7·5 % 97 78 73 69 84 95 97 88 87 86 84 88 85 88 85 88 88	7·7 % 99 80 67 68 82 97 95 92 90 84 87 86 98 84	mb. 7.7 9 94 77 68 73 83 94 94 92 78 90 99 85 86 84 85 89 88 84	7·7 % 96 78 66 70 84 90 93 88 87 77 88 88 94 84 87 88 88 86 95 98 84	7·6 % 93 78 79 82 94 100 91 94 75 88 91 86 87 97 84	7·6 % 87 87 79 84 94 100 90 89 98 88 89 90 88 88 87 95 84	7·6 % 99 94 86 90 94 93 93 88 91 99 88 91 99 88 91 99 88 91 87	7·5 % 100 93 88 92 86 97 86 99 80 93 97 99 90 91 88 94 91 92 84	7·4 % 96 99 85 93 90 100 89 99 96 90 91 91 92 91 91 84	7·0 % 96 97 91 94 84 95 87 94 96 87 99 90 90 90 92 82	7.2 % 97 93 91 93 80 100 84 96 75 90 97 98 86 89 91 90 88 88 88 88 88 88 88 88 88 8	7·3 % 97 90 89 91 77 96 90 100 72 89 95 99 90 87 83 83 85	7·33 Fee % 92 93 89 92 79 90 86 93 74 94 100 91 90 86 84 93 86	\$\frac{1}{7\cdot4}\$ \$\frac{1}{90\cdot3}\$ \$\frac{84\cdot2}{81\cdot3}\$ \$\frac{84\cdot5}{86\cdot9}\$ \$\frac{90\cdot2}{89\cdot4}\$ \$\frac{90\cdot2}{88\cdot6}\$ \$\frac{91\cdot6}{88\cdot6}\$ \$\frac{91\cdot4}{90\cdot2}\$ \$\frac{92\cdot1}{89\cdot6}\$ \$\frac{80\cdot4}{88\cdot4}\$ \$\frac{90\cdot2}{88\cdot4}\$ \$\	mb. 10:2 8:5 7:6 6:2 7:5 7:0 7:0 8:1 6:8 7:5 8:7 7:4 6:9 5:6 6:0 7:3 6:1 5:6 5:2
Mean Vapour Pressure* 42. Eskdale 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 28	mb. 7·2 mb. 7·2 mb. 7·2 mb. 7·2 mb. 7·8 ms. 89 ms. 89 ms. 89 ms. 81 ms. 89 ms. 81 ms. 81 ms. 81 ms. 85 ms.	mb. 17·2 : L % 69 81 77 84 90 83 100 87 88 97 95 93 92 99 84 84 84 80 93 866 88 91 96 85 94	mb. 7.7 ouvr % 72 79 80 80 89 95 80 92 92 92 92 92 92 93 84 95 86 80 83 89 87 91 92 87 89	mb. 7·2 1 1 1 1 1 1 1 1 1	mb. 7·2	mb. 7 · 1 l ht = % 84 l 78 82 86 86 86 89 99 89 95 88 88 89 39 95 82 82 82 82 82 82 82 92 88 89 95 91 89 91	mb. 7·1	mb. 7·11 9 m % 89 76 86 88 86 89 91 95 92 88 92 93 97 96 96 90 86 90 87	mb. 7·11 etre. % 92 83 85 86 88 87 99 88 87 92 92 92 88 89 93 93 90 95 94 81 96 91 85 91 88 87	mb. 7·4 % 94 86 76 83 86 92 91 95 88 88 91 95 84 100 81 98 88 88 91 95 84 88 88 91 88 88 88 91 88 88 88 91 88 88 88 88 88 88	mb. 7.5 % 100 86 74 76 84 92 89 97 81 87 93 100 88 88 91 94 86 70 93 87 84 82 93 88 86 91	mb. 7·5 % 97 78 73 69 84 95 97 88 87 86 84 88 85 88 87 86 84 88 85 88 81 86 98 84 70 92 86 81 83 95 88 84 91	7·7 9% 99 80 67 68 82 97 95 92 90 87 86 91 86 98 84 69 93 81 80 83 90 89 87 88 88 88 88 88 88 88 88 88	mb. 7.7 7 94 77 68 83 83 94 94 92 78 99 85 86 84 74 93 79 80 83 90 89 89 90	7.7 % 96 78 66 70 84 90 93 88 77 88 88 94 84 87 88 86 95 98 88 81 93 83 83 100 90 94 93	7·6 93 78 79 94 75 88 91 86 87 97 88 91 86 87 97 88 91 86 87 97 86 87 97 97 88 88 91 86 87 97 97 97 97 97 97 97 97 97 9	7·6 % 97 87 79 84 100 90 88 97 88 91 89 90 88 88 87 95 84 83 93 91 82 85 95 83 91	7·6 % 99 94 86 90 94 93 93 93 93 87 94 88 93 88 97 96 76 96 89	7·5 % 100 93 88 92 88 97 86 99 80 93 97 99 90 91 88 94 91 92 84 88 93 90 89 87 96 79 90 92	7·4 % 96 99 85 93 90 100 89 99 83 90 91 91 92 91 91 84 89 93 90 81 97 76 88 88	7.0 %6 96 97 91 94 84 95 87 91 90 90 90 92 82 79 92 84 96 76 91 89	7·2 % 97 93 91 93 80 100 84 96 75 90 97 98 86 91 90 89 88 93 80 91 88 96 79 88 90	7·3 % 97 90 89 91 77 96 90 100 72 89 95 99 90 87 83 93 93 85 82 93 90 88 95 81 88	7·3 Fee % 92 93 89 92 90 86 86 89 91 90 86 84 93 86 80 93 88 89 93 85 89 89	\$\frac{1}{90.3} \\ 84.2 \\ 81.3 \\ 84.5 \\ 90.2 \\ 89.4 \\ 91.6 \\ 88.0 \\ 89.1 \\ 89.4 \\ 90.2 \\ 92.1 \\ 89.0 \\ 91.6 \\ 88.6 \\ 85.9 \\ 93.3 \\ 86.3 \\ 88.3 \\ 89.6 \\	mb. 10·2 8·5 7·6 6·2 7·5 7·0 7·0 8·1 6·8 7·5 8·7 7·4 6·9 5·6 6·0 7·3 6·1 5·6 5·2 5·0 4·9 5·6 6·0
Mean Vapour Pressure* 42. Eskdale 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 28	mb. 7·2 mb. 7·2 mb. 7·2 mb. 7·2 mb. 7·2 mb. 7·8 mb. 7·	mb. 17·2 : L % 69 81 77 84 90 84 89 83 100 87 88 97 95 99 84 84 84 86 88 91 96 88 91 88 188	mb. 7.7 ouvr % 72 79 80 80 89 95 80 92 92 92 92 92 92 93 84 95 86 80 83 89 87 91 92 87 89	mb. 7·2 1 1 1 1 1 1 1 1 1	mb. 7·2	$\begin{array}{l} \text{mb.} \\ 7 \cdot 1 \\ \\ 7 \cdot 1 \\ \\ 84 \\ 78 \\ 82 \\ 86 \\ 86 \\ 86 \\ 86 \\ 86 \\ 86 \\ 8$	mb. 7·1 86 71 86 71 87 89 99 91 88 92 95 91 88 92 95 91 88 92 95 91 88 92 95 91 88 91 89 92 85 89 1 89	mb. 7·11 9 m % 89 76 86 88 86 89 91 95 92 88 92 93 97 96 96 90 86 90 87 91 88 88 92	mb. 7·1 etre. % 92 83 85 86 88 85 79 88 89 93 90 95 94 81 85 91 85 91 89 88 87 89 1 mb.	% 94 86 76 76 883 886 92 91 100 888 88 89 1 95 884 99 90 881 98 88 88 89 90 88 88 88 89 90 88 91 98 88 88 88 88 91 90 88 90 80 90 90 80 90 90 80 90 90 90 90 90 90 90 90 90 90 90 90 90	mb. 7.5 % 100 86 74 76 84 92 89 97 81 87 93 100 88 88 91 94 86 70 93 87 84 82 93 88 86 91	mb. 7:5 % 97 78 73 69 84 95 97 88 87 86 84 88 85 88 87 86 84 88 85 88 81 86 98 84 70 92 86 81 83 95 88 84 91	7·7 % % 99 80 67 68 82 97 95 90 87 92 90 84 86 98 84 69 93 81 80 83 99 87 88 88 88 88 88 88 88 88 88	% 94 77 68 73 83 94 94 92 78 99 85 86 84 85 89 98 85 89 99 86 84 94 94 94 94 94 95 86 84 85 89 98 89 98 89 89 89 89 89 89 89 89 89	7·7 % 96 78 66 70 84 90 93 88 88 88 84 87 88 88 86 95 98 88 81 93 76 83 83 100 94 93 86 93 88 88 88 88 88 88 88 88 88 8	7·6 % 93 78 79 82 94 100 91 94 75 88 88 891 86 87 97 84 86 87 97 84 86 89 91 87 97 84 86 88 91 87 97 88 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 91 88 88 88 88 91 88 88 88 88 91 88 88 88 88 91 88 88 88 88 91 88 88 88 88 88 91 88 88 88 88 88 91 88 88 88 88 88 88 91 88 88 88 88 88 88 91 88 88 88 88 88 91 88 88 88 88 88 91 88 88 88 88 88 91 88 88 88 88 88 91 88 88 88 88 88 91 88 88 88 88 88 88 91 88 88 88 88 88 88 88 91 88 88 88 88 88 88 88 88 91 88 88 88 88 88 88 88 88 88 88 88 88 88	7·6 % 97 87 79 84 100 90 88 97 88 91 89 90 88 88 87 95 84 83 93 91 82 85 95 83 91	7·6 % 99 94 86 90 91 93 93 91 87 94 88 93 88 93 88 97 96 96 96 91 91 91	7·5 % 100 93 88 92 88 97 86 93 97 99 90 91 88 93 90 89 87 96 79 90 90 92	7·4 % 96 99 85 93 90 99 96 90 91 91 92 91 94 89 93 90 97 76 88 88 90 90 90 90 90 90 90 90 90 90 90 90 90	7·0 % 96 97 91 94 84 95 87 91 90 90 92 82 79 92 84 96 76 91 89 89 89 77	7·2 % 97 93 91 93 80 100 84 96 75 90 97 98 86 91 90 89 88 93 80 91 88 96 79 88 90	7·3 % 97 90 89 91 100 72 89 95 99 90 87 83 93 85 82 93 90 98 88 90 88 88 90 88 88	7·33 Fee % 92 93 89 92 79 90 86 93 74 94 100 91 90 86 84 93 86 89 93 88 89 93 88 89 89 89 89 80 80	\$\frac{1}{90.3} \\ 84.2 \\ 81.3 \\ 84.5 \\ 90.2 \\ 89.4 \\ 91.6 \\ 88.0 \\ 89.1 \\ 89.4 \\ 90.2 \\ 92.1 \\ 89.0 \\ 91.6 \\ 88.6 \\ 85.9 \\ 93.3 \\ 86.3 \\ 88.3 \\ 89.6 \\	mb. 10.2 8.5 7.6 6.2 7.5 7.0 8.1 6.8 7.5 8.7 7.4 6.9 5.6 6.0 7.3 6.1 5.6 5.6 6.0 6.6 6.9 7.5

^{*} Computed from the mean temperatures and the mean relative humidities.

[†] Mean of the column.

[‡] Mean of the row.

Percentages at exact hours, Greenwich Mean Time. Determined as explained on page 16.

143. Eskdalemuir: Louvred Hut: h $_t$ (Height of thermometer bulbs above ground) = 0.9 metre.

March, 1923.

143. Eskdal	emu	r:]	Louv	rea	nut	. 111	1110	15111	OI U				1105 0		0 81		., —		111001						Maici	
Day.	т.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
1 2 3 4 5	90 92 88 96	% 90 90 89 91 100	% 86 95 88 88 96	% 89 89 89 89 90	% 87 86 90 90 92	% 89 89 90 90	% 94 85 95 87 99	% 94 84 95 88 95	% 94 89 92 84 91	% 90 88 90 78 95	% 94 88 94 77 93	% 94 79 87 71 97	% 94 89 86 68 90	% 89 81 89 62 78	% 94 84 89 66 75	% 95 84 88 77 76	% 95 96 89 79 83	% 94 90 88 76 82	1 -0 1	% 100 100 89 85 81	% 94 84 86 95 78	% 89 95 88 92 77	% 83 92 87 94 88	94 90 86 96	91·9 88·7 89·4 83·2 88·8	mb. 7 · 9 7 · 0 7 · 2 6 · 7 7 · 2
6 7 8 9	89 90 82 85 88	92 87 81 86 73	90 90 83 91 76	93 91 79 89 80	97 91 82 89 80	95 91 85 91 81	95 94 92 86 81	91 91 89 85 81	94 93 89 85 81	88 81 88 79 80	90 80 92 84 80	90 76 88 82 79	91 72 91 92 76	93 77 81 85 64	90 80 78 84 71	86 80 92 81 79	97 87 88 87 82	86 84 86 87 85	91 86 90 88 85	86 85 90 85 88	94 85 89 91 90	83 88 88 88 88	88 88 77 90 88	91 85 76 90 93	90·9 85·6 85·9 86·4 81·2	7·9 7·7 6·9 6·2 5·4
11 12 13 14	91 82 89 85 88	91 87 85 82 87	91 87 88 80 86	91 85 82 82 85	88 84 78 84 84	89 83 83 85 76	91 84 86 85 82	88 93 86 84 78	87 93 83 78 83	87 88 68 82 82	80 85 66 72 82	71 83 62 70 78	72 78 58 68 76	67 88 58 66 82	65 90 62 76 82	67 91 68 72 87	74 91 67 75 84	77 92 79 85 87	73 96 76 87 88	76 88 74 88 91	78 90 76 89 93	77 90 80 87 93	80 92 80 89 93	80 89 80 87 97	80·7 87·7 75·8 80·6 85·0	5·9 6·7 7·0 6·7 6·4
16 17 18 19 20	97 86 90 91 95	97 91 89 88 89	97 87 89 91 86	99 87 88 95 87	97 100 91 90 88	97 87 86 96 88	95 85 90 95 88	95 84 85 92 90	91 84 80 87 89	85 86 69 81 84	84 85 71 75 81	81 77 66 71 74	76 65 64 68 67	76 63 62 67 64	73 60 58 63 65	74 61 52 65 65	80 64 59 67 72	84 72 62 81 81	84 80 76 84 90	87 84 85 88 99	86 87 91 90 95	87 87 92 88 92	89 89 88 89 91	91 95 91 89 88	87·7 81·0 78·2 83·0 83·7	7·0 7·6 6·5 6·7 6·8
21 22 23 24 25	93 95 78 94 95	91 95 80 94 95	90 99 88 94 100	92 99 88 94 91	89 96 88 94 91	94 95 91 94 96	94 96 89 94 93	94 96 79 94 85	91 88 75 94 83	90 79 81 93 87	87 74 71 87 77	80 82 71 64 71	69 59 70 67 81	67 50 65 66 72	77 55 57 58 75	76 54 64 49 77	78 53 70 64 80	86 62 84 70 86	85 71 89 80 87	87 66 91 82 87	88 88 88 97 92	95 84 93 96 91	95 78 93 99 97	95 80 93 91 95	86·6 79·3 80·4 83·7 86·7	7·1 6·7 6·8 6·4 7·6
26 27 28 29 30	96 87 88 91 86	91 89 89 94 89	95 89 93 97 95	93 93 94 99 93	99 90 96 99 89	97 87 92 100 91	94 85 94 100 91	92 82 95 100 92	83 82 97 97 86	60 77 84 77 84	58 73 84 66 79	60 69 83 54 74	57 71 77 52 86	59 65 80 53 66	58 57 85 53 63	60 51 79 63 63	67 59 78 56 67	69 65 83 57 69	79 67 88 72 74	87 72 93 79 79	80 79 92 85 84	79 87 93 82 87	80 87 94 83 88	82 93 92 83 93	78·4 77·1 88·5 79·0 81·8	7·9 10·7 10·0 7·9 8·3
31	93	93	93	93	95	89	88	88	88	81	82	80	71	67	73	80	80	79	81	82	87	88	91	91	84.7	7.2
Mean	89.7												74.2	71 · 0	71.5	72.8	76.4	79·6	83·6 mb.	85·6	87·8	87·9	88·4	89·3	83·9 mb.	†7.2
√apo ur Pressure*				mb. 6·7								mb. 7:5	7·6	7.5	7.6	7.5	7.5	7:3	7.1	7.0	7.1	7.0	6.9	6.8	‡7·I	
144. Eskdale	muir	: L	ouvi	ed I	Hut	: h <i>t</i> :	= 0	9 n	ietre).																l, 1923.
1 2 3 4 5	% 91 91 97 86 81	% 91 93 99 85 81	% 93 93 97 83 82	% 94 96 94 82 83	% 91 93 95 77 86	% 92 96 98 75 86	% 90 96 99 73 89	% 88 93 96 73 94	% 88 94 93 65 86	% 94 92 83 60 83	% 91 90 77 61 66	% 90 92 76 56 66	% 91 87 72 52 64	% 96 90 66 58 65	% 94 90 65 60 73	% 90 90 66 71 66	% 93 89 72 76 66	% 88 89 71 86 66	% 91 92 85 85 89	% 87 92 86 96 83	% 95 93 89 85 91	% 99 92 86 85 85	% 97 91 92 87 82	% 94 100 87 85 73	% 92·0 92·1 85·3 75·1 78·8	mb. 8·3 8·4 8·3 8·1 7·2
6 7 8 9	74 78 85 72 90	74 79 88 72 88	81 84 89 73 92	76 .81 87 73 94	73 79 85 77 95	72 89 85 76 96	70 89 82 83 96	69 91 75 76 91	66 80 67 64 95	69 82 60 60 95	70 84 58 62 90	65 87 59 65 82	64 76 59 67 66	71 77 59 62 67	68 72 58 59 66	69 66 59 59 66	69 76 62 61 67	75 81 65 67 68	75 87 68 68 80	75 88 70 78 87	74 88 71 81 86	74 92 71 81 87	76 91 72 83 77	74 88 73 87 95	71·7 82·4 71·4 70·8 83·8	6·2 6·8 5·7 5·1 6·2
11 12 13 14 15	91 94 89 75 91	95 97 94 79 87	94 99 98 76 85	92 92 100 76 88	88 97 100 68 88	89 96 100 76 89	94 91 97 81 84	92 90 98 86 85	86 94 92 76 81	86 93 90 95 69	86 100 84 94 67	69 97 70 100 68	75 95 71 100 61	73 97 71 90 61	68 95 80 91 74	69 97 72 88 62	60 97 72 89 68	80 93 73 87 76	91 96 75 90 77	93 95 77 87 84	93 96 85 90 85	97 94 82 90 88	93 95 76 87 95	99 96 74 89 92	85·5 95·3 84·6 85·5 79·3	8·6 9·5 8·6 7·1 7·0
16 17 18 19 20	95 91 89 91 81	94 91 89 92 82	98 91 90 92 87	90 91 91 89	93 89 92 89 87	91 88 92 84 88	91 86 90 79 81	94 72 80 81 73	87 71 80 75 74	82 62 79 69 64	80 62 68 71 60	77 64 71 65 63	76 58 68 74 59	75 57 67 74 62	69 57 70 74 58	71 62 70 74 59	71 62 73 78 57	75 65 71 77 70	79 72 71 79 73	81 80 76 77 81	89 87 76 89 87	91 89 80 89 86	91 90 91 88 78	91 90 87 82 72	84·6 76·1 79·7 80·7 74·0	6·9 5·9 5·5 6·0 5·6
		1 02	,	_	1 -				!		1	1	ı	0.7	87	92	92	92	90	91	93	91	90	90	83.3	6.1
21 22 23 24 25	70 88 87 72 92	71 88 71 77 92	73 88 73 72 92	78 94 76 72 92	71 88 77 76 92	78 82 82 70 91	68 77 78 69 87	66 70 67 59 80	70 63 65 50 75	82 66 87 51 76	95 66 98 53 72	86 63 97 51 73	68 74 50 74	74 74 43 73	63 71 48 81	66 57 52 76	68 67 50 76	66 74 52 85	73 84 68 86	86 87 73 87	88 82 72 84	88 80 65 89	88 80 66 89	88 76 89 88	77·1 77·9 62·3 83·4	6·1 5·7 4·7 6·1
22 23 24	70 88 87 72	71 88 71 77	73 88 73 72	78 94 76 72	71 88 77 76	82 82 70	77 78 69	70 67 59	63 65 50	66 87 51	66 98 53	63 97 51	68 74 50 74 74 55 89 58 93	74 74 43 73 83 56 87 54 94	63 71 48 81 84 62 80 57 91	66 57 52 76 91 67 81 56	68 67 50 76 77 64 70 56 96	74 52 85 70 63 68 74 95	84 68 86 68 79 77 78 92	87 73 87 71 81 78 87 91	82 72 84 70 86 80 90 90	80 65 89 69 89 87 94 91	80 66 89 67 90 88 95 72	76 89 88 72 88 94 94 72	77.9 62.3 83.4 79.9 67.0 83.4 76.5 92.8	6·1 5·7 4·7
22 23 24 25 26 27 28 29	70 88 87 72 92 87 71 89 96 99	71 88 71 77 92 88 71 89 90 97	73 88 73 72 92 88 69 90 90	78 94 76 72 92 89 69 92 93	71 88 77 76 92 89 68 92 88 95	82 82 70 91 85 73 93 87 76	77 78 69 87 80 63 86 80 96	70 67 59 80 82 51 76 75 97	63 65 50 75 76 48 70 68 92	66 87 51 76 84 46 84 59 91	66 98 53 72 81 54 77 60 91	63 97 51 73 84 54 88 57 95	68 74 50 74 74 55 89 58 93 72·3	74 74 43 73 83 56 87 54 94 72·2	63 71 48 81 84 62 80 57 91	66 57 52 76 91 67 81 56 97 72.0	68 67 50 76 77 64 70 56 96	74 52 85 70 63 68 74 95	84 68 86 68 79 77 78 92 80·6	87 73 87 71 81 78 87 91 83.5	82 72 84 70 86 80 90 90 85.5	80 65 89 69 89 87 94 91	80 66 89 67 90 88 95 72 85 · 2	76 89 88 72 88 94 94 72 86·0	77.9 62.3 83.4 79.9 67.0 83.4 76.5 92.8	6·1 5·7 4·7 6·1 7·2 5·2 6·4 7·0
22 23 24 25 26 27 28 29 30	70 88 87 72 92 87 71 89 96 99	71 88 71 77 92 88 71 89 90 97	73 88 73 72 92 88 69 90 90 97 87·0	78 94 76 72 92 89 69 92 93 97 87.0	71 88 77 76 92 89 68 92 88 95 85.9	82 82 70 91 85 73 93 87 76	77 78 69 87 80 63 86 80 96 84·2 mb.	70 67 59 80 82 51 76 75 97 80·7	63 65 50 75 76 48 70 68 92 76·4	66 87 51 76 84 46 84 59 91	66 98 53 72 81 54 77 60 91 75.6	63 97 51 73 84 54 88 57 95 74·3	68 74 50 74 74 55 89 58 93	74 74 43 73 83 56 87 54 94 72·2 mb.	63 71 48 81 84 62 80 57 91 72·2	66 57 52 76 91 67 81 56	68 67 50 76 77 64 70 56 96 72.5	74 52 85 70 63 68 74 95 75·4 mb.	84 68 86 68 79 77 78 92 80·6	87 73 87 71 81 78 87 91 83·5 mb.	82 72 84 70 86 80 90 90 85.5	80 65 89 69 87 94 91 86.0	80 66 89 67 90 88 95 72 85·2 mb. 6·5	76 89 88 72 88 94 72 86 · o	77.9 62.3 83.4 79.9 67.0 83.4 76.5 92.8	6·1 5·7 4·7 6·1 7·2 5·2 6·4 7·0 10·2

^{*} Computed from the mean temperatures and the mean relative humidities. † Mean of the column.

145. Eskdalemuir: Louvred Hut: h_t (height of thermometer bulbs above ground) = 0.9 metre.

May, 1923.

Day.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
1 2 3 4 5	% 71 88 92 94 92	83 89 94 97 94	% 89 79 95 98 95	% 87 81 97 87 88	% 86 89 98 93	% 87 87 97 86 88	% 81 78 95 90 87	% 80 70 82 98 81	% 75 68 70 97 85	% 72 65 65 93 83	% 72 65 61 78 77	% 79 59 63 70 62	% 74 63 61 70 68	% 71 59 58 74 64	% 78 73 61 76 67	% 75 75 57 68 61	% 70 76 59 75 62	% 72 81 63 77 61	% 81 84 71 81 74	% 84 87 77 85 81	% 87 89 87 91 92	% 89 95 87 92 89	% 91 94 90 94 92.	% 89 94 90 93 92	% 79·7 78·6 78·0 85·6 80·4	mb. 9·1 8·4 9·2 9·6 9·9
6 7 8 9 10	95 86 75 87 80	92 88 96 90 79	94 89 91 91 75	97 90 87 92 78	93 91 86 92 75	94 92 87 91 71	83 69 89 91 63	92 68 84 90 61	82 60 82 87 62	76 56 75 90 64	67 52 66 82 56	65 48 76 85 66	65 49 64 77 88	58 45 60 75 89	59 48 51 67 87	82 44 54 75 94	85 47 52 73 92	79 62 56 99 94	85 70 61 95 86	72 74 72 93 87	72 71 80 95 82	79 74 77 88 81	85 77 77 83 87	84 86 87 78 90	80·8 68·1 74·4 86·3 78·4	8·1 6·3 7·5 6·4 6·0
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31	87	85	91	94	89	87	88	82	85	85	82	75	75	72	73	78	76	78	86	85	87	85	85	86	83.2	8.0
Mean Vapour	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	70·7	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	1 †7·5 1
Pressure*		6.8									7.6	7.8	7.9	8.0	8.0	8.0	8.0	7.8	7.8	7:4	7:3	7.1	7.0	6.9		1000
146. Eskdale	. 0/	- 0/									1.0/		• 0/	I 0/	1 0/	1.0/	1.0/	1.0/	1.0/	1 0/	1 0/	1.0/	0/	1 0/		e, 1923.
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11 12 13 14	88	87 89 87	89 89 87	90 89 88	89 88 85	89 88 85	86 89 91	88 92 92	83 93 87	78 99 81	72 96 77	79 94 80	80 96 86	83 99 89	69 94 94	71 97 96	69 99 98	79 99 93	84 96 97	82 96 97	86 93 97	88 88 97	92 84 95	93 82 97	82·8 92·8 89·9	10·4 10·9 12·0
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11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	88 97 82 81 92 75 91 89 89 93 85 70 84 85 91 79 90 93 84 82 97 87	87 89 87 97 90 85 90 77 91 87 89 87 87 87 87 87 87 87 87 87 89 87 87 87 87 87 87 87 87 87 87 87 87 87	89 89 87 91 80 86 88 84 91 87 90 83 84 78 85 88 88 87 89 87 89 87 87 87 87 88 88 88 88 88 88 88 88 88	90 89 88 86 81 85 88 83 91 86 88 87 97 88 88 88 92 89 88 88 85 95 87 77 77 77	89 88 85 86 77 89 80 68 90 85 85 99 88 82 86 95 99 88 85 90 88 85 90 88 86 86 86 86 86 86 86 86 86 86 86 86	89 88 85 81 72 83 79 71 82 97 73 71 84 85 92 86 78 93 88 93 88 93 88 88 88	86 89 91 79 69 85 77 64 96 66 67 89 85 88 86 71 70 81 82 83 91	88 92 92 78 68 86 83 59 84 61 61 85 83 64 82 67 78 79 72 93 76 · 9	83 93 87 85 59 92 72 61 72 66 62 58 85 82 72 81 63 67 73 68 73 68 75 73 66 73 67	78 99 81 83 56 91 73 52 79 67 58 88 65 85 84 63 72 62 65 73 71 71 mb.	72 96 77 81 55 92 78 51 55 55 86 59 51 79 72 79 51 58 69 69 69 4	79 94 80 79 57 93 73 48 84 64 54 77 62 52 79 79 62 75 57 64 73 69:5	80 96 86 86 78 55 95 70 48 85 61 54 73 64 53 74 66 66 66 66 66 69 69	83 99 89 67 58 95 68 47 89 57 61 70 68 68 79 63 74 69 58 67 70 68 68 79 70 68 68 79 70 69 70 70 70 70 70 70 70 70 70 70 70 70 70	69 94 94 70 53 92 146 87 57 66 65 62 60 77 77 85 69 66 71 69 \cdot 2 mb.	71 97 96 76 58 89 71 48 95 60 62 64 76 59 78 79 59 81 56 55 71 59 68 75 70 59 68 75 75 75 75 75 75 75 75 75 75 75 75 75	69 99 98 67 61 90 71 52 96 65 58 72 67 65 78 80 65 82 60 71 71 71 71 71 71 71 71 71 71	79 99 93 65 66 90 75 61 83 69 62 78 70 75 62 77 75 74.0 mb.	84 96 97 66 88 83 72 63 81 72 63 84 89 80 88 74 67 75 75 75 66 67 87 77 75 75 75 75 75 75 75 75 75 75 75 75	82 96 97 74 83 76 67 77 75 74 77 86 70 85 99 89 99 79 73 80 78 80 3 mb.	86 93 97 77 80 90 78 80 80 85 83 81 83 86 86 89 86 87 87 87 87 88 88 88 88 88 88	88 88 97 77 77 92 83 79 84 89 85 80 78 73 91 96 89 91 79 76 90 93 84 93 84 4 mb.	92 84 95 82 75 93 80 84 89 87 90 80 88 88 98 78 88 98 79 82 85 2 85 2 86 86 87 88 88 88 88 88 88 88 88 88 88 88 88	93 82 97 84 80 91 79 91 86 85 76 86 88 89 90 94 82 89 94 81 83 86 3	82.8 89.8 89.9 79.7 68.8 88.7 78.3 64.9 86.2 74.1 72.8 67.1 81.9 85.1 77.6 83.6 73.1 71.0 78.5 77.5 79.1 79.7 78.4 mb.	10·4 10·9 12·0 9·8 8·0 10·2 9·6 7·6 8·1 7·5 7·7 12·2 8·7 8·5 11·5 12·4 12·6 12·1 8·9 9·1 11·2 12·6

^{*} Computed from the mean temperatures and the mean relative humidities.

[†] Mean of the column.

[‡] Mean of the row.

147. Eskdalemuir: Louvred Hut: h_t (height of thermometer bulbs above ground) = 0.9 metre.

July, 1923.

Target T	147. Eskuale	muir	• L	Ouvi	GO 1	iut.	. 117	(neig	111 0	1 1110	51 111C	micu	ci buii	US ai		810			, , ,		٠.					- ui	y, 1920.
Section Sect	Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	
17-64 18-1	2 3 4	93 97 97	93 97 97	95 93 97	97 96 99	97 95 94	79 96 96 91	76 98 96 92	75 96 94 86	69 99 95 80	70 89 92 78	77 83 99 89	73 83 100 92	69 87 99 92	98 96	63 89 88 99	62 88 89 98	69 90 91 95	76 98 92 98	77 98 94 99	83 96 92 100	86 95 99 100	96 97 100	95 93 100	96 96 97 100	77·2 93·1 94·7 94·5	10·2 12·8 13·8 13·5
1	7 8 9	83 94 91	82 98 89	82 98 88	85 96 92	81 96 83	78 98 83	76 94 79	65 98 78	68 98 80	58 98 84	69 94 78	75 99 70	80 95 71	89 88 71	77 82	77 83 73	78 80 74	87 80 70	83 81	89 91 84 88	91 94 89	95 90	90 96 91	92 95 88	79·8 92·5 80·9	17·6 14·9 15·1
19	12 13 14	94 96 91	95 96	94 96 91	100 99 92	95 92	93 88 90	93 88 91	96 82 84	75 72 78	67 73 77	64 79 82	66 68 76	58 68 72	56 64 73	54 65 78	49 68 77	48 69 77	63 73 80	72 74 80	74 82 84	81 88 87	85 91 87	92 89 90	90 89 91	77·8 81·3 84·0	14·9 15·1 14·5
22	17 18 19	93 89 91	97 91 96	97 89 92	92 94 95	91 99 96	92 87 90	89 80 93	83 82 93	75 91	77 79 100	76 81 95	88 67 96	86 74 96	76 76 98	67 68 96	86 64 87	66 81	63 82	72 87	86 69 89	84 87 95	89 90 95	90 87 98	90 92 94	86·0 80·0 92·7	11·3 10·7 12·9
27	22 23 24	92 93 86	92 96 85	93 96 85	90 95 86	90 96 86	94 94 87	96 95 83	95 87 83	93 86 63	92 76 63	91 77 58	89 66 60	81 60 66	92 64 59	92 71 63	93 75 68	92 73 71	89 88	94 78 74	90 83 85	92 84 87	89 85 90	92 88 90	90 87 92	91·4 83·1 76·8	15·8 12·8 11·0
Mean	27 28 29	83 89 93	84 92 92	88 92 91	86 92 91	85 96 90	75 95 94	72 91 89	68 95 88	61 92 82	70 96 94	61 96 89	60 92 87	65 91 86	68 90 79	67 92 88	67 91 91	70 87 91	67 90 91	77 96 92	87 93 94	92 99 94	91 97 91	88 90 91	89 96 90	75.7 92.8 90.0	10·1 12·7 12·6
Pressure 1. mb, mb, mb, mb, mb, mb, mb, mb, mb, mb,	31	91	92	92	92	88	88	83	80	89	89	78	88	72	87	91	86	72	82	86	87	90	90	84	90	86.3	11.9
148. Eskdəlemuir: Louvred Hut: hr = 0-9 metre. 1	Mean	91.0	91 · 9	90.6	91.4	90 · 8	88.7	87.2	84 · 1	80.4	79.7	78.5		76.0	76.2	75 · 8	77 · 7	78.3	80.7	82.7	86.0	89·c	89.4	89.4	91.5	84.3	†13.5
## August, 1923. ## August, 1	Vapour Pressure*	mb. 12·6	mb.	mb. 12·5	mb. 12·5	mb.	mb.	mb.	mb. 13·2	mb.	mb.	mb.	mb.	mb. 14 · o	mb. 14·3	mb.	mb.	mb.	mb.	mb.	mb.	mb.	. mb. 3 13•c	mb.	mb.	mb. ‡13·3	
1	148. Eskdale	muii	·: I	ouv	red l	Hut	: h _t	= 0	·9 m	etre	•															Augus	t, 1923.
2 91 80 91 91 92 95 07 06 80 81 185 87 84 83 90 85 86 181 92 87 7 7 78 80 87 7 85 82 86 82 77 76 76 76 71 64 57 50 53 50 55 66 69 69 77 88 82 87 90 94 92 78.7 10-6 5 80 91 94 96 93 80 78 78 60 67 52 48 46 85 53 53 78 78 78 78 83 81 81 82 88 81 132 80 81 133 81 82	_	1 %	%		%	%	%	%	%			%	0/0 96	% 66	1 %	1 %	%	%	%	1 %	%	% %	% 88	1 %	%		
7 93 94 95 95 95 96 96 96 84 86 97 97 16 96 94 94 98 92 92 95 95 97 81 88 88 87 97 96 96 97 96 96 97 97 96 98 98 98 98 98 98 99 99 99 99 99 99 99	2 3 4 5	91 94 77	89 94 85	91 89 82	92 88 86	95 86 82	97 90 77	96 83 76	89 85 76	81 85 71	85 81 64	87 77 57	84 78 56	83 68 53	90 72 50	81 69 58	88 64 66	90 80 69	90 69 69	95 77 75	95 78 82	97 83 87	98 81 90	95 81 94	93 82 92	90·6 80·8 73·7	10.6 11.3
12	7 8 9	95 93 98	94 93 95	95 95 95	95 93 97	95 97 96	96 96 95	96 86 94	93 79 94	94 69 89	96 62 81	94 71 78	94 78 72	98 93 71	98 96 67	92 96 66	92 98 60	95 96 68	77 99 71	81 99 71	80 97 79	83 96 85	85 95 85	91 95 78	93 96 76	91·8 90·3 82·1	14·3 13·5 14·0
17 91 95 93 92 92 94 96 86 84 76 73 87 84 80 78 77 78 88 85 85 87 89 89 85 77 12:1 18 91 87 85 87 90 90 86 84 78 77 79 73 66 66 68 86 70 84 88 88 94 91 95 92 92 89 84:1 12:0 92 95 91 91 90 94 90 86 81 79 72 71 68 73 73 76 82 93 95 95 92 92 95 95 85:7 12:7 21 97 99 99 98 88 87 88 88 93 94 89 81 79 78 69 74 61 66 71 79 82 91 97 92 86:8 12:2 91 90 90 80 88 89 88 88 88 88 89 89 19 19 96 95 95 95 85:7 12:7 21 97 99 99 99 80 88 89 99 99 99 96 93 94 89 81 78 75 77 72 76 76 76 73 77 78 80 82 85 88 82 4 10:0 23 93 88 88 88 88 88 88 89 89 89 89 89 89 89	12 13 14	91 88 92	97 95 91	93 98 91	94 96 96	96 99 93	93 99 93	94 99 90	96 98 84	89 96 82	81 98 78	75 92	72 93 69	77 91 69	90 69	79 65	83 82 60	87 78 67	90 68 77	93 69 80	93 82 85	95 86 89	89 85 89	87 87 89	91 91	88·5 89·1 81·7	12·0 14·5 11·1
21 91 90 90 89 88 88 93 87 85 80 84 81 78 75 77 72 76 76 73 77 78 80 82 85 88 82.4 10.0 c 23 93 88 88 88 88 84 88 92 86 84 76 79 90 85 91 93 91 91 96 95 95 95 95 88.9 11.0 c 24 93 96 96 96 100 94 95 79 77 68 81 75 77 77 76 75 76 73 76 71 77 80 80 80 80 88 82.2 10.6 c 25 87 87 90 86 93 95 91 83 84 72 66 73 73 73 73 87 96 95 97 98 96 97 90 88 91 87.0 9.9 26 91 97 92 95 94 94 95 88 87 74 77 76 76 72 78 88 86 88 81 81 81 88 88 88 88 88 88 88 88 88	17 18 19	91 91 87	95 87 85	93 89 87	92 91 90	92 91 90	92 89 86	94 88 84	90 87	86 84 77	84 81 79	76 67 73	73 69 66	87 72 66	84 72 86	80 78 70	78 76 84	77 78 88	78 82 88	88 84 94	85 88 91	85 88 95	85 94 92	87 92 92	89 91 89	85·9 83·7 84·1	12·1 12·3 12·0
27	22 23 24	91 93 93	90 88 96	90 88 96	89 88 96	88 84 100	93 88 94	87 92 95	85 86	80 8 4 77	84 76 68	81 79 81	78 90 75	75 85 72	77 91 70	72 93 75	76 91 76	76 91 73	73 88 76	77 91 71	78 91 77	80 96 80	82 95 80	85 95 80	88 95 88	82·4 88·9 82·2	10.6 11.0 10.0
Mean 89·9 90·5 90·3 91·0 91·1 90·8 88·7 85·1 81·9 77·9 74·0 73·8 78·3 76·4 74·2 76·7 78·3 79·5 82·3 85·9 88·1 88·5 89·6 90·2 83·7 †11·5 Vapour Pressure* 10·6 10·5 10·5 10·5 10·5 10·5 10·5 10·7 10·9 11·3 11·6 11·8 11·7 11·9 11·8 12·2 12·0 12·0 11·9 11·8 11·7 11·5 11·3 11·0 10·9 10·6 11·4	27 28 29	88 93 90	88 91 89	88 91 92	88	91 95	89 89 95	86 86 92	85 85 93	82 86 88	77 86 76	71 73	77 69 76	73 69 76	81 83 87	79 71 91	87 66 90	87 67 89	82 72 95	90 72 93	91 72 95	89 80 92	91 84 90	92 87 90	91 89 85	84·9 81·0 88·6	10·7 9·8 8 · 7
Vapour Pressure* mb. m	31	87	86	87	87	96	96	96	84	86	86	79	76	79	88	82	88	84	86	88	93	96	89	96	97	87.7	9.3
Pressure* 10·6 10·5 10·5 10·5 10·5 10·7 10·9 11·3 11·6 11·8 11·7 11·9 11·8 12·2 12·0 12·0 11·9 11·8 11·7 11·5 11·3 11·0 10·9 10·0 11·4														73 · 3	76.4	74.2	76.7	78.3	79.5	82.3	85·9	88.1	88·5	89·6	90 · 2	83·7	†11·5
G.M.T I. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. Noon. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. Mean. —		mb. 10·6	mb. 10·5	mb. 10·5	mb. 10·5	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	11.3	3 11.0	10.0	10.6	‡11.4	
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 $[\]boldsymbol{\ast}$ Computed from the mean temperatures and the mean relative humidities.

[†] Mean of the column.

149. Eskdalemuir: Louvred Hut: h_t (height of thermometer bulbs above ground) = 0.9 metre.

September, 1923.

Day.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
I 2	% 93 82	% 96 82	% 92 86	% 90 79	% 90 93	% 98 82	% 93 83	% 91 ·72	% 77 67	% 74 70	% 69 72	% 67 67	% 72 54	% 67 60	% 69 54	% 78 54	% 74 66	% 88 70	% 82 88	% 82 84	% 82 84	% 83 97	% 85 89	% 83 92	% 82·6 75·9	mb. 8•9 8•6
3 4 5	95 94 88	96 97 87	96 95 88	96 87 92	96 86 90	96 83 91	95 80 93	88 79 91	81 72 90	79 64 88	73 59 82	75 59 80	76 59 79	73 65 77	74 68 77	79 67 70	82 64 70	85 71 78	86 69 81	87 81 83	87 79 84	87 84 86	95 78 81	93 84 84	86·3 76·2 83·8	8·8 9·9 11·2
6 7	81 94	83 94	84 94	83 87	88 88	88 86	88 76	88 69	85 64	86 7 0	83 69	81 64	80 63	84 67	79 64	83 63	89 65	96 74	95 80	97 83	96 80	96 82	86 83	95 87	87·0 77·1	12·2 10·4
8 9 10	94 91 96	96 92 94	99 93 93	94 93 94	91 95 92	96 95 91	91 93	96 87 85	93 87 83	82 89 69	74 89 63	70 92 67	69 94 60	65 96 63	76 86 64	69 79 59	79 78 62	79 74 67	84 77 72	91 84 75	90 86 80	90 89 84	95 88 83	93 89 83	85·9 88·2 78·1	9·4 11·6 9·4
11 12	83 95	8 ₄ 9 ₄	86 94	85 94	86 91	82 84	84 91 98	85 86	81 88 96	80 71	81 66 92	79 70	81 66 91	81 61 89	84 58 88	87 65 88	84 69 88	91 75 88	90 78 89	88 79 90	91 84 92	91 89 92	91 89 95	91 95 97	85·1 80·4 92·6	10·8 10·2 10·9
13 14 15	91 96 93	91 91 89	94 87 92	97 88 92	96 91 92	96 91 95	98 87 92	95 84 82	80 80	97 74 85	72 80	93 67 88	66 84	67 69	63 84	69 75	69 72	80 76	86 86	85 81	90 86	94 95	92 96	95 93	81·9 85·8	10·1 8·5
16 17 18	95 89 91	90 87 93	90 87 90	95 86 94	91 82 97	93 78 95	97 . 93 94	89 88 95	80 88 84	79 89 74	74 89 70	68 82 61	69 87 60	68 92 67	67 93 67	69 92 76	73 89 82	80 89 86	77 89 84	86 89 90	87 92 88	87 93 83	87 96 86	91 92 83	82·6 88·8 83·1	8·6 9·3 9·0
19 20	86 89	82 80	86 88	84 93	97 88 93	87 88	90 91	88 89	86 91	85 78	87 69	82 71	84 60	88 64	92 60	91 66	90 69	92 7 0	93 75	94 76	84 86	83 87	80 93	8ī 93	86·8 79·7	9·0 8 ·0
21 22 23	95 96 97	95 93 96	92 92 98	93 88 97	96 89 94	97 89 97	96 88 98	86 89 99	80 85 93	85 80 79	81 77 72	74 79 74	71 76 70	67 87 68	68 76 66	63 90 70	65 89 61	72 88 86	85 93 84	80 93 91	92 95 90	91 97 95	94 92 95	93 93 94	83·8 88·1 86·0	8·2 9·5 9·2
24 25	95 90	93 90	93 94	97 96	89 97	92 96	93 94	90 96	80 94	80 90	77 95	76 87	68 87	90	58 89	69 89	76 90	89 90	94 91	95 91	84 82	80 86	77 85	93	83.3	8·8 10·9
26 27 28	83 88 95	85 89 96	85 95 96	85 95 98	80 93 96	80 95 89	93 83	93 91 88	87 92 85	78 90 79	71 91 75	72 91 67	68 96 70	73 99 63	86 98 65	96 65	87 95 74	90 98 82	91 96 87	90 94 87	92 96 87	91 98 92	89 96 89	94 96 100	83·8 94·0 83·4 95·6	11.4 13.0 11.8
30	91 ——	100	91	100	99	92	92	99	100	92 100	100	96 99	100	100	99 95	96 97 76·6	99 100	95	96 96	99 97	99 94 	93	97	99	98.3	14.8
Wean Vapour Pressure *	mb	mb.	mb.	mb.	91·4 mb. 9·5	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	110 2
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1 2 3 4 5	100 85 89	80 84	88 88	100 89 88	95 82 92	88 84 93 91 97	79 80 89 90 95	80 69 88	75 72 84	74 65 78 66	73 65 78 68	72 66 83 65 89 76 96	63 67 84 64 92 73	65 66 82 64 92 70 89	66 64 80	66 71 88 66 94 79 89	74 71 87 67 94 76 88	77 74 80 83 93 78 86	81 79 91 82 91 84 86	82 79 84 88 83 91 82	86 84 88 86 89 81	87 85 89 87 88 78	89 80 90 90 88 77	89 81 94 93 88 78	81·7 76·9 85·2 78·7 92·7 85·5 88·2	10·0 8·1 7·3 6·4 8·0 9·2 10·7
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2 3 4 5 6 7 8 9 10	100 85 89 83 96 88 88 84 93 85	80 84 81 98 88 90 84 97 84	90 81 93 87 79 95	91 92 85 77 85 78 93	95 82 92 89 98 91 91 83 88 82	88 84 93 91 97 94 83 72 88 81	79 80 89 90 95 97 92 84 72 88	80 69 88 83 96 89 93 77 70 89	75 72 84 75 99 90 87 76 70 92 75 93	74 65 78 66 88 93 91 74 66 88 70 92	73 65 78 68 88 79 92 66 65 83 64 95	72 66 83 65 89 76 96 66 61 87 60	63 67 84 64 92 73 91 65 58 84	65 66 82 64 92 70 89 67 57 86	66 64 80 60 90 77 91 72 62 88	66 71 88 66 94 79 89 78 77 88	74 71 87 67 94 76 88 85 76 86	77 74 80 83 93 78 86 90 78 82 83 83	81 79 91 82 91 84 86 92 73 79 88 81	82 79 84 88 83 91 82 94 72 78	86 84 88 86 81 96 81 78	87 85 89 87 88 78 97 75 76	89 80 90 90 88 77 96 83 81	89 81 94 93 88 78 94 83 81	81·7 76·9 85·2 78·7 92·7 85·5 88·6 75·0 84·7 76·8 91·1	10·0 8·1 7·3 6·4 8·0 9·2 10·7 8·8 9·0 9·1 7·1 8·1
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2 3 4 5 6 7 8 9 10 11 12 13 14 15	100 85 89 83 96 88 88 84 93 85 75 97 96 90	100 80 84 81 98 88 90 84 97 84 79 94 95 92	100 88 88 82 98 91 90 81 93 87 79 95 96 91	91 92 85 77 85 78 93 93 94 86	95 82 92 89 98 91 91 83 88 82 94 97 91 89 85	88 84 93 97 94 94 83 72 88 81 97 100 86 75	79 80 89 90 95 97 92 84 72 88 81 97 85 92 92 85 82	80 69 88 83 96 89 93 77 70 89 75 86 93 86 80	75 72 84 75 99 87 76 70 92 75 93 85 79 92 83 75	74 65 78 66 88 93 91 74 66 88 70 92 80 79 91 84 71	73 65 78 68 88 79 92 66 65 83 64 95 77 74 86	72 66 83 65 89 76 96 61 87 60 97 73 65 87	63 67 84 64 92 73 91 65 58 84 59 83 73 65 83	65 66 82 64 92 70 89 67 57 86 61 85 73 66 78 66 69	66 64 80 60 90 77 91 72 62 85 73 76 65 70	66 71 88 66 94 79 89 78 77 88 57 76 60 73 83	74 71 87 67 94 76 88 85 76 86 77 82 72 77 84	77 74 80 83 93 78 86 90 78 82 83 83 88 81 86 78 85	81 79 91 82 91 84 86 92 73 79 88 81 92 85 87	82 79 84 88 83 91 82 94 72 78 90 88 87 90 90 85 94	86 84 88 86 89 81 96 81 78 92 93 84 88 93	87 85 89 87 88 78 97 75 76 94 98 83 94 93 85 94	89 80 90 90 88 77 96 83 81 93 95 90 88 85 94	89 81 94 93 88 78 94 83 81 97 98 93 95 89	81·7 76·9 85·2 78·7 92·7 85·5 88·2 81·6 75·0 84·7 76·8 91·1 83·9 84·8	10·0 8·1 7·3 6·4 8·0 9·2 10·7 8·8 9·0 9·1 7·1 8·1 6·6 6·1
2 3 4 5 6 7 8 9 10 11 12 13 14 15	100 85 89 83 96 88 88 84 93 85 75 97 96 94 90	80 84 81 98 88 90 84 97 84 97 94 96 95 92	95 95 95	100 89 88 87 98 91 92 85 77 85 78 93 93 97 88	95 82 92 89 98 91 81 83 88 82 94 87 97 91	88 84 93 97 94 83 72 88 81 94 85 97 100	79 80 89 90 95 97 92 84 72 88 81 97 85 92 92	80 69 88 83 96 89 93 77 70 89 75 91 85 86 93	75 72 84 75 99 90 87 76 70 92 75 93 85 79 92 83	74 65 78 66 88 93 91 74 66 88 70 92 80 79 91	73 65 78 68 88 79 92 66 65 83 64 95 77 74 86	72 68 83 65 89 76 96 61 87 60 97 73 65 87	63 67 84 64 92 73 91 65 58 84 59 83 73 65 83	65 66 82 64 92 70 89 67 57 86 61 85 73 66 78	66 64 80 60 90 77 91 72 62 88 62 85 73 77 76	66 71 88 66 94 79 89 78 77 88 57 76 60 73 83	74 71 87 67 94 76 88 85 76 86 77 82 72	77 74 80 83 93 78 86 90 78 82 83 83 88 81 86	81 79 91 82 91 84 86 92 73 79 88 81 92 85 87	82 79 84 88 83 91 82 94 72 78 90 88 87 90 85	86 84 88 86 89 81 96 81 78 92 93 84 88 93	87 85 89 87 88 78 97 75 76 94 98 83 94 93	89 80 90 90 88 77 96 83 81 93 95 90 89 88	89 81 94 93 88 78 94 83 81 97 98 93 95 89	81·7 76·9 85·2 78·7 85·5 88·6 75·0 84·7 76·8 91·1 83·9 84·8 88·1 82·4 82·3	10·0 8·1 7·3 6·4 8·0 9·2 10·7 8·8 9·0 9·1 7·1 6·6 6·1 7·9 8·3 9·4
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	100 85 89 83 96 88 88 84 93 85 75 96 94 90 91 92 88	100 80 84 81 98 88 90 84 97 84 79 94 96 95 92 94 99 98 92	100 88 88 88 98 91 90 93 87 79 95 96 91 95 92 91 90	98 88 87 98 91 92 85 77 78 88 94 86 91 98 99 98 87	95 82 92 98 91 91 81 83 88 82 94 87 91 89 92 94 90	88 84 93 97 94 94 83 72 88 81 94 95 100 86 75 90 96 86	79 80 99 95 97 92 88 81 97 88 85 92 92 85 94 94 87	80 69 88 88 89 93 77 77 89 85 86 93 76 91 89 93	75 72 84 75 99 90 87 76 70 92 75 93 85 79 92 83 75 96 74 89 88 88 88	74 655 78 66 88 93 91 74 66 88 79 91 84 71 93 68 86 85 85	73 655 78 88 88 79 92 66 65 83 64 95 77 74 86 92 74 89 78 82	72 66 83 65 89 76 66 61 87 60 97 73 65 87 68 87 68 85	63 67 84 64 92 73 91 65 58 84 59 83 73 65 86 66 75	65 66 82 70 89 57 86 61 85 73 66 76 65 86 66 82	66 64 80 60 90 77 91 72 62 88 62 85 77 76 65 67 66 85 66 86	66 71 88 86 66 94 79 89 77 88 57 76 60 73 83 70 75 81 67 79	74 71 87 67 94 76 88 88 76 86 77 82 72 77 84 85 69 72 83 83	77 74 80 83 93 78 86 90 78 82 83 88 81 86 78 85 90 81 78	81 79 91 82 91 84 86 92 73 79 88 81 92 85 87 79 86 97 82	82 79 84 88 83 91 82 94 72 78 88 87 90 88 87 90 89 90 85	86 84 88 86 89 81 96 81 78 92 93 84 88 93 84 89 97	87 85 89 87 88 78 97 75 76 94 98 83 94 93 85 91	89 80 90 90 88 77 96 83 81 93 95 90 89 88 88 85 94 92 87	89 81 94 93 88 87 84 83 81 97 98 93 95 89 91 94 95 95	81·7 76·9 85·2 78·7 85·5 88·6 75·0 84·7 76·8 91·1 83·9 88·1 88·1 82·4 82·3 81·8	10·0 8·1 7·3 6·4 8·0 9·2 10·7 8·8 9·0 9·1 7·1 6·6 6·1 7·9 8·3 9·4 10·7
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2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	100 85 89 96 88 88 84 93 85 75 96 94 90 93 100 91 88 88 83 87 87 87	100 80 84 98 88 99 84 97 84 96 95 92 94 99 93 88 92 92 93 84 87 86	100 88 88 88 98 91 90 81 93 87 79 95 96 91 91 91 91 92 91 91 90 81 81 87	100 89 88 88 98 91 92 85 77 85 78 93 93 97 88 99 98 98 98 98 98 98 98 98 98 98 98	95 82 92 89 91 81 83 88 82 94 87 97 91 89 85 92 94 96 87 99 98	88 84 93 97 94 94 98 83 72 88 81 94 85 97 100 86 75 99 86 93 94 87 85 97 87 87 87 87 87 87 87 87 87 87 87 87 87	79 80 90 95 97 92 88 81 97 85 92 92 85 82 94 94 87 89	80 69 88 88 88 89 77 70 89 75 91 85 86 80 93 87 69 93 89 93 89 93 89 93 89 93 89 94 89 95 89 95 89 95 89 95 89 89 89 89 89 89 89 89 89 89 89 89 89	75 72 84 75 99 90 87 76 70 92 75 93 85 79 92 83 75 96 84 86 93 84 86	74 655 78 66 88 93 91 74 66 88 79 91 84 71 93 88 86 85 59 82 80 87 85 87 85 87	73 65 78 68 88 79 92 66 65 83 64 95 77 74 86 89 27 48 89 78 89 81 85 85 81 87	72 66 83 65 89 76 96 66 61 87 60 97 73 65 87 68 87 68 85 77 82 91 79 78 78 78 78 78 78 78 78	63 67 84 64 92 73 95 58 83 73 65 88 75 76 75 76 75 77 77	65 66 82 64 92 70 89 67 57 86 66 69 76 65 86 77 80 80 80	66 64 80 60 90 77 72 62 88 62 85 73 77 66 67 66 86 86 93 78 85 85 85 85 85 86 86 86 86 86 86 86 86 86 86 86 86 86	66 71 88 88 66 94 79 88 77 78 88 57 76 60 73 83 83 83 83 83 83 83 84 78	74 71 76 76 76 88 88 85 76 86 77 82 72 77 84 85 69 72 83 83 83 84 85 78 84 85	77 74 80 80 83 93 78 86 90 78 82 83 88 81 86 78 85 90 87 90 87 88 90 87 88 88 88 88 88 88 88 88 88 88 88 88	81 79 182 91 84 86 92 73 79 88 81 92 85 87 79 86 97 82 78 90 86 91 88 88 88 88	82 79 84 88 83 91 82 94 72 78 90 88 87 90 85 94 90 85 91 90 85 91 91 91 91 91 91 91 91 91 91 91 91 91	86 84 88 86 89 81 92 93 84 88 89 97 89 83 98 98 98 98 98 98 98 98 98 98 98 98 98	87 85 89 87 88 78 97 75 76 94 83 94 93 85 94 85 91 77 77 86 86 86 93	89 80 90 88 77 96 83 81 93 95 90 88 87 88 88 88 88 88 88 88 88	89 81 94 93 88 87 84 94 83 81 97 98 99 95 95 95 95 95 96 82 86 87	81·7 76·9 85·2 792·7 85·5 888·6 76·8 89·8 80·8 80·8 80·8 80·4 80·4	10·0 8·1 7·3 6·4 8·0 9·2 10·7 8·8 9·0 9·1 7·1 6·6 6·1 7·9 8·3 9·4 10·7 9·2 8 9·0 8·1 8·7 7·7 8·2 8·3 9·0
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	100 85 89 83 96 88 88 84 93 85 75 96 94 90 91 92 88 88 83 87 87 84	100 80 84 98 88 88 99 84 97 84 96 95 92 94 99 93 98 92 92 92 93 84 87 86	100 88 88 88 98 91 90 91 93 87 79 95 96 91 91 92 91 92 91 93 88 88 88 88 88 88 88	100 89 88 88 87 98 91 92 85 77 85 78 93 93 93 94 86 99 87 88 99 87 89 89 99 90 90 90 90 90 90 90 90 90 90 90 90	95 82 92 89 91 81 83 88 82 94 87 97 91 89 85 92 94 90 96 87 93 85 93 85 93 85	88 84 93 97 94 83 72 88 81 94 85 97 100 86 75 96 86 93 87 87 85 94	79 80 90 95 97 92 88 81 97 85 92 92 85 82 94 87 94 87 94 89 89 89 89	80 69 88 88 88 89 77 70 89 75 91 85 86 89 93 87 91 89 93 89 93 89 93 89 94 89 95 89 95 89 95 89 95 89 95 89 95 89 95 89 95 89 95 89 95 89 89 89 89 89 89 89 89 89 89 89 89 89	75 72 84 75 99 90 87 76 70 92 75 93 85 79 92 83 75 96 74 89 88 86 93 84 86	74 655 78 66 88 93 91 74 66 88 70 92 80 79 91 84 71 93 86 88 85 93 89 89 80 89 80 80 80 80 80 80 80 80 80 80 80 80 80	73 65 78 68 88 79 92 66 65 83 64 95 77 74 86 88 92 95 81 82 95 81 85 81	72 66 83 65 89 76 96 66 61 87 60 97 73 65 87 68 87 68 87 68 87 77 82 91 79 78	63 67 84 64 92 73 91 65 58 84 59 83 73 65 86 66 75 76 75 73	65 66 82 70 89 67 577 86 66 69 76 65 86 66 82 91 80 77 80	66 64 80 60 90 77 72 62 88 62 85 73 77 66 67 66 86 93 78 85 85	66 71 88 86 66 94 79 88 77 76 60 73 83 70 75 81 67 79 82 93 83 83 83 83 83	74 71 87 67 94 76 88 85 76 86 76 91 77 82 72 77 84 85 69 72 83 83 94 87 78 84	77 74 80 83 93 78 86 90 78 82 83 83 88 81 78 86 78 86 86 86 86 84 85	81 79 91 82 91 84 86 92 73 79 88 81 92 85 87 79 86 97 82 78 90 86 91 86 91 86 86 87 88 88 88 88 88 88 88 88 88 88 88 88	82 79 84 88 83 91 82 94 72 78 90 88 87 90 88 87 90 88 87 97 88 87 97 88 87 97 88 88 87 97 97 98 97 97 97 98 97 98 97 97 97 97 98 97 97 97 97 97 97 97 97 97 97 97 97 97	86 84 88 88 86 89 81 78 92 93 84 88 93 84 88 93 88 93 88 93 88 93 88 93 88 94 88 94 88 94 88 94 94 94 94 94 94 94 94 94 94 94 94 94	87 85 89 87 88 78 97 75 76 94 98 83 94 93 85 94 85 97 77 86 86 93 80 90 90 90 90 90 90 90 90 90 90 90 90 90	89 80 90 90 88 77 96 83 81 93 95 99 88 88 87 93 81 88 81 88 81 83 81 83 81 84 84 85 86 86 86 86 86 86 86 86 86 86 86 86 86	89 81 94 93 88 87 84 97 98 93 95 95 95 95 95 95 96 82 86 87 77 88	81·7 76·9 85·2 792·7 85·5 88·6 88·7	10·0 8·1 7·3 6·4 8·0 9·2 10·7 8·8 9·0 9·1 7·1 6·6 6·1 7·9 8·3 9·4 10·7 9·2 8·9 9·0 8·1 8·7 7·7 8·2 8·3 9·0
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	100 85 89 83 96 88 88 84 93 85 75 97 96 92 88 83 87 87 87 87 88 88 88 88 88 88 88 88 88	100 80 84 98 88 88 99 84 97 84 99 94 99 93 98 92 92 92 93 84 87 86 91 88 90 85	100 88 88 88 98 91 93 87 79 95 95 96 91 91 90 89 88 88 86 95 88 99 88	100 89 88 88 88 98 91 92 85 77 85 78 93 93 97 88 88 99 98 99 87 82 86 93 98 87 88 88 98	95 82 92 98 91 81 83 88 82 94 87 97 85 92 94 90 96 87 85 93 85 97 89 97	88 84 93 91 97 94 83 72 88 81 94 85 97 100 86 75 99 96 86 93 99 87 87 87 85 97 87 87 88 87 87 87 87 87 87 87 87 87 87	79 80 90 95 97 92 84 72 88 81 97 85 92 92 85 87 89 89 89 89 89 89 89 89 89 87	80 69 88 88 88 89 77 70 89 75 91 85 86 93 93 89 89 89 89 89 89 89 89 89 89 89 89 89	75 72 84 75 79 90 87 76 70 92 75 93 85 79 92 83 75 96 74 89 88 86 93 88 87 87 88 88 88 88 88 88 88 88 88 88	74 65 78 66 88 93 91 74 66 88 70 92 80 79 91 84 71 93 86 85 85 85 85 85 85 85 85 85 85 85 85 86 86 87 87 87 87 87 87 87 87 87 87 87 87 87	73 65 78 68 88 79 96 66 65 83 64 95 77 74 86 88 89 95 81 87 76 84 87 77	72 66 83 65 89 76 96 66 61 87 60 97 73 65 87 75 69 87 88 87 77 85 73 88 87 77 88 77 77	63 67 84 64 92 73 91 65 58 83 73 65 86 66 75 76 75 77 77 72	65 66 82 64 92 70 89 67 57 86 61 85 73 66 69 76 65 86 77 80 80 77 80 80 77 80 80 77 80 80 77 80 80 80 80 80 80 80 80 80 80 80 80 80	66 64 80 60 90 77 72 62 88 62 85 73 77 66 67 66 86 93 78 85 85 87 80 78 80 78 80 78 80 80 80 80 80 80 80 80 80 80 80 80 80	66 71 88 86 66 94 79 88 77 78 88 57 76 60 73 83 83 70 75 82 93 83 83 83 83 83 83 85 75 86 75 86 75 86 86 75 86 86 86 87 87 87 87 87 87 87 87 87 87 87 87 87	74 71 76 87 67 94 76 88 85 76 86 76 91 77 82 72 77 84 85 69 72 83 83 94 87 78 84 85 97 84 85 97 84 85 86 86 86 87 88 88 88 88 88 88 88 88 88 88 88 88	77 74 80 83 93 78 86 90 78 82 83 88 86 78 85 90 81 78 86 86 87 94 86 88 84 85 90 82 84	81 79 82 91 84 86 92 73 79 88 81 92 78 85 87 79 86 97 82 78 90 90 86 91 88 88 88 88 88 88 88 88 88 88 88 88 88	82 79 84 88 83 91 82 94 72 78 90 88 87 86 87 88 87 87 88 87 88 87 88 88	86 84 88 88 89 81 78 92 93 84 88 93 84 89 97 89 89 89 89 89 89 89 89 89 89 89 89 89	87 85 89 87 88 78 97 75 76 94 98 83 94 93 85 91 77 86 86 86 86 86 99 97 73 87	89 80 90 88 77 96 83 81 93 95 99 88 87 88 88 81 88 88 81 88 88 81 88 81 88 81 88 81 88 81 88 81 88 81 88 81 88 81 88 81 88 81 88 81 81	89 81 94 93 88 87 88 97 98 99 95 89 95 89 86 82 86 87 77 88 89 89 89 89 89 89 89 89 89 89 89 89	81·7 76·9 85·2 792·7 85·5 88·6 75·0 85·6 88·1 82·4 82·3 88·1 82·4 82·3 85·6 85·6 85·6 86·1 85·6 86·1 86·1 86·1 86·1 86·1 86·1 86·1 86	10·0 8·1 7·3 6·4 8·0 9·2 10·7 8·8 9·0 9·1 7·1 6·6 6·1 7·9 8·3 9·4 10·7 9·2 8·9 9·0 8·1 8·7 7·7 8·2 8·3 9·0 10·1 11·2
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Mean	100 85 89 83 96 88 88 84 93 85 75 97 96 94 90 91 92 88 87 87 88 87 87 88 88 88 88 88 88 88	100 80 84 98 88 99 84 97 84 97 84 99 99 93 98 92 93 88 90 85 100 87 90.3	90 88 89 91 90 88 97 99 95 96 91 99 99 84 88 88 86 99 86 99 86 99 86 90 3	98 88 87 98 91 92 85 77 85 78 93 997 88 99 98 87 86 99 98 87 99 98 87 99 90 2	95 82 92 98 99 91 83 88 82 94 87 97 91 89 85 92 94 96 87 97 85 93 88 93 88 94 95 96 87 97 87 88 98 98 98 98 98 98 98 98 98 98 98 98	88 84 93 97 94 94 94 83 72 88 81 94 85 97 100 86 75 90 96 86 93 91 87 87 87 87 87 88 89 97 97 98 98 99 90 90 90 90 90 90 90 90 90	79 80 89 90 95 97 92 88 81 72 88 85 92 92 85 82 94 87 87 89 89 85 98 98 98 98 98 98 98 98 98 98 98 98 98	80 69 88 88 89 93 77 70 89 93 75 86 93 86 80 93 93 93 93 93 85 86 95 89 89 89 89 89 89 89 89 89 89 89 89 89	75 72 84 75 99 90 87 76 70 92 83 75 96 74 89 88 86 93 84 86 97 86 87 97 86 87	74 655 78 666 88 93 91 74 666 88 79 91 84 71 93 88 86 85 85 93 85 94 81 94 81 94 81	73 65 78 68 88 79 92 66 65 83 64 95 77 74 86 88 92 78 81 87 76 84 87 77 79 66 77 77 79 70 70 70 70 70 70 70 70 70 70 70 70 70	72 68 83 65 89 76 96 66 61 87 77 68 87 77 88 87 77 88 87 77 87 88 87 77 87 8	63 67 84 64 92 73 91 65 58 84 59 83 73 65 86 66 75 76 77 77 71 89 87 72 72 74 89	65 66 82 70 89 67 86 68 78 66 69 76 80 80 77 80 80 77 80 80 77 80 80 77 80 80 77 80 80 77 80 80 80 70 80 80 70 80 80 70 80 80 80 80 80 80 80 80 80 8	66 64 80 60 90 77 91 72 62 88 62 85 73 77 66 86 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 88	66 71 88 86 66 94 79 89 77 88 57 76 60 73 83 70 75 81 77 93 83 83 87 98 88 77 98 89 77 98 99 78 77 79 79 79 79 79 79 79 79 79 79 79 79	74 71 87 94 76 88 88 85 76 86 77 82 77 84 85 69 97 84 85 90 97 84 86 97 84 86 87 88 88 88 88 88 88 88 88 88 88 88 88	77 74 80 83 93 78 86 90 78 82 83 88 81 86 78 85 90 87 90 87 94 86 86 86 86 87 88 88 88 88 88 88 88 88 88 88 88 88	81 79 82 91 84 86 92 83 87 88 81 92 85 87 79 86 97 86 97 86 97 88 89 86 99 86 86 86 86 86 86 86 86 86 86	82 79 84 88 83 91 82 94 72 78 90 85 94 97 86 87 99 87 90 87 90 87 90 87 88 88 88 88 88 88 88 88 88	86 84 88 86 89 81 78 92 93 84 88 93 84 89 97 89 89 89 89 89 89 89 89 89 89 89 89 89	87 85 89 87 88 78 97 75 76 94 88 83 94 93 85 94 85 91 77 86 86 86 86 97 73 87 87 87 87 87 88 87 88 87 88 87 88 88	89 80 90 90 88 77 96 83 81 93 95 90 89 88 87 81 88 81 88 81 88 88 87 88 88 87 87 88 88 87 88 88	89 81 94 93 88 97 98 93 95 89 91 94 95 95 89 86 82 87 77 88 81 99 89 89 89 89 89 89 89 89 89 89 89 89	81·7 76·9 85·2 792·7 85·5 88·6 75·0 85·6 83·8 85·4 82·3 85·6 85·6 85·6 85·6 85·6 85·6 85·6 85·6	10·0 8·1 7·3 6·4 8·0 9·2 10·7 8·8 9·0 9·1 7·1 6·6 6·1 7·9 8·3 9·4 10·7 9·2 8·9 9·1 8·7 7.7 8·2 8·3 9·0 10·1 11·2
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	100 85 89 83 96 88 88 84 93 85 75 97 96 92 88 83 87 87 87 87 88 88 88 88 88 88 88 88 88	100 80 84 98 88 88 99 84 97 84 96 95 92 94 99 93 98 92 92 92 93 84 87 86 91 88 90 85 100 87 87 88 90 88 90 88 90 88 90 88 90 90 88 90 90 90 90 90 90 90 90 90 90 90 90 90	100 88 88 88 98 91 90 81 93 87 79 95 96 91 91 90 91 91 90 88 88 88 98 86 98 90 81 90 90 90 90 90 90 90 90 90 90 90 90 90	100 89 88 88 88 98 91 92 85 77 85 78 93 93 97 88 99 99 87 86 93 93 99 87 86 97 86 98 98 98 98 98 98 98 98 98 98 98 98 98	95 82 92 98 98 91 81 83 88 82 94 87 97 89 85 92 94 90 96 87 88 97 88 89 89 89 89 89 89 89 89 89 89 89 89	88 84 93 97 94 94 83 72 88 81 94 85 97 100 86 75 99 86 93 91 87 87 87 87 87 87 87 89 91 89 89 89 89 87 87 87 87 87 87 87 87 87 87 87 87 87	79 80 89 90 95 97 92 88 81 72 88 85 92 92 85 82 94 87 87 89 89 85 98 98 98 98 98 98 98 98 98 98 98 98 98	80 69 88 88 88 89 77 70 89 75 91 85 86 80 93 87 89 89 89 89 89 89 89 89 89 89 89 89 89	75 72 84 75 99 90 87 76 70 92 83 75 96 74 89 88 86 90 87 97 86 87 97 86 87 87	74 655 78 66 88 93 91 74 66 88 79 91 84 71 93 88 86 85 85 93 82 80 87 85 85 94 84 81 94 84 85 85 85 85 85 85 85 85 85 85 85 85 85	73 65 78 68 88 79 92 66 65 83 64 95 77 74 86 89 95 81 87 76 81 87 77 77 77 79 68 87 77 77 77 77 77 77 77 77 77 77 77 77	72 68 83 65 89 76 96 66 61 87 75 69 87 65 87 77 82 91 78 77 85 73 88 87 77 88 87 77 88 77 77	63 67 84 64 92 73 91 65 58 83 73 65 86 66 75 76 75 77 77 72	65 66 64 92 70 89 67 57 86 61 85 73 66 69 76 65 80 77 80 80 77 80 80 77 80 80 77 80 80 77 80 80 77 80 80 80 80 80 80 80 80 80 80 80 80 80	66 64 80 60 90 77 91 72 62 88 62 85 73 77 66 86 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 88	66 71 88 66 94 79 88 77 78 88 57 76 60 73 83 83 70 75 81 82 93 83 83 83 83 83 87 75 98 80 75 98 98 98 98 98 98 98 98 98 98 98 98 98	74 71 76 87 67 94 76 88 85 76 86 76 91 77 82 72 77 84 85 69 72 83 83 94 87 78 84 85 97 84 86 86 87 88 88 88 88 88 88 88 88 88 88 88 88	77 74 80 83 93 78 86 90 78 82 83 88 81 78 86 86 86 86 84 85 90 97 82 84 84 85 90 87 82 84 84 55 mb.	81 79 82 91 84 86 92 73 79 88 81 92 73 79 86 97 82 78 86 91 86 91 88 80 91 88 88 88 88 88 88 88 88 88 8	82 79 84 88 83 91 82 94 72 78 90 85 94 97 86 87 99 87 90 87 90 87 90 87 88 88 88 88 88 88 88 88 88	86 84 88 88 89 81 78 92 93 84 88 93 84 89 97 89 89 89 89 89 89 89 89 89 89 89 89 89	87 85 89 87 88 77 75 76 94 98 83 94 93 85 91 77 86 86 86 93 80 92 97 73 87 87 87 87 87 87 87 87 87 87 87 87 87	89 80 90 88 77 96 83 81 93 95 99 88 87 88 88 81 88 88 81 88 88 81 88 81 88 81 88 81 88 81 88 81 88 81 88 81 88 81 88 81 88 81 88 81 81	89 81 94 93 88 97 98 93 95 89 91 94 95 95 89 86 82 87 77 88 81 99 89 89 89 89 89 89 89 89 89 89 89 89	81·7 76·9 85·2 792·7 85·5 88·6 75·0 84·7 76·8 83·8 88·1 82·4 82·3 88·8 85·8 85·8 86·4 88 87·6 88 88 87·6 88 88 87·6 88 88 88 88 88 88 88 88 88 88 88 88 88	10·0 8·1 7·3 6·4 8·0 9·2 10·7 8·8 9·0 9·1 7·1 6·6 6·1 7·9 8·3 9·4 10·7 9·2 8·9 9·0 8·1 8·7 7.77 8·2 8·3 9·0 10·1 11·2
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Mean	100 85 89 83 96 88 88 84 93 85 75 97 96 94 90 91 92 88 83 87 87 87 87 88 88 83 87 87 88 88 88 88 88 88 88 88 88 88 88	100 80 84 98 88 88 99 84 97 84 96 95 92 94 99 93 98 92 92 92 93 84 87 86 91 88 90 85 100 87 87 88 90 88 90 88 90 88 90 88 90 90 88 90 90 90 90 90 90 90 90 90 90 90 90 90	100 88 88 88 98 91 93 87 79 95 95 99 91 99 93 88 88 99 88 88	100 89 88 88 88 98 91 92 85 77 85 78 93 93 97 88 99 99 87 86 93 93 99 87 86 97 86 98 98 98 98 98 98 98 98 98 98 98 98 98	95 82 92 98 98 91 81 83 88 82 94 87 97 91 89 85 92 89 89 87 89 98 98 98 98 98 98 98 98 98 98 98 98	88 84 93 97 94 94 83 72 88 81 94 85 97 100 86 75 99 86 93 91 87 87 87 87 87 87 87 89 91 89 89 89 89 87 87 87 87 87 87 87 87 87 87 87 87 87	79 80 90 95 97 92 88 81 97 85 92 85 82 94 87 87 89 89 89 89 85 93 88 89 89 85 89 89 89 85 89 87 87 88 89 89 89 89 89 89 89 89 89 89 89 89	80 69 88 88 88 89 77 70 89 75 91 85 86 80 93 87 89 89 89 89 89 89 89 89 89 89 89 89 89	75 72 84 75 99 90 87 76 70 92 75 93 85 79 92 83 75 96 48 89 88 86 89 87 97 88 89 87 88 88 88 88 88 88 88 88 88 88 88 88	74 655 78 66 88 93 91 74 66 88 79 91 84 71 93 68 86 85 85 93 82 80 87 85 85 94 84 81 94 84 85 85 85 85 85 85 85 85 85 85 85 85 85	73 65 78 68 88 79 92 66 65 83 64 95 77 74 86 88 92 78 88 82 95 81 85 87 77 79 66 84 87 77 79 66 87 77 79 88 88 88 88 88 88 88 88 88 88 88 88 88	72 68 83 65 89 76 96 66 61 87 75 69 87 65 87 77 82 91 78 77 85 73 88 87 77 88 87 77 88 77 77	63 67 84 64 92 73 91 65 58 83 73 65 83 73 65 73 76 75 77 77 77 72 74 74 86 86	65 66 64 92 70 89 67 57 86 61 85 73 66 69 76 65 80 77 80 80 77 80 80 77 80 80 77 80 80 77 80 80 77 80 80 80 80 80 80 80 80 80 80 80 80 80	66 64 80 60 90 77 91 72 62 88 62 85 73 77 66 67 66 86 93 78 85 85 78 80 78 80 78 80 78 80 78 80 78 80 80 80 80 80 80 80 80 80 80 80 80 80	66 71 88 66 94 79 88 77 78 88 57 76 60 73 83 83 70 75 81 82 93 83 83 83 83 83 87 75 98 80 75 98 98 98 98 98 98 98 98 98 98 98 98 98	74 71 87 67 94 76 88 85 76 86 76 91 77 82 72 77 84 85 69 72 83 83 94 87 78 84 85 97 88 88 89 97 88 88 89 97 88 88 89 97 88 88 88 88 88 88 97 88 88 88 88 88 88 88 88 88 88 88 88 88	77 74 80 83 93 78 86 90 78 82 83 88 81 86 78 85 90 87 82 86 86 86 86 84 85 90 97 82 84 84 5 90 97 82 84 84 5	81 79 82 91 84 86 92 73 79 88 81 92 73 79 86 97 82 78 86 91 86 91 88 80 91 88 88 88 88 88 88 88 88 88 8	82 79 84 88 83 91 82 94 72 78 90 88 87 90 85 94 90 85 91 86 87 87 88 87 90 88 88 88 88 88 88 88 88 88 8	86 84 88 86 89 81 96 81 77 89 83 84 89 97 89 89 85 80 98 85 87 88 87 87 88 87 87 88 87 87 87 87 87	87 85 89 87 88 77 75 76 94 98 83 94 93 85 91 77 86 86 86 93 80 92 97 73 87 87 87 87 87 87 87 87 87 87 87 87 87	89 80 90 88 77 96 83 81 93 95 90 88 87 88 88 87 88 88 87 93 88 87 93 88 88 87 93 88 88 88 88 88 88 88 88 88 8	89 81 94 93 88 93 95 89 91 95 89 95 86 82 86 87 77 88 89 89 89 89 89 89 89 89 89 89 89 89	81·7 76·9 85·2 78·7 85·2 85·5 88·6 75·0 84·7 76·8 88·1 88·1 88·1 88·1 88·1 88·1 88·1 8	10·0 8·1 7·3 6·4 8·0 9·2 10·7 8·8 9·0 9·1 7·1 6·6 6·1 7·9 8·3 9·4 10·7 9·2 8·9 9·0 8·1 8·7 7.77 8·2 8·3 9·0 10·1 11·2

^{*} Computed from the mean temperatures and the mean relative humidities.

151. Eskdalemuir: Louvred Hut: h_t (height of thermometer bulbs above ground) = 0.9 metres.

November, 1923.

151. Eskd																,			enes						Volling	
Hour.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
Day.	1 %	%	%	1 %	% 98	%	1 %	%	(% 98	%	1 %	% 84	%	% 80	% 84	% 84	% 81	% 85	% 87	% 84	% 96	% 90	% 88	% 96	% 90·7	mb. 6∙9
I 2	96 90	97	97 88	98 88	80	97 83	96	97	84	92 86	91 79	82	84 82	69	62	68	85	86	91	90	94	97	92	96	84.7	7·9 8·5
3	91	96	96	90	90	91	91	79 89	83	75 86	81 82	86	76 84	79 85	82 80	78 83	83	78 87	76 98	83 86	75 86	89 89	83 84	77 87	84·5 85·8	8·5 6·5
4 5	82 90	82 86	84	8 ₅ 8 ₇	85 94	93	91	98	78 90	81	84	96 81	73	82	8o	91	97 95	96	97	98	99	98	97	93	90.7	6.5
		0 -	0.0	ł		80	82	0.	-0		72	70	72	69	76	85	90	89	93	88	90	91	93	92	82.7	5.1
6 7	87 88	8 ₅	82 80	81 87	82 76	79	80	81	78 83 88	75 87 88	73	72 65	72 58 84	60	68	88	91	94	96	97	98	98	98	93	83.4	4.8
7 8	92	92	90	95	95	98	93	90	88	88	80	90 98	84 98	72 90	88	91	92 78	88 87	90 89	92 87	94 84	95 89	96 84	96 91	90.3	6·6 6·2
9	96	96	95	94	93	92 89	91 87	90 88	88	86	97 79	66	65	7I	77	77 83	81	83	80	85	85	84	90	89	84.5	6.2
		06	1	1	88			08	06	0.7	0.2	02	05		05	100	97	98	97	9 6	96	96	99	99	94.2	8.5
11	92 93	86	84	85	98	93	98	98	96	97 92	93	93 86	95 84	94 92	95 77	76	74	74	80	76	84	85	84	87	87.8	9.4
13	92	92	97 88	94	90 83	98 82	91 81	92 81	94 86	98 91	92 91	95 89	97 8 8	96	96 76	97 80	95 66	96 68	97 70	97 77	96 86	90 89	88 90	86 91	93·6 82·6	8·8 5·5
14	8 ₅ 9 ₅	89 95	85 96	83 96	96	95	90	90	87	89	91	94	95	77 95	95	95	94	93	92	93	88	84	86	98	92.5	5.6
	- 1		80		76	-	70	80	86	76	7.5	82	70	79	84	84	81	82	83	90	94	96	100	87	82.8	5.7
16 17	87 84	79 85	84	77 82	76 84	73 88	72 90	82	94	87	75 85	81	79 78 82	75	69	70	88	93	91	91	92	84	93	89	84.9	5.7
18	91	87	85 80	89	92	88	94	96	95	82	79	82	82 72	79 72	79 72	74 71	74 72	76 73	79 70	79 82	75 80	78 83	80 84	75 85	83·2 76·2	5·8 5·2
19 20	79 86	75 82	82	79 82	73 82	78 82	75 81	72 82	73 85	77 82	75 83	73 91	94	91	91	91	91	90	79 88	89	90	89	98	91	87.1	š·9
21		96	92	86	85	84	82	81	78	75	75	71	70	72	74	74	75	78	79	80	81	82	79	8o	80.3	5.3
2I 22	93 76 85	77	85	84	87	87	94	89	92	91	75 88	87	85	86	74 88	74 84	75 82	81	80	79 84	82	82	79 82	85	84.6	5.7
23	85	84 85	84 84	84 80	84 80	84 80	84	80 80	80	79 75	70 70	76 69	79 65	79 74	80 75	82 81	85 85	85 89	85 90	90	85 92	84	83 94	84 94	82·1 81·9	4·9 3 · 7
24 25	85 95	95	95	95	96	97	79 97	96	96	96	96	98	91	91	97	97	88	89	95	95	98	93 98	9i	92	94.8	5.3
26	03	91	0.2	91	94	98	98	98	95	96	96	95	03	93	97	96	97	97	97	97	96	97	95	95	95.3	6.3
27	93 95	95	93 93	93	93	93	94	93	92	93	92	92	93 87	85	85	79	85	97 86	86	83 88	82	82	81	77	88.5	5 ⋅ 1
28	78 85	73 85	75 83	75 81	85 81	90	92 85	92 83	92 86	92 86	93	8 ₅ 86	92 86	92 82	92	92 83	92 85	88	88 82	82	88 82	87 74	8 ₇	87 76	87·1 82·9	5·3
29 30	79	85	87	91	92	92	92	92	92	93	93	91	83	87	91	92	91	92	91	87	91	91	97	95	89.9	4.2
Mean	88.4	88.2	87.0	87.4	87.6	88.3	88 · 5	87.7	87.7	86.6	84.6	84.5	82.4	81 · 6	82.2	84.2	85.7	86.1	87.5	87.5	88.6	88.8	89 · 0	88 · 8	86.7	†6·1
Vapour	mb.	mb.	mb.	⊢mb.	l mb.	∣mb.	mb.	mb.	⊢mb.	mb.	mb.	mb.	mb.	mb.	ī mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	
Pressure* .	5.9	5.9	5.8	5.7	5.7	5.8	5.8	5.8	6.0	6.1	6.2	6.4	6.3	6.2	6.2	6.1	6.0	5.9	5.9	5.8	5.9	5.8	5.9			1
152. Eskd	alemuii	: L	ouvi	red I	Hut :	: h _t :	= 0	9 m	etre.															De	cembe	r, 1923.
	1 %	%	%	/ %	%	%	% [%	%	%	%	%	%	%	%	%	%	%	1 %	%	% 98	%	%	%	1%	mb.
I	98	100	98	95 100	94	96	97	98	100 98	97 93	97 87	95 89	95 90	98 89	94 91	93 93	95 90	96 96	95 96	95 93	98 91	92 90	90 92	92 92	93.3	7·1
2 3	91 93	100 91	97 92	93	97 92	94 93	97 94	94 94	94	92	83	80	82	84	85	90	93	96	96	96	96	96	96	96	91.5	5.4
4	96 92	96	96 93	93 91	93 91	92	91 87	92 88	94 92	98 97	98 95	96 95	96 90	96 91	96 88	96 91	96	96	96	94 89	94 88	94 87	94 85	94	94.9	5·9 6·2
5	1	92	93	91	91		-		-		93		ĺ ,	_					_					94	88.7	5.0
6	84 92	82 92	84	81 92	83 91	85 90	85 83	90 86	93 88	91 88	84 89	85 96	79	81 91	90 94	92	93	94	96	96	97	97 98	97 100	94	93.2	
7 8	98						1 2						45							97	97			97	75 -	6.7
10 9	93	98	92 98	100	100	98	88	87	83	87	84	81	95 76	73	76	95 78	80	84	85	82	82	83	86	97 91	86.7	, 6.3
		92	98 92	100 85	87	87	8o	83	86	79	84 76	81 78	76 80	84	76 92 96	95	80 95 99	84 93 97					86 98 100	97	86·7 88·7 97·4	
	100	92 98	98 92 98	100 85 97	87 98	87 98	80 98	83 98	86 97	79 92	8 ₄ 7 ⁶ 94	81 78 97	76 80 97	84 96	76 92 96	95 97	95 99	93 97	85 93 97	93 97	82 95 98	83 98 99	98 100	97 91 98 99	86·7 88·7 97·4	, 6·3 4·6 9·4
I I I 2	100 96	92 98 99	98 92 98 98	100 85 97	87 98 97	87 98 98	80 98 98	83 98 98	86 97 97	79 92 98	84 76 94 97	81 78 97 94	76 80 97	84	76 92 96	95	95	93 97 96	85 93 97 97 97	82 93	82 95	83 98	98 100 95 96	97 91 98 99 97 94	86·7 88·7 97·4 96·6 95·6	6·3 4·6 9·4 9·5 9·3
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12 13 14	96 98 97 97	92 98 99 97 97 97	98 92 98 98 97	100 85 97	87 98 97 96 88 87	87 98 98	80 98 98 94	98 98 98 93	97 97 94	79 92 98 93	84 76 94 97 94	81 78 97 94 95	76 80 97	96 97 96	76 92 96 97 97	95 97 96 96	95 99 96 97	93 97 96	85 93 97 97 97	82 93 97 94 96	95 98 94 96	98 99 99 94 96	98 100 95 96	97 91 98 99 97 94	86·7 88·7 97·4 96·6 95·6	6·3 4·6 9·4 9·5 9·3
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12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	96 98 97 97 84 86 86 84 86 84 80 98 82 81 94 94 98 95 98	92 98 99 97 97 84 84 87 83 82 96 80 98 95 98 98 98 99	98 92 98 97 96 97 98 82 86 87 83 87 82 98 83 75 73 95 98 100 99	100 85 97 97 97 94 88 82 86 87 81 82 81 98 94 97 94 98 100	87 98 97 96 88 87 84 87 90 85 85 85 98 85 98 91 90 91 91 91 96 91 90 90 90 90 90 90 90 90 90 90 90 90 90	87 98 98 95 83 86 85 93 90 81 88 94 76 88 94 94 96 87 99 100	80 98 98 94 81 86 85 89 95 80 97 73 93 90 83 95 85 98 97 100	83 98 98 93 83 84 85 90 93 76 85 72 94 86 76 95 85 98 100	86 97 94 90 91 84 90 86 73 87 71 98 87 93 95 98 100	79 98 93 81 96 85 89 90 76 88 76 69 98 87 73 92 95 96 84 99 98	84 76 94 97 94 82 96 79 88 86 77 80 62 98 82 67 65 85 95 96 99 99 100	81 78 97 94 95 77 95 80 87 90 65 65 87 99 66 65 85 99 99	76 80 97 97 95 77 98 88 86 62 64 65 90 94 95 88 99 95	84 96 97 96 79 95 78 88 92 70 66 95 73 65 72 98 96 98 98 99 99 99 99 99 99 99 99	76 92 96 97 97 81 89 89 82 62 69 94 79 67 98 99 96 100 91 99 99	95 96 96 75 95 84 92 94 76 65 71 99 81 71 84 98 95 100 100	95 99 96 97 73 86 85 95 89 76 66 80 99 79 73 80 98 90 100 100	93 97 96 95 86 87 88 95 91 79 69 78 80 78 80 98 95 99 98 81 100 100	85 93 97 97 97 93 83 91 95 87 87 87 87 87 87 98 98 99 100 100	82 93 97 94 96 94 98 93 95 88 72 71 98 73 88 79 98 99 90 100 100	82 95 98 94 96 94 99 92 86 85 87 86 84 97 96 99 92 100 99 93 90 4	83 98 99 94 96 94 97 95 89 82 81 71 66 98 75 99 99 90 100 90 90 90 90 90 90 90 90 90	98 100 95 96 94 82 91 89 77 83 71 66 97 80 82 92 94 99 98 97 100 100 100	97 91 98 99 97 94 93 80 88 88 89 81 84 72 72 97 81 83 93 94 99 97 97 100 100 89	86·7 88·7 97·4 96·6 95·6 86·8 89·4 85·1 89·3 87·9 79·2 76·1 73·2 92·8 84·6 76·9 90·1 95·0 97·5 89·6 98·9 98·6 89·8	6.3 4.6 9.4 9.5 9.3 6.9 6.4 9.5 9.1 6.0 4.5 4.7 4.0 5.7 5.7 4.7 4.6 6.6
12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Mean Vapour	96 98 97 97 84 86 86 84 86 84 80 98 82 81 94 98 95 98 98 Ioo mb.	92 98 99 97 97 97 84 87 83 82 96 80 98 83 78 95 98 98 99 99 97 84 85 86 86 98 98 98 98 98 98 98 98 98 98	98 98 98 98 97 96 86 87 82 98 83 75 73 95 98 100 99 91·3 mb.	100 85 97 97 97 94 88 82 81 82 81 82 81 82 81 98 97 94 97 94 99 90 55 mb.	87 98 97 96 88 87 84 87 90 85 85 98 78 81 94 96 93 98 100 100 90 90 90 90 90 90 90 90 90	87 98 98 95 83 86 85 93 90 81 87 76 88 94 94 95 87 99 100 100 100 100	80 98 98 98 91 86 85 89 95 80 91 73 93 90 75 90 83 97 100 89 4 mb.	83 98 98 93 83 84 85 90 93 76 85 72 94 86 76 98 98 98 98 90 93 76 85 90 91 91 91 91 91 91 91 91 91 91	97 94 90 91 84 90 86 73 87 71 98 86 73 99 90 100 90 · I	79 92 98 93 81 96 85 89 90 76 88 76 99 98 87 92 95 96 84 99 98 100 89·2 100	84 76 94 97 94 82 96 77 80 62 98 82 67 65 85 95 96 82 97 98 80 62 98 80 60 80 80 80 80 80 80 80 80 80 8	81 78 97 94 95 77 95 80 87 90 65 87 96 65 85 94 95 83 99 99 86·5	76 80 97 97 95 77 98 88 86 72 64 65 95 79 65 66 90 94 95 100 85.9	84 96 97 96 97 98 88 92 70 64 66 95 73 65 72 98 87 99 95 96 96 97 96 97 97 98 98 98 98 98 98 98 98 98 98	76 92 96 97 97 81 89 89 89 62 69 94 79 67 98 99 96 100 91 99 95 89.2 89.2 89.2 89.3 89.3 89.3 89.3 89.3 89.3 89.3 89.3	95 97 96 96 97 97 98 97 99 81 91 100 100 99 89·7 mb.	95 99 96 97 73 86 85 95 89 76 66 80 99 79 73 80 98 90 100 100 100 89·9	93 97 96 95 86 87 88 95 91 79 98 80 98 95 99 88 95 99 98 80 100 98 91 100 100 100 100 100 100 100	85 93 97 97 97 93 83 91 95 87 87 87 87 87 87 87 98 99 100 100 100	82 93 97 94 96 94 81 93 95 86 72 71 98 73 88 79 98 99 87 100 100	82 95 98 94 96 94 99 92 86 85 87 86 84 97 96 99 92 100 99 93 90 4	83 98 99 94 96 94 97 95 89 82 81 71 66 98 75 99 99 90 100 90 90 90 90 90 90 90 90 90	98 100 95 96 94 82 91 89 77 83 71 66 97 80 82 92 94 99 98 97 100 100 100 mb.	97 91 98 99 97 94 93 88 88 89 81 84 72 72 97 81 83 93 94 98 97 100 100 89	86.7 88.7 97.4 96.6 95.6 86.8 89.3 87.9 276.1 73.2 92.8 84.6 76.9 81.9 90.1 95.0 97.5 89.6 98.9 98.9 98.9	6.3 4.6 9.4 9.5 9.3 6.9 7.6 6.4 9.5 9.1 6.0 4.5 4.1 5.7 7.1 5.7 4.7 4.0 5.7 5.4 4.4 6.6
12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Wean	96 98 97 97 84 86 86 84 86 88 89 98 81 94 94 98 95 98 98	92 98 99 97 97 97 84 87 83 82 96 80 98 83 78 95 98 98 99 99 97 84 85 86 86 98 98 98 98 98 98 98 98 98 98	98 92 98 97 96 97 98 97 98 82 98 83 75 73 95 98 100 99 91:3	100 85 97 97 97 94 88 82 81 82 81 82 81 82 81 98 97 94 97 94 99 90 55 mb.	87 98 97 96 88 87 84 87 90 85 85 98 78 81 94 96 93 98 100 100 90 90 90 90 90 90 90 90 90	87 98 98 95 83 86 85 93 90 81 87 76 88 94 94 95 87 99 100 100 100 100	80 98 98 98 91 86 85 89 95 80 91 73 93 90 75 90 83 97 100 89 4 mb.	83 98 98 93 83 84 85 90 93 76 85 72 94 86 76 98 98 98 98 90 93 76 85 90 91 91 91 91 91 91 91 91 91 91	97 94 90 91 84 90 86 73 87 71 98 86 73 99 90 100 90 · I	79 98 93 81 96 85 89 90 76 69 87 69 73 92 95 96 84 99 98 100 89.2	84 76 94 97 94 82 96 77 80 62 98 82 67 65 85 95 96 82 97 98 80 62 98 80 60 80 80 80 80 80 80 80 80 80 8	81 78 97 94 95 77 95 80 87 90 65 65 85 94 95 83 99 99 99 86 · 5	76 80 97 97 95 77 98 88 86 72 64 65 95 66 90 94 99 95 100 85 9	84 96 97 96 97 98 88 92 70 64 66 95 73 65 72 98 87 99 95 96 96 97 96 97 97 98 98 98 98 98 98 98 98 98 98	76 92 96 97 97 81 89 89 89 62 69 94 79 67 98 99 96 100 91 99 95 89.2 89.2 89.2 89.3 89.3 89.3 89.3 89.3 89.3 89.3 89.3	95 97 96 96 75 95 84 92 94 76 65 71 71 84 98 95 100 100 100 99 89 · 75	95 99 96 97 73 86 85 95 89 76 66 80 99 79 73 80 98 90 100 100 100 89·9	93 97 96 95 86 87 88 95 91 79 98 80 98 95 99 88 95 99 98 80 100 98 91 100 100 100 100 100 100 100	85 93 97 97 97 93 83 91 95 87 87 87 87 87 87 87 98 99 100 100 100	82 93 97 94 96 94 81 93 95 88 72 71 98 73 88 79 98 71 100 100 100 100 100 100 100 100 100	82 95 98 94 96 94 99 92 86 85 87 86 84 97 96 99 92 90 90 90 90 90 90 90 90 90 90	83 98 99 94 96 94 97 99 89 82 81 71 66 98 75 94 86 95 99 99 90 100 96 90 90 90 90 90 90 90 90 90 90	98 100 95 96 94 82 91 89 77 83 71 66 97 80 82 92 94 99 98 97 100 100 100 mb.	97 91 98 99 97 94 93 80 88 88 89 81 84 72 72 97 81 83 93 94 97 97 100 100 89 90 90 90 90 100 100 100 100 100 100 10	86·7 88·7 97·4 96·6 95·6 86·8 89·4 85·1 89·3 87·9 77·2 92·8 84·6 76·9 90·1 95·0 97·5 89·6 98·9 98·9 98·6 89·8	6.3 4.6 9.4 9.5 9.3 6.9 7.6 6.4 9.5 9.1 6.0 4.5 4.1 5.7 7.1 5.7 4.7 4.0 5.7 5.4 4.4 6.6
12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Mean Vapour	96 98 97 97 84 86 86 84 86 84 80 98 82 81 94 98 95 98 98 Ioo mb.	92 98 99 97 97 97 84 87 83 82 96 80 98 83 78 95 98 98 99 99 97 84 85 86 86 98 98 98 98 98 98 98 98 98 98	98 98 98 98 97 96 86 87 82 98 83 75 73 95 98 100 99 91·3 mb.	100 85 97 97 97 94 88 82 81 82 81 82 81 82 81 98 97 94 97 94 99 90 55 mb.	87 98 97 96 88 87 84 87 90 85 85 98 78 81 94 96 93 98 100 100 90 90 90 90 90 90 90 90 90	87 98 98 95 83 86 85 93 90 81 87 76 88 94 94 95 87 99 100 100 100 100	80 98 98 98 91 86 85 89 95 80 91 73 93 90 75 90 83 97 100 89 4 mb.	83 98 98 93 83 84 85 90 93 76 85 72 94 86 76 98 98 98 98 90 93 76 85 90 91 91 91 91 91 91 91 91 91 91	97 94 90 91 84 90 86 73 87 71 98 86 73 99 90 100 90 · I	79 92 98 93 81 96 85 89 90 76 88 76 99 98 87 92 95 96 84 99 98 100 89·2 100	84 76 94 97 94 82 96 77 80 62 98 82 67 65 85 95 96 82 97 98 80 62 98 80 60 80 80 80 80 80 80 80 80 80 8	81 78 97 94 95 77 95 80 87 90 65 87 96 65 85 94 95 83 99 99 86·5	76 80 97 97 95 77 98 88 86 72 64 65 95 79 65 66 90 94 95 100 85.9	84 96 97 96 97 98 88 92 70 64 66 95 73 65 72 98 87 99 95 96 96 97 96 97 97 98 98 98 98 98 98 98 98 98 98	76 92 96 97 97 81 89 89 89 62 69 94 79 67 98 99 96 100 91 99 95 89.2 89.2 89.2 89.3 89.3 89.3 89.3 89.3 89.3 89.3 89.3	95 97 96 96 97 97 98 97 99 81 91 100 100 99 89·7 mb.	95 99 96 97 73 86 85 95 89 76 66 80 99 79 73 80 98 90 100 100 100 89·9	93 97 96 95 86 87 88 95 91 79 98 80 98 95 99 88 95 99 98 80 100 98 91 100 100 100 100 100 100 100	85 93 97 97 97 93 83 91 95 87 87 87 87 87 87 87 98 99 100 100 100	82 93 97 94 96 94 81 93 95 88 72 71 98 73 88 79 98 71 100 100 100 100 100 100 100 100 100	82 95 98 94 96 94 99 92 86 85 87 86 84 97 96 99 92 90 90 90 90 90 90 90 90 90 90	83 98 99 94 96 94 97 99 89 82 81 71 66 98 75 94 86 95 99 99 90 100 96 90 90 90 90 90 90 90 90 90 90	98 100 95 96 94 82 91 89 77 83 71 66 97 80 82 92 94 99 98 97 100 100 100 mb.	97 91 98 99 97 94 93 80 88 88 89 81 84 72 72 97 81 83 93 94 97 97 100 100 89 90 90 90 90 100 100 100 100 100 100 10	86.7 88.7 97.4 96.6 95.6 86.8 89.3 87.9 79.2 76.1 73.2 92.8 84.6 76.9 81.9 90.1 95.0 97.5 89.6 98.9 98.9	6.3 4.6 9.4 9.5 9.3 6.9 7.6 6.4 9.5 9.1 6.0 4.5 4.1 5.7 7.1 5.7 4.7 4.0 5.7 5.4 4.4 6.6

^{*} Computed from the mean temperatures and the mean relative humidities.

From the monthly means for exact hours, Greenwich Mean Time.

Eskdalemuir: (Louvred Hut) $h_t = 0.9$ metre.

1923.

G.M.T.	ı.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
Relative Humidity	% 88·8	89.2	% 89·1	89·1	% 88·9	% 88·4	% 87·1	% 85·2	83.3	% 81·5	% 79·3	% 78·1	% 77·1	% 77·3	% 77:3	% 78·5	% 80·1	% 82·3	% 84·4	% 85·9	% 87·3	% 87·6	% 87·9	% 88·6	% 84·3
Vapour Pressure (in millibars)	mb. 8·o	mb. 8·o	mb. 8∙o	mb. 7·8	1	mb. 8·o	mb. 8·2	mb. 8·3	mb. 8•4	mb. 8·6		mb. 8·7	mb. 8 ·8	mb. 8 ·8	mb. 8 ·8	mb. 8 ·8			mb. 8·5				mb. 8·2		

RELATIVE HUMIDITY: MONTHLY MEANS AND DIURNAL INEQUALITIES.

The departures from the mean of the day are adjusted for non-cyclic change.

154. Eskdalemuir: (Louvred Hut) $h_t = 0.9$ metre.

1923.

Month.	Mean.			G.M.T 2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.
Jan. Feb. Mar.	88.6	-	o·4 -	– o∙5	0.0) 0·2	શે+ છ∙	I + 0·2		+ o·3	1+ 0.5	+ 0.5	— o⋅6	- 2.3	- 2.4	- 2.6	- 2.0	- I·I	0.0	+ 2.5	+ 2.3	+ 2.1	+ 1.1	+ 0.9	+ 0.7	1+ 0.3
April May June	80·4 78·5	 + + ;	5·4 - 6·4 -	+ 5·5 + 8·3	+ 6.3	+ 6·4 + 7·6	+ 5.	3 + 5·9 7 + 6·9	0 + 3.6 0 + 1.8 5 + 1.5	+ o·1	- 4·1	- 4·0	- 4·9 - 9·1	- 6·1 - 8·4	- 8·1	- 8·1 - 6·9	- 8·2 - 8·7	- 8·3 - 8·2	- 7·8 - 5·5	- 4·9	+ 0·4 - 0·6	+ 3.3	+ 5·3	+ 5·9 + 3·7	+ 5·1	+ 5.9
July Aug. Sept.	84·3 83·7 85·2	+ (6·8 6·4 6·4	+ 7·7 + 6·9 + 5·7	+ 6·3 + 6·7 + 6·5	+ 7·1 + 7·4 + 6·3	+ 6· + 7· + 6·	+ 4·4 + 7·2 + 5·6	+ 2·9 + 5·1 + 5·9	- 0·2 + 1·5 + 3·2	- 3·9 - 1·7 - 0·5	- 4·6 - 5·7 - 3·9	- 5·9 - 9·6 - 6·8	- 7·1 - 9·8 - 8·6	- 8·3 - 10·3 - 9·9	- 8·1 - 7·3 - 9·5	- 8·6 - 9·5 - 9·6	- 6·7 - 7·1 - 8·6	- 6·1 - 5·4 - 6·8	- 3·7 - 4·3 - 1·9	- 1·7 - 1·5 + 0·6	+ 1.6 + 2.1 + 2.2	+ 4.6 + 4.3 + 2.8	+ 5·0 + 4·7 + 4·6	+ 4.9 + 5.8 + 4.2	+ 7·0 + 6·4 + 5·7
Oct. Nov. Dec.	84·8 86·7 89·8	+ 4	4·7 1·9 2·1	+ 5·4 + 1·7 + 1·9	+ 5·3 + 1·4	+ 5·3 + o·6 + o·6	+ 5°0 + 1°0 + 1°0	0 + 4·5 0 + 1·7 0 + 0·8	+ 3.4 + 1.9 - 0.5	+ 1·5 + 1·1 - 0·6	+ 0.3 + 1.1	- 2·9 0·0 - 0·7	- 5·2 - 2·1 - 2·9	- 6·9 - 2·1 - 3·3	- 10·0 - 4·3 - 4·0	- 9·5 - 5·1 - 3·2	- 8·1 - 4·5 - 0·7	- 6·3 - 2·5 - 0·1	- 2·8 - 1·0 + 0·1	- 0.6 - 0.6 + 1.2	+ 1·3 + 0·8 + 1·6	+ 0.8 + 0.8	+ 3.0 + 1.9 + 0.6	+ 2.6 + 2.0 + 1.2	+ 3·1 + 2·2 + 1·3	+ 4.4 + 2.0 + 1.1
Year.	84.3	+ 4	4.6	4 ∙9	+ 4.8	+ 4.8	+ 4.0	+ 4.1	+ 2.8	+ 0.0	— o·9	- 2:7	— <u>5</u> ·o	— 6·1	− 7·1	- 7·o	- 7·o	- 5·7	- 4·I	- 2.0	+ 0.1	+ 1.6	+ 3.0	+ 3.3	+ 3.7	+ 4.3

RAINFALL: ANNUAL TOTALS OF HOURLY VALUES.

† Amounts, in millimetres; durations, in hours, for periods of sixty minutes between the exact hours, Greenwich Mean Time.

155. Eskdalemuir: $H_r = 242.0$ metres + 0.4 metre.

1923.

G.M.T.	 	o to I	I to 2	2 to 3	3 to 4	4 to 5	5 to 6	6 to 7	7 to 8	8 to 9	9 to 10	to	11 to Noon	Noon to 13	13 to 14	14 to 15	15 to 16	16 to 17	17 to 18	18 to 19	19 to 20	20 to 21	21 to 22	22 to 23	23 to 24	o to 24
Amount*		mm. 64·9											mm. 64·1						mm. 82·1			mm. 64·6				mm. 1745·2
Duration*	 •••	hr. 70·5	hr. 69·1	hr. 70-6	hr. 69·2	hr. 65·8	hr. 64·6	hr. 69·3	hr. 60·9	hr. 60·1	hr. 58·7	hr. 46·9	hr. 61·5	hr. 54·1	hr. 64·0		hr. 69·0		hr. 68·3	hr. 66·5	hr. 67·9	hr. 63·1	hr. 59·6	hr. 58·6	hr. 64·5	hr. 1527·3

[†] The totals and durations for individual months are printed in the tables on the following pages.

156. Eskdalemuir.

1923.

Notable Falls of the Year.

(a) The greatest amount in a 60 minute period was 13.0 mm., which was recorded between 22h. and 23h., August 23rd. There were a number of occasions when 4 or 5 mm. were recorded in the space of an hour.

(b) Details of the greatest continuous falls are as follows:—

Date.	are as i	OHOWS	•					Amount. mm.	Duration. hr.
April 12th	•••			• • • •	 		 	32	12.9
June 8th	•••		•••	• • • •	 		 	26	10.5
August 2nd	•••			• • •	 •••		 	25	7.6
August 6th-			•••	• • • •	 		 	27	18·3
August 8th-	9th		• • •		 		 	33	13.5
August 20th		• • •	•••		 		 	36	16.3
September 2		th	• • •		 		 	28	13.3
October 29th	1–30th		• • • •	•••	 •••		 	39	18.5
November 21			•••	•••	 	•••	 	29	13.8
November 1	3th			•••	 		 	3 6	21.5
December 11	th-13t	h			 •••		 •••	27	32.3

Wet Periods.

(a) There were five "rain spells" (i.e., a period of fifteen or more consecutive days on each of which o·2 mm. or more of rain fell), viz., January 19th to February 12th, July 19th to August 3rd, August 15th to September 15th, September 30th, October 15th to October 30th. The periods January 28th to February 12th, and August 16th to August 31st were nearly "wet spells," for on only one day in each period was the rainfall less than 1 mm.; and in the period September 30th to September 30th there were only three days on which less than 1 mm. of rain was recorded.

Dry Periods.

- (a) There were no periods of "absolute drought" (i.e., fifteen or more consecutive days on each of which less than 0.2 mm. of rain fell), or of "partial drought" (i.e., (a) There were no periods of absolute drought (i.e., litteen or more consecutive days on each of which twenty-nine or more consecutive days, the mean rainfall of which did not exceed 0.2 mm. per day).

 (b) Details of the principal relatively dry periods are as follows:—

 (i) March 10th to March 26th. Total rain 6.5 mm., all of which fell on the 12th and 13th.

 (ii) April 16th to April 24th. Total rain 2.2 mm., all of which fell on the 21st.

 (iii) June 19th to June 29th. Total rain 0.7 mm., of which 0.4 mm. occurred on the 25th.

^{*} Hourly totals of amount and duration are for 358 days only. Annual total of daily (0-24 hr.) amounts refer to 365 days, but the total duration for the year refers to 358 days. See footnotes to monthly tables.

RAINFALL.

Amounts in millimetres, for periods of sixty minutes, between the exact hours, Greenwich Mean Time.

157. Eskdalemuir: H_r (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + h_r (height of receiving surface above ground) = $242 \cdot 0$ metres + $0 \cdot 4$ metres. January, 1923

157.	Eskd			•				1	above	e grou	ind) =	= 242	∵U m	etres	+ 0.	4 me	tres.						U	anua	r y , 19	72.5.
Day	0-I	1-2	2-3	3-4	4-5	5-6	6-7	7-8	89	9–10	10-11	11-12	12-13	13-14	14-15	15–16	16–17	17–18	18–19	19–20	20–21	21-22	22–23	23-24		0-24
I	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm. •8	mm. 3·1	hr. 2·0
2	1.3	1.0	•1	1.1	1.6	1.3	⋅8	3.0	6.0	2.3	2.3	2.3	 I			·4 2·1		· 5				2.0	2 · I		29·8 4·8	15·3 1·9
3	:::										•••						•••	•••	•••				•••	•••	' *15∙1	
5*						•••					•••		•••				•••	•••				• • •		•••		
6	 1·6	2.3	2.0	2.7													·1		•••	···			·1	• 4	0·6 14·9	15.0 15.0
7 8 9	•2	.3	2.3	.7	1·2 5·3	1.7													•••					• • • • • • • • • • • • • • • • • • •	4·9 13·3	6·o
10		• 2	2.5	4.7	3.3	1.9	1.2	6										•••	•••					•••	7.3	6.1
11			•••																•••					•••		•••
12											• 1			• 2	• 5	• 2									2.0	3.2
14 15	·2	•2	.1	•••			4.4	.3		· I							· · I		• • • • • • • • • • • • • • • • • • • •	·.ı			:::	:::	6.3	6.3
			•••	•••																.3	.3	l			2.0	6.5
16	:::	:::			:::															•2	'4	.3	•1	.1	1.3	6.0
18				•••					·		• • • • • • • • • • • • • • • • • • • •				1.7	1.9		•••							 5·6	5·6
20	•4		.3								•••							• • • • • • • • • • • • • • • • • • • •	•…		.1			•••	0.7	1.6
21										.1		.1	٠ı				•••	•••	•••	•••					0·3 *2·7	2.2
22*	:::				:::		:::				•••						•••				••2		• 2		0.7	2.9
24 25	:::				:::		1.0	·		···						· I			·6					•••	1.8	4·3 1·2
										.2															0.2	0.4
26 27					:::																				o·4 *3·7	o∙6 ?
28 *				1.2	1.0											1.0			•1		:::			•••	6.9	8.4
30	4	.1		ı.	•••				• • • • • • • • • • • • • • • • • • • •			•••			.3			• 2					• 5	•••	1.6	4.0
31				· · ·		.1	•1			.2			1.2	1.0	1.3	2.7	2.3	.7	.3			•••		• • • •	9.8	5.8
Sums.*	4.5	4.1	7.0	13.3	12.2	6.5	9.3	4.5	7.6	3.7	2.6	3.2	1.7	1.2	4.7	9.0	5.5	3.0	1.3	1.4	2.0	3.4	6.0	1.8	141.0	110.4
Total	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	
					1 111.	111.																				
Dura-	6.3	4.8	7.0	7.7	7.0	6.3	7.0	3.9	3.3	3.4	1.8	2.9	2.0	1.2	3.4	6.2	4.6	4.6	3.1	2.8	5.4	2.3	5.6	4.5	110.4	
Dura- tion.*	<u> </u>	4.8	7.0	7.7	1	6.3	7.0	3.9	3.3	3.7	1.8	1	2.0	1.5	3.4	6.2	4.6	4.6	3.1	2.8	5.4	5.3			ry, 19	
158.	<u> </u>	4.8	7.0	7.7 H _r =	7.0	6.3	tres -	3.9	3·3 met	3·7 res.	mm.	2·9	mm.	mm.	mm.	mm.	mm.	mm.	mm.	m·m.	mm.	mm.	Fe	bruai	ry, 19)23.
tion.*	Esko	alem	7.0 uir :	7.7 Hr =	7·0 = 242·	6·3	tres -	3·9 + 0·4	3·3	3·7	1	2.9	<u> </u>			<u> </u>		mm. 3·1	mm. 3.7	n.m. 1·4	mm. ·8 ·7	mm.	Fe mm. 2·2 ·2	mm. 2·3 ·3	ry, 19	hr. 13.7 4.6
158. I 2 3	mm3 .2	4·8 alem mm. · · · · · 6	7.0 uir:	7.7 H _r = mm	7·0 = 242·	6·3 •0 me	7.0 etres -	3·9 + 0·4 mm. 	3·3 metronomic mm. ··· ··· ···	3·7 res. mm. 1·5	mm. 1·6 	mm.	mm. •8 •••	mm. ·9	mm. '4	mm.	mm.	mm. 3·1	mm. 3·7	n.m.	mm. -8	mm. ··2 I·6 ···	mm.	bruai	mm. 20·1 4·0 7·8 0·4	hr. 13.7 4.6 6.7 2.3
158.	Esko	alem	7.0 uir:	H _r = mm 8	7·0 = 242·	6·3 •0 me	7.0 etres -	3·9 + 0·4	3·3	3·7 res. mm. 1·5	mm. 1·6	mm.	mm. •8	mm.	mm. '4 	mm. `3 	mm. • 5	mm. 3·1	mm. 3.7	n.m. I·4 I·2	mm. ·8 ·7 ·1	mm. ·2 I·6 ···	mm. 2 · 2	mm. 2·3 ·3 ·1	ry, 19 mm. 20·1 4·0 7·8	hr. 13.7 4.6 6.7
158. 1 2 3 4 5 6	mm	4·8	7.0 uir: mm	7.7 H _r = mm	7.0 = 242.	6·3 •0 me	7.0 etres -	3·9 + 0·4 mm. 	3·3 metronomic mm.	3·7 res. mm. 1·5 .	mm. 1·6 	mm. ·4 ··· ··· ··· ··· ··· ··· ··· ··· ···	mm. ·8 ··· ··· ··· ··· ··· ··· ··· ··· ···	mm. '9	mm. '4 7	mm. 3 1.5	mm5 1-9 1-0	mm. 3·1 2·3 1·6	mm. 3.7 2.1 1.4	mm. 1·4 1·2 	mm.	mm2 1·6 8 ·5	Fe mm. 2·2 ·2 ·1 ··· ·2	mm. 2·3 ·1 · ·1	min. 20·1 4·0 7·8 0·4 6·7	hr. 13.7 4.6 6.7 2.3 4.6
158. 1 2 3 4 5	mm3 .2 .2	4·8 alem mm. · · · · · 6 · · 1 · · ·	7.0 uir: mm	7.7 H _r = mm 	7.0 = 242.4 mm 	6·3 •0 me	7.0 etres -	3·9 + 0·4 mm.	3·3 meta	3.7 res. mm. 1.5 	mm. 1·6 	2·9 mm. ·4 ··· ··· ···	mm. -8 	mm. ·9	mm. '4	mm.	mm. ·5 ··· ··· 1·9	mm. 3·1 2·3 1·6	mm. 3.7 2.1	n·m. I·4 I·2	mm. ·8 ·7 ·1 · ·9	mm.	F6 mm. 2·2 ·2 ·1 ··· ·2 ···	mm. 2 · 3 · 1 · 1	min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2	hr. 13.7 4.6 6.7 2.3 4.6 14.4 6.4 9.4
158. 1 2 3 4 5 6 6 7 8 9	mm.	4·8	7.0 uir: mm. 1.0	7·7 H _f = mm. ··· ·	7·0 = 242· mm	6·3 · 0 me mm. 3·7 ·1	7.0 etres - mm	3.9 + 0.4 mm. 	3·3 meta mm.	3·7 res. mm. 1·5 .	mm. 1 · 6 2 · 2 · 2 ·	mm.	mm8	mm9	mm. '4	mm.	mm5 1-9 1-0	mm. 3·1 2·3 1·6	mm. 3.7 2.1 I.4	mm. 1·4 1·2 1·5 ·3	mm. ·8 ·7 ·1 ··· ·9 I·ó ·2	mm. ·2 I · 6 · · · · · 8 · 5 · · ·	F6 mm. 2·2 ·2 ·1 ··· ·2 ···	mm. 2·3 3 ·1 ·1	min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4	hr. 13.7 4.6 6.7 2.3 4.6 14.4 6.4
158. 1 2 3 4 5 6 7 8 9 10	mm. '3 '2 '2	4·8	7·0 uir: mm	7·7 Hr = mm	7.0 = 242.	6·3 •0 me mm	7.0 etres - mm 3.82	3.9 + 0.4 mm. 1.3 1.0	3·3 mets mm. 1·9 1·0 1·0	3·7 res. mm. 1·5 .	mm. 1 · 6 1 · 2 2 · 2 1 · 5	mm. '4 1.1 1.4 '3 1.0	**************************************	mm9	mm. '4	mm. 3 1.5 1.5 2	mm5	mm. 3·1 2·3 1·6	mm. 3.7 2.1 I.4	I · · · · · · · · · · · · · · · · · · ·	mm. ·8 ·7 ·1 ·· ·9 1·6 ·2 ··	mm. ·2 1 · 6 · · · · · · 8 · · 5 · · · · · · · · · · · · · · ·	Fe mm. 2·2 ·2 ·1 ··· ·2 ··· ·2 ··· ·	mm. 2 · 3 · 1 ·	min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0	hr. 13·7 4·6 6·7 2·3 4·6 14·4 6·4 9·4 3·4
158. 1 2 3 4 5 6 7 8 9 10 11 12	mm.	4·8	7.0 uir: mm. 1.0	7·7 H _f = mm. ··· ·	7·0 = 242· mm	6·3 · 0 me mm. 3·7 ·1	7.0 etres - mm	3.9 + 0.4 mm. 	3·3 meta mm.	3·7 res. mm. 1·5 .	mm. 1 · 6 2 · 2 · 2 ·	mm.	mm8	mm9	mm.	mm.	mm.	mm. 3·1 2·3 1·6	mm. 3.7 2.1 1.4	mm. 1·4 1·2 1·5 .3	mm	mm. ·2 ·6 · ·8 ·5 · · ·	Fe mm. 2·2 ·2 ·1 ··· ·2 ··· ·2 ··· ·4 ···	mm. 2·3 ·1 ··· ·· ·1 ·1	y, 19 min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7	13.7 4.6 6.7 2.3 4.6 14.4 6.4 9.4 3.4 14.6 11.3 5.9
158. 1 2 3 4 5 6 7 8 9 10 11	mm. '3 '2 '2	4·8	7.0 uir: mm	7·7 Hr = mm	7.0 = 242.	6·3 O me mm 3·7	7.0 etres - mm.	3.9 + 0.4 mm. 1.3 1.0 .5	3·3 mets mm.	3°7 res. mm. 1°5	mm. 1 · 6 1 · 2 2 · 2 1 · 5	mm4 1 · 1 1 · 4 - 3 1 · 0	mm. -8 1 · 0	mm. '9	mm.	mm.	mm5 1 · 9 1 · 0	mm. 3·1 2·3 1·6	mm. 3.7 2.1 1.4	Inm. I · 4 I · 2 I · 5 · 3	mm8 -7 -19	mm2 1-68 -5	F6 mm. 2·2 ·2 ·1 ·· · · · · · · ·	mm. 2·3 ···	min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7 9·3 5·7 	hr. 13.7 4.6 6.7 2.3 4.6 14.4 6.4 9.4 14.6 11.3 5.9 ?
158. 1 2 3 4 5 6 7 8 9 10 11 12 13	mm. '3 '2 '2 '	4·8	7.0 uir: mm	7·7 H _f = mm	7.0 = 242.1 mm	6·3 mm.	7.0 etres - mm 3.8	3.9 + 0.4 mm. 1.3 1.0 	3·3 metri	3°7 res. mm. 1°5 .	mm. 1 · 6 · · · · · · · · · · · · · · · · ·	mm. '4 1 · 1 1 · 4 3 1 · 0	**************************************	mm. ·9 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	mm.	mm.	mm5 1.9 1.0	mm. 3·1 2·3 1·6	mm. 3 ' 7 2 ' 1	I · · · · · · · · · · · · · · · · · · ·	mm8 -7 -19 1-6 -2	mm2 1-68 -5	F6 nnm. 2·2 ·1 ·2 ·4	mm. 2·3 ·3 ·1 ··· ·· ··· ··· ··· ··· ··· ··· ··· ··· ··· ··· ·	ry, 19 mm. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7 9·3 5·7 †2·0	P23. hr. 13.7 4.6 6.7 2.3 4.6 14.4 6.4 9.4 3.4 14.6 11.3 5.9
158. 1 2 3 4 5 6 7 8 9 10 11 12 13 †14 15 16	mm. '3 '2 '2 '	4·8	7.0 uir: mm	7.7 H _f = mm	7.0 = 242.1 mm	6·3 •0 me mm	7.0 etres - mm	3 · 9 + 0 · 4 mm	3°3 meti mm 1°9 1°0 1.8	3°7 res. mm. 1°5 .	mm. 1 · 6 1 · 2 2 · 2 1 · 5	mm. '4 1 · 4 1 · 0	mm. -8	mm.	mm.	mm. 3 1.5 1.5	mm55	mm. 3·1 2·3 1·6	mm. 3 · 7 2 · 1	Inm. I · 4 I · 2 I · 5 · 3	mm8 -7 -19	mm2 1-68 -5	F8 mm. 2·2 ·2 ·1 ·· · · · · · · ·	mm. 2·3 ···	min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7 9·3 5·7 	hr. 13.7 4.6 6.7 2.3 4.6 14.4 6.4 9.4 14.6 11.3 5.9 ?
158. 1 2 3 4 5 6 7 8 9 10 11 12 13 †14 15 16 17 †18	Eskd mm. '3 '2 '2 ' 1 3 ' ' 1 ' 3	4·8	7.0 uir: mm	7.7 H _f = mm	7.0 = 242.1 mm	6·3 •0 me mm. 3·7 ·1 	7.0 etres - mm	3.9 + 0.4 mm. i.o i.o 	3·3 meti mm 1·9 1·0 1·8	3°7 res. mm. 1°5 .	mm. 1 · 6 1 · 2 2 · 2 1 · 5	2·9 mm. ·4 ··· ··· ··· ··· ··· ··· ··· ··· ··· ··· ··· ··· ··· ··· ·	mm. -8	mm.	mm. '4	mm.	mm. '5	mm. 3·I 2·3 I·6	mm. 3·7 2·1	1.4 1.2 1.5 .3	mm8 -7 -19 1.6 -27	mm2 1.68	F6 mm. 2·2 ·2 ·1 ·· · ·1 ·1 ·1	mm. 2·3 ·3 ·1 ··· ·· ··· ··· ··· ··· ··· ··· ··· ··· ··· ··· ·	min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7 †2·0 · 4·0 0·2 †8·1	P23. hr. 13.7 4.6 6.7 2.3 4.6 14.4 6.4 9.4 3.4 14.6 11.3 5.9 ?
158. 1 2 3 4 5 6 7 8 9 10 11 12 13 †14 15 16 17	mm. '3 '2 '2 '	4·8	7.0 uir: mm	7.7 Hr = mm	7.0 = 242. mm	6·3 •0 me mm	7.0 etres - mm.	3.9 + 0.4 mm. i.3 i.0 	3°3 mett mm	3°7 res. mm. 1°5 .	mm. 1 · 6 1 · 2 2 · 2 1 · 5	2·9 mm.	mm8	mm.	mm.	mm. 33 1·5 1·5	mm55	mm. 3·1 2·3 1·6	mm. 3·7 2·1	Inm. I · 4 I · 5 · 3	mm8 -7 -19 1-6 -2	mm.	F6 mm. 2·2 ·2 ·1 ·· ·1 ·1 ·1 ·	mm. 2·3 ·1 ···	min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7 9·3 5·7 †2·0 ·	hr. 13·7 4·6 6·7 2·3 4·6 14·4 6·4 9·4 14·6 11·3 5·9 9·9
158. 1 2 3 4 5 6 7 8 9 10 11 12 13 † 14 15 16 17 † 18 19 20 10 11 19 20 10 11 19 20 10 10 10 10 10 10 10 10 10 10 10 10 10	mm. '3 '2 '2 '	4·8	7.0 uir: mm	7.7 Hr = mm	7.0 = 242. mm	6·3 •0 me mm	7.0 etres - mm	3.9 + 0.4 mm. 1.3 1.0 	3°3 met: mm	3°7 res. mm. 1°5 .	mm. 1 · 6 1 · 2 2 · 2 1 · 5	mm. '4	mm. -8	mm.	mm. '4	mm. 3 1·5 1·5	mm. ·5 ···	mm. 3·I 2·3 I·6	mm. 3·7 2·1	Inm. I · 4 I · 2 I · 5 · 3	mm8 -7 -19 1-6 -2	mm.	F8 mm. 2·2 ·2 ·1 ···	mm. 2·3 ·3 ·1 ··· ·· ··· ··· ··· ··· ··· ··· ··· ··· ··· ··· ·	Ty, 19 min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7 9·3 5·7 †2·0 · 4·0 0·2 †8·1 1·6	P23. hr. 13.7 4.6 6.7 2.3 4.6 14.4 6.4 9.4 3.4 14.6 11.3 5.9 9.9 2.5.0
158. 1 2 3 4 5 6 7 8 9 10 11 12 13 †14 15 16 17 †18 19 20 †21 22	Eska mm	4·8	7.0 uir: mm	7.7 Hr = mm	7.0 = 242. mm	6·3 •0 me mm	7.0 etres - mm.	3.9 + 0.4 mm. 	3°3 met: mm	3°7 res. mm. 1°5 .	mm. 1 · 6 1 · 2 2 · 2 1 · 5	mm. '4	mm. -8	mm.	7 · 3 · 3 · 3 · · · · · · · · · · · · ·	mm. 3 1·5 1·5	mm5	mm. 3·I 2·3 I·6	mm. 3 · 7 · 2 · 1 ·	1.5	mm8 -7 -19 1.6 -27	mm.	** F8 mm. 2 · 2 · 2 · 1 · · · · · · · · · · · · · · ·	bruai mm. 2·3 ·1 ·1 ·1	7, 19 min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7 9·3 5·7 †2·0 · 4·0 0·2 †8·1 1·6	hr. 13·7 4·6 6·7 2·3 4·6 14·4 6·4 9·4 14·6 11·3 5·9 ?
158. 1 2 3 4 5 6 7 8 9 10 11 12 13 †14 15 16 17 †18 19 20 †21 22 23 24	mm. '3 '2 '2 '	4·8	7.0 uir: mm	7.7 Hr = mm	7.0 = 242. mm	6·3 •0 me mm	7.0 etres - mm	3.9 + 0.4 mm. 1.3 1.0 	3°3 met: mm	3°7 res. mm. 1°5 .	mm. 1 · 6 1 · 2 2 · 2 1 · 5	2·9 mm.	mm. -8	mm.	mm.	mm.	mm55	mm. 3·1 2·3 1·6	mm. 3.7 2.1 1.4	mm. 1 · 4 1 · 2	mm8 -7 -19 1.6 -2	mm2 1.6	** F8 mm. 2 · 2 · 2 · 1 · · · · · · · · · · · · · · ·	bruai mm. 2·3 ·1	7y, 19 min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7 9·3 5·7 †2·0 †2·9 0·6	P23. hr. 13.7 4.6 6.7 2.3 4.6 14.4 6.4 9.4 14.6 11.3 5.9 ? 9.9 ? 2.1
158. 1 2 3 4 5 6 7 8 9 10 11 12 13 114 15 16 17 18 19 20 121 22 23	mm. '3 '2 '2 '	4·8	7.0 uir: mm	7.7 Hr = mm.	7.0 = 242. mm	6·3 •0 me mm.	7.0 etres - mm.	3.9 + 0.4 mm. 1.3 1.0 	3·3 met: mm	3°7 res. mm. 1°5 .	mm. 1 · 6	2·9 mm. ·4 ···	mm. ·8 ···	mm.	mm. '4	mm. 3 1·5 1·5	mm. '5	mm. 3·I 2·3 I·6	mm. 3 · 7 · 2 · 1 ·	Inm. I · 4 I · 2 I · 5 · 3 · 8	mm8 -7 -19 1-6 -2	mm	** F8 mm. 2 · 2 · 2 · 1 · · · · · · · · · · · · · ·	bruai mm. 2·3 ·1 ·1 ·1	Ty, 19 min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7 9·3 5·7 †2·0 · 4·0 0·2 †8·1 1·6 †2·9 0·6 7·6	hr. 13.7 4.6 6.7 2.3 4.6 6.4 9.4 3.4 14.6 11.3 5.9 ? ? ? ? ? ? ? ? ? ? ?
158. 1 2 3 4 5 6 7 8 9 10 11 12 13 †14 15 16 17 †18 19 20 †21 22 23 24 25 26	Eskd mm. '3 '2 '2 '1 '3 '1 '3 '1 '3 '1 '4 '1 '3 '1 '3 '1 '3 '1 '3 '1 '3 '1 '3 '1 '3 '1 '3 '1 '3 '1 '3 '1 '3 '1 '3 '1 '3 '1 '3 '1 '3 '1 '3 '1 '3 '1	4·8	7.0 uir: mm	7.7 Hr = mm.	7.0 = 242. mm	6·3 •0 me mm.	7.0 etres - mm.	3 · 9 + 0 · 4 mm	3·3 met: mm. .	3°7 res. mm. 1°5 .	mm. 1 · 6	mm. '4	mm. ·8 ···	mm.	mm. '4	mm. 3 1·5 1·5	mm. ·5 ···	mm. 3·1 2·3 1·6	mm. 3.7 2.1 1.4	mm. 1 · 4 1 · 2	mm8 -7 -19 1.6 -2	mm2 1.6	** F8 mm. 2 · 2 · 2 · 1 · · · · · · · · · · · · · · ·	bruai mm. 2·3 ·1	7y, 19 min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7 9·3 5·7 †2·0 †2·9 0·6 7·6 12·8 7·2 7·2 7·2 7·2 7·2 7·2 7·2 7·2 7·2 7·2 7·2 7·3 7·4 7·5 7	hr. 13.7 4.6 6.7 2.3 4.6 6.4 9.4 3.4 14.6 14.3 5.9 9.9 7.5 7.5 7.5 7.5 7
158. 1 2 3 4 5 6 7 8 9 10 11 12 13 †14 15 16 17 †18 19 20 †21 22 23 24 25	Eskd mm	4·8	7.0 uir: mm	7.7 Hr = mm	7.0 = 242. mm	6·3 •0 me mm 3·7 ·1	7.0 etres - mm.	3.9 + 0.4 mm. 	3·3 met: mm	3°7 res. mm. 1°5	mm. 1 · 6	mm. '4	mm. -8	mm.	mm. '4	mm. 3 1·5 1·5 1·1	mm5	mm. 3·1 2·3 1·6	mm. 3 · 7 · 2 · I ·	mm. 1·4 1·2	mm8 -7 -19 1.6 -2	mm.	** F8 mm. 2 · 2 · 2 · 1 · · · · · · · · · · · · · ·	bruai mm. 2·3 ·1 ·1	Ty, 19 min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7 9·3 5·7 †2·0 · 4·0 0·2 †8·1 1·6 0·6 7·6 12·8	hr. 13·7 4·6 6·7 2·3 4·6 6·4 9·4 3·4 14·6 11·3 5·9 9·9 ? ? 2·1 10·9 9·8
158. 1 2 3 4 5 6 7 8 9 10 11 12 12 13 †14 15 16 17 †18 19 20 17 12 22 23 24 25 26 27	Eskd mm. '3 '2 '2 '3 '1 '1	4·8	7.0 uir: mm	7.7 Hr = mm.	7.0 = 242. mm	6·3 •0 me mm.	7.0 etres - mm.	3 · 9 + 0 · 4 mm	3·3 met: mm. ·· ·· ·· 1·9 ·· 1·0 1·8 ·2 ·· ·· ·· ·· ·· ·· ·· ··	3°7 res. mm. 1°5 .	mm. 1 · 6	2·9 mm. ·4 ···	mm8	mm.	mm. '4	mm.	mm. 1.5 1.9 1.0 1.1	mm. 3·1 2·3 1·6	mm. 3.7 2.1	n.m. 1·4 1·2 1·5 .38	mm8 -7 -19 1.6 -2	mm.	** F8 mm. 2 · 2 · 2 · 1 · · · · · · · · · · · · · · ·	bruai mm. 2·3 ·1 ·1 ·1	Ty, 19 min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7 9·3 5·7 †2·0 · †2·9 0·6 7·6 12·8 7·2 1·6	hr. 13.7 4.6 6.7 2.3 4.6 6.4 9.4 3.4 14.6 14.3 5.9 9.9 7.5 7.5 7.5 7.5 7
158. 1 2 3 4 5 6 7 8 8 9 10 11 12 13 †14 15 16 17 †18 19 20 †21 22 23 24 25 26 27 28	Eskd mm	4·8	7.0 uir: mm	7.7 Hr = mm	7.0 = 242. mm	6·3 •0 me mm	7.0 etres - mm	3 · 9 + 0 · 4 mm	3 · 3 met: mm	3°7 res. mm. 1°5	mm. 1 · 6 1 · 2 2 · 2 1 · 5	mm. '4	mm8	mm.	mm. '4 '7 '33 '33 '55 1.66	mm.	mm. ·5 ···	mm. 3·1 2·3 1·6	mm. 3.7 2.1 1.4	1.5	mm8 -7 -19 1.6 -27	mm2 1.68 -5	** Fe mm. 2 · 2 · 2 · 1 ·	bruai mm. 2·3 ·1 ·1 ·1	7y, 19 min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7 9·3 5·7 †2·0 · †2·9 12·8 7·6 12·8 7·6 157·5 hr.	hr. 13·7 4·6 6·7 2·3 4·6 6·4 9·4 14·6 11·3 5·9 ? ? ? ? ? ? ? 2·1 10·9 9·8 12·1 3·3 150·4
158. 1 2 3 4 5 6 7 8 8 9 10 11 12 13 †14 15 16 17 †18 19 20 12 22 23 24 25 26 27 28 Sum†. Total Dura-	Esko mm. '3 '2 '2	4·8	7.0 uir: mm	7.7 Hr = mm	7.0 = 242. mm	6·3 •0 me mm	7.0 etres - mm.	3 · 9 + 0 · 4 mm 4 · 8 4 · 8	3·3 met: mm i.g i.o i.s i.o i.s i.o i.s i.o i.s i.o i.s i.o i.s i.o i.s i.o i.o i.s i.o i.o i.o i.o i.o i.o i.o i.o i.o i.o	3°7 res. mm. 1°5	mm. 1 · 6 1 · 2 2 · 2 1 · 5	mm. '4	mm8	mm.	mm. '4 '7 '3 '3 '3 '5 I·6	mm. 3 1·5 1·5	mm5	mm. 3·1 2·3 1·6	mm. 3.7 2.1	n.m. 1·4 1·5	mm8 -7 -19 1-6 -2	mm2 1.68 -5	** F6 mm. 2 · 2 · 2 · 1 · · · · · · · · · · · · · · ·	brual mm. 2·3 ·1 ···	Ty, 19 min. 20.1 4.0 7.8 0.4 6.7 13.6 14.4 14.2 2.0 10.7 9.3 5.7 †2.0 * 4.0 0.2 †8.1 1.6 †2.9 0.6 7.6 12.8 7.2 1.6	hr. 13·7 4·6 6·7 2·3 4·6 6·4 9·4 14·6 11·3 5·9 ? ? ? ? ? ? ? 2·1 10·9 9·8 12·1 3·3 150·4
tion.* 158. 1 2 3 4 5 6 7 8 9 10 11 12 13 † 14 15 16 17 † 18 19 20 17 22 23 24 25 26 27 28	Esko mm	4·8	7.0 uir: mm	7.7 Hr = mm	7.0 = 242. mm	6·3 •0 me mm	7.0 etres - mm	3.9 + 0.4 mm. 1.3 	3·3 met: mm i.9 i.0 i.8	3.7 res. mm. 1.5	mm. 1 · 6	mm. '4	mm8	mm.	mm.	mm. 3 1·5 1·5	mm5 1·9 1·01 -2	mm. 3·1 2·3 1·6	mm. 3.7 2.1 1.4	1.5	mm8 -7 -19 1.6 -27	mm2 1.68 -5	** Fe mm. 2 · 2 · 2 · 1 ·	bruai mm. 2·3 ·1 ·1 ·1	7y, 19 min. 20·1 4·0 7·8 0·4 6·7 13·6 14·4 14·2 2·0 10·7 9·3 5·7 †2·0 · †2·9 0·6 7·6 12·8 7·2 1·6 157·5 hr. 150·4	hr. 13·7 4·6 6·7 2·3 4·6 6·4 9·4 14·6 11·3 5·9 ? ? ? ? ? ? ? 2·1 10·9 9·8 12·1 3·3 150·4

^{*} The Sums of hourly amounts are for 28 days only. On 5th, 22nd, 28th, the amounts of rain could not be distributed among the actual hours of fall, and have been omitted from the hourly columns but have been included in the daily totals (0-24 h.). The hourly durations and the total duration refer to 28 days only.

days only.

† The sums of hourly amounts, the totals of hourly duration and the total duration refer to 25 days only.

The amounts of snow and rain on 14th, 18th, 21st could not be distributed among the hours of fall, but have been included in the daily total (0-24 h.). Snow was blown out of rain gauge on 18th by wind.

Amounts in millimetres, for periods of sixty minutes, between the exact hours, Greenwich Mean Time.

159. Eskdalemuir: Hr (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + hr (height of receiving surface

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160. Eskdalemuir: H _r = 242·0 metres + 0·4 metres. mm.	8 65.1	,5.1		5.1	05	3⋅8		1.7	5	1.	1.3	1.9]]	3.2	.0	3	2.2	1.4	3.1	2.8	1.4	2.9	'	1.0	4.0	4.3	3.8	4.5	3.8	2.2	.3	2.	2.8	1.7	3.3	Dura-
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^{*} Sums of hourly amounts, total hourly durations and total duration refer to 29 days only. On the 25th the amount of snow could not be distributed among the actual hours of fall, but has been included in the daily total (0-24 hr.).

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Amounts in millimetres, for periods of sixty minutes, between the exact hours, Greenwich Mean Time.

161. Eskdalemuir: H_r (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + h_r (height of receiving surface above ground) = $242 \cdot 0$ metres + $0 \cdot 4$ metres. May, 1923.

Dura

Day.	o–1	I-2	2-3	2-4	4-5	5–6	6-7	7-8	8–9	9–10	10–11	11-12	12–13	13–14	14-15	15–1 6	16–17	17–18	18–19	19-20	20–21	21-22	22-23	23-24	024	tion. 0–24
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1																										
162.	Eskd	alemi	uir :	Hr =	242 ·	0 me	tres -	⊢ 0·4	metr	es.														Jun	10, 19	23.
162.			uir:	$H_r = mm.$	242·	0 me	tres -		metr	es.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	Jun	19, 19	23.
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1 2 3 4 5 5 6 7 8 9 10 11 12 13 14	mm	mm	mm	mm	mm.	mm	mm	mm	mm	mm 2·9 1·8	 3.6 1.8	 3·2 ·6	 4.8 	 6.0 .1 1.2	 		 	 				 		mm	mm	hr 0·5 2·7 2·0 10·5 (8·7) 6·9 0·8 4·4 2·8 1·0
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1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	mm	mm	mm	mm	mm.	mm	mm.	mm	mm	mm 2·9 1·8	 3.6 1.8	 	 4·8 ·3 ·1 				 	 				 	 	mm	mm 0.2 0.8 1.6 0.2 26.2 5.9 7.9 0.2 5.1 1.1 1.1 1.2 0.6 0.2	hr 0.5 2.7 2.0 10.5 (8.7) 6.9 0.8 4.4 2.8 1.0 3.4 2.0
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	mm	mm	mm	mm	mm.	mm	mm.	mm	mm	mm 2·9	3.6 1.8		 4.8 									 		mm	mm 0.2 0.8 1.6 0.2 26.2 5.9 7.9 0.2 5.11 1.1 1.2 0.6 0.2	hr 0.5 2.7 2.0 10.5 (8.7) 6.9 0.8 4.4 2.8 1.0 3.4 2.0 1.9
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	mm	mm	mm	mm	mm.	mm	mm.	mm	mm	mm 2·9 1·8	3.6 1.8		4.8	6·0								 	 	mm	mm 0.2 0.8 1.6 0.2 26.2 5.9 7.9 0.2 5.1 1.1 1.2 0.6 0.1 0.4	hr 0.5 2.7 2.0 10.5 (8.7) 6.9 0.8 4.4 2.8 1.0 3.4 2.0
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mm	mm	mm	mm	mm.	mm	mm.	mm	mm	mm 2·9	 3.6 1.8 		 4.8 	6.0 11.2								 		mm	mm 0.2 0.8 1.6 0.2 26.2 5.9 7.9 0.2 5.11 1.1 1.2 0.6 0.1 0.4	hr
1 2 3 4 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum.	mm	mm	mm	mm	mm	mm	mm.	mm	mm	mm 2·9 1·8	 3.6 1.8 		 4.8 	 6·0 .1 1·2 				 					 	mm	mm 0.2 0.8 1.6 0.2 26.2 5.9 7.9 0.2 5.1 1.1 1.1 1.2 0.6 0.1 0.4 0.7	hr 0.5 2.7 2.0 10.5 (8.7) 6.9 0.8 4.4 2.8 1.0 1.0 1.9 1.9
1 2 3 4 5 6 77 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum. Total Dura-	mm	mm	mm	mm	mm.	mm	mm	mm	mm	mm 2·9	 3.6 1.8 		 4.8 		 							 		mm	mm 0.2 0.8 1.6 0.2 26.2 5.9 7.9 0.2 5.11 1.1 1.2 0.6 0.1 0.4 0.7	hr 0.5 2.7 2.0 10.5 (8.7) 6.9 0.8 4.4 2.8 1.0 1.0 1.9 1.9
1 2 3 4 5 5 6 77 8 8 9 10 11 12 13 14 15 16 177 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum. Total	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm 2·9 1·8	3.6 1.8		4.8											mm	mm 0.2 0.8 1.6 0.2 26.2 5.9 7.9 0.2 5.11 1.1 0.6 0.2 0.1 0.4 0.7 53.5	hr

RAINFALL. 145

Amounts in millimetres, for periods of sixty minutes, between the exact hours, Greenwich Mean Time. Amounts in millimetres, for perioas of sixty minutes, occurrent the station above M.S.L.) + h_r (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + h_r (height of receiving surface above ground) = $242 \cdot 0$ metres + $0 \cdot 4$ metres.

Day.															+ 0.4										iy, it	
,	0-I	1-2	2-3	3-4	4-5	56	6-7	7-8	8–9	9–10	10–11	11-12	12–13	13–14	14–15	15–16	16-17	17–18	18–19	19–20	2021	21-22	22–23	23-24	0-24	Dura- tion. 0–24
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	hr.
1 2				• 5			···	· · · I						•••								• 2			2.3	0·5 5·4
3 4	•4	•4	1.4	2.5	1.5	·8	.3	1.2	•8	.7		·2 ·5	 •6	·5	·1		 •4								11·7 4·2	7·I
5		••2	7	• 3			• 5	• • 5	•6		•3	.1			'										5.7	10.5
. 6						•••								···												
7 8													·5	8.2			• 5	1.2							10.5	2.2
9 10	:::						1.0	 1·8	2.4		•••					•••									5·7	4·4
	ľ									İ	•••										[0.8	1.4
11 12																		•••					:::			
13 14			•••	•••				•••		•••		•••	•••		:::	•••						:::				:::
15			•••	•••	•••			• 1	•••		•••	•••	•••	• • • •		.1	• 2	•2	• 2	.3	.1	.1	.3	.3	1.7	(9·2)
16 17	1.1											 •6	 I·2		·			···	···	·8					2·1 4·5	1·6 4·3
18			•••											•••						•••						
19 20								2.0	2.2	1.4	·6	·6	·4 			:::				1.0		· I	.1	1.0	9.5	9·9
21	1.2	.8	1.1	1.4																					4.5	3.8
22 23	·	1.9	3·5	2.2	 1·8	2.6	1.3	·6		1.1	1.3		•••			1.1							· · · I	.3	7.3	12·9 7·9
24			•••									•••	•••			•••		···							0.2	0.7
25	'''	•••			•••	•••	•••		•••		•••	•••		•••			•••		ł	}	-	1			0.6	2.2
26 27		•••		•••					• • • • • • • • • • • • • • • • • • • •													2.0	• 5		3.6	4.2
28 29	1.0 .1		1.0	• 2	·2 ·4	2.7	·		•••	.5					.6	1 .1	• • • • • • • • • • • • • • • • • • • •			:::		4	5		7·6 5·4	8.1
30		•5	•••	•2	••••				•••			1.0	·ı		• • • • • • • • • • • • • • • • • • • •				2.2	2.0	2.2	3.6	1.3	1.0	14.1	7.3
31	·2	•1								1.2		4.1	٠1	.7	1.3	3.1		2.4	3.3	•8	•8				18.0	9.2
Sum.	4.8	4.8	8.2	7.4	5.2	8.0	4.4	6.6	7·1	6.1	3.4	7.9	3.1	11.2	3.8	6.6	1.8	5.1	6.8	5.6	4.0	6.7	3.9	4.2	137.0	138.1
Total	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	
Dura- tion.	8.4	5.4	6.5	5.2	6.2	5.6	6.3	7.8	5.6	6.4	4.6	7.1	5.1	5.6	5.0	2.1	2.1	5.2	4.3	5.7	4.3	4.6	2.2	7.3	138.1	
164.	Eskd	alem	uir :	$H_r =$	242	0 me	tres -	+ 0·4	met	res.													- 1	Augus	st, 19	23.
ı	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	hr. 0·3
2				•••		···		•••	٠1	.8	1.6	•2	٠ı	• • • • • • • • • • • • • • • • • • • •		.3	2.1	2.0	6.2	5.8	6.6	2.6	∙8	1.0	30·2 2·6	11.0
3 4	·8 			·4 						·														:::		4.5
5		•••	•••	•••			•••		• • • • • • • • • • • • • • • • • • • •		•••	•••	•••	•••		•••	.1								0.1	
6 7	1.7	 3·o			2.4	2.6	3.1	1·1	1.0		1.4	 I·2	 ·7	•••		·5						1.3	'4	I · 2	5.7	7·3 15·1
8 9		, ,	1.4	1.0								1					i	.2	T		,	• • • •		1	22.9	
10	2.7	4.5	1.9	•••		 T:4	T.6	•••	•••		•••	, · · ·		• 1	.3	·ı	•••		1.5	4.3	2.0	1.3	 1·6	3.4	14.7	8.7
	1	4·5 	5·2	1·6 2·9	-	1·4 	1·6 					•••								4.3	1	1				8·7 7·0
11			 5·2	2.9	··6	1.4	1.6			1	J			•••		•••				•••	2.0	1.3	 1·6 	3.4	14·7 18·9 	7.0
11 12 13	 		 5·2 	 2·9 	···6	1.4	1.6		•••		•••	•		•••	•••	•••					2.0	1.3	 1·6 	3.4	14·7 18·9	7.0
12 13 14	 ·6 		 5·2 	2.9			1·6 .8	 i.o				···					···				2.0		i·6	3·4 	14·7 18·9 	7.0
12 13 14 15	 .6 	 .5 	 5·2 	 2·9 	······································		 .8 	 I.0	 .5		···	···					 				2·0 		 i·6 	3.4	14·7 18·9 0·2 5·3 0·8	7·0 8·0
12 13 14 15 16 17	 6 	··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	 5·2 .6 	 2·9 3 	 .6 .7 	1·4 .3 	 .8 	 1·0 				···· ··· ··· ··· ··· ···					 			 2.3	2·0 I·3	 	 1·6 2·8 (·1)	3.4 2	14.7 18.9 0.2 5.3 0.8 9.5 14.6	7.0 8.0 1.8 4.6
12 13 14 15 16 17 18	 .6 	 .5 	 5·2 .6 	2·9	 .6 .7 		 .8 	 I·O	 .5 		···		···	···			···			 2.3 .2 .5	2·0 1·36 1·2	1·3 	 1·6 2·8 (·1)	 3·4 2 I·4 ()	14.7 18.9 0.2 5.3 0.8 9.5 14.6 7.3 1.4	7.0 8.0 1.8 4.6 10.5 8.7 1.3
12 13 14 15 16 17	 .6 .8 .1	 .5 	 5·2 	 2·9 3·8 I·I 	 .6 .7 2·I I·8	1·4 2·1	 .8 	 			···	···	 	 			 	 		 4.3	2·0 1·3 ·6	1·3 1·7 2·4	 1·6 2·8 (·I)	3·4 2	14.7 18.9 0.2 5.3 0.8 9.5 14.6 7.3 1.4	7.0 8.0 1.8 4.6 10.5 8.7 1.3 6.6
12 13 14 15 16 17 18	 .6 .8 .1		 5·2 .6 1·2 .6	 2·9 3·8 1·1	 .6 .7 2.1 1.8	1·4 2·1	 .8 	 	 		···	 	 	 			 			 2.3 .2 .5	2·0 1·36 1·2	1·3 	 1·6 2·8 (·1)	 3·4 2 I·4 () I·3	14.7 18.9 0.2 5.3 0.8 9.5 14.6 7.3 1.4	7.0 8.0 1.8 4.6 10.5 8.7 1.3
12 13 14 15 16 17 18 19 20 21 22 23	 .6 .8 .1 5.2 	 	 5·2 1·2 1·8 	 2·9 3·8 1·1 4·8	67	1·4 2·I	 		 .5 		 			 	 	 	 			 4.3	2·0 1·36 1·2 1·8	1·3 1·7 2·4	 1·6 2·8 (·1) 2·0	 3.4 2 I.4 () I.3	14.7 18.9 0.2 5.3 0.8 9.5 14.6 7.3 1.4 17.0 19.6 4.1	7.0 8.0 1.8 4.6 10.5 8.7 1.3 6.6
12 13 14 15 16 17 18 19 20	 .6 .8 .1 5.2	 	 5·2 1·2 1·8	 2·9 3·8 1·1 4·8 	·6 ·7 ·7	1·4 2·1	1.6	 				 	 	 		 		 I·o	 4.2	 4.3 	2·0	1·3 1·7 2·4	 1·6 2·8 (·1) 2·0 	 3·4 1·4 () 1·6	14.7 18.9 0.2 5.3 0.8 9.5 14.6 7.3 1.4 17.0 19.6 4.1 25.7	7.0 8.0 1.8 4.6 10.5 8.7 1.3 6.6 12.7 4.6 14.9
12 13 14 15 16 17 18 19 20 21 22 23 24 25	 .6 .8 .1 5.2 	 	5·2	 2·9 3·8 1·1 4·8 	·6 ·7 · · · · · · · · ·	1.4 2.1	1.6		 .5 	 										 2.3 2.5 4.3 2.5 2.5	2·0	1·3 1·7 2·4	1.6 2.8 (· I) 2.0 13.0 2.7	3·4	14.7 18.9 0.2 5.3 0.8 9.5 14.6 7.3 1.4 17.0 19.6 4.1 25.7 0.9 8.4 5.9	7.0 8.0 1.8 4.6 10.5 8.7 1.3 6.6 12.7 4.6 14.9 0.7 5.5
12 13 14 15 16 17 18 19 20 21 22 23 24 25	 .6 .8 .1 5.2 .1 .1	 2.7 	5·2	 2·9 3·8 1·1 4·8 	·6 ·7 ·	1·4 2·1	1.6	 I.O 		 					 			 1.0		2·3 ··2 ··5 ··. 4·3 ··2 ··1 ··2 ··1	2·0	I·3 I·7 2·4	1.6 2.8 (· I) 2.0 13.0 2.7	3·4	14.7 18.9 0.2 5.3 0.8 9.5 14.6 7.3 1.4 17.0 19.6 4.1 25.7 0.9 8.4 5.9 7.2 6.8	7.0 8.0 1.8 4.6 10.5 8.7 1.3 6.6 12.7 4.6 9.7 5.5 7.0 9.4 9.4
12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	 .6 .8 .1 .5.2 .1 		5·2 1·2	 2·9 3·8 I·I 4·8 	·6 ·7	1·4 2·1	1.6	 I·O 	 	 										 2.3 2.5 4.3 2.5 2.5	2·0	1·3 1·7 2·4	1.6 2.8 (· I) 2.0 13.0 2.7	3·4	14.7 18.9 0.2 5.3 0.8 9.5 14.6 7.3 1.7 17.0 19.6 4.1 25.7 0.9 8.4 5.9 7.2	7·0 8·0 1·8 4·6 10·5 8·7 1·3 6·6 12·7 4·6 14·9 0·7 5·5 7·0
12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	·6		5·2	2·9 4·8	·6 ·7 ·7 · · · · · · · · ·	1.4 2.1	1.6		 											2·3 4·3 2·5 3·3	1·3	I·3 I·7 2·4	1·6 2·8 (·1) 2·0 13·0 2·7 1·3	3'4	14.7 18.9 0.2 5.3 0.8 9.5 14.6 7.3 1.4 17.0 19.6 4.1 25.7 0.9 8.4 5.9 7.2 6.8 18.6	7·0 8·0 1·8 4·6 10·5 8·7 1·3 6·6 12·7 4·6 14·9 5·5 7·0 5·9 4·2 11·7
12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	·6 ·8 ·1 ·5·2 ·1 ·1 ·1 ·2 ·3 ·5 ·5		5·2	2·9	·6 ·7 ·2·1 1·8 · · · · · · · · ·	1·4 2·1	1.6		 	 											2·0	1·3 1·7 2·4	1·6 2·8 (·1) 2·0 13·0 2·7 1·3	3'4	14.7 18.9 0.2 5.3 0.8 9.5 14.6 7.3 1.7 17.0 19.6 4.1 25.7 0.9 8.4 5.9 7.2 6.8 18.6 4.4 8.1	7.0 8.0 1.8 4.6 10.5 8.7 1.3 6.6 12.7 4.6 9.7 5.5 7.0 5.9 4.2 11.7 3.9 6.3
12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	·6 ·8 ·1 ·5 ·1		5·2	2·9	·6 ·7 ·7 ·2·1 1·8 · · · · · · · · ·	1.4 2.1	1.6		 							 1.5 1.6 1.6				 2·3 4·3 2·5 3·3 	1·3	1·3 1·7 2·4	1.6 2.8 (·1) 2.0 13.0 2.7 1.3 1.3 24.8	3·4	14.7 18.9 0.2 5.3 0.8 9.5 14.6 7.3 1.4 17.0 19.6 4.1 25.7 0.9 8.4 5.9 7.2 6.8 18.6 4.4 8.1 261.9	7.0 8.0 1.8 4.6 10.5 8.7 1.3 6.6 12.7 4.6 9.7 5.5 7.0 5.9 4.2 11.7 3.9 6.3
12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	·6 ·8 ·1 ·5·2 ·1 ·1 ·1 ·2 ·3 ·5 ·5		5·2	2·9	·6 ·7 · · · · · · · · ·	1·4 2·1	1.6														2·0	1·3 1·7 2·4	1·6 2·8 (·1) 2·0 13·0 2·7 1·3	1.4 () 1.3 1.6 1.6 1.6	14.7 18.9 0.2 5.3 0.8 9.5 14.6 7.3 1.7 17.0 19.6 4.1 25.7 0.9 8.4 5.9 7.2 6.8 18.6 4.4 8.1	7.0 8.0 1.8 4.6 10.5 8.7 4.6 6.6 12.7 4.6 4.9 9.7 5.5 7.0 3.9 6.3

Day.

0-1

1-2

mm. mm. mm.

2-3

Amounts in millimetres, for periods of sixty minutes, between the exact hours, Greenwich Mean Time.

 $9-10 \left| 10-11 \right| 11-12 \left| 12-13 \right| 13-14 \left| 14-15 \right| 15-16 \left| 16-17 \right| 17-18 \left| 18-19 \right| 19-20 \left| 20-21 \right| 21-22 \left| 22-23 \right| 23-24$

• 2

O-24 Dura-

mm.

0-24

hr.

165. Eskdalemuir: H_r (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + h_r (height of receiving surface above ground) = $242 \cdot 0$ metres + $0 \cdot 4$ metres. September, 1923.

7-8

mm.

5-6

mm. mm. mm. mm.

6-7

3 4	 3'4	 4·8	 1·8																		 			1·8	 1·8 12·8	 1·0 6·9
5	··I	··I		••2							· I								2.7	2.3				···	3°4 6°2	5.8
7 8 9	·3 	·3	·2 													•••									 1.1	3.4
10		•••					• 2																	•••	3.2	3.3
11 12 13	··· ·4	···	 5		··i	··· ··2 I··2	·6	1·1 1·8	··· ·2 I·0	··· ·5 2·0	 1·6	 I·I	··· ···			· I	· I		· 1	· 2 ·	2.2	1·4 	·6 	·3 	5·7 5·9 15·7	5·8 8·7 13·5
14	1.3	2.0		1.5								·	'	··· •4	···										5·4 1·0	4·5 1·3
16 17				·6		·4 ·1	·1	·1		 •9	 1·6	 ·6	 I·2	 1·6	 1·6	2.2		1.3	2.2	I.0	 •8	2.6	 •4	 ·3		4·I 15·2
18 19 20	::: ::::					1.3	1.0		··· ·· ₇			····	··· ·4 ···	···	· · · · · · · · · · · · · · · · · · ·	··· ·4 ···	·8 ·2 ···	· · · · · · · · · · · · · · · · · · ·	2 · 2	···			 .3		1·0 4·9 5·2	7·9 4·0
2I 22	 •5	 I·o			•2	.8 1·6	·4 ·8									3.4	·				 ·6			·6	2·0 10·8	3·4 8·2
23 24	:::									•••							•••	· 5					· I	 1·7	0·7 1·8	0.8
25 26		2.8	2.8					.7		4.4			2.2	2.6	4.9		.3	3.2	·2	1.0	. I				1.9	3·8
27 28 29	 '4	 I·0	···						· I	···	4.3	1·3 	4.2	4.0	2.3	2.0	1·6 	3.8	1·3 		·8 	·4 	·4 	2.2	30·6 2·5 2·6	14·9 5·0 4·6
30	<u></u>			• 2	.1					()	(.1)	()	(.1)	()	<u></u>						•••			•••	0.2	1.7
Sum Total	8·1	12·4 hr.	6·4 hr.	5·1 hr.	5·6 hr.	6·8 hr.	7·8 hr.	5.7 hr.	3·4 hr.	8·8 hr.	8·8 hr.	5·7 hr.	10·2 hr.	9·7 hr.	9·5 hr.	10·1 hr.	6·o hr.	hr.	hr.	7·7 hr.	5.4 hr.	5.4 hr.	3·0 hr.	9·0 hr.	181·9 hr.	151.9
Dura- tion.	6.7	7.0	7.3	7.7	8.5	7.7	7:3	6.4	5.6	4.0	4.6	7.3	6.0	6.0	5.0	5.9	5.8	8.1	7.6	6.7	5.6	4.8	4.2	5.8	151.9	_
166.	Eskd	alem	uir :	H _r =	= 242·	·0 me	etres -	+ 0 · 4	l met	res.													0	ctobe	r, 19	23.
I	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	hr. 0·8
3				·4 	•••		· 1	 •5					•1		· I	···							•••		3.1	3·0 4·6
					1	1	1			ı	1	1		ł	1				l .	i	1	1		1		3·0 4·6 8·9
3 4 5					 		·8 ··. ·5 · 2·5	·5 ··4 ··1	·5 ··2 ··.	·2 ·9 ·4	···· ···· ··6 ··5	··· ·4 ··· ·4	·1 ·6 · ·3	 I·0	···· ··6	·4 ··· ·4	· · · · · · · · · · · · · · · · · · ·		3·3 	··· ·· ·· ·1 ··2 ···			··· ·3		3·1 8·2 2·3 6·8	4·6 8·9 3·4 8·6
3 4 5					···		·8 ··· ·5	·5 ··· ·4	·5 ····	·2 	···· ····	··· ·4	·1 ·6	 I·0	 ·6	·4 ··· ·4	···		3·3 	 .1			··· ··3	2	3·1 8·2 2·3	4·6 8·9
3 4 5 6 7 8 9		 		···· ··· ··· 2·4	··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	 .2 1.3 	·8 ·5 2·5 	·5 ·4 ·1 ·1	·5 ·2 ·2	·2 ·9 ·4 	··· ··· ··6 ··5 ···	··· ·· ·4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ··	·1 ·6 · ·3 ·	 I·0	6	'4 '4 I·2	· 1	 .6	3·3 2·1 	··· ·· ·· ·1 ·2 ··· 1·7 ···		 2.6	 .3 1.4 2.2	2	3·1 8·2 2·3 6·8 11·4 11·6	3·4 8·6 6·6 9·1
3 4 5 6 7 8 9 10	 .8 	 		 2·4 ·I	 	 	.8 .5 2.5 .7 .3 .1 .2 	.5 .4 .1 	 .2 2.2 2.3 	·2 ·9 ·4 I·7 I·9	 	··· ··4 ··· ··4 ··· ·· ·· ·· ·· ·· ·· 4·7 ···	·1 ·6 ·3 ·2 ·9	 1·0 ·2 		'4 '4 I'2 '9	·1 ··· ·1 ··· ·7 5·0	 	.5 3·3 2·1 ·2	 .1 .2 1.7 .2	 2·2 ·2	 2.6 1.2	 .3 1.4 2.2 1.0	 .2 .8 .5 	3·1 8·2 2·3 6·8 11·4 11·6 16·9 (0·3) 14·2 	4·6 8·9 3·4 8·6 6·6 9·1 10·3 0·8 8·2
3 4 5 6 7 8 9 10 11 12 13 14 15	 .8 	 		 2·4 ·I	 	 1·3 ·1 ·2	.8 .5 2.5 .7 .3 .1 .2	·5 ·4 ·1 1·8	 2.2 2.3 	·2 ·9 ·4 I·7 I·9	 	··· ··4 ··· ··4 ··· ··4 ··· ·· ·· ·· ··	·1 ·6 ·3 ·2 ·9	1.0		·4 ·4 I·2 ·9	· I	 	3·3 2·1 2·2	 1.7 .2 	 2·2 ·2 	 2.6 I.2	 .3 1·4 2·2 1·0 		3·1 8·2 2·3 6·8 11·4 11·6 16·9 (0·3) 14·2 0·9 5·8	4.6 8.9 3.4 8.6 6.6 9.1 10.3 0.8 8.2 2.7
3 4 5 6 7 8 9 10		 		 2·4 ·I	 .9 .2 .7	 1·3 ·1 ·2 I·1	·8 ·5 2·5 ·7 ·3 ·1 ·2	·5 ·4 ·1 ·1	 .2 2.2 2.2 	·2 ·9 ·4 I·7 I·9	 	 .4 .4 4.7 	·1 ·6 ·3 ·2 ·9	1.0		'4 '4 I'2 '9	· I	 	.5 3·3 2·1 	 .1 .2 1.7 .2 	 2·2 ·2 	 2.6 1.2	 .3 1·4 2·2 1·0 		3·1 8·2 2·3 6·8 11·4 11·6 16·9 (0·3) 14·2 	4.6 8.9 3.4 8.6 6.6 9.1 10.3 0.8 8.2 2.7
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	 		 	 2·4 ·I 2·0 	 		·8 ·5 2·5 ·7 ·3	.5 .4 .1 	.5 .2 2.2 2.3 	·2 ··· ··9 ·4 ··· I·7 ··· I·9 ··· ··· ··· ··· ··· ··· ···		·4 ·4 ·4 ·4 ·4 ·1	·1 ·6 ·3 ·2 ·9	 I·O ··· ··· ···		'4 '4 I'2 '9	· I	 	.5 3·3 2·1 ·2 2·2 		 2·2 · 		1.4 2.2 1.0		3·1 8·2 2·3 6·8 II·4 II·6 I6·9 (0·3) I4·2 0·9 5·8 0·4 7·3 I2·2 0·8	4.6 8.9 3.4 8.6 6.6 9.1 10.3 0.8 8.2 2.7 5.2 0.9 7.2 6.7 1.9
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	 		 .3 .8 	 2·4 ·1 2·0 	 		·8 ·5 2·5 ·7 ·3	.5 '4 .1 	 2 2 	·2 ·9 ·4 I·7 I·9	 	 .4 4.7 	·1 ·6 ·3 ·2 ·9	1.0		'4 '4 1'2 '9	· 1 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·		.5 3·3 2·1 ·2 2·2 	 1.7 	 2·2 	 2.6 1.2 	 1.4 2.2 1.0 		3·1 8·2 2·3 6·8 II·4 II·6 I6·9 (0·3) I4·2 0·9 5·8 0·4 7·3 I2·2	4·6 8·9 3·4 8·6 6·6 9·1 10·3 0·8 8·2 2·7 5·2 0·9 7·2 6·7
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20				 2·4 ·1 			·8 ·5 2·5 ·73 ·1 ·2	.5 '4 .1 	·5 ·2 2·2 2·2	.29 .4 1.7 1.9	 	·4 ·4 · · · · · · · · ·	·1 ·6 ·3 ·2 ·9	1.0		'4 '4 I'2 '9	· I · · · · · · · · · · · · · · · · · ·	 	 3·3 2·1 2·0 		 2·2 ·2 I·3 	 2·6 1·2 		 	3·1 8·2 2·3 6·8 II·4 II·6 I6·9 (0·3) I4·2 0·9 5·8 0·4 7·3 I2·2 0·8 I0·5 7·6	4·6 8·9 3·4 8·6 6·6 9·1 10·3 0·8 8·2 2·7 5·2 0·9 7·2 6·7 1·9 8·6 8·4
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27			2.4	 2·4 2·0 4·I 			.85 2.57 .3 .1 .2	.5 '4 .1 1.8 	 	·2 ··· ·· ·9 ·4 ··· I·7 ··· I·9 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	 	·4 ·4 ·4 · · · · · · · · ·	·1 · ·6 · ·2 · ·9 · · · · · · · ·	 I·0 ·2 ·5	··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	·4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	· I ··· ·· · I ··· · 7 5· 0 ··· ··· ··· ··· ··· ··· ··· ··· 2· 0 ···	 	3·3 2·1 · · · · · · · · ·		2·2	2.6 1.2			3·1 8·2 2·3 6·8 II·4 II·6 I6·9 (0·3) I4·2 ··· 0·9 5·8 0·4 7·3 12·2 0·8 10·5 5·3 5·3 5·3 24·1 24·3	4·6 8·9 3·4 8·6 6·6 9·1 10·3 0·8 8·2 2·7 5·2 0·9 7·2 6·7 1·9 8·6 8·4 9·2 4·3 4·2 8·2 14·6
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26				 2·4 ·I 			·8 ·5 2·5 ·7 ·3 3·1 2·8	.5 '4 .1 	·5 ·2 2·2 2·3	.29 .4 1.7 1.9			·1 · ·6 · ·3 · ·2 · ·9 · · · · · · · ·	I.0		·4 ·4 I·2 ·9	· I ··· ·· · I ··· · 75·0 ··· ··· ··· ··· ··· ··· ··· ··· 2·0 ··· ···		.5 3·3 2·1 2·0 1·4 1·2 1·8		2·2	2.6 1.2			3·1 ··· 8·2 2·3 6·8 II··6 I6··9 (0·3) I4·2 ··· 0·9 5·8 0·4 7·3 I2·2 0·8 I0·5 7·6 I2·3 5·3 5·3 24·1 24·1 24·1	4·6 8·9 3·4 8·6 6·6 9·1 10·3 0·8 8·2 2·7 5·2 0·9 7·2 6·7 1·9 8·6 8·4 9·2 4·3 4·2 8·2 10·0 11·0 10·0 10·0 10·0 10·0 10·0 10
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29				2.4			·8 ·5 2·5 ·73 ·1 ·2 3·1 2·8 1·2	.5 '4 .1 	.5 .2 	.29 .4 I.7 I.9			·1 · ·6 · ·3 · ·2 · ·9 · · · · · · · ·	I · O		·4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	· I ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·		3·3 2·1 · · · · · · · · ·			2.6 1.2			3·1 ··· 8·2 2·3 6·8 II··6 I6·9 (0·3) I4·2 ··· 0·9 5·8 0·4 7·3 I2·2 0·8 I0·5 7·6 I2·3 5·3 24·1 24·3 9·2 9·3 9·3	4·6 8·9 3·4 8·6 6·6 9·1 10·3 0·8 8·2 2·7 5·2 0·9 7·2 6·7 1·9 8·6 8·4 9·2 4·3 4·2 8·2 10·0 11·0 10·0 10·0 10·0 10·0 10·0 10
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30				2.4			.85 2.573 .1 .2 3.1	.5 '4 .1 	.5 .2 	.29 .4 I.7 I.9			·1 ·6 ·3 ·9	1.0 2		·4 ·4 I·2 ·9	· I ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·		.5 3·3 2·1 2·0 1·4 1·2 5 1·8 			2.6 1.2			3·1 ··· 8·2 2·3 6·8 II··4 II··6 I6··9 (0·3) I4·2 ··· 0·9 5·8 0·4 7·3 I2·2 0·8 I0·5 7·6 I2·3 5·3 24·1 24·3 9·9 23·8 I7·2 0·1	4·6 8·9 3·4 8·6 6·6 9·1 10·3 0·8 8·2 2·7 5·2 0·9 7·2 6·7 1·9 8·6 8·4 9·2 4·3 4·2 14·6 10·0 15·4 11·0
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Sums Total Dura-				2.4			.85 2.57 .3 .1 .256 I.4 2.8 I.2 3.0 IT.9	.5 '4 	·5 ·2 ·2.2 2·2	.29 .4 I.7 I.9			·1 ·6 ·3 ·2 ·9	I.0		·4 ·4 I·2 ·9	· I ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·		3·3 2·1		2·2	2.6 1.2			3·1 ··· 8·2 2·3 6·8 II··4 II··6 I6··9 (0·3) I4·2 ··· 0·9 5·8 0·4 7·3 I2·2 0·8 I0·5 7·6 I2·3 5·3 24·1 24·3 9·9 23·8 I7·2 0·1	4.6 8.9 3.4 8.6 6.6 9.1 10.3 0.8 8.2 2.7 5.2 0.9 7.2 6.7 1.9 8.6 8.4 9.2 4.3 4.2 8.2 14.6 10.0 15.4 11.0 0.1
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Sums Total				2.4			.8577 .3 .1 .2556 .1.4		.52	.2			·1 ·6 ·3 ·2 ·9	1.0 2			· I ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·		.5 3·3 2·1 2·0 1·4 1·2 		2·2 2·2	2.6 1.2			3·1 8·2 2·3 6·8 II·4 II·6 I6·9 (0·3) I4·2 0·9 5·8 0·4 7·3 I2·2 0·8 I0·5 7·6 I2·3 5·0 5·3 24·1 243·3 hr. I82·9	4·6 8·9 3·4 8·6 6·6 9·1 10·3 0·8 8·2 2·7 5·2 0·9 7·2 6·7 1·9 8·6 8·4 9·2 4·3 4·2 14·6 10·0 15·4 11·0 0·1

Amounts in millimetres, for periods of sixty minutes, between the exact hours, Greenwich Mean Time.

167. Eskdalemuir: H_r (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + h_r (height of receiving surface above ground) = 242·0 metres + 0·4 metres. November, 1923.

Day.	0-1	1-2	2-3	3-4	4-5	5-6	6-7	7-8	8-9	9–10	10-11	11-12	12-13	13-14	14-15	15-16	16–17	17–18	18-19	19–20	20-21	21-22	22-23	23-24	0-24	
1 2 3 4 5	mm 2·0 ·2	mm 2·4 ·2	mm 2·0 ·4	mm 2.4 2.6	mm 2 · I I · I	mm 2.8	mm 1.8 1.5	mm. 4.6 I.2	mm 2.0	mm4	mm2	mm1 .8	mm 1·1 2·7	mm. '4 '2	mm.	mm6 .7	mm. .9	mm3 .2	mm 1.7 2.8	mm. '3 '1 '2	mm	mm. 1·7 1·8 ·4	mm. 1·9 ·2 ···	mm. 1 · 8 · 1 ·	mm. 0·8 6·5 28·6 16·7 	1·0 5·0 15·7 10·8
6 7 8 9 10					 I.o	3.8	 2·2 		···	··· ·· ·1 ·4 ···		 .8 .3		 ·2 ·3						· · · · · · · · · · · · · · · · · · ·					8·8 1·6 0·2	5·3 4·3 0·2
11 12 13 14 15	··· ·2 ·1 ·1 ·1	 1·8 ·7	3.2	 •I 2•2 	2 · 2	 1.3 	· I · 8 2· 4 · · ·	1·2 2·7 	1.0 1.2 .1	 ·2 1·5 1·3	 1·1 1·0 ·5	2·3 1·6 2·0	 1·5 ·4 3·7	··· ··9 ··· 4·4	··· ··6 ··· 2··6	· I · · 8 · · · · 2	·6 1·0 	·4 2·6 	· 5 1 · 5 	·3 1·8 	1·6 	1·4 	1·5 ·4 	·6 ·1 ·1	4.5 3.7 36.2 5.3 14.0	6·7 6·7 22·5 5·7 7·7
16 17 18 19 20	·4 ·9 	 1·6 	··· ·4 ··· ···		··· ·4 ···	 .3 	 1·6 ·6 	 .6 	 5 				··· ··· ··· ·4				 I.0	 1·3 	1·2 	··6 ···	1·7 ·4 ···	3.3	2.8		8·2 7·9 5·1 1·9	3·1 7·3 4·2 (3·0)
21 22 23 24 25	···				··· ··· ···							··· ·4 ··· ···		 .5	··· ··· ··· ··5										0·1 0·7 1·1	0·4 1·2 2·5
26 27 28 29 30	·2 	·2 		·4 		· · · · · · · · · · · · · · · · · · ·		· 1						· · · · · · · · · · · · · · · · · · ·											1·8 0·3 0·3 2·8	5·4 (1·8) (1·6) (5·0)
Sum. Total Dura-	4·4 hr. 5·2	6·9 hr. 5·9	6·2 hr. 4·4	8·2 hr. 5·1	7·5 hr. 4·6	8·5 hr. 5·4	hr. 5·8	11·6 hr. 6·0	5.4 hr. 5.7	4·I hr. 5·8	3·3 hr. 5·2	8·7 hr. 7·6	10·3 hr. 6·7	7·0 hr. 5·7	4·4 hr. 4·1	2·4 hr. 3·1	3·5 hr. 3·5	5·3 hr. 3·9	7·7 hr. 4·8	3·6 hr. 6·0	5·6 hr. 5·2	9·2 hr. 6·2	7·7 hr. 4·9	4·6 hr. 6·3	157·1 hr. 127·1	<u> </u>
168.	Esk	daler	nuir	Hr:	= 242	2·0 m	etres	+0	4 me	tres.		<u> </u>								-,			Dec	embe	or, 19	23,
ı	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm. 6·3	hr. 13.0
2 3 4		·6 	1·6 	3.4	1.5		 			·3 ·6 ·2		 .6 .4	 5	 .8 .2	 I·I		··· ·8 ·4	·2 ·6 ·5	· · · · · · · · · · · · · · · · · · ·						8·4 6·3 2·2	6·1 10·2 4·6
5 6 7 8 9	 	 1.6		 1·6 	 1·8 	···	 •1 •6 				·I				 1·6 	 1·6 	 I·2 	 1·7 	 1·4 	···	 I·4 	 .7 .6	 2·I ·8 ·3	 I·I ·5 ·2	 13·8 5·5 1·9	 10·4 (5·2) 2·7 11·9
11 12 13 14	'4 '4 2'4 	'4 '5 '3 	 '4 1·8	 3 3·1 	·2 ·5 ·2 ···	·2 ·2 ·2 ·	·1 ·5 ·1 ···		 •9 	·1 ·5 ···	 .3 .2	·2 ·3 I·4	·1 ·6 ·6 ··	··· ·4 ··· ·8	·1 ·7 ·6 ···	 I·I 	 .7 1.3	·1 ·8 · ·5	·4 ·7 ···	 	1·6 	 1·3 	.7 1·5 	1·0 1·5 	4·4 16·7 8·1 6·6 o·2	10·8 24·0 6·5 8·0 0·8
16 17 18 19 20	 ·2 	(.1) 	··· ·1 ·2 ··· (···)	···			··· ·1 ·4 ···	· I · I · 2 · · ·							····	1·5 	1·7 	 •8 	··· ··7 ···	····					0·1 6·3 1·4 	0·4 8·3 2·1
21 22 23 24 25	 I·3 	 1.0	 I·2 	·8 ···	 	 .3 		···	(·1)· ·4 ··· ·4 ···	() • I ···				1.0 	·2 2·5	·5 ·4 1·8	·6 ·9	·1 		·7 1·3	·2 1·6	·5 ··· ··· ··9	·8 ·2	1.0	4·8 5·3 o·9	7·9 6·5 1·5 9·3
26 27 28 29 30	 :3 1.8	··· ··2 ··· ···	 ·2 ·I	··· ··· ··3			 	 	 I·2		 		 	 .4				 1.6	 ·2 ·5 I·2	 •1 1•4 •6	··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	·4 ·5	 I.I 	·2 ·9	1·3 1·3 5·6	2·9 (6·2) 6·0 19·0
31											8	1.7	2.4	.9	1.0	• 5	•4	.3	1.1	· 1	.1	•••			9.3	10.8
Sum.	8.7	6·2 hr.		11.0	4.9	2.4	2.7	1.4	3.6	3.5	2.3	5.3	5.0	5.2	8.8	9.5	8.0	10.0	8.4	7.0	6.7	5.2	8.4		148.8	195 • 1
Total			hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	1

DURATION OF BRIGHT SUNSHINE. For periods of sixty minutes, between the exact hours of Local Apparent Time.

Eskdalemuir: h_s (height of recorder above ground) = $1 \cdot 5$ metres. 169.

January, 1923.

		<u> </u>		1					abov										Total	Per cent.		Radiati	ion by	10+0=
Day.	3 to	4 to	5 to 6.	6 to	7 to 8.	8 to 9.	9 to	10 to		Noon to 13.		14 tc 15.	15 to 16.	16 to 17.	17 to 18.	18 to 19.	19 to 20.	20 to 21.	for Day.	of Possible	Time.	Inten-	Theliom	1
	· ·																				G.M.T.	sity.	$\frac{p/p_0}{\sec Z}$.	J. Sky.
I	hr.	hr.	hr.	hr.	hr.	hr. •1	hr. 1·0	hr.	hr.	hr. 1·0	hr. •1	hr. 	hr.	hr. 	hr.	hr. —	hr.	hr.	hr. 4°2	% 59	12 16	mw/cm² 56	4.87	Ci.∙St.
3	_	_	_	_	_				 '4			•••			_	_	_	_	 o∙6	 8				
4 5	_	=	_	_	_	·3	1.0	I.0	1.0	·9	·5 	·6		_	_	_	_	_	5.3	74 				
6	_	_	_		_	•4	•2	.3	.3		٠1					!		_	1.3	18				
7 8	_	_	_	_	_			I.0	1.0	 .9	I.0	···	•••	_		_	_	_	 4·6	 63				
9	_	_	_	_	_			·2 ·8	1.0 .1	·				_	_	_	_	_	0·3	4 27				
111	_	_			_	•2	.6	1.0	1.0	.3	1.0	-8			_		_	_	4.9	66				
12	_	_	_	_	_					1.0	I.0	 I.O		_	_	_	_	_	4·3	58 				
13	_	_	_	_	_		·7 ·6	·9	1.0	1.0	1.0	.7 .2		_	_	_	_	_	1.0 2.3	70 13			•••	
15					_										_	_								
16	_	-		_	_	•••	I.O	1.0	I.0			···		_		=	_	_	 6·1	 79				
18	_	=		_	_	·4 ·6	···	1.0	1.0	I.O		 •9	·	_	_	=	_	_	 6∙6	 84				
20		_										٠1		_	_	_	_		0.1	1				
21	_	=	_	=	_		٠.1	•5	•2	···				_	_	_	_	_	o·8 o·3	10 4		•••		
23 24	_	_	_		-			·1			·	.5	•••		_	_	_	_	0.3	4 5				
25	_	-		-	•••	•••				.3		•••				_	_	_						
26 27	_	_	_	=								•••	•••		_	_	_	_						
28 29	_	=	=													_	_							
30			_	-	•••	•••	•••		• • • •			•••	•••	•••			· .							
31																			48.4					-
Sum.						2.0	6.6	9.3	9.9	8.0	6.8	5.6	0.2						1.56	<u> </u>				
Mean.			ł .							•26	.22	.18	.01	• • •					1 200	20	1	1		!
1,100,11.				_		•06	.31	.30	.32							<u> </u>			<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>
170.	Esk	dalen	nuir :	h _s =	= 1.5			-30	355												<u> </u>	Febru	ary, 1	923.
170.	hr.	hr.	nuir :	hr.	= 1 · 5	met	res.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr	/ / / / / /	h. m.	Febru		923.
170.					= 1 · 5	hr.	hr.	hr. 	hr. 	hr	hr. .5	hr. 	hr. 	hr. 		1	hr.	}	hr 0·9 2·0	% 10	1	mw/cm²		Ī
170.	hr. —	hr. 	hr. —	hr. 	= 1 · 5	hr 1.0	hr	hr2	hr2	hr	hr. .5 	hr2 -9 I.0	hr. .9	hr.		_		-	hr 0·9 2·0 7·9	/ % 		mw/cm³	· · · ·	
170.	hr. —	hr. 	hr.	hr.	= 1·5	hr 1.00	hr	hr ·2 1·0	hr2 1.0	hr	hr59	hr2 .9 I.0	hr. .9	hr			- - -	-	hr 0.9 2.0 7.9	% 10 23 90		mw/cm³		
170.	hr. —	hr. 	hr. —	hr.	= 1·5	hr	res. hr '5 I'0	hr2 I.0	hr2 I.0	hr2 .2 I.0	hr '5 '9	hr2 .9 I.0	hr9	hr				-	hr 0·9 2·0 7·9	% 10 23 90		mw/cm²		
170.	hr. — — —	hr. 	hr.	hr.	= 1·5	hr	res. hr	hr2 I.0	hr 2 1.0	hr2 .2 I.0 4	hr59	hr2 .9 I.0	hr	hr					hr o·9 2·0 7·9 2·6	% 10 23 90 		mw/cm³		
170. 1 2 3 4 5 6 7 8	hr. — — — —	hr.	hr.	hr.	= 1·5	hr	res. hr '5 I'0	hr 1.0	hr 2 1.0	hr2 .2 .1.0	hr '5 '9	hr	hr9	hr.					hr 0.9 2.0 7.9 2.6	% 10 23 90 29				
170. 1 2 3 4 5 6 7 8 9	hr. — — — — — — — — — — — — — — — — — — —	hr.	hr.	hr.	= 1·5	hr i.o	hr	hr2 I.0	hr 2 1.0	hr2 .2 I.0	hr59	hr2 .9 I.0	hr9	hr					hr 0.9 2.0 7.9 2.6 0.1	% 10 23 90 29		mw/cm³		
170. 1 2 3 4 5 6 7 8 9 10 11	hr	hr.	hr. —	hr. —	= 1.5	hr i.o	res. hr '5 1.0	hr2 1.0	hr 2 1 0	hr2 .2 1.0	hr59 I.0	hr2 .9 I.0	hr94						hr 0·9 2·0 7·9 2·6	% 10 23 90 29		mw/cm³		
170. 1 2 3 4 5 5 6 7 8 9 10 11 12 13	hr	hr. —	hr.	hr.	= 1·5	hr	res. hr	hr	hr2 I.0	hr2 .2 I.0	hr '5 '9 I'0 I'0	hr '2 '9 I '0	hr	hr					hr 0.9 2.0 7.9 2.6 1.8	% 10 23 90 29 1 19		mw/cm³		
170. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16	hr	hr. —	hr.	hr.	= 1 · 5	hr	res. hr '5 1.0	hr2 1.0	hr 2 1 0	hr2 .2 1.0	hr59 I.0	hr2 .9 I.0	hr94	hr					hr 0.9 2.0 7.9 2.6 1.8	% 10 23 90 29 1 19 4		mw/cm³		
170. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	hr.	hr.	hr.	hr.	= 1·5	5 met hr 1.0	res. hr	hr	hr	hr	hr	hr	hr	hr					hr 0.9 2.0 7.9 2.6 0.1 1.8	% 10 23 90 29 1 19 4 15		mw/cm³		
170. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16	hr	hr.	hr.	hr.	= 1 · 5	5 met hr		hr	hr	hr	hr	hr	hr	hr					hr 0.9 2.0 7.9 2.6 0.1 1.8 0.4 1.5 3.4	% 10 23 90 29 1 19 4 15 34		mw/cm³		
170. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	hr.	hr.	hr.	hr.	= 1·5	5 met hr I·o		hr	hr	hr	hr	hr	hr	hr					hr 0.9 2.0 7.9 2.6 0.1 1.8	% 10 23 90 23 90 29 1 19 4 15 34 18		mw/cm³		
170. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	hr.	hr	hr.	hr.	= 1·5	5 met hr I · o	res. hr	hr	hr	hr	hr '5 .	hr	hr	hr					hr 0.9 2.0 7.9 2.6 0.1 1.8 0.4 1.8 6.0	% 10 23 90 23 90 10 23 90 10 29 11 19 4 15 34 18 59				
170. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	hr.	hr	hr.	hr.	= 1.5	5 met hr	res. hr	hr	hr	hr	hr	hr	hr	hr					hr 0.9 2.0 7.9 2.6 0.1 1.8 0.4 1.5 3.4 1.8 6.0	% 10 23 90 23 90 10 23 90 11 15 34 18 59 18 59		mw/cm³		
170. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	hr.	hr	hr.	hr.	= 1·5	5 met hr	res. hr	hr	hr	hr	hr	hr	hr	hr					hr 0.9 2.0 7.9 2.6 0.1 1.8 0.4 1.8 6.0	% 10 23 90 23 90 11 19 4 15 34 18 59 18 59 3				
170. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	hr.	hr	hr.	hr.	= 1.5	5 met hr		hr	hr	hr	hr	hr	hr	hr					hr 0.9 2.0 7.9 2.6 0.1 1.8 0.4 1.5 3.4 1.8 6.0	% 10 23 90 23 90 15 34 18 59 18		mw/cm³		
170. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	hr.	hr	hr.	hr.	= 1·5	5 met hr		hr	hr	hr	hr	hr	hr	hr					hr 0.9 2.0 7.9 2.6 0.1 1.8 0.4 1.5 3.4 1.8 6.0 0.3 28.7	% 10 23 90 23 90 11 19 4 15 34 18 59 18 59 3				
170. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	hr.	hr	hr.	hr.	= 1.5	5 met hr		hr	hr	hr	hr	hr	hr	hr					hr 0.9 2.0 7.9 2.6 0.1 1.8 0.4 1.5 3.4 1.8 6.0	% 10 23 90 23 90 15 34 18 59 18		mw/cm³		
170. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 Sum.	hr.	hr	hr.	hr.	= 1·5	5 met hr		hr	hr	hr	hr	hr	hr	hr					hr o.9 2.0 7.9 2.6 1.8 o.4 1.5 3.4 1.8 6.0	% 10 23 90 29 11 11 11 11 11 10 11 11 11 11 10 11 11 11 11 11 10 11 11 11 11 10 11 11 11 10 11 11 11 10 11 11 10 11 11 11 11 11 10 11 11 11 10 11		mw/cm³ .		
170. 1 2 3 4 4 5 5 6 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 Sum.	hr.	hr	hr.	hr.	= 1·5	5 met hr		hr	hr	hr	hr	hr	hr	hr					hr o.9 2.0 7.9	% 10 23 90 23 90 11 19 4 15 34 18 59 18 59 3		mw/cm³		

DURATION OF BRIGHT SUNSHINE.

For periods of sixty minutes, between the exact hours of Local Apparent Time.

171.	Eskdalemuir	: h.	(height o	of recorder	above ground)	= 1	·5 metres.
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March, 1923.

				Ī	Ī	1)]	Radiati	on by	
Day.	3 to 4.	4 to 5.	5 to 6.	6 to 7.	7 to 8.	8 to 9.	9 to	no to	II to Noon		13 to 14.	14 to 15.	15 to 16.	16 to 17.	17 to 18.	18 to 19.	19 to 20.	20 to 21.	for	Per cent. of Possible.	Time	Inten-		Sky.
	hr.	hr.	hr.	hr.	hr.	 hr.	hr.	hr.	 hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	%	G.M.T.	sity.	sec. Z.	
1	_	_	_														-				•••	•••		
3	=							:::								_		_	o·6	6				
4 5	_								-8	·5	·8 ·6	···				_	_	_	2·9 1·0	² 7				
6	_		_									i												
7 8	—		-				•2	•2		٠٠.			•••			_ '		_	0·5	 5				
9	=	_					•2			···	·2 ·4					_			0.5	2 11			•••	
10	-	-	-													_	-						•••	
11	_	_	_													_	_	_						
13	_	_				1.0	1.0	1.0	.7	.9	•5	.5	·5 ·2	.2		_		-	5·8 3·8	50			•••	
15	-	_	-													_	=	=		33				
16	_	-	-				·ī	.2	.5	.8	•4	1.0	1.0	.5			—	_	4.5	38				
17		_	_			3.3	1.0	1.0	1.0	1·0	1.0	I.O I.O	1.0	·5 ·7		_		_	6·0 8·9	51 75				
19 20	_	_	_					·5	·9 ·7	.3 .3	I.0 .8	·7	·2 I·0	·5		_	_		5.5	46 42		•••	•••	
									}				ļ											
21 22	_	_				1.0	1.0	1.0	I.0 I.0	I.O	I.0 I.0	1.0	I.O I.O	·7		:::	_	_	9.6	53 79	12 8	78	1.72	Slight
23	_	_		.4	1.0	.9	1.0	1.0	1.0	1.0	1.0	1.0	1.0	-8			_		10.1	82				haze.
24 25	_	_				1.0			.I I.O	.3 1.0	1·0 ·5	1.0	1.0	·I I·O			_	_	7.0	57 27	12 6	71	1.71	haze.
26					ì	1.0	1.0	1.0		.8									1					
27 28	_						.2	.2		•2	.6	·5						=	7·0	56 14				
29 .	=						1.0	1.0	1.0	I.O		•6							6.9	 54	12 15	76	1.63	Clear.
30	-	-				8.	.2	.3	.2	·ı	.6	.8	.7						3.9	30		•••	•••	
31	_		.1	.3	<u> </u>	.7	.1	<u> </u>			•••		•••						1 · 2	9				
Sum.			0.1	0.9	2.8	9.3	11.2	11.0	11.6	11.5	13.8	13.0	10.3	7.0	0.7				103.5					
												1												
Mean.	<u> </u>	<u> </u>	.00	.03	.00	.30	•36	•35	37	·37	·45	•42	.33	•23	.02	<u> </u>	<u> </u>		3.33	28	<u> </u>	<u> </u>		<u></u>
Mean.	Esk	dalen	<u></u>	<u></u>		o ·30 5 met		•35	37	•37	·45	•42	.33	.23	·02	<u> </u>	<u> </u>		3.33	28	<u> </u>	A	 pril, 1!	923.
172.	Esk	dalen	nuir :	hs =	= 1 · :	5 met	res.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	%	h. m.	mw/cm ²	1	
172.			hr.	hs =	hr.	5 met	res.	hr.	hr. 	hr	hr. 	hr. 	hr. 	hr. 		hr. 	hr. 		hr	% 	h. m.	mw/cm²		
172.	hr.	hr.	huir :	hs =	= 1 · 8	5 met	res. hr i.o	hr.	hr6	hr	hr. 	hr. 	hr.	hr.	hr.	hr. 	hr.	hr.	hr. 	/ / / //	h. m.	mw/cm²		
172. 1 2 3 4 5	hr. — —	hr.	hr.	hs =	hr.	5 met	res.	hr	hr	hr	hr. .7	hr. 	hr. 	hr. .2	hr .	hr.	hr. 	hr.	hr 5·6	% 43	h. m.	mw/cm²		
172.	hr. — —	hr.	nuir :	hs =	= 1 · !	5 met	res. hr. i.o ·i ·3	hr 1.0 4	hr	hr	hr	hr	hr '3	hr2	hr .	hr.	hr.	hr.	hr 5.6 0.1 2.0	% 43 1 15	h. m.	mw/cm²		
172. 1 2 3 4 5 6 7 8	hr. —	hr.	nuir :	hs =	hr	5 met	res. hr 1.0 ·1 ·3 ·9	hr 1·0 48	hr69	hr643 I.0	hr	hr7 1.0	hr3 4 I.0	hr22 1:0	hr	hr	hr	hr.	hr 5.6 0.1 2.0 1.3 9.4	% 43 1 15 10 70	h. m.	mw/cm²		
172.	hr. 	hr.	nuir :	hs =	= 1 · 8	5 met	res. hr i.o 3	hr I·o '4	hr	hr	hr	hr7	hr3	hr2	hr .	hr	hr	hr.	hr 5.6 0.1 2.0 1.3	% 43 1 15	h. m.	mw/cm²		
172. 1 2 3 4 5 5 6 7 8 9 10 11	hr.	hr.	nuir :	hs =	hr	5 met	res. hr. i.o '1 '3 '9 '1	hr I · o '48	hr69 1.0	hr643 I.o .4	hr	hr	hr34 I.0	hr222	hr	hr.	hr.	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9	% 43 1 15 10 70 21	h. m.	mw/cm²		
172. 1 2 3 4 5 6 7 8 9 10	hr.	hr.	hr	hr	hr	5 met	res. hr. i.o '1 '3 '9 '1 '3	hr i.o '48 '4	hr69 1.0 2	hr	hr	hr7	hr34 I.0 .5 .1	hr22 I.0 .4	hr	hr	hr.	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9	% 43 I 15 10 70 21 12	h. m.	mw/cm²		
172. 1 2 3 4 5 6 7 8 9 10 11 12 13 14	hr. —	hr.	nuir :	hs =	= 1 · ! hr	5 met	res. hr. 1.0 .1 .3 .	hr i.o 48 4 .8	hr69 1.0 2 1.0 6	hr	hr	hr	hr34 I.0 .5 .1 .5 .1	hr22 I.0 .472 I	hr	hr	hr.	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6	% 43 I 15 10 70 21 12 39	h. m	mw/cm²		
172. 1 2 3 4 5 5 6 6 7 8 9 10 11 12 13 14 15	hr.	hr.	nuir:	hr	= 1 · !	5 met hr.	res. hr 1.0 '11 '3 '9 '11 '3 '2 1.0 I1.0	hr I · o '4 '4 '8 I · o	hr69 1.0 2 1.067	hr	hr	hr72 I.0 .7 .1111	hr3	hr22 I · 0 .4777	hr	hr.	hr.	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5	% 43 1 15 10 70 21 12 39 14 48	h. m	mw/cm²		
172. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	hr.	hr.	nuir:	: hs = hr	= 1 · { hr	5 met hr.	res. hr 1 · 0 · 1 · 3 9 · 1 · 3 · 2 1 · 0 1 · 0	hr i.o 444 .8 i.o	hr69 1.067 .2	hr	hr	hr	hr	hr	hr	hr.	hr	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5	% 43 1 15 10 70 21 12 39 14 4 68 25 67	h. m	mw/cm²	 	
172. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	hr	hr.	nuir:	: hs = hr	= 1 · { hr.	5 met hr.	res. hr. i · o · i · 3 · · · · · · · · · · · · · · · · · · ·	hr i.o '48 '4 .8 i.o i.o	hr69 1.02 1.067	hr	hr	hr	hr	hr	hr	hr	hr.	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5 3.5 9.5	% 43 1 15 10 70 21 12 39 14 4 68 25 67 6	h. m	mw/cm²		
172. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	hr.	hr.	nuir:	: hs = hr	= 1 · { hr.	5 met hr.	res. hr. 1.0	hr i.o 44 .8 i.o i.o	hr69 1.067 .2 1.07	hr	hr	hr	hr	hr	hr	hr.	hr.	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5 3.5 9.5 0.9 6.6	% 43 1 15 10 70 21 12 39 14 4 68 25 67	h. m	mw/cm²		
172. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	hr	hr	nuir:	: hs = hr	= 1 · { hr.	5 met hr.	res. hr 1 · 0 · 1 · 3 · 9 · 1 · 3 1 · 0 1 · 0 1 · 0 1 · 0	hr i.o '48 '4 .8 i.o i.o	hr	hr	hr	hr	hr	hr	hr	hr	hr	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5 3.5 9.5 0.9 6.6	% 43 1 15 10 70 21 12 39 14 4 68 25 67 6 46 30	h. m	mw/cm²		
172. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	hr.	hr	nuir:	: hs = hr	= 1 · { hr. i · o	5 met hr.	res. hr 1:0 '1 '3 '9 '1 '3 1:0 1:0 1:0 1:0 1:0 1:0	hr 1·0 4 8 4 .8 1·0 1·0 1·0 1·0 1·0	hr	hr	hr	hr	hr	hr	hr	hr	hr.	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5 3.5 9.5 0.9 6.6	%	h. m	mw/cm²		
172. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	hr.	hr	nuir:	: hs = hr	= 1 · { hr.	5 met hr.	res. hr 1.0 .1 .39 .1 .3 .2 1.0 1.0 1.0 1.0 2 .9	hr	hr	hr	hr	hr	hr	hr	hr	hr	hr	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5 3.5 9.5 0.9 6.6	%	h. m	mw/cm²		
172. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	hr.	hr	nuir:	: hs = hr	= 1 · \(\) hr	5 met hr	res. hr 1.0 .1 .0 .1 .39 .1 .31.0 1.0 1.0 1.0 1.0 1.0 1.0	hr 1.0484 .81.01.0	hr	hr	hr	hr	hr	hr	hr	hr	hr	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5 3.5 9.5 0.9 6.6 4.3 5.9 2.4 10.9 7.4	% 43 1 15 10 70 21 12 39 14 4 68 25 67 6 46 30 41 16 74 50 44	h. m	mw/cm²		
172. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	hr.	hr	nuir:	: hs = hr	= 1 · (hr	5 met hr	res. hr 1:0 '1 '3 '9 '1 '3 '2 1:0 1:0 1:0 1:0 1:0 1:0	hr	hr	hr	hr	hr	hr	hr	hr	hr	hr.	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5 3.5 9.5 0.9 6.6 4.3 5.9 10.9 7.4 6.5 8.6 5.0	%	h. m	mw/cm²		
172. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	hr.	hr	nuir:	: hs = hr	= 1 · \(\) hr	5 met hr	res. hr 1.0 .1 .0 .1 .39 .1 .3 1.0 1.0 1.0 1.0 1.0 1.0	hr 1·0 4 4 .8 1·0 1·0 1·0 1·0	hr	hr	hr	hr	hr	hr	hr	hr	hr	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5 3.5 9.5 0.9 6.6 4.3 5.9 2.4 10.9 7.4 6.5	%	h. m	mw/cm²		
172. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	hr.	hr.	nuir:	: hs = hr	= 1 · \(\) hr	5 met hr.	res. hr 1.0 .1 .0 .1 .39 .1 .3 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	hr 1.0 4 8 1.0	hr	hr	hr	hr	hr	hr	hr	hr	hr	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5 3.55 9.5 0.9 6.6 4.3 5.9 2.4 10.9 7.4 6.5 8.6 5.0 7.2	%	h. m	mw/cm²		
172. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	hr.	hr.	nuir:	: hs = hr	= 1 · (hr	5 met hr.	res. hr 1.0 .1 .39 .1 .3 .2 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	hr	hr	hr	hr	hr	hr	hr	hr	hr	hr	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5 3.5 9.5 0.9 6.6 4.3 5.9 2.4 10.9 7.4 6.5 8.6 5.0 7.2 119.0	% 43 1 15 10 70 21 12 39 4 68 25 67 6 46 30 41 16 74 50 44 58 33 48 ————————————————————————————————	h. m	mw/cm² .		
172. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum.	hr.	hr.	nuir:	: hs = hr	1 · · · hr.	5 met hr.	res. hr 1.0	hr 1.0 4 8 1.0	hr	hr	hr	hr	hr	hr	hr	hr	hr	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5 3.5 9.5 0.9 6.6 4.3 5.9 2.4 10.9 7.4 6.5 8.6 5.0 7.2 119.0	% 43 1 15 10 70 21 12 39 4 68 25 67 6 46 30 41 16 74 50 44 58 33 48 —	h. m	mw/cm² .		
172. 1 2 3 4 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum. Mean.	hr	hr	nuir: hr.	: hs = hr. hr.	1 · · · · · · · · · · · · · · · · · ·	5 met hr.	res. hr. 1.0	hr	hr	hr	hr	hr	hr	hr	hr	hr	hr	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5 3.5 9.5 0.9 6.6 4.3 5.9 2.4 10.9 7.4 6.5 8.6 5.0 7.2 119.0 3.97	% 43 1 15 10 70 21 12 39 44 68 25 67 6 46 30 41 16 74 50 44 58 33 48 — 28 Per cent.	h. m	mw/cm² .		
172. 1 2 3 4 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum. Mean.	hr.	hr.	nuir:	: hs = hr. hr. hr. hr.	= 1 · · · · · · · · · · · · · · · · · ·	5 met hr.	res. hr 1.0 .1 .0 .1 .39 .1 .3 1.0	hr	hr	hr	hr	hr	hr	hr	hr	hr	hr	hr.	hr 5.6 0.1 2.0 1.3 9.4 2.9 1.7 5.3 1.9 0.6 9.5 3.5 9.5 0.9 6.6 4.3 5.9 2.4 10.9 7.4 6.5 8.6 5.0 7.2 119.0 3.97 Total for	% 43 1 15 10 70 21 12 39 4 68 25 67 6 46 30 41 16 74 50 44 58 33 48 —	h. m	mw/cm² .		

DURATION OF BRIGHT SUNSHINE.

For periods of sixty minutes, between the exact hours of Local Apparent Time.

173.	Eskdalemuir :	hs	(height o	f recorder	above	ground)	=1.5	metres.

May, 1923.

173.	ESK	IZIOIII	uir :	ns (I	neign	I OI I	record	ier a	bove	grou	na) =	= 1.9	met	res.									May, 1	320.
Day.	3 to	4 to 5.	5 to 6.	6 to	7 to 8.	8 to 9.	9 to 10.	10 to	11 to Noon	Noon to 13.	13 to 14.	14 to 15.	15 to 16.	16 to 17.	17 to 18.	18 to 19.	19 to 20.	20 to 21.	Total for Day.	Per cent. of Possible.	Ångst Time G.M.T.	Radiat röm Py Inten- sity.	rheliom	Sky.
<u>-</u>	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	%	h. m.	mw/cm³	1	1
1			.3	.9	•5	·1	.3		.2		•5		⋅8	·3 ·6	.2	.1		_	4.2	28				•••
2					·4 ·6	1.0	1.0	1.0	1.0	·4 ·5	·6 ·9		1.0	1.0	.9			_	4·8 9·8	32 64				
3 4	l							.4	.3		.2								0.9	6				•••
5	-		•••					.9	1.0	•6	•4	•••	.7	1.0	⋅8		•••		5.4	35			•••	•••
6			.1		·4				-6			·ı	.1						1.3	8				•••
7 8				1.0	1.0	1.0	.I I.O	1.0	1.0	1.0	·9 ·5	·9 ·8	·8	.7	1.0	•6			7.5	69 48				•••
9	_				:::	1		.5	1 .4	1 .4	.3	.6	•4	.5					3.1	20				•••
10	-	.3	.9	1.0	1.0	1.0	1.0	.9				•••					•••		6·1	39			•••	•••
11	-				.5	.3	.4		.1		٠ı								1.4	9				
12	_	.1	∙8	1.0	.I		.I I.O	1.0	.6	·3 ·8	·3 ·5	·9 ·5	1.0	1.0	·5			_	10·1	64 26				•••
14	_	·1					·1		•6	•5	·5 ·8	∙6	.1			•••		_	2.5	16		•••		•••
15	<u> </u>	•••			.4		.3	.9	.6	•2	-8	1.0	1.0	.7	.7	.I	•••		6.7	42		•••		•••
16				.3		.2		.2	.5	1.0	٠1	.3	.7	•2					3·5 6·8	22				
17		.9	1.0	•5	.6	·	·1	·	•2	•6	1.0	•2	.9						0.8	42 8				
19	:::																							
20											•••	•••				•••	• • • •	•••	•••	•••			•••	•••
21	 				.2	.2	.2	.7	.3	.1		•6	1.0	1.0	∙6	.2			5.1	31.				
22				8.	.9	.9	7	•5	.4			 ·6		 ·8	•••	•••			4·2 7·0	26 42				
23 24			·7	I.0 I.0	I.0	1.0	·4 ·4	·2 ·6		·5		.1	·5						5.0	30				
25			.1	.1	.3	.7	.9	.6	•5	٠6	.5	.7	.9	•6	.7	1.0	.3		8·5	51	•••	•••	•••	•••
26			.9	-8	.5	.7	.6	.2	.6	.7	•5	.5	.1	.5	·ı				6.7	40				
27 28	• • • • • • • • • • • • • • • • • • • •			.3	•5	.8	.6	.5	1.0	.5	·I	•6	1.0	1.0		•••	•••	•••	6.2	37 20	•••		•••	•••
25			·3	'4 1·0	1.0	1.0	1.0	1.0 I.1	I.O	1.0	1.0	I.O	1.0	1.0	0.8				3·3 12·1	72	12 12	86	1.20	Clear
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Sum.	•••	I.4	5.9	10.1	11.0	11·1	11.7	13.4	13.2	10.6	10.1	10.5	13.4	12.8	8.3	4.1	0.6		148.8					
Mean.		; 95		ł 1															4.80	1 20	í	ľ		1
i	• • • • •	0.5	.19	·33	.39	•36	.38	· 4 3	43	•34	.33	•33	· 4 3	.41	.27	.13	•02	• • •	4.00	30	<u> </u>	<u> </u>	•••	•••
174.								•43	43	•34	•33	•33	•43	·41	•27	•13	•02	•••	4.80	30	1		ıne, 19	
174.	Esk	dalem	uir :	hs =	= 1 · 5	5 met	res.				·33	•33 hr.	• 43	·41	•27	•13	hr.	hr.	4.80	1 %				
ī	Esk	dalem				hr.	res.	hr.	hr.	hr. -8	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr. 2·9	% 17	h. m.	Jı mw/cm³	ıne, 19	923.
1 2	Esko	hr.	hr.	h _s =	= 1 · 5	hr.	res.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	%	h. m.	Jı mw/cm³	ıne, 1	923.
1 2 3 4	hr	hr.	hr6 .3	hs =	hr	hr '4 '2	res. hr2 1.0 2	hr. 1 0 1 0	hr. '4 1.0 '2	hr. ·8 1·0 	hr3 -62	hr8	hr. .9	hr. 1·0	hr2 1-0	hr. .7 	hr. 	hr. 	hr. 2·9 9·4 0·6 1·7	% 17 55 4	h. m	Jt mw/cm² 	 	923.
1 2 3	hr	hr.	hr. 	hs =	hr.	hr '4	res. hr. '2 1:0	hr. 1.0 1.0	hr. '4	hr. -8 1.0	hr3 -6	hr ·8	hr. .9	hr. 1.0	hr. •2 1•0	hr. .7	hr.	hr. 	hr. 2·9 9·4 o·6	% 17 55 4	h. m.	J(mw/cm' 	 	9 23.
1 2 3 4 5	hr	hr.	hr6 .3	hs =	hr	hr '4 '2	res. hr2 1.0 2 2	hr. 1.0 1.0	hr. '4 1.0 '2 .1	hr. -8 1·0 -3	hr. '3 '6 '2	hr8	hr9	hr 1.0	hr2 1-0	hr	hr	hr. 	hr. 2·9 9·4 0·6 1·7 3·8	% 17 55 4 10 22	h. m.	Jt mw/cm² 	19	923.
1 2 3 4 5	hr	hr.	hr6 .3 1.0	hs =	= 1 · 5 hr2 .5	5 met	res. hr. '2 1'0 '2 2	hr. 1.0 1.0	hr. '4 1.0 '2 ·1	hr. .8 1.0	hr3 -621	hr8	hr9	hr. 1.0 	hr2 1-0	hr. '7 	hr.	hr. 	hr. 2·9 9·4 0·6 1·7 3·8	% 17 55 4 10 22	h. m.	Jt mw/cm² 	 	923.
1 2 3 4 5 6 7 8	hr	hr	hr	hs =	hr	5 met	res. hr2 1·02 2 -28	hr. 1.0 1.0	hr. '4 1.0 '2 ·1	hr. ·8 I·0 ·3	hr.	hr8	hr98 .6	hr 1·0	hr2 I-0	hr '7	hr	hr	hr. 2·9 9·4 0·6 1·7 3·8 1·5 2·7	% 17 55 4 10 22 9 16 9	h. m	Jt mw/cm²	19	923.
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1 2 3 4 5 5 6 7 8 9 10 III	hr	hr	hr	hs =	= 1·5 hr	5 met	res. hr2 1·02 2 -28	hr. 1.0 1.0	hr. '4 1.0 '2 ·1	hr. ·8 I·0 ·3	hr.	hr8	hr98 .68 I.0	hr 1·0	hr2 1-017	hr7	hr	hr	hr. 2·9 9·4 0·6 1·7 3·8 1·5 2·7 1·5 5·0	% 17 55 4 10 22 9 16 9 29	h. m.	Jt mw/cm²	19	923.
1 2 3 4 5 5 6 7 8 9 10 11 12	Eske	hr	hr	hs =	= 1 · 5 hr	hr '4 '2 '6	res. hr2 1.02 2 -28 -1 1.0	hr. 1.0 1.0 1.0 1.0 1.0	hr. '4 1.0 '2 ·1	hr8 1.03	hr3 -621 -35 -8	hr85 .75 .7	hr.	hr 1·0	hr2 1-0	hr	hr	hr.	hr. 2·9 9·4 0·6 1·7 3·8 1·5 2·7 1·5 5·0 14·5	% 17 55 4 10 22 9 16 9 29 84 21	h. m	Jt mw/cm³	19	923.
1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14	Eskc hr	hr	hr6 .3 1.0	hs = hr.	= 1.5 hr2 .5	hr '4 '2 '6 1:0	res. hr. '2 1.0 '2 2 *8 '1	hr. 1:0 1:0 1:0 1:0	hr. '4 1.0 '2	hr8 1.03	hr.	hr	hr98 .68 I.0	hr 1.0	hr2 1-017 1-05	hr	hr	hr	hr. 2·9 9·4 0·6 1·7 3·8 1·5 2·7 1·5 5·0 14·5 3·6 11·6	% 17 55 4 10 22 9 16 9 29 84 21 67	h. m	Jt mw/cm³		923.
1 2 3 4 5 5 6 7 8 9 10 11 12 13	Eske	hr	hr6 .3 1.0	hs =	= 1 · 5 hr	5 met	res. hr. '2 1.0 '2 2 *8 '1 1.0 '3	hr. 1.0 1.0	hr. '4 1.0 '2 ·1	hr8 1·0 3 3	hr3 -621 -35 -82	hr85 .75 .7	hr98 .68 I.0	hr 1.0	hr2 1.0	hr7	hr	hr	hr. 2·9 9·4 0·6 1·7 3·8 1·5 2·7 1·5 5·0 14·5 3·6	% 17 55 4 10 22 9 16 9 29 84 21	h. m	Jt mw/cm³		923.
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1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	Eske	** ** ** ** ** ** ** ** ** ** ** ** **		hs = hr.	= 1·5 hr	5 met hr. '4 '2 .6	res. hr. 2 1.0 8 11.0 1.0 1.0 2 1.0 1.0 1.0 1.0 1.0	hr. 1·0 1·0 1·0 1·0 1·0 1·0 1·0 1·0 1·0 1·0	hr. '4 1.0 '2 '1 '2 '5 1.0 '6 1.0 '8 '7 .9 '7 .9	hr8 I-03	hr3 -61 -335 -82 -917 -3 -76	hr	hr	hr I-0	hr2 1-07 1-05 -7 -13	hr	hr	hr	hr. 2·9 9·4 0·6 1·7 3·8 1·5 2·7 1·5 5·0 14·5 3·6 10·2 1·7 7·3 5·4 7·8 7·9 0·6 8·4	% 17 55 4 10 22 9 16 9 29 84 21 67 1 10 42 31 45 45 45	h. m.			923.
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1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	Eske			hs = hr	= 1·5 hr. hr. hr. hr. hr. hr. hr. hr. hr. hr.	5 met hr. .4 .2 .6 .	res. hr2 1·03 1·03 1·05 -8 -1 1·07 -9	hr. 1·0 1·0 2 55 1 1·0 9 1·0 1·0 1·0 1·0 1·0 1·0	hr. '4 1.0 '2 '5 1.0 '6 1.0 '8 '7 '9 '1 1.0 '2 '6	hr. -8 I-033 I-01 I-03 I-0 I-0 I-0 I-0 I-0 I-0 I-0 I-0 I-0 I-0	hr3 -61 -35 -82 -97 -3 -7 -3 -7 -161 -1 -0 -3 -1 -0	hr	hr	hr I·0	hr2 1-07 1-07 1-05 -17 -17 -19	hr	hr	hr	hr. 2 · 9 9 · 4 0 · 6 1 · 7 3 · 8 1 · 5 5 · 0 14 · 5 1 · 6 1 · 6 0 · 2 1 · 7 7 · 3 5 · 4 7 · 9 0 · 6 1 · 6 8 · 4 0 · 2 5 · 4 8 · 6 3 · 2 8 · 3	% 17 55 4 10 22 9 16 9 29 84 21 67 1 10 42 31 45 45 45 3 9 48 1 31	h. m			923.
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1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum.	Eske	### Annual Property of the Internal Property o		hs = hr	= 1·5 hr. hr	5 met hr '4 '2 .6 '1 1.0 '6 1.0 '8 '9 '8 '8 '1 10.6	res. hr2 1:03 1:03 1:05 -8 -1 1:0 -7 -9 1:0 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7	hr. 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.	hr. '4 1.0 '2 '1 '2 '5 1.0 '8 '7 '9 '1 1.0 '1	hr8 1·03 3 1·03 1·03 1·0 -2 -93 -8 -2 -1 -9 -8 1·0 -81 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1	hr. 3 6 2 1 3 5 8 2 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	hr	hr	hr 1·0	hr2 1-07 1-07 1-05 -15 -7 -119 -97 -1	hr	hr	hr	hr. 2 · 9 9 · 4 0 · 6 1 · 7 3 · 8 1 · 5 5 · 0 14 · 5 3 · 6 11 · 6 0 · 2 1 · 7 7 · 3 5 · 4 7 · 8 7 · 9 0 · 6 1 · 6 8 · 4 0 · 2 5 · 4 8 · 6 3 · 2 8 · 3 8	% 17 55 4 10 22 9 16 9 29 84 21 67 1 10 42 31 45 45 45 3 9 48 1 31 50 18 48 68 10	h. m	Jt mw/cm²		923.
1 2 3 4 5 5 6 7 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	Eske	** ** ** ** ** ** ** ** ** ** ** ** **		hs = hr	= 1·5 hr. hr	5 met hr.	res. hr2 1:03 1:03 1:05 -8 -1 1:0 -7 -9 1:0 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7	hr. 1.0 1.0 5.1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1	hr. '4 1.0 '2 '1 '2 '5 1.0 '8 '7 '9 '1 1.0 '1	hr8 1·03 3 1·03 1·03 1·0 -2 -93 -8 -2 -1 -9 -8 1·0 -81 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -9 -8 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1	hr.	hr	hr	hr I·0	hr2 1-07 1-07 1-05 -15 -7 -119 -97 -1	hr	hr	hr	hr. 2 · 9 9 · 4 0 · 6 1 · 7 3 · 8 1 · 5 5 · 0 14 · 5 3 · 6 1 · 0 2 1 · 7 7 · 3 5 · 4 7 · 8 6 · 4 0 · 2 5 · 4 8 · 6 3 · 2 8 · 3 1 · 8 1 · 7	% 17 55 4 10 22 9 16 9 29 84 21 67 1 10 42 31 45 45 45 3 9 48 1 31 50 18 48 68 10	h. m	Jt mw/cm²		923.
1 2 3 4 5 5 6 6 7 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum. Mean.	Eske	** ** ** ** ** ** ** ** ** ** ** ** **		hs = hr	= 1·5 hr. hr. hr. hr. hr. hr. hr. hr. hr. hr.	5 met hr.	res. hr2 1·08 -1 1·03 1·05 -8 -1 1·07 -9 1·0 -7 -7 -7 -13·4 -45	hr. 1·0 1·0 2 55 1 1·0 1·0 1·0 1·0 8 5 1·0 1·0	hr.	hr8 1·03	hr. 3 6 2 1 3 5 8 2 9 1 6 1 10 3 10 10 10 97 32	hr8	hr	hr I·0	hr2 1-07 1-05 -1319 -9 -97·1 -24	hr	hr	hr	hr. 2 · 9 4 0 · 6 1 · 7 3 · 8 1 · 5 5 · 0 14 · 5 3 · 6 1 · 6 0 · 2 1 · 7 7 · 3 5 · 4 7 · 8 7 · 9 0 · 6 8 · 4 0 · 2 5 · 4 8 · 6 3 · 2 8 · 3 1 · 8 1 · 7 1 3 8 · 9 4 · 6 3	% 17 55 4 10 22 9 16 9 29 84 21 67 1 10 42 31 45 45 45 3 9 48 1 31 50 18 48 68 10	h. m.	Jt mw/cm³		923.
1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum.	Eske	### Annual Property of the Internal Property o		hs = hr	= 1·5 hr. hr	5 met hr '4 '2 .6 '1 1.0 '6 1.0 '8 '9 '8 '8 '1 10.6	res. hr2 1·08 -1 1·03 1·05 -8 -1 1·07 -9 1·0 -7 -7 -7 -13·4 -45	hr. 1.0 1.0 1.0 1.0 1.0 1	hr. '4 1.0 '2 '1 '2 '5 1.0 '8 '7 '9 '1 1.0 '1	hr8 1-033 1-01 1-03 1-03 1-03 1-03 1-03 1-03 1-03 1-03 1-03 1-03 1-03 1-03 1-03 1-03 1-0 -9 -8 -1 -9 -8 -8 -9 -1 -9 -8 1-0 -8 -8 -9 -9 -93 -8 -9 -93 -9 -8 -9 -93 -9 -93 -9 -8 -9 -93 -9 -9 -93 -9 -9 -93 -9 -9 -93 -9 -9 -9 -9 -9 -9 -9 -9 -9 -9 -9 -9 -9	hr3 -6 -1 -3 -1 -3 -7 -1 -1 -6 -1 -1 -6 -1 -1 -7 -32 -1 -3 -3 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1	hr8	hr	hr I·0	hr2 1-07 1-05 -1319 -9 -97·1 -24	hr	hr	hr	hr. 2 · 9 9 · 4 0 · 6 1 · 7 3 · 8 1 · 5 5 · 0 14 · 5 3 · 6 1 · 6 0 · 2 1 · 7 7 · 3 5 · 4 7 · 8 7 · 9 0 · 6 8 · 4 0 · 2 5 · 4 8 · 6 3 · 2 8 · 3 1 · 8 1 · 7 138 · 9 4 · 63	% 17 55 4 10 22 9 16 9 29 84 21 67 1 10 42 31 45 45 45 45 45 3 9 48 1 1 50 18 48 68 10	h. m	Ju mw/cm²		923

DURATION OF BRIGHT SUNSHINE.
For periods of sixty minutes, between the exact hours of Local Apparent Time.

175. **Eskdalemuir**: h_s (height of recorder above ground) = 1.5 metres.

July, 1923.

	ato			6 to		8 to	9 to	40	to	Noon	to		re to	16 to	77 to	18 to	19 to	20 to	Total	Per cent.		Radiat	ion by	neter.
Day.	3 to	4 to 5.	5 to 6.	7.	7 t o 8.	9.	10.		Noon		14.	15.	16.	17.	18.	19.	20.	21.	for Day.	of Possible.	Time.	Inten-	1	Sky.
\ 	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	% 8	h. m.	mw/cm²	<u> </u> 	<u></u>
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3					•••							•2		٠				•••	0.3	2		•••	•••	
5				··I			:::									••2	•4		0.6 0.1	3				
6	 			•5	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	.5		.6	.1	l		9.7	56	 			
7				.1	.1	.5	.8								•••				1.5	9			•••	
8										 '9	·2 I·0	·6 ·8	·8	·6	I.O I.O	.9			4·7 5·4	²⁷ 32				
10						•••	•••		.5	1.0	.7	٠ı	•2		•••			•••	2.2	13		•••	•••	
11					•6		.8	.3	.8	.6	·8	·9	.3	·7 1·0	.7 1.0	'4 1.0			6·9 12·3	41 73				
12				••5	1·0	I.0 I.0	.2	.0 I.0	I.0 I.0	I.O I.O	I.0 I.0	1.0	I.0 I.0	1.0	•6	.1			10.6	63				
14 15						1.0				·6	·6								4.3	25			•••	
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16 17 18					·5 ·8	·I	•5	5	.3	·5	·7		·5	·1	•1	••2	:::		4·3 5·9	35		:::	•••	
18			•4	.7	.1			·1					.1	·8	1.0				3.4	20 4				
20			٠	···	··8	1.0	1.0	1.0	1.0	10	1.0								8.2	49				
21			•••	.3	.5	1.0	.5	.6	1.0	-6	∙6				•••				5.1	31				
22 23									I.O	1.0	···				···		:::		3.6	22				
24			•••	•3	.7	1.0	1.0	1.0	1.0		·3 ·8	.3			• • • • • • • • • • • • • • • • • • • •				5.6	34				•••
25		•••	•••	.I	.I	4	•••			·2		1.0	1.0	.7	.7	'4	.I	•••	5.5	34				
26 27			·1	·5 ·4	·9	1.0	1.0	.I I.O	1.0	1.0	1.0	1.0	1.0	I.0 I.0	1.0				12·3 7·8	75 48				
27 28																								
29 30	:::	:::	:::		1.0	I.O								••2					6.0	37				
31					l					.2		l	·1	.3				_	0.6	4				
	<u> </u>		<u> </u>				<u> </u> -			 _	13.6				7.8		1.6		129.5	<u>-</u> -	<u> </u>	-		
Sum.	<u> </u>	0.3	1.2	4.7	9.7	10.8	10.9	9.5		11.9		11.0	9.0	10.4		4.6	ļ				<u> </u>	ļ		
Mean.	<u> </u>	.01	•05					.31	.40	.39	-44	•35	.29	34	.25	•15	.05		4.18	25	<u> </u>			002
176.		dalen			= 1.5			hr.	hr	hr	he	he	he	hr.	hr.	hr.	hr.	hr.	hr.	1 %	h. m.	mw/cm²	ust, 1	923.
I	hr. —	hr.	hr.	hr. •2	hr. 	hr.	hr. •2	.7	hr. '7	hr.	hr. •9	hr. 1.0	hr. •6		·1	.6	•4	—	6.8	43				
3											 ·6	·3	···		···				0.3	2 27				
4		•4	1.0	-8	•2	'4 ·1	.5	1.0 1.0	I.0 I.0	I.0	·6	∙6	.7	•2	·4		•••	_	9.2	58 28				
5	-	•••	•••	•••	•••		'4			10		.3	•••	***	•••									
6						·	8	8					···						0.8	15 5				
8			•2	1.0	1.0	1.0	-8				•••	 ·6	··.						4·0 5·5	26 36				
9 10	=		.1			···	·3 ·6	.2	1.0	·3	·5 	.6	.9	·5	•2	•4		_	2.1	33				
11				.3	.7	.9	.1	.2	.8	·4	.5	.8	.5	•4	-8	.2		_	6.6	43				
12	_				• • • •						•••	···		 ·6		 I·o		<u> </u>	2.8	 18	:::			
14			•••							.I	.I	٠ı			•••				1.7	69				
15	-	•••	·I	.9	-8	•5	'4	1.0	1.0	٠6	.7	1.0	1.0	1.0	1.0	.3			10.3	1	•••	•••	•••	•••
16 17	_					·2		·6	.3		·4	·1		.3		•••		_	2·3 0·6	15 4				
18			•••	•••			.5	.9	'4		٠ı			•••					1.6	11				
19 20	=		•••		•••		•••								•••			_	 I.O					
21									 	.2	٠1	•5	.5	1.0	٠8				3.1	21				•••
22			•••		•••	.I	.3	.7	.7	٠6	•5	•2	·5 ·6	.7	•••	•2			4.2	31				•••
23 24			•••	··6	1.0	I.O				···	···						:::		5·4	38 -	•••	•••		•••
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26	<u> </u>		•••	··ı		·3	·7 ·9	4	·8	·7	·6		.3		•••			_	3·6 4·6	25 32				•••
27 28			•••		.4 .1	··3	٠ı	- 4	·4 ·3	·7	·7	·2 I·0	I.O	I.0	···	·1		_	6∙1	43				•••
29 30	_	_	•••						 ·8	 .5	···	···	I.O		···			_	0·1	1 39				•••
31		_	•••		٠ı	•6	·4	.5	.3	.3	٠1	٠1							2.4	17				
	<u>_</u>			<u> </u>									9.6		···									
Sum.		0.4	1.8	4.1	2·I	5.8				10.1	9.4	9.9	8.6	8· ₄	6.7	3.2	0.4		105.9					
Mean.	l —	.01	• o 6	.13	.16	.19	•26	.38	-38	•33	.30	.32	•28	.27	.22	•11	.01		3.42	23			-	
				6 L-		8+-	0.40	TO 4	ايري	No -			_ ,			_0 .			Total	Per cent.	Time. G.M.T.	Inten- sity.	<i>p/p₀</i> sec. Z.	Sky.
Hour. L.A.T.	3 to	4 to	5 to 6.	6 to 7.	7 to 8.	8 to 9.	9 to	10 to	II to Noon	to 13.	13 to	14 to 15.	15 to 16.	16 to	17 to 18.	18 to 19.	19 to 20.	20 to 21.	for	of		Radiati	on by	
		-				1			1			-		.		-			Day.	T OSSIDIG.	Ångst	röm Py	rheliom	eter.
			1							- 1		1				- 1				•				

DURATION OF BRIGHT SUNSHINE.

For periods of sixty minutes, between the exact hours of Local Apparent Time.

177. Eskdalemuir: h_s (height of recorder above ground) = 1.5 metres.

September, 1923.

177.													meti											
Day.	3 to	4 to 5.	5 to 6.	6 to 7.	7 to 8.	8 to 9.	9 to	Io to		Noon to 13.		14 to	15 to 16.	16 to	17 to 18.	18 to	19 to	20 to	Total for Day.	Per cent. of Possible.		röm Py	rheliom	eter. Sky.
																					G.M.T.	sity.	p/p_0 sec. Z .	Sky.
	hr.	hr.	hr.	hr.	hr.	hr.	hr. -8	hr.	hr. •3	hr. '4	hr. •8	hr. '4	hr.	hr.	hr.	hr.	hr.	hr.	hr. 4·6	% 33	h. m.	mw/cm³		•••
2	_	_		.3	1.0	1.0	•4	'4	.9	.9	1.0	1.0	1.0	1.0	1.0	.3	-	-	10.2	33 74 18			••• [•••
3 4		_			3	1.0	1.0	'4 1.0	1.0	1.0		•7	•4				_		2·4 7·4	54				•••
5	-													٠ı	•••				0.1	I			•••	•••
6	_	-								·ı	2	٠1					_	-	0·4 8·9	3	•••			•••
7 8		=			1.0	1.0	1.0	·8 ·8	·9	·9 ·2	·4 ·2	·4 ·3	.1 .6	·8 	·6		_	_	2.3	67 17			•••	•••
9				·	1.0	···	···8	··.	···	 '7	 ·6	I.0	1.0	·		:::	_		 7·8	 59				•••
	l					ļ												_	0.3	2				•••
11		=						·3			··8						_		3.3	25		•••		•••
13 14		_					···			···			···	···					 6·9	 54		•••		•••
15	—	-		.1	•2	.3				·4	٠ź	•5	∙6	•2	٠1	•••	-		3.1	24				•••
16	l —				.3	.3	.4	.9	1.0	.5	.9	∙8	1.0	.7	·ı				6.9	54		•••		•••
17 18		_							 ·8	 .9	···	 •9	•••				_	_	5·0	 40				•••
19		_							1.0		 I·O	1.0							 6·8	 55				•••
20	-	_				.1	.5	1.0	1.0	1.0			.9	.3		•••	.							
2I 22	_	_					-8	1.0	 .7	·1	·1	·6	···	1.0	·6 		_	_	3·6 5·0	29 41		•••		•••
23	—	_				1.0	1.0	·5 ·8		·2 ·8		1.0 .1	1.0				_		1·7 8·0	14 66				•••
24 25		_	=						.2	.2									0.4	3				•••
26		_	_				•4	•5	-8	.2							_	_	1.9	16				•••
27 28	_		_						I.O	I.0	 I·0	 ·8	•••				_		4.7	 40			•••	•••
29		-	-													-	_	_	•••					•••
30					<u> </u>		<u> </u>																	
Sum.				0.9	6.3	7.9	10.1	12.2	12.0	11.2	11.5	11.7	8.8	6.1	2.6	0.3			101.6					
Mean.	<u> </u>		ļ	•03	•21	•26	:34	·41	•40	.37	·38	•39	•29	•20	-09	.01			3.39	26				
178.	Esk	dalem	uir :	hs =	= 1.5	metr	res.															Octo	ber, 19	23.
	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	% 26	h. m.	mw/cm³		
I 2		_	_			·2 ·9	I.O	1.0	.3	·6	·5 ·9	·1	·3 ·6	·4 ·3		_	_	_	3·0	62		•••	•••	•••
3 4	_	_			 I·0						···					_	_		6·5	 57				•••
5		_														-	-					•••	•••	•••
6			_	l				.1	-8	.7	.5	·4	-8						3.3	29		•••		•••
7 8		_	_		···	··6	•1				:::					_	_	_	1·9	17				
9	_		_		••••		•2	.3	.5	1.0						_	_		2.8	26 				•••
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11		_			·8 		 I.O	···	 I.O	·4	.I I.O	···	·9 ·4	•2		_		_	1.1	10	•••	•••	•••	•••
13 14		_			·2 ·4		.4 1.0	1.0	1·0			·3	 •5	·1			_		6·9	9 65		•••	•••	•••
15	_	-	_									'								•••		•••	•••	•••
16	_		_			·ı				.7	.9	1.0	.7	.7				_	4·I	39 40				•••
17 18	_	_							1.0	·5 ·4		.2		:::		_	_	_	4·1 1·4	40 14		•••		•••
19						•2	1.0	1.0	1.0	.9	.9	-8	•5		•••	_	_	_	6·3	62		•••	:::	•••
20	_	_	_		•••			•••								}			2.6	26				•••
2I 22	_		_	_					.3	·9 ·4					_	_	_	_	0.0	9		•••		• • • •
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25	_	—		_	٠ı	.1	.7	.2	·6	1.0	.7				-	-			3.7	38	•••	•••		•••
26	_	_		_				.5	1.0	.9			•2		-	-			2.6	27				•••
27 28	_		_	_						.3	·5 ·9	·3			_	_	_	_	3.6 1.3	13 38		•••		•••
29	—		_	_			•••							•••	_	_	_	_	0· I	 I		•••		•••
30	-				•••	•••		•••		•••		•••		•••					2.1	22				
31							 -6		.3		I		·2											
Sum.	_			0.1	3.3	6.0	8.7	9.7	11.0	14.0	10.8	7.8	5.7	1.7					78.8			<u> </u>		
Mean.	<u> </u>		_	.00	.11	•19	•28	.31	.35	∙45	•35	.25	8	.05					2.54	24	l — 	7-4		
Hour	3 to	4 to	5 t o	6 to	7 t o	8 to	9 to	10 to	II to	Noon	13 to	ia to	ıs to	16 to	17 to	18 to	19 to	20 to	Total for	Per cent. of	I	Inten- sity.	sec. Z.	Sky.
L.A.T.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	to 13.	14.	15.	16.	17.	18.	19.	20.	21.	Day.	Possible.	Ångst	Radiat tröm P	ion by yrhelion	neter.

DURATION OF BRIGHT SUNSHINE. For periods of sixty minutes, between the exact hours of Local Apparent Time. November, 1923. **Eskdalemuir:** h_s (height of recorder above ground) = 1.5 metres. 179. Radiation by Total Per cent Ångström Pyrheliometer. 10 to 11 to Noon 13 to 14 to 15 to 16 to 17 to 18 to 19 to 20 to 3 to 6 to 7 to 8. 8 to q to 4 to 5 to for Day. Noon to 13. 14. 15. 16. 17. 18. 19. 20. 21. 10. II. Possible. 5 7. Q. Day. Time Inten p/p_0 sec. Z Sky. G.M.T. sity. h. m. hr. hr. hr. hr. hr. hr. hr. hr. mw/cm hr. hr. hr. hr. hr. hr. hr. hr. hr. hr. 15 41 3·8 ·9 ·8 ... ٠6 ٠6 .2 •6 ... ٠3 ٠6 •6 ٠ı 1.4 15 •т 1.5 173 ... ٠2 ·7 3.28 ٠ı 35 ٠7 ٠9 5 ... 69 **87** -8 1.0 1.0 1 ·O 1.0 6 7.7 1 ·0 1.0 1.0 .3 T .O T.O 1.0 1.0 •4 2·5 1·7 4·8 28 •6 ٠2 . . . 19 • • • ·4 ·2 ... 55 . . . ٠8 1.0 1.0 • т .3 10 12 13 . . . 1.9 ٠.. .2 23 ٠2 •5 ٠2 .3 .3 •2 14 15 - - -. 52 4·3 1·6 . . . ·5 16 19 •2 17 18 ... 2.0 25 868 ٠3 ... 7·0 1·6 1.0 1 ·0 1 ·0 1.0 ٠5 1.0 •5 1.0 ... 19 20 2Ó ·q • 7 4 · I 51 .8 1.0 •6 ٠4 ٠5 21 22 5·7 6·7 72 86 I .O 1.0 1.0 ٠9 ٠5 23 1.0 1.0 .8 ٠9 1.0 ٠3 •7 . . . ٠.. 25 26 1 0.1 • • • 28 ··8 33 ... ٠4 ٠2 1.0 .2 29 0.83 •5 30 12.4 72.5 11.7 9.1 9.1 3.1 5.7 11.0 9.9 Sum 0.5 2.42 29 ·41 .10 •39 .33 .30 .30 .19 .37 Mean December, 1923. 1.5 metres. $h_s =$ 180. Eskdalemuir: h. m. hr. % hr. mw/cm hr. hr. hr. hr. hr. hr. hr. hr. hr. hr. hr. hr. $6 \cdot 2$ 84 1.0 1.0 1.0 1.0 1.0 1.0 3 ٠., ... ٠.. ٠.. 5.4 74 .8 1.0 1.0 •6 1.0 1.0 . . . 6 7 8 61 5.2 1.0 1.0 .8 .2 72 ... • • • •5 .7 10 • • • II • • • 12 5.8 82 1.0 1 ·0 1.0 1.0 1.0 •7 ... 13 ٠6 1.7 24 ٠ı .7 •3 15 ٠.. . . . 16 ... 0 · I • т ··· ... 17 18 ... 2.8 ٠8 •2 1.0 ... ٠8 1.0 1.0 67 ٠6 •9 • • • IQ 53 ٠ı $\mathbf{i} \cdot \mathbf{o}$ 1.0 ٠9 .7 208 24 **87** ٠1 •5 ٠3 ... 22 1.0 ٠8 6.1 • • • 1.0 1.0 1.0 .3 1.0 ... 23 ___ .8 ٠8 3.2 46 1.0 •4 25 26 • • • 27 6 ٠., ٠2 0.4 **2**8 • • • 29 30 31 ___ 9.3 10.7 51.4 7·1 7.8 5.4 0.2 Sum. I · 66 23 .23 .30 .35 .25 ٠17 ·oı .03 Mean. Annual 126. 112·4 128·0 **132·0** 124·4 116·1 107·8 81·1 3.0 36.6 81.4 65∙0 39.1 17.6 57.4 20.5 Total. 4.3 Annual 25 0.22 0.31 0.35 0.36 0.34 0.32 0.29 0.22 0.18 0.11 0.05 0.01 3.09 **o·o**6 Mean. O.OI Time *⊅|⊅₀* sec. Z Inten-Sky. Total Per cent G.M.T. sity. Io to II to Noon 13 to 14 to 15 to 16 to 17 to 18 to 19 to 20 to 11. Noon to 13. 14. 15. 16. 17. 18. 19. 20. 21. 7 **t**o 8 to 9 to 3 to 5 to 6 to Hour 4 to for 8. 10. Possible. 7. L.A.T. 5. Day. Radiation by Ångström Pyrheliometer.

Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$). Speed in metres per second.

181. Eskdalemuir:

Ha (height of anemograph above M.S.L.) = Height of ground above

Day.	I.		2	2.	.3	3.	4	1 .		5.		5.	1	7.	8	i.	9).	I	o.	I	I.	N	oon.
	0	m/s.	0	m/s.	0	m/s.	-	m/s.	0	m/s.	0	m/s.	-	m/s.		m/s.	-	m/s.	_	m/s.	· —	m/s.	-	m/s.
I 2	180	4.8	180	5.5	190	5.4	190	3.0		1.5	200	7.9	200	10.1	200	12.7	200	13.8	210	14.1	210	14.8	250	10.0
3	220	10.5	210	11.5	210	9.4	230	12.4	250	12.2	250	11.6	250	8.6	240	7.6	230	7.1	190	6.2	220	9:4	240	9.4
4	-	o·8		0.2	260	3.3	290	5.1	300	6.1	320 160	7:5	320 160	7·1 7·5	310 150	5·5 7·5	290 150	7.8	160	† 6·9	160	7.5	160	8.4
5	190	7·1	180	8.6	170	7.0	160	2.1	160	5.6	100	6.5	100	/ 3	150	1 / 3	150	/ "	100	. ,	-00	, ,		'
6		1.4		1.4	270	3.4	260	3.6	250	3.7	220	4.2	260	6.7	270	5.7	240	5.3	220	5·1	220	4.9	210	4.8
7	170	9.2	170	8.1	170	7.3	180	8.5	180	7.8	180	6.1	180	5.2	180	3.4	180	3.6	190	3.3	220	4.5	200	5.0
8	210	11.8	210	12.9	210	12.8	220	15.4	230	13.2	250	14.6	250	10.8	250	7.4	250	7·2 8·6	260	8.6	250	9.9	260 220	11.8
9	190	12.8	180	12.3	180	15.4	180	15.5	230	13.4	240	10.9	240	9.6	240 260	8·4 9·3	220 260	10.8	220 280	9·8 13·9	220 280	11.2	280	10.4
10	220	15.0	220	16·1	230	13.8	230	13.5	240	12.9	240	10.0	240	0.0	200	9.3	200	10.0	200	139	200	23 3	-30	0
11	300	9.4	300	8.2	300	8.2	300	6.5	300	6.6	290	3.8	290	2.7	290	3.8	290	7.3	300	11.8	280	8.6	290	6.7
12	330	3.1	300	0.6	360	1.6	J	0.0	_	0.0	<u></u>	0.4	_	0.0		0.0		0.0		0.0	<u> </u>	0.0		0.0
13		0.0	_	0.0	J	0.0		0.0	<u> </u>	0.0	l —	0.0	_	0.2	150	2.5	210	2.2	190	3.4	200	5.0	200	6.0
14	190	5.5	240	8.5	240	11.9	230	14.3	230	12.5	230	11.0	250	11.3	260 280	9.4	280	10.2	280	10.6	290 280	7.8	280 280	7.7
15	280	13.1	280	12.8	280	11.8	280	12.4	280	14.5	280	11.9	280	10.9	280	7.8	280	5.0	270	7.9	200	1.0	200	1 /
16	210	5.0	210	4.6	310	2.5		0.4		0.4		0.4	_	1.1		0.5		1.0		1.0	_	0.3		1.2
17	310 200	5·0 2·4	310 200	3.0	200	4.8	210	4.4	230	4.0	220	3.0	210	2.4	210	4.6	210	3.6	220	4.5	220	4.6	220	5.4
18	280	1.7	_	0.5	260	2.3	270	2.5		0.5	310	2.6	330	4.0	330	3.9	320	4.3	340	3.8	340	2.3	330	3.8
19	210	5.6	210	6.5	200	4.9	210	4.2	230	3.6	220	5.9	190	5.5	200	5.4	210	6.4	220	7.4	210	10.3	220	14.4
20	280	11.1	290	12.8	290	14.6	290	12.4	290	13.2	300	16.6	290	15.0	290	14.0	310	14·I	330	11.3	340	12.7	340	13.5
	250			1.1	220	4.7	220	4.4	230	3.9	220	4.2	200	5.5	200	3.4	210	5.0	210	8.2	200	7.4	190	4.7
21 22	270 280	2·4 7·6	270	6.8	230 250	7.5	250	7.2	210	9.2	270	10.8	270	12.6		14.0	26 0	13.9	270	13.6	270	13.1	260	13.3
23		1.4	280	2.6		1.4		1.3		1.5	<u></u>	o·8	<u>.</u>	0.7		0.5	_	0.7	230	6.1	230	6.5	210	5.3
23 24	210	8.2	220	7.6	240	8.8	240	9.6	240	11.8	250	11.7	250	8.9	210	5.0	220	4·1	230	9.4	260	9.5	260	9.1
25	260	6.8	270	7.2	270	6.8	270	7 · 3	240	5.9	230	6.7	250	8.5	250	7.4	240	7.1	240	6.0	230	7.2	210	6.5
			2 4 0		250		260	10.5	250	10.0	260	8.2	220	4.0	220	5.0	260	6.8	270	6.5	260	6.7	250	7.0
26	240	6.9	250 250	10.0	250 240	8.8	260 250	8.4	250	6.5	260	7.1	250	6.6	260	7.4	260	6·1	250	6.8	260	7.6	260	8.4
27 28	240 270	5.2	280	6.2	280	6.4	280	6.4	270	5.2	270	5.4	270	6.6	270	5·1	270	5.1	270	5.8	270	5.3	270	5.5
20 29	230	6.5	230	5.5	240	7.8	230	8.1	240	8.2	260	8.1	270	8.7	270	6.9	270	4.7	280	3.7	260	3.9	260	6.0
30	280	4.9	270	4.1	270	4.8	220	3.7	190	1.6	180	1.7	200	1.6	260	3.4	260	4.8	250	4.4	220	3.3	220	4.6
31	250	6.4	230	5.5	230	4.5	240	4.8	220	5.0	230	5.4	240	6.6	230	4.4	310	4.3	230	8∙0	220	8.6	210	7.6
Mean‡		6.6		6.8		7.0		6.9		6.5		6.6		6.4		5.9		6.0		6.9		7.3		7:3

182. Eskdalemuir: $H_a = 235 \text{ metres} + 15 \text{ metres}$.

102. L	Nuui	,,,,,	• 114		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		, ~~																	
Day.	0	m/s.		m/s.	0	m/s.	0	m/s.	0	m/s.	ı °	m/s.	1 °	m/s.	l °	m/s.	l °	m/s.	l °	m/s.	ľ°	m/s.	ľ	m/s.
Day. I	240	11.3	250	15.1	250	13.8	250	11.7	240	10.0	230	12.9	230	13.0	230	13.4	230	13.4	230	10.7	220	10.1	220	10.1
2	260	17.3	260	14.5	270	12.2	280	10.7	280	9.9	260	9.9	250	8.6	230	7.2	220	7.5	210	7.1	210	7.5	220	8.1
3	220	9.8	1	11.5	250	7.8	230	7.4	230	9.6	230	10.0	230	9.9	230	10.2	220	9.4	230	9.6		11.3	250	10.4
3	260	5.3	290	3.6	330	4.5	340	4.2	340	3.5	320	2.4	310	2.3	300	6.3	290	3.6	280	5.6	290	5.0	280	3.5
4 5	170	3.5	190	5.5	180	5.7	180	9.1		11.5	180	10.9	190	11.8	200	13.0	190	13.0	200	11.7	200	13.0	200	15.0
3	1,0	33	190	33] ,				, š.											1			
6	190	11.6	180	13.2	170	12.8	160	10.0	170	9.0	160	9.8	160	10.2	170	11.3	160	10.3	160	9.5	170	10.4	170	10.0
7	200	8.6	200	7.9	200	7.0	200	5.0	180	4.8	170	4.8	160	6.1	140	7.8	130	8.5	150	12.8	150	14.6	150	11.9
8	150	4.6	150	6.0	150	6.9	150	6.8	170	6.0	170	3.2	220	4.6	280	5.0	280	3.7	280	3.6	I —	1.2	270	3.4
=	150	0.3	150	0.3		1.5	210	3.0	18o	3.0	180	3.7	180	3.4	200	2.7	190	2.8	210	3.0	200	3.3	180	3.2
9 10	130	6.0	130	6.6	130	7.2	130	7.1	130	7.6	120	8.6	120	8.9	130	8.6	120	7.8	130	9.5	140	10.1	140	9.8
10	130	00	130		130	, -	1 200	′ -	-3-	, -	_		l		1	ł	i	1	1					
11	100	5.8	80	4.0	60	5.0	80	7.8	90	7.5	80	7.9	80	7:4	90	6.7	100	5.7	90	6.6	90	5.6	90	5.3
12	200	2.9	210	5.0	220	5.0	210	4.9	220	5.2	220	4.5	180	2.3	200	4.0	200	5.5	190	5.4	220	5.3	240	3.7
		4.8	70	4.3	90	4.9	90	3.4		1.5	80	3.3	80	4.1	110	4.8	110	4.6	140	4.7	130	5.2	130	5.9
13	50		120	7.1	120	5.3	120	4.7	120	3.6	110	3.3	110	3.3	130	3.1	120	2.6	120	2.2	-	1.0	130	2.8
14	120	7:4		1.0	120	1.0		1.0		1.0	_	1.0	20	2.0	20	3.0	20	3.2	40	3.2	60	3.6	70	2.8
15	ļ —	1.0		1.0		1.0		1 0		1 0	1	1			l	"	l		l	1				
-6					130	3.9	140	3.4	150	3.4	150	1.9	l —	0.5		0.6		0.7		0.0		0.0	180	2.5
16	130 80	5 4	130 80	4.5	80		90	11.3	90	11.7	90	11.0	90	10.5	90	12.0	90	10.7	90	10.0	90	6.2	100	5.4
17	•	8.3	ł	7.1		9.7	-	12.3	130	11.2	130	10.3	130	9.3	130	8.2	130	8.5	130	9.3	130	11.0	140	9.6
18	130	8.6	130 80	10.4	130 80	12.5	120			1	90	3.2	80	3.3	60	3.0	6o	2.9	60	3.2	70	5.5	60	5.4
19	80	2.6]	2.3		2.6	90	4.3	90 60	3.5	90	1.0		0.0		0.5		0.3		0.8	130	3.4	150	2.4
20	50	2.8	-	1.5	_	1.5	60	3.3	00	2.9		1.0			i	- 5	l	"	ľ	i i	Ĭ		-	
			l	6			7.00	0.0	120	10.1	120	10.0	120	8.6	130	6.6	130	7.1	130	8.4	130	8.3	150	7.4
21	140	6.3	130	6.1	120	7.5	130	9.0	130	(120	1.4	350	2.0	20	1.7	40	2.0	360	2.0	10	2.7	10	2.1
22		0.2	_	0.0		1.0		I.I		0.9	l .	1.7	40	2.0	20	1.8	30	2.2	350	1.6	20	4.0	50	3.7
23	40	2.0	40	2.0		1.5		1.0	40	2.2	40		80	6.1	80	4.8	80	5.0	90	6.0	8o	7.3	70	6.1
24	70	3.6	70	3.0	70	2.9	70	2.4	70	3.3	70 60	5.2	60	2.3	70	2.8	50	2.3	100	3.6	110	4.2	120	5.2
25	80	3.3	80	2.9	80	4.0	70	2.2	70	2.1	00	3.1	00	2 3	/	1 2 0	ا ا	- 5		"	ľ	l .		
	1		l			- 6	١					1.6	70	7.1	70	9.9	80	10.4	100	12.0	110	14.6	120	13.1
2 6		1.0		0.1	_	0.6	10	2.1	50	4.2	50	4.6	70			5.5	130	7.4	140	7.5	130	6.7	100	6.1
27	140	11.2	140	11.9	140	11.5	140	9.8	140	9.0	140	7:4	140 280	5.7	140 280	3.6	130	1.5	260	3.5	260	2.4		0.4
28		1.5	310	1.6	310	2.4	320	3.1	290	3.2	280	4.2	200	2.0	200	3.0				33		. <u>'</u> _	ļ	ļ <u>-</u>
Mean	<u> </u>	5.6		5.7	_	5.8	_	5.8		5.8		5.8	_	5.7		6.0		5.8	_	6.2	-	6.6	_	6.3
	<u> </u>		<u> </u>		<u> </u>		<u> </u>		l	<u> </u>	<u> </u>				<u> </u>	<u></u>	<u> </u>		<u> </u>			1	<u> </u>	<u> </u>
CMT					ĺ.				١.	_	,	5.		,.	8	3.	ç).	1	o.	,	II.	N	oon.
G.M.T.	1 '	ι.	2	•	3	3.	1	.	1	5.	Ι ΄	<i>,</i> .	. '				1				1		l	
	<u>'</u>		!		<u> </u>		<u> </u>		<u> </u>		<u> </u>		<u> </u>											

Average for periods of sixty minutes, centred at the exact hours, Greenwich Mean Time.

 $M.S.L. + h_a$ (height of anemograph above ground) = 235 metres + 15 metres.

January, 1923.

r	3.	I	4.	I	5.	1	6.	I.	7.	ı	8.	1	9.	2	о.	2	ı.	2:	2.	23	3.	2.	1 .	Mean	Day.
210 230 —	m/s. o·o 6·4 9·5 1·o 7·1	200 240 220 220	m/s. 0·4 8·4 10·1 1·6 5·0	200 240 190 250	m/s. 0·1 8·1 11·9 2·2 4·4	210 250 200 240	m/s. 0·1 10·8 12·3 2·1 5·8	210 250 — 300	m/s. 0·0 13·2 9·9 1·5 7·6	210 280 — 300	m/s. o·o 14·9 10·1 o·o 8·5	° 210 300 300	m/s. o·o 13·5 9·5 o·1 6·3	210 300 300	m/s. o·o 13·3 9·o o·o 3·4	200 210 310 — 300	m/s. 2·0 13·3 10·4 1·5 3·6		m/s. 4·1 13·3 11·7 0·6 5·0	170 240 310 200	m/s. 4.0 12.7 8.8 2.3 0.6	170 220 300 190	m/s. 4·6 11·7 2·4 3·4 0·6	m/s. 0·5 10·0 9·8 — 6·0	1 2 3 4 5
220 210 260 220 280	5·6 5·9 12·7 12·1 10·7	220 210 270 230 280	5·2 9·1 11·1 12·4 12·1	220 210 270 230 280	5·1 9·1 10·9 15·2 11·2	220 210 260 220 280	5·1 8·0 9·5 11·5 12·2		7.5 8.5 6.6 11.0	230 230 250 210 280	6·5 8·6 6·4 10·5 8·8	230 220 250 220 280	5.4 7.4 7.6 10.6 5.5	210 230 190 210 300	4.2 8.9 3.4 11.1 5.9	200 220 200 210 300	4·3 8·4 6·5 13·1 9·0		4.4 9.6 10.5 14.8 12.0	180 210 200 220 300	5·9 14·3 9·6 12·7 10·1	180 210 200 220 300	9·0 12·4 11·5 13·0 10·1	4·8 7·5 10·1 11·9 11·3	6 7 8 9
270 200 280 280	12·6 0·0 5·2 12·7 9·1	270 — 190 280 280	12·1 1·0 5·4 13·5 10·2	270 — 190 280 280	11·4 0·5 6·1 11·0 7·0	330 — 190 280 270	8·6 0·3 5·2 12·5 5·9	330 — 190 280 270	6·9 0·0 3·7 11·8 6·1	340 — 160 280 280	5.0 0.0 4.0 12.5 10.4	340 — 190 270 280	3.6 0.0 3.4 13.5 10.0	340 200 280 310	2·1 0·0 5·9 13·0 6·6	330 	4·1 0·0 5·0 12·6 3·0	340 — 170 280 —	1·8 0·0 3·2 I4·4 1·0	 180 280 	1·2 0·0 3·3 13·8 1·2	330 — 190 280 310	1·6 0·0 4·7 14·6 4·1	6·6 0·3 3·0 11·6 8·5	11 12 13 14 15
220 340 230 330	1·1 5·6 3·8 13·8 12·8	220 290 230 330	0·4 6·8 2·0 12·9 10·6	220 280 240 330	0.0 5.6 2.5 12.8 11.4	220 280 240 340	0.0 4.9 2.1 12.2 8.4	220 270 260 340	0·9 5·5 2·3 12·0 4·2	220 260 280 350	0·5 5·4 3·2 12·0 2·9	220 250 280 350	0·4 4·8 3·6 12·6 3·3	220 240 280 280	1.0 5.5 3.5 13.6 3.9	220 240 280 300	1·1 4·8 3·8 13·0 4·3	180 220 190 280 290	2·4 4·0 3·8 12·0 4·4	180 220 210 280 280	2·8 3·0 5·5 II·5 I·8	200 220 220 280 290	2·9 1·8 6·1 11·2 1·8	1·3 4·4 3·0 9·5 9·8	16 17 18 19 20
230 260 230 270 230	6·3 13·1 6·5 9·1 7·5	240 260 230 270 240	5·5 13·4 7·5 11·0 10·1	240 270 220 270 250	3·8 10·8 8·0 12·0 10·6	270 280 240 250 230	4·1 10·5 8·5 7·9 8·1	270 310 230 260 230	6·0 10·6 10·1 8·1 8·2	280 310 240 260 240	9·5 10·4 11·0 9·0 10·0	280 310 240 270 240	7·1 9·0 10·3 8·0 9·5	290 310 220 270 240	10·8 7·8 10·1 8·5 7·2	280 320 220 270 250	6·5 6·2 10·4 7·6 10·0	280 300 230 260 250	8·8 6·0 10·8 7·2 9·6	290 270 240 250 220	12·8 2·0 12·1 5·4 6·5	270 300 240 250 230	6·5 3·7 10·0 6·3 9·3	5·8 9·7 5·9 8·6 7·9	21 22 23 24 25
270 260 280 260 210	6·8 8·6 5·3 5·0 5·0	260 270 270 270 270 220	5·2 9·1 5·2 5·9 6·0	240 270 280 270 220	5·9 8·0 6·4 6·0 6·2	230 270 270 270 240	4·6 7·9 5·1 5·9 6·5	230 270 280 260 250	6·0 9·0 4·4 3·5 7·2	250 280 270 — 230	6·1 8·5 5·8 1·4 6·2	230 280 250 280 240	5·9 9·5 6·4 3·6 6·3	230 280 240 280 220	6·0 8·4 5·9 5·0 5·0	230 280 230 280 230	7·3 9·4 5·6 3·2 5·6	220 280 210 280 230	5·6 10·1 6·7 4·4 7·6	230 280 230 270 240	5.5 8.3 7.6 2.0 9.3	240 280 240 280 240	6·5 5·9 7·2 4·4 6·0	7·2 8·1 5·8 5·4 5·0	26 27 28 29 30
200	7·0 7·6	200	7.4	230	7·8	230	7.2	230	7.2	230	7.3	240	6.8	220	6.6	230	6.9		7.4	230	6.9	230	6.7	7·9 6·9	‡

February, 1923.

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0	m/s.	°	m/s.	l °	m/s.		m/s.	200	m/s.		m/s.	200	m/s.	210	m/s.	220	m/s. 14·2	230	13.1	230	12.7	250	16.3	11.3	1
220	8.2	210	8.5	210	7.9	210	7.8	2 0 0	8.4	210	9·3		9·5 8·6	230	7.3	210	7.2	210	7.2	230	10.2	230	10.6	9.6	2
220	8.0	240	9.9	230 260	10·4 12·1	230 260	10.1	230 260	9·5 6·4	230 270	6.3	230 270	5.8	260	6.0	190	2.7	210	2.8	240	4.0	250	5.5	8.5	3
250 280	11.7		11.5		1	220	9.4	200	1.2	2/0	0.6	-/-	0.9	180	1.6		1.3	190	3.7	180	3.1	160	2.7	3.2	4
200	3.0	270	2.7	270 200	3.2	200	13.3	200	14.6	200	14.2	180	13.5	180	13.3	180	12.8	190	12.7	190	12.9	190	10.7	12.0	5
200	17.4	210	17.1	200	15 2	200	23 3	200	14 0	200	-4 -	200	-5 -		-3 3				<i>'</i>						_
170	8.8	170	8.0	160	7.2	160	5.5	160	5.6	170	6.1	160	6.5	160	6.5	160	6∙0	160	6.2	160	5.0	170	8.3	8.7	6
170	9.8	190	7.2	200	7.0	200	5·5 8·8	180	7.5	170	5.4	170	5.0	170	5.4	170	5.8	180	5.6	170	4.2	170	4.9	7.4	7 8
250	3.9	270	3.9	250	5.6	270	3.4	240	1.8	_	1.5		1.4		1.5	240	2.8		0.2	-	0.3		0.3	3.5	
160	3.5	150	2.8	150	2.8	100	2.9		1.4		0.6		o·8	120	3.1	130	4.6	140	4.6	130	5.0	130	6.2	2·7 6·4	9 10
140	8.4	150	6.5	150	5.3	140	4.3	150	3.2	140	3.3	140	2.4	130	2.8	110	2.6	110	3.2	110	5.4	120	7.5	0.4	10
				I -								-6-					2.8	200		200	4.7	200	3.4	5.3	11
80	5.2	90	4.6	110	5.9	100	5.7	90	4.6	120	4.5	160	2.6	170	2.6	170	2·8 0·8	200	4·4 2·4	350	3.2	350	1.8	2.8	12
230	1.8	210	2.2		0.1		0.0		0.1		0.1		0.I		0.3	i i		350 130	7.6	130	7.7	120	7.0	5.5	13
130	6.3	130	6.5	130	6.5	130	5·I	130	6.0	120	7°4 1·8	120	7.3	130	7.1	130	7.4 1.0		1.0		1.0		1.0	2.6	14
130	1.0	-	1.0		0.9	-	0.4		0.2	70 110		110	6.8	120	6.3	130	6.7	120	6.5	130	7.7	130	6.9	3.5	15
70	3.0	60	3.9	8o	2.7	011	3.0	100	3.2	110	4.6	110	0.0	120	ν э	130	٠,	120	ر	3-	, ,				
190	3.1	190	4.2	180	2.5	130	3.7	80	2.5		1.0		1.5	150	1.9	130	5.4	120	7.3	110	6.3	100	7.5	3.1	16
110	5.8	110	6.8	120	7.2	110	6.1	110	5.9	130	8.3	120	8.1	130	7.6	130	9.5	130	9.0	130	8.5	140	7.7	8.5	17
140	8.8	140	8.9	130	5.9	110	3.0	130	6.7	140	6.3	140	2.1	100	1.7	_	1.4	60	1.6	_	1.4	90	2.3	7.3	18
50	3.1	50	2.0	40	1.8	50	2.2	50	2.4	-	1.5		1.5		1.4	_	1.3		1.5	50	2.6	50	1.8	2.7	19
140	2.8	150	3.0	140	3.5	140	3.2	130	3.9	140	2.5	130	4.8	130	6·i	140	5.2	130	7.4	140	8·o	140	6.8	3.1	20
•												_	·										0.5	5.0	21
150	6.4	160	3.8	150	3.1	140	2.0		0.3		0.6		0.4		1.0	_	1.0		1.2		0.3		3.5	2.7	22
30	2.9	80	3.1	70	3.3	50	3.7	50	4.3	50	4.9	50	5.0	50	4.2	40	4.0	40	4.5	40	3.9	40 70	3.2	2.4	23
60	3.0	60	2.7	60	2.2	60	2.3	60	3.2		1.1	_	o·8	_	1.4	60	4.2	60	4.3	60	2.9	70	2.8	3.9	24
60	4.4	70	3.3	70	3.7	50	3.1	50	2·I	50	2.7	60	3.3	80	4.2	80	3.1	80	2.2	70	2.0	200	2.4	2.2	25
130	2.1		0.5		0.6		1.4	-	0.4	_	0.1	_	1.0		0.1		0.2	200	3.3	200	2.0	200	- 4	" "	-3
			8.9	T00	6.1	120	6.7	120	7.4	120	8.2	1 720	8.6	120	8.6	1,40	17.2	140	12.5	130	12.3	140	11.2	7.8	26
130	9.7	130 60	- 1	120 70	3.2	140	2.3	140	7.4	130	0.3	130	1.3	130	1.6	140	0.2	140	1.0		0.8		0.9	5.3	27
100	4.4 0.1		3.2	250	2.5	260	3.2	260	2.6	260	2.5	260	3.0	360 250	2.8		0.3	_	0.1		0.4		0.3	2.2	28
	0.1		- 4				3 3				- 3		3 5	250	123	ļ	<u> </u>		-	<u> </u>	·		-	 	
	5.6	_	5.3	-	4.9		4.2	-	4.3	_	4.0	-	4.1	_	4.3	-	4.2	_	4.9	_	5.0	-	2.1	2.3	
	<u> </u>		<u>'</u>	<u> </u>		<u> </u>	·!			Ì		 		<u></u>	<u>′</u>	! -	<u> </u>	<u>. </u>		<u>. </u>				1,,,,	D
I	3. I	I.	4.	I	5.	I	6.	I	7.	13	8.	x,	9.	2	0.	2	1.	2	2.	2	3.	2	4.	Mean	Day.
				j		<u> </u>				<u> </u>		.		I .		i				J		<u> </u>		<u> </u>	<u> </u>

Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$). Speed in metres per second.

183. Eskdalemuir:

Ha (height of anemograph above M.S.L.) = Height of ground above

Day.	1		2		:	3.		4 .		5.	,	5.		7.		3.	ç	9.	1	о.	1	I.	No	on.
1 2 3 4 5	120 190 —	m/s. 0·9 6·0 7·2 0·8 1·5 3·4 8·2	360 110 190 360 190	m/s. 2·1 4·7 5·7 2·3 3·3	360 180 190 360 200	m/s. 2·8 3·7 5·6 4·0 2·8	230 180 360 190 210 210	m/s. 1·4 8·5 5·6 2·8 3·0 3·6	230 180 360 180	m/s. 0·5 6·8 5·8 2·8 3·9 3·7 6·5	220 170 360 200	m/s. 0·5 6·5 5·7 2·8 4·1	220 150 360 190 180 220	m/s. 0·7 7·0 4·3 3·4 5·1 5·4 6·9	220 140 350 190 200 240	m/s. 0·6 5·9 3·5 3·9 7·6 8·6 3·3	210 140 360 190	m/s. 0·3 4·8 2·1 2·4 10·0 7·7 0·8	220 120 360 190	m/s. 0·1 8·4 2·2 4·0 7·9	220 360 190 200 360	m/s. 0·2 8·5 1·5 2·9 8·1	220 130 360 210 200 360	m/s. 0·0 8·6 1·6 3·0 9·4 12·4 5·6
7 8 9 10	210 360 50 70 150	2·8 4·9 3·0	220 350 50 100	3·5 3·5 3·5	350 50 120	7·4 4·5 4·2 2·2	360 30 —	7·3 6·5 4·4 0·9	360 40 —	6·8 3·6 1·4	360 40 —	6·4 3·6 0·4	360 20 	4·1 4·0 0·9	350 10 —	4.2 0.3 4.0	360 20 —	5·4 4·8 o·5	360 40 150	6·0 6·2 3·9 4·9	10 30 150	6·4 5·7 4·4	360 40 150	6·7 5·8 4·9 5·5
12 13 14 15	160 200 — 50	5·1 7·8 0·9 3·6 6·5	160 220 † 50	.5·9 9·2 † 3·7	160 220 † 50	5.4 6.2 † 4.2	160 240 † 60	5·4 6·2 † 5·2 6·4	160 250 † 60	5·0 6·5 † 3·6 4·1	150 260 350 70 340	5·1 2·0 3·6	160 260 † 40	5.9 3.8 1.5 3.8	160 260 20 30 350	6·1 4·2 3·2 5·2	160 40 30	7·3 1·5 5·3 7·0 5·2	170 290 † 50	6·6 5·5 † 7·4 8·2	170 290 † 50	7·1 6·2 † 8·4	160 310 70 50 360	7·0 5·9 5·0 8·6
17 18 19 20	20 20 10 30	5·5 5·0 4·4 2·5	30 30 20 30	9.0 6.4 4.9 5.5 2.8	30 40 30 20 360	7·5 7·3 4·8 4·1 4·5	50 30 30 360	6·5 4·8 5·5 3·5	350 50 30 20 360	6·1 5·0 4·8 4·9	40 20 10 30	3.5 6.5 5.0 3.4 6.4	40 10 360 30	8·6 4·1 4·2 6·4	50 30 350 40	8·0 6·5 5·0 7·6	60 30 350 50	8·5 5·4 6·1 6·5	70 40 30 50	8·2 6·3 6·0 6·6	70 60 40 50	6·2 7·1 6·4 5·3	50 40 40 50	6·1 6·0 7·6 6·0
21 22 23 24 25	360 10 † —	2·6 3·1 3·6 0·5 0·2	350 † † —	3·5 3·0 4·4 1·1 0·3	350 † † —	3·9 2·6 4·0 0·4 0·1	350 † † 360	3·8 2·8 3·8 1·6 0·0	360 † † 360	4.0 2.3 2.8 1.7 0.0	35° † † —	3.0 1.4 0.0	350 360 360 —	2·8 2·1 3·9 1·5 0·0	350 360 360 — —	3·5 2·7 5·1 0·3 0·6	360 360 360 —	4·1 2·8 5·2 0·0 0·3	10 40 † — 150	5·8 5·0 0·0 3·6	20 50 † 150 150	4·6 6·4 3·3 3·5 3·4	30 60 60 210 150	4·8 6·0 3·2 6·0 3·4
26 27 28 29 30	140 170	0·4 0·0 5·2 2·2 0·5	 150 40	0·0 0·4 5·1 1·0	150 160 — 40	0·7 2·9 4·2 0·1 2·2	150 210 —	0·2 3·4 5·5 0·0 1·4	150 190 —	1·0 4·6 0·6 2·0	150 190 — †	0·7 4·5 3·1 0·4 2·1	140 180 —	0·2 4·5 1·9 0·2 2·8	140 180 —	1·2 3·6 2·4 0·1 1·8	150 200 †	0.8 3.8 3.1 0.0 3.0	150 140 240 — 350	5·0 6·0 2·5 0·0 1·8	140 150 230 — 360	5·7 6·5 3·2 0·5 2·5	150 170 230 150	6·0 6·3 2·6 2·6 0·7
31 Mean ‡		3.4		3.9	 	3.6	<u>†</u> —	3.1	† —	3.7		3.4		3.6	-40 	3.9	40	4.0	60 	4.4	60	3.4	90	5.4

184.	Eskdalemuir	:	$H_a =$	235	metres	+	15	metres.
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184. Es	kdaler	nuir :	Ha	= 23	5 met	res +	- 15 r	netre	s.															
1 2 3 4	 	m/s. 0·8 1·0 1·5 0·3 2·5	80 — — —	m/s. 3°3 1°1 1°0 0°2 3°7	70 † —	m/s. 2·6 2·2 0·8 0·3 3·7	80 † —	m/s. 3·0 2·5 0·5 0·5 5·2	90 † — 130 20	m/s. 2·8 3·3 0·5 3·0 5·0	90 † — 130 20	m/s. 3·4 3·5 o·5 5·4 5·5	100 40 — 130	m/s. 5·0 4·4 0·5 5·9 5·4	100 40 — 130 20	m/s. 4·6 3·8 1·0 4·4 5·5	100 40 — 130	m/s. 4·9 4·1 0·4 5·2 5·4	0 100 50 — 140 40	m/s. 3·3 3·6 0·8 6·1 5·0	80 50 150 130 60	m/s. 2·9 4·0 2·5 5·6 5·4	80 60 160 140 60	m/s. 2·9 4·2 2·2 5·0 6·9
6 7 8 9	70 100 340 90 30	5·4 6·9 6·6 6·7 7·6	70 90 40 90 30	6·2 6·7 5·2 6·0 8·7	60 90 40 80 20	5·5 5·6 5·2 4·2 10·0	60 90 50 60 20	5·0 5·9 6·8 4·0 9·4	70 90 60 70 20	4·9 5·6 6·6 5·1 8·3	80 90 70 60 30	5·4 4·5 9·0 5·4 7·1	80 60 60 60 30	7·3 2·8 5·4 6·0 7·0	90 60 70 80 20	8·0 4·5 6·4 6·5 5·4	90 70 90 70 30	8·5 6·0 8·5 8·2 5·4	90 90 110 80 50	8·0 5·6 10·4 8·7 5·6	90 90 100 70 50	8·5 5·5 8·6 9·0 6·4	100 80 90 70 80	9·2 5·8 10·5 9·4 5·5
11 12 13 14 15	70 20 250 30 360	7·4 3·9 3·7 4·3 2·5	70 20 230 40	7·4 6·6 1·7 3·7	† 40 210 40	9·1 9·7 0·9 4·9	† 40 210 20	7·5 9·2 1·3 4·3 1·0	† 40 210 20	7·4 6·6 2·4 5·1 1·1	† 30 — 10	6·3 6·1 0·4 4·8	130 20 200 200 50	3·5 4·7 5·7 5·1 3·0	140 20 200 30 40	2·5 5·0 4·4 5·8 4·8	140 30 200 30 50	3·2 4·8 3·9 7·8 5·5	130 40 190 40 100	3·0 † 5·8 6·9 6·5	† 40 200 40 100	2·0 5·6 6·8 6·1 6·8		1·1 4·6 8·2 6·0 6·4
16 17 18 19 20	† <u>-</u> 70 <u>-</u>	2·9 0·8 1·4 4·3 0·8	30 60 	4·4 0·9 0·8 5·1 0·7	30 — — 40 —	4·4 0·8 0·8 6·0 0·5	30 — 60 —	4·7 1·1 1·5 6·0 1·2	60 30	4·1 1·0 1·5 4·4 3·0	30 — 60 —	4·1 1·2 1·5 5·1 1·3	40 30 60 60	4·6 0·8 2·8 4·3 2·0	60 90 40 50 50	3·0 3·3 3·2 5·8 5·9	50 110 40 50 60	2·8 6·2 3·8 7·5 7·3	50 120 80 70 50	3·2 6·3 5·4 7·8 7·5	60 120 100 60 50	3·6 6·5 6·0 7·3 7·3	50 120 110 50 40	4·6 6·4 6·5 7·3 7·8
21 22 23 24 25	20 20 — 350 170	6·6 9·9 o·6 † 7·5	20 30 230 340 180	5.0 7.8 3.6 † 8.6	20 30 250 340 180	6·7 9·0 2·2 † 5·8	30 — 330 180	9·0 8·5 0·5 5·6 5·0	60 30 250 330 180	10·1 7·5 2·5 1·9 4·2	20 30 — 350 180	9·4 7·0 0·6 3·2 4·5	20 30 — 360 200	9·6 7·0 1·1 5·6 9·6	20 30 230 360 220	9·4 7·6 2·0 5·6 10·8	20 30 340 350 230	9·2 7·5 4·4 3·4 9·9	20 30 20 30 230	10·0 7·8 6·4 2·3 8·9	20 40 20 †	7·7 7·8 †	20 40 30 † 200	13·1 6·5 8·8 † 10·6
26 27 28 29 30	220 320 — 230 180	7·9 4·9 0·4 3·2 3·6	220 320 — 220 180	8·9 2·5 0·4 2·4 2·9	220 — — 240 —	10·5 0·8 0·4 3·1 0·7	220 — — 250	9·2 0·4 0·2 3·8 0·3	220 — — 250 230	8·5 0·3 0·2 2·5 4·0	250 — 240 230	6·0 0·3 0·4 3·1	260 — — 260 240	5·0 0·5 0·4 3·9 10·5	260 — 190 250 240	5·5 1·0 2·6 6·0 9·9	270 330 200 240 230	6·8 2·5 6·0 5·2 10·0	270 240 220 270 230	6·8 3·5 5·7 5·7	270 230 210 270 240	8·5 6·1 6·5 5·9 10·0	280 210 210 260 240	8·7 7·1 8·7 6·5 9·1
Mean §	_	4.1		4.0		3.8		4.0	-	4.2	_	4.3		4.7		5.2		6.0		6.2	<u> </u>	6.6		6.9
G.M.T.		ī.	2	z. /;	:	3.	4	1		5.	6	5.	,	7·	1	8.	ç). \	I	10.	1	· .	No	oon.

Averages for periods of sixty minutes, centred at the exact hours, Greenwich Mean Time.

M.S.L. + ha (height of anemograph above ground) = 235 metres + 15 metres.

March, 1923.

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I	3∙	1.	4.	I	5.	1	6.	1	7.	1	8.	1	9.	2	о.	2	I.	2	2.	2	3.	2.	4.	Mean	Day.
210 — 40 220	m/s. 0·4 8·1 1·4 1·6 8·8	220 360 — 240	m/s. 0·1 8·8 2·0 1·2 9·9	° — 200 — — 240	m/s. 0.0 9.8 1.1 1.4 11.1	200 360 50 240	m/s. 0·1 9·6 1·6 2·4 11·8	200 350 250	m/s. 1·5 8·7 1·8 1·3 12·4	180 190 — — 270	m/s. 3·1 8·8 0·7 1·1 11·9	180 200 — — 270	m/s. 2·5 9·2 0·5 0·5	° — 200 — 270	m/s. 1·1 9·5 0·2 0·2 9·8	150 210 — — 270	m/s. 1·6 9·5 1·1 0·2 10·0	° 100 200 — — 250	m/s. 2·8 7·6 1·3 0·2 6·0	90 200 350 —	m/s. 1·6 7·8 2·7 0·1 3·8	110 200 350 — 180	m/s 5·6 7·5 1·8 0·1 3·5	m/s 1·2 7·6 2·9 1·9 7·3	1 2 3 4 5
210 10 360 60 150	11·2 5·9 5·5 5·5 5·1	210 10 40 50 160	10·2 5·6 6·7 5·5 5·5	220 360 40 70 150	7·9 5·7 5·6 4·4 4·6	220 360 50 60 140	6·1 5·5 5·9 4·4 4·0	220 360 40 — 130	5.0 5.4 5.5 0.5 4.5	210 360 40 —	5·5 3·9 5·3 1·4 4·8	210 10 50 60 130	4·1 3·6 5·4 1·6 4·5	210 10 50 —	3.0 5.1 0.8 4.0	220 10 50 — 150	6·6 4·4 5·2 0·5 2·7	230 10 40 50 160	6·0 2·8 5·6 1·7	210 10 30	4.7 2.7 5.4 0.8 0.5	210 	7.0 0.8 1.6 1.6 1.2	6·4 5·0 5·3 3·4 2·9	6 7 8 9 10
150 160 320 50 40	6·4 7·6 5·3 5·4 8·7	140 160 330 60 40	5·6 6·4 5·1 5·0 8·9	150 170 340 60 40	5.0 6.8 3.8 6.4 9.3	150 170 340 80 30	5·5 5·8 3·0 6·3 8·1	140 160 320 80 30	4·9 6·5 3·8 4·4 6·8	150 160 340 100 30	3·9 5·3 2·0 4·1 6·1	150 160 360 80 30	4·6 6·4 2·4 1·8 5·9	150 170 360 70 20	4·7 9·3 3·6 7·0	140 170 360 50 20	4·6 8·0 2·9 2·7 7·3	150 190 — 50 10	4·3 10·4 0·4 3·7 6·6	160 200 - 50 20	5.0 10.3 0.4 3.6 6.9	150 200 — 50 20	5·3 8·4 0·9 3·7 6·5	4·4 6·7 4·4 6·3	11 12 13 14 15
360 60 40 50 80	6·4 7·4 5·1 7·0 6·4	360 80 50 50 80	5·7 8·2 5·4 7·4 5·8	50 90 60 50 70	6·6 9·2 6·0 8·6 6·5	50 50 70 50 70	5·5 6·0 6·3 9·1 7·0	20 360 50 40 40	4·0 4·4 4·8 7·9 6·6	360 50 30 20 60	4·4 4·5 4·0 5·1 6·6	60 40 40 30 40	7·4 3·2 3·4 6·1 2·1	60 360 40 30 40	3·9 2·3 2·6 7·0 3·6	40 40 20 20 50	4·I 4·0 2·7 4·6 3·5	40 20 20 50 50	6·8 4·9 2·8 4·1 2·9	20 10 50 340	1·3 4·7 4·0 3·9 1·5	30 20 20 20 20 360	2·5 4·0 5·0 3·6 I·I	5·5 6·1 4·9 5·8 4·9	16 17 18 19 20
50 60 70 210 190	4·8 5·2 3·0 6·1 7·9	50 50 70 210 200	4·4 6·4 2·4 7·1 9·6	60 50 70 220 200	3·8 4·9 2·4 5·5 12·8	50 40 70 270 190	5·1 5·5 2·4 5·1 11·6	40 40 60 230 200	4·2 5·4 4·1 5·6 8·5	360 40 50 220 190	3·0 2·0 3·2 4·9 6·5	360 360 30 230 190	3·6 3·6 2·7 5·5 4·6	360 360 20 230 200	4·0 6·1 4·3 1·6 4·4	360 360 360 140	3·2 4·6 4·1 1·7	20 360 360 —	4·4 3·8 3·4 0·5 0·8	40 † 360 —	4.4 4.8 2.0 0.5 0.2	20 † 340 —	4·4 3·4 2·1 0·0 0·2	3·8 4·1 3·5 2·6 3·3	21 22 23 24 25
140 200 220 160	5·9 5·0 3·0 3·5 0·2	140 190 210 150 70	5·8 4·4 4·8 3·5 1·6	140 160 200 170 200	6·4 3·9 5·8 2·8 3·5	140 150 210 120 190	4·6 3·7 4·9 3·7 2·9	140 140 200 100	3·0 3·9 3·7 4·2 0·5	130 150 — 70	3.2 5.1 0.8 1.8 0.1	130 140 200 30	3·I 3·0 I·6 I·8 0·2	130 140 180 —	2·2 5·2 2·0 I·2 2·0	130 140 — — 10	2·0 7·0 0·7 1·5 1·8	140 	1·0 5·0 1·0 1·3 0·8	140 — — —	0·7 4·5 0·4 1·5 2·0	- 140 - †	1·1 4·8 0·6 1·0 2·0	2·5 4·1 3·1 1·5 1·6	26 27 28 29 30
140	3·2 5·4	110	3·6 5·6	90	5·0 5·7	110	5.4	100	5·5 4·8	90 —	4·1	80 —	5·4 4·0	100	4.0	90	3.9	100	3.0	_	3 ·o		2.9	3.4	31 ‡

April, 1923.

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0	m/s.	°	m/s.	°	m/s.	°	m/s.	0	m/s.	0	m/s.	°	m/s.	°	m/s.	°	m/s.	°	m/s.	°	m/s.	ľ	m/s.	m/s.	•
90 60	4.0	110	3.2	120	3.4	130 80	2.4	170	1·6	170 80	2.2	 80	1.5		0.5	_	0.6		0.5	20	1.8	20	1.2	2.2	I 2
160	5·5 3·2	70 160	5.3	70 140	4·5	150	3.5	90 150	1.6		0.7		2.5	_	0.5		0.1		0.8		0.5		0.7	$\begin{bmatrix} \tilde{1} & \tilde{3} \end{bmatrix}$	3
150	5.0	140	4.8	150	3.5	140	4.6		1.0		0.8		1.4	140	1.6		1.5		0.5		0.4		1.0	2.8	4
60	6.8	70	7.7	80	6.0	60	8.3	60	8.5	60	8.1	60	7.8	50	5.7	40	4.5	50	6.4	70	6.6	80	5.0	5.8	5
1		l '	' '	1									'	J -	,	1	" "]		1		l	_		-
100	9.1	100	7.9	100	8.8	100	7.9	100	7.7	100	6.8	100	7.5	90	6.9	90	7.0	90	6.8	90	6.6	90	6.5	7.1	6
80	6.5	70	5.9	50	5.8	60	6.0	50	6.6	40	6.9	40	7.6	40	5.4	340	5.4	360	5.6	10	5.0	†	5.3	5.7	7
90	12.0	100	10.4	90	11.4	100	11.0	90	9·I	80	9.6	80	9.5	70	6.0	70	7.0	70	7.2	80	6.8	90	7·5 7·8	8.1	8 6
70	9.0	60	9.3	70	9.8	60	9.5	60	8.7	60	8·4 6·1	50 80	5·6 2·8	30	5.8	30	6.1	20	7·2 6·5	30 80	7·6 7·5	30 70	6.3	7·2 6·5	10
120	6.4	140	5.1	140	4.9	120	5.2	110	6.5	110	0.1	80	2.0	70	5.2	70	5.9	90	0.3	- 60	1.3	,,,	ر ک	ľ	10
	1.5	_	1.2	_	0.5		1.3	10	3.3	50	5.6	30	4·1	50	4.7	50	4.6	l t	3.0	l †	2.3	20	3.2	4· I	ΙĪ
40	5.0	100	3.7	l —	0.7	_	0.0	 	0.9		1.3		0.0		0.9	60	3.3		1.5	230	2.2	230	2.2	-	12
200	9.0	180	7.4	160	4.4	150	4.4	140	3.2	120	3.1	20	5·1	20	7.0	20	5.9	30	4.5	30	5.4	30	4.5	4.5	13
50	6.0	50	7·I	170	9.1	160	7.4	160	4.6	160	4.8	190	2.8	210	4 · I	l —	1.5	_	0.6	-	1.1	360	2.1	4.9	14
130	6.6	130	5.8	70	5.6	30	5.9	70	6.6	70	6. I	60	3.8	80	4.0	40	4.6	Ť	5.3	1	4.1		1.0	4.3	15
50	4.0	50	4.8		1	60	2.7	70		80	6	00	2.7	- 00	2.8	l	0.1		1.4		0.7		0.5	3.4	16
130	4·9 5·0	50 110	5.0	40 110	4.0	120	3·1	70 120	4·4 5·2	100	4·6 4·8	90	3.7	90 40	1.6	_	1.5		1.5		1.5	30	1.6	3.1	17
90	5.9	90	5.4	80	5.0	90	6.2	90	4.7	80	5·I	80	4.9	70	5.6	70	5.8	70	5.4	70	5.0	70	4.4	4·1	18
60	6.7	70	6.7	70	7.5	60	8·1	60	8.1	50	8.0	. 50	8.0	60	6.4	60	3.0	<u> </u>	0.8	<u> </u>	1.1	<u> </u>	0.0	5.7	19
40	7.2	40	7.4	40	8.1	40	8.8	40	8.2	30	7.3	30	7.0	30	6.3	30	7.1	20	6.5	20	5·1	20	6.3	5.3	20
		Ι.						l	}							l	}	ŀ					8.0	10.3	21
50	13.5	†	12.0	40	12.6	40	14.1	40	12.5	40	11.4	40	II.I	30	10.6	30	10.9	30	11.6	30	9.7	30	0.6	5.8	22
40 20	6·0 7·8	30 20	5·1	40 20	5·1	50 30	4·9 6·8	70 20	4·8 5·6	70	1.6	-	0.6	260	0.6	<u> </u>	0.2	360	0.4	360	0.4	360	+	<u> </u>	23
220	1.0	220	5.6	230	5.7	220	6.7	210	6.7	30 200	3·6 5·8	20 190	2·5 4·8	360 180	2.7	180	4·I 4·0	180	4.1	170	6.4	170	7:7	- 1	24
200	9.0	210	8.9	200	8.9	190	9.0	200	7.9	200	7.4	200	7.0	200	8.9	200	8.3	220	6.6	220	6.0	220	8.0	8.0	25
	1	l		I			_				′ ~		′				-	1							
290	8·o	280	9.2	300	7·4 7·8	310	6.7	320	8.9	320	10.4	330	9.0	320	7.4	320	8.5	320	7.0	330	8·o	310	8.1	8.0	26
220	7.0	220	7.7	210	7.8	230	8.5	220	6.8	220	6.2	240	5.3	240	4.0	250	4.1	260	2.8	260	1.7	-	0.2	4.0	27 28
210	8.6	220 260	7.5	220	7.8	220	6.6	240	6.3	260	5.9	270	5·1	270	6.2	260	4.0	250	2.4	270	1.8	180	1·5 4·8	4.8	20 29
270	7·0 8·5	200	6·3 8·3	270 220	5·9 9·4	270 220	6·0	260 220	5·9	240	8.8	240	5.2	220	4.2	220	3.0	190	4.0	190 240	9·0	250	12.0	7.7	30
	0.3		- 3		9 4	440			0.1	220	0.0	220	10.2	220	10.1	220	6.6	230	7.0		9 5				
-	7.0		6.6	_	6.5	_	6.5	_	6.0		6.0		5.3		4.9	_	4.4		4.2	-	4.1	_	4.1	5.2	§
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13	3.	14	J	1	5.	16).	1	7. ઁ	I.	8.	19	9.	2	0.	1	21.	2	2.	2	3.	1 2	4.	Mean	Day.
				J				l				1		ļ		l		1		l		<u> </u>		<u> </u>	

Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$). Speed in metres per second.

185. Eskdalemuir:

Ha (height of anemograph above M.S.L.) = Height of ground above

Day.	I	•	2	2.	3		4	•		j.	6	5.	7	'.	8	3.	9		10.		11	t.	No	oon.
	10	m/s.	0	m/s.	0	m/s.	•	m/s.	0	m/s.	0	m/s.	0	m/s.	•	m/s.	0	m/s.	0	m/s.	0 1	m/s.	۰	m
1	250	12.4	250	10.4	240	10.4	240	9.8	240	10.8	240	11.3	240	11.0	230	8.0	230	7.5	230	8.6	230	7:5	230	8
2	-30	0.0	-5-	1.2	260	4.2	240	1.8	200	2.1	<u>.</u>	0.7	260	3.4	280	5.0	270	3.5	270	3.0	270	2.4	-	I
3	360	1.6		0.8		0.4		0.3		0.3		0.3		0.6	210	2.8	210	3.3	240	4.6	240	5.2	220	6
4	1300	0.1		0.1		0.1		0.1		0.1	240	2.8	220	4.0	200	3.1	200	3.8	220	7.2	210	8·5	220	9
5	200	4.5	200	3.9	200	3.7	210	3.5	210	4·I	210	6.0	210	8.4	210	8.6	210	6.8	210	6.1	200	7.4	210	8
										0.6	200	2.4	250	4.7	240	T	270	F.6	270	2.2	260	5∙0	240	6
6		0.4	-	0.6	_	0·6 0·8		0.2	_	0.6	200	3.4	250	4.1	240	2.1	270 260	5.6	270 260	3.2			240	7
7 8	270	2.5		0.2				0.5		0.5	T-00	1.1		1.5	250 220	6·1		4.4 6.0		4·7 6·5	250 260	5·5	270	5
-	240	5.8	240	5.1	240	5.7	240	5.8	220	5.8	190	4.9	210	5.0	l .		230 190	1.8	250	0.6		0.5	300	5
9		0.4		0.3		0.3		0.3	_	0.8		0.4		0.3	280	0.3	260		270	6.8	250			7
10	350	6.6	340	6.4	330	7.1	320	5.7	_	0.8	310	2.9	290	2.7	200	4.8	200	5 2	270	0.0	250	7.5	240	1
11	250	7.5	300	8.4	300	9.0	300	6.9	300	4.9	300	4.9	330	5.5	340	8.4	340	8.6	330	9.5	340	9.6	340	10
12	300	7.9	290	8.6	290	8.4	280	6.5	290	6.9	280	8.4	280	9.6	280	9.9	300	10.0	290	8.9	280	8∙0	280	17
13	210	6.3	210	6.5	210	6.7	220	6.7	230	6.5	240	5.1	240	4.1	250	3.3	300	3.1	330	2.6	340	2.9	340	3
14	290	6.5	290	8.7	290	8.4	300	5.9	<u> </u>	1.5	190	2.2	220	3.6	220	6.4	220	8·1	220	8∙0	220	9.0	220	10
15	230	4.2		1.0	_	0.9	_	1.0	_	0.4		0.4	- 1	0.2	_	0.6	220	3.3		0.3	_	0.6	180	13
16	330	2.8	330	3.5	350	5.7	350	5.5	340	6.3	330	6.7	320	7.2	310	5.5	330	4.0	330	5.7	320	6.2	310	1 2
17	320	4.6	290	5.0	300	5.6	280	2.7	300	4.5	300	6.8	300	9.7	290	12.1	290	10.1	290	14.4		13.1	290	12
18	3	0.5	350	2.3	350	2.6		1.0		0.5		0.7	310	1.7	290	3.8	290	2.8	290	3.4	280	3.5	270	1 4
19	250	5.6	240	6.0	240	6.0	230	6.0	230	6.5	230	6.7	220	6.3	230	5.0	220	5.0	230	6.8	250	5.4	260	1 :
20	220	5.7	220	7.3	230	7.4	230	7.3	230	6·0	230	6.6	210	7.6	210	7.8	210	9.7	220	9.5	220	9·i	220	10
21	270	8.9	270	9.0	270	12.0	270	9.7	240	4.8	230	4.4	250	5.0	260	6.1	270	7.2	270	8·o	270	8.5	270	1 8
	2/0	1.1	2/0	1 -	2/0	0.3	2/0	1.1	-40	0.2		0.5		1.4	50	2.4	60	2.4		1.0	50	2.8	50	
22	50	1.8	1 40	0.4		1.3	30	2.5	50	3.2	40	3.0	30	4.5	30	3.4	30	2.4		0.8	180	2.2	40	1
23	1 -	1	40	1		0.5	30	0.4		0.3	4	0.4	300	3.0	290	4.7	280	5.1	270	6.6	260	7.8	270	1 8
24 25	250	5.9	260	5.6	270	5.2	250	6.1	260	4.9	300	5.0	340	5.8	350	6.1	350	6.5	350	6.2	350	6.5	360	
-	*	_		-		-		0.5			265		266		260		260	7.6	360	7.4	250	8.0	360	
26	350	8.1	350	9.5	340	8.0	340	8.0	350	10.6	360	10.I	360	9.4	360	7:4	360	7·6 8·4		7·4 8·4	350	Į.	, ~	
27	30	4.1	30	4.6	30	5.0	20	4.0	20	4.9	30	5.2	40	6.5	40	7:3	40	9.8	40	12.1	30	7.7	40	10
28	20	5.3	30	7.4	20	7.5	20	7.9	20	10.2	20	9·I	20	9.4	30	9.6	30	-	40	8.3	40	8.4	40	18
29	30	7.9	30	5.4	30	6.6	20	5.6	20	5.6	40	7.1	30	7:4	30	6.9	40	7:4	40		40	6.4	40 60	16
30	20	3.5	20	3.3	20	3.8	30	4.1	30	3.7	30	5.0	40	6.7	40	7.2	50	7.4	70	7.3	50	0.4	"	1
31	20	2.5	20	2.0	30	2.5	30	2.5	30	2.9	20	3.8	20	4.1	30	4.8	30	6.1	30	6.7	40	7.0	40	-
Mean.		4.4		4.4		4.7		4.2		3.9		4.4		5.1	_	5.7	_	5.9		6.2	_	6.5	_	

186 Fekdalemuir: $H_a = 235$ metres ± 15 metres

186.	Eskdalo	muir	: n	a = 2	oo me	erres -	+ 13	metr	es.															
ı .	40	m/s. 6·o	30	m/s. 4.9	40 40	m/s. 5;3	40 40	m/s. 6·2	40	m/s.	30 †	m/s. 7·0	30 20	m/s. 5·9 3·1	40 30	m/s. 4.5 2.5	40 40	m/s. 5·5 2·1	40	m/s. 6·4 1·5	40 120	m/s. 7:3 1:6	30 120	m/s. 5·6 2·0
2 3 4 5	20	5·0 0·5 6·2 3·0	20	0·5 5·5 3·1	† 20 †	0·2 5·4	20	4·6 0·3 5·2	† 20 †	4·4 0·3 7·9	- - +	3·4 0·4 6·1	280 20 180	2·9 7·2 3·6	260 10 200	3·8 7·1 4·7	240 30 200	3·0 6·7 4·7	280 30 230	4·6 5·2 5·7	300 360 210	8·6 4·1 7·5	290 350 240	3·8 7·1
6 7 8 9	310 270 210 230	5·7 3·9 12·4 10·9	300 260 200 230	4·0 3·8 12·0 12·4	† 240 190 230	3·8 2·1 11·1 15·0	240 200 220	0·6 1·6 11·5 14·4	† 240 190 230	2·1 3·3 11·3 14·5	50 230 200 220	2·9 2·9 11·4 15·1	60 260 200 230	2·5 3·4 12·7 13·5		3·5 2·5 12·2 12·8	40 250 200 240	3·0 3·4 15·1 10·7	† 270 200 240	1·8 5·2 16·4 11·6	230 240 200 240	3·6 5·6 15·0 10·0	210 220 210 230	3·2 7·0 15·3 9·9
10 11 12 13 14 15	270 270 240 290	5·6 5·5 8·8 2·9	270 270 270 250 300	6·7 5·0 6·4 6·2	280 270 260 310	7·7 4·8 6·6 6·4 0·6	220 290 240 270	8·0 4·3 9·4 0·8	290 210 270 280	10·9 4·1 10·6 1·8 0·4		11·5 6·4 10·8 7·4 0·4	290 230 270 350	12·3 10·1 6·8 13·9 6·3 0·6	300 210 270 340	14·4 10·0 8·5 15·1 5·9 1·5	310 210 270 350 210	15·2 10·5 8·9 12·8 5·1 3·1	310 210 270 340 210	15·1 10·6 10·7 11·2 4·6 3·3	310 220	9·9 11·7 13·0 3·9 4·2	310	8·5 11·5 11·8 4·4 4·1
16 17 18 19	30 190 290 350	6·2 0·1 2·4 10·0 7·1	40 180 310 350	5·7 o·1 4·3 8·0 5·9	† 210 330 350	5·2 0·2 6·1 2·9 5·0	† † 210 320 350	3·4 2·1 4·9 1·6 2·8	† 210 300 350	2·0 0·5 3·5 5·5 4·0	† 210 330 350	4·1 1·0 4·3 7·1 3·8	360 30 200 310 340	4·6 2·5 5·2 9·1 5·1	10 30 200 310 330	5·1 2·6 3·5 10·6 6·1	20 — 250 300 340	5·0 1·0 3·9 8·5 6·9	10 240 310 320	3·6 1·5 4·6 10·0 4·9	† 260 250 290 290	3·5· 2·2 3·6 9·7 5·1	† 250 260 300 300	2·7 2·9 3·6 8·6 5·0
21 22 23 24 25	180 260 250 240 280	3.0 8.1 † 7.5 2.8	160 270 250 240 280	5·4 9·1 † 5·4 3·8	240 270 220 210 280	4·7 8·5 † 2·8 3·4	250 270 230 170 280	2·5 9·0 † 3·7 2·8	250 270 230 200 280	5·8 10·1 † 3·2 1·6	260 280 230 240	7.0 12.1 † 5.0 1.5	230 270 230 250	6·2 10·7 4·6 3·5 1·1	240 270 250 260	5·5 9·9 4·9 4·9 0·5	250 270 250 270	5·2 10·8 6·6 4·6 1·2	250 270 260 260 290	4.6 10.2 6.5 4.6 2.0	260 270 260 260 —	4·4 9·8 5·8 5·3 1·5	260 270 250 260 270	5.4 11.0 7.3 5.5 2.5
26 27 28 29 30	330 - 270	0·6 0·2 2·1 0·3 3·4	 270	0·4 0·3 0·9 0·1 5·4	 280	0·8 0·4 0·5 0·0 5·3	300 290 280	1·9 0·3 1·8 0·0 5·5	330 260	0·9 0·3 1·9 0·0 4·6	320 240	0·2 0·2 3·3 0·0 4·5		0.6 0.6 1.3 0.0 4.9	350 — — — 210	2·9 0·2 0·7 0·6 6·2	350 320 250	2·5 0·5 3·4 1·5 5·8	60 † 250 130 260	3·5 1·7 † 3·4 5·7	40 280 230 200 270	1·8 1·7 † 4·1 5·5	20 280 250 210 270	1·9 4·7 4·7 4·4 6·1
Mean ‡	_	5.0		5.0		4.7		4.2		4.7		5.3		5.7		6.0		6.0		6.3		6.4		6.6
G.M.T.	. ,		<u> </u>	2.	3	,	4		5		6		7		8	j.	9		10	о,	1	1.	No	on.

[†] Defective record

[‡] Mean for 25 days only, omitting the 2nd, 5th, 22nd, 23rd and 28th.

Averages for periods of sixty minutes, centred at the exact hours, Greenwich Mean Time.

M.S.L. $+ h_a$ (height of anemograph above ground) = 235 metres + 15 metres.

May, 1923.

I	3.	I	4.	I	5.	1	6.	I	7.	I	8.	I	9.	20	о.	21	τ.	2	2.	2	3.	2	4.	Mean	Day.
230 230 220 210 210	m/s. 8·3 4·1 6·8 9·1 8·2	230 250 250 250 200 210	m/s. 11·3 3·9 6·5 8·9 8·7	230 50 230 210 210	m/s. 10·0 5·8 7·0 9·0 6·5	230 50 220 220 210	m/s. 10·9 5·0 7·2 10·0 5·4	230 40 220 220 210	m/s. 12·0 6·5 7·5 10·1 5·1	230 50 210 220 200	m/s. 10·9 7·3 5·8 9·4 3·0	230 40 200 220 240	m/s. 8·6 6·8 5·7 8·5 2·8	230 360 230 210 270	m/s. 9·0 3·4 2·0 4·6 2·5	230 340 — 200	m/s. 9·2 2·5 0·3 3·4 0·4	230 350 — 200 —	m/s. 8·7 2·1 0·5 3·4 0·3	240 360 — 200	m/s. 7·4 2·2 0·2 5·1 0·3	240 360 — 200	m/s. 4·I 1·6 o·I 5·5 o·5	m/s. 9·6 3·4 3·2 5·2 4·9	1 2 3 4 5
240 230 270 310 220	7·2 7·2 7·3 2·2 10·0	250 220 270 310 210	7·8 7·0 7·5 4·7 10·1	250 240 280 320 210	9·0 6·4 7·4 5·4 12·3 9·0	270 270 280 340 210	7.5 6.3 6.8 5.2 15.5	270 230 280 360 200	6·3 6·1 6·5 4·5 13·3	270 230 280 20 210	6·2 8·4 6·9 6·1 12·9	270 240 280 360 250	6·0 7·0 6·1 7·5 10·1	260 240 290 360 260	7·7 5·0 4·1 7·5 7·8	260 240 290 360 240	5.6 3.3 9.5 10.5	260 240 — 360 220	1.7 5.9 0.6 10.8 9.0	240 	0·9 5·6 0·8 10·2 8·6	250 240 — 360 230	3·2 4·5 0·5 9·6 10·2 8·5	4·3 4·5 5·4 3·7 8·1	6 7 8 9 10
280 340 220 140 310	8·0 4·4 9·7 4·0 7·5	290 320 210 190	7·5 5·0 9·7 4·5	290 310 200 200	9·4 6·0 10·0 5·5	280 310 190 240	9·9 6·3 10·0 5·4 7·1	270 300 210 240	9·6 3·1 4·4 6·6	270 310 200 260 290	8·3 6·6 3·1 8·9	270 320 180 270	7·7 3·7 6·2 2·0	260 300 190 —	7·4 4·6 5·6 0·9	270 320 190 —	6·4 2·8 4·5 0·4 5·1	240 320 — — 290	4·4 6·8 0·9 0·4 6·0	210 300 — — 300	4.6 6.1 0.6 0.3	300 210 —	6·5 6·0 3·2 0·5	8·0 4·8 6·5 2·0 5·8	12 13 14 15
280 260 270 220	3·5 6·1 9·2 7·6	290 270 270 230	11·4 4·4 6·9 9·3	280 270 270 230	9·8 5·8 6·3 9·4 6·6	280 270 270 230	9·4 5·4 6·3 8·9 7·9	280 270 270 230	8·3 6·3 5·3 9·3	280 270 250 260	8·0 3·8 5·4 7·8	280 270 260 260 260	8·1 5·0 6·4 6·2 5·1	280 280 270 260	8·4 8·7 6·5 7·3	280 250 270 260 270	6·6 3·7 5·6 7·7	310 230 270 260	5.5 2.6 5.8 6.2 4.9	290 200 240 270	5·1 2·0 4·7 7·5	250 210 270	0·9 4·3 5·2 8·6	8·2 3·4 5·9 7·9 6·6	17 18 19 20
40 80 270 360	5·8 2·5 8·5 6·0 8·4	50 360 260 360 360	6·7 4·6 10·6 6·0	50 60 250 350	5·9 4·0 10·5 5·9	60 70 220 350	5·4 3·4 9·1 8·3	60 250 360	5.4 1.5 9.7 8.7	80 — 230 350 40	5·6 0·3 10·2 8·4	80 — 230 360	3·5 0·5 10·1 9·9 5·6	90 — 230 360 30	i·8 o·5 io·4 8·5	50 — 240 360	2·5 0·4 10·5 6·9	60 — 260 340 30	2·8 0·5 9·5 6·6	30 260 340 30	1·9 0·3 8·1 8·1	30 — 260 340 20	1·7 0·3 6·0 8·6	2·8 2·1 6·2 6·7	22 23 24 25
40 30 40 70	8·9 11·4 9·4 6·2	40 40 40 80	8·4 9·5 9·3 4·9	30 40 40 80	9·2 10·2 8·5 5·1 6·5	40 30 40 70	10·7 11·0 7·4 5·5	30 40 50 90	9·9 13·0 7·2 5·1	30 40 50 60	9·2 14·4 6·7 5·0 6·8	30 40 40 60	8·8 14·5 6·2 5·1	40 40 40 60	8·3 11·3 5·0 5·0	30 30 40 50	9·4 5·5 4·2	30 30 40 30	7·7 8·3 4·4 3·4	30 30 20 30	7·2 8·1 3·9 3·1 5·0	20 30 20 20 20	6·1 9·9 4·5 2·6	7·4 9·9 6·9 5·0	27 28 29 30
	7:3	_	7.6	_	7:4	 -	7.7		7.4	-	7.0	_	6.6		5.9	<u></u>	5.2		4.9		4.2		4.2	5.8	

June, 1923.

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°	m/s.	°	m/s.	ľ°	m/s.	l °	m/s.	ľ	m/s.	°	m/s.	l °	m/s.	ı °	m/s.	l °	m/s.		m/s.	l °	m/s.	l °	m/s.	m/s.	
30	5.5	50	5:8	50	5.9	40	5.3	40	5.2	50	5.0	40	4.6	40	3.0	30	3.4	Ť	4.2	l İ	4.0	1 !	5.0	5.4	I
170	2.1	200	3.4	10	2.8	160	3.5	220	5.6	210	4.7	260	4.1	I —	0.8		0.2		I.I	†	3.0	Ţ	1.7		2
280	9.1	300	7.6	270	8.4	270	9.6	280	9.0	290	9.4	300	10.2	300	10.2	300	7.0	320	5.9	320	5.6	360	3.8	5.2	3
340	3.3	30	2.6		1.0	50	1.0	_	0.0	_	0.5		0.4		1.1	40	2.9	Ť	3.4	†	3.0	Ţ	3.1	3.9	4
240	6.3	250	5.0	260	2.1	270	6.8	270	9.3	280	13.0	290	13.4	290	10.0	280	9.8	300	8.3	300	8.5	300	7.2	_	5
				262		200		280	66	250	- 0					202		280		270	8.5	280	6.9	4.5	6
200	4·I 8·4	250	3.2	260	9·1	280	7.0		6.6	270 210	5.8	270	5.0	270	5.2	280	7·0	200	7·0 8·4	270 210	9.8	210	11.6	6.1	7
200		220	9.0	210	13.0	200	9.1	210	9.7	220	13.1	210	7.1	200	5.6	190	11.1	220	11.1	230	12.6	230	12.0	12.8	8
220	14·5 9·0	210	9.0	210	9.3	210	8.8	200	8.7	200	10.1	200	13.1	230	8.9	230 190	10.1	190	10.8	200	10.3	190	11.6	11.2	9
230	14.8	250	14.8	240	17.1	250	17.6	250	18.0	260	17.3	270	14.4	250	11.0	270	9.9	260	8.4	260	7.0	270	5.5	13.1	10
230	-40	250	14 0	-40	., -	250	., 0	2,50	100	200	17 3	-/-	** *	250		1 2/0	99	200	. 4		' "	-/-			
300	8.6	300	7.6	290	8.8	280	9.0	280	7.9	280	9.4	290	7.0	280	6.6	270	4.5	270	5.4	280	6.5	270	6.8	8.2	11
220	11.0	220	9.2	220	8.7	250	8.4	270	7.9	270	6.9	270	6·1	250	3.2	220	3.4	210	5.5	220	5.5	230	7.7	7.1	12
280	9.7	290	10.4	290	9.0	280	7·1	280	7.9	290	10.4	310	9.4	300	10.0	300	11.1	310	10.2	320	8.7	290	6.6	10.1	13
320	4.1	320	4 · i	290	3.5	300	3.1	290	4.8	280	7.2	290	7.6	360	2.5	360	1.6	360	2.8	360	2.4		1.3	4.3	14
220	4.7	220	5.9	220	5.8	220	7.6	210	5.6	270	7.2	280	8.3	310	6.7	310	7.1	310	7.0	320	5.0	350	5.5	4.0	15
	' '			l		l	1			•					'	ľ	1							1	_ [
310	2.3	300	1.9	290	3.6	310	2.4		1.3	310	2.8	310	3.5	20	3.5	50	2 · I		0.2		0.1		0.2	3.3	16
240	4.4	220	6.5	200	5.8	200	4.2	240	4.4	270	4.1	270	4.4	250	3.5	230	2 · 1	200	2.6	190	3.8	190	4.9	2.7	17
290	5.1	280	5.2	270	5.3	270	5.0	270	5.4	280	5.5	270	6.4	250	3.1	270	4·1	270	6.5	270	7.2	290	7.7	4.8	18
280	8.0	290	7.8	290	8.7	290	8·0	290	7.0	290	8.7	300	8.6	320	7.9	330	7.2	330	7.4	350	7.9	350	5.6	7.7	19
320	4.6	300	5.3	310	5.2	300	4.5	290	5.0	290	3.7	280	1.8	270	2.4	280	4.0	300	5.4	290	9.2	300	5.2	4.9	20
																		_				26-	~	6.1	21
260	5.7	260	6.5	260	6.1	260	8.7	260	8·o	270	8.2	270	6.6	270	8.6	260	9.0	260	6.2	260	5:7	260	7:5		22
270	6.8	270	10.6	260	6.8	260	9.8	260	9.7	260	8.2	250	6.5	250	5.4	260	5.2	260	5.6	260	2.8	250 240	6.0		23
260		260	5.6	260		250	6·5 8·o	250	5.0	260	5.0	250	2.2	240	2.8	240	3.7	230	4.6	230	3.8	280	3.4	5.6	24
260	7.6	260 220	7.2	270	7.9	270		270	6.4	270	7.0	270	6.1	270	6.5	270	6.7	270	7.2	270	4·2	200	0.2	2.3	25
240	3.8	220	4.6	230	3.4	290	3.1	290	4.9	300	4.0		1.2	320	2·I		0.4		0.2		1 0		~ ~	- 3	-5
340	2.1	+	2.0	ŧ	1.9		1.3		1.3	70	7.0		7.4		1.2	250	3.8	250	1.6		1.0		0.4	1.6	26
290	5.0	280	4.9	310	5·I	310	4.1	330	2.1	70 330	2.5	_	1.4	_		350	0.2	350	0.2	330	3.2	330	1.7	1.7	27
260	4.6	270	3.6	270	2.2	240	2.2	250	3.6	240	5.0		1.5		0.4	_	1.3		0.0	330	0.1	33	0.0		28
210	4.8	190	5·I	180	6.2	180	6.0	180	6.8	180	6.0	240 250	4.2	230	3.4 4.8	260	4.0	270	4.4	280	3.3		1.5	3.0	29
270	6.4	280	6.2	270	6.5	260	5.4	250	4.9	260	5·I	260	4·3 5·2	270	5.0	270	6.1	270	4.0		1.2	_	1.5	5.0	30
	<u>-</u>						<u> </u>				J -		J ~		J 0										
-	6.7		6.7	-	6.8		6.7		6.5		6.8		6.2		5.4		5.5		5.5		5.2		5.1	5.8	1
1																									
	- 1		1		1		. 1		ī														!	l., 1	D
13	}.	14	ŀ [15	5·	16	·	17	·]	18	3.	10	.	20).	21	ι.	2:	2.	2	3.	24	4 ·	Mean	Day.
1							i					l						ĺ		Ī	j				

Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$). Speed in metres per second.

187. Eskdalemuir:

Ha (height of anemograph above M.S.L.) = Height of ground above

Day.	I		2		3		4			5.	6		7		8	3.	ç).	10	ο.	1	1.	No	on.
	٥	m/s.	٥	m/s.	c	m/s.	0	m/s.	°	m/s.	ı °	m/s.	٥	m/s.	0	m/s.	٥	m/s.	٥	m/s.	o	m/s.	°	m/s
I	320	2.6	310	4.0	†	1.8		1.0		1.4	290	4.9	290	4.6	290	5.0	270	5.4	260	5.6	250	4.3	250	3.0
2	200	4.1	200	5.4	200	3.2	200	3.3	200	4.4	200	5.2	200	6.4	220	6.5	220	7.5	210	7.6	210	8.6	200	8.5
3	220	8.7	220	7.1	220	7.6	220	7.3	220	8.5	220	8.7	210	8.3	180	8.9	180	9.6	190	8.4	190	6.2	190	6.8
4	190	2.2	190	2.4	190	3.9	190	3.2	190	4.3	190	2.8	190	4.4	190	2.5	190	2.1	200	4.9	200	3.9	200	4.4
5	200	3.2	200	3.6	200	5.1	200	6.1	200	5.8	200	7.0	200	6.2	190	6.0	190	6·1	190	7.2	190	7.0	190	6.6
6	330	3.2	330	3.5	330	2.6	330	1.9	330	2.5	330	2.7	_	1.1		0.3		0.1	120	2.6	120	3.7	120	3.7
7	360	4.4	360	3.2	360	2.3	360	2.2	360	3.4	360	3.0	360	2.4	360	2.4	360	2.6	350	2.4		1.5	250	7.6
8	150	2.7	150	2.8	150	3.1	150	2.2	150	1.7	190	2.9	200	3.0	190	2.6	190	3.6	200	3.6	200	4.0	200	4.6
9		1.1		1.0		1.1		0.1		0.2	190	1.7	190	2.0	190	4.3	180	5.0	180	5.0	180	0.1	180	6.7
10	-	1.0	350	1.6	_	1.4		1.5	350	1.6	_	1.5		1.1	350	3.3	360	5.3	360	4.7	360	5.5	360	8.4
11	360	2.4	360	2.4	_	0.6	360	2.2	360	3.5	360	3.1	20	3.4	30	3.0	60	3.4	†	2 · 2	Ť	1.8	_	0.2
12	ļ	0.0		0.0		0.0	_	0.0		0.0		0.0	l —	0.0		0.0	190	3.4	190	5.2	210	6.2	220	7.6
13	l —	0.3	Ţ	1.9	İ	3.1	l †	1.6		0.7	1 !	1.8	l İ	3.4	30	3.2	60	3.8	80	5.3	40	3.7	l İ	3.0
14	†	3.1	†	3.9	1 1	3.6	† †	5.0	Ť	4.7	†	3.2	Ť	3.1	20	4.1	30	5.6	70	6.4	80	6.3	80	5.6
15	_	1.4	_	0.2		0.5		0.3	_	0.1		0.0		0.0		1.5	190	2.8	200	4.9	200	5.4	200	5.7
16	220	5.0	220	4.4	270	4.5	260	4.6	240	4.0	260	4.7	260	5.9	270	6.3	260	6.3	270	6.5	270	6.9	240	9.0
17	210	4.1	220	4.5	220	4.2	220	4.7	210	5.2	220	4.2	220	7.0	230	8.5	250	8.9	230	8.7	230	9.9	230	10.0
18	260	3.0	260	4.1	240	2.8	220	1.7	210	2.0	240	3.7	240	5.0	260	4.6	270	5.0	280	3.6	280	3.9	260	5.3
19	230	2.0	-	1.5	_	1.4	210	1.8	210	4.4	220	5.3	200	5.2	210	8.5	210	9.4	200	8.4	220	10.5	210	10.7
20	240	8.6	250	8.7	250	10.5	240	9.0	250	9.1	270	9.9	260	9.6	260	9.4	270	8.6	270	9.7	270	9.5	270	9.5
21	220	10.0	230	11.9	240	11.7	270	9.9	270	6.6	270	8.4	270	7.0	270	6.7	270	5.7	250	6.7	240	6.4	240	7:4
22	240	7.2	220	6.5	240	8.6	240	10.2	240	7.9	230	7.2	240	7.0	230	7.5	230	7.3	220	7.1	230	7.9	240	8.0
23	220	13.0	220	10.2	220	10.1	210	10.0	210	10.0	250	7.6	250	6.5	270	6.3	270	6.9	270	7:3	270	7.0	270	8.0
24	290	6.3	280	5.9	270	3.8	270	2.6	250	2.3	260	3.1	270	3.1	270	4:3	280	5.8	280	7·1 6·2	280	5.7	270	6.5
25	_	0.7	_	1.4		1.5	240	4.5	260	3.2	230	3.0	240	5.0	250	5.8	260	6.5	270	0.2	270	7.8	270	7.0
26	250	10.5	250	10.7	260	10.4	260	9.6	260	9.4	260	9.5	260	8.6	270	10.0	270	11.4	270	12.6	270	12.9	270	10.0
27	†	8.3	!	7.4	l †	4.4	1 -	0.8	-	1.0	-	1.5	l -	0.8	-	1 4	190	1.6	190	4.0	190	4.7	200	4:5
28	_	1.5	j †	1.6	ļ †	2.3	†	1.0	†	2.2	[—	1.2	Ť	1.8	†	3.4	lĪ	3.8	†	3.0	100	3.1	180	3.0
29	-	0.9	760	0.8		0.4		0.1		0.0		0.1		1.4	170	2.6	1	3.5	190 220	3.8	190	4·9 5·6	190	4.0
30	210	2.9	160	1.8	_	0.5	_	0.8	240	3.2	260	2.9	240	5.1	250	6.1	240	0.2	1 20	5.3	190	3.0	,90	5.1
31	180	5.6	190	5.0	210	4.4	230	3.4	250	2.9	270	3.4	260	2.9	250	3.6	250	3.1	260	3.3	260	3.0	210	3.0
Mean ‡	_	4.3		4.3		3.9		3.7		3.9		4.1		4.3		4.9		5.5		5.8	_	6.0	_	6.4

188	Fekdalemuir	H 235 metres	15 metres

188.	Eskdale	muir	: Ha	a = 23	35 me	tres -	+ 15	metre	es.															
1 2 3 4 5	280 † 200 190 —	m/s. 2·6 † 12·5 2·6 0·1	270 † 210 220	m/s. 1·8 † 10·4 3·4 0·7	270 † 230 210	m/s. 2·6 † 10·1 5·1 1·0	260 † 230 210 300	m/s. 2·6 † 10·7 4·3 1·9	† 230 230 310	m/s. 1·5 † 11·7 4·8 1·9	260 † 230 240	m/s. 2·6 † 10·7 4·4 1·0	260 † 230 220	m/s. 5·9 † 12·5 3·7 1·5	260 † 220 230	m/s. 5·6 1·9 12·7 5·2 1·5	250 120 220 230 120	m/s. 4·6 4·4 13·0 4·0 3·6	260 120 240 240 140	m/s. 5·2 5·0 12·2 5·0 4·2	250 110 240 250 140	m/s. 5·9 6·1 11·6 5·5 6·6	250 110 250 240 160	m/s. 5·7 7·4 11·3 5·0 7·0
6 7 8 9 10	210 180 — 190 250	3.5 6.2 0.3 7.8 2.8	200 180 — 190 240	3·7 7·0 1·5 7·1 2·4	200 180 — 190 220	3·8 7·8 1·5 5·5 3·2	200 180 — 180 210	2·4 6·6 1·4 5·4 2·9	180 190 190	0·2 7·4 1·4 5·7 3·2	190 190 — 200 190	2·9 8·0 0·5 5·4 2·8	190 190 — 210 190	3.7 8.5 0.3 3.6 4.5	190 190 — 190 210	4·3 8·7 1·0 3·9 5·2	190 190 — 200 220	4·9 8·2 1·5 5·5 6·3	200 200 170 210 240	7.6 8.0 2.8 4.8 6.5	200 200 170 200 240	8·8 8·1 4·3 6·6 7·0	190 200 180 200 250	8·8 8·8 4·5 7·4 6·2
11 12 13 14	240 — 210 — 230	2·3 0·0 5·3 1·0 2·0		1·1 0·0 5·5 1·0 2·2	210 — 190 — 270	1·9 0·0 5·4 0·7 2·9	240 	2·8 0·0 6·6 1·6 4·1	240 — 190 — 270	4.5 0.0 6.3 1.0 5.2	230 — 190 — 260	2·9 0·0 4·3 0·9 2·5	240 — 190 240 250	3.0 0.0 4.4 2.5 2.0	240 200 240 250	3.6 0.1 3.5 4.3 3.8	240 200 240 250	4·0 0·0 4·5 3·6 4·1	250 220 230 270	3.6 0.0 4.0 3.5 5.8	250 200 220 270	4·0 0·1 3·2 4·3 6·7	250 — 210 220 260	4·4 1·4 4·5 5·5 7·9
16 17 18 19 20	270 200 260 270 240	8·4 4·7 4·0 2·5 2·0	270 200 280 280 —	8·5 5·6 4·8 4·5 o·8	260 † 270 280 —	5·5 † 3·7 4·1 1·3	230 † 280 270	2·7 † 4·5 2·5 1·0	260 † 270 250	3.0 † 4.5 2.5 1.2	260 † 270 260 —	5·4 † 3·9 2·3 0·7	260 230 260 260 —	4.7 6.8 2.0 2.5 0.3	260 250 280 270 220	4·8 7·0 3·5 3·5 2·0	270 250 290 270 220	5.5 6.3 4.0 3.2 2.0	280 250 300 280 210	5·1 7·1 4·8 3·8 3·1	280 260 300 280 210	5.4 6.8 4.7 3.1 2.8	280 250 320 280 210	6·2 7·5 5·5 3·2 2·8
21 22 23 24 25	160 230 240 †	4·4 6·0 9·0 †	170 220 240 †	4·8 6·0 10·3 †	200 230 250 †	8·o 5·5 8·6 †	200 220 240 †	11·6 5·7 7·6 †	200 230 230 †	13·0 5·6 5·1 †	200 220 220 †	7·4 6·0 †	200 230 220 —	16·4 7·5 6·5 o·o o·4	200 230 220 240 220	18·5 7·3 6·5 2·8 3·5	200 240 230 280 200	17.5 8.6 6.8 5.1 3.9	210 † 230 290 210	17·7 † 7·5 5·1 5·8	230 † 230 290 220	12·6 5·2 5·6 6·7	260 † 210 300 200	10·5 † 4·2 5·6 7·0
26 27 28 29 30	220 230 220 — 310	6·6 6·5 5·6 0·5	220 230 220 — 310	4·6 5·3 6·0 0·2 10·8	210 230 220 — 300	4·8 5·7 5·0 0·1 8·1	220 220 230 — 300	8·4 6·6 5·6 0·3 7·9	210 230 230 — 290	8·5 7·5 5·6 0·4 7·9	210 220 230 — 290	8·0 8·2 5·6 0·5 8·8	210 220 240 — 290	8·5 9·2 6·6 0·7 9·8	220 220 240 — 280	9·1 8·2 6·4 0·6 9·5	210 220 250 150 280	8·8 8·6 5·4 2·1 7·4	220 220 270 140 280	10·0 10·3 4·8 4·0 8·0	230 210 280 130 280	12·0 9·8 6·9 4·3 7·3	230 210 280 130 270	12·9 10·4 7·0 4·2 8·7
31	230	4.6	240	4.8	250	4.6	250	3.2	_	0.5		0.9	160	2.0	140	2.2	140	3.1	140	1.7	140	2.3	170	2.4
Mean§		4.3		4 · 1		3.9		4.0		4.0		3.9		4.3	_	4.7		4.9		5.4	_	5.9	_	6.3
G.M.T.	İ		<u>.</u>	2.	3	3.	4	1.	5	5.	6		7	•	8	3.	ç).	1	o.	I	Ι.	No	on.

[†] Defective record.

[‡] Mean for 30 days only, omitting 13th.

WIND: DIRECTION AND SPEED.

Average for periods of sixty minutes, centred at the exact hours, Greenwich Mean Time.

M.S.L. $+ h_a$ (height of anemograph above ground) = 235 metres + 15 metres.

July, 1923.

<u> </u>				l .		Ι.		l .		Ι.	8.	Ι,			0.		Ι.	<u> </u>	2.					Mann	D
I	3∙	1	4.	ļ	5.	1	6.	1	7.		о.	, '	9.	2	0.	2	1.	2	2.	2	3.	2.	4.	Mean	Day.
250 200 190 190 190	m/s. 4.5 8.3 7.5 7.9 6.4	250 210 220 190 190	m/s. 4·8 8·0 6·9 8·9 4·8	250 220 210 190 190	m/s. 4.6 8.0 5.5 8.4 3.6	250 220 210 190 190	m/s. 5.7 8.0 4.4 9.0 2.9	270 220 210 190 190	m/s. 8·1 6·6 5·4 7·5 2·2	270 210 200 190 190	m/s. 6·4 5·9 5·8 6·7 3·0	260 200 190 190	m/s. 4·0 7·6 6·1 5·8 1·5	250 180 190 190	m/s. 4·0 8·1 5·0 5·1 0·4	250 180 190 190	m/s. 5·I 8·6 5·2 5·0 0·0	250 190 190 200	m/s. 3·2 9·3 4·2 5·5 0·0	230 220 190 200	m/s. 3·0 10·5 3·4 4·2 0·0	200 220 190 200	m/s. 4·6 10·0 2·9 3·5 0·5	m/s. 4·2 7·0 6·7 5·2 4·0	1 2 3 4 5
100 200 210 360	4·I I·2 5·5 5·0 7·9	100 200 210 360	4·5 0·9 5·6 3·3 5·0	120 200 210 360	4·3 0·0 6·1 2·5 3·6	140 — 190 200 360	4·2 0·0 7·2 2·4 4·6	140 210 190 — 360	4.0 2.2 7.5 1.4 4.6	140 — 190 — 360	4·6 1·2 7·1 1·4 3·4	130 — 190 — 360	2·5 0·7 6·0 0·2 2·5	130 — 190 — 360	1·6 0·0 4·5 0·0 3·0	190 360	0·5 1·0 3·7 0·2 4·0	200 190 — 360	1·5 3·3 2·5 0·3 4·0	360 170 — 360	2·5 3·1 1·3 0·5 3·7	360 150 — — 360	3·7 1·9 1·5 0·5 4·7	2·7 2·3 4·0 2·2 3·6	6 7 8 9 10
180 220 † 80 200	1·7 7·4 † 4·9 7·1	210 210 † 80 200	3·4 6·8 † 4·0 7·0	230 220 † 70 200	4·5 6·1 † 4·7 6·7	210 220 † 70 200	4·9 5·7 5·5 4·7 5·9	200 230 † 80 200	5·2 5·0 6·0 4·5 5·6	190 290 † 60 200	3·1 4·1 5·0 5·0	310 60 60 210	1·4 2·6 6·7 3·9 6·3	320 30 60 210	0·0 1·6 † 3·4 6·5	- † 60 210	0·0 0·2 † 2·2 6·0	† 60 210	0·0 1·3 3·4 2·8 4·7	- † 60 210	0·0 0·7 3·9 2·1 4·4	- † - 210	0·0 0·4 3·6 1·0 4·1	2·3 2·7 — 4·2 3·9	11 12 13 14 15
240 250 270 210 250	8·2 9·4 5·4 9·6 10·2	240 230 260 210 250	9·4 10·1 4·2 8·6 10·0	220 210 270 240 240	9·1 10·3 5·1 7·0 12·2	220 230 270 270 230	10·4 8·6 5·4 8·9 11·5	220 220 270 270 220	8·6 6·6 5·5 9·5	220 220 270 270 220	8·4 7·3 5·0 7·0	210 210 260 240 220	7·3 3·4 4·5 5·5 12·6	210 220 250 230 220	5·2 4·5 3·1 5·8	220 230 — 220 220	5.0 5.5 1.5 5.2	230 230 250 220 220	5·9 3·5 3·2 5·9	230 210 250 220 210	5·5 3·4 3·4 7·6 9·9	220 240 230 240 220	4.0 4.1 2.6 8.0 10.9	6·4 6·5 3·9 6·5 10·2	16 17 18 19 20
210 230 270 270 270	9·1 8·1 7·0 6·8 7·5	210 220 270 260 270	9·6 7·6 7·4 6·6 8·3	210 220 270 250 270	8·9 7·9 6·9 7·9	220 220 270 240 270	8·3 9·0 6·3 7·7	220 230 270 220 270	7·9 8·5 5·0 8·6 11·6	220 220 270 210 270	6·2 8·8 5·0 6·8	270 220 -270 210 270	4.0 8.8 4.0 4.4 11.2	260 210 280 210 270	4·1 6·5 5·4 5·5 7·6	260 210 270 200 270	2·7 6·9 4·2 3·1 7·4	230 210 270 200 270	3·0 7·9 3·9 3·5 8·0	250 230 280 210 250	7·5 9·9 5·0 4·5 7·5	240 220 290 220 240	9.0 12.9 5.1 2.0 8.1	7.5 8.1 7.2 5.2 6.6	2I 22 23 24 25
270 190 † 210 180	11·8 5·4 3·1 5·9 7·4	270 190 † 180 180	12·8 6·6 3·3 6·5 9·4	270 180 † 180 170	13·7 6·9 3·5 7·2 7·7	270 180 † 180 170	12·5 6·7 4·0 6·7 7·4	280 180 † 190 170	14·9 5·6 5·0 6·7 7·5	310 190 † 190 180	14·8 4·6 4·1 6·1 5·6	310 180 † 200 170	13·5 2·4 3·5 5·6 4·0	310 † 190 170	13·2 1·4 3·0 5·3 2·7	300 † 190 120	9·3 0·4 2·7 4·6 2·4	† 190 110	6·5 0·8 2·5 4·5 1·1	† † 210 130	4·5 0·3 2·5 4·0 5·1	† † 210 160	6·2 0·3 2·0 3·3 5·0	3.5 2.8 3.7 4.6	26 27 28 29 30
220	6.6		6.6		6.5	240	6.5	170 —	3·o 6·5		4·7 6·0	_	4.9		4.3	_	3.8		3.8	<u>-</u>	4·I	310	4.2	2.1	‡

August, 1923.

1 0	l m le		m/s.	1 0	m/s.	1 0	m/s.	1 0	m/s.	0	m/s.	0	m/s.	0	m/s.	1 0	m/s.	0	m/s.	0	m/s.	7	m/s.	m/s.	i
250	m/s.	250	5.9	250	7.0	250	5.4	220	5.2	210	5.0	230	6.0	230	4.8	240	3.6	240	2.6	_	0.2	_	0.2	4.2	1
110	8.4	110	10.0	110	11.1	120	9.9	130	7.5	150	9.0	140	11.1	160	16.1	170	18.7	180	16.4	190	15.1	200	15.0	-	2
250	12.4	250	11.8	250	11.4	250	9.9	250	7.5	250	6.3	250	5.5	250	7.8	250	6.6	250	7.2	250	6.7	240	4.2	10.1	3
230	5.5	210	5.3	190	5.0	190	6.3	180	6.0	190	4.5	190	2.5	190	2.0		1.0	_	0.1		0.3		0.0	3.9	4
170	5.7	160	4.7	180	5.2	230	5.2	200	2.4	180	1.8	190	1.8	180	2.1	190	2.9	200	3.2	220	3.6	220	3.2	3.0	5
1	• •		1	ĺ	1	ł				l						}		ł				-0.	6.0		
200	10.0	190	9.5	190	9.0	190	7.2	190	7·1	190	7.7	180	7.3	180	7.3	170	6.3	170	4.5	180	6.5	180	6.8	5.9	6
200	9.0	210	8.3	200	8.2	210	7.0	190	5.5	250	4.5	260	4.5	240	4.5	260	1.9	230	3.0	200	7.9	190	8.3	6·5	7 8
180	4.8	190	7.6	190	8.8	180	8.2	190	10.0	190	9.8	180	10.3	190	0.0	190	9.5	180 190	9.4	190 250	3.0	240	1.0	4.8	9
220	5.4	250	5.3	250	5.3	250	5.0	260	5.7	280	4.5	280	3.8	250		240	2.4	190	1.2	230	3.0	240	2.5	4.6	10
250	6.3	250	6.7	250	7.3	250	7.3	250	0.7	250	2.1	240	3.0	230	4.2	240	2 4	l		1 230	, ,	-4-	- 3	, ,	
1 +	4.0	250	4.1	260	3.3	260	3.4	260	3.5	270	3.2	230	1.8		0.6		1.3		0.9		1.4		0.1	2.8	11
190	5.1	180	4.4	190	3.8	190	3.4	190	2.6	180	2.0		0.7		0.4		1.0	180	2.5	180	4.8	190	5.2	1.5	12
210	4.6	230	5.2	250	5.5	250	4.7	250	4.0	240	3.3	230	2.3	210	2.1		0.9	220	1.8	210	3.3	_	1.3	4.1	13
230	6.3	250	4.3	250	5.6	260	5.0	250	4.8	270	5.4	270	4.2	270	2.5	270	2.2	280	1.6		1.3		1.1	3.1	14
270	7.0	270	7.4	270	8.0	270	7.7	270	7.5	270	8.2	270	7.1	260	6.5	250	6.6	240	4.0	250	4.8	270	8.3	5.4	15
1	•	1		'										ĺ		İ			_				- 0	1	-6
280	5.5	280	5.1	280	5.I	280	4.3	270	5.2	260	4.9	260	4.0	240	6.2	220	5.8	230	6.5	220	5·1	220	5.8	5.4	16
250	7.2	250	7·I	270	6.2	280	6.1	270	5.6	270	6.2	290	5.4	280	3.2	270	3.2	270	4.7	250	4.2 0.0	250	4.5	3.3	17
310	5.3	320	5.6	320	5.0	310	4.2	340	4.0	350	2.2		0.6		0.3		0.1	200	2.6	_	1.2	230	1.0	3.1	19
260	4.0	240	4.0	230	3.3	210	4.0	220	3.2	230	3.9	240	4.4	230	2.5	210	2·1	200	6.5	190	5.8	180	3.5	2.7	20
210	3.0	210	3.0	210	2.9	200	4.1	210	3.3	210	3.0		1.3	200	3.3	210	5.3	200	ر ن	190	ا ت			l	
260	11.7	260	11.3	250	13.8	250	14.7	250	14.4	250	12.0	250	12.6	250	13.1	t	t	t	+	230	5.7	210	4.3		21
1 200	+	250	9.4	260	11.3	260	9.6	260	10.4	270	8.7	270	7.5	260	8.0	250	8.0	230	6.3	230	6.2	230	6.9	-	22
180	3.5	170	3.1	150	4.2	150	5.2	140	5.0	150	7.2	140	6.6	†	†	t	†	Ť	† l	Ť	†	Ť	†		23
300	7.5	330	7.5	340	8.0	350	7.1	350	4.8	340	2.7	330	4.9	330	3.4	i i	i i	Ť	†	†	Ť	, †	†	-	24
200	8.3	200	9.7	190	9.0	180	8.7	180	8.6	180	10.2	190	11.1	200	0.11	210	10.9	210	10.0	220	10.3	220	9.6		25
			1							ļ.		1													-6
230	13.2	230	12.7	210	9.5	200	12.6	210	12.8	200	10.2	200	8.2	210	9.0	210	9.0	210	6.0	220	7.8	230	7.2	9.2	26 27
210	9.8	210	9.2	210	8.1	230	7.1	230	6.6	240	5.3		1.5	250	2.9	240	4.3	220	5.8	240	5.8	240	1.0	7.1	27 28
280	7.5	280	7.7	280	8.6	280	8.5	280	6.3	280	4.3	240	2.1	240	3.8	240	2.5	220	1.7	190	2.0	320	10.1	5·4 4·0	20
100	3.2	60	4·1	50	4.5	60	5.4	40	5.8	20	7.5	10	7.7	10	7.3	350	7.1	340	9·1 8·5	330	9.4	220	3.9	7.8	30
280	8.8	280	7.7	270	7.4	260	8.1	260	7.6	270	5.8	240	5.6	230	5.0	230	6.5	240	0.2	210	4.0	220	3 9	′	J
190	2.9	150	2.8	_	1.3		o·6		0.4	_	0.5		o ·6		0.4		0.2		0.2	_	0.4		0.0	1.9	31
					6 -				<u> </u>										- 0		2.7		3.6	4.8	§
	6.5		6.3	_	6.2	_	6.0	_	5.6	-	4.9		4.0	_	4.0	_	3.8		3.8	_	3.7		9.0	4 0	2
						<u></u>					<u>' </u>				<u>' </u>			<u> </u>		Ī		1		Man	Dor
) I.	3.	I	4.	1	5·	10). 	17	7.	I	8.	19).	20	o.	21	τ.	2:	2.	2	3.	2	4.	Mean	Day.
l							!		I					<u> </u>								<u> </u>		<u>. </u>	!

Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$). Speed in metres per second.

189. Eskdalemuir:

Ha (height of anemograph above M.S.L.) = Height of ground above

Day.	1		2	2.		3.	4	1 .		5.		5.		7·		8.		9.	1	10.	1	ı.	No	oon.
I	<u> </u>	m/s.	°	m/s.	-	m/s.	·	m/s.	-	m/s.	·	m/s.	°	m/s.	°	m/s.	-	m/s.	° 350	m/s.	° 330	m/s.	350	m/s. 3.4
2	†	†	†	†	†	†	†	†	l f	†	†	1.0	1	2.2	Ť	3.8	†	3.9		1.5	310	2.5	†	6.5
3	-	0.1		0.2		0.3		0.1		0.1	200	0.4	220	0.3	200	0.1	290	1.5	220	5·1 6·7	230 300	6·5 5·0	230 290	7.6
4	190	9.4	200	8.9	230	7.0	300	5.5	320 220	3.1	300 220	4.2	320 220	5.9	300 240	5.4	250	5.4 10.7	300 270	9.8	270	9.6	260	7.6
5	220	6.1	230	7.0	230	9.1	220	10.0	220	99	220	10 0	220	92	1 240	100	250	10 /	2,0] 9 0	2,0	"	-00	, ,
6	220	3.1	260	5.9	260	7.4	250	6.6	250	5.6	230	3.9	210	5.1	210	6.5	220	6.5	220	6.4	220	6.7	220	8.1
7	220	10.0	230	8.9	250	6.5	270	5.1	270	5.3	280	4.4	290	5.0	290	4.5	290	3.5	280	4.3	280	6.5	280	7.5
8	240	1.6	Ť	1	Ť	1 †	l †	†	Ť	†	†	†	†	†	190	0.8	180	4.1	210	6.8	230	7.7	220	8.8
9	220	6.5	220	6.6	220	7.7	220	6.8	210	6.2	210	6.6	200	8.0	210	8.7	200	8·o	210	10.0	210	11.3	210	11.5
10	200	2.0	150	2.0	150	2.0	150	2.1	180	2 · I	180	1.6	200	3.4	210	3.7	230	3.4	270	5.7	270	6.6	270	5.6
	200	.	220	5.2	270	F. 4	220	6.5	220	6.5	210	6.5	210	6.7	230	9.6	230	9.5	220	11.0	230	11.3	220	11.7
11	230	5.3	220	2.3	210 230	5.4	240	10.8	240	12.8	230	13.6	230	11.8	250	10.3	250	10.5	260	14.2	260	15.0	250	14.5
12	230	1.0	230 60	2.0	60	2.0	60	2.0	60	2.0	60	2.0	40	2.0	360	2.9	360	3.0	10	2.4	20	2.8	110	4.9
13	170	10.2	200	7.9	230	4.9	220	4.2	200	5.0	200	3.5	210	5.0	230	6.7	220	6.7	220	7.1	220	8.9	220	8.7
14	1 1/0	+	1 +	1 1	7	†	†	†	t	†	†	†	220	4.6	230	5.6	210	7.3	210	6.0	210	6.2	230	5.9
13	1 '	'	'	'	['	· ·	1 '	[' [' '	· ·	' '		i .				. "	1	l i		1		-
16	180	2.8	220	6.0	210	5.9	210	6.4	220	7.4	220	7.1	240	6.6	240	5.8	260	5.9	270	6.2	270	6.7	270	7.5
17	190	4.4	190	2.8	190	3.9	190	4.0	190	5.2	190	5.5	170	8.3	170	10.0	170	11.5	160	10.6	170	9.0	180	10.1
18		1 · 1		0.1	I —	0.0		0.0		0.1		0.1		0.1		0.1		1.0	270	4.1	270	5·0	260	5.0
19	260	4.6	250	3.1	240	3.6	230	3.4	210	2.2	220	3.9	230	6.3	230	6.6	230	7.6	220	7.9	210	8.4	210	8·0
20	170	2.8	240	6.0	230	5.7	190	4.3	210	5.6	210	6.6	210	8.9	220	7.6	230	7.1	260	7.1	290	0'4	300	0.9
21	180	1.7	180	2.0	190	2.5	190	2.5		0.9		0.4		0.3	260	2.5	270	3.0	280	3.4	300	2.8	320	3.7
22	190	4.6	180	4.5	230	6.9	220	9.8	240	10.6	240	8.9	230	6.5	230	8.0	230	9.2	220	9.4	220	8.9	240	7.6
23	-	0.0	l —	0.0	-3-	0.0		ó∙o		0.0	<u> </u>	0.0	_	0.2		0.3	_	1.2	140	2.5	220	3.2	230	3.3
24	l —	0.7	<u> </u>	0.1		0.1		0.2	_	0.7	280	1.8		0∙8		0.7		0.5	180	4.0	†	†	180	4.6
25	100	8.1	100	7.9	110	8.2	130	5.8	120	3.8	130	3.4	130	3.9	130	5.8	150	7.0	170	8∙0	190	8.6	210	9.5
-6	-6.	0 -	26.5	6.0	26.5		250		250	4	220	4.5	220	5.6	220	5·1	240	5.5	250	8.2	260	6.2	260	8.0
26	260	8.9	260	6.3	260 220	5.6	250 210	5.0	250 210	4.9	230 210	4.2 9.2	230 220	12.5	210	10.0	210	10.4	200	11.9	200	13.4	†	13.8
27	230	7.6	220	6.5	230	6.5	240	7.5	230	9·5 14·9	220	7.4	240	7:5	260	6.5	260	5.3	260	3.2	270	5.6	260	5.2
1	240 220	13·0 2·0	230 180	15·4 2·4	200	19.5	200	2.0	200	2.4	200	2.9		1.5	210	3.0	210	3.9	200	3.7	210	4.9	210	4.6
29 30	100	3.8	180	5.6	190	6.6	200	8.8	210	9.1	210	8.6	200	6.4	200	5.5	200	6.1	220	8.5	230	10.1	210	9.3
										- <u>-</u>														
Mean‡	_	5.1		5.3		5.7	_	5.6	_	5.4	_	5.1		5.2		5.8		6.1		7·1	_	7.6		7.9
	<u> </u>			<u>' </u>				!						<u></u>	<u> </u>	1 1	<u> </u>	<u>'</u>		1		·	!	1

190.	Eskdalemuir	:	$H_a =$	235 metres	+	15	metres.
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190. E	kdale	muir	: Ha	; = :	235 n	netres	+ 18	met	res.															
	٥	m/s.	°	m/s.	٥	m/s.	٥	m/s.	0	m/s.	٥	m/s.	٥	m/s.	°	m/s.	0	m/s.	°	m/s.	°	m/s.	۰	m/s.
1	210	5.7	210	5.0	210	5.0	†	4.6	†	5.0	†	5.4	280	3.6	280	6.2	270	8.5	280	7.6	290	7.8	280	7.4
2	230	9.6	230	11.5	220	11.8	230	14.2	240	16.0	260	15.4	270	13.2	280	4.1	280	6.5	290	8.9	290	9.9	280	8.0
3	230	3.1	240	3.1	230	2.2	210	3.1	230	2.0	_	0.9		0.4		0.4	260	0.4	20	2.5	30	4.4	360	3.8
4	360	5.0	360	5.0	360	7.0	360	7.1	360	6.4	360	3.1	360	3.0	360	5'4	360	6.5	360 200	5.4	20 210	5·0 6·3	20 210	5·5 8·5
5	-	0.3	-	0.3	_	0.3	_	0.3	_	0.3	_	0.3		0.3	_	0.4	190	4.1	200	0.0	210		2.10	0.2
6	230	6.6	240	7.1	230	5.2	220	7.1	210	6.7	210	6.2	210	7.5	220	8.0	220	9.5	250	9.7	260	8.4	260	8.3
7	240	6.7	240	8.1	240	5.8	210	5.8	230	8.5	220	9.3	220	9.9	220	10.6	230	12.3	220 260	13.1	220	12.0	230	6.0
8	270	6.5	260	4.0	260	4.8	170	2.1	210	1.8	180	3.5	180	3.9	190	2.2	230	4·6 13·6	260	5·3	270 250	7.5	270 250	16.4
9	220	12.4	220	10.3	220	10.9		10.6	260	10.2	260	8.6	250 220	9.0	250 220	9.0	250 220	10.1	220	10.3	230	9.2	220	9.4
10	240	9.1	230	8.1	230	8.6	230	9.5	240	9.3	230	8.0	220	9.0	220	9.0	220		220	10 3	250	9 2		
11	270	7.2	270	7.6	270	8.0	270	8.9	270	8.6	270	9.8	270	9.6	270	8.5	270	8.3	270	9.0	270	7.6	270	8.4
12	I —	1.3	180	3.6	140	3.0	200	4.6	200	4.4	180	5.2	160	4.2	180	5.5	200	6.0	160 360	2.1	150	4.6	200	3.2
13	—	1.5		1.5	330	2.8	350	3.5	350	3.9	360	3.1	360	2.8	360	2.5	350 310	3.4	300	5.6	350 300	5.7	340 320	5·3 3·5
14		1.1	270	I.I	250	3.5	250	3.2	240	3.5	240	3.2	240	3.1	340 190	3.0	180	4.5	210	5.0	220	6.4	240	6.9
15	270	3.2	2,0	3.4	250	3 3	250	33	240	3 3	240	3 3	240	3 1	190	, ,						'		- 9
16	230	7.4	240	7.3	240	6.4	250	5.3	260	5.0	260	5.6	270	4.9	270	6.2	280	5.8	280	7.6	300	6.1	290	5.4
17	210	5.3	220	6.5	230	7· I	240	6.0	250	7.5	270	7.6	260	6.5	260	6.4	270	5.0	260	4.6	260	5.9	270	7.9
18	210	2.1	210	5.6	210	6.8	200	5.2	200	5.4	200	4.6	190	2.8	180	4.1	190	6.4	170	5.5	160	3.9	150	4.0
19	180	10.2	180	9.4	150	4.0	160	7.1	160	9.5	170	11.9	190	16.0	230	12.5	240 200	13.4	240 210	9.7	240	13.8	250 200	19.1
20	190	2.6	200	4.3	190	3.2	200	5.4	180	2.1	190	6.4	200	6.4	200	6.5	200	7.0	210		200	11. 5	200	13.1
21	150	8∙0	140	8.0	140	9.9	150	10.1	160	8.6	180	10.4	180	11.0	230	7.1	270	5.2	270	4.8	240	6.4	240	9.1
22	220	7.0	200	6.0	210	5.2	210	7.3	200	6.3	200	4.9	200	6.8	200	6.4	230	6.8	230	7.0	250	6.4	260	6.0
23	240	14.9	220	5.9	220	7.5	220	8.4	210	7.4	210	5.2	180	2.6	180	3.8	170	3.2	150	5.4	150	4.8	140	5.4
24	230	7.0	230	6.2	230	5.0	230	6.0	220	7.2	230	7.9	230	5.8	230	5.2	230	5.7	220 220	7.2	220 230	7·0 10·3	220 220	8.3
25	210	9.0	230	7.5	220	5.8	220	6.6	220	7.8	220	8∙0	210	9.0	210	9.0	220	9.8	220	10.2	230	10.3	220	11.5
26	190	3.4	170	5.0	150	4.9	140	5·1	150	3.6	150	3.0	180	3.3	190	4.3	210	6.4	230	5.9	230	8.3	220	10.2
27	130	6.0	110	6.5	110	9.6	120	10.0	120	8.5	130	7.1	140	5.9	160	6.0	160	5.4	170	6.1	140	2.9	150	4.2
28	170	5.3	170	5.7	170	10.1	200	9.4	190	9.9	180	8.4	190	9.0	200	8.5	190	9.0	210	8.5	200	8.0	190	8.5
2 9	230	5.6	230	6.0	230	6.0	230	7.9	230	10.5	220	9.1	220	8.7	220	8.5	220	9.9	210	10.6	200	9.8	200	11.1
30	190	13.6	190	12.1	190	13.2	190	15.0	190	17.1	190	15.8	190	16.0	190	13.5	190	11.2	220	12.5	220	9.8	220	9.6
31	220	8.9	220	8.5	210	7.6	200	7.3	210	7.2	220	6.4	210	6.0	220	6.7	210	6.4	220	6.4	240	8.0	240	8.6
Mean		6.4		6.3	_	6.2		6.7		6.9	-	6.7		6.7	_	6.4		7.1	-	7.7		7.7	_	8.2
G.M.T.	1	ι.	:	2.		3.		.		5.	(5.	,	7.	ł	В.	٩).	1	10.	,	II.	N	oon.
	<u> </u>		<u></u>	411	Dofoot	ive re	l nord				<u> </u>								<u>. </u>		<u>. </u>		·	

† Defective record.

† Mean for 24 days only, omitting 1st, 2nd, 8th, 14th, 15th, 24th.

Averages for periods of sixty minutes, centred at the exact hours, Greenwich Mean Time.

 $M.S.L. + h_a$ (height of anemograph above ground) = 235 metres + 15 metres.

September, 1923.

1,	3.	1.	4•	I	5.	I	6.	r	7.	18	3.	ıç).	20).	21	ı.	22	2.	23	3.	24	j.	Mean	Day.
310	m/s. 5.7	290	m/s. 5.0	300	m/s. 6·5	300	m/s. 5.7	†	m/s. †	310	m/s. 1 · 8	300	m/s. 5·6	300	m/s. 6·4	320	m/s. 3·8	310	m/s. 1 · 8	300	m/s. 5·0	320	m/s. 5 4	_	I
290	8.5	280 210	4·3 8·0	300 210	2.1	300 200	5.3	280 200	4.7 8.1	280 210	3.5	280 210	3·0 8·2	200	7·9	210	8.6	210	0.0	200	0.1	200	8.8	4.9	3
220	6.6	280	6.5	270	6.7	270	7.5	270	6.4	270	5.0	270	5.2	270	5.3	260	5.9	240	4.6	230	2.I	230	6.2	6.1	4
250	5.7	260	8.6	260	10.3	260	9.4	250	8.6	240	7.0	250	6.7	250	7.1	270	8.6	270	7.8	270	9.9	220	4.6	8.5	5
		l					0 -				0.4			270	7. 0	100	5.0	200	6.7	190	7.5	210	8.9	6.9	6
220	9.9	220	9.5	210 280	7.0	210 290	8·9 6·4	210 290	10.0	210 280	8·3 6·5	200 280	7·1	210 280	7·0 3·3	190	5·2	300	3.5	220	3.0	180	2.2	5.6	7
220	7.5	210	7.3	210	7.3	220	10.0	210	5.4 8.1	210	6.6	210	6.4	210	6.4	220	7.8	220	9.4	220	8.9	220	7.3		8
220	10.5	220	10.1	260	7.2	260	7.0	260	6.4	260	4.9	250	3.7	240	2.4		1.5	240	2.3	240	2.7	250	2.6	6.7	9
270	6.4	270	6.5	270	6·1	270	4.6	260	4.5	260	5.6	270	4.6	250	3.4	200	3.0	200	2.2	230	5.0	240	5.3	4.0	10
									0		- 0					270	70.0	270	10.5	220	11.0	220	10.8	9.5	11
220	12.0	220 260	10.6	220	14.9	210 260	10.6	200 260	8.1	210 260	9·8	200	10·0 5·0	220 240	3.4	210	10.9	210 250	2.4	220 270	2.8	230	1.1	9.2	12
190	7.9	200	8.5	270 190	9.9	190	7.4	190	5·4 7·4	170	7.5	250 180	8.5	180	9.5	170	9.0	170	8.5	170	8.5	170	9.2	5.2	13
210	9.1	210	9.2	210	8.5	220	7.0	200	5.9	200	3.8	200	3.4	200	2.2	200	2.1	200	3.3	200	3.6	Ιŧ	†		14
230	6.4	230	7.0	220	6.4	240	7.4	240	6.7	240	5.0	250	4.4	240	4.0	220	2.5	210	2.8		1.5		1.5		15
	1					'		`													2.6	700	0.5		٠
270	5.6	270	6.6	270	6.0	270	6.4	270	5.0	270	2.I	260	4.4 8.0	240	3.7	230 160	3.9	230 170	2.9	200 180	2·6 4·8	190 210	2.5	5·4 7·2	16 17
170	8.5	170	8.4	160 220	8·9 8·4	160 220	9.7	160	8.7	160	0.7	150	2.6	160	3.0	270	4.2	260	7.6	260	4.9	270	5.5	2.8	18
250	5·0 7·8	220	6.6	210	8.4	210	5.3	210 220	3.3	220	10.0	240	6.5	240	4.2	250	5.0	270	5.6	270	4.1	220	4.0	6.1	19
300	9.1	300	8.4	310	5.2	290	5.0	280	4.9	270	2.7	270	3.9	260	4.4	250	2.5	140	2.1		0.3		o∙5	5.4	20
J	-	3		ľ		_		ĺ	' -	′	<i>'</i>	'										l			
1	4.1	270	4.9	270	4.6	260	4.9	260	4.0	260	3.1	260	3.1	240	2.5	240	1.8	240	2.2	230	2.5	200	4.6	2·8 6·1	21
240	8.5	230	8.0	220	8.4	240	4.7	210	2.1	230	3.2	210	4.0	190	3.9		0.6	_	0.8	190	2.0	200	2.5	1.8	22 23
240	4.5	180	4·5 6·4	230	4.4	260	3.2	270	3.6	300	3.8	290	3.3	290	1.1		0.6	110	4.1	120	5.6	100	6.1	1	24
190	10.0	200	10.4	200	7.0	190	7.5	190 200	4.0	210	10.0	210	10.0	230	9.5	250	8.0	260	9.0	260	6.9	260	8.0	8.0	25
200	100	1 200	10 /	1 200	10 4		10 4	200	10 1	-10			1.0	-30	1.	-3-			-		1	1		1	ľ
250	7.7	240	6.4	240	7.5	240	7.1	240	6.8	230	8.3	230	8.4	230	8.8	220	7.8	230	8.0	230	7.8	230	8.2	6.9	26
210	13.9	210	15.3	210	15.5	220	12.9	210	11.9	210	12.0	220	13.9	220	14.0	220	13.1	220	13.1	220	12.5	230	10.9	11.6	27
270	4.3	260	5.9	260	6.0	270	4.7		1.5	280	1.8	_	0.2		0.6	-0-	0.2	180	1.5	230	2.4	230	2.1	6.6	28 29
210	4.7	1 1	4.5	180	3.3	170	2.5	200	1.3	180	1.9	180	2·8 8·0	180	3.2	180 210	4·1	210	3.6	190 200	6.8	200	4.7	3.1	30
200	5.2	210	7.5	210	6.1	210	9.2	200	10.0	210	10.0	210	3.0	210	/ 1	210							-		
_	7.7		8.0		7.8	-	7.1		6.3		6.1		6·o		5.8	_	5.2		5.3		5.3	_	5.1	6.2	‡
	7.7	<u> </u>	8.0		7.8		7.1		6.3		6.1		6.0		5.8		5.2		5.3		2.3		9		-1 0.2

October, 1923.

	3.	I	4.	I)·	1,	·.	1,	/•		J,	I	y	20	υ ,	2	1.		4.		J.		 -		1
	_					10	6	· · · · · · · · · · · · · · · · · · ·	<u>' </u>	1	Q		0	2				<u>'</u> ^	2.	2	3.	,	4.	Mean	Day.
_	8.4		8 · r		7.7		7.2		6.6		6.3		6.3		6.1		6.0		5.8	_	5.9		6.3	6.8	
230	7.5	230	7.9	240	7.0	210	4.8	220	5 4	210	4.9	220	5.2	230	4.1	240	4.2	240	1.8		0.9		1.1	6·1	31
190 220	10.1	220	10.0	220	9.6	200	8.8	200	6.6	190 210	7.5	190 220	9.9	190 220	9.0	220	10.6	210	10.6	220	10.4	210	9.3	11.4	30
210	7.9	210 180	6.5	200 180	4.6	200 180	5·0 14·5	200 190	4.3	190	4.2	190	5.3	210	7.3	210 190	6.3	230	6.5	260 190	6.7	230 190	5.1	7·1 10·7	28 29
220 140	10·9	210 140	9·5 6·4	220 140	9·1	230 140	10·6 6·4	230 130	9.0	230 140	10·1	230 140	5·0 8·8	210 130	6·5 7·7	180 140	4·5 8·4	180 140	3·1	140 150	2.2 3.1	130 170	6.3	6.9	27
	' '						i . i										1		•	7.40	2.7	120	6.0	6.3	26
220 220	8.2	220 220	7.6	210 220	6·9	210 210	2·9 13·0	200 220	2·1 13·5	220 220	3.6	200 220	2.2	180 220	8·1	180	3·4 8·4	190 220	3.8	170 210	3·5 8·0	180 210	5.5	5·6 9·7	24 25
240 130	9.6	240 130	5.4	120	3.0		0.4	230	0.1	230 250	4.7	250	8.3	230	8.6	240	9.0	230	7.6	230	8∙0	230	7.2	6.2	23
230	10.6	230	9.9	220 220	8.6	210 220	7·1 10·6	190	5.9	190	7·4 12·5	200 230	8·4 12·7	220 230	8·4 11·9	210 230	8·4 13·0	210 230	8·1 13·4	230 240	8·4 13·6	220 230	8.4	8·2 8·9	2I 22
190	13.3	190	13.5	190	14.3	190	13.1	180	12.0	170	10.0	170	9.8	170	8∙0	160	8.0	150	6.1	150	6.4	150	7.0		20
250	14.9	240	13.6	240	13.0	240	12.0	220	7.9	190	2.0	180	1.6	190	2.6	200	3.2	190	3.6	210	4.0	220	4.9	9·4 8·4	19 20
260 140	6.9	260 140	5·5 4·0	260 150	5.6	260 150	5·1	240 150	4·3 3·3	240 150	5.4 4.0	180 160	3·1 4·0	180 160	3·1 5·7	220 170	8.3	210 180	5·9 9·5	220 190	3·9 9·6	180	5.3	5.4	18
280	5.7	300	6.5	280	5·1	280	4.8	280	5.9	280	4.6	270	4.2	280	4.0	270	2.1		1.3	200	1.9	200	2.9	5·2 5·6	16 17
240	7.4	240	7.5	240	8.0	230	7.4	220	5.2	230	5.2	240	6.0	230	5.9	220	2.1	220	5.2	220	7.1	230	7.8	5.2	15
330 340	4.2	340 310	4'4 2'1	330	4.5	340 310	3.0	320 310	2.8	300	2.9	280	3.2	280	3.4		0.2		0.9		0.9	280	2.2	2.3	14
210	5.0	250	5.4	240	4.2	230	3.9	220	3.0	210	4·2 0·5	230	4·7 o·6	210 310	3·1	250	0.5		0.4		0.0		0.9	2.8	12 13
270	7.8	270	7.8	270	7.9	260	7.2	260	6.3	250	3.5	250	2.4		o·8		0.7	-	0.1		0.2		0.9	6.3	11
230	10.0	230	8.6	220	9.8	230	10.2	250	9.7	250	7.6	260	7.4	270	7.3	270	7·1	270	8.7	270	8.6	270	7.9	8.9	10
250	7.5	240 270	7.1	230 270	6.3	220 270	12.3	200 270	5.3	270	11.5		11.0		11.9	260	10.1	260	10.1	260	8.7	250	8.5	12.2	9
230	14.6	230	14.0	230	13.9	230	12·2 6·0	230	12.4	240 200	12·6 6·0	240 200	12·6 8·5	240 190	14·4 8·9	240 190	7.5	240 180	13·4 5·3	270 190	8.2	270	10.4	11·3 5·8	7 8
280	6.7	280	5.9	270	7.5	270	6.8	270	6.3	270	4.5	220	3.9	210	3.0	230	5.7	240	5.5	240	5.6	240	6.5	6.6	6
200	9.2	200	8.4	210	8.5	230	7.0	210	5.5	210	5.4	260	5·1	270	5.1	240	3.6	240	5.6	250	6.7	240	5.9	4.2	5
350	5.6	340 10	3.2	340 30	5·5 3·0	360 30	5.3	350 30	4·3 2·0	330	0.8	340	1.0	350	5.0 1.5	340	5.4 1.3	340	0.4		0.4		0.4	3.7	4
290	7.6	280	7.4	280	5.9	280	6.5	280	6.5	280	5·8 6·8	260	4·I	260	4.3	250	4.6	230	4·0 5·7	230 350	3.3	230 350	3.3	3.9	2 3
280	m/s. 6·9	280	m/s. 5.4	280	m/s. 4·8	280	m/s.	270	6.5	270	m/s.	240	3.2	240	3.1	210	3.0	180	3.2	230	4.9	220	6.7	5.4	I
,	1 m/s 1	0	mle	0	l m/e		l m/e l	0	m/s.	0	m/s I	0	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s. 1	0	m/s.	l	

Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$). Speed in metres per second.

191. Eskdalemuir:

Ha (height of anemograph above M.S.L.) = Height of ground above

Day.	1		2		3	, ·	4		5	5.	6	5.	7		8		9).	10	о.	1	Ι.	No	oon.
	٥	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	°	m/s.	0	m/s.	6	m/s.	0	m/s.	i °	m/s.	i °	m
I	l i	1.2		1.3		0.5		0.7		1.3		1.3		1.0		0.9		0.8		0.2		1.5	190	5
2		0.4	200	3.4	220	5.7	260	5.3	280	4.4	260	2.6	270	3.4	240	3.1	230	3.4	190	4.6	230	5.9	230	6
3	220	14.0	220	14.4	220	13.3	220	11.4	220	11.6	220	14.0	230	14.1	230	13.9	260	11.2	270	11.4		12.8	260	10
4	250	10.3	250	10.4	250	7.5	230	9.0	240	9.8	240	9.4	240	9.5	240	10.0	240	10.6	270	8.7	260	8.9	270	9
5	250	8.0	240	6.9	220	5·1	250	5.9	230	5.3	200	3.4	230	7.5	220	2.1	230	6.0	240	7.1	230	7.9	240	5
6	350	3.3	350	2.6	350	4.0	10	4.0	360	4.1	360	5.0	360	3.5	360	4.1	340	6.0	340	6.9	340	6.5	330	$ \epsilon $
7	290	5.6	280	5.0	280	3.7	290	5.0	290	4.4	340	3.2	300	3.4	310	3.1	110	1.9		1.2	310	4.3	280	3
8	180	5.0	190	6.4	170	6.0	180	7.1	190	7.5	180	8.6	220	8.9	220	6·1	230	6.0	240	7.9	250	7.5	260	1
9	330	2.0	3.40	2.4	340	4.1	360	4.6	30	6.0	10	8.3	360	6.1	360	6.8	360	6.1	360	7.0	10	9.6	30	10
10	†	†	†	†	†	†	†	†	†	†	Ť	†	Ť	†		0.2		0.2	_	0.5	_	0.3		1
11	180	4.3	210	6.1	210	4.0	190	4.2	160	5.0	180	4.9	190	6.4	180	4.2	200	5.5	220	7.1	220	8.6	210	1
12	180	7.0	160	5.9	190	8.0	190	8.8	200	11.0	210.	12.6	210	11.1	220	10.9	220	8.9	230	12.4	230	14.4	240	1
13		1.5		0.1		0.3		1.4	100	2 · I	360	3.0	360	3.4	360	4.6	360	4.5	360	2.6		I · I	220	1:
14	260	7.8	260	7.1	270	10.9	270	9.9	270	8.6	270	7.9	260	6.5	260	6.4	240	9.0	240	8.5	230	8.9	210	19
15	240	2.8	150	2.2	<u> </u>	1.0		0.7	_	0.8	130	3.8	120	5.6	120	6.7	120	8.0	120	11.0	120	9.5	130	1
16	+ 1	14.8	†	15.8	†	17.3	†	16.3	†	15.9	t	12.2	†	9.4	260	8.5	250	10.6	250	10.6	240	8.7	220	1
17	200	7.3	220	9.0	220	8.9	210	10.0	220	10·1	210	9.9	220	11.4	240	12.0	270	10.1	300	6.5	290	7.6	270	9
1 8	240	10.1	240	10.6	230	12.8	230	11.0	230	8.9	250	10.0	240	10.8	240	10.0	260	8.5	270	6.9	270	10.0	280	110
19	300	10.9	300	11.5	310	10.7	300	9.8	300	9.4	320	7.5	330	7.5	340	8.0	340	7.4	320	10.2	320	10.0	320	
20	300	6.8	310	7.2	330	7.8	330	5.8	300	6.4	330	7.0	340	9.4	340	9.6	340	8.5	340	7.2	350	6.5	360	1
21	1 +	4.1	†	4.2	†	4.5	t	5.5	†	4.5	†	3.2	†	2 · I	340	3.6	340	3.4	340	4.2	340	3.6	340	;
22	360	5.0	360	5.2	360	3.8	360	5.0	360	5.5	360	5.2	360	3.9		1.0	360	4.9	10	4.9	10	4.2	360	1
23		1.0		o·8		0.7		0.7		1.0		I · I		1.3		1.0	Ť	2.9	†	1.6	1	2 · I	†	13
24	350	5.0	350	4.0	330	4.1	360	5.6	360	4.9	360	4'4		1.2		0.9	_	0.0	_	0.5		0.2		(
25	-	0.4		0.6		0.4	_	0.2		0.9	150	4.0	140	3.3	150	2.2	180	4.6	180	5·1	190	5.4	210	1
26	160	2.6	180	3.5	190	3.1	180	2 · I	170	3.1	_	1.3		1.2		0.2	170	2.6		1.5	170	1.6	180	
27		1.3		0.2		1.0		0.1		0.2		0.6		0.4		0.2		1.3		0.4		1.3	=	
28	30	2.5	360	3.0	20	4.8	30	5.6	30	8.1	30	6.9	20	4.5	30	4.0	10	4.6	40	5.1	50	5.3	10	13
29	10	5.8	10	4.7	10	5.3	10	6.0	10	7.6	10	6.4	360	4.5	360	4.9	10	4·1	T	5.2	†	5.4	T	1
30		0.4		0.4		0.2		0.2		0.3	_	0.2		0.4		o·8		0.7		0.3		0.2		-
ean ‡		5.3		5.5		5.6		5.7		5.8		5.7		5.6		5.3		5.6		5.7		6.1	_	1

192. Eskdalemuir: $H_a = 235 \text{ metres} + 15 \text{ metres}$.

							•																	
	1 0	m/s.	0	m/s.	0	m/s.	٥	m/s.	°	m/s.	ı °	m/s.	°	m/s.	0	m/s.	°	m/s.	l °	m/s.	°	m/s.	ı °	m/s.
I	180	5.6	180	5.9	190	5.1	230	4.6		0.4	l	0.7		0.2	†	2.5	Ť	2.1	-	0.2		0.3	-	0.6
2		1.1		1.5		1.1		1.0	130	4.5	140	6.0	130	7.0	150	9.6	180	9.0	250	6.5	210	5.8	210	6.1
3	240	2.5		1.2		1.5		0.8	240	2.2	<u> </u>	1.0	_	0.6		0.4	l	0.4		0.6		0.9		0.9
4	<u>-</u> -	0.1		0.1		1.5	140	4.0	130	3.6	130	5.6	130	5.0	130	4.6	130	4.7	130	4.1	120	3.7	110	2.9
5	360	1.8	360	1.6	_	0.6	l	1.2	_	1.4	360	3.9	360	6.8	360	7.9	360	7.2	10	7·1	10	7.6	360	7.0
	١		ľ				l				1					ļ			ł		Į.		1	
6	360	6.6	350	3.6	360	3.0	330	2.9	330	3.6	l —	I · I		1.1		0.3		0.6		0.5	_	0.5	_	0.5
7	190	3.4	160	5.1	160	5.1	160	7.1	150	8.1	150	7.5	150	7.0	150	6.6	150	8.5	160	8.0	160	9.6	160	10.6
8	180	6.6	180	9.6	180	8.4	190	7.1	190	7.1	200	6.3	260	9.9	270	10.8	270	15.0	270	12.6	280	10.5	290	10.3
9		0.2	_	0.4		0.4		0.3		0 · I		0.2		0.5		0.2		0.5		0.0		0.0		0.3
10	190	8.0	210	9.4	210	10.2	200	7.2	200	6.4	190	5.8	190	6.6	200	6.1	210	7.1	210	8.8	220	10.2	220	10.0
	_		[1	1	ł	1	ì		l	l	ł				l		ŀ		l	
11	190	6.5	190	6.6	190	6.9	190	8.4	180	7.1	180	7.5	180	8.9	190	8.5	180	7.6	190	8.4	190	9.5	200	10.1
12	180	9.0	180	9.0	180	9.0	170	8.1	180	9.5	190	10.0	190	10.1	190	10.1	190	9.8	190	10.6	200	10.0	200	11.1
13	190	10.0	180	9.5	180	9.0	260	7.0	300	6.2	330	4.5	360	4.6	340	3.0	310	4.1	280	3.1	300	1.6	290	5.7
14	180	3.8	190	5.5	190	7.5	200	9.4	200	10.0	210	14.0	200	12.6	210	14.2	170	7.I	210	9.9	220	10.2	230	14.5
15	280	7.0	280	5.1	280	5.1	280	4.5	300	6.4	290	6·1	300	5.6	290	7.3	280	7.7	260	2.2	270	3.6	270	3.6
	1	'	Ì				1		Ī .		ĺ		ĺ	1		1		1				0		
16	240	11.9	240	7.6	240	7.1	240	9.0	240	8.2	250	11.9	250	11.0	250	10.9	260	10.2	270	11.4	270	11.8	270	12.0
17	250	7.0	250	7.5	250	6.5	250	6.0	230	5.7	230	5.3	220	5.9	230	8.6	250	9.8	250	10.1	220	7.0	230	7.1
18	270	11.1	270	10.7	270	12.4	270	10.5	270	11.0	270	12.5	270	10.5	270	12.7	270	11.0	280	11.2	280	12.2	270	12.7
19	300	7.1	300	6.5	300	4.8	300	3.6	170	2.5	210	2.3	280	3.2	300	4.1	280	4.5	310	6.0	320	6.9	320	9.2
20	350	11.0	360	9.5	360	9.9	360	10.1	360	9.9	360	7.4	350	4.9	350	5.3	340	6.5	330	7.9	300	5.1	310	5.6
	33		ľ	' '	٦		ľ				Ĭ	' '	1				Ī			i i				
21	290	3.9	300	5.3	300	4.2	300	4.5	300	5.0	300	5.5	290	3.8	290	2.4		0.8	_	0.2		0.0		0.0
22	180	3.1	210	2.6	210	2.4	170	4.4	240	5.6	270	11.5	280	13.9	290	15.1	280	15.2	290	17.1	300	17.2	300	15.6
23	270	6.8	280	7.5	290	7.6	300	12.0	300	10.8	290	14.9	290	14.6	290	12.5	290	10.9	300	14.3	310	13.0	310	10.0
24	270	2.6	270	5.0	260	5.0	220	4.3	230	6.5	240	8.4	250	8.4	260	6.6	280	8.7	300	9.9	320	8.0	300	8.6
25	1 -	0.6	250	5.5	290	4.5	l t	†	Ť	†		0.0		0.0		0.0		0.0		0.1		0.4		0.3
,	ł				-	•	1		· '	'			l										- 6 -	
26	10	3.4	10	3.6	20	3.9	20	4.8	30	6.4	30	6.5	30	6.8	50	5.9	40	4.7	50	3.9	10	2.6	360	3.6
27	l t		l t	1 1	1	t	l †	1	Ť	1 † 1	ΙŤ	†		0.5		0.5		0.4		0.1		0.2		1.1
28	360	4.6	360	5.1	20	5.8	360	8.4	360	9.4	360	5.1	30	3.0	240	1.8	340	4.0	340	6.4	340	6.6	340	6.5
29		0.4		0.4		0.5		0.5		0.5	-	0.6		0.6		0.4		0.2		0.4		0.7		0.4
3ó	190	3.5	200	2.6	200	†	200	†	260	2.0		0.9		0.9		0.9	310	1.6		1.3	320	1.7	340	1.6
3.	1	3 3	1			i i	ł				į		l											
31	l —	0.6		0.5		0.9	_	0.9		1.0		0.9	—	0.6		0.2	180	1.9	170	4.0	160	3.2	220	3.1
	 												 	<u> </u>				6.5		6.8		6.7		7.1
Mean §	-	5.4		5.3	-	5.4		5.6	_	5.9		6.2		6.2		6.4	_	6.5	_	0.3		0.7		1
	1		<u> </u> 	1	<u>'</u>		<u></u>	<u>' </u>	<u> </u>	1	<u> </u>	1	i –		ī		Ī				<u> </u>		\ \r	
G.M.T.		I.]	2.		3⋅		4.		5.		6.	1	7∙	1	8.	1	9.		10.		11.	No	on.
			 				<u> </u>				<u> </u>		<u> </u>		<u> </u>		<u> </u>		<u> </u>		<u> </u>		<u> </u>	

Averages for periods of sixty minutes, centred at the exact hours, Greenwich Mean Time.

M.S.L. $+ h_a$ (height of an emograph above ground) = 235 metres + 15 metres.

November, 1923.

13	3.	14	. .	15	j.	16	j.	17	,.	18	3.	19	.	20	.	21	.	22	.	23	.	24		Mean	Day.
200	m/s.	180	m/s.	210	m/s.	200	m/s.	210	m/s. 3·6	210	m/s.	210	m/s.	°	m/s.	0	m/s.	-	m/s.	•	m/s.	,	m/s.	m/s. 1·8	
230	7.2	220	7.3	220	6.8	220	7.1	210	6.6	200	6.7	190	7.2	190	10.0	190	9.5	190	9.8	210	11.0	220	13.0	6.0	2
260	11.0	250	12.1	260	12.4	260	10.8	240	9.6	250	10.0	250	12.8		11.5	240	14.6	250	11.5	240	10.1	250	10.2	12.1	3
250	9.2	240	10.1	250	9.8	240	10.0	240	9.0	240	9.4	260	9.1	250	9.5	250	8.9	260	6.9	250	6.0	240	7.2	9.1	4
240	4.1	230	3.4	230	1.6	250	2.2		1.4		0.9		0.6		1.4		1.1	_	1.0	350	2.6	350	3.2	4.3	5
340	6.8	330	6.6	310	5·1	310	3.4	310	1.8		0.4		0.2	320	3.6	300	6.1	280	5.5	280	5.2	280	5.5	4.4	6
260	3.1	260	3.6	230	3.6	240	3.8	220	1.7		0.9		0.4		1.2		0.2		1.0	190	2.4	190	4.8	3.0	$\frac{7}{8}$
260	4.6	250	5·1 8·8	140	4.9	170	4.2	200	3.8	210	8.6	210	8.6	200	4.2	230	4.5 6.9	170	1.8		2.6		0.6	5.2	_
40	1.2	30 360	2.3	40 270	2.5	30 260	6.4	20 240	7·6 2·9	20 230	2.6	30 †	†	20 †	7.0	†	†	10	4.8	30 200	3.0	20 180	3.5	_	9 10
210	7.1	210	6.9	200	7.4	200	6.6	200	7.0	190	7.0	190	6.6	190	7.1	190	7.0	18o	6·o	200	7.6	200	7.9	6.2	11
240	14.0	250	11.8	260	11.5	260	9.4	250	7.5	250	6.5	250	5.5	270	2.9	250	1.6	220	2.4	170	2.8	170	2.9	8.6	12
220	11.6	210	10.1	210	8.5	200	8.5	200	9.5	200	10.3	190	10.6	190	11.0	200	11.5	230	9.9	260	6.5	260	6.5	6.0	13
250	11.4	270	11.1	260	8.0	250	7.4	260	7.9	260	7.2	260	5.6	250	8·o	240	4.1	-	1.4	240	3.0	240	4.0	7.6	14
140	7.8	170	4.1	220	4.1	240	2.1	250	6.0	210	5.4	220	3.1	250	3.0	270	9.9	l †	13.2	†	12.2	†	14.9	6.0	15
220	7.0	220	7·1	220	6.1	210	4.6	220	6.5	210	6.9	210	6.8	200	4.2	200	9.0	170	6.2	190	7.0	220	7.1	9.5	16
270	10.3	240	11.5	240	12.1	230	11.9	220	10.5	220	11.0	230	10.7	230	11.0	230	10.2	240	8.9	230	9.0	240	10.6	9.9	17
290	10.2	280	10.1	270	10.0	270	9.9	290	12.6	290	13.7	290	12.6	280	10.9	300	10.4	310	10.0	320	7:4	280	5.8	10.3	18
310	10.0	310	12.0	310	12.6	310	11.7	310	9.0	310	8.3	300	7.0	300	7.1	300	7.5	300	9.9	300	9.8	290	9.5	9.4	19
360	6.6	360	5.2	360	4.2	360	4.6	360	0.1	10	6.7	10	6.3	10	5.4	360	2.5	360	4.7	20	5.0	20	3.4	6.4	20
	1.5	-	0.9	†	1·8	†	2.5		0.9	360	4.9	l t	4.2	†	5.0	, †	4.0	†	2.9	Ť	5.1	360	4.6	3.2	21
360	2.0	360	2.7		1.4	360	2.4	360	3.6	360	3.0	360	2.8		1.3	_	1.4		1.3		1.1		0.8	3.3	22
360	4.1	36 0	3.4	360	3.0	360	3.4	360	4.2	360	4.0	360	4.0	360	4.0	36 0	2.6	360	7.0	360	5.6	350	5.3	2.8	23
-	0.3		0.4		0.2		0.1		0.1	_	0.1		0.3		0.3		0.3	7.00	0.2	180	0.2	180	0.4	1.5	24
210	6.5	220	5.5	210	5.9	210	6.4	210	5.0	220	5.2	-	0.9	180	3.2	190	4.6	190	3.1	100	3.4	180	3.2	3.6	25
-	0.4	_	0.4	_	0.3	_	0.3	_	0.2	_	0.0	_	0.3		3.5	330	3.3	350	2.7	340	0.5	300 360	1.6	1·3 1·1	26 27
50	0.4 0.4	20	3.2	30	3.9	30	4·I	40	5.0	20	5.1	20	5.1	330	6.4	20	6.2	20	6.8	10	7.4	20	6.5	5.0	28
50	6.5	l #	4.0	†	3 9	†	3.6	l †	4.6	l Ŧ	5.0	Ť	3.8	ĪŤ	3.0	Ť	5.1	Ī	4.8	l Ŧ	3.4	Ī	2.0	4.9	29
160	1.6	170	3.0	190	2.9	180	3.3	190	3.8	170	3.4	180	4.2	190	7.0	190	8.5	190	6.5	200	8.9	180	6.9	2.6	30
_	6.3	_	6.0		5.6		5.4		5.3	_	5.3	_	4.9	_	5.2	-	5.5		5.2		5.3	_	5.4	5.6	‡

December, 1923.

13.		14	.	15	j.	16	5.	17		18	3.	19).	20).	21		21	2.	2	3.	2	4.	Mean	Day.
_ 7	7.1		6.6		5.7		5.7		5.2		5.1		5.1	-	5.2	_	5.2	_	5.2		5.7	_	5.8	5.9	§
220 4	4.0	230	2.8		1.1	180	1.7	180	1.9	190	3.1	210	2.4	300	4.1	290	9.9	290	12.0	300	12.1	300	12.4	3.3	31
200 2 340 6 — 0	1·6 2·3 6·3 0·4 1·4	180 340 — 350	1·4 1·6 8·4 0·4 2·0	360 150 360 —	1·7 2·5 6·5 0·4 1·5	140 360 —	0·9 2·6 4·1 0·4 0·9	130 360 —	1.0 2.5 4.1 0.4 0.5	170 360 —	0·4 2·5 4·0 0·4 0·4	170 — —	1·2 2·5 1·4 0·4 1·5	170 180 320	2·3 1·6 2·1 0·3 0·9		0·9 0·4 0·5 1·0	160 — — 180	3.4 1.4 0.4 2.5 0.4	140 — — 190 —	6.0 1.5 0.4 3.0 0.5	140 10 — 200 —	3·2 0·3 3·1 1·0	 4·4 0·7 	26 27 28 29 30
300 13 310 10 350 8	0·0 3·0 0·0 8·4	 300 310 360	0.1 8.1 6.0	280 310 10 150	0·0 7·5 8·7 8·8 2·0	280 300 10 140	0·0 8·9 8·6 6·0 6·5		0·0 10·1 5·1 5·6		0·0 8·5 5·9 1·4 3·0	 290 290 90	0·9 9·6 2·5 1·5 3·3	190 290 230 — 50	2·4 10·0 4·0 0·8 2·3	190 290 270 — 40	2·5 10·5 2·9 0·4 2·8	210 280 200 — 40	4.0 9.2 2.7 0.4 3.4	210 270 260 — 50	7·7 4·1 0·4 3·8	190 270 240 — 20	6·8 3·0 0·4 2·8	8·7 5·2	21 22 23 24 25
230 7 280 15 320 10	1·0 7·5 5·3 0·2 5·2	270 220 290 320 300	10·3 8·0 14·4 9·9 4·5	270 230 290 320 280	11·8 11·2 11·1 9·9 4·1	270 240 290 310 280	12·5 12·5 9·9 10·6 4·1	300	10·6 14·8 9·0 10·4 4·0	270 260 300 300 260	8·5 13·9 8·8 12·2 3·4	270 270 290 300 280	7·0 14·7 9·1 12·3 5·0	270 270 290 310 290	7·3 13·5 9·7 13·0 5·0	260 280 290 320 290	4·9 15·0 8·6 13·6 4·1	250 270 290 330 300	4·0 11·3 7·3 14·0 5·4	260 270 280 320 300	7.0 12.3 6.6 13.8 6.4	260 270 290 330 290	6·9 10·7 6·0 12·6 4·0	9·4 9·6 10·7 8·3 6·4	16 17 18 19 20
200 IO 290 5 230 IO	0·5 0·5 5·1 6·0 3·7	200 180 300 230 280	11·3 9·5 5·6 14·1 3·1	190 190 160 220 270	9·1 8·2 2·9 10·6 2·5	190 190 250 220 270	7·5 9·4 1·8 10·4 2·6	190 190 — 260 210	10·6 8·9 1·2 8·4 3·0	190 190 270 190	8·5 9·5 0·6 8·4 3·6	190 190 — 280 180	10·5 9·6 0·2 11·0 3·9	190 190 — 280 180	11·2 10·2 0·5 9·0 4·3	190 190 — 280 200	10·7 10·0 0·2 8·6 5·6	200 190 280 230	11·5 10·2 0·0 7·6 7·5	190 190 280 240	11·2 10·0 0·8 6·1 9·0	180 190 190 280 250	11·3 10·1 3·5 7·0 9·8	9·0 9·7 3·9 9·8 5·1	11 12 13 14
160 16 280 9 160 1	0·2 0·0 9·2 1·7		0·6 10·5 8·1 1·0 7·8	150 290 — 200	0·9 8·4 5·2 0·6 5·4		1·0 9·0 2·5 3·2 7·5		0·1 6·5 1·7 3·6 8·6	150 280 170 210	0·0 5·1 3·8 2·6 8·5	160 280 200 210	0.0 6.4 3.0 4.5 7.3	160 — 190 210	0·1 7·1 0·2 3·3 9·0	160 — 160 210	0·2 6·6 0·4 2·5 7·7	160 — 170 190	0·4 7·0 0·3 4·0 5·4	170 170 — 180 190	1·8 5·5 0·2 6·6 5·8	190 180 — 190 190	3·4 7·3 0·2 7·5 5·5	1·4 7·3 6·2 1·7 7·7	6 7 8 9
210 6 150 2 — 1	m/s. 0·3 6·1 2·4 1·4 5·4	200 - 360	m/s. 1·4 3·8 0·9 0·9 5·6	220 190 — — 360	m/s. 3·5 3·2 0·1 0·7 5·5	180 210 — — 360	m/s. 2·5 3·7 0·0 1·0 7·5	180 210 — — 360	m/s. † 2·5 0·0 1·5 6·6	170 — — 330 360	m/s. 1·6 1·0 0·0 1·6 7·6	160 — — — — 360	m/s. 3·1 1·3 0·4 1·3 6·5	160 240 — — 360	m/s. 4·8 2·8 0·2 0·8 6·1	180 240 — 20 360	m/s. 5·4 1·7 0·1 2·5 7·0	180 230 — 360 360	m/s. 5·0 2·3 0·1 2·0 7·1	180 240 — 10 360	m/s. 6·0 3·6 0·1 2·6 6·6	260 10 360	m/s. 1·5 3·1 0·1 2·2 7·8	m/s. 3.9 0.8 2.4 5.4	1 2 3 4 5

HIGHEST INSTANTANEOUS WIND SPEED RECORDED EACH DAY BY THE DINES TUBE ANEMOGRAPH.

193. Eskdalemuir: $H_a = 235 \text{ metres} + 15 \text{ metres}$.

1923.

						· ·																		
	J.	an.	F	eb.	М	ar.	A_{I}	oril.	М	ay.	Ju	ine.	Jı	ıly.	A	ug.	Se	pt.	0	ct.	N	ov.	D	ec.
Day.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.
1 2 3 4 5	m/s. 8 22 19 12	h. m. 23 45 18 10 3 45 6 15 2 10	m/s. 27 27 27 24 11 25	h. m. 23 50 1 5 1 30 1 40 12 30	m/s. 9 16 11 7 18	h. m. 24 0 20 30 0 35 3 10 15 15	m/s. 8 8 6 9	h. m. 7 15 13 15 13 35 9 50 22 55	m/s. 19 10 11 15	h. m. 6 40 14 35 15 25 16 15 13 45		h. m. 11 10 16 35 12 10 5 5 18 30	m/s. 12 15 15 13	h. m. 17 15 23 15 0 30 14 10 10 10	m/s. 13 28 22 10	h. m. 12 35 21 30 11 40 6 40 11 20	m/s. 10 7 15 14 18	h. m. 15 5 17 0 21 55 1 20 14 55	m/s. 15 24 12 12	h. m. 8 45 5 20 18 45 0 25 13 0	m/s. 12 17 29 19	h. m. 13 10 23 30 16 0 9 40 0 20	m/s. 10 17 5 9	h. m. 23 o 7 55 4 45 7 o 18 30
6 7 8 9	14 19 22 25 24	24 0 23 5 3 45 15 5 11 0	20 23 11 10 16	2 25 10 45 2 50 23 45 11 40	19 16 11 10 9	12 20 1 35 5 45 9 50 13 30	15 13 19 15 15	9 50 1 50 14 30 15 5 3 30	13 13 14 16 22	19 55 11 40 13 55 22 15 16 0	12 17 23 20 28	17 0 23 55 9 55 5 35 15 20	8 14 12 9 12	18 0 11 50 17 30 12 20 11 40	14 13 16 13 12	13 15 8 40 13 15 19 10 0 10 17 5	15 15 15 17 12	16 35 0 45 14 30 11 45 14 55	16 22 16 27 19	10 5 22 30 0 5 11 20 16 5	10 8 15 16 †	10 10 1 30 6 40 12 45 †	12 17 25 10 16	0 10 14 5 9 40 24 0 2 45
11 12 13 14	19 6 11 26 25	13 25 0 40 20 20 22 20 5 15	15 8 12 11	5 5 9 25 21 55 1 15 22 55	9 16 14 10 14	13 50 22 15 1 50 15 30 15 10	15 14 13 15	2 45 3 10 12 55 15 0 17 35	19 18 15 20	13 45 13 45 15 25 17 5 14 50		5 45 11 30 7 50 18 55 18 20	10	16 10 12 10 18 30 9 50 13 5	9 8 12 10 15	11 20 13 25 4 10 12 35 18 20	21 21 15 16	14 45 10 25 20 50 0 50 13 10	17 12 9 9	8 25 5 10 10 40 9 35 14 40	13 22 19 19	10 55 12 15 20 55 13 15 23 55	18 17 15 21 16	22 20 11 35 0 35 12 55 23 5
16 17 18 19 20	8 10 9 24 25	0 15 14 10 19 35 20 0 6 10	12 18 19 9 12	21 30 5 30 4 10 11 35 23 0	14 15 12 13	2 20 15 15 10 30 14 30 12 55	12	2 5 10 5 12 30 16 35 15 30	14 20 12 12	16 30 10 0 20 0 14 25 11 35	10 10 16 17	1 15 14 20 22 50 8 25 23 10	15 11 19	16 20 14 55 17 5 17 5	16 14 11 9	1 0 † 13 40 2 0 21 25	14 19 12 15	14 5 11 50 15 35 16 25	12 16 15 27 23	9 40 3 40 23 45 7 5 14 20	25 21 20 17 16	3 10 2 5 18 0 14 50 8 5	26	16 0 20 45 10 55 21 50 4 15 0 5 1 40
21 22 23 24 25	22 23 19 19 17	23 2 7 5 22 45 15 20 14 25	7 7 7 11 8	5 0 18 30 11 0 10 50 11 40	9 10 8 11 19	5 30 20 0 8 45 14 0 14 55	25 14 16 15 18	11 40 0 45 11 50 23 0 14 50	20 10 9 17	3 15 13 5 14 5 22 15 16 30	16 19 15 17 8	16 55 12 40 0 25 14 45 0 5	18 17 20 13 21	3 55 23 55 0 5 14 10 18 55	27 16 16 13	7 55 15 15 2 5 15 15 18 10	11 16 † 11 18	15 35 5 25 † 13 5 15 0	20 20 14 22	7 35 22 35 0 55 15 15 17 15	9 9 12 9 10	4 10 5 5 22 15 3 55 12 35	27 22 17 9	10 40 6 40 10 0 15 55
26 27 28 29	17 18 11 13	2 0 22 0 23 5 6 30	22 19 10	II 40 I 20 6 20	11 12 10 6	14 45 21 0 3 25 15 45 14 10	14	14 25 15 45 12 30 15 25	16 17 21 15	5 20 16 0 18 20 0 20		10 0 12 35 13 30 21 40	24 13 8 11	15 10 0 35 16 45 14 40	16	12 30 12 5 15 30 23 50	15 23 26 8	0 45 14 15 3 30 11 30	15 21 17 21	16 30 4 5 3 25 15 45 5 0	7 5 12 11	1 55 22 20 5 5 5 30 22 50	13	7 35 15 35 4 45 23 30 0 50
30 31	15	22 45 22 20			55	15 45 15 20	18	23 45	11	10 5	13	2 15	13	0 45	7	3 35	10	11 23	14	3 10	^4		_	23 55

† Defective record.

DISTRIBUTION OF WIND SPEED: EXTREME VELOCITIES, AS RECORDED BY THE DINES TUBE ANEMOGRAPH.

194. Eskdalemuir: $H_a = 235 \text{ metres} + 15 \text{ metres}$.

1923.

		DIS	TRIBUTI	ON OF W	IND SPE	EED.					EXTREM	E VELO	OCITIES.			
Month.	More than 1	7·1 m/s.	10.8 to	17·1 m/s.	5.5 to 10.7 m/s.	1.6 to 5.4 m/s.	Less than r.6 m/s.	No Record.]	Highest Ho	ourly Wind		Н	ighest G	ust.	
	Dates of Occurrence.	Duration.	No. of Days.	Duration.	Duration.	Duration.	Duration.	Duration.	Veer from N.	Speed.	M Tir		Speed.		Date	
Jan	 	hr.	17	hr. 149	hr. 306	hr. 191	hr. 96	hr.	300	m/s. 17	day. 20	hour. 6	m/s. 26	day.	h. 22	m. 20
Feb	 2nd, 5th	2	10	64	218	280	108	0	200	17	5	13	27	2	I	5
Mar	 		3	10	216	378	133	7	200	13.	25	13	19	25	14	5 5
April	 -		4	16	32 ⁵ 3 2 5	252	128	. 9	40	14	21	16	25	21	11	40
Мау	 	_	7	29	399	220	96	0	210	15	10	16	22	10	16	o
June	 10th	3	10	72	258	275	96	16	250	18	10	19	28	10	15	20
July	 _	_	6	28	274	331	106	5	280	15	26	17	24	26	15	10
Aug	 2nd, 21st	4	7	43	268	297	94	38	170	19	2	21	28	2	21	3 0
Sept	 28th	2	6	44	330	245	79	20	230	19	28	3	26	28	3	3 0
Oct	 _		13	98	367	228	51	0	190	17	30	5	27	19	7	5
Nov	 16th	1	10	67	264	239	137	12	270	17	16	3	29	3	16	0
Dec	 22nd	ı	12	75	268	201	185	14	300	17	22	11	27	22	10	40
Year	 8 days	13	105	695	3,483	3,137	1,304	123	230	19	Sept. 28	3	29	Nov. 3	16	0

MINIMUM TEMPERATURE "ON THE GRASS" DURING THE INTERVAL 18H. TO 7H. G.M.T.

Readings, in degrees absolute.

195. Eskdalemuir.

1923.

Day.	Jan.	Feb.	Mar.	April	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
	<i>a</i> .	a.	a.	a.	a.	a.	<i>a</i> .	<i>a</i> .	a.	<i>a</i> .	<i>a</i> .	a.
1	63.8	80.0	74.4	77.1	77.8	78.3	77.2	80.7	72.9	82.0	70 · 2	73.0
2	63·4	76.9	74.0	74.0	73.0	76.3	81.3	74· I	74.2	75.8	71.8	74.0
3	75.5	76.6	75.3	72.0	75.9	75.0	84.3	83∙0	67.6	75.0	78.3	70.6
4	70.1	70.2	72 · 1	76.0	72.0	76.2	83.9	80.4	80.2	72.0	73.8	70.3
5	71.6	71.0	70.7	74.3	79.7	70.7	85·o	76.4	79.0	67.8	73.0	65.4
6	69.8	81.2	73.7	72.8	73.5	78·o	84·o	81.9	83.3	77.8	69.0	68.9
7 8	73.9	71.8	75.9	73.4	73·5 67·5	80.3	85.3	85.8	81.9	79.0	66.9	65.8
8	78.7	76.1	73.6	76.3	74·8 67·5	81.0	86·o	78·o	72.0	75.0	66.2	75.8
9	72.8	69.3	73.9	72.9		82.0	84.0	86∙0	83.6	79.3	70.2	64.4
10	73.0	71.5	71.2	71.7	69.0	82.0	85·o	81.0	75.3	78·o	71 · 2	71.6
11	70.9	76.8	72.8	73.2	73.0	76.2	86.8	79.2	79.3	75.0	71.0	78.9
12	67.2	74.1	72.7	77.0	72.0	76·1	84.9	76.0	83.6	70.6	79.8	78·8
13	64.5	72.0	.76.6	78.5	70.9	81.6	80·1	85.2	75.6	71.2	73.0	76.2
14	76.2	72.6	70.9	75.6	71.2	74.2	85∙0	76.7	81 · 1	67.2	72 · 2	69∙0
15	·	71.0	74.8	70.8	70.0	69.4	86·o	76·1	72.0	70.2	65.3	72.6
16	76.9	73.8	75.0	71.9	72.9	74.0	84.5	8o·o	73.5	77.0	68.6	74.9
17 18	77.0	74.1	71.5	67.5	69.0	68.2	79.9	81.9	72.8	66.9	73.0	79.0
18	72.2	70.0	72.2	67.9	69.6	79.9	75.4	82.5	75.0	77.8	72.0	74.9
19	76.5		71.3	70.2	77.2	74.8	78·o	81.0	74.0	82.0	72.5	66.9
20	73.3	69.7	71.0	67.0	76.4	76·o	86.2	81.7	72.9	74.0	70.7	65 · 1
21	66.5	68.7	70.0	72.2	75.2	81.0	83·o	83.7	75.6	79.0	70.0	67.7
22	78.0	70.5	72.8	74.0	74.9	83.2	85.5	78.8	73·I	76.8	71.2	72.8
23	65.8	69.2	70.6	71.2	73.1	82.9		79.0	74.8	77.4	69.8	72.0
24	75.6	70.2	68.8	66.2	69.9	82.6	8o·6	80⋅3	73.3	74.0	66.3	67·o
25	78.7	73·1	72.0	73.0	· 75·5	79.0	83.5	72.0	75.9	74.3	61 · 3	60.0
26	77 · 4	72.3	72.2	76.3	75.2	71.0	79.7	80.7	79.5	74 · 1	72.8	71.0
	78 · i	75.8	78.2	66.5	75.1	79.3	77.3	81 · 1	83.1	76.4	69.9	71.8
27 28	79.6	75.7	80.2	66.3	75.7	83.0	81.9	79.9	84.4	78.3	68·1	72.9
29	77.5		74.9	70.6		75.0	83.1	71.0	78.6	78·1	71 · 2	60.3
30	79·o	_	71.0	76.6	77.5	8o·o	82.0	77.9	84.9	74 · 2	63.1	72 · I
31	79.5	_	69.8		76.9		82.5	75.5		78.7		73·1
an	73.4	73·I	73.0	72.4	73.4	77.6	82.7	79.6	77.1	75.3	74 · 1	70.9

Notes.—(1) The initial 2 or 3 of the readings is omitted, i.e., 275.0 is written 75.0.

⁽²⁾ The minimum refers to the interval from 18h. the previous day to 7h. on the day to which it is entered. Means for January, May and July are for 30 days only. Mean for February is for 27 days only.

196	Eskdalemuir.	. 1886-1986 manada an B ay an mangga pagagina yang man a man ngalijish biyaya	na ana ali gayanggan man Aliffeld aya nguh bib alikun dan a di ninggana ng Aliffelinggan bib													January, 1923.
		Cloud Forms,				oud . MI F						Wea	ther.			
Day.	7 h	13h	18h	7h	9h	131	15h	18h	2 I h	7h	9h	13h	15h	18h	21h	Remarks.
1 2 3 4 5	Nb. St. Cu. Nb.	Ci. St. St. : St. Cu. St. Cu. Ci. Cu. : Ci. St. Nb.	A. St. : St. Nb. St. St. Cu. : Cu. A. St. : St. Cu.	0 10 4 0	5 10 5 0	7 10 10 5	10 10 10 3	10 7 0	10 10 2 10		1 •≡° 1 d	 •≡°		□=° ··· ···	● ≡ ⁰ ≡ ⁰	$\begin{bmatrix} o & \bigoplus & \bigoplus \\ b & \bot & \text{to } c & \bot & a : c & \bot & \text{to } o & \coprod & \bigoplus^0 & p : o & \\ o & \bigoplus & \text{to } o & a : o & \text{and } o & p : o & \bullet & n : \\ o & \bigoplus & \text{early, bc } a : o, \text{ and } op^0 & p : c & \text{to } b : \\ b & \coprod & \text{to } bc & a : b & \text{and } bc & p : b & \text{to } o & \boxtimes^0 & p : \\ od & \bigoplus^0 & \text{to } o & \bigoplus^0 & a : \text{od } \text{and } o & p : c & \text{and } o $
6 7 8 9	St. Cu. Nb. St. Cu. St. Cu. St. Cu.	St. Cu. St. St. Cu. St. Cu. St.Cu. : F.Cu. : Ci.Cu	St. Cu. Nb. St. Cu. St. Cu. St. Cu.	1 10 9 9	3 10 4 7 8	10 10 5 10	8 10 1 10 10	10 1	10 3 10 1	d≡: 	d ₀ ≡ ₀	 ≡° e 	d ≡° p * °	d ≡⁰	d °≡	blat first; b, op $\Re^0 a$: c, op and o p : o od \equiv : to $\equiv^0 a$: od $\equiv^0 p$: od \equiv : n : o \bullet q early; bc a : b and bc p : bc n : o \bullet \equiv^0 , c to o a : o and op $\Re^0 \Re^1 p$: o, o $\Re^0 \circ a$ t first, o to c a : c, op $\Re^0 \circ a$: o
11 12	St. Cu. St. Cu.	St. Cu. A. Cu.	St. Cu. St. Cu.	3	3 6	5 4	4 7		2 0	<u>ר</u> ב					 ப	b \sqcup to bc a : bc, b, op $^{0} \bullet p$: b to op $^{0} \circ \sqcup$ to bc a : c and bc p : bc to b \sqcup :
13	St.	Nb.	Nb.	10	10	10	10		0	=	* ⁰p≡	d ≡ 0	d <u>≡</u> 0	d ≡º	≡ :	$ \begin{array}{c} [o \equiv \vdots \\ o \equiv, \text{ op } {}^{0}\text{\bigstar to od \equiv^{0} } a : \text{ o D \equiv^{0}, od \equiv^{0}} \\ \text{[bc and op } {}^{0}\text{\bigstar} \end{array} $
14 15	St. Cu. : Nb. St. Cu.	F. Cu. St. Cu.	St. Cu. St. Cu.	10 4	5	10	10	8 7	4 6	•	 d0					o \bigcirc \bigcirc \bigcirc early; o \bigcirc to ba: b to c, op \bigcirc be to od \bigcirc a: o, c and op \bigcirc \bigcirc p: c and be
16 17 18 19 20	Nb. St. Cu. St. Cu. : Cu. A. St. : St. Cu. St. Cu.	St. St. St. Cu. St. Ci, St. : F. Cu.	St. Nb. Ci. St. : A. Cu. St. Cu. St. Cu.	10 10 10 1	10 10 5 10 4	10 10 4 10 4	10 6	10 I 10 I	0 0 0 1	$\begin{matrix} \mathbf{d}_0 \equiv_0 \\ \cdots \\ \cdots \\ \cdots \\ \end{matrix}$	d ≡ ⁰ ∞ ≡ ⁰ p * ⁰	≡ ⁰ ≡ ⁰ 	≡ :	d ₀ ≡ ₀ 	=: •°=° · ·	od \equiv^0 to $o \equiv^0$ $a: o \equiv \vdots$, $o \equiv^0$ $p: o \equiv \vdots$ o $a: o$ to od \equiv^0 $p: o \bullet^0 \equiv^0$ $n:$ b and be $a: b$ to o $p: o$ $n:$ [b o, o to $o \equiv^0$ $a: o \bullet \equiv^0$ and o $p: o$, b, op \bullet b, bep $\circ *$ $a: b$ to b $p: b$ to b i i]
21 22 23 24 25	Nb. Nb. St. Cu. St. Cu. Nb.	St. Cu. : St. St. Cu. St. Cu. Nb. : St. Cu. St. Cu.	A. Cu. : St. Cu. St. Cu. St. : St. Cu. Nb. : St. Cu. St. Cu.		10 10	10	10 10 10 8 10	5 10 1 9	2 0 0 0	P * ⁰ d ⁰ ⊔	d ⁰ ≡ ⁰ ⊔	 P ● 0	 • 0 	 b ● 	 d ⁰ ≡ ⁰ p • 0	o, p 0 \times , od \equiv 0 to o a : o, d 0 to c p : b and od and o a : o, o \bullet 0 to be p : b and be n be \sqcup to o a : o p : o to od \equiv 0 n : od and o a : o to c, op \bullet p : op \bullet \bullet and o od, o \bullet and o a : o p and p : of p and p :
26 27 28	Nb. St. Cu. Nb. : St. Cu.	Nb. : St. Cu. St. Cu. Nb. : St. Cu. : St.	St. Cu. St. Cu. Nb. : St. Cu.	10 10	10 10	10	10 10	10 1	0 0	$\mathbf{q_0}$	d⁰ d	 p	 	 p	d ⁰ 	od and o $a : o$ to od ⁰ \equiv ⁰ $p : od^0 n :$ o, op ⁰ \bullet $a : o p : o$, od ⁰ , o $n :$ op \bullet and od $a : op \bullet and o, c p : opd and o$
29 30	St. Cu. St. Cu.	St. : St. Cu. St.	A.St. : St.Cu. : Nb. St. Cu. : Nb.	10	10	1	()		0			 =0	$d_0 \equiv_0$	p_0	P^0	od ⁰ \equiv ⁰ carly; o and od ⁰ a : o to op ⁰ \bullet p : o to o \equiv ⁰ , \bullet ⁰ a : od ⁰ \equiv ⁰ and o p : od n :
31 Iean	St. Cu.	Nb.	Nb.	9	10	10	10	10 1	0	•••	<u></u>	<u>●°</u> ≡°	<u>d</u> <u>≡</u> ⁰	<u>d ≡</u>		$ \begin{array}{c} [\text{od } \equiv^0 \\ \text{o to o } \bullet \equiv^0 a : \text{od } \equiv^0 \text{ and o } \bullet \equiv^0 p : \text{od} \end{array} $
loud m'nt				7.5	7.8	8.4	8.5	7 · 8	0							
197.	Eskdalemuir.			yt-m-tt-												February, 1923
I	Ci. St. : St.	Nb.	Nb.	9	10	10	10	10 1	0			$d \equiv^0$		● ≡0	• =°	[≡⁰
2 3 4 5	St. Cu. St. Cu. St. Cu. St. Cu.	St. Cu. St. Cu. Cu. : F. Cu. St.	St. Cu. : St. Nb. : St. Cu. St. Cu. Nb.	1	9 10 0 10	9 3 10	5	10 I	8 0	 	:: 1	···		р 	● ≡°	o
6	St. Cu.	St.	Nb.	1	10				0	•••	•		• ≡⁰	● ≡0	• =°	o, o $lacktriangle$ and o $a: o, o lacktriangle$ $\equiv 0$ $p: o lacktriangle$ $\equiv 0$
7 8 9 10	St. Cu. Nb. St. Nb.	Nb. Nb. St. Cu. Nb.	St. Ci.: St. Cu. A. St. St.	10	01 01 01	10	6 10	6 2	0 0	 ● ≡ ⁰ = : • ≡ ⁰		$\begin{array}{c} \bullet \equiv^0 \\ d^0 \\ \equiv^0 \\ \bullet \equiv^0 \end{array}$	 • ≡⁰	 ==0	 =0 =0	$\begin{array}{c} \text{op} \bigwedge \text{ \star}, \text{o, o} \bullet \stackrel{\bigstar}{\Rightarrow} \stackrel{\bullet}{\Rightarrow} ^{0}a : \text{o} \bullet \stackrel{\bullet}{\Rightarrow} \stackrel{\bullet}{\Rightarrow} ^{0}, \text{p} \bigwedge \\ \text{o} \bullet, \text{o} \bullet \stackrel{\bullet}{\Rightarrow} ^{0}\text{to} \text{od}^{0}a : \text{o} \bullet \text{to} \text{bc} p : \text{b} \text{ and b} \\ \text{o} \bullet \stackrel{\bullet}{\Rightarrow} ^{0}\text{early}; \text{o} \stackrel{\bullet}{\Rightarrow} ^{0}\text{to} \text{c} \stackrel{\bullet}{\Rightarrow} ^{0}a : \text{o} \bullet \stackrel{\bullet}{\Rightarrow} ^{0}p \text{ and } n : \\ \text{o} \bullet \stackrel{\bullet}{\Rightarrow} ^{0}\text{ and o} \bullet \text{a} : \text{o} \bullet \stackrel{\bullet}{\Rightarrow} ^{0}p \text{ and } n : \\ \text{fto o} \end{array}$
11 12 13 14 15	Nb. St. Cu. St. Cu. Nb. St. Cu.	Nb. St. Cu. St. Cu. St. : St. Cu. St. Cu. : St.	Nb. St. St. Cu. St. St.	10	10 10 10 10		10 10 10	01 1 01 1 01	0 I 0 0	• ≡° * ≡° =°	● ≡ ⁰ d ≡ ⁰ ⇒ ≡ ⁰ ⇒ ≡ ⁰	d ≡ ⁰ ≡ ⁰ ≡ ⁰	● ≡° … ≡°	● ≡° ≡° ≡° ≡°	 =0 =0 =0	o, o
16 17 18 19 20	Nb. St. Cu. Nb. St. St.	Nb. : St. Cu. St. Nb. St. Cu. St. Cu.	St. St. St. St. St. Cu.	10 10	10 10 10 10 10	10	10	10 II 10 II	0 0 0 0 2	d ≡ ⁰ ≡ ⁰ * ≡ ⁰ ≡ ⁰	d ≡° ≡° * ≡° 	 ≡° * ≡° 	 ≠ ≡ ⁰ 	=0 =0 =0 	=° =° *° =° ⊔	$o \equiv^{0}, \text{ od } \equiv^{0}, \text{ o } \bullet a : \text{ o, bc, o} \equiv^{0} p : \text{ o} \equiv^{0} \text{ od}^{0} \equiv^{0}, \text{ o } \equiv^{0} a : \text{ o } \equiv^{0} p \text{ and } n :$ $[\Xi, o \bigstar \equiv^{0} a : \text{ o } \bigstar \equiv^{0}, \text{ o } \equiv^{0} p : \text{ o } \star \equiv^{0} \Xi \oplus^{0}, \text{ o } \equiv^{0} p : \text{ o } n :$ $[\Xi, o, \text{ bc } a : \text{ bc, op}^{0} \star p : \text{ b } \blacksquare n :$ $[\sigma \equiv^{0}]$
21	Nb.	Nb.	Nb.	10	10	10	10	1 01	0	* ≡ 0	* ≡ °		* ° ≡°	% ° ≡°	≡0	\boxtimes bc, o $\overset{\circ}{X^0} \equiv \overset{\circ}{O}$, o $\overset{\circ}{X^0} \equiv \overset{\circ}{O} a : o \overset{\circ}{X^0} \equiv \overset{\circ}{O}$ $[o \equiv \overset{\circ}{O}$
22 23 24 25	St. Cu. : St. A. Cu. : St. Cu. A.Cu. : A.St. : St.Cu. Nb.	St. Cu. : Nb. St. Cu. A. St. : St. Cu. Nb.	St. St. Cu. St. Cu. Nb.	9 5 7 10	7 5 10	10 10 10	9	5	0 9 0 0]]:•		• • • • • • • • • • • • • • • • • • •	 d⁰ ●	d ≡ ⁰	=° d° ≡°	\bigcirc \bigcirc \bigcirc \bigcirc \bigcirc \bigcirc \bigcirc \bigcirc \bigcirc \bigcirc
26 27 28	Nb. Nb. St. Cu. : St.	Nb. Nb. Nb.	St. Cu. Nb. : St. Cu. St. Cu. : St.	10	l .	01		10 1	0 0 9	● ≡ 0 • ≡ 0 	•		•	 ● 0 = 0	 	\boxtimes o \bigoplus and o \bigoplus a: o, c p : o n: o \bigoplus \equiv 0, o, o \bigoplus a: o and o \bigoplus 0 p: o \bigoplus 0 o a: o \bigoplus 0, o \equiv 0 p: o n:
lean loud m'nt				9.1	9.3	8.9	9.2	8.98	3.5	ı						
ay.	7 h	13h	18h	7h	9h	13h	15h	18h 2	I h	7h	9h	13h	15h	18h	21 h	Remarks.
		Cloud Forms.				ud A ll Fo						Weath	er.			

		Cloud Forms.					Amo orm					Weat	her.			
Day.	7h	13h	18h	7h	9h	13h	15h	18h	2 I h	7h	9h	13h	15h	18h	21h	Remarks.
1 2 3 4 5	St. St. Cu. Nb. St. Cu. St. : St. Cu.	Nb. Cu.: Cu. Nb. St. Cu. Cu.: St. Cu. St. Cu.	St. Cu. : St. Nb. A. St. : St. Cu. St. Cu. : A. St. St. Cu.	5 10 8	7	10 9 10 8 10	10 10 10 9	10 10 10	10 10 6 10 5	 •0=0 	 d≡⁰ .:. *≡⁰	d ⁰ 	b₀ 	 •° 	 d ≡°	o $a : od^0$, o, $o \oplus \equiv^0 p : o n : [o \oplus^2, od n : o \oplus, bctoo, \triangle at 11.40 a : o \triangle q \oplus, o \oplus^0 p : o \oplus \equiv^0, od \equiv^0, o a : o \oplus too p : o to c n : o, c a : ctoo p : o, o \equiv^0 n : [bc : n : o \equiv^0, o, o \bigstar \equiv^0 a : op^0 \oplus \& o p : op^0 \oplus,$
6 7 8 9	St. Nb. Nb. St. Cu. St. Cu.	Nb. St. Cu. St. Cu. Nb. St. Cu.	St. Cu.: Cu. Nb. St. Cu.; Cu. Nb. St. Cu. St. Cu. St. Cu.	10 10 10	I	10 10 10 10	10 10 10 9	9	10 10 10 5	=; d⁰ d⁰ 	≡ ⁰ e p ⁰ 	•≡° p•		 ≡0 	P ● 0 = 0 	b, $o \equiv 0$, $o \oplus 0$ a : $o \not = 0$ a : $o \not = 0$ b : $o \not = 0$ a : $o \not = 0$ b : $o \not = 0$ a : $o \not = 0$ b : $o \not = 0$ a : $o \not = 0$ b : $o \not = 0$ a : $o \not = 0$ b : $o \not $
11 12 13 14 15	St. Cu. Nb. St. Cu. : Nb. Ci. St. Cu.	St. Cu. St. Cu. : Nb. Cu. : F. Cu. St. Cu. St. Cu.	St. Cu. Nb. St. Cu. : F. Cu. St. Cu. : St. St.	10 10 10 1	10 3 2 10	10 10 5 9	10 10 5 8 9	10 4 10	10 10 3 10	p * ⁰=⁰ 	 *=° 	d°≡° y 	 •°≡° y 	 ●°=° 	 =0	Overcast all day $(a, p & n)$ [$o = 0$ to $o n$: $op^0 \times = 0$, $o \times to$ od $= 0$ $a : o = 0$ $= 0$ $p : o, o = 0$, bey $a : b = 0$, $b : to o = 0$ $=$
16 17 18 19	St. St. Cu. St. : St. Cu. St. St. Cu.	St.: F. St. St. Cu.: Cu.: Ci. St. F. Cu.: Ci.: Ci. St. Ci.: Cu. St. Cu.: Cu.	St. : St. Cu. St.Cu. : Ci.St. : Ci.Cu. Ci. : Ci. St. : St. Cu. Ci.Cu. : A.Cu. : St.Cu. St. Cu.	7 8 10	10 8 10	8 9 4 8 7	6 6 7 8 2	9 9 6 7 1	0 1 3 10 3	 <u>=</u> 0	≡° 		у 			o, $o \equiv^0$ to c $a : c \& bc p : o to b n : b, c to o a : o, bcy p : bcy, o to b n :bc, o, bc a : c \& bc p : bc n :o \equiv^0, c a : c p : c, bc to o n :o, o \equiv^0 to c a : b p \& n :$
21 22 23 24 25	St. Cu. Cu. : F. Cu. St. Cu. St. A. Cu. : St. Cu.	Ci. Ci. St. Cu. : A. Cu.	F. Cu. : A. Cu. Ci. Ci. ——————————————————————————————	7 5 5 10 5	9 5 9 10 1	0 1 0	1 2 2 2 8	3 1 2 0 5	4 9 0 9 5	□ ≡° □≡°	=0 =0 =0 %	∞ y ≡°	 y ∞ 	8 8 : .		cu, $o \equiv^0$ to b $a : b$ & bc $p : bc$ $n :$ bc, $bc \equiv^0$, by $a : by p : bc$, co $n :$ bc, b , o , b $a : b \infty p : b$ $n :$ [20h. $n :$ b, bc, ou \equiv^0 , $b \equiv^0 a : b \infty p : b$ to $\equiv \coprod^2$ o \equiv , bc, o $a : o$, c, bc $p : bc$ & c $n :$
26 27 28 29 30	St. : St. Cu. St. Cu. Nb. St. St. Cu.	Cu. : F. Cu. St. Cu. St. Cu. Cu. St. Cu.	St. : St. Cu. St. Cu. : A. Cu. Nb. : St. Cu. St. Cu. : Cu. Cu. : St. Cu.	8 10 10 10	I 10 10 2 3	7 10 10 5	9 9 10 8 8	10 9 10 5 8	10 10 0	≡° •≡° ≡°	 •°=° =°	y y y	у у 	=0 ∞ p 	$\begin{bmatrix} \equiv_0 \\ q_0 \\ \vdots \\ b_0 \equiv_0 \end{bmatrix}$	bc, $o \equiv^0$, cy $a : cy$, $o \equiv^0 p : op^0 \equiv^0 n :$ o, $p \bigoplus^0$, o $a : o p : o$, op $\bigoplus^0 n :$ o \bigoplus^0 to o $a : o & o \bigoplus^0 p : oi \bigoplus^0$, od $^0 : n :$ o \equiv^0 , bc o $a : o & o \bigoplus^0 p : oi \bigoplus^0$, od $^0 : n :$ bc \equiv^0 , oc, b to o $a : c p : c$, bc, o $\equiv^0 n :$
31 Mean Cloud	St. Cu.	St. Cu.	St. Cu.	1-		10		10	7.2		<u></u>		<u> </u>			$o \equiv 0$, c to o $a : 0$, op $\bigcirc 0$, $d^0 p : o n :$
Am'nt				1 3		1'	' '	'	′ -				1			
100	. Eskdalemuir.															April, 1923.
199.	. Eskuajemuir.			1	ī	ī	1	Ī			i -	<u> </u>	1	1	1	1
1 2 3 4 5	St. Cu. St. St. St. St. St. St. Cu. St. A. St.	Nb. St. St. Cu. St. St. Cu. : A. St.	St. Cu. St. St. Cu. Nb. St. : A. St.	10 10	10 9 10	10	10	10 8	10 9 10 10		=0 =0 	● ≡ ⁰ y	●0≡0 =0 ∞ p0y 	□ ≡ 0 ≡ 0 • ≡ 0 	=0 =0 =0 =0 	$ \begin{array}{c} o, o \equiv^{0}, o \bigoplus \equiv^{0} a : o \bigoplus \equiv^{0}, o p : o, o \equiv^{0} n : \\ o \equiv^{0}, o \bigoplus^{0} \equiv^{0}, o a : o \equiv^{0} p \Leftrightarrow n : \\ o, o \equiv, o \equiv^{0} o a : o, o \equiv^{0} p : c & o \equiv^{0} n : \end{array} $
1 2 3 4	St. Cu. St. St. St. St. Cu.	St. St. Cu. St.	St. St. Cu. Nb.	10 10 10	10 9 10 10	10	9	10 8 10	9 10 10	≡° ≡ d°	● ≡ ⁰ = 0 	 y	=0 ∞ p⁰y	=0 =0 =0	=0 =0 ●=0	$ \begin{array}{c} o, o \equiv^{0}, o \bullet \equiv^{0} a : o \bullet \equiv^{0}, o p : o, o \equiv^{0} n : \\ o \equiv^{0}, o \bullet^{0} \equiv^{0}, o a : o \equiv^{0} p & n : \\ o, o \equiv^{0}, o \equiv^{0} o a : o, o \equiv^{0} p : c & o \equiv^{0} n : \\ o \equiv^{0}, op, oy a : op, y, o \bullet \equiv^{0} p : o \bullet \equiv^{0} n : \end{array} $
1 2 3 4 5 5 6 7 8 9	St. Cu. St. St. St. Cu. St. : A. St. St. Cu. Nb. St. Cu. St. Cu. St. Cu. St. Cu.	St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.	St. St. Cu. Nb. St. : A. St. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.	10 10 10 10 10 10 10	10 9 10 10 10 10 8 10 10	10 10 10 10 6 9 8	10 9 10 10 10 10 2 8 8 8	10 8 10 9 10 9 1 7 10	9 10 10 2 10 10 10 7 7	*° ≡° b* b*	● ■ ⁰ □ ··· ··· ··· * ⁰ = ⁰	 y 	=0 ∞ p ⁰ y 	=0 =0 •=0 ···· ··· ··· ∞	=0 =0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	o, $o \equiv 0$, $o \bigoplus a : o \bigoplus a : o \bigoplus b$, $o p : o$, $o \equiv 0 n : o \equiv 0$, $o \bigoplus o \bigoplus a : o \bigoplus o \bigoplus b : o$, $o \equiv 0$, $o \bigoplus o \bigoplus o a : o$, $o \equiv 0$, $o \bigoplus o \bigoplus o a : o$, $o \equiv 0$, $o \bigoplus o \bigoplus o \bigoplus o \bigoplus o \bigoplus o \bigoplus o \bigoplus o \bigcap o \bigoplus o \bigoplus $
1 2 3 4 5 6 7 8 9 10 II 12 13 14 15	St. Cu. St. St. St. Cu. St. : A. St. St. Cu. Nb. St. Cu. St. Cu. Nb. St. Cu. Nb.	St. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.	St. St. Cu. Nb. St. : A. St. St. Cu. St. Cu. : A. Cu. F. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. St. Cu. : A. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. St. Cu. St. St. Cu. St. St. Cu. : A. Cu. : A. St. St. Cu. : A. St. St. Cu. : A. St.	10 10 10 10 10 10 10 10 10	10 9 10 10 10 8 10 10 10	10 10 10 10 10 6 9 8 10	10 9 10 10 10 2 8 8 8	10 8 10 9 10 9 1 7 10 6	9 10 10 2 10 10 10 7 7 5 10 10 8 4	=0 =1 d0 p★ ★0=0 d=0 	★ ₀ ≡ ₀	у 	=0 ∞ p ⁰ y	© 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	=0 =0 p * 0 p0 =0 d0 =0 d0 =0 d0 =0	o, $o \equiv 0$, $o \bigoplus 0$ a: $o \bigoplus 0$, $o \not p$: o, $o \equiv 0$ n: $o \equiv 0$, $o \bigoplus 0$ o a: $o \equiv 0$ p & n: o , $o \equiv 0$, $o \equiv 0$ o a: o , $o \equiv 0$ p: o c & $o \equiv 0$ n: o , $o \equiv 0$, o , o , o , $o \equiv 0$ o a: o , o , $o \equiv 0$ p: o c & $o \equiv 0$ n: $o \equiv 0$, o , o , o , o , o , o , o , o
1 2 3 4 5 6 7 8 9 10 11 12 13 14	St. Cu. St. St. St. Cu. St. : A. St. St. Cu. Nb. St. Cu. Nb. St. Cu. Nb. St. Cu. Nb. St. Cu. Nb.	St. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.	St. St. Cu. Nb. St. : A. St. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Nb. Nb.: St. Cu. Nb.: St.	10 10 10 10 10 10 10 10	10 9 10 10 10 8 10 10 10	10 10 10 10 10 6 9 8 10	10 9 10 10 10 2 8 8 8	10 8 10 9 10 9 1 7 10 6	9 10 10 2 10 10 10 7 7 5	=0 =0 d0 p★ d=0 	d ₀ = 0	 y d ⁰ ≡ ⁰	□ □ 0	© 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	=0 =0 p**0 p0 =0 d0 =0 d0 =0	o, $o \equiv 0$, $o \bigoplus 0$ a: $o \bigoplus 0$, $o \not p$: o , $o \equiv 0$ n: $o \equiv 0$, $o \bigoplus 0$ o a: $o \equiv 0$ p & n: o , $o \equiv 0$, $o \equiv 0$ o a: o , $o \equiv 0$ p: o & $o \equiv 0$ n: o , $o \equiv 0$, o , o , $o \equiv 0$ o a: o , $o \equiv 0$ p: o & $o \equiv 0$ n: $o \equiv 0$, o , o , o , o , o , o , o , o
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	St. Cu. St. St. St. St. Cu. St.: A. St. St. Cu. Nb. St. Cu. St. Cu. Nb. St. Cu. Nb. St. Cu. Nb. St. Cu. Nb. St. Cu. St. Cu.	St. St. Cu.	St. St. Cu. Nb. St. : A. St. Cu. : A. Cu. : A. Cu. F. Cu. St. Cu. St. Cu. : St. Cu. St. Cu. : Ci. Nb. : St. Cu. : A. Cu. : A. Cu. : A. Cu. : A. Cu. : A. Cu. : A. Cu. : A. Cu. : Ci. St. Cu. : Ci. : Ci. St. Cu. : Ci. St. Cu. : Ci. St. Cu. : St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.	10 10 10 10 10 10 10 10 10 10 10 10 10 1	10 9 10 10 10 10 8 10 10 10 10 4 10 6 1	10 10 10 10 10 10 6 9 8 10 10 10 10 8 9 3 10 10 8	10 9 10 10 10 2 8 8 8 10 10 7 9	10 8 10 9 10 9 1 7 10 6 10 8 8 6 6 10 10 2	9 10 10 2 10 10 10 7 7 5 10 10 8 4 10 3	=0 =1 d0 p★ ★0 =1 d=0 d0=0 d0=0 	 	 y d⁰≡⁰	□ □ 0	=0 =0 •=0 ···· ··· ··· ∞ •0 •1 •1 •1 •1 •1 •1 •1 •1 •1 •1 •1 •1 •1	=0 =0 -=0 	o, $o \equiv 0$, $o \bigoplus 0$ a: $o \bigoplus 0$, $o \not p$: o , $o \equiv 0$ n: $o \equiv 0$, $o \bigoplus 0$ o a: $o \equiv 0$ p & n: o , $o \equiv 0$, $o \equiv 0$ o a: o , $o \equiv 0$ p: o a: o , $o \equiv 0$ p: o a: o , $o \equiv 0$ p: o a: o , $o \equiv 0$ p: o a: o , $o \equiv 0$ p: o a: o , o , o , o , o , o , o , o ,
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	St. Cu. St. St. St. St. Cu. St. Cu. Nb. St. Cu. St. Cu. Nb. St. Cu. Nb. St. Cu. Nb. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.	St. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. Cu. St. Cu. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. Cu. Cu. Cu.	St. St. Cu. Nb. St.: A. St. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. St. Cu. St. St. Cu. St. Cu. St. Cu. Nb.: St. Cu. St. Cu.: Ci. St. Cu.: Ci. St. Cu.	10 10 10 10 10 10 10 10 10 10 10 10 10 1	10 9 10 10 10 10 10 10 10 10 10 10 4 10 6 1 8 9 10 10 8 10 10 10 10 10 10 10 10 10 10 10 10 10	10 10 10 10 10 6 9 8 10 10 10 8 9 3 10 10 8 8 10 10 10 8 10 10 10 10 10 10 10 10 10 10 10 10 10	10 9 10 10 10 2 8 8 8 10 10 7 9 8 6 10 10 8 7 9	10 8 10 9 10 9 1 7 10 6 10 8 10 8 10 10 7 7 10 7	9 10 10 2 10 10 10 7 7 5 10 10 18 4 4 10 3 6 10 9 1	=° = d°	P ★ 0 = 0	 y d⁰≡⁰ y y y	=0 ∞ poy	=0 =0 -=0 	=0 =0 p * 0 p0 =0 d0 =0 d0 =0 	o, $o \equiv 0$, $o \bigoplus 0$ a: $o \bigoplus 0$, $o p$: o , $o \equiv 0$ n: $o \equiv 0$, $o \bigoplus 0$ o a: $o \equiv 0$ p & n: o , $o \equiv 0$, $o \equiv 0$ o a: o , $o \equiv 0$ p: o c & $o \equiv 0$ n: o , $o \equiv 0$, o , o , o , o , o , o , o , o
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	St. Cu. St. St. St. St. Cu. St. : A. St. St. Cu. Nb. St. Cu. St. Cu. Nb. Nb. St. Cu. Nb. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.	St. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. Nb. St. Cu. St. Cu. St. Cu. Cu. St. Cu.	St. St. Cu. Nb. St. : A. St. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. St. Cu. St. St. Cu.	10 10 10 10 10 10 10 10 10 10 10 10 10 1	10 9 10 10 10 10 10 10 10 10 10 10 10 10 10 1	10 10 10 10 10 10 10 10 10 10 10 10 10 8 8 10 10 10 8 8 10 10	10 9 10 10 10 2 8 8 8 10 10 7 9 8 6 10 10 18 8 9 6 9 10 10 8 8	10 8 10 9 10 9 1 7 10 6 10 8 10 8 10 7 7 6 10 7 7 6 10 10 10 10 10 10 10 10 10 10 10 10 10	9 10 10 2 10 10 7 7 7 5 10 10 8 4 10 3 6 10 9 1 10 6 5 3 4 10	=°	● ≡ 0	 y d ² ≡ ⁰ d ⁰ ≡ ⁰ y y p△ y d y d y	=0 ∞ poy	=0 =0 =0 	= 0 = 0 	o, $o \equiv 0$, $o \bigoplus 0$ a: $o \bigoplus 0$, $o p$: $o, o \equiv 0$ n: $o \equiv 0$, $o \bigoplus 0$ o a: $o \equiv 0$ p & n: $o, o \equiv 0$, $o \equiv 0$ o a: $o, o \equiv 0$ p: $o = 0$ n: $o, o \equiv 0$, $o, o \equiv 0$ o a: $o, o \equiv 0$ p: $o \equiv 0$ n: $o \equiv 0$, $o, o, o, o \equiv 0$ o a: $o, o, o \equiv 0$ p: $o \equiv 0$ n: $o \equiv 0$, $o, o, o, o = 0$ p: $o \equiv 0$ n: $o \equiv 0$, $o, o, o = 0$ p: $o, o, o = 0$ p: $o, o, o = 0$ p: $o, o, o = 0$ p: $o, o, o, o, o, o, o, o, o, o, o, o, o, o$
1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Mean Cloud	St. Cu. St. St. St. St. Cu. St. : A. St. St. Cu. Nb. St. Cu. St. Cu. Nb. Nb. St. Cu. Nb. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.	St. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. Nb. St. Cu. St. Cu. St. Cu. St. Cu. Cu. St. Cu.	St. St. Cu. Nb. St. : A. St. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. St. Cu. St. St. Cu.	10 10 10 10 10 10 10 10 10 10 10 10 10 1	10 9 10 10 10 10 10 10 10 10 10 10 10 10 10	10 10 10 10 10 10 10 10 10 10 10 10 10 1	10 9 10 10 10 2 8 8 10 10 10 10 10 10 10 10 10 10	10 8 10 9 10 9 1 7 10 6 10 8 10 8 10 7 7 6 10 10 10 10 10 10 10 10 10 10 10 10 10	9 10 10 2 10 10 10 10 10 8 4 10 3 6 10 9 1 10 6 5 3 4 10 10 10 10 10 10 10 10 10 10 10 10 10	=° = d°	● ≡ 0	 y d ² ≡ ⁰ d ⁰ ≡ ⁰ y y p△ y d y d y	=0 ∞ poy	=0 =0 =0 	= 0 = 0 	o, $o \equiv 0$, $o \bigoplus 0$ a: $o \bigoplus 0$, $o p$: $o, o \equiv 0$ n: $o \equiv 0$, $o \bigoplus 0$ o a: $o \equiv 0$ p & n: $o, o \equiv 0$, $o \equiv 0$ o a: $o, o \equiv 0$ p: $o = 0$ n: $o, o \equiv 0$, $o, o \equiv 0$ o a: $o, o \equiv 0$ p: $o \equiv 0$ n: $o \equiv 0$, $o, o, o, o \equiv 0$ o a: $o, o, o \equiv 0$ p: $o \equiv 0$ n: $o \equiv 0$, $o, o, o, o = 0$ p: $o \equiv 0$ n: $o \equiv 0$, $o, o, o = 0$ p: $o, o, o = 0$ p: $o, o, o = 0$ p: $o, o, o = 0$ p: $o, o, o, o, o, o, o, o, o, o, o, o, o, o$

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200.	ESKOS	lemuir.

		Cloud Forms.					Am						Wea	ther.		7	Remarks.
Day.	7h	13h	18h	7h	9h	13	h 15	h	8h	2 I h	7 h	9h	13h	15h	18h	21 h	Remarks.
1 2 3 4 5	F. Cu. : Ci. St. Cu. St. Cu. : Ci. St. Cu. : Ci. St. St. Cu.	St. Cu. St. Cu. St. Cu. : A. Cu. St. Cu. Cu. : A. St.	St. Cu. : Ci. Cu. St. Cu. St. Cu. : Ci. St. St. Cu. A. St. : Ci.		7 8 8 10	8 7	9		5 1	2 10 2 9	 2 	: : =		•			od ⁰ a : od, od \equiv ⁰ p : o \equiv ⁰ , oid n : oco a : o, bc p : bc, o n : c, o \equiv ⁰ , c a : o, bc p : bc, b n : co, o \equiv , o a : oc, o p : o n : o, co a : oc p : co n :
6 7 8 9 10	St. Cu. Cu. : A. St. St. Cu. St. Cu. Ci. St.	St. Cu. Cu. : F. Cu. Cu. : F. Cu. St. Cu. : Ci. St. Nb.	Nb. : A. St. St. Cu. Cu. : F. Cu. Nb. Nb.	2 10	10 5 10 10	10 6 4 9	6 7 7	1	3 6 0 1	7 9 1 10		 p ==0 	 у р	 у •	• y •	 P ⁰ ₽	o, co a : co, op
11 12 13	St. Cu. : Ci. St. St. Cu. : A. Cu. St. : St. Cu.	Nb. Nb. : Cu. Cu. : St. Cu.	St. Cu. : Ci. St. Cu. Ci. St. : St. Cu. Cu. : Cu. Nb.	8 5 to	9 5 10	10 8 8	9	- (6	9 3 6		d ⁰ 	*⁰ p *	*		 dº	op \bigoplus , c, oi \bigoplus ⁰ , \bigstar ⁰ a : oi \bigstar , o p : o n : bc, co \bigstar a : op \bigstar , bc p : bc, b n : o \bigoplus ⁰ ,op ⁰ &c a : c & op to bc p : op \bigoplus ,od,c n :
14 15	St. Cu. : A. St. St.	Nb. St. Cu.	Nb. Cu. : Ci. St.	1	10	10 9	1 -			10 6	 ≡°	$\mathbf{d}_{0} \equiv_{0}$	р Д. ●		•	d 	o, o $igoplus^0 A^0 a$: c, op $igoplus A$, c p : oi $igoplus^0 n$: o $igoplus q \blue A$, $igoplus^2$, c & o a : c & o p : c, be n :
16 17 18 19 20	Cu.: St. Cu. Cu.: St. Cu. St. Cu. Nb. Nb.	St. Cu. : Cu. Nb. St. Cu. Nb. : St. Cu. Nb. : Nb. Nb.	St. Cu. : A. St. St. Cu. Nb. : St. Cu. Nb. St. Cu.	10 10	8 10 9 10	8 10 10	10 10	10	6 0 1	10 2 10 10 5	 d ≡0 d ≡0	 • ≡ ⁰	 • = 0 = 0	p ★ • • = •	 •° d	р ж 	o $lacktriangle^0$ carly, o, c, op \bigstar $a:c$, op \bigstar p and $n:$ bc, c & o $a:c$, be $p:$ bc to b $n:$ \blue{M} be, o, o $lacktriangle^0$ $a:$ oi $lacktriangle^0$ p and $n:$ oid $\blue{\oplus}^0$ to o $lacktriangle^0$ $a:$ o $lacktriangle^0$, od & o p and $n:$ oid $\blue{\oplus}^0$, o $lacktriangle^0$ $a:$ o $lue{\oplus}^0$, o $\blue{\oplus}^0$ $p:$ o, bc $n:$
21 22 23 24 25	St. Cu. Cu. : F.Cu. : Ci.Cu. Cu. : F. Cu. Cu. St. Cu.	St. Cu. St. Cu. Cu. Nb. : Cu. St. Cu. Cu. : Cu.Nb.	Cu.: A. Cu. Nb.: St. Cu. St.Cu.: Cu.Nb.: A.St. St. Cu.: Nb. St.Cu.: Ci.St.: Cu.Nb.	7 2 2	8 6 8 7	8 10 8 10 8	10 9 10	10	O I	10 5 10 4		• • • • • • • • • • • • • • • • • • • •		 •° jp	d° d° 	 • ≡°	o \bigoplus^0 early, op 0 , o & c a : c, be p : c to o n : o, bc, o a : o, o \bigoplus^0 p : o n : o, b, op \bigoplus^2 ; c a : cp \bigoplus^0 to bc p : o, be n : b, bc, op 0 a : o, op 0 p : od, o \bigoplus \equiv^0 n : bearly, o \bigoplus , c, op \bigoplus q a : c, op \bigoplus \bigoplus \bigoplus p : c, for n :
26 27 28 29 30	St. Cu. St. Cu. Nb. : St. Cu. F. Cu. Nb.	St. Cu. St. Cu. St. Cu. F. Cu. St. Cu.	St. Cu. : Ci. St. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.	9 5	9 10 9 1	9 10 10 2 10	9 9	I	0 1 8 6 1	10 10 8 10	 P ⁰ d ⁰	 b ₀				d 	bc, c, op a : op, bc, od 0 p : op \bullet^{0} , od n : o, co a : o p and n : o, cpd 0 , o a : o, c p : c n : c, bc, b a : b, bc p : bc, o n : o, od 0 , o a : o p : od 0 , o n :
31 Mean Cloud Am'nt		St. Cu.	St. Cu.	8·1		8.7	1-	- -	0 1			do					o, od 0 , o a : o p and n :
201.	. Eskdalemuir.																June, 1923.
1 2 3 4 5	St. St. Cu.: Ci. St. St. Cu. Ci.Cu.: A.Cu.: F.Cu.	St. Cu. Cu. : Ci. St. Cu. : A. St. St. Cu. Nb. : St. Cu.	St. Cu. Cu. : Ci. St. Cu. St. Cu. Nb. : Cu.Nb. : St.Cu.	10	6 10	9 5 10 10	10	10	-	8 10 10	•••	•••	 у р ⁰	 у р ^о	Ъ ₀	 P ⁰	o, co $a : oc p : o n :$ o, bc, bcy $a : bcy$, b $p : b$, c $n :$ c, o $a : o p$ and $n :$ op ⁰ early, o $a : o p : o$, op ⁰ $n :$ bc, c, op ⁰ $a : op$, o \bullet \circ \circ \circ \circ \circ \circ \circ \circ \circ \circ
6 7 8 9	Nb. : St. Cu. Nb. : St. Cu. Nb. : St. Nb. St. Cu.	St. Cu. : A. St. Cu. Nb. : St. Cu. Nb. Nb. St. Cu.	St. Cu. St. Cu. Nb. Nb. St. Cu. : Cu.	10 10 10	10 10 10 10	10 10 10 10	9 10 10	10	0 I	9	d ⁰ d ⁰ ≡ ⁰ d ⁰ ≡ ⁰ d ≡ ⁰	$\begin{array}{c} \cdots \\ p^0 \\ d \equiv^0 \end{array}$	 d ≡ ⁰	$\mathbf{d} \stackrel{\mathbf{=}_{0}}{\equiv_{0}}$	 d ≡⁰ 	j p d ≡ 	co, opd ⁰ , o $a: o$, op ⁰ , o $p: o n:$ o, od ⁰ \equiv ⁰ , o $a: o p$ and $n:$ o, od ⁰ \equiv ⁰ , o $\bigoplus a: o \bigoplus o$, o $\bigoplus o$ $p: o \bigoplus o$, o $n:$ o, co, d \equiv ⁰ , op $a: od \equiv$ ⁰ $p: od \equiv$ 0, od \equiv 0, od \equiv 0, od \equiv 0, od \equiv 0, od \equiv 0, od \equiv 0, od \equiv 0, of $\bigoplus od$ 0, co, co, fod ⁰ od 0.
11 12 13 14 15	Cu. : F. Cu. : Ci. Nb. F. St. : St. Cu. Cu. St.	Cu. Nb. St. Cu. Cu. Nb.	St. Cu. St. St. Cu. St. Cu. : Ci. St. St.	9	2 10 10 6 10	6 10 6 10	10 10 6	10	0 8	2 10 7 9	р ::-	 • ≡⁰ 	$d^0 \equiv^0$	у у d		 	op, be, by a : bey, cy, be p : b n : o, o $lacktrian$, oi $lacktrian$ a : o $lacktrian$ o , o p : o n : o $lacktrian$, o a : o p : o, co n : be a : bey, c p : co $lacktrian$ a : od 0 , o p : od 0 , o p : od 0 , o p : od 0 , o p : od 0 , o p : od 0 , o p : od 0 , o p : od 0 , o p : od 0 , o p : od 0 , o p : od 0 , o p : od 0 , o p : od 0 , od 0
16 17 18 19 20	St. Cu. Cu. : F. Cu. St. Cu. St. Cu.	St. Cu. Cu. : Ci. St. St. Cu. St. Cu. St. Cu. St. Cu.	St. Cu. Cu.: A. St. St. Cu.: Ci. St. Cu.: A. Cu. St. Cu.: Ci.	1	10 6 10 8 8	10 6 9 8	10 7	10	7 8	10 4 7	:: d	 =0 				•	c, o a : o p and n : b, bc, o a : o $\oplus p$: o, o $\oplus n$: o, o \equiv^0 , c a : c p : c, bc n : bc, co a : o, c p : c n : bc, c a : co p : o n :
21 22 23 24 25	St. Cu. St. Cu. St. Cu. Nb. : St. Cu. Cu. : Ci. St.	St. Cu. : A. St. St. Cu. Cu. : Ci. St. St. Cu. Cu. : Ci. St.	St. Cu.: A. St. St. St. Cu. St. Cu. St. Cu. St. Cu.	01 01 01	10 10 6 10	10 6 10	3 10	10	0 I	10 10 10 10	≡° j p 			j p		d ≡ ⁰ d ⁰ ≡ ⁰	o, op ⁰ , o $a : o p$ and $n :$ op ⁰ , o $a : o p : o$, od ⁰ \equiv $n :$ o, bc $a : bc$, o $p : o n :$ overcast all day, od ⁰ \equiv $21-24$ hrs. $a, p, n :$ o to o $a : o p : o$ to bc $n :$
26 27 28 29	Ci. St. : Ci. A. St. St. Cu. Ci. : Ci. St. Nb.	Cu.: Ci. St. St. Cu.: F. Cu. Cu. Ci. Cu. St. Cu.	St. Cu. St. Cu. Cu. Ci. St. Cu. St. Cu.	8 10 8 10	9 10 7 8 8	6 8 7 7 9	10 5 6	10	4	10 10 6 7 9	 d 			у	у 		bc to o, bc a: bcy, oy to o p and n: o & c a and p: o & op ⁰ \bullet n: o & c a: c to bc p: bc n: bc & c a, p, n: c to o, od, c a: o & c p and n:
30				. 1		1	i	- 1	- 1				1	ł.	l	1	1
Mean Cloud Am'nt				8.6	8 · 7	8.6	8.	68	.6	8.8							
Mean Cloud		13h	18h	8·6		<u> </u>	<u> </u>	+	$\frac{1}{1}$			9h	13h	15h	18h	21h	Remarks.

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		Cloud Forms.				ad A						Wea	ther.			
Day.	7h	13h	18h	7h	9ь	13h	15h	18h	21 h	7 ^h	9h	13h	15h	18h	21 h	Remarks.
1 2 3 4 5	St. Cu. St. Nb. St. Cu. : A. Cu. Nb.	St. Cu. St. Cu. Nb. Nb. St.	St. Cu. : Ci. Cu. Nb. St. Cu. St. St.	10 10	10 10 10	10		10	10 10 10 10	 d ≡º d ≡º	d ≡°	 d ≡° d ≡° ≡°	 • 0 • 0 • 0 • 0 • 0 • 0 • 0 • 0	 ●° ≡° ≡ :	d° ≡° ≡ : ≡ :	Mainly overcast, $p^0 \oplus 20h$. a , p , n : $o \equiv 0$, $o \equiv 1$ to $o = 0$; $o \oplus 0$ $o \oplus 0$;
6 7 8 9 10	A. Cu. : A. St. Cu. : A. St. : A. Cu. St. St. Cu. Nb.	Ci. St.: Cu. St. Cu.: St. St. St. Cu.: A. Cu. St. Cu.: Ci. St.	A. St. : A. Cu. St. Cu. St. Cu. : Cu. St. Cu. : Ci. : Ci. Cu. A. St. : Nb.	10	5 7 10 10	4 10 10 6 4	4 9 8 5 8	6 10 3 5 10	10 9 10 10	8 8 III : Î	● : : 8 8 • : : : • • • • • • • • • • • • • • • •	∞ y =° 	∞ y ≡° 	∞ ∞ p ⁰ 	:: ® 8 8 8	c ∞ , bc, o ∞ a and p : bc ∞ to o n : c $\&$ o ∞ , \mathbb{K} and \mathbf{T} a: \mathbb{K} , o $\equiv^{0} p$: o $\equiv^{0} n$: o \equiv ; to o $\equiv^{0} a$: o ∞ to bc p : bc, o ∞ n : o to bc a : bc ∞ p : bc to o ∞ n : o $\bigoplus^{0} \equiv^{0}$ at first, bc a : bc, op ⁰ \bigoplus ∞ p : o $\&$ [op ⁰ \bigoplus n :
11 12 13 14	St. Cu. St. St. Cu. St. St.	Cu. Cu. F. Cu. St. Cu. St.	St. Cu. : Cu. Nb. Cu. : Ci. St. A. Cu. : St. Cu. St. Cu. Nb.	10 7 10	10 2 4 8 10	6 3 2 8 10	6 2 2 10 10	5 2 5 10 10	5 1 5 10 10	:: :: :: :: :: :: :: :: :: :: :: :: ::	 =:	∞ y ≡:	∞ y ≡:	∞ •°	∞ ∞ ≡° d° ≡°	op ⁰ $igoplus$ early, bc ∞ $a:$ bc ∞ p and $n:$ o $\equiv \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $
16 17 18 19 20	St. Cu. St. Cu. St. Cu. Nb. Nb. : St. Cu.	St. Cu. St. Cu. St. Cu. Nb. St. Cu. : F. Cu.	St. Cu. Nb. : St. Cu. St. Cu. St. Cu. Nb. : St. Cu.	10 8	10 9 9 10 2	9 10 10	9 9 9 10 6	10 7 10 10	10 8 10 10	 •0 ≡0 j p	 p ● j p ● ≡ ⁰	 d ≡º y	 d ≡º	 p ● po	 d ⁰ ≡ ⁰ j p	o $lack o$ early, c $a: o p: o, op^0 lack o, on:$ o & op^0 $lack o, a, p$ and $n:$ o & c $a: o, op lack oc p: c n:$ od \equiv^0 , o $lack oldon^0 \equiv^0$ & o p and $n:$ o $lack oldon oldon occupants of a: occupants oldon occupants oc$
21 22 23 24 25	St. Cu. Nb. Nb. St. Cu. Nb. : St. Cu.	St. Cu. Nb. Cu. St. Cu. St. Cu.: Nb.	St. Cu. Nb. Nb. : St. Cu. Nb. St. Cu.		10 5	10 7	10 10 10 10	10	10 6 10 9	 d ⁰ ≡ ⁰ p ⁰	d ⁰ ≡ ⁰ 	 d° ≡° y jp	d° ≡°	 d° ≡° p p° 		bc to o $a: o & \operatorname{op^0} \bullet p: o n:$ od ⁰ $\equiv ^0 a: \operatorname{od} \equiv ^0 \& o \bullet \equiv ^0 p: \operatorname{od^0} \equiv ^0 \& o n:$ o \bullet at first, cy $a: o & \operatorname{op^0} \bullet p: \operatorname{op^0} \bullet \operatorname{to}$ bc, op ⁰ \bullet , bc & o $a: o & \operatorname{op^0} \bullet p \ and n: [bc n:$ op ⁰ \bullet , c $a: c$, op ⁰ \bullet to bc $p: bc$ to o $n:$
26 27 28 29 30	St. Cu. A. St. : A. Cu. Nb. St. : St. Cu. St. Cu.	St. Cu. St. Cu. St. St. Cu. : Nb. Nb. : St. Cu.	Cu.: F. Cu. St. Cu.: A. St. St. Nb.: St. Nb.: St. Nb.: St. Cu.	8 10		8 9 10 10 9	5 8 10 10	10	6 10 10 10	 dº ≡ ≡º 	p d ≡⁰ 	 pº jp	 • ≡° d°	 p ⁰ jp	 ● 0 = 0 = 0 ● = 0	o \bigoplus \cong 0 & o \cong 0 a , p and n : o \bigoplus \cong 0 to op 0 \bigoplus a : op 0 \bigoplus p and n : op \bigoplus & bc a : op \bigoplus p : o \bigoplus \cong 0 n : [c & o n :
Mean Cloud	St. Cu.	Nb.: St. Cu.	Nb.	9.3	10			10	9	=0	d	jp_	jp_	•		$0 \equiv {}^{0} to op {}^{0} \bullet a : op \bullet {}^{2} T to o \bullet p : o \bullet,$
Am'nt				9 3	4	0 2	° 3	3	0 9							A
203.	<u> </u>				_		_									August, 1923.
1 2 3 4 5	St. Cu. : A. Cu. St. : A. St. Nb. Cu. A. St. : Ci. St.	St. Cu. : Cu. St. St. Cu. : Ci. Cu. : Ci. A. Cu.	St. Cu. : Cu. Nb. St. Cu. A. Cu. : Ci. Nb. : St. Cu.			7 10 9 8 5	8 7	8 10 7 7 10	1 10 8 7 10	:: b	d 	 y 	 y 	d⁰	• _	o, bc, op \bullet $a:c$, bc to c $p:c$ to b $n:$ bc, o \bullet , o \bullet , o \bullet , o $a:c$, c to \bullet \bullet $p:o$ \bullet , o \bullet ² o \bullet $=$ ⁰ , op \bullet , oa:cp \bullet ⁰ p and $n:$ c, bcy $a:c$ to c p and $n:$ o to bc $a:c$ bc, op \bullet $p:c$ \bullet o \bullet
6 7 8 9 10	St.: St. Cu. Nb. A. Cu.: Ci. St. Nb. Nb.	Nb. Nb. Nb. St. Cu. St. Cu.	Nb. St.: St. Cu.: Ci. Nb. St. Cu.: Ci. St.Cu.: Ci. St.Cu.: A.Cu.: Ci.St.	10 7 10	10 7 10	10 10 10 9 10	10	10 9 10 9	10 9 10 9 6	 • ≡⁰ d d⁰	d ≡º 	d ≡0 d ≡0 	p ●0 d ≡0 d ≡0	d ⁰ ≡ ⁰ d ≡ ⁰ ⊕	d ≡° d ≡°	$0, 0 \bullet^{0} a : op^{0} \bullet, 0 \bullet^{0} \equiv^{0} p : 0 \bullet^{0} \equiv^{0} n : 0$ $0 \bullet \equiv^{0}, 0 \bullet^{0} \equiv^{0} a : op \bullet^{0} \equiv^{0}, 0 p : 0 n : 0$ $0, 0 \bullet^{0} \equiv^{0} a : op^{0} \bullet \equiv^{0} e p : 0 \bullet^{0}, op \bullet^{2}$ $0 \bullet \equiv^{0} e, c & 0 a : c & 0 p and n : [\equiv^{0} e n : 0]$ $0, 0 \bullet^{0} to c a : c to 0, \oplus p : 0 to bc n : 0$
11 12 13 14 15	St. Cu. : A. St. A. St. Nb. St. Cu. St. Cu.	Cu. A. St. St. St. Cu. St. Cu.	St. : A. St. F. Cu.	10	ю	9 10 10 10	7 10 9 9	7 8 1 10 7	3 9 1 9 7	: : ≝ d d	 ≡° 	 d ≡⁰ 	d 			o, bc to o a : o to c p : c \oplus to b n : o, od a : opd p : o n : o, od, p $\bigoplus \equiv^0$, o \equiv^0 a : op 0 \bigoplus to b p : b n : b to o \bigcap , o a : o, op 0 \bigcap , o p : o n : o, c \bigcap , c \bigotimes op \bigoplus a : c \bigotimes op \bigoplus p and p :
16 17 18 19 20	St. Cu.: A. St. St. Nb.: St. Cu. St. Cu. St. Cu. St.: F. St.: St. Cu.	St. Cu. : A. Cu. Nb. : A. Cu. St. Cu. St. Cu. St. Cu. St. Cu.	Nb.: St.Cu.: A.St. St. Cu. St. Cu. Nb.: St.: St. Cu. Nb.	10 10 9	ю	10	9 10 9	10 10	10	 dº 	 pd 	 p ● 	•°	p ⁰ j p ● ≡ ⁰	d • ≡⁰	o a and $p : \operatorname{op} \bigoplus_{n} \operatorname{o} \bigoplus_{n} \operatorname{p} \bigoplus_{n}^{2} n :$ o $\bigoplus_{n} \operatorname{op} \bigoplus_{n}^{2} a : \operatorname{op} \bigoplus_{n}^{2} p : \operatorname{opd} n :$ op $\bigoplus_{n} \operatorname{opd} a : \operatorname{op} \bigoplus_{n}^{0} p : \operatorname{op} \bigoplus_{n}^{0} \operatorname{to} \operatorname{on} :$ o $a : \operatorname{ot} \operatorname{op} \bigoplus_{n}^{0} p : \operatorname{op} \bigoplus_{n}^{0} n :$ o $a : \operatorname{ot} \operatorname{op} \bigoplus_{n}^{0} p : \operatorname{op} \bigoplus_{n}^{0} n :$
21 22 23 24 25	Nb. St.: F. St.: Nb. St. St.: Ci. F. St.: St. Cu.	St. Cu. Nb. : St. Cu. Nb. St. Cu. St. Cu.	Cu. : F. Cu. Cu. Nb. : St. Cu. Nb. St. Cu. Nb.	10 10 3	6	9	10		3 2 10 3 10	• •° ··· ···	₽°	j p ● 	 ● • ≡°	 jp d ≡º • ≡⁰	 ● ≡° ≡°	o $lacktriangle$ to op $lacktriangle$ a: op $lacktriangle$, bc, b to on: op $lacktriangle$, op $lacktriangle$ a: o, ojp p : o, b to on: o $lacktriangle$ conditions of $lacktriangle$ conditions of $lacktriangle$ to $lacktriangle$ conditions of $lacktriangle$ condit
26 27 28 29 30	Nb. St. Cu. Nb. Nb. St. Cu.: A. St	Cu. St. Cu. St. Cu. Nb. Nb.	Nb. : St. Cu. St. Cu.	10 10		8	10 8	10 10 4 10 7		d⁰ d d	 d ⁰ 	 • p	jp jp ●	p ● p ● • ≡°	 • ≡°	op \bigoplus , opd $a : \text{op} \bigoplus^2 p : \text{op} \bigoplus^2 \text{to op } n :$ op \bigoplus & c $a : \text{op} \bigoplus p : \text{op, o} n :$ opd, c $a : \text{c}$ & op, bc $p : \text{bc, b, c} n :$ c to opd $a : \text{o} \bigoplus$, o \bigoplus $\bigoplus^0 p : \text{o} \bigoplus \bigoplus^0 n :$ o, op \bigoplus $a : \text{op} \bigoplus^2$, bc, c $p : \text{c to b} \triangleleft n :$
Mean Cloud Am'nt	Nb.	Nb.	St. Cu.	9·3	9.2		0.0 10		10 7·4	_d		_ p	<u>p ●°</u>			od, o & op a : op, op $\bullet^2 \triangle$, o p : o, op n :
	7 h	13h	18h	7h	9h	13h	15h	18h	21h	7h	9h	13h	15h	18h	21h	Remarks.
Day.	·	Cloud Forms.	1			ud A ll Fo			-			Wea	ther.		•	Kemarks.

The content of the	September, 1923.
The content of the	
\$ \$\frac{\text{Sc Cu}}{3}\$ \$\frac{\text{Sc Cu}}{\text{Sc Cu}}\$ \$\frac{\text{Cu}}{\text{Sc Cu}}\$ \$\frac{\text{Sc Cu}}{\text{Sc Cu}}\$ \$\frac	Remarks.
Y St. Cat. Cu. St	
13	●, od ≡ ⁰ n : co p : b, b in: co a : o, od ⁰ p : od ⁰ , o n : co a : od ≡ ⁰ to o p : o, bc n : co oy a : oy, c p : c & o n :
13 St. Ca.	$ \begin{array}{l} 0, 0 & p : 0 & 0, 0 & 2 & n : \\ 0 & c & p : c to 0 & n : \\ 0 & a : od & 0 & 0 & 0 & 0 & 0 & 0 \\ 0, p & and & n : & 0 & 0 & 0 & 0 & 0 \end{array} $ $ \begin{array}{l} 0, 0 & p : 0 & 0 & 0 & 0 & 0 & 0 \\ 0, 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{array} $
21 St. Cu. St. Cu. St. Cu. Nb. St. Cu. St. Cu. Nb. St. Cu. St. Cu. Nb. Nb. Nb. Nb. Nb. Nb. Nb. Nb. Nb. Nb	$cop \bullet a : c, cp \bullet p : c, bc n : co \bullet a : o \bullet p \ and n : cp \land at 17h. p : bc to b n : a : o \bullet o, od = o, o \bullet = o p : co \bullet e o n : co bc to a p : o o o o o o o o o o o o o o o o o o$
25 Nb. St. Cu. St	c to b p : b to o n : op
St. St. St. Cu. St.	$a: o ldot, o ldot^2 p: o ldot to c n:$ $a: o, od^0, o ldot p: od, o ldot \equiv^0 n:$
205. Eskdalemuir.	$lacktriangleda: 0 lacktriangledown, 0 lacktriangledown = 0 p: 0 lacktriangledown to od n: st, o to c a: c & bc p: c, o n: c \lefter a: a: o \lefter & cd \lefter p and n: \lefter \lefter \lefter a: o \lefter \lefter & cd \lefter p and n: \lefter \le$
1	
1	October, 1923.
St. Ch. St.	to be $a : c \& be p \ and n :$ ely, b to o $a : c p \ and n :$ $0 a : o \bullet \equiv^0 \text{ to } o \equiv^0 p :$ $[op \bullet] \text{ to } b n :$
7 St.: St. Cu. 8 St.: Cu. Nb.: St. 9 St. Cu. 10 St.: St. Cu.	$0, 0 & c p : c to b n :$ $0 \equiv 0 a : od & $
11 St. F. St. St. Cu.	, c $a : \operatorname{cp} \bullet p : c \& o, o \bullet^{\circ} n :$ o $a : o, \operatorname{od} =^{\circ} \operatorname{to} c p : c, \operatorname{op} \bullet$ $\bullet p : o \bullet =^{\circ} n :$ [to be $n :$ rly, oy $a : \operatorname{oy}, \operatorname{op} \bullet p : \operatorname{bc},$ & $o : p : o, \operatorname{op} \bullet n :$ [op $\bullet n :$ [c & bc $n :$
St. Cu. St.	urst, bey a : be, op \bigoplus to c p : a : o \bigoplus , d to b p : b & be n : o b p : b & be n : : o & c p : be, b n : : o & c p : be, b n : : o, od p : o & o \bigoplus p : o
St. Cu. St.	c, b p : b to c n : & o p : o, o \equiv 0 n : [od \equiv 0 n : \equiv 0 to bc a : bc to od \equiv 0 p : at first, bc a : b & bc p : [c & bc n : \bigoplus at 2 ohrs.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$: $c & o p : o & op \bullet n :$ $c, op \bullet p : op \bullet, o n :$ • $a : o \bullet = p : op = o to c n :$ hr., bc $p \bullet to c a : o, op \bullet p :$ [c, op \end{array}
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$p: bc, cp \bullet q p: op \bullet, c n: [< 18h19h.]$
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ly; o, bc a bc, op ϕ : bc, [op ϕ n:
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$: o, bc to c p : c, o \bigcirc \nwarrow n : [T at o9.45. : c, op \bigcirc p : o \bigcirc \bigcirc \bigcirc n :
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	o to c p : c & bc n : [c & bc n :
1/2m nu 1	9h.) o <i>a</i> : 0, op ⁰ to be <i>p</i> :
7h 13h 18h 7h 9h 13h 15h 18h 21h 7h 9h 13h 15h 18h 21h	Para d
Cloud Forms. Cloud Forms. Cloud Amount (All Forms). Weather.	Remarks.

November, 1923.

206.	Eskdalemuir.															November, 1923.
		Cloud Forms.				ud / All I						Wea	ther.			
Day.	7h	13h	18h	7h	9h	13h	15h	18h	21h	7h	9h	13h	15h	18h	21h	Remarks.
1 2 3 4 5	St. St. Cu. Nb. St. Cu. St.: St. Cu.	St. Cu. St. Cu. : Cu. St. Cu. St. Cu. St. Cu. : Ci.	Nb.: St. Cu. St. Cu. Nb. Nb.: St. Cu. St. Cu.	10 3 10 10	10 6 9 10 8	10 8 9 8 8	9 9 9 9	9	5 10 10 6 10	≡° •≡° p	≡ jp 		 p• p* p•°	p p• p* 	 • 	
6 7 8 9	St. Cu. Nb. St. Cu. A. Cu. : Cu. : F. Cu.	Cu.: F. Cu.: St. Cu. Ci. St. St. Cu. Nb. A. Cu.: Ci. St.	 St. Cu. St. Cu. A. Cu.	3 0 10 9	2 0 10 8 2	5 1 8 10 9	5 1 7 8 5	0 0 7 1 7	0 8 1 1	בנ ∰ננ	[: • : :]]]:::::::::::::::::::::::::::::::::::::	: : : [[bc_to b, bc a : bc to bc_p and n : b_to by a : b, bc to b_p: b_, c_n: $0 \bullet^0 \equiv^0 \bigstar$ to $c : a : op \bullet \& c : c : to b : n$: o_, bc to $o \bigstar \& \bullet : a : o : to b : b$, op $\bigstar : n$: b_to $o : a : o$, bc $p : c : to b : m$:
11 12 13 14 15	St. Nb. Nb. Nb. St. Cu.	St. St. Cu. : Ci. St. Nb. Nb. : St. Cu. Nb.	Nb. St. Cu.: Ci. St. Nb. St. Cu.: Ci. St. St. Cu.: Ci. St.	10 10 10 2 10	10 10 10 7 10	10 10	10 10 10 5	10 10 10 4 3	10 10 3 10	=° •=° ···	=° •=° •=° p* *=°	≡° •≡° ≡ :	≡° •≡° 	d≡ •≡° 	d≡ •≡° ∴. *°	o \equiv ⁰ a : o \equiv ⁰ d to od \equiv p and n : o \bigoplus & d \equiv ⁰ to o a : o p and n : o \bigoplus \equiv ⁰ a : o \bigoplus ⁰ \equiv ⁰ to o \bigoplus ² \equiv ⁰ p and n : o to b at first, cp \divideontimes a : bc p and n : \cong op \ggg , o, o \ggg \cong a : o, bc, b p : b to o \ggg n : [o \ggg \bigwedge \cong n : \leftarrow at 21h.
16 17 18 19 20	St. Cu. Nb. Nb. St. Cu. St. Cu. : A. St.	St. Cu.: A. Cu. St. Cu.: A. Cu. St. Cu.: A. Cu. Cu.: A. Cu. St. Cu.	St. Cu. Nb. St. Cu. St. Cu.: A. Cu. Cu.: F. Ci.: A. St.	10 10 7 7	3 9 9 1 8	7 9 9 3 9	9 8 2 9	3 10 8 4 6	10 8 1	 *≡⁰ *° 			j * 	 * °≡°	★ ≡ p * ⁰≡⁰ 	$\fill \fil$
21 22 23 24 25	St. Cu. St. Cu. : Ci. St. A. Cu. St.	A. Cu. : Ci. St. St. Cu. A. Cu. : Cu. : Ci. Ci. Cu. St.	A. Cu. : Ci. St. St. Cu. St. Cu. : A. Cu. St. Cu.	9 7 9 0 10	8 10 9 6 10	8 9 3 2 10	8 9 3 1	6 10 3 0 6	8 10 0 0	 ⊔≡º	.:. p * .:. ⊔≡⁰	 e	 d		:: :: :: ::	$\footnote{f x}$ op $\footnote{f x}$ early, o to c a : c to bc p : c & bc n : $\footnote{f x}$ op $\footnote{f x}$, $\footnote{f x}$ to o a : o $\footnote{f p}$: o, op $\footnote{f x}$ of to b $\footnote{f a}$: b & bc $\footnote{f p}$ and $\footnote{f n}$: $\footnote{f x}$ b $\footnote{f x}$ b $\footnote{f x}$ = $\footnote{f x}$ op $\footnote{f x}$ 0, e $\footnote{f a}$: od $\footnote{f v}$ 0 to bc $\footnote{f p}$: bc to o $\footnote{f n}$:
26 27 28 29 30 Mean	St.: St. Cu.	St. St. Cu. : A. Cu. Nb. St. Cu. : A. Cu. St. Cu.	St St St.	10 10 10	10 10 10 10	9 10 7 7	10 10 1 1 10	10 0 10 0	10 9 0 10	 ≡° ≡° 	 ≡° p * °≡°	*≡°	e *°≡° =°	e ≡° ≡°	e ≡° ≡°	o, od, $o \oplus$ to o $a : oe p \ and n :$ o at first, $op^0 \cancel{X} \ a : o$ to $b \equiv^0 p : b \equiv^0 n :$ o, $o \equiv^0$, $o \cancel{X}^0 \equiv^0 a : op \cancel{X}$, $o p \ and n :$ o, $op^0 \cancel{X}$, $c \ a : c$ to $b \ p : b \ n :$ $b \coprod$, $op^0 \cancel{X}$, $c \ a : c$ to $o \equiv^0 p : o \equiv^0$, $o \oplus \equiv^0 n$
Cloud Am'nt				7.2	7.7	7.9	7.6	5.0	6.1							
207	. Eskdalemuir.	<u> </u>			1	1	1			·		,———	1			December, 1923.
1 2 3 4	St. St. Cu. St. Cu. Nb.	Nb. St. Cu. Nb.	Nb. St. Cu. St. Nb.	10 10	10 10 2 10		i	10 10	8 10	≡ *°⊔	≡ =° ⊔ *=°	• *≡°	d≡° ≡° *=°	●≡° ≡ *≡°	≡ : ≡°	o \equiv to o \equiv to o \bullet \equiv a : o \bullet , od 0 \equiv 0 p : o \bullet & o \equiv 0 to c a : c & o p and n : o \square to b a : b to o $\equiv p$: o \equiv to o n : o \square , o \times 0 \equiv 0 a : o \times , o \times 0 \cong 0 p : o \times 0 \cong 0 to 0 p : o \times 0 \cong 0 n :
5	Nb.	St. : St. Cu.	Nb.	1	10		}	10	1	*°	★⁰		•••	●°≡°		$0 \bullet^{0} * 0 * 0 * 0 * 0 * 0 * 0 * 0 * 0 * 0 *$
6 7 8 9 10	 Nb. F. St. : St. Cu. St. Cu. St.	 Nb. F. Cu. St. Cu. : A. Cu. Nb.	 Nb. St. Cu. St. Nb.	0 10 10 2 10	2 10 10 1 10	0 10 1 7 10	3 8 10	0 10 1 9	1 10	 * "! ≡ :	p d°≡°	d° d°≡°	 •≡° od°≡°	.:. •≡° 1 od°≡°	d ≡°	$0 *^{0} \bot = {}^{0} to od^{0} a : od^{0}, o ⊕ = {}^{0} p : od = {}^{0} n : od = {}^{0} n : od = {}^{0} n : od = {}^{0} n : od = {}^{0} n : od = {}^{0} a : od^{0} = {}^{0} to o ⊕ = {}^{0} n : od = {}^{0} n : od = {}^{0} n : od = {}^{0} a : od^{0} = {}^{0} to o = {}^{0} n : od = {}^{0}$
11 12 13 14	St. Nb. St. Cu. St. Cu.	St. Nb. Ci. : A. Cu. Nb.	Nb. Nb. A. Cu. Nb. : St. Cu.	1	10 10 3 10	10 10 10	10 10 4 10	10 10 2 10	10 8 1	=0 ●=0 	= : •≡° 	d°≡° d°≡° •°≡°	d°≡° •°≡° d°≡°	d°≡° •°≡° •°≡°	d°≡° •≡° 	$0 \equiv^0$, $0 \equiv^1$ at $9h$., $0d^0 \equiv^0 a : 0d^0 \equiv^0 p$ and $n : 0 \oplus \equiv^0$ to $0d^0 \equiv^0 a : 0 \oplus & \oplus^0 \equiv^0 p$ and $n : 0$ to $b : a : bc$ and $b : b$ to $c : a : c$, $0 \in a : 0d^0 \equiv^0$, $0 \oplus^0 \equiv^0 a : 0d^0 \equiv^0$, $0 \oplus^0 \equiv^0 p$ b to $c : a : c & bc : p : c$ to $0p^0 \oplus n :$
15 16 17 18 19 20	St. Cu. Nb. Nb. St. Cu. St. Cu	A. Cu. St. Cu. St. Cu.: Nb. St. Cu. Cu.: F. Cu. St. Cu.	A. Cu. Nb.: St. Nb.: St. Cu. F. Cu. St. Cu.: A. Cu.	10 10 8 6 0	7 10 10 9 8 0	7 10 10 8 3 5	10 10 9 1 8	8 10 10 1 0 8	9 10 2 1 1 8	:: d°≡° ::: ∐		 jp 	 d₀ d₀ 	$\begin{array}{c} \cdots \\ d^0 \\ d^2 \equiv^0 \\ \cdots \\ \cdots \\ \cdots \end{array}$	d°	od ⁰ \equiv ⁰ & o a : o, od p : od ⁰ & o n : od \equiv ⁰ , o a : o \bigoplus \equiv ⁰ , od \equiv ⁰ p : od ² to be n : od, c, op \bigoplus a : o to b p : b \bigsqcup n : b \bigsqcup , c \bigsqcup to b a : b p : b \bigsqcup n : b \bigsqcup , op \bigotimes , bc a : bc to c p : c n :
21 22 23 24 25	Nb. St. Cu. Cu. St. Cu. A. St.	Nb. St. Cu. : Ci. St. F. Cu. St. Cu. : Cu. Nb. : St.	Nb. St. Cu. : Ci. St. Nb.	10 9 1 10 10	10 9 1 10 10	8 1 4	10 10 10	10 9 0 0	10 6 0 10	*° ≡° 	*° ⊔	P * ⁰	P * °≡° *≡° *≡°	*≡° *≡°	* °≡°	o, $o \times^0 \equiv^0$, $o \times^0$, $op^0 \times a : op^0 \times \equiv^0 p : o \times$, $o \bullet to c a : cto o p : cto b n : b a and p : bc n : op^0 \times = arly, op to bc a : bc, o \times \equiv^0 p : b n : \boxtimes off at 7h., ohread off arrow of arrow of ar$
26	St. Cu.	St.	St.	10	10		10	10	10						* ≡⁰	\times 7". overcast all day, snow at night [a, p, n:
27 28 29 30	St. St. Cu. St. Cu. Nb.	St. Cu. St. Cu. St. Nb.	Nb. St. Cu. St. Nb.	10	10 10 10	9	8 10 10	10 2 10 10	0 10	≡° d°≡°	=° ∪ *=°	=° jp * ° •°≡°	= : d≡⁰	● ≡° ≡ ● ≡°	●°≡° *≡ =°	[o, o
31 Mean	St.	Nb.	Nb.	1-		10				_ <u>=</u> 0	<u>d°≡°</u>	●≡0	<u>d≡</u>	d ≡ 0	● ⁰ ≡ ⁰	$ \begin{array}{c} [\circ \bullet^0 \equiv^0 n: \\ \circ \bullet \equiv^0 \text{ to od } \equiv^0 p: \end{array} $
Cloud Am'nt				8.3	8.1	7.5	8.2	7.4	7.3	<u> </u>	<u> </u>					
Day.	7 ^h	13h	18h	.	<u></u>	13h		<u> </u>	21h	7h	9h	13h	15h	18h	21h	Remarks.
		Cloud Forms.				ud A			i			Wea	ther.			

POTENTIAL GRADIENT (reduced to level surface): VOLTS PER METRE. Mean Values for periods of sixty minutes, centred at the exact hours, Greenwich Mean Time.

208. Eskdalemuir. 1923.

200. Lakuai		January. 1	Factor 6.68.			February.	Factor 6.81		. 	March. Fa	actor 6.87.	
Day.	3 h.	9 h.	15 h.	21 h.	3 h.	9 h.	15 h.	21 h.	3 h.	9 h.	15 h.	21 h.
	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.
I	375	632	814	z-	40	68	180	0		_		
2	217	-237	<u> </u>	<u> </u>	72	128	176	z-	_	-		
3	-316	292	-296	245	104	84	124	148	92	-1,299	-238	337
4	174	296	818	877	40	232	196	640	264	311	143	370
5	379	-205	-20	355	260	216	24	-8	520	-1,087	135	135
6	225	198	324	517	160	-1,012	-1,160	z-	403	260	212	190
7	-731	478	356	154	164	z	404	368	- 5 86	209	-37	73
8	130	119	225	363	68	60	z —	752	201	-933	168	146
9	z-	186	126	134	z-	972	356	580	176	157	146	209
10	z	z+	182	182	-1,36o	-2,448	-1,280	88	110	234	95	183
11	103	182	190	434	352	-832	-660	-68	99	88	113	143
12	474	387	352	308	20	-480	z+	608	187	293	66	209
13	359	415	280	494	292	316	240	88	113	348	300	300
14	174	415 87	209	118	172	48	216	208	677	366	242	505
15	107	174	205	225	184	456	260	104	209	106	172	190
16	197	533	194	399	-348	20	172	576	300	234	238	362
17 18	197	134	221	-1,066	280	232	208	188	168	194	245	490
18	-158	134 186	419	205	56	z+	z+	656	253	201	234	512
19	138	276	-849	122	368	i	\	<u> </u>	384	267	322	220
20	87	146		_	-	_	180	280	161	_	340	. 461
21	 	_	198	170	620		272	134	311	505	307	311
22	87	55	32	494	163	717	380	239	633	721	285	575
23	186	340	138	71	243	322	311	297	227	121	410	113
24	43		103	118	195	264	188	243	392	538	282	611
25	99	158	103	¹ 74	76	-724	-1,539	376	242	212	176	498
26	67	111	158	229	181	-369	-	243	443	198	139	355
	111	32	67	134	-453	116	-507	36	92	194	300	-92
27 28	40	67			-453 673	210	-134	<u> </u>	-113	220	26	117
29	1 -		28	340				i	458	157	165	501
30	111	99	170	71		1			212	436	157	285
31	150	276	z	146					439	. 392	245	124
(a)	176	234	246	272	208	275	229	311	288	278	215	304
(a) (b)	101	207	157	234	15	-57	-93	197	247	130	176	285
lean	. (a)	232	(b)	175	(a	256	(b)	15	(a)	271	(b)	209

Mean	. (a)	232	(b)	175	(a)	256	(b)	15	(a)	271	(b)	209
Eskdalemuir.					,							1923.
		April. Fa	ctor 6.83.		1	May. Fa	ctor 6.86.			June. Fa	ctor 6.52.	
Day.	3 h.	9 h.	15 h.	21 h.	2 h.	9 h.	15 h.	21 h.	3 h.	9 h.	15 h.	21 h.
	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m. v/m. 213 92 116 203 155 179 106 121 194 150 194 116 232 208 -407 -121 145 213 48 2- 247 165 -513 218 73 - 202 -52 183 98 163 222 202 202 156 124 163 222 65 150 163 176 222 261	v/m.	
I	249	187	88	333		<u> </u>		_	53			203 378
2	242	-805	260	322	228	110	231	180	155	ľ		370
3	538	410	183	172	202	396	220	591	348			-266
4	238	168	216	384	506	352	202	378	82		1	82
5	4 ⁸ 3	245	414	633	338	132	253	352	169	194	150	179
6	278	146	234	318	187	81	95	187	-281			213
7 8	161	165	285	245	206	202	143	213	242			232
8	99	238	340	231	132	26	206	367	48	145 213		247
9	132	146	179	329	172	-92	_	-	44	145 213 48 z — 247 165		145
10	267	73	176	128	-	_	_	_	92	48	z	102
11	-2,050	340	183	304	_		_		121			286
12	425	51	-81	-271		<u> </u>	_	_	140			82
13	-48	88	11	40	154	239	z+	37	179			
14	256	212	-33	135		_	_		_		232 208 -407 -121 145 213 48 2- 247 165 -513 218 73 -	143
15	190	560	z-	307	143	z+	275	180	209	-52	183	-248
16	329	157	187	564		_	_		202			189
		300	242	384	! —			l —	248			117
17 18	377 684	373	242	256	l –				365			326
19	150	132	66	216		_		_	215			280
20	216	168	128	157	177	81	-4º	132	209	163	222	437
21	77	70	z+	51	-35	127	172	278	404			228
22	44	70 66	84	99	142	167	55	-5	163			143 228
23	92	150	110	223	146	10	z—	473	274			228
24	231	190	110	282	382	186	111	z-	183	215		189
25	z±	73	z±	-322	136	236	z-	216	111	143	156	143
26	-329	92	z±	183	221	-40	136	z	163	163	189	111
	242	110	256	238	96	216	75	111	85	209	143	339
27 28	201		-183	143	116	75	111	156	352	163	176	391
29	70	110	106	-329	146	166	166	151	241 98	261	189	378
30		_	-	–	116	86	191	141	98	209	143	202
31					70	80	136	15	}			
(a) (b)	251	186	186	257	191	161	163	231	186	166	172 160	222
(b)	154	143	166	225	150	143	148	216	172	119		194
Mean	. (a)	220	(b)	172	(a)	187	(b)	164		187	161	
					·					tial aradian	4 43 . £ - 11	

Note.—The Potential Gradient is reckoned as positive if the potential increases upwards. For indeterminate potential gradient the following notation is used: z + Indeterminate, positive value; z - Indeterminate, negative value; z ± Indeterminate in magnitude and sign.

(a) Mean of all positive readings.

(b) Mean from all complete days using both positive and negative readings.

208. Eskdalemuir.

1923. July. Factor 6.51. August. Factor 6.37. September. Factor 6.48. Day. 3 h. 9 h. 15 h. 21 h. 3 h. 9 h 21 h. 15 h. 3 h. 9 h. 21 h. 15 h. v/m. v/m. v/m. v/m. v/m. v/m. v/m. v/m. v/m. v/m. v/m. v/m. 89 206 198 -267 -59 166 178 563 -23 164 5 -212 -30 12 150 8 297 167 168 158 III -247 -8o 178 II 167 166 510 6<u>0</u>6 208 **1** 121 67 80 166 0 15 ²⁷³ 178 285 188 61 486 185 182 -74I 18 267 -593 Zgg -1,366 148 -<u>5</u>9 20 80 178 -649 III -534 z+-185 III -8oI 1,198 -30 z+ 200 III III III -36-103 87 178 z ---30 -486 81 -30 -12 -95 85 - 182 87 28 -136 -830 558 z — -356 -178 t ţ (a) (b) 82 78 189 161

			_
Eskd	ala	100	ıi#
Lonu			

(a) 203

(b) 184

Mean

(19889)

1923.

(b) 163

Eskdalemuir.												1923
		October.	Factor 6·50.		1	Vovember.	Factor 6.	63.	De	cember. F	actor 6·44.	
Day.	3 h.	9 h.	15 h.	21 h.	3 h.	9 h.	15 h.	21 h.	3 h.	9 h.	15 h.	21 h.
	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.	v/m.
I	260	127	175	212	210	191	62	358	′ ₇ 8	491	-958	246
2	6 r	188	163	188	376	136	185	-62	z+	-300	305	371
3	67	61	-756	436	802	62	z+	265	246	359	246	282
4	200	182	182	212	z +	z +	†	†	389	563	940	300 288
5	151	182	*	224	†	†	93	321	551	-204	114	288
6	194	-121	127	61	167	247	309	487	300	413	749	671
7 8	109	91	115	109	222	222	364	753	539	300	-1,827	-12
	121	151	_†	-375	93	93	191	475	240	150	317	. 785
9 10	-212	67	169	6	302	228	210	228	240	300	785	377
10	-254	-1,392	z	30	185	² 47	302	333	126	341	252	359
11	103	188	127	266	185	222	204	210	210	407	300	359
12	169	z-	-424	738	253	-19	148	154	347	311	431	407 827
13	188	393	127	436	-1,067	154	8o	-802	162	270	401	827
14	200	200	315	303	25	142	228	247	401	30 180	96	252
15	163	73	169	61	² 34	-43	1,246	136	138	180	437	144
16	z-	175	260	266	512	130	136	z +	60	102	108	120
17 18	115	163	91	230	62	740	19	740	72	78	-180 120	300
	182	188	218	151	228	185	² 47	253	24 180	150 204	294	413
19 20	224	67	200	430	130	346	302	518	126	204	389	30
20	127	121	200	296	309	432	173	210	120	·	309	
21	-393	91	139	145	228	241	740	636	240	186	443	1,090
22	121	157	-182	54	432	259	494	740	-928	-24	162	150
23	103	-1,029	-847	157	506	185	463	1,111	126	132	204	443
24	212	-151	-545	z +	784	†	555	543	90	-108	779	69
25	-109	91	-182	218	302	438	123	352	359	†	Į Į	2,150
26	-272	242	-61	617	-1,018	512	309	512	60	180	222	47
27 28	-1,059	242	478	†	271	216	679	438	665	503	671	53:
	-6 1	79	121	-121	185	413	481	333	371	365	371	89
29 30	-73	194	998	-181	62	123	481	413	317	347	60 180	-1,61 6
30	321	-139	242	218	191	346	444	-1,018	150	-329	100	1
31	139	182	97	303					240	270	240	36
(a) (b)	160	156	187	245	258	269	331	431	251	276	356	46.
(b)	73	77	-16	200	123	250	339	310	199	213	213	32
ean	(a)	187	(b)	83	(a)	322	(b)	255	(a)	337	(b)	237

(a) 198

(b) 95

(a) 217

Note.—The Potential Gradient is reckoned as positive if the potential increases upwards. For indeterminate potential gradient the following notation is used: z + Indeterminate, positive value; z - Indeterminate, negative value; z ± Indeterminate in magnitude and sign.

* Defector of all positive readings.

† Light failed.

† Tank empty.

† Tank of all positive readings.

(a) Mean of all positive readings.

(b) Mean from all complete days using both positive and negative readings.

O 3

POTENTIAL GRADIENT (reduced to level surface): DIURNAL INEQUALITIES (in volts per metre).

The departures from the mean of the day are adjusted for non-cyclic change.

209. Eskdalemuir.

* 0a DAYS ONLY.

1923.

													-														
Month and Season.	Hour	G.M.T.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	Midt.	24-0.	No. of Days used.	Mean Values
Jan Feb Mar	- 37 - 52	- 37 - 74	- 67 - 78	- 75 - 17	-106 + 12	- 94 + 30	- 29 + 33	+ 10 + 156	+ 8 + 118	- 31 + 44	-53	v/m. - 29 + 61 - 53	- 53 - 3	- 6 + 4	- 14 - 6	+ 19 - 13	+ 78 - 3	+125 + 39	+151 + 41	+ 74 + 0	+ 29 64	+ 43 - 82	+ 68 - 74	+ 20 - 89	+106 - 3	7 3 16	v/m. 294 306 291
April May June	+ 9	+ 18	+ 16	+ 56	+104	+ 86	+ 16	- 28 + 9 - 14	- 24	- 34	一 55	- 99 - 62 - 32	→ 42	- 29	一 .27	- 23	- 44	- 34	- 39	+ 36	+ 62	 + 17	- 4	- 6	— 10	7 7 15	279 229 194
July Aug Sept	+ 106		. + 8	+ 32	+ 4	+ 27	- 19	一 72	- 66	 6 6	— 81	+ 11 - 66 - 3	129	-125	90	- 90	一 73	– 61	— 10	+ 68	+166	+252	+192	+ 70	156 + 142 80	5 2 6	299 250 271
Oct Nov Dec	- 21	- 71	-106	-103	-146	147	-140	-127	-140	118	-118	- 32 - 44 - 43	- 48	+ 33	+ 22	- 14	+ 89	十170	+309	十307	+242	J+ 98	+ 25	+ 51	+ 73	4 5 9	209 392 319
Year	+ 16	- 12	_ 28	- 17	- 24	_ 8	 - з	- 6	– 2 6	– 43	- 52	— 33	– 50	- 32	- 31	- 31	— 10	+ 25	+ 72	+ 84	+ 79	+ 69	+ 47	+ 17	-	_	278
Winter	- 37	- 62	80	- 67	– 7 9	- 63	- 49	- 5	— 11	- 34	<u> </u>	— , I,4	- 29	+ 3	— 1	+ 1	+ 56	+111	+173	+125	+ 75	+ 39	+ 15	- 15		-	328
Equinox	+ 33	3 - 1	- 17	- 21	- 29	- 7	+ 15	+ 5	- 27	- 47	- 53	- 47	- 46	33	– 31	- 31	- 20	+ 13	+ 66	+ 91	+ 72	+ 67	+ 38	+ 15		-	263
Summer	+ 52	+ 26	+ 11	+ 37	+ 37	+ 45	+ 25	- 17	– 4 0	- 47	- 53	- 37	– 76	– 66	- 61	- 64	– 66	- 50	- 22	+ 36	+ 91	+101	+ 88	+ 50		_	243

210.	E.	kda	lam	orie.

* 1a AND 2a DAYS ONLY.

1923.

2.0	LUNU	Ø101111										2111		<i>D</i>	0.												
Month and Season.	Hour.	G.M.T.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	Midt.	24-0.	No. of Days used.	Mean Values.
Jan Feb Mar	+ 12	+ 10	+ 0	- 9 - 231	- 49 - 158	+113	1 3	+ 49 + 35	- I + 77	-122	+ 02	- 59 + 04	- 59 + 32	+ O	- 40 + 23	- 89 + 50	+ 7	+226	+202	+102	+ 111 - 49	+ 44 - 73	- 16 - 6	- 90	- 44 - 328	2 2 4	v/m. 219 268 249
April May June	+ 25	+ 30	 	i — 5	: ac) — 31	32	l 62	i — 83	- 27	!∔ I	1 + 13	I 6	 + 12	 	1+ 22	1+ 35	+ 24	1+ 8	十 22	I- 9	+ 24	🕂 3	+ 40	十 10	3 2 4	143 88 197
July Aug Sept	I— 30	I- 13	— IQ) 3	1 50	1 2	— 4I	I— 30	I — 45	- 26	-10	ı —	— <u>4</u> 2	- 46	- 72	80	I— 57	ı— 9	14 70	 1 00	T-121	T-103	T 90	T 29	- 10 - 13 - 33	10 5 7	173 214 155
Oct Nov Dec	I 18a	- II2	- 45	I7I	-120	- IQ2	-253	-236	I I 36	- 20	I— I7	'l II	1 + 25	I+ 81	(+ I 30	1+200	+ 201	1+50T	J+227	T 229	7 101	T 201	_ 20		-057	3 2 3	188 113 140
Year	– 35	- 37	- 29	- 44	- 50	- 29	_ 20	- 19	- 16	— 10	- 7	- 4	- 19	+ 3	- 6	- 2	+ 35	+ 64	+ 68	+ 71	+ 48	+ 43	+ 13	- 14		-	179
Winter	- 88	- 91	- 69	-118	96	5 - 57	- 41	- 41	- 16	- 12	+ 2	+ 11	+ 9	+ 47	+ 26	+ 34	+110	+149	+121	+123	+ 71	+ 48	- 19	- 97	_		185
Equinox	- 22	- 25	- 17	- 39	<u> </u>	 - 9	+ 6	+ 6	+ o	— 1	- 3	– 10	– 33	- 20	- 25	- 28	+ 1	+ 39	+ 47	+ 47	+ 34	+ 55	+ 21	- 8	_	_	184
Summer	+ 6	+ 4	— т	+ 26	- 39	- 22	- 26	- 20	- 33	- 16	_ 21	- 14	- 34	- 19	- 19	- 11	- 5	+ 4	+ 35	+ 43	+ 38	+ 27	+ 38	+ 62			168

1923.

ELECTRICAL CHARACTER OF EACH DAY.

210A. Eskdalemuir.

					1	1		1		1		1
Day.	Jan.	Feb.	Mar.	April	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
I	2 <i>b</i>	2 <i>b</i>	*	ıb	*	oa	*	1b	1b	oa	16	20
2	2 <i>b</i>	2b	*	16	oa	oa	*	20	0a	1 <i>a</i>	1a	20
	1 <i>b</i>	20	20	oa	00	16		2b	14	2b	20	oa
3	0a	16	00	16	oa	1 <i>b</i>	oa	04	2b	00	*	16
4 5	20	2b	20	oa	oa	2b	1a	1a	Ia	2 <i>b</i>	*	2 <i>b</i>
6	16	26	2 <i>b</i>	oa	16	1 <i>b</i>		1a	1 <i>b</i>	16	04	oa
	2b	20	26	16	oa	Ia	*	2b	oa	16	oa	20
7 8	1 <i>b</i>	20	20	oa	16	26	oa	16	oa	2b	20	1b
	2b	1b	1 <i>a</i>	I a	*	1 <i>a</i>	oa	*	14	2b	2b	1b
9 10	2 <i>0</i>	26	oa	20	*	26	16	0a	oa	20	16	1b
	0.4	20	oa	2b		ıa.	1a	1а	1 <i>b</i>	ıb	1 <i>b</i>	oa
II	0a	2b	2b	20		2 <i>b</i>	oa	1a	16	20	14	oa
12	oa La	1a	1a	20	20	1 <i>a</i>	oa	1a	1a	16	20	1b
13	1 <i>a</i> 1 <i>b</i>	1 <i>b</i>	oa	20	20	*	ıa	oa	16	oa	10	16
14			oa	16	16	16	Ia	16	16	16	10	10
15	oa	Ia	000	10	10	10	14	10		j		
16	oa:	2 <i>b</i>	0a	oa		Ia	1 <i>a</i>	2b	16	2b	16	oa
17 18	1 <i>b</i>	0a	oa	oa	*	oa	20	2b	20	oa oa	16	1a
18	1 <i>b</i>	IC.	oa	oa	*	oa	1a	20	16	I a	16	Ia
19	2b	*	oa	oa	*	. oa	2 <i>b</i>	1a	2 <i>b</i>	2 <i>b</i>	oa	oa
20	1 <i>a</i>	*	oa	1a	2 <i>b</i>	Ia	Ia	2 <i>b</i>	1 <i>b</i>	1 <i>b</i>	16	16
21	oa	16	oa	I C	16	oa	16	2 <i>b</i>	1a	20	1 <i>b</i>	16
22	1 <i>b</i>	oa	oa	Ia	1 <i>b</i>	oa	Ia	26	2 <i>c</i>	20	1 <i>b</i>	2 <i>b</i>
23	oa	oa	oa	1 <i>b</i>	20	oa	1b	20	1 <i>b</i>	20	0a	oa
24	2b	1 <i>b</i>	oa	1 <i>b</i>	2 <i>b</i>	oa	1a	1 <i>b</i>	1 <i>b</i>	10	0a	16
25	1 b	20	1a	20	20	04	1a	1 <i>b</i>	26	20	16	10
26	oa	20	oa	26	20	oa	1 <i>a</i>	26	1a	20	26	04
27	1a	20	1 <i>b</i>	1 <i>b</i>	16	oa	1a	20	20	20	oa	1 <i>b</i>
27 28	*	2 <i>b</i>	2 <i>b</i>	1 <i>b</i>	1a	oa	1 <i>b</i>	20	Iа	2 <i>b</i>	1 <i>b</i>	0a
29	*		oa	2 <i>b</i>	oa	04	1a	20	0a	2 <i>b</i>	16	2 <i>b</i>
30	oa		oa	2 <i>b</i>	oa	oa	2 <i>b</i>	2b	oa	2b	10	2 <i>b</i>
31	2 <i>b</i>	_	1 <i>a</i>	_	1 <i>a</i>		*	2 <i>b</i>	_	та	_	2 <i>b</i>
			0.66	7.04	7.00	0.62	0.02	Y . 42	1.00	1.42	0.96	0.97
Iean Character Figure	1.00	1.45	0.00	1.04	1.00	0.02	0.92	1.43	1.00		_	-
No. of days used	29	26	29	30	22	29	25	30	30	31	28	31

^{*} Defective Record.

Explanatory Note.—The electric character of the day is indicated by the figures o, 1, or 2 according to the character of the trace of the electrograph as regards negative potential gradient. The explanation of these symbols is as follows:—

o, denotes a day during which from midnight to midnight no negative potential was recorded.

I, denotes one or more excursions of limited duration to the negative side of the scale.

^{2,} denotes negative potential extending in the aggregate over 3 hours or more.

[&]quot;a,"denotes that within the 25 periods of 60 minutes for which an estimate of the mean potential gradient has to be made in the process of tabulation there was in no case a range of potential gradient in the open exceeding 1000 volts.

[&]quot;b,"denotes that a range of potential gradient in the open exceeding 1000 volts was reached in at least one but in fewer than six of the 25 hourly periods referred to above.

[&]quot;c,"denotes that a range of 1000 volts or more occurred in at least six of the 25 hourly periods.

TERRESTRIAL MAGNETIC FORCE: NORTH COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

211. Eskdalemuir. (X.)

15.000 v (·15 C.G.S. unit) +

January, 1923.

\$\frac{4}{5}\$ \frac{1600}{99}\$ \frac{998}{99}\$ \frac{996}{996}\$ \frac{998}{996}\$ \frac{992}{991}\$ \frac{991}{994}\$ \frac{997}{997}\$ \frac{992}{991}\$ \frac{996}{994}\$ \frac{997}{997}\$ \frac{997}{993}\$ \frac{996}{996}\$ \frac{998}{998}\$ \frac{1000}{995}\$ \frac{1000}{998}\$ \frac{996}{996}\$ \frac{998}{998}\$ \frac{1000}{996}\$ \frac{998}{998}\$ \frac{999}{999}\$ \frac{999}{998}\$ \frac{999}{999}\$ \frac{999}{999}\$ \frac{999}{999}\$ \frac{1000}{1000}\$ \frac{1000}{1000}\$ \frac{1000}{998}\$ \frac{991}{991}\$ \frac{996}{995}\$ \frac{998}{996}\$ \frac{1000}{996}\$ \frac{1000}{998}\$ \frac{1000}{1000}\$ \frac{1000}{1000}\$ \frac{1000}{998}\$ \frac{991}{999}\$ \frac{1000}{998}\$ \frac{1000}{996}\$ \frac{998}{998}\$ \frac{1000}{999}\$ \frac{1000}{999}\$ \frac{1000}{998}\$ \frac{1000}{1000}\$ \frac{1000}{988}\$ \frac{991}{991}\$ \frac{1000}{995}\$ \frac{998}{996}\$ \frac{1000}{996}\$ \frac{1000}{998}\$ \frac{1000}{1000}\$ \frac{1000}{996}\$ \frac{998}{999}\$ \frac{1000}{999}\$ \frac{1000}{1000}\$ \frac{1000}{1000}\$ \frac{1000}{1000}\$ \frac{1000}{1000}\$ \frac{1000}{1000}\$ \frac{1000}{996}\$ \frac{998}{999}\$ \frac{1000}{999}\$ \frac{1000}{1000}\$ \fra												15	,000 γ	(·15 C.0	3.5. ur	11t) +											
1 995 992 992 992 994 996 996 996 996 996 996 996 996 996 996 997 997 997 998 992 998 999 998 999 998 999 998 999 998 999 998 999 998 999		о.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
2 996 999 1001 1001 1005 1006 1005 1006 1005 1006 1005 990 993 990 995 1001 1006 1005 1005 1005 1005 1005 100	Day.	γ	γ	γ	γ	γ			γ	γ	Y	γ			γ	γ			γ				γ	γ		γ	γ
3 996 995 1004 996 996 1001 1006 1000 1006 1001 997 997 997 998 1002 1000 1000 1998 998 1002 1000 1000 1998 998 1000 1000 1009 998 995 1000 1000 1000 1000 1000 1000 1000	1		1										_	-					1			4				999	997
\$\frac{4}{5}\$ \frac{1000}{99}\$ \frac{99}{99}\$ \frac{996}{990}\$ \frac{996}{990}\$ \frac{998}{990}\$ \frac{1000}{991}\$ \frac{1000}{994}\$ \frac{1000}{994}\$ \frac{1000}{997}\$ \frac{1000}{1000}\$ \frac{1000}{997}\$ \frac{1000}{997}\$ \frac{1000}{997}\$ \fra				1	1		1 !	118 -	l									1	1							996 1001	998 999
5 997 1002 990 996 999 997 1002 1004 1002 1000 996 995 998 1000 1000 1000 1000 1000 1000 1000	1 -							2 I i										1	, .				1	1		997	999
6		I	1				1 :	\$13	i	í		1 -				1			1	, ,					1	995	996
7 Q 996 995 993 994 995 997 999 999 1003 1006 1006 1006 1006 1006 1006 1006	, ,	997	1002	990	990	990	992	991	994	997	997	993	990	907	993		990	999	1.000	1000	995	1000				100	
8 \(\begin{align*}{8} \(\begin{align*}{9} \) \(\begin{align*}{98} \) \(\begin{align*}{99} \)	6	995	995	993	996	997	1002	1004	1002	1000	996	995	998	1002	1002	998	1000	995	986	992	998	995	992	995	1000	996	997
9 999 998 998 999 999 999 1003 1006 1013 1009 1004 1001 998 992 989 991 994 994 997 997 997 997 997 997 998 999 998 999 999	7 Q		995	993	994		996	1000	1004			991	991	995	996	1000	1000	1000	996			1000	1	1	1	998	997
10 997 999 999 998 993 1006 1007 1006 1007 998 992 988 992 988 987 987 987 988 988 988 988 988 988	1								1	1	1							l .				-				1000	999
11 995 994 996 999 1003 1006 1007 1006 1005 995 987 987 987 987 988 988 988 988 989 999 1013 1007 1003 1003 1003 1000 995 994 998 999 999 999 999 999 999 999 1014 1016 1014 1016 1021 1022 1004 1004 1024 10	1									1			1						1			,				997	999
12 993 991 993 995 995 999 999 999 999 1002 1004 1008 1013 1009 1013 1007 1003 1003 1000 995 995 995 995 995 995 995 997 1004 1008 995 995 995 995 995 995 995 995 995 99	10	997	999	999	998	993	1000	11013	1009	1004	1001	998	992	989	991	994	997	997	990	970	972	979	907	993	995	995	995
12 993 991 993 995 995 999 999 999 999 1002 1004 1008 1013 1009 1013 1007 1003 1003 1000 995 995 995 995 995 995 995 997 1004 1008 995 995 995 995 995 995 995 995 995 99	7.7	005	90.1	996	900	1003	1006	1007	1006	1005	005	087	087	087	085	087	980	988	986	980	004	997	996	995	997	993	995
13 D 995 995 995 997 994 995 997 994 1004 1004 1005 1905 994 994 988 989 989 999 995 1001 1000 1	t																	1 -	1 -			985				995	996
14 995 995 995 997 997 999 999 1004 1008 995 994 994 995 998 999 995 999 1001 1002 1008 1003 1003 1003 1003 1003 1003 1003																										995	999
16 996 995 999 1003 1007 1009 1012 1008 1003 1000 992 989 995 999 1001 1003 1005 1004 1001 1003 1005 1004 1008 1013 1005 1004 999 994 992 994 889 995 999 1001 1003 1005 1005 1004 1008 1013 1001 1002 1003 1004 1004 1007 1009 1009 1008 1004 1000 997 999 999 1004 1003 1004 1006 1006 1006 1006 1006 1006 1007 1001 1001											994		989			995				999	998					994	997
17		994	996	997	997	999	999	1001	1003	1003	997	999	998	994	992	996	996	999	996	1004	1008	1008	1001	999	997	996	999
17									0				-0-									7007	000	7074	1002	1002	1002
18 O 1012 1006 1004 1003 1004 1003 1004 1007 1009 1009 1008 1006 1003 1006 1006 1004 1004 1006 1007 1002 1001 1001 1002 1003 1006 1009 1009 1009 1009 1009 1009 1009									í		1				999	999	1001	1003	1005	1005	1004	*				1003	1002
19 0 1001 1001 1002 1003 1006 1009 1009 1010 1009 1009 1009 1010 1001 1000 1009 1001 1001 1000 1						1			1						1006	1006	1004	1004	1006	1006	тоо8	1007	, .		, 0	1001	1005
20 D 1005 1005 1005 1006 1009 1010 1014 1016 1017 1009 1009 1017 1014 1009 1005 1011 1014 992 985 995 1003 1005 1023 21 D 990 989 990 1000 1010 929 1010 1005 1005 999 990 980 976 990 981 1001 997 985 990 1010 1000 996 981 1000 1000 1000 1000 1000 1000 1000		1	1						-	1 =	i i	!	, ,			Ł			1			1	1	1	1	1004	1004
21 D		l.	1	T .	, .	1					, .	1										995	1003	1005	1023	990	1008
22				1	ì] .	Ì) '		_	•					1								
23	21 D				1	}											1								1 -	1003	996
24	1	, ,																				1				1008	994
25 998 1000 998 1000		Į.				1	1 1									1							, -		1	998	996 999
26					(1 -										3		\$	1		1	1000	999
27 Q 1000 1000 1000 1001 1001 1002 1004 1005 1007 1005 1005 1000 992 991 991 993 996 995 995 998 1000 1000 1000 1000 1000 1000 1000	25	990	1000	990	1000	1000	1000	1007	1002	1000	990	909	903	900	993	993	994	991	990	1000	1001	1002	1003	1	12004		990
27 Q 1000 1000 1000 1000 1001 1002 1004 1005 1007 1009 1010 1009 1010 1009 1010 1009 1010 1009 1010 1009 1010 1009 1010 1009 1010 1000 1	26	1000	1000	1000	1000	1002	1005	1007	1007	1006	1004	997	995	993	991	992	996	997	1000	1000	1002	1004	1005	1004	1001	1000	1000
28	27 Q	1000	1000	1000	1001	1004				1005						996			998	1 8		1			1	1001	999
30 D 1000 999 1000 1000 1000 1005 1012 1000 1000 999 990 982 971 975 987 981 991 986 990 1000 1006 1000 997 1002 31 1001 998 1000 1001 1001 1003 1014 1011 1005 1000 989 983 982 985 992 996 996 1004 1004 1002 1001 1001 1008 1003					, ,		1 1	_	l l	1009	1			986	990		1	1								1005	1000
31 1001 998 1000 1001 1001 1003 1014 1011 1005 1000 989 983 982 985 992 996 996 1004 1004 1002 1001 1001 1008 1003		_	,	ľ	l .	_	1 1:		1	l .	, ,					1		į.							1	1000	1004
31 1001 990 1001 1001 1001 1000 909 903 902 909 990 1001	30 D	1000	999	1000	1000	1000	1005	1012	1000	1000	999	990	982	971	975	987	981	991	986	990	1000	1000	1000	997	1002	1000	995
	31	1001	998	1000	1001	1001	1003	1014	1011	1005	1000	989	983	982	985	992	996	996	1004	1004	1002	1001	1001	1008	1003	1003	999
Mean † 999 998 998 999 1000 1002 1006 1005 1004 1000 994 991 990 993 997 997 997 998 997 999 999 999 1001 1001	Mean †	999	998	998	999	1000	1002	1006	1005	1004	1000	994	991	990	993	997	997	997	998	997	999	999	999	1001	1001	999	999

TERRESTRIAL MAGNETIC FORCE: WEST COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

212. Eskdalemuir. (-Y.) 4.000 ν (·o4 C.G.S. unit) +

January, 1923.

							<u>. </u>					4,000	y (·04 C.0	3.5. ui	11t) +				i							
Hour. G.M.T.	О.	I.	2.	3⋅	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21,	22.	23.	24.	Mean.
Day. 1 2 3 4 5	γ 685 691 685 687 681	9 687 692 688 687 677	γ 688 695 687 690 675	9 691 697 680 691 676	9 692 698 690 691 671	9 691 693 689 688 683	9 689 692 687 689 691	γ 688 690 686 689 688	9 687 687 687 686 686	9 687 685 690 686 687	γ 688 685 692 685 688	9 691 693 693 695	γ 695 697 707 700 693	γ 698 701 704 702 698	γ 698 703 703 703 698	7 694 701 703 702 697	9 693 695 697 700 695	γ 694 689 696 697 693	γ 696 683 695 696 694	γ 695 689 692 695 693	γ 694 684 683 688 691	9 691 681 689 684 686	7 690 682 687 650 684	9 689 684 687 667 683	γ 692 685 687 681 681	7 691 691 692 689 688
6 7 Q 8 Q 9 10	680 679 680 685 682	678 676 684 685 686	682 680 686 687 686	690 682 685 689 686	685 685 689 691 696	690 686 687 693 688	690 686 686 693 686	689 687 686 692 683	686 686 685 690 685	687 682 685 687 688	692 681 686 687 691	695 690 686 690 691	704 696 690 694	702 695 696 698 698	700 697 697 698 698	698 694 694 699 696	698 692 692 700 696	696 692 692 697 696	694 692 691 692 701	694 692 690 690 702	678 690 689 690 687	668 685 686 681 682	677 684 686 674 683	681 681 685 679 684	679 680 685 682 683	689 687 688 690 690
11 12 13 D 14 15	683 681 683 701 679	680 683 685 694 683	683 683 686 681 685	680 685 686 681 687	679 686 690 699 685	684 685 691 694 686	689 685 689 695 685	690 687 707 685 685	690 691 705 683 683	692 691 692 687 680	695 694 696 691 683	696 697 697 692 687	698 703 698 695 696	700 703 701 695 698	701 701 701 690 696	695 693 695 690 692	696 691 698 690 691	693 693 694 689 688	690 691 682 688 690	687 689 686 685 690	686 687 669 685 689	683 686 638 684 685	681 685 643 681 681	681 684 675 674 674	682 683 701 679 676	689 690 687 688 687
16 17 18 Q 19 Q 20 D	676 677 685 685 685	680 681 685 687 685	683 685 683 688 688	686 688 685 690 690	691 689 690 691 691	691 689 690 689 691	690 685 687 688 691	688 684 686 685 689	683 682 688 684 688	681 679 683 684 688	682 680 686 686 689	687 683 690 691 693	696 691 699 697 705	697 701 701 700 706	693 696 693 698 695	690 692 689 695 705	689 694 689 693 698	690 694 690 690 701	690 692 689 687 695	687 689 689 686 672	683 686 686 684 679	681 685 682 682 679	663 680 680 681 667	669 674 683 683 618	677 685 685 685 646	685 687 688 689 686
21 D 22 23 24 25	646 659 679 675 675	673 683 692 677 682	713 683 685 681 679	689 692 685 681 678	685 691 683 679 679	690 685 685 694 682	699 688 688 680 680	691 688 694 682 677	683 707 690 685 681	680 696 691 688 680	680 695 686 690 688	683 694 692 689 688	690 701 685 694 694	702 702 698 694 697	702 697 698 693 695	697 691 696 689 688	695 689 689 681 690	689 685 661 689 686	679 685 679 678 685	675 669 682 675 684	679 671 683 685 684	679 659 674 681 681	670 663 679 671 682	666 670 675 675 682	659 679 675 676 682	685 686 685 684 684
26 27 Q 28 29 D 30 D	682 680 682 684 677	682 683 684 686 672	683 684 687 689 682	682 684 688 688 662	692 684 684 689 669	679 684 684 685 675	682 684 684 688 678	681 682 684 690 683	682 679 682 685 689	683 676 680 678 679	686 678 682 678 673	689 682 688 684 679	694 685 692 690 684	702 694 699 700 688	698 698 700 700 701	691 690 694 704 700	688 691 690 700 684	687 690 686 705 689	686 688 685 704 677	682 687 684 691 674	684 680 683 688 673	684 678 678 668 677	682 676 678 652 678	682 678 683 664 677	680 682 684 677 681	686 684 686 687 680
Mean †	681 680	68 ₂	690	679 685	678 687	682	680	679 687	674	673	674	678 690	688	695 699	694 698	692 695	683	679 691	685 689	685 686	681	677 679	679 676	679 676	678 680	682
	1	١	1		1	,	•	1	/	1	1	1 090	095	""	-,-	"	1	-	1	ł	l		<u> </u>	<u> </u>		j

^{*} Light failed. † Mean of 30 days; 17th omitted. Q denotes an "International Quiet Day." while D denotes a disturbed day used for the computation of Tables 271-276.

TERRESTRIAL MAGNETIC FORCE: VERTICAL COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

Eskdalemuir. (Z.)

Mean values for perious of sixty minutes centrea at the Hours of Greenwich Mean 1 ime.

January.

<u> 213.</u>	Esko	lalem	uir. (Z.)							44,00	ογ(•.	44 C.G.S.	unit)	+				1					Janu	ary,	1923.
Hour G.M.T.	о.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	.Mean.
Day. 1 2 3 4 5	941 939 939 936 942	941 938 938 938 936 939	γ 940 937 932 936 938	939 937 933 935 931	938 935 931 935 931	938 934 930 934 931		γ 938 934 930 932 934	938 935 930 933 934	936 935 930 933 933	936 933 931 931 934	939 932 931 929 933	939 933 931 930 935	γ 938 933 932 932 934	940 935 935 935 935 935	942 938 938 938 938 935	944 938 938 937 937	γ 942 940 936 936 936	γ 939 942 936 938 935	938 938 937 937 938 935	938 939 938 938 941 935	γ 938 942 937 943 936	938 942 936 949 936	938 941 935 947 936	γ 939 939 936 942 938	939 937 934 936 935
6 7 Q 8 Q 9 10	939 938 935 933 934	939 937 934 933 932	939 937 932 932 931	936 937 932 932 930	936 938 932 931 929	936 936 933 930 924	935 936 934 930 924	935 934 934 929 926	934 934 932 929 926	932 934 931 929 926	932 932 932 929 929	932 931 931 928 930	931 930 930 926 930	933 930 929 926 931	937 932 933 930 934	939 936 936 933 935	939 936 936 933 935	940 936 936 934 937	940 937 935 935 942	940 937 935 936 947	943 937 934 934 953	943 938 934 937 951	942 937 932 936 946	938 935 932 935 942	938 935 932 933 938	937 935 933 932 934
11 12 13 D 14 15	938 934 936 926 932	936 932 934 923 932	934 931 934 926 931	930 931 932 928 930	930 931 932 924 929	928 931 930 917 929	929 931 931 919 928	930 931 928 924 928	930 931 924 928 929	930 931 924 928 930	931 933 920 932 931	930 931 923 933 930	931 930 925 932 927	934 931 930 933 928	936 933 933 936 930	938 933 934 936 932	940 935 934 935 933	939 935 935 935 934	939 935 939 935 932	938 939 940 935 932	938 943 945 934 930	937 940 947 934 931	936 938 943 933 933	934 936 936 933 936	933 935 926 932 935	934 934 933 930 931
16 17 18 Q 19 Q 20 D	936 930 927 931 929	935 930 925 931 929	933 930 927 931 929	930 930 928 931 928	928 929 928 929 928	928 929 929 928 927	928 930 929 928 926	929 930 928 927 925	930 930 928 927 924	929 930 929 927 920	931 930 927 929 920	930 929 929 929 918	929 928 930 930 916	931 928 931 931 923	934 931 933 935 928	933 933 933 935 928	932 933 934 933 928	931 932 933 933 928	931 930 932 932 935	930 930 931 931 946	932 930 931 930 941	933 931 932 929 935	931 932 929 932	932 930 931 928 928	929 926 931 928 923	931 930 930 930 930 928
21 D 22 23 24 25	924 930 930 933 937	922 929 924 935 935	910 928 927 935 937	913 930 931 935 937	922 923 932 936 937	922 918 932 931 937	915 922 930 927 935	920 924 927 931 937	925 926 927 931 937	929 926 926 931 936	930 926 927 932 936	930 926 927 934 937	931 929 933 936 934	933 932 932 938 937	936 935 934 940 940	936 938 937 942 942	940 939 942 944 941	943 939 949 941 941	947 939 947 942 941	943 942 944 941 945	939 940 941 939 945	937 937 939 936 943	937 934 935 936 941	933 934 931 936 940	929 929 932 936 940	930 931 934 936 939
26 27 Q 28 29 D 30 D	941 942 942 944 947	941 941 940 942 944	940 941 939 941 937	940 940 939 940 921	937 940 939 940 929	936 941 940 940 933	937 941 940 938 933	938 941 940 936 937	940 942 940 937 939	940 942 942 940 941	938 942 943 942 943	937 942 944 939 941	937 941 945 939 945	936 941 943 935 946	939 939 945 936 948	942 942 947 941 953	942 941 947 941 956	942 942 947 942 956	944 942 947 948 956 946	944 942 947 951 953	943 944 947 948 949	942 944 947 955 948	942 943 946 955 948	942 942 944 948 945	942 941 943 946 944	940 942 943 942 944
Mean †	936	935	939	932	932	931		932	932	932	932	932	933	933	936	947	939	939	940	940	940	940	939	937	936	935

DAILY EXTREMES OF EACH COMPONENT OF TERRESTRIAL MAGNETIC FORCE: MAGNETIC CHARACTER FIGURES: TEMPERATURE IN MAGNET HOUSE.

214. Eskdalemuir.

January, 1923.

214.	Eskuaie												_						y, 1929.
							Te	rrestrial l	Magnetic Fo	orce.							racter ures.§	Magnetic	Temperature in
Day.		Nor	th Compo	onent.			Wes	st Compo	nent.			Vert	ical Com	onent.			Ī	Character of Day	Magnet
	Maximi 15000 y	ım.	M	inimum. 000 γ +	Range.	Maxit 4000	num.	M	inimum. 100 γ +	Range.	Maxii			nimum.	Range.	$oldsymbol{\mathcal{E}}$ R $^{f a}$	ρ	(0-2).	House 200 +
	h. m.	·γ	$\frac{1}{\gamma}$	h, m.	7	h. m.	1 2	7	h. m.	- v	h. m.	1 2	$\frac{1}{\gamma}$	h. m.	Y	$\frac{100\gamma^2}{}$		İ	a.
1	19 40	1016	986	11 50	30	13 5	699	683	0 20	16	15 52	946	935	9 40	II	13	0.27	1 0	84.5
2	7 40	1009	982	21 30	27	14 15	704	677	17 41	27	17 45	943	931	10 45	12	16	0.34	0	84.5
3	2 7	1010	986	10 50	24	12 6	712	673	2 33	39	15 21	939	929	5 30	10	22	0.46	0	84.4
4	22 15	1015	976	10 38	39	15 30	704	636	22 13	68	22 5	959	928	11 10	24	67	1.42	1	84.4
5	0 53	1005	984	11 36	21	13 20	702	665	3 25	37	0 1	942	930	3 16	12	20 -	0.41	0	84.3
	21 52	_					1								1 .	١.			
6	20 26	1013	981	16 57	32	11 57	707	659	20 17	48	20 15	947	931	12 0	16	36	0.76	0	84.3
7	7 20	1005	989	I 39	16	13 53	698	673	1 0	25	21 35	939	929	11 36	10	10	0.31	0	84.3
8	19 5	1005	991	12 58	14	13 44	698	679	0 10	19	15 10	936	928	12 40	8	6	0.13	0	84.3
9	20 11	1010	986	16 10	24	16 16	706	670	22 10	36	2I II	937	925	12 40	12	20	0.42	0	84.2
IO	6 23	1016	969	19 20	47	4 12	712	679	20 50	33	20 3	953	923	6 12	30	42	0.88	0	84.1
11	6 10	1009	982	13 20	27	14 5	706	676	3 23	30	15 45	941	928	5 30	13	18	0.38	0	84 • 1
12	5 55	1003	979	20 12	24	12 40	706	679	0 1	27	20 15	943	929	11 30	14	15	0.32	0	84 • 1
13	7 30 9 55	1019	979	22 51	40	7 20	717	615	21 35	102	21 10	949	920	9 56	29	128	2.71	1	84 · 1
14	5 50	1014	983	4 9	31	4 16	712	669	22.4	42	T4 20	936	915	4 39	21	33	0.69	ı	84.1
15	18 45	1011	987	4 9 12 35	24	12 42	712	670	23 4 23 49	43 33	14 20 23 20	936	927	12 10	9	17	0.37	0	83.9
16	21 48	1022	984	IO 22	38	12 40	701	654	22 19	47	ОІ	936	927	5 58	9	37	0.79	0	83.9
17	22 53	1020	989	11 30	31	13 15	704	668	23 15	36	15 52	933	925	24 0	8	23	0.49	0	83.9
18	0 28	1014	999	2 10	15	12 46	702	679	21 37	23	14 30	934	923	0 33	II	9	o.18	0	83.9
19	5 15	1010	995	11 10	15	12 46	701	680	21 50	21	14 25	935	927	9 0	8	7	0.12	0	83.9
20	23 2	1040	973	18 34	67	12 51	722	595	22 50	127	18 58	949	915	11 42	34	218	4.59	2	83.9
21	23 20	1053	965	11 50	88	I 52	720	647	оі	73	17 55	948	904	2 20	44	150	3.16	1	83.8
22	21 2	1029	971	12 55	58	$\begin{bmatrix} 8 & 24 \\ 12 & 32 \end{bmatrix}$	711	648	20 56	63	19 40	942	918	5 5	24	79	1.67	1	84.0
23	22 30	1035	947	11 59	88	12 40	702	639	17 2	63	17 13	951	923	0 55	28	125	2.63	1	83.9
24	21 5	1029	980	12 35	49	12 20	701	663	18 16	38	15 45	946	925	5 29	21	43	0.90	I	83.9
25	21 38	1015	981	10 35	34	12 12	699	672	ог	27	19 40	946	933	12 20	13	21	0.43	0	83.9
26	4 44	1014	989	13 44	25	12 56	705	676	5 0	29	18 55	945	934	4 40	11	16	0.33	0	84.0
27	6 2	1007	989	12 50	18	13 40	699	674	9 16	25	20 22	945	934	13 0	8	10	0.31	0	84.∙0
28	7 40	1010	979	12 25	31	13 34	704	675	21 28	29	20 22	943	937	3 0	9	19	0.40	0	84.0
29	21 43	1029	976	17 48	53	12 59	727	636	21 48	91	21 30	940 959	939	13 18	27	811	2.49	I	84·1
30	5 26	1024	961	11 37	63	14 34	710	642	3 7	68	16 41	958	917	2 49	41	103	2.17	I	84·1
31	22 12	1021	977	10 45	44	13 28	698	668	10 41	30	16 30	949	935	2 48	14	30	0.64	0	84 · 1
Mean .		1017	980		37		70 6	662		44		944	927		17	47		0.35	84 · 1
No. of Days used.	-	31	31	-	31	-	31	31		31	_	31	31	-	31	31		31	31

[§] For explanation see page 105. † Mean of 30 days; 17th omitted. Q denotes an "International Quiet Day," while D denotes a disturbed day used for the computation of Tables 271-276.

TERRESTRIAL MAGNETIC FORCE: NORTH COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

215.	ESKO	ialem	uir.	(X.)			I				15,0	οο γ (•	15 C.G.S	unit)	+				1	4				repru	iary,	1923.
Hour G.M.T.	О.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
Day.	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	Y	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ
I	1003	1000	999`	999	1003		1007	1006	1005	1001	1000	996	996	994	997	997	981	995		1001	1002	999	1003	1012	997 1001	1000
2	997	999	1001	1002	1001	1005		1005	1003	1001	997	996	996	997 978	986	988	985	980		993 1001	995	997	983	987	992	993
3	1001	1001	988	1001	1005	1005		1005	1002	992	986	975 983	971 976		986	991	988	986		1001		1006		1001	992	995
4	992	1001	998	997	1001		12 ~		1003	992	996	995	991	977 991	992	1000	1001	1006	1006		1001	1011	1006	1005	1005	1000
5	997	997	990	997	1002	990	1001	1005	1005	997	990	993	991	991	992	1000	1001	1000	1000	1000	1002	1011	1000	1005	1005	1000
6	1006	1007	1010	1011	1016	1017	1014	1017	1010	1003	1003	1000	997	995	997	1001	1002	1003	1006	1006	996	1004	1003	1004	1007	1005
7	1007	1012		1006		1007			1007	1006	1001	999	998	1001	997	996	982	978	998	997	986	992	1001	1004	1001	1000
8	1001	1003	999	997		1007		998	999	1002	997	990	987	983	985	993	996	998		1002	1002	1013	1007	1006	1002	999
9 Q	1002	1002	1002	1002	1002	1005	x 006	1006	1003	998	1001	998	997	997	1001	1002	1004	1006	1007	1009	1008	1009	1007	1006	1006	1003
10	1006	1003	1009	1006	1012	1018	1013	1012	1007	999	992	982	958	969	983	989	997	997	992	992	997	1013	IO2 I	1002	1002	999
	1	1		1			ł		1		i	_	1	1		ì	1		1 8		1	Ì				Ì
II	1002	999	1002	1002		1004		ľ	1007	997	993	998	997	992	986	997	999	1002			1006		1007	1006		1001
12Q	1007	1008	1002	1003	1003	1007	T	1012	1011	1002	997	990	995	1000	1003	1003		1007	1007			1009	1009	1	1008	1005
13Q	1008	1008		1009	1	1008		1	1008	1003	998	994	995	996	999	1003		1005	1008		1009		–	l	1012	1006
14		1012	_	1011		1013			1014	1008	1000	996	998	1000	1003	} /		1013	1014			1018		5	1007	1000
15	1007	1003	1007	1008	1008	1012	1013	1013	1013	1008	999	993	993	995	1001	1009	1012	1012	1009	1005	1004	1009	1012	1009	1000	1000
-6	1008	1008	1012	1013	1014	1021	T02 T	1023	1018	1017	1005	999	.998	1003	1000	998	1003	994	1003	1007	1007	1007	1008	1008	1011	1008
16 17D		1008			1007	1010	F		1011		988	985	993	998	999			1014	1010		994	998	1013	999	1002	1004
18	1	1000	1002	1008	1008	1017			1013	1007	993	983	979	983	990	998	1002	1006	1007		1007		1005	1014	1013	100
19	1013	1004	1006	1007	1008	1009		1017	1014	1009	999	993	989	988	999	999	1000	1012	1008		1005	1007	1008	1007	1008	100
20	1008	1008	1008	1008	1	1013			1014	-	1003	990	988	989	1002			1003	1008		1012		1010	1010	1008	100
								1 .	'							'				•					ļ	
21Q	1008	1009	1012	1009	1011	1012	1022	1018	1014	1010	1002	991	988	995	999	1003		10.12	1013	1013	1013	1012	1011		1005	1008
22~	1005	1013	1010	1018	1016	1024	1031	1019	1013	1010	997	994	992	994	997	1003	1007	1008	1008	1009	1009	1011	1 -		1008	1000
23Q	1008	1008	1008			1009		1012	1011	1003	993	987	985	993	999		1	1013	1013				1013		1012	1000
24	1012	1019	1010			1015			1018	1012	1003	998	995	998	1003	1		1013	1014		1017	1018	1016	1018	1018	1013
25D	1018	1021	1027	1034	1023	1027	1018	1006	1027	1012	979	984	979	965	968	979	993	1037	999	978	965	994	1003	988	935	999
·CD								00.	000	0.56		085	06.	, e.	000	08.	1000	1000		005	1002	1017	1011	997	997	990
26D	934	1003	992	994	992	1002		994	982	959 968	940	982	967	984 984	988	984	978	979	997	997 1012	982	1017	988	997	982	988
27D 28D	997	1002	996	996	1 -		1007	1007	978	986	963	986	975 984	9°4 984	999	904	993	983	1008	4	1001	997	998	997	1003	99
200	982	995	992	909	991	997	993	991	990	900	903	900	904	904	990	992	993	903	1000	997	1001	- 997				
Mean	1002	1006	1004	1005	1006	1010	1012	1011	1007	1001	993	990	988	990	995	998	1000	1002	1003	1004	1002	1007	1007	1005	1002	100
mican	1002	1.000	1004	1005	1200	1.510			1207	1	293	390	550	1	1 333	790			36	1		1	1			

TERRESTRIAL MAGNETIC FORCE: WEST COMPONENT.

					Mea	ın val	ues fo	r per	iods o	f sixt	y mir	ıutes	centred	at the	How	rs of (Green	wich .	Mean	Tim	e.					
216.	Eskd	alem	uir.	(—Y.) <u>,</u> (,	ξ, τ <u>.</u>		ì												•				Febru	ary,	1923.
			5		<u>,</u>	أنسب		,			4,00	ογ (·ο	4 C.G.S.	unit)	+					Ĺ						
Hour G.M.T.	О.	I,	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day 1 2 3 4 5	γ	γ	9	γ	7	7	γ	γ	γ	γ	γ	9	γ	7	7	7	7	9	9	γ	9	γ	9	9	9	γ
	678	679	680	684	679	682	680	683	679	678	679	682	690	701	702	702	689	695	693	660	682	679	678	656	662	683
	662	681	684	682	680	682	679	679	678	673	677	684	692	695	695	692	689	685	673	663	679	678	678	679	679	681
	679	682	684	684	684	684	683	682	678	678	679	684	700	705	710	711	711	707	696	693	668	653	653	647	662	684
	662	656	636	654	666	666	673	679	684	683	682	691	697	701	701	695	688	688	690	688	679	669	668	668	666	678
	666	666	666	673	674	674	680	680	678	673	682	685	690	701	706	710	707	698	694	689	680	675	678	678	678	684
6	678	677	679	682	685	685	689	689	684	679	682	687	689	688	688	685	682	683	684	684	672	660	677	674	674	682
7	674	682	679	680	683	684	686	681	679	678	684	688	688	695	694	694	693	689	657	677	664	668	674	673	668	681
8	668	674	678	684	685	682	684	695	689	680	685	690	693	693	693	690	689	686	684	683	684	678	679	679	678	685
9Q	678	679	678	679	681	682	682	679	682	679	684	690	693	695	693	689	684	685	685	684	684	682	680	679	682	684
10	682	678	680	684	679	678	679	684	682	677	689	688	693	700	703	696	690	690	684	675	677	670	658	677	669	683
11	669	674	680	684	684	679	679	682	678	677	678	683	693	695	694	686	686	688	683	682	679	679	678	679	680	682
12Q	680	677	676	677	679	680	681	679	678	674	672	678	684	686	686	684	680	684	684	684	682	682	680	682	682	680
13Q	682	679	684	684	684	682	680	678	677	674	678	682	685	689	690	688	684	682	680	682	679	679	682	679	679	682
14	679	679	682	683	681	680	682	679	678	673	673	679	690	694	695	694	689	688	688	688	671	647	668	653	667	679
15	667	679	679	683	683	683	680	678	677	673	673	679	688	689	690	693	686	683	683	679	676	679	679	678	678	681
16	678	679	680	684	684	682	680	678	674	673	678	685	690	700	703	694	699	691	685	668	674	674	676	678	679	683
17 D	679	679	684	680	680	680	681	679	678	682	678	684	689	695	695	693	694	690	688	662	655	667	658	666	678	680
18	678	678	682	685	685	685	688	695	669	668	666	673	678	685	689	689	684	682	679	678	674	674	669	674	679	680
19	679	678	679	679	679	679	679	678	676	668	668	676	689	693	700	692	678	684	684	678	674	669	669	677	678	679
20	678	684	679	680	684	678	675	676	676	673	678	684	690	693	694	695	689	675	678	677	678	677	673	674	676	681
21Q	676	688	685	684	679	679	679	678	678	677	678	682	689	694	694	689	683	680	683	683	683	679	678	677	663	682
22	663	658	662	656	659	666	663	673	679	678	679	689	692	693	694	689	683	679	678	677	678	678	678	678	678	676
23Q	678	678	678	678	678	678	678	677	673	668	668	678	687	694	694	693	684	684	684	684	684	684	682	681	679	681
24	679	678	679	679	679	679	682	678	673	669	669	674	684	690	694	690	688	684	684	684	684	684	678	673	680	681
25D	679	673	671	652	635	640	646	671	672	681	688	695	694	7 09	709	700	704	624	640	668	662	661	657	614	652	668
26D	652	667	656	652	646	662	664	668	665	669	677	689	693	691	693	678	677	681	677	673	662	662	661	663	655	670
27D	655	679	677	662	666	672	671	683	684	685	693	687	691	704	693	649	673	684	661	645	615	629	634	657	629	668
28D	629	667	665	668	673	667	668	677	678	682	688	687	694	699	695	688	688	683	635	668	678	673	669	667	649	675
Mean	672	676	676	676	676	677	678	68o	678	676	679	684	690	695	696	691	688	684	679	677	673	671	671	670	671	68o

(5) 8 1923 023 01 36年年 TERRESTRIAL MAGNETIC FORCE: VERTICAL COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

217. Eskdalemuir. (Z.)

February, 1923.

				(-/	,						44	,000 _. 3	· (·44 C.C	S.S. un	it) +		`									
Hour G.M.T.	о.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day 1 2 3 4 5	γ 945 947 945 952 949	943 944 944 941 949	945 943 944 942 949	942 943 944 934 949	942 943 944 933 949	942 943 944 936 949	γ 942 943 944 937 947	942 943 944 937 945	γ 942 943 944 937 945	γ 946 943 944 941 945	946 943 945 941 945	946 939 948 941 943	946 939 947 941 944	γ 946 939 948 943 945	948 942 952 945 948	950 946 956 950 949	956 945 956 953 947	954 944 964 956 949	950 947 964 953 949	957 951 959 950 949	γ 949 947 960 950 952	947 946 958 952 949	946 946 946 956 949 948	946 944 956 949 946	946 944 951 949 945	947 944 951 944 947
6	946	946	945	945	943	942	942	942	942	942	942	942	942	942	945	946	947	949	947	946	950	950	946	946	944	945
7	945	943	943	943	944	945	944	943	943	943	943	943	943	943	944	951	955	962	967	959	963	959	954	951	948	949
8	948	940	938	941	945	947	946	943	943	945	943	943	943	947	951	951	951	951	951	951	951	949	947	947	947	946
9Q	948	948	947	946	946	948	948	948	948	948	948	949	947	944	944	948	948	948	948	948	948	948	948	948	948	947
10	949	949	945	940	937	937	941	941	945	949	945	949	949	953	954	956	957	957	960	960	958	953	949	949	949	949
11	950	950	946	946	946	946	947	949	950	950	950	949	946	946	950	951	951	950	950	951	951	950	950	950	950	949
12Q	951	949	951	949	949	949	948	949	950	954	954	952	951	951	952	955	954	951	951	951	951	951	951	951	951	951
13Q	952	952	951	949	948	948	948	948	949	951	948	948	948	947	948	949	949	948	948	948	948	948	948	948	948	949
14	949	949	949	949	949	949	947	947	949	949	949	949	945	945	946	949	949	949	946	945	949	960	946	949	949	948
15	949	949	949	949	949	949	947	946	947	949	945	945	945	945	945	949	949	949	949	950	951	949	949	949	949	948
16	950	950	948	947	946	946	946	946	946	946	942	942	942	947	949	954	955	955	956	960	957	954	953	951	950	950
17D	951	951	951	950	951	948	948	948	948	946	947	947	946	943	946	951	951	951	953	962	960	958	952	952	948	950
18	948	943	945	943	940	932	931	928	939	940	940	938	939	940	943	947	951	951	950	948	948	948	949	946	943	943
19	943	944	947	947	947	947	947	946	947	948	947	943	940	942	943	952	959	952	951	952	954	952	951	950	947	948
20	947	947	947	947	946	944	943	943	943	944	942	942	943	943	944	947	951	955	953	951	951	951	950	947	947	947
21Q	947	943	941	940	943	945	945	945	945	945	940	938	935	936	939	943	947	947	947	947	947	947	947	946	947	944
22	948	944	941	939	937	934	931	933	937	941	940	936	936	940	943	949	954	952	952	952	949	948	947	946	946	943
23Q	946	946	946	946	946	947	947	947	948	950	948	945	944	944	944	947	948	948	948	948	948	948	948	947	946	947
24	946	944	944	944	944	944	944	944	944	944	944	941	937	940	943	944	944	944	945	945	945	945	947	946	944	944
25D	945	942	937	929	927	929	930	928	925	927	946	929	935	938	943	953	965	988	977	978	987	981	930	934	879	945
26D	879	903	933	863	905	929	935	941	944	945	946	942	943	949	949	957	960	957	957	957	958	949	945	949	949	939
27D	949	944	929	933	938	937	937	937	937	939	944	945	946	946	958	985	980	969	980	972	969	934	937	914	933	948
28D	933	937	940	942	945	945	946	948	945	944	942	942	941	944	950	957	962	972	981	965	960	960	961	961	945	951
Mean	945	944	944	941	942	943	943	943	944	945	945	943	943	944	947	951	953	954	955	954	954	952	948	947	944	947

DAILY EXTREMES OF EACH COMPONENT OF TERRESTRIAL MAGNETIC FORCE: MAGNETIC CHARACTER FIGURES: TEMPERATURE IN MAGNET HOUSE.

218. Eskdalemuir.

February, 1923.

	Farant															Char		I w	Temperature
							Terresti	rial Magn	etic Force.							Figu	res.§	Magnetic Character	in Magnet
Day.			h Compo					Compon			76		al Compo	nent. nimum		Σ R 2	ρ	of Day (0-2).	House
1	Maxim 15000			nimum oo y +	Range.	Maxin			nimum ooγ+	Range.	Maxii 44000			00γ+	Range.				200 +
	h. m.	γ	ν	h. m.	7	h. m.	1 2	γ	h. m.	γ	h. m.	1 2	γ	h. m.	γ	100 y²			a.
ı	19 15 }	1026	969	18 49	57	13 36	705	629	19 2	76	19 2	962	942	3 35	20	94	0.76	1 .	84.1
1	22 41 5		982	18 22	29		698	652	18 23	46	18 35	954	939	12 15	15	32	o·26	0	84 · 1
3	16 30 20 49	1011	967	12 24	49	13 O 15 31	717	644	21 30	73	17 52	966	944	7 8	22	82	o ·66	1	83.9
4	20 38	1020	968	12 41	52	13 27	706	614	1 39	92	17 0	957	933	2 48	24	117	0.94	1 0	84·0 83·9
5	21 1	1020	986	12 40	34	15 38	716	662	1 14	54	20 2	953	943	11 28	10	42	0.34	ľ	63.9
6	20. 20	1042	992	12 58	50	11 25	690	646	20 25	44	20 40	957	941	7 0	16	47	0.38	0	83.9
	20 50	•		_	-	_	1		"	68		970	942	i o	28	78	0.63	1	83.9
7	0 58	1016	967	16 40	49	11 19	705	637	17 53		17 54	1	1	13 14 5	16		0.27		83.9
8	21 16	1021	976	12 39	45 20	7 8	699	666	0 32	33	17 0	951 950	935 944	1 52 13 29	6	34 10	0.08	o	83.9
9	19 38 22 3	1012	992	13 0	80	13 12 13 59	701 710	677	1 13 22 20	24 58	10 50 19 2	950	937	4 40	24	103	0.83	1	83.9
10	22 3	1032	952	12 1/		13 39	/10) 0,2)	-			İ					84.7
11	7 20	1012	973	14 12	39	12 50	702	663	o 16	39 22	14 12	954	944	3 40 6 10	10	31	0.25	0	84·1 84·1
12	6 15	1015	988	10 59	27	12 50	690	668	10 6	22 22	15 10 O I	955	948 945	13 10	7 7	13 12	0.00	ő	84.1
13	22 2	1014	989 988	11 13	25	14 23	695 700	673 626	9 35 20 40	74	20 55	952 963	945	10 45	18	93	0.75	r	83.9
14 15	21 30 7 49	1047 1015	989	20 20 12 50	59 26	14 19 12 2	694	667	0 I	27	20 5	952	945	14 30	7	15	0.13	0	83.9
-3	1 43	1015		3-				,		1					20	50	0.41		83.9
16	7 15	1027	983	14 40	44	14 4	714	662	19 2	52 82	19 I 19 17	961 971	941 943	12 4I 13 20	28	50 190	1.52	í	83.9
17	19 27	1086	979	19 42	107	13 33	701	619	19 16		' '	1 -,	1			88	0.41	1	83.9
18	6 32	1052	972	11 50	80	6 44	705	662	20 10	43	17 10	951	927	641	24		•	0	83.9
19	ог	1023	986	13 11	37	14 10	705	662	20 40	43	15 50	959	939	2 0	20	36 32	0·29 0·26		83.8
20	5 55	1023	983	12 22	40	¹ 4 54	704	667	17 0	37	17 10	956	941	10 40	15	34	0 20	1	
21	6 12	1023	983	12 9	40	13 o	695	662	24 0	33	16 41	947	935	12 0	12	28	0.23	0	83.7
22	6 15	1035	988	12 0	47	11 55	695	654	3 0	41	16 o	955	930	6 12	25	45	0.36	0	83.7
23	19 19	1014	983	12 3	31	13 48	695	666	9 25	29	9 30	952	944	13 39	8	19 27	0.12	0	83·7 83·7
24	22 55	1032	993	11 53	39	14 I	700	668	9 35	32	22 40	948	936 861	12 O 24 O	135	746	6.00	2	83.8
25	21 41	1093	897	23 59	196	21 21	726	592	23 14	134	21 9	990	801	24 0	100]	
26	20 36	1094	890	0 6	204	11 25	720	603	3 19	117	20 29	961	846	2 27	115	685	5.21	2	83.7
27	22 23	1090	934	20 9	156	12 59	710	570	20 17	140	18 31	1004	908	23 10	96	532	4·27 1·63	2	83·7 83·7
28	17 58	1032	958	17 34	74	12 54	709	599	17 42	110	17 45	985	933	O I	52	203		ļ	
Mean		1034	972		62		704	645	_	59_		961	933		28	124		0.24	83.9
No. of								_				-0	28		28	28	l	28	28
Days		28	28	_	28		28	28		28	_	28	28	-	1 20			1	l
used	<u> </u>			·	<u></u>		<u> </u>		<u> </u>	<u>!</u>	<u> </u>	-	' -	1	<u></u>				

[§] For explanation see page 105. Q denotes an "International Quiet Day," while D denotes a disturbed day used for the computation of Tables 271-276.

1011 1014

1006 1008

Mean†

TERRESTRIAL MAGNETIC FORCE: NORTH COMPONENT. Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

219.	Esko	lalem	uir.	(X .)	1/2		,) U. PU	., , , , , ,	o j				a a	•••	•	•							Ma	arch,	1923.
) . [-]	23	01	1.	۱ ۵	1	(12	<i>'</i>				I	5,000 j	ν (·15 C.	G.S. u	nit) +	-	<u> </u>									
Hour G.M.T.	0.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day	Y	γ	γ	y	Y	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	ν	γ	ν	γ	γ	ν ,	γ	Y	ν	γ	γ
ĭ	1003	997	998	999	998		1002	999	997	1002	992	992	992	991	994	996	994	997	1001		998	997	1006	1000	1007	998
2	1007	999	999	999	1003		1003	1007	1006	1002	997	988	988	989	989	989	993	993	1000		999	1006	1006	1004	1006	999
3	1006	1007	1006	1002	1002		1007	1008	1011	1002	997	994	993	997	998	992	988	992		1000 1006	1002	1004	1006	999	1003	1001
4	1003	1002	1001	997	1004			1016	1010	1006	1000	995	993	994	993	993	995	997		1006	1	1006	1	1016	1010	1005
5	1004	1004	1004	1004	1006	1008	1007	1007	1008	1003	1002	1002	1002	1002	1002	1002	1002	1002	1005	1000	1000	1000	1007	1010	1010	1005
6	1009	1006		1006		1		1010	1007	1004	999	996	993	996		1006	1008	1008 979	1011		1010	1010	1010	1007	1007	1006
7	1007	1006	1006	1006			1015	1015	1014	1001	998	995	990 991	992 994	999	997		1002		1005	1 77	1006	1	1005	1006	1003
8Q	1		1	1006	1005		1006	1007	1000	1000	995	996	993	994	997	1001	1004	1006	1007		1011	1	1011	1011	1011	1006
9Q	1	1005	1005	1007	1	1	T	1016	1013	1008	1001	996	995	999							1011		1012	1015	1011	1007
10Q	1011	1009	1008	1007	1010	1010	1013	1010	1013	1000	1001	990	990	333	1	1200	3		,		}			"	1	· '
110	TOTT	1011	1011	1012	1016	1016	1020	1021	1017	1016	1010	1001	996	993	995	1000	1001	1010	1010	1011	1011	1011	1014	1012	1012	1009
112		1014	1014	1011	1010		1010	1015	1015	1010	1006	1001	999	1001	1000	1006	1011	1012	1012	1016	1016	1011	1011	1007	1011	1010
13	1011	1007	1007	1008	1010			1011	1007	1001	1000	995	989	986	983	991	1001	1006	1010	1011	1012	1	1011	1011	1011	1004
14	1	1000	1006	1006	1009	1011	1015	1015	1010	1004	995	985	987	989	997	1001	1005	1010	1010		1028	1024		1043	1009	1008
15D	1009	1008	1011	1014	1018	1020	1025	1011	1014	1004	998	987	987	990	991	1002	999	1000	1005	1008	1015	1015	1010	1030	1023	1007
	-	ł	l					ĺ			1 _	_										0				
16	1023	1005	1005	1009			1000	1009	1002	993	982	976	982	970	981	998	, , , ,	1004				1028		, ,	1021	1002
17	1021	1020	1005	l .			1011	1014	990	995	994	987	985	990	995	999	1000	1005	1009	1005	1010	1006	1010	1010	1006	1003
18	1 .	1009	1009	1010	1011		1010	1014	1002	987	978	970	971	980	988	1000	1009	1006	1006				1010	1010	1000	1000
19	1006	1011	1009	1004	1001			1015	1005	996	984	966	964	973 989	987 1000	1000		1016	1012		1020	1	1010	1011	1009	1005
20	1009	1009	1009	1009	1010	1011	1012	1011	1007	991	978	977	979	909	1000	1007	1013	1010	1012	1010	1020	1025	1010	1011	1009	1005
			7000	1010	1010	TOTT	1014	1014	1010	1000	990	976	970	970	980	986	989	992	998	994	995	998	992	998	1004	997
21	1009	1006	1006		1008	1010		1006	1005	997	985	976	97I	971	976	985		1001	1008		1010			1010	1010	999
22	1010	1010	1010	1	1010	1 2	31		1010	1000	986	980	977	980	986	998	1005	1009	1010	1010	1011	1014	1015	1015	1015	1004
23Q 24D	1015		1015		1010	1017			1011	1004	961	951	946	957	971	1009	996	1034	1010	946	979	995	1010	980	1000	995
25D	1000	946	985	936	960	972		951	961	970	966	957	956	961	975	985	991	991	995	1014	1002	998	1000	1002	995	976
1 232	1.000	940	روو	353	1	1	1)J-	<i>J</i> - ··	<i>''</i>		-5.								1	Ì					
26D	995	1000	986	980	983	980	993	985	961	942	951	960	961	951	965	1000	1002	991	1000	1.	1005	1 222	1010	995	995	984
27D	995	976	984	990	990	977		995	986	975	955	947	951	966	976	982	990	1000	997		995		1005	1001	1001	984
28	1001	998	1000	991	1000	1001		988	992	984	947	961	972	976	990	992	995	1000	1012	F		, ,	1020	1010	1000	994
29	1000	1014	998	1001	1000	1002		1000	995	985	975	976	979	984	984	1000	997	996	1001		1008		1018	996	998	997 998
30	998	1000	1000	1000	1000	1010	1015	1006	997	990	980	984	985	985	988	988	996	996	1003	1005	1008	1006	1005	1002	1002	990

TERRESTRIAL MAGNETIC FORCE: WEST COMPONENT.

March, 1923.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time. Eskdalemuir. (-Y.)220.

				<u> </u>	<u> </u>					4.	,000 γ	(.04 (C.G.S. ur	$\frac{1}{1}$ $\frac{1}{1}$												
Hour G.M.T.	О.	ı.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day. 1 2 3 4 5	γ. 649 672 673 662 668	γ 667 674 672 667 662	γ 667 676 673 666 667	9 671 673 672 666 662	9 671 669 671 667 666	γ 670 668 672 657 666	γ 668 671 673 662 668	γ 667 672 673 668 673	γ 668 668 672 671 673	γ 673 666 669 671 673	γ 668 672 673 673 674	7 672 682 683 686 677	γ 682 688 693 691 684	γ 693 694 700 697 689	9 691 693 703 695 688	9 693 689 698 694 687	γ 684 686 689 692 682	678 669 685 684 679	γ 677 677 683 682 677	9 674 671 681 683 677	9 672 673 677 678 682	661 675 668 677 674	9 667 675 667 673 677	667 672 661 666 661	672 673 662 668 667	9 673 676 678 676 674
6	667	673	672	672	672	672	668	670	672	670	668	677	684	690	690	687	679	677	679	679	679	680	677	673	672	676
7	672	671	672	671	671	669	669	673	674	673	676	692	705	714	717	715	709	699	682	672	657	676	677	676	673	683
8 Q	673	672	674	672	672	673	672	672	668	667	668	675	687	689	688	683	677	677	678	678	677	677	676	673	673	676
9 Q	673	672	672	672	672	671	673	676	675	673	674	682	689	693	693	691	683	679	678	679	679	678	677	677	676	678
10 Q	676	675	673	674	677	675	678	674	670	668	671	677	688	699	694	688	682	678	681	682	681	677	677	677	677	679
11 Q	677	677	677	678	677	674	673	673	670	669	672	677	687	691	689	690	682	677	678	678	679	679	679	677	677	678
12	677	677	672	669	671	673	678	677	673	671	672	678	688	694	693	689	686	682	682	683	683	681	674	664	666	678
13	666	672	672	673	671	672	671	671	667	665	668	682	692	699	698	692	683	676	677	677	674	677	677	677	674	677
14	674	676	675	672	673	673	672	672	667	660	668	677	693	693	690	687	682	682	689	693	691	689	661	629	657	676
15 D	657	671	679	672	669	672	673	677	673	671	678	683	694	698	694	695	692	680	677	673	682	677	668	660	677	678
16	677	678	678	677	677	676	684	676	666	658	672	680	701	689	693	689	683	677	674	674	665	655	656	671	661	676
17	661	666	651	666	667	671	672	673	678	682	672	685	691	696	690	684	677	676	677	677	676	670	670	672	675	675
18	675	672	672	674	675	677	683	667	661	652	657	672	686	695	699	694	687	678	669	674	673	673	646	662	666	674
19	666	673	671	668	686	674	672	671	664	663	669	679	694	704	704	693	683	677	677	676	674	677	677	677	676	678
20	676	677	677	677	677	676	671	663	657	657	662	676	685	693	695	689	683	677	677	682	684	648	668	668	673	675
21	673	673	673	672	671	671	668	667	662	663	669	675	693	703	7°4	700	700	690	683	679	667	662	645	651	645	675
22	645	642	649	656	662	661	662	661	661	661	673	682	692	698	698	692	683	677	674	676	676	676	676	677	677	672
23 Q	677	676	676	676	673	672	670	662	656	655	660	673	688	698	699	693	684	677	677	677	677	677	677	678	677	676
24 D	677	677	677	677	674	671	668	662	656	656	676	698	718	753	732	741	762	756	613	635	652	609	607	579	603	675
25 D	603	609	625	582	623	645	655	657	672	666	668	675	683	693	683	690	694	687	673	677	663	673	677	677	683	662
26 D	683	669	683	678	672	668	661	655	652	658	665	672	689	694	703	694	678	681	673	651	657	660	660	661	675	671
27 D	675	690	677	667	665	684	673	666	661	660	666	677	698	694	702	699	689	661	668	672	666	666	668	688	670	676
28	670	662	657	656	660	664	660	662	658	656	661	678	698	698	699	687	683	674	654	668	672	667	653	671	667	669
29	667	687	662	673	662	660	657	655	649	650	659	677	693	699	693	690	683	668	667	672	672	666	652	655	666	669
30	666	662	666	661	660	660	655	655	654	658	672	682	688	693	695	684	677	674	672	669	671	671	666	663	661	670
Mean †	661	672 670	657 669	657 668	661	661	661	658 667	656 665	658 664	661	678 679	689	698 698	694 697	691	683	673 681	674	672 674	672	671 670	666	668	662	670

[†] Mean of 29 days; 4th and 5th omitted. Q denotes an "International Quiet Day," while D denotes a disturbed day used for the computation of Tables 271-276.

BBULLO B 1923 033 01

948

948

23 Q

26 D

27 D 28

Mean †

TERRESTRIAL MAGNETIC FORCE: VERTICAL COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

221. Eskdalemuir. (Z.)March, 1923. 44,000 γ (·44 C.G.S. unit) + 18. 8. Noon. 16. 21. 22. Mean. 6. IÒ, 15. 17. 20. 23. 3. 4. 5. 7. g. 13. 14. 10. G.M.T Day. 95I 8 Q 958 Q51 ro Q 948 948 948 946 948 15 D 948 94 I 18

94 I

958

948

962

DAILY EXTREMES OF EACH COMPONENT OF TERRESTRIAL MAGNETIC FORCE: MAGNETIC CHARACTER FIGURES: TEMPERATURE IN MAGNET HOUSE.

222.	Eskdale															I Cha	racter	1	h, 1923.
							Terrestr	ial Magne	tic Force.								ures.§	Magnetic Character	Temperatur in
Day.	Maxir		h Compo	nent.	1	Maxir		t Compo	nent.		Maxii		ical Com	ponent. nimum	T	ΣRª	ρ	of Day (0-2).	Magnet House
	15,000			000γ+	Range.	4,000			οοογ+	Range.	44,000			οοο γ +	Range.		·		200 +.
	h. m.	ν ,	γ	h. m.	γ	h. m.	γ	Y	h. m.	Y	h. m.	γ	γ	h. m.	γ	100γ2	- 0		a.
I	22 13	1018	986	13 11	32	12 50	703	640	0 7	63	16 35	959	944	O I	15	52	0.28	0	83.7
2	0 10	1013	982	16 34	31	14 9 14 8	695	662	16 58	33	16 50	957	942	13 12	15	23	0.12	0	83.7
3	21 32	1014	982 986	15 38	32		705	651	22 43	54	22 42	957	941	12 3		42	0.55	0	83.7
4	6 52	1018		11 41	3 ² 19	13 32	699	655	3 2	44 38	70 0			70.00	-		0.70	0	84.1
5	22 48	1017	998	12 33	19	13 11	693	655	23 0	30	19 0	951	941	13 20	10	19	0.10	0	83.7
6	19 5	1016	991	12 3	25	13 22	693	666	O I	27	_		939	12 5	_		_	0	83.7
7	7 0	1016	967	17 10	49	14 25	725	652	19 52	73 26	20 0	974	934	12 11	40	93	0.20	1	83.7
8	20 40	1011	991	10 47	20	13 43	692	666	8 55		16 20	967	947	11 15	20	15	0.08	0	83.7
9	20 35	1014	986	12 44	28	13 10	695	667	3 33	28	16 45	955	946	13 30	9	16	0.09	0	83.9
IO	6 38	1017	991	12 26	26	13 4	703	666	8 31	37	16 40	951	938	11 50	13	22	0.13	0	83.9
11	6 8	1021	991	13 50	30	13 34	698	666	8 11	32	17 30	951	931	12 25	20	23	0.12	o	83.9
12	18 38	1019	995	12 23	24	13 50	700	660	22 40	40	22 55	951	939	12 30	12	23	0.15	O	83.9
13	18 28	1016	980	14 7	36	12 33	708	661	7 55	47	17 0	950	928	12 33	22	40	0.31	0	83.7
14	23 7	1055	982	11 4	73	12 52	699	622	23 3	77	22 35	959	932	11 30	27	120	0.64	I	83.5
15	23 10	1054	980	13 10	74	15 31	710	640	22 32	70	18 40	951	930	24 0	21	108	o·58	I	83.6
16	23 32	1043	959	12 54	84	12 26	705	646	21 42	59	16 30	959	929	0 10	30	114	o·61	I	83.5
17	22 18	1034	980	10 50	54	13 26	700	642	2 19	58	21 10	953	924	1 16	29	7I	o·38	I	83.7
18	21 55	1043	965	10 55	78	14 38	704	629	21 50	75	18 2	957	935	11 28	22	122	0.65	I	83.7
19	7 12	1018	961	11 12	57	13 19	709	661	9 10	48	17 O	956	937	12 30	19	59	0.35	0	83.7
20	20 59	1049	975	10 46	74	14 3	699	635	21 2	64	21 30	951	933	12 10	18	99	0.23	I	83.8
21	6 30	1015	962	12 33	53	14 56	709	635	24 0	74	19 48	970	939	12 5	31	92	0.49	0	83.7
22	2 40	1015	966	13 20	49	13 10	700	630	o 6	70	16 32	960	936	11 30	24	7 9	0.42	0	83.7
23	21 40	1018	975	11 49	43	14 12	702	652	8 28	50	17 33	953	935	12 30	18	47	0.25	0	83.8
24	21 26	1141	917	18 44	224	17 10	848	479	21 25	369	17 21	1104	876	21 45	228	2383	12.72	2	83.8
25	18 26	1058	896	2 33	162	12 32	715	517	2 42	198	18 19	988	812	3 24	176	964	5.12	2	83.9
26	15 16	1052	932	8 44	120	14 47	725	635	18 48	90	15 30	1002	924	3 50	78	286	1.53	2	83.9
27	17 10	1015	941	10 43	74	14 10	708	645	17 4	63	17 12	994	916	1 28	78	155	0.83	r	83.8
28	21 50	1041	930	10 11	III	12 18	703	645	22 10	58	17 50	964	924	0 1	40	173	0.92	I	83.7
29	21 37	1031	971	9 47	60	13 17	706	641	22 9	65	17 20	965	936	1 25	29	87	0.46	1	83.7
30	5 32	1019	976	9 52	43	13 49	699	651	8 43	48	16 o	963	941	II 20	22	46	0.25	0	83.7
31	0 27	1030	976	11 10	_ 54_	0 28	699	651	8 30	_48	17 19	959	932	12 0	_ 27_	59	0.32	0	83.6
Iean		1030	970		6o		_708	639		69		967	929		38	187		0.52	83.7
No. of		27	21		31		27	27				20	•••		20			o.r	
Days used.		31	31		3.		31	. 31	_	31		29	30		29	29	_	31	31

^{*} No trace; lights not adjusted. † Mean of 29 days; 4th and 5th omitted. § For Q denotes an "International Quiet Day," while D denotes a disturbed day used for the computation of Tables 271-276. § For explanation see page 105.

TERRESTRIAL MAGNETIC FORCE: NORTH COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

223. Eskdalemuir. (X.)

Table 1 (Are C.C.S. unit)

April, 1923.

	3	041	,			15	. 5				15,00	00 γ (·	15 C.G.S	. unit)	+											
Hour G.M.T.	0.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day.	γ 1000	γ 1006	γ 1005	γ 1004	γ 1000	γ 1009	γ 1014	γ 1015	γ 1006	γ 995	γ 984	γ 983	γ 985	γ 990	γ 992	γ 998	γ 1000	γ 1000				γ 1015	γ 1014		γ 1009	γ 1003
20	1009			1005		1010			1000	986	979	977	980	984	992	1000		1010				!	1018	1	1016	1003
3~	1016	1015	1019				1019			990	977	971	974	978	990	996	1005	1005	1006		1015			1014	1011	1004
4	1011	1010	1010	1014	1015	1016	1016	1015	1008	996	979	967	970	976	986	995	994	1011	1011	1010	1014	1013	1015	1014	1011	
5 Q	1011	1011	1011	1014	1015	8101	1017	1014	1008	997	985	977	980	985	995	1005	1009	1005	1006	1013	1013			1011		1005
1 6 %	i		1	1011			1016		1016	1011	997	981	972	976	985	992	998	1011	1016					1015		1006
7			1	1021			1023		1015	1001	990	981	977	978	987	992	, .				1011				1012	1007
8	1012	1016	1019	-		1011			1006	1000	991	988	989	992	994	1001	,	1	1010		1018		1017	1017	1021	1003
9		1020		1010		1017		1016		992	981	981	981 981	987 991	990	1001	998	1010			1029			1021	1	1013
10	1010	1011	1012	1015	1010	1019	1025	1021	1024	1010	991	986	901	991	993	1000	990	1010	1021	1034	,	102,				
11	1050	1015	1014	1019	1021	1023	1023	1021	1016	1001	991	985	981	981	991	998	1003	1013	1021	1016	1017	1018	1041	1029	1019	1011
12 D			1007				1023		1006	1016	1001	985	981	983	991	990	1006	1020	1017			1040		1010	1006	1008
13 D			1006					1	1007	997	986	977	975	987	993	1000					1020			1025		1005
14	998	1029	1011	986		1010			1005	992	982	981	977	986	991	993		1015			1015		1016	1016	1025	1005
15	1026	1011	1012	1013	1013	1016	1018	1011	1007	998	983	978	979	979	900	993	999	1010	1017	1010	1022	1010	1020	1010	1010	2000
-6	1016	1013	1013	TOTA	1013	TOTE	1016	1016	1008	997	982	974	974	978	988	1004	1015	1021	1025	1024	1025	1022	1022	1021	1019	1008
16 17 Q			1019			1022			1012	994	971	966	964	979	992	1002		1020			1019	1 -	1	1019	1017	1008
18							1022		1014	998	978	977	985	992	1002			1011					1022	1022	1020	IOII
19	1020	1018	1016			1019		1	1008	993	978	977	982	993			1018	1019	1021	1022				1025	1025	1011 1013
20	1025	1020	1019	1018	1018	1024	1024	1023	1016	1011	981	968	986	998	1008	1005	1018	1031	1019	1010	1021	1020	1025	1017	1019	1010
T				7020	000	1012	1022	1008	997	972	982	970	959	961	993	984	994	1010	1023	1028	1014	1028	1018	1007	1018	1002
21 D 22 D		1019		1004		1006		1001	986	982	969	955	964	977	993	997	1007		1022		1022	1015	1012	1026	1024	1004
23D	l .		IOII			1011		1	1005	997	988	985	981	998		1003	1015	1025			1020	1 -	1 -		1021	1009
24	1 -	1035	1015	, -		1014	1009	996	994	995	972	969	982	989	990	997	999		1023				1013	1012	1017	1005
25	1017	1014	1013	1016	1001	1016	1015	1011	1009	1001	992	993	992	993	999	1001	1006	1009	1017	1018	1016	1015	1010	1022	1025	1009
1									T005	008	988	983	987	997	1002	1004	1012	1016	1015	1022	1020	1017	1015	1014	1015	1008
26 Q			1009		1010				1005	998	989	987	990	997		1011		1021	1024		1020			1011	1017	1009
27 Q	1015		1013						1006	1001	991	982	984	987	996	1003	1011	1018	1021	1023	1021	, ,	1016	1	1015	1008
29			1012			1014			1011	1001	987	979	985	991	I			1021			1027			1021	1019	1011
30	1019	1018	1017		1019	1020		1019	1009	996	985	981	986	991	999	1007	<u> </u>	1019			1025	·	1021		1022	1012
Meant	1017	1016	1013	IOII	1012	1015	1017	1014	1007	997	984	978	979	985	994	1000	1006	1015	1017	1020	1019	1021	1021	1018	1018	1007
1	'	l		1		1	•									1	ļ	1		!	1	1.	<u> </u>			

TERRESTRIAL MAGNETIC FORCE: WEST COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

224. Eskdalemuir. (-Y.)

4,000 y (.04 C.G.S. unit) +

April, 1923.

											4,000	ο γ (.ο	4 C.G.S.	unitj	+											 1
Hour G.M.T.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day. 1 2 Q 3 4 5 Q	γ 662 668 663 673 673	γ 665 667 667 672 672	γ 662 665 667 672 671	9 665 667 667 671 671	γ 667 671 668 668 672	9 672 664 669 666 672	γ 667 662 668 662 668	9 661 657 659 656 661	γ 651 651 651 646 652	γ 646 650 646 645 652	9 654 661 651 656 657	γ 670 673 667 667 665	9 689 688 686 678 682	γ 702 698 693 693 691	7 703 697 700 703 692	γ 694 689 697 703 688	9 688 684 692 690 687	7 678 681 683 688 683	673 677 677 677 677 683	9 667 677 673 675 681	γ 665 677 673 677 677	661 672 677 668 675	668 673 677 677 673	671 666 673 677 672	9 668 663 673 673 671	7 671 672 673 673 674
6 7 8 9 10	671 671 666 651 672	671 659 659 645 671	671 656 646 657 669	671 649 661 661 667	669 651 663 661 667	668 661 665 661 667	665 666 663 661 667	658 662 660 651 661	651 655 656 642 654	651 655 656 646 647	655 661 661 661 652	661 671 672 673 667	673 688 685 686 684	687 699 695 695 700	692 701 695 695 698	689 694 693 694 699	687 695 690 686 687	683 689 689 684 684	681 683 677 684 685	673 677 677 673 689	673 667 680 646 674	673 671 679 649 668	677 661 672 645 657	676 661 652 665 656	671 666 651 672 656	672 671 671 666 672
11 12 D 13 D 14 15	656 663 666 640 677	652 667 681 656 672	665 662 681 645 667	667 688 673 678 667	667 673 677 681 667	667 675 672 663 666	666 673 666 660 657	662 666 657 652 652	665 662 645 645 645	661 652 645 645 642	665 662 657 652 646	683 671 672 671 660	695 688 681 684 679	701 699 694 705 694	702 705 703 709 695	694 694 700 701 693	688 699 688 693 687	682 668 678 684 682	683 672 673 677 677	678 672 671 670 672	677 661 668 657 663	673 666 667 656 665	656 651 634 667 667	676 661 603 672 671	663 666 640 677 670	674 673 668 670 669
16 17 Q 18 19 20	670 672 670 668 662	671 672 671 670 663	671 671 671 671 665	671 671 671 676 663	667 671 670 670 663	667 668 668 666 671	665 670 665 661 670	657 660 654 652 660	646 650 646 641 649	641 646 639 639 647	645 649 645 652 651	661 667 661 676 673	684 686 687 693 693	702 699 699 703 706	705 698 700 701 707	700 689 697 691 695	693 684 689 683 691	683 679 679 677 689	677 677 675 674 675	673 673 675 675 668	674 673 674 675 660	675 670 673 674 660	673 669 665 672 661	673 669 667 663 655	672 670 668 662 667	673 672 671 672 671
21 D 22 D 23 D 24 25	666 672 660 666 669	664 648 640 666 661	664 661 618 652 658	646 665 619 656 654	644 654 653 664 660	678 677 660 658 658	650 658 650 659 654	642 645 648 658 656	638 645 645 655 659	642 639 647 651 660	645 646 655 652 666	662 666 667 667 670	680 688 682 683 676	692 701 698 696 684	706 701 698 695 684	697 694 693 688 680	685 680 681 679 676	682 671 690 674 674	678 676 662 675 675	680 661 656 673 673	657 651 668 666 670	645 650 669 656 670	656 634 662 667 671	674 656 669 666 672	672 660 666 669 664	666 664 662 668 668
26 Q 27 Q 28 29 30	664 667 666 666 656	661 667 662 667 664	661 665 659 661 662	660 664 654 656 661	659 661 650 655 656	659 657 646 651 655	656 654 646 650 650	654 651 645 644 648	650 648 644 641 644	646 649 648 644 648	655 661 658 656 662	666 671 668 670 679	677 682 680 684 692	685 686 688 690 694	684 685 690 688 692 698	679 683 685 682 686	680 677 680 675 682 686	679 676 680 673 681	675 675 679 670 678	670 672 673 670 675 673	672 672 672 671 670 668	672 672 667 669 667	671 672 665 648 668	669 670 669 651 669	667 666 666 656 673 666	667 668 666 664 669 670
Meant	665	664	662	664	665	666	662	655	649	647	655	669	685	696	080	693	000	001	0//	0/3	1	'		<u> </u>		

j Mean of 28 days; 27th and 28th omitted. Q denotes an "International Quiet Day," while D denotes a disturbed day used for the computation of Tables 271-276. B 1923 043 0 TERRESTRIAL MAGNETIC FORCE: VERTICAL COMPONENT.

Mean values for periods of circle minutes.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

225. Eskdalemuir. (Z.)

April, 1923.

April, 1923.

										44,00	ογ(·44 C.	G.S. uni	t) +												
Hour G.M.T.	o.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day.	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ
1 2 Q	952 953	952 953	951 953	949 953	948 950	948 950	948 952	952 953	955 953	956 950	952 943	944 942	941 942	942 942	94 5 949	952 953	955 953	955 953	953 953	952 953	954 953	953 952	952 952	952 953	952 952	951 951
3	952	952	950	949	949	949	949	952	953	950	945	942	942	945	949	953	954	955	957	955	953	950	950	949	949	950
5 Q	949 952	953 954	953 954	952 953	950 951	949 950	951 952	953 954	949 950	945 946	941 942	941 939	942 935	942 935	942 938	950 944	954 949	953 952	954 951	957 950	953 950	953 950	952 950	950 950	951 950	950 948
6	950	950	950	950	950	950	950	953	949	943	939	935	933	930	934	941	945	947	950	952	952	950	950	950	945	946
8	946 952	943 951	940 946	939 947	939 948	939 951	940 951	943 951	944 948	943 943	940 940	935 939	934 937	935 940	942 946	947 948	951 950	955 951	963 956	964 956	965 955	963 951	959 955	955 953	952 944	947 948
9	944	943	940	946	947	948	948	951	949	947	940	939	939	939	944	949	951	951	952	956	959	952	947	947	948	947
IO	949	952	952	952	952	951	952	952	951	948	944	940	936	936	943	948	952	951	950	949	953	956	952	948	925	948
11 12 D	926	936	942	945	945	945	946	949	948	945	945	939	938	942	945	946	948	950	950	953 962	953 960	956	950	935	940	945
13 D	941 950	946 946	945	932	934 939	9 <u>3</u> 8 943	942 947	947 951	948 951	947 950	946	944 941	943, 942	948 939	952	947	965 950	973 956	970 957	957	956	947 954	946	946	950 929	949 947
14 15	930	908	919	923	927 948	939	945	948	951	951	948	940	935	935	941	948	951	955	956	1	956	957	953	951 951	947 951	943
	947	943	944	947	-	951	951	955	954	952	950	944	943	944		954	955	955	955		955	954	951			950
16 17 Q	951 951	951 951	951	951 951	951	951 950	951 951	954 952	954 952	950 948	944 944	936	932 936	934 937	939	945 952	948	951 955	952 952	952 952	951 952	951 951	951 951	951 951	951 951	948 949
18	951	951	951	951	951	951	951	953	951	948	943	935	927	930	936	943	950	955	955	954	952	952	951	950	949	948
19 20	949	948	949	948	948	951 946	952 944	954 944	955 946	950 947	940	935	933 928	937 929	944	950	951	952 954	952 965		950 975	950	949	948	947	948 950
		ĺ	}	1		1			}				-	l `	1]						-	-		
21 D 22 D	957	955 928	950	930 941	934	926	935 935	946	950 948	955 948	948	941	933 938	933	942	957 952	959	960	958 971	956 964	963	959	954	948	929 894	947 944
23 D	894	895	902	910	920	926	934	939	944	943	940	937	934	939	948	953	959	960	970	970	960	952	952	947	938	940
24 25	939 951	929 949	929	936	940	942	945 944	948	948	945 944	943	945	940 933	938 933	946	953	957 950	959	961	960 955	960	954 954	951	952 951	951 946	947 946
26.0	046	<u> </u>	948			1												052			960	959	956	956	956	951
26 Q 27 Q	946 956	945 955	955	949 955	952 956	952 956	952 955	952 956	949 956	945 953	946	945	943	942	947	950	951	952	955	959 —		-	l —	950	95°	951
28 29	954	954	954	954	954	954	 954	954	954	951	945	945 945	949 945	940 946	946	950 955	952 957	952 957	955 957	956 957	956 956	956 956	956 955	954 950	9 53 9 4 9	953
30	934	954	951	954	954	954	954	954	954 952	950	945	935	945	933	939	933	949	950	957	952	952	952	953	953	952	948
Mean†	945	944	945	945	945	946	947	950	950	948	944	940	937	938	944	949	953	955	956	956	956	953	951	949	945	948
<u> </u>		<u></u>	1		1	<u></u>		·	<u> </u>		<u> </u>	<u> </u>	1	<u> </u>	1		<u>'</u>	<u>'</u>	!	<u>, </u>	1			1	1	1

DAILY EXTREMES OF EACH COMPONENT OF TERRESTRIAL MAGNETIC FORCE

CHARACTER RATIOS: MAGNETIC CHARACTER FIGURES: TEMPERATURE IN MAGNET HOUSE. 226. Eskdalemuir.

	1	ŝ		·			Terresti	rial Magn	etic Force.		· · · · · · · · · · · · · · · · · · ·					Char Figu		Magnetic	Temperature in
Day.		Nort	h Compo	nent.			Wes	t Compo	nent.		1	Verti	cal Comp	onent.			1	Character of Day	Magnet
	Maxin 15,000			nimum 200γ+	Range.	Maxin			nimum οογ+	Range.	Maxir 44,000			nimum 100γ+	Range.	ΣR	ρ	(0-2).	House 200 +.
	h. m.	γ	γ	h. m.	γ	h. m.	γ	γ,	h. m.	γ	h. m.	ν -	γ γ	h. m.	- Y	$100\gamma^2$			a.
1	20 26	1028	981	10 50	47	13 50	704	645	9 12	59	16 35	956	940	12 20	16	59	0.50	0	83.7
2	22 10	1025	976	10 23	49	12 56	699	646	8 43	53	15 58	954	941	12 50	13	54	o·46	0	83.7
3	2 54	1023	967	11 20	56	14 22	703	645	8 52	58	18 o	957	941	11 28	16	68	0.57	0	83.6
4	17 11	1020	960	11 10	60	14 25	709	643	8 54	66	18 31	957	940	10 50	17	82	0.70	0	83.7
5	5 30	1019	975	II O	44	14 0	693	651	8 36	42	7 0	954	934	12 40	20	41	0.35	0	83.7
6	23 58	1035	971	12 33	64	14 20	694	650	8 42	44	19 32	954	930	13 0	24	66	0.56	0	83.7
7	0 12	1035	972	12 28	63	13 58	706	645	2 48	61	18 30	966	932	12 30	34	88	0.75	I	83.7
8	23 32 20 6	1035	986 972	11 20 12 16	49 72	13 38 14 30	699	636 634	2 10 20 26	66	18 40 19 50	959	937	11 38 11 13	22 25	69 102	o·58 o·86	I I	83·7 83·7
10	23 48	1044	972	12 10	107	13 36	700 705	644	22 41	61	20 42	957	937 921	24 0	36	165	1.39	ī	83.7
						1			1				_			ľ		_	0
11	22 I4 20 54	1087 1064	968 971	12 13	93	13 23 14 18	708 719	630 645	22 30 9 10	78 74	21 38 17 23	957 976	922 930	0 I 3 IO	35 46	215 162	1·82 1·37	I	83·7 83·7
13	22 7	1059	959	11 50	100	14 41	710	585	22 38	125	18 11	958	930	24 0	28	264	2.24	ī	83.7
14	0 55	1044	970	11 26	74 68	13 43	714	635	0 1	79	20 31	959	904	i o	55 13	147	1.25	I	83.7
15	o 16	1041	973	11 21	68	13 20	699	640	8 45	59	15 50	955	942	0 30	13	83	0.70	٥	83.6
16	18 30	1027	969	11 45	58	13 50	709	636	9 30	73	7 30	955	931	12 10	24	93	0.78	0	83.6
17	22 18	1027	959	11 35	68	13 8	702	643	9 27	59	16 50	955	935	12 30	20	85	0.72	0	83.6
18	20 6 22 23	1029	973 973	10 30 10 40	56 61	14 13 13 12	704 704	635 635	9 27 8 41	69	17 5 8 0	956 955	926 933	12 10	30	88 90	0·74 0·76	0	83·6 83·6
20	20 49	1037	960	10 32	77	13 45	7º4 7º5	639	22 56	76	19 18	978	933	12 10	51	143	1.21	ī	83.6
21	20 38	1047	948	12 40	00	74.00	MIA	6	0		0	-60			l l		0.00		83.6
21	18 48	1047	948 944	11 30	99 130	14 22 23 33	719 711	610	3 28 21 34	109	20 28 18 30	968 974	924 892	5 IO 24 O	44 82	236 321	2.00	I 2	83.2
23	18 42	1050	974	12 8	76	13 13	708	610	I 42	98	18 20	976	892	0 I	84	224	1.90	I	83.5
24	20 48	1067	957	10 24	110 41	13 10	700	625	20 40	75	18 o	962	926	1 17	36	190	1.61	1	83.6
25	23 15	1028	987	9 53	-21	12 38	688	646	3 20	42	19 50	956	932	12 18	24	40	0.34	0	83.2
26	0 20	1026	981	11 12	45	13 15	687	645	8 45	42	19 20	961	941	12 43	20	42	0.35	0	83.7
27 28	18 42	1030 1026	986 981	10 33 11 34	44	13 37	689	646	8 43	43					1 - 1	-		0	83.7
29	20 22 21 50	1052	977	11 34 10 53	45 75	13 55 13 9	692 693	643 638	7 52 22 18	49 55	21 20 21 35	958	937	12 20 12 20	13	49 88	0.41	0	83·7 83·7
30	19 20	1035	976	10 57	_59_	13 2	697	641	8 33	56	19 40	957 953	944 929	12 15	24	72	0.61	o	83.7
Mean.		1041	971		70		703	636		67		960	929		31	118		0.47	83.7
No. of															<u> </u>				
Days used		30	30		30		30	30		30		29	29		29	29		30	30
uscu					<u>' </u>								1	1	1 1	l	l	J	1

^{*} No trace; lights out of adjustment. † Mean of 28 days; 27th and 28th omitted. Q denotes an "International Quiet Day," while D denotes a disturbed day used for the computation of Tables 271-276.

TERRESTRIAL MAGNETIC FORCE: NORTH COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

227.	Esko	ialem	uir.	(X .)			,	-		•	15,0	οογ(·15 C.G.	S. uni	t) +								·		May,	1923.
Hour G.M.T.	О.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day.	Y	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	- Y	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ
I Q	1022	1023		1016	1017		1021		1024	1017	1007	997	996	1000	1003	1009	1020	l .	1018		1030	1028	1029	1026	1025	1017
2	1025	1026	1025	1021	1021	1022	1022	I .	1012	1001	990	987	992	1002	1011		1019	1020	1022			1024	1022	1022	1022	1015
3 D	1021	1020	1021	1020	1020	1021	-		1012	1001	1000	996	1002	1009	1014	1020	1014	1031	1037	1027		1024	1025		1029	1013
4	1015	1	,	1016	-	1010			1006	995	992	995	998	1003	1005	1004	1015	1016			1			-	1013	1010
5	1029	1015	1002	1007	1015	1015	1015	1008	1001	1001	995	990	989	993	1002	1002	1007	1020	102/	1023	1033	1023	1015	1015	1013	
6	1013	1015	1015	1014	TOTE	1015	1012	1013	1014	1013	1000	993	1002	1006	1007	1007	1011	1017	1025	1028	1021	1022	1025	1019	1020	1014
7	1020	1015		1017	1016		1018	, ,	1013	1008	1003	998	1002	1005	1005	1011	1014	1019	1030	1032	1033	1033	1036	1037	1031	1018
8	1030			1020		1025		,	1018	1015	1003	994	988	988	1000	999	1005	1008	1025		1029	1028		1039	1023	1016
9	1023	1013		1014	1016		1014		1020	1013	998	994	1002	1002	1000		1013	1019	1026	1	1022	1019		1014	1014	1013
10	1014	1014	1014		1	1018		1019	1023	1014	1004	1002	999	1001	997	1008	1015	1023	1026	1026	1021	1019	1018	1014	1015	1014
	•	l '								1			_	l											1018	1012
11	1015	1018	1019	1018	1018	1015		1	1015	1009	1002	995	998	1000	993	1002	1007			1026	1025	1023	1019	1021	1013	1013
12 Q	1018	1016	1016	1017	1016	1018	1	1010	1009	1006	998	990	992	995	1000	1011	1019	1028	1025		1022	1024	1023	1023	1023	1015
13 Q	1023	1019	1020		1017	1021		1	1006	999	988	988	991	1000	1013		1018	1022	1025			1025	1027	1027	1018	1014
14	1023	1020	1	1023		1025			1010	1001	977	978	986	992	1000	1001	1025	1030	1029	1023	1021	1019	1019	1019	1021	1010
15	1018	1019	1019	1019	1020	1015	1013	1011	1004	999	994	989	982	977	987	1001	1010	1021	1023	1023	1021	1019	1019	1019		
1 -6				7075	1015	7000	1010	1018	1011	1005	993	991	993	1001	1008	1015	1026	1029	1033	1029	1023	1025	1029	1030	1028	1016
16	1021	1020		1015	1017	1020 1032	_	1020	1011	1014	1000	993	995	1004	1018	1039	993	1048	1053			1032	1027	1038	1026	1023
17 D 18 D	1028	1025	į.	1034	1035	989	999	986	974	968	963	983	993	981	1001			1025	1044		1022	1028	1020	1019	1001	1002
19	1000	974		1001	1004	1002		992	983	984	977	972	976	980	987	1003	1017	1030	1035		1038	1018	1017	1015	1026	1004
20	1026	1012	1014			1013			1005	1000	992	983	982	979	996	1000	1013	1025	1041	1028	1018	1016	1023	1019	1025	1009
	1020	1			,		′.						-						}	1					0	
21	1025	1008	1011	1008	1008	1008	1008	1006	1000	993	991	984	987	993	997	1003	1013		1027	, .	1017		1012	1010	1018	1007
22 Q	1018	1004	1004	1005	1007	1004	1003	1001	993	988	979	973	975	983	985	993	1000	1	1026	, -				, ,	1014.	1002
23 ~	1014	1019		1007	1011	1012		1003	995	993	988	988	994	999	1005	1008		1020	1026		1027	•	1016	1013 1016	1009	1010
24 Q	1009	1009	1008	1008	1012	1014			1004	997	984	982	988	1000	1007	1021	1022	1026	1028						1014	1013
25	1014	1013	1017	1014	1021	1021	1019	1018	1022	1015	1002	989	993	993	1003	1013	1017	1019	1021	1025	1020	1010	1017	1010	1011	1013
					7072		TOT 4		T000	7006	TOOC	007	1002	005	994	1003	1016	1023	1030	1027	1023	1018	1018	1018	1018	1012
26	IOII					1017			1009	1006	1000	997 984	983	995 992	1002		1		1013				1019		1017	1010
27	1018		,			1017			1003	998	992	992	995	992	1012	1020		1025	1026					1019	1016	1012
28 20 D	1016		,	1017	1010	1013		1002	997	988	982	981	993		1018	997	1007	1031	1045			1026	1014	3026	1000	1012
29 D 30 D	1000	1016		1017	1019	1020		993	981	973	973	976	978	979	985				1042			1012	1008	1002	1004	1004
301	1000	1.00/	1001	2013	101/	-~-	-010	773		2/3	3,3	,,	"	^′′	- 3											1001
31	1004	1006	996	1002	999	1006	1002	994	983	973	970	977	982	987	997	1003	1009	1017	1018	1021	1022	1022	1023	1017	1010	1001
Mean	1018	1014		1015		1016	1014	1010	1005	1000	991	988	991	995	1002	1008	1014	1023	1029	1027	1024	1022	1020	1022	1018	1012
Mican	12010	1.014	-0.4		1-023												<u>-</u> _			8						

TERRESTRIAL MAGNETIC FORCE: WEST COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

				, ,,		an va	iiues j	or pe	rioas	- ,			centre			urs oj	Gree	nwich	, INI CU	/v 1 v/				A	lay,	1923.
228.	Eskd	alemu	iir.	(-Y.) `-	<i>-</i>	·	<u> </u>			4,0	οο γ ((•04 C.G.	.s. um	··· +										,,,,	
Hour G.M.T.	о.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
Day. 1 Q 2 3 D 4 5	γ 673 667 668 623 640	γ 669 667 667 646 650	γ 665 666 669 655 664	γ 665 665 669 643 675	γ 664 665 666 650 661	γ 661 662 656 652 655	γ 659 659 650 656 653	γ 655 655 644 650 655	γ 654 653 643 651 655	γ 653 652 650 656 654	γ 655 663 655 657 660	γ 661 672 662 668 667	7 672 684 674 680 676	9 684 690 687 688 682	9 688 693 692 686 688	9 683 692 696 682 682	9 684 688 693 687 674	9 679 685 696 684 676	677 681 695 682 677	9 675 676 672 678 668	670 672 655 673 675	671 671 667 669 663	9 670 669 667 655 667	9 668 668 640 654 666	9 667 668 623 640 665	9 669 672 667 664 666
6 7 8 9 10	665 661 664 652 665	665 662 658 654 662	665 669 662 653 661	666 656 667 654 661	664 653 658 656 660	662 652 654 656 660	659 650 654 660 661	657 650 653 662 660	652 654 655 656 655	651 657 660 655 656	656 663 665 656 655	664 672 671 665 660	675 680 681 673 669	680 686 684 676 673	679 684 687 673 671	679 684 684 677 676	675 685 680 680 672	673 689 677 676 669	674 687 679 676 669	672 682 674 674 668	667 677 671 672 665	665 671 672 669 661	658 663 666 668 668	660 660 671 666 667	661 664 652 665 666	666 669 668 665 664
11 12 Q 13 Q 14 15	666 668 673 666 668	666 669 671 668 667	665 667 671 666 667	663 667 666 661 666	661 665 658 659 666	658 659 656 655 650	654 655 644 654 648	650 649 642 650 646	653 649 645 649 646	659 649 648 649 652	667 654 655 656 656	671 665 669 677 667	679 676 682 691 676	681 682 688 697 677	676 678 687 697 682	678 673 678 687 679	677 671 671 673 679	681 672 671 667 676	677 671 675 666 673	673 671 676 666 667	669 669 671 668 665	671 671 671 670 666	671 674 671 672 667	671 672 670 672 666	668 673 666 668 665	668 667 667 668 665
16 17 D 18 D 19 20	665 669 612 650 650	668 665 653 656 662	669 676 661 652 663	664 653 638 644 661	659 641 644 658 660	654 635 644 652 650	650 630 637 650 643	648 631 636 643 634	647 635 639 640 635	645 644 648 641 644	653 654 653 651 647	661 665 666 661 655	672 677 681 672 666	681 683 676 682 673	686 698 683 683 683	685 714 680 682 689	681 692 679 680 692	676 713 680 674 690	676 655 668 676 678	674 665 669 674 675	672 674 668 675 669	674 656 665 666 667	677 639 660 664 659	675 645 648 661 658	669 612 650 650 634	667 662 659 662 662
21 22 Q 23 24 Q 25	634 665 663 656 666	629 660 655 656 660	636 658 654 650 661	644 657 651 649 657	653 654 650 648 653	650 650 649 645 642	650 649 640 643 638	647 644 640 644 639	644 640 635 645 643	643 639 634 653 646	651 644 646 661 654	658 654 659 674 671	664 667 671 679 681	671 677 677 682 685	674 681 681 681 687	678 682 676 681 682	684 678 675 680 681	682 681 676 681 673	682 681 675 680 672	665 676 675 677 676	664 661 671 671 673	661 662 669 671 671	665 662 666 667 671	662 666 660 666 670	665 663 656 666 666	659 662 660 664 665
26 27 28 29 D 30 D	666 668 663 665 661	665 666 666 664 635	662 660 660 664 635	665 657 659 661 631	661 649 659 655 626	654 640 654 651 631	650 644 654 648 630	650 644 650 642 625	649 641 643 641 629	650 637 637 644 641	656 646 646 651 651	662 658 657 671 672	676 672 673 696 688	677 684 676 710 698	677 687 677 718 699	672 682 676 701 700	671 681 673 708 690	673 675 671 709 673	675 672 671 687 675	668 676 673 660 667	667 674 668 665 637	667 671 666 640 652	668 670 669 664 656	669 664 671 676 661	668 663 665 660 667	665 663 663 670 657
31	667	668	666	661	658	651	642	640	638	635	645	663	682	689	693	688	682	674	667	666	666	666	657 665	652 664	654 659	665
Mean	659	660	661	658	656	652	649	646	646	648	654	665	677	683	685	684	681	680	676	672	1 000	1 000	003	004	\J9	

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

229.	Esko	ialem	uir.	(Z.)	IVI	ean i	aiues	jor p	erious	oj si	<i>xiy m</i> 4	4,000	y (•44 C.	G.S. w	nit) +	,,,,,,	, 4,00	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,						1	fay,	1923.
Hour G.M.T.	о.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day. 1 Q 2 3 D	γ 952 945 951	γ 950 945 952	γ 951 945 951	γ 951 945 952	γ 952 945 952	γ 953 945 952	γ 952 944 951	γ 952 943 949	γ 953 945 946	γ 950 943 942	936 947 938	γ 934 945 935	γ 930 939 929	γ 932 935 933	γ 937 940 939	γ 941 945 942	γ 942 950 946	γ 943 954 946	945 956 953	γ 945 955 959	γ 945 954 964	γ 945 952 957	γ 945 951 954	γ 945 951 945	γ 945 951 938	945 947 947
4 5	938 942	939 937	939 930	941 930	945 939	948 947	946 950	946 949	941 946	939 940	937 937	934 935	934 935	934 940	939 946	943 948	946 951	948 955	951 959	952 963	954 959	956 952	953 952	951 952	942 950 949	944 946 949
6 7 8 9	949 949 953 938 952	950 949 947 941 952	950 947 949 944 952	950 948 947 946 952	950 951 949 948 951	951 952 950 949 951	951 952 947 949 949	950 953 945 951 949	949 952 938 950 947	947 947 937 945 946	944 941 942 944 945	937 940 939 943 944	933 939 939 942 943	940 942 940 944 949	945 944 941 947 952	948 943 943 951 952	952 945 950 953 952	955 949 955 955 953	956 954 956 955 953	956 955 956 956 954	956 961 956 956 955	955 960 955 955 953	954 959 955 953 951	950 958 948 952 951	953 938 952 951	949 950 947 949 950
11 12 Q 13 Q 14 15	951 949 948 948 948	950 949 948 947 948	949 950 947 947 948	949 949 947 948 948	949 950 948 948 948	950 951 948 948 949	947 950 947 947 948	946 949 947 947 947	942 945 946 944 940	937 940 946 938 935	936 937 944 934 932	938 936 938 926 931	940 933 934 925 932	942 932 937 929 936	942 935 943 936 941	944 943 947 943 945	945 945 946 950 947	945 949 945 953 950	951 951 948 952 952	953 951 951 950 952	954 949 952 949 951	953 950 951 947 950	951 949 949 946 948	950 949 949 947 948	949 948 949 948 948	946 945 946 944 945
16 17 D 18 D 19	948 948 915 946 939	947 948 902 937 937	948 943 861 932 943	948 939 875 937 947	951 943 884 940 949	951 945 892 941 950	949 944 919 941 950	949 943 935 940 950	947 940 939 941 947	947 939 938 939 944	947 932 936 939 942	944 932 935 941 940	944 933 935 939 937	943 932 943 937 937	943 936 950 940 941	944 944 954 944 946	945 961 952 950 949	950 971 952 955 953	952 1010 959 959 959	952 988 959 963 960	951 971 959 959 959	950 965 955 952 956	947 959 949 949 954	947 932 947 948 943	948 915 946 939 937	948 949 932 944 947
21 22 Q 23 24 Q 25	937 942 950 951 951	935 943 944 950 951	943 946 946 951 950	942 948 947 951 950	947 951 947 951 948	948 952 947 951 950	948 952 947 948 947	950 951 947 946 943	950 948 946 946 940	948 943 940 943 936	943 940 939 935 934	937 936 935 931 928	935 932 932 928 927	934 935 939 939 924	939 939 947 946 929	948 943 946 948 936	952 947 950 950 941	956 951 952 952 948	963 955 955 955 954	964 956 955 955 954	962 959 958 955 954	957 955 955 955 952	953 953 952 952 951	950 951 951 951 951	942 950 951 951 951	948 947 947 947 944
26 27 28 29 D 30 D	951 950 949 947 923	950 948 949 947 927	951 949 948 946 929	949 950 949 947 927	949 951 950 949 925	951 950 950 948 925	949 948 947 947 929	947 948 950 946 935	944 944 950 944 934	942 943 948 937 925	941. 939 945 927 923	939 935 945 921 929	937 932 942 919 936	942 930 940 928 951	944 932 940 940 967	947 940 945 954 980	952 944 951 959 987	955 951 956 967 989	955 952 955 982 986	955 952 954 986 978	954 952 953 971 977	951 951 952 969 962	951 951 949 958 954	951 948 947 941 951	950 950 947 923 950	948 945 948 949 948
31	950	946	943	943	947	951	951	951	945	942	938	938	935 935	941	946	950 947	950 950	950	951 958	950 958	949	950	949	947 948	946 945	946 946
Mean.	945	944	943	944	945	947	947	947	945	941	939	936	935	937	942				A C N	,		·				

DAILY EXTREMES OF EACH COMPONENT OF TERRESTRIAL MAGNETIC FORCE: MAGNETIC CHARACTER FIGURES: TEMPERATURE IN MAGNET HOUSE.

230. Eskdalemuir.

May, 1923.

Maximim 15,000 y + 15,00	Range. 7 23 22 37 24 39 23 25 21 18 15		ο·35 ο·45 1·82 1·12 ο·78 ο·32 ο·52 ο·90 ο·31	Magnetic Character of Day (0-2).	Temperature in Magnet House 200 + . a. 83.7 83.6 83.5 83.5 83.6 83.6
Day. North Component. West Component. W	γ 23 22 37 24 39 23 25 21 18 15	37 47 189 116 81 33 54 93 32	0·35 0·45 1·82 1·12 0·78 0·32 0·52 0·90	of Day (0-2).	Magnet House 200 +. a. 83.7 83.7 83.6 83.5 83.5 83.6 83.6
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	γ 23 22 37 24 39 23 25 21 18 15	37 47 189 116 81 33 54 93 32	0·35 0·45 1·82 1·12 0·78 0·32 0·52 0·90	0 I	200 +. a. 83 · 7 83 · 6 83 · 5 83 · 6 83 · 6 83 · 6
1	23 22 37 24 39 23 25 21 18	37 47 189 116 81 33 54 93 32	0·45 1·82 1·12 0·78 0·32 0·52 0·90	0 1 1 0 1 0 0	83.7 83.7 83.6 83.5 83.5 83.6
1 20 27 1034 992 11 33 42 13 33 14 10 2 0 52 1030 985 10 52 45 14 25 697 650 8 18 47 17 40 957 935 12 40 3 22 46 1078 989 10 53 89 15 8 701 603 23 56 98 19 40 965 928 11 45 4 23 35 1040 989 9 18 51 16 24 696 604 0 1 92 20 38 957 933 12 40 5 19 52 1040 985 11 10 55 14 3 692 632 0 13 60 19 20 965 926 2 30 6 22 6 1030 990 11 10 40 12 46 682 648 8 40 34 20 15 956 933 11 50 7 23 11 1048 996 10 57 52 17 48 695 649 6 40 46 19 38 964 939 11 50 8 23 18 1054 976 12 36 78 12 44 692 639 1 6 53 20 8 957 936 8 42 9 18 13 1028 990 13 52 38 14 52 682 644 0 36 38 19 15 956 938 0 1 9 18 13 1028 990 13 52 38 14 52 682 644 0 36 38 19 15 956 938 0 1 17 27 1032 992 13 33 40 14 56 677 652 9 33 25 20 11 956 941 11 40 11 19 41 1028 989 14 32 39 15 27 685 649 6 52 36 20 20 955 936 9 10 12 16 58 1030 988 11 11 42 12 56 683 647 8 50 36 17 50 952 931 12 45 13 18 28 1033 988 11 11 42 12 27 691 640 6 53 51 20 0 952 933 12 0	23 22 37 24 39 23 25 21 18	47 189 116 81 33 54 93 32	0·45 1·82 1·12 0·78 0·32 0·52 0·90	0 1 1 0 1 0 0 1	83.7 83.6 83.5 83.5 83.6 83.6
1 20 27 1034 992 11 33 42 14 10 f 080 031 9 35 37 0 1 935 23 2 0 52 1030 985 10 52 45 14 25 697 650 8 18 47 17 40 957 935 12 40 3 22 46 1078 989 10 53 89 15 8 701 603 23 56 98 19 40 965 928 11 45 4 23 35 1040 989 9 18 51 16 24 696 604 0 1 92 20 38 957 933 12 40 5 19 52 1040 985 11 10 55 14 3 692 632 0 13 60 19 20 965 933 11 240 6 22 6 1030 990 11 10 40 12 46 682 648 8 40 34 20 15 956 933 11 50 7 23 11 1048 996 10 57 52 17 48 695 649	22 37 24 39 23 25 21 18 15	47 189 116 81 33 54 93 32	0·45 1·82 1·12 0·78 0·32 0·52 0·90	0 1	83.7 83.6 83.5 83.5 83.6 83.6
2 0 52 1030 989 10 53 89 15 8 701 603 23 56 98 19 40 965 928 11 45 4 696 604 0 1 92 20 38 957 933 12 40 40 19 52 1040 985 11 10 55 14 3 692 632 0 13 60 19 20 965 926 2 30 11 50 19 52 1040 985 11 10 55 14 3 692 632 0 13 60 19 20 965 926 2 30 11 50 19 52 1040 985 11 10 10 10 10 10 10 10 10 10 10 10 10	37 24 39 23 25 21 18 15	189 116 81 33 54 93 32	1 · 82 1 · 12 0 · 78 0 · 32 0 · 52 0 · 90	0 1	83.6 83.5 83.5 83.6 83.6
3	24 39 23 25 21 18 15	33 54 93 32	1·12 0·78 0·32 0·52 0·90	0 1	83·5 83·5 83·6 83·6
4 23 35 1040 985 918 11 10 51 10 24 692 632 0 13 60 19 20 965 926 2 30 6 22 6 1030 990 11 10 40 12 46 682 648 8 40 34 15 32 18 1054 976 12 36 78 12 44 692 639 1 6 53 10 17 27 1032 992 13 33 40 14 56 677 652 9 33 25 648 8 40 34 20 15 956 933 11 30 88 11 11 42 12 56 683 644 0 36 38 19 15 956 938 0 1 11 19 41 1028 989 14 32 39 15 27 685 649 6 52 36 17 58 1030 988 11 11 42 12 56 683 647 8 50 36 17 50 952 931 12 45 13 18 28 1033 984 11 32 49 12 27 691 640 6 53 51 20 0 952 933 12 0	39 23 25 21 18 15	33 54 93 32	0·32 0·52 0·90	0	83·5 83·6 83·6
5 19 52 1040 905 11 10 55 14 3 692 632 615 60 19 20 90 11 10 10 12 46 682 648 8 40 34 20 15 956 933 11 30 7 23 11 1048 996 10 57 52 17 48 695 649 6 40 46 19 38 964 939 11 50 8 23 18 1054 976 12 36 78 12 44 692 639 1 6 53 20 8 957 936 8 42 9 18 13 1028 990 13 52 38 14 52 682 644 0 36 38 19 15 956 938 0 1 10 17 27 1032 992 13 33 40 14 56 677 652 9 33 25 20 11 956 941 11 40 11 19 41 1028 989 14 32 39 15 27 685 649 6 52 36 20 20 955 936 9 10	23 25 21 18 15	54 93 32	0·52 0·90	ı	83.6
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7 23 11 1048 996 10 57 52 17 48 695 649 6 40 46 19 38 964 939 11 50 8 23 18 1054 976 12 36 78 12 44 692 639 1 6 53 20 8 957 936 8 42 95 18 13 1028 990 13 52 38 14 52 682 644 0 36 38 19 15 956 938 0 1 10 17 27 1032 992 13 33 40 14 56 677 652 9 33 25 20 11 956 941 11 40 11 19 41 1028 989 14 32 39 15 27 685 649 6 52 36 20 20 955 936 910 12 16 58 1030 988 11 11 42 12 56 683 647 8 50 36 17 50 952 931 12 45 13 18 28 1033 984 11 32 49 12 27 691 640 6 53 51 20 0 952 933 12 0	21 18 15	93 32	0.90		
8 23 18 1054 976 12 36 78 12 44 692 639 1 6 53 20 8 957 936 8 42 9 18 13 1028 990 13 52 38 14 52 682 644 0 36 38 19 15 956 938 0 1 10 17 27 1032 992 13 33 40 14 56 677 652 9 33 25 20 11 956 941 11 40 11 19 41 1028 989 14 32 39 15 27 685 649 6 52 36 20 20 955 936 910 12 16 58 1030 988 11 11 42 12 56 683 647 8 50 36 17 50 952 931 12 45 13 18 28 1033 984 11 32 49 12 27 691 640 6 53 51 20 0	18 15	32	1		83.7
9 18 13 1028 990 13 52 88 14 52 682 644 0 36 38 19 15 956 938 0 1 11 40 11 19 41 1028 989 14 32 39 15 27 685 649 6 52 36 20 20 955 936 9 11 12 16 58 1030 988 11 11 42 12 56 683 647 8 50 36 17 50 952 931 12 45 13 18 28 1033 984 11 32 49 12 27 691 640 6 53 51 20 0 952 933 12 0	15		1 0.31	0	83.7
10 17 27 1032 992 13 33 40 14 56 677 652 9 33 25 20 11 950 941 11 40 11 19 41 1028 989 14 32 39 15 27 685 649 6 52 36 20 20 955 936 9 10 12 16 58 1030 988 11 11 42 12 56 683 647 8 50 36 17 50 952 931 12 45 13 18 28 1033 984 11 32 49 12 27 691 640 6 53 51 20 0 952 933 12 0		23	0.24	l ő	83.6
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12 16 58 1030 988 11 11 42 12 30 603 647 6 30 36 7 30 952 933 12 0 13 18 28 1033 984 11 32 49 12 27 691 640 6 53 51 20 0 952 933 12 0	21	35	0.34	0	83.7
13 1 18 28 1033 904 11 32 49 12 27 57 57 57 57 57 57 57	19	54	0.2	0	83.7
$\begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 $	32	83	0.80	0	83.7
14 17 52 1034 9/2 9 33 51 173 6 687 628 77 8 40 17 55 952 928 10 40	24	59	0.57	0	83.7
13 13 14 1333 374 3	9	46	0.44		83.7
16 21 19 1038 989 10 45 49 14 16 690 644 8 40 46 17 32 952 943 13 51	112	451	4.34	2	83.8
1 100 070 15 51 123 14 38 730 598 18 6 132 18 6 1027 915 24 0	113	348	3.35	2	83.7
		1	1.25	1	83.7
19 19 57 1056 964 10 42 92 13 23 689 630 8 7 59 19 5 963 930 2 19	33	130		1	1
20 18 21 1052 974 12 55 78 15 1 703 632 7 20 71 18 52 962 934 0 30	28	119	1.14	1	83.7
20 16 21 1652 974 35 / 7			1.07	1 1	83.7
2I 19 0 1054 980 12 6 74 16 8 689 622 I 0 67 18 50 966 932 12 45	34	64	0.62	0	83.8
22 18 13 1030 970 11 60 14 22 683 637 9 10 46 20 0 959 932 11 41	27 28	54	0.52	0	83.7
22 10 IT 1032 984 10 II 48 13 50 682 634 9 IO 48 20 42 959 931 11 40	29	55	0.52	0	83.7
24 17 53 1030 90 10 30 10 10 10 10 10 10 10 10 10 10 10 10 10	32	65	0.62	0	83.7
25 19 8 1030 983 13 10 47 12 36 692 635 6 16 57 18 0 955 923 12 40	J-	}		1	
26 17 50 1035 983 13 14 52 12 38 683 645 7 8 38 16 50 955 935 11 39	20	45	0.44	0	83.8
20 17 30 1008 070 11 43 49 13 51 698 635 8 56 63 18 42 955 928 12 48	27	71	0.68	0	83·8 83·7
1 20 1020 900 11 26 40 13 2 681 634 9 22 47 17 50 957 938 13 50	19	42	2.81	0	83.7
20 17 50 1075 978 10 30 97 14 28 726 607 21 3 119 18 28 993 918 12 0	75	292 278	2.67	i	83.7
29 1/39 1084 963 11 14 121 15 27 709 619 6 59 90 16 51 993 922 9 32	71	2/0	2.07	1	1 3
6 22 6 72 6 62 62 0 0 62 77 72 072 073 174 175 10	18	83	0.79	0	83.7
31 17 21 1027 903 9 20 04 3 40 093 031 0 40 02 17 32 930 334		104		0.45	83.7
Mean. — 1043 980 — 63 — 693 634 — 59 — 962 928 —	_33_	104	-	-	
No. of	31	31		31	31
Days - 31 31 - 31	٠,٠			1	1
§ For explanation see page 105. Q denotes an "International Quiet Day," while D denotes a disturbed day use	ad for	the com	putation	. C. Tables	

[§] For explanation see page 105. Q denotes an "International Quiet Day," while D denotes a disturbed day used for the computation of Tables 271-276.

188 TERRESTRIAL MAGNETIC FORCE: NORTH COMPONENT.

231.	Esk	lalem	uir. /`	(X.)	carrier & The selfe		,			-			s <i>centre</i> ·15 C.G.											J	une,	1923.
					, -		.	· 					15 0.0.	J. um	· ·	1	1		1	<u> </u>		1		1		
Hour G.M.T.	о.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day.	γ	ν ν	\rightarrow \frac{\gamma}{\gamma}	2.	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	γ	γ	1 v	V	V	\ \v	V	ν	ν	V	γ	ν	γ	v	γ	γ	Y	7	γ	γ	V
ī		1007	1007		1012	1013		1006	996	987	982	978	983	990	1003		1014	1022				1025	1022	1017	1020	1008
2	1020	1029	1016	1019	1017	1012	1009	1011		994	984	978	978	983	997	1010				1019		1018	1016	1012	1012	1008
3	1012	1016	1016	1013	1016	1018	1016	1012	1005	995	988	983	994	1007	1013	1020	1021			1032				1035	1032	1015
4D	1032	1021	1017	1020			1020	1016	987	991	981	983	989	992	1002		999					1028		1037	1026	1011
5	1027	1020	1024	1030	986	1004	1017	1001	1006	1004	1000	969	974	990	1002	1003	1011	1015	1021	1025	1022	1018	1016	1014	1013	1008
6	1013	1014	1013	1015	1018	1018	1016	1015	1008	998	989	991	994	994	1005	1007	1022	1034	1034	1037	1047	1019	1017	1016	1024	1014
1 7						1018			1003	997		988	995	1000	1003		1012	1019	1027	1022	1019		1013			1011
8	1013	1017	1011	1014	1016	1013	1011	1009	1002	996	993	990	993	998	1000	1003	1017	1018	1019	1028	1036	1018	1016	1014	1013	1010
9 Q	1013	1011	1011	1012	1013	1015	1015	1010	1000	993	988	985	986	988	990	1000	1001	1011	1018	1021	1020	1019	1015	1014	1013	1006
10 Q	1014	1014	1017	1014	1014	1014	1009	1001	1000	999	996	990	989	986	991	1006	1013	1019	1022	1023	1023	1024	1020	1019	1020	1009
11	1020	1020	1024	1025	1027	1027	1023	1018	1006	992	987	989	990	1013	1026	1026	1025	1024	1026	1031	1026	1027	1021	1021	1018	1017
12	1019	1018	1019	1020	1022	1021		1013		1004	1005	1006	1004	1008	1010	1022	1018	1019	1025	1029	1036	1052	1063	1066	1050	1022
13 D		1031	1035	962	1018	1022	1011	969	979	993	972	957	978	984	1000		1005							1016	1009	1006
14 D	1010	1000	1004	1010	1020	1000	994	983		964	965	966	981	986	992	1005	1005	1014	1045	1040	1026	1028	1022	1013	1019	1002
15		1016	1007	1000	1002	1003	992	997	992	985	983	972	986	993	1008	1014	1006	1007	1020	1025	1024	1025	1023	1017	1012	1005
16	1012	1013	1003	1002	1002	1009	1009	1007	1004	995	976	975	973	982	998	1000	1014	1019	1029	1026	1022	1020	1013	1012	1011	1005
17 Q	1012		1012		1013				1010	1003	994	989	991	998		1013				1024		1023	1022	1018	1018	1011
18 Q	1019	1015	1015	1019	1021	1022	1021	1014	1005	994	978	971	968	976	990	1002	1013	1023		1028		1025	1023	1022	1023	1009
19	1024	1019	1018	1020	1022	1025	1026	1023	1019		1007	994	987	988	995	1013	1019	1022	1030	1029	1029	1031	1032	1031	1031	1018
20	1032	1031	1030	1021	1019	1026	1031	1024	1024	1013	1006	998	993	994	1005	1008	1008	1011	1029	1037	1038	1039	1025	1024	1033	1019
21 D	1034	1034	1034	1024	1047	1046	1038	1025	1022	1007	983	998	1008	994	1002	1009	1013	1034	1038	1045	1036	1031	1028	1033	1034	1023
22			1021			1018		1023			1004	998	990	995		1015				1037		1026		1022	1023	1017
23	1023	1022	1018	1016		1017		1013		1001	998	1000			1025		1019			1035		1028	1024	1024	1025	8101
24 Q	1026					1027					995	991					1030					1028	1027	1024	1024	1019
25	1025					1030					1007						1036					1028	1027	1023	1022	1024

TERRESTRIAL MAGNETIC FORCE: WEST COMPONENT.

 1044 1044 1035 1036 1019 1010

1028 1030

30 D

1035 1027 1029 1033 1022 1022 1042 1043

1020 1018

232.	Esko	alem	uir.	(—Y ,) /:	ean v	aiues .	jor pe	rnods	of si	•		s centre 04 C.G.S.			urs oj	Gree	nwich	i IVI ea	n 111	me.			J	une,	1 92 3.
four .M.T.	o.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mear
Day. 1 2 3 4 D 5	γ 654 662 661 653 659	9 655 665 660 651 657	9 657 665 660 654 663	9 657 661 657 655 675	γ 655 648 658 659 690	7 650 638 648 666 696	γ 643 636 646 673 670	7 636 632 646 673 640	9 633 628 647 665 637	7 630 631 649 656 636	9 644 641 654 657 651	9 661 659 664 667 661	7 676 677 676 683 671	9 682 683 686 - 689 684	9 686 685 689 690 692	9 685 687 693 693 689	9 683 682 685 682 679	7 677 677 677 681 678	9 664 675 675 677 675	9 663 672 678 675 671	γ 666 668 678 675 665	9 667 666 679 669 662	9 666 662 674 662 662	9 663 661 667 665 662	9 662 661 653 659 662	9 66 66 66 67 66
6 7 8 9 Q 10 Q	662 665 662 663 667	658 654 661 661 667	656 654 658 662 668	656 664 657 658 657	653 661 651 655 656	645 653 646 651 650	638 648 643 648 641	635 645 636 644 640	633 641 634 641 640	639 640 631 643 644	657 651 639 649 651	663 663 652 659 666	676 676 668 675 682	678 686 679 683 689	687 688 680 683 687	695 685 677 683 686	702 681 678 676 677	698 678 674 671 669	684 675 669 667 663	680 669 666 667 663	651 666 664 663 666	661 666 664 663 666	666 662 665 666 668	662 665 664 668 667	665 662 663 667 666	66 66 65 66 66
11 12 13 D 14 D 15	666 665 660 649 652	665 662 635 656 677	663 661 611 663 659	660 659 650 665 656	654 656 618 651 662	649 655 623 644 646	642 645 628 647 637	635 642 607 631 628	633 643 626 630 621	634 649 657 626 624	646 662 660 641 635	667 672 669 659 646	682 683 685 671 661	687 687 698 679 673	684 685 707 679 683	682 686 711 682 686	676 677 680 690 684	668 668 686 689 677	665 666 686 673 676	669 668 676 671 661	670 676 666 672 664	672 684 654 669 663	671 690 643 659 661	665 688 651 645 654	665 660 649 652 657	66 65 65 65
16 17 Q 18 Q 19 20	658 656 662 662 657	658 665 659 660 657	662 659 656 659 659	674 653 657 655 651	661 651 652 650 654	650 646 646 644 642	638 643 639 638 637	636 638 638 627 634	632 631 634 637 632	633 632 635 637 635	639 638 645 643 641	650 649 655 658 658	666 662 663 674 669	676 674 673 685 673	690 680, 683 686 685	694 685 684 692 686	693 684 678 689 690	680 678 675 679 680	678 674 671 678 682	670 668 670 672 681	665 662 667 668 677	664 663 665 664 672	662 663 664 663 650	656 662 666 660 655	656 662 662 657 660	60 60 60 60
21 D 22 23 24 Q 25	660 653 664 669 664	659 646 663 665 665	652 653 660 660 665	678 652 658 652 665	663 650 656 647 659	645 651 653 644 649	646 642 644 644 638	650 632 643 644 643	645 630 643 643 648	652 630 645 639 652	658 635 651 640 650	666 649 656 645 657	675 657 670 659 669	679 665 675 666 674	680 670 679 666 677	681 674 677 669 678	668 674 673 669 671	678 671 671 669 671	676 667 672 670 679	677 668 672 673 679	671 670 669 674 678	668 669 669 673 672	661 666 669 665 670	660 665 669 667 668	653 663 669 664 667	66 66 65 66
26 27 28 29 30 D	667 664 661 659 661	664 661 641 658 665	659 659 646 656 655 658	654 658 633 653 653 658	651 654 647 650 650	644 659 637 640 641	634 663 634 637 648	627 651 637 634 650 640	629 649 647 632 649	637 649 641 635 651 639	653. 656 644 640 648	664 666 655 652 657 658	679 ₄ 677 677 667 684	687 691 691 678 705 681	692 690 692 683 733 686	683 689 690 681 733 687	673 681 679 676 739	670 682 677 668 756 680	670 669 670 668 717 675	671 659 665 665 669	676 667 663 660 670 668	673 667 661 660 660	669 659 659 663 647 663	668 661 661 660 653	664 661 659 661 661	66 65 65 67 66

TERRESTRIAL MAGNETIC FORCE: VERTICAL COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

233. Eskdalemuir. (Z.)

June, 1923.

189 -

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Hour G.M.T.	О.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day.	7	7	7	7	7	γ 950	γ 952	y 950	γ 948	γ 945	γ 943	γ 941	y 940	γ 941	γ 943	y 950	γ 952	γ 955	γ 959	γ 959	γ 955	γ 952	γ 949	γ	γ 946	γ 949
2	945 946	946 939	949	949 938	949 943	948	947	947	948	943	934	930	926	928	935	939	946	950	950	949	947	946	949	949 946	946	949
3	946	946	946	946	948	947	946	946	946	944	942	936	930 932	931	937	943	947	952	952	950	949	945	944	944	940	944
4 D	940 942	942 943	944 944	945 942	945 934	944 906	937 907	934 926	937 935	930 935	935	936	939	933 941	935 942	939 946	949 950	953 953	953 954	953 956	950	950 954	949 951	944 950	942 950	941 941
6	950	949	950	950	950	950	950	949	946	940	933	930	926	932	941	947	953	959	961	959	957	951	948	947	944	947
7	944	940	941	941	944	944	945	945	946	945	939	931	932	937	941	949	954	954	955	960	958	955	953	952	951	946
9Q	951 949	946 949	946 948	946	949 950	953 949	952 948	952 952	953 954	951 953	948	945	937 934	938	941 942	945 943	946	951 952	955 953	957 953	955	953 950	950 950	949	949 949	949 948
ıó Q̃	949	948	946	947	949	951	953	952	950	944	941	942	938	940	939	942	946	949	952	951	950	949	949	949	949	947
11	949	949	949	949	951	952	952	953	952	947	•	_	-	_	_		_	_	-	-		1			•	
12 13 D		_	=		_			_	_	_		•	933	027	-	957	981	986	979	978	972	961	953	942	941	^
14 D	941	938	918	922	929	935	941	947	949	947	941	940	933 941	937	944 952	963	965	970	979		971	963	933	937	940	947
15	940	933	934	942	943	948	955	957	956	950	946	944	946	952	956	960	959	959	959		958	955	955	954	955	951
16	955	954	950	940	939	947	952	954	955	953	950	945	943	944	944	950	954	959	962		963	960	956	955	954	952
17 Q 18 Q	954	951	948	952	955	955	955	955	954	955	952 948	944 941	945	948	944	947	955	960 959	961	962	961 957	958 954	955 952	954 953	953 951	953 952
19	953 951	953 952	953 954	954 955	957 957	957 955	957 953	957 955	955 955	954 948	942	940	939 943	940 944	942 946	948	955 948	955	956	956	957	953	953	953	952	951
20	952	950	946	949	951	951	950	953	950	946	939	939	941	940	941	949	954	956	956	961	963	960	962	953	945	950
21 D	945	946	948	945	930	934	936	941	944	945	948	946	947	952	957	958	967	966	964		961	961	963	960	949	951
22	949	949	950	954	956	957	954	957	959	958	953	949	945	948	955	954	957	962	963		961	959	957	955	955	955
23 24 Q	955 955	954 949	955 950	957 952	957 955	957 956	956 956	952 952	951 953	946 953	946	945 946	950 946	953 950	955 952	953 952	956 953	957 954	959 954	953	955	961 957	959 957	957 957	955 956	955 953
25	956	956	956	956	955	955	954	951	949	947	949	952	953	952	955	956	960	900	958		959	961	961	961	961	955
26	961	961	961	961	960	959	959	956	952	946	946	945	943	943	945	943	950	957	957	957	957	957	957	957	957	954
27	957	957	957	957	958	957	950	948	946	944	940	942	945	953	957	961	965	961	904	970	965	964	965	963	953	956
28 29	953	953 958	953 957	950 95 8	948 959	942 962	944 962	944	944 961	943 961	941	942	946 956	947 956	946	953 961	961	964	966	968	967	964	961	959	957 960	953 961
30 D	957 960	957	957	958	958	958	956	957	959	962	957	952	948	953	966	996	1030	1050	1064	1040	1010	991	976	969	968	979
Meant	950	949	948	949	949	949	949	950	950	948	944	942	941	944	947	952	957	961	963	962	960	957	954	953	951	95I
					J								1			1		l		1	l	l				

DAILY EXTREMES OF EACH COMPONENT OF TERRESTRIAL MAGNETIC FORCE: MAGNETIC CHARACTER FIGURES: TEMPERATURE IN MAGNET HOUSE.

234. Eskdalomuir.

June, 1923.

234.	ESKGAN	muir.																vun	0, 1923.
							Terrestri	al Magne	tic Force.								racter ures.§	Magnetic	Temperature in
Day.		Nor	th Compo	opent.		1	Wes	t Compo	nent.		1	Vert	ical Comp	onent.			Ī	Character of Day	Magnet
•	Maxis	no uno.	M	inimum	Range.	Maxit	num) Mi	nimum	Range.	Maxis	mum,) Mi	nimum	Range.	ΣR¹.	ρ	(o-2).	House 200 +.
	15,000			οοο γ +		4,000			00 γ +			0 y +		00 y +			 		
	h. m.	γ	γ	h. m.	67	h. m.	1	y	h. m.	1 7	h. m.	1 7	γ	h. m.	γ	100y2		1 .	a .
I	18 24	1041	974	11 0	07	14 13	690	629	9 6	61	18 15	961	939	11 58	22	87	0.67	0	83.7
2	0 43	1036	973	11 26	63	15 17	694	626		1	18 10	952	924	12 20	28	94 88	0.73	0	83.7
3	19 12	1050	981	10 54	69 80	15 13	699	640	5 39	59	17 3	953	929	12 20	24 28		0.68	0	83.7
4	22 46	1051	97,1	10 21		15 0	699	645	9 26	54 85	17 15	953	925 901	10 3		101 160	0.78	1	83.7
5	3 6	1036	955	11 30	81	4 34	709	624	7 18	05	18 47	957	801	5 8	56	109	1.31	I	83.7
6	20 9	1059	984	14 55	75	15 31	715	629	7 28	86	17 25	963	926	11 58	37	144	1.12	1	83.7
7	0 58	1036	984	11 14	52	14 19	692	637	8 51	55	19 15	961	930	11 20	31	67	0.22	0	83.8
8	19 47	1054	987	9 58	67	13 8	683	629	8 50	54	19 20	959	937	12 30	22	79	0.61	0	83.8
9	19 39	1023	983	12 10	40	14 58	686	639	7 45	47	8 14	955	932	11 25	23	43	0.34	0	83.9
10	19 34	1027	984	12 50	43	12 30	690	639	6 50	51	5 50	953	937	12 10	16	47	0.36	0	83.9
11	18 59	1039	980	11 25	59	13 45	689	628	8 14	61	-							0	83.9
12	23 29	1077	1000	12 26	77	23 32	700	640	7 15	60	-	-	-	_	-		_	I	83.9
13	2I I	1059	932	2 55	127	14 35	732	578	2 20	159	17 0	989	933	12 11	56	445	3.45	2	83.9
14	18 16	1091	951	11 21	140	21 34	707	618	22 24	89	18 4	980	914	2 5	66	319	2.47	I	84.1
15	19 4	1040	956	11 25	84	10	699	617	8 16	82	18 50	963	928	1 23	35	150	1.16	I	84.0
16	18 20	1032	966	11 52	66	14 40	700	631	8 19	69	18 45	965	937	3 40	28	99	0.77	0	84·1
17	17 30	1031	988	10 55	43	15 36	687	629	8 10	58	19 50	962	942	11 25	20	56	0.44	0	84·I
18	23 40	1029	965	12 5	64	14 35	685	630	8 26	55	17 45	961	937	11 40	24	77	0.60	0	84.1
19	22 50	1035	981	13 0	54	15 20	695	624	7 15	7I	19 10	957	938	10 52	19	83	0.64	0	84.2
20	20 44	1049	989	11 43	60	15 45	691	630	8 10	61	19 22	963	937	10 15	26	80	0.62	0	84.2
21	5 22	1057	968	10 3	89	3 18	705	635	5 14	70	16 9	968	929	3 45	39	143	1.11	I	84.2
22	19 21	1043	986	12 14	57	15 22	678	624	7 25	54	17 30	964	944	12 25	20	66	0.21	0	84.3
23	14 58	1039	994	10 23	45	14 57	683	641	7 57	42	19 47	964	943	10 40	21	42	0.33	0	84.3
24	I5 45	1036	990	10 50	46	19 50	675	637	9 30	38	22 20	958	945	11 35	13	37	0.29	0	84.3
25	15 23	1040	995	11 15	45	19 0	680	637	6 o	43	16 35	961	946	9 20	15	41	0.32	0	84.3
26	19 30	1045	990	11 2	55	14 5	694	621	7 41	73	3 40	961	941	15 3	20	88	o·68	o	84.3
27 28	23 54	1050	977	12 14	73	13 26	697	645	8 30	52	18 50	971	939	10 10	32	91	0.70	. 0	84.5
	O I	1048	969	11 50	79	13 0	695	627	3 0	68	19 10	969	939	10 25	30	118	0.01	Ţ	84.5
29	22 0	1041	984	11 58	57	15 14	685	631	7 40	54	17 25	969	954	13 47	15	64	0.20	0	84.7
_30	17 28	1119	964	18 3	155	17 30	791	624	9 3	167	18 1	1079	947	II 43	132	693	5.38	2	84.7
Mean.	_	1047	977		70		697	629		68		967	935		32	129		0.40	84.1
No. of																-0			
days	_	30	30	_	30	_	30	30	_	30		28	28		28	28		30	30
used.		<u> </u>	l		1		<u> </u>			<u> </u>		l	l .		<u> </u>	'		l	<u> </u>

^{*} No trace. † Mean of 27 days: 11th, 12th, 13th omitted.
Q denotes an "International Quiet Day," while D denotes a disturbed day used for the computation of Tables 271-276.

190

14 9168150 TERRESTRIAL MAGNETIC FORCE: NORTH COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

235. Eskdalemuir. (X.)

July, 1923.

	`			. ,							15,00	ογ(1	5 C.G.S	. unit)	+											
Hour G.M.T.	О.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
Day.	γ	γ	γ	γ	γ	γ	γ_	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	1013
1	1012	1018	1	1014	1016			1 -			1001	996	993	988	1008	1009	1016	1023	1029		1031	1029	1031	1025	1020 1021	1018
2	1021	1016		1016	1022	1011	1026	l -	1017	1007	1009	1004	998	997	1012	}	1023	1024	1028		1031	1	1 -	1025	1024	1020
3 4	1025			1028	1	1025	• •	1	1 1	1	1000	998	1003	999	1		1011		1032	1033	1033	1028	1023	1023	1023	1018
5 Q	1024	1020	1021	1024	1024			1019	1014	1009	1000	996	1002	1000	1004	1005	1013	1023	1026	1035	1035	1030	1031	1034	1034	1018
6 .	1035	1035	1032	1030	1030	1034	1030	1026	1022	1013	1006	1007	1010	1011	1012	1015	1020	1029	1046		1054	1046	1046	1045	1036	1029
7 D	1037			1026		1015		1017	1007		1003	1000	1005	1		1				1036			1026		1024	101
8	1024	1021	1	1021		1023		•	1026	1018		1007	1008	1009	1	1024		1016			1037	1032	1031	1027	1026	1022
9 10 D	1027	1023	1023	1024	1026		1024 1028		1025	1021	1006	998	990 976	991 1010	1003	1007		1030	1033		1042		1038		1035	1026
101	1030	1039	1019	1030	1030	1033	1020	1023	1010	1009	1		"				1	""							0	
11 D	1021	1021	1	1			1011		1009	1006	"	1005	977	999	1006	1024	1024	1028	1045			1038	1043	1029	1028	101 102
12	1 -	1032		1025	1 -	1024	•	1	1012	1009	1	1008	1012 1012	1029 1011	1035	1019	1026	1022	1025		1034 1035	1031	1032		1027	102
13 14 Q	1027	1025	1025	1025		1021	1021 1026		1016	1016	1015	1014	1012		1016	, -	1024		1032		1 00	1032	1032	1031	1031	102
14 Q 15 Q	1	,				1027			1017	1	1004	1005		1007	1017	1020	1021	1026				1037	1032	, ,	1031	102
+6		7020	1021	1000	1022	1033	1022	1029	1025	1018	1012	1008	1005	1014	1019	1021	1027	1033	1041	1038	1041	1038	1043	1033	1032	102
16 17	1032	, ~	"	1	1 -	1033	• -	1	1036	1032		1018	, ,	1005		1022			1048		1046		1032	1 00	1035	103
18 D		· · ·	_		1				1028	1024		1021	1008	-		1014			1057		1047	1049	1038	1045	1046	103
19	1 -	1044	1039	1029			1033		1018	1005	995	989	989	999	1006	1013	1015	1033	1039	1040	1042	1035	1036	1037	1038	102
20	1039			1022		1035		1021	1020	1011	1005	999	1004	1009	1010	1013	1023	1029	1035	1040	1039	1035	1034	1034	1033	102
21 Q	1033	1033	1030	1030	1031	1030	1030	1029	1021	1011	1005	995	996	1006	1012	1021	1025	1032	1034	1036	1035	1034	1034	1033	1030	102
22 ~			, -	1033			1034		1021	1011	1006	1002		1014	1020	_	1040	1040	1040			1041	1051		1069	103
23 D	1069			1043			1041			1002	991	991		1007	-	1022		1040			1035		1025	, -	1025	102
24 Q	1	1	, .			1026			•		1006	1002		,	1022	ł.	1018	1022	1027		1031	1031	1030	"	1031	102
25	1031	1031	1030	1026	1031	1031	1031	1026	1022	1012	1007	1003	1011	1017	1025	1033	1038	1038	1037	1031	1020	102/	1031	1033	1033	102
26	1033	1032	1032	1032	1032	1031	1031	1029	1027	1022	1016	1013	1021											1034	1038	103
27	1039	1037	1028	1032	1033	1043	1042	1036	_	1		1015		,	•	1008			1038	V /	1034	1	1038		1033	103
28	0.0	1027					1032)			1014	1017	1022	1029	1032	1027			1038	1041		1035	, .,	1038	102
29		1042			I ~~		, ,,		•	,		1003	1006	1022 1018		1030			1029		1042 1040		1037		1033	103
30	1034	1034	1033		-		Ĭ		•	}	1	1007			}						, -					
31	1038	1034	1033	1038	1038	1036	1032	1024	1018	1015	1010	1003	1004	1008	1014	1023	1018	1024	1033	1042	1043	1042	1042	1044	1042	102
Mean	1032	1030	1028	1028	1028	1020	1028	1024	1019	1013	1008	1004	1004	1009	1015	1020	1024	1030	1037	1039	1038	1035	1034	1034	1032	102

TERRESTRIAL MAGNETIC FORCE: WEST COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

Eskdalemuir. (-Y.)

4,000 y ('04 C.G.S. unit) +

July, 1923.

											4,000	γ (.07	C.G.S.	unit)	+											
Hour G.M.T.	О.	-2.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day. 1 2 3 4 5 Q	661 653 660 657 658	γ 669 653 663 656 653	γ 664 656 661 653 653	γ 664 653 656 653 655	γ 647 663 654 649 653	γ 642 657 658 648 649		γ 646 637 649 645 649	γ 651 634 651 641 652	γ 638 636 652 637 652	9 637 648 657 637 650	γ 643 663 658 646 657	9 657 677 673 664 668	y 670 679 679 669 676	γ 679 688 679 670 680	γ 676 693 678 673 679	9 674 686 669 673 675	9 674 674 664 673 669	9 674 685 664 674 662	9 670 674 663 665 660	9 667 668 663 662 661	9 662 668 663 660 663	9 654 668 660 660 663	γ 653 663 658 658 663	γ 653 660 657 658 662	9 659 664 662 657 660
6	662	658	657	655	653	646	637	635	631	632	644	657	669	683	685	685	685	681	681	676	663	670	669	668	669	662
7D	670	665	655	655	658	659	638	633	641	639	643	653	665	678	680	680	680	675	675	675	675	661	655	657	657	661
8	657	657	658	654	663	648	638	632	629	633	645	653	662	666	669	671	667	665	671	672	670	664	663	659	659	657
9	659	654	653	654	652	644	641	643	644	642	646	655	659	661	669	672	670	670	669	674	671	673	659	659	659	658
10 D	659	669	697	648	638	631	633	630	632	643	647	665	687	702	707	699	690	684	702	664	659	659	670	649	645	663
11 D	645	658	643	642	660	648	638	639	638	641	648	654	659	671	677	682	680	675	674	671	663	658	659	655	659	658
12	659	679	648	643	645	640	640	633	628	627	637	654	670	680	681	666	668	667	670	670	669	660	659	659	658	656
13	658	659	658	654	648	645	645	646	644	644	648	656	665	674	679	671	667	664	659	659	659	664	660	651	652	657
14 Q	652	650	650	648	648	643	638	636	632	637	644	649	664	675	679	675	669	665	665	668	667	664	660	658	654	656
15 Q	654	654	653	654	649	645	640	643	639	638	644	655	670	680	686	681	675	670	670	670	665	664	659	658	654	659
16	654	654	648	643	642	633	638	638	637	637	638	644	659	665	674	673	671	667	669	670	669	664	658	647	653	654
17	653	654	653	654	654	653	650	653	653	656	655	663	671	672	678	683	677	679	680	675	670	666	643	643	648	662
18 D	648	643	638	638	644	641	637	635	631	633	644	661	674	679	691	690	690	669	675	671	664	670	665	658	643	658
19	644	645	645	650	660	671	660	649	644	646	651	660	668	671	672	675	671	671	671	666	666	663	658	649	656	660
20	656	655	646	660	658	654	645	643	639	639	649	659	666	676	685	688	680	671	670	667	665	663	660	658	656	661
21 Q	656	655	656	655	653	645	639	629	628	632	639	649	661	667	670	665	660	660	660	665	664	660	660	660	659	654
22	659	658	655	654	650	648	641	637	631	628	634	647	660	675	676	681	676	670	671	671	669	670	672	671	673	659
23 D	673	639	612	595	618	660	633	632	627	624	632	646	667	685	693	681	670	674	670	670	659	662	662	659	655	651
24 Q	655	662	655	651	646	642	634	633	635	639	641	651	669	670	664	656	655	655	656	659	655	659	659	655	655	652
25	655	655	649	649	646	645	644	640	638	640	644	649	665	677	680	676	672	665	660	659	657	656	658	659	656	656
26	656	654	655	654	650	644	644	639	636	634	642	657	670	672	674	676	673	665	656	659	659	660	662	657	658	656
27	658	647	642	639	641	646	633	635	638	640	655	669	681	688	692	687	681	672	665	659	659	659	657	639	639	657
28	639	641	652	650	650	643	642	640	640	644	647	655	666	676	681	676	668	659	663	661	655	655	656	659	660	656
29	661	660	661	651	646	644	642	639	639	640	652	666	682	686	692	687	682	672	669	667	666	663	659	654	656	662
30	656	655	652	651	650	644	639	630	626	634	645	655	667	677	675	670	667	666	665	665	661	661	661	661	660	656
Mean	660 656	656 656	656 653	660	652 650	645 647	641	639 639	640 638	646	655 645	665	676	683 676	682 680	677 678	672 674	669	670	661	661	661	663	657	651	660 658
	·	·	· O d	unotos	00 "	Inter	ation	al Oui	et Da	37 '' 337	hile D	deno	tes a dis	turbe	dav	used	for the	e com	putati	on of	Table	s 27I-	276.			

"International Quiet Day," while D denotes a disturbed day used for the computation O denotes an

TERRESTRIAL MAGNETIC FORCE: VERTICAL COMPONENT.

B1923 073 01 B8440

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

44,000 y (·44 C.G.S. unit.)+

July, 1923.

237.	Eskd	alem	uir.	(Z.)	,						44	,000 γ	· (·44 C.	G.S. u	nit.) +		-							U	uiy,	1923.
Hour G.M.T.	0.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day. 1 2 3 4 5Q	γ 968 968 973 970 972	γ 961 968 973 970 972	961 964 970 972 973	γ 962 957 972 972 973	968 956 974 974 973	972 952 973 975 976	γ 970 950 974 973 975	968 953 975 973 972	967 956 973 973 969	965 960 972 972 961	γ 965 965 965 968 957	γ 966 965 961 966 954	γ 970 965 961 965 958	973 966 961 965 966	970 970 970 965 965 968	972 974 968 968 965	974 981 973 969- 969	976 994 976 970 976	976 997 997 977 970 980	976 1000 973 975 980	976 999 972 977 977	975 991 973 976 977	γ 970 981 972 974 975	969 974 971 973 973	968 973 970 972 973	970 971 971 971 971
6	973	972	972	973	976	977	977	977	977	976	973	969	966	966	966	968	970	977	980	984	986	980	977	973	968	974
7 D	968	950	927	930	933	937	953	964	965	968	966	965	964	962	965	966	969	972	976	981	981	983	982	977	976	963
8	976	975	973	974	973	972	973	977	979	977	976	974	969	966	968	970	976	976	981	981	979	977	977	977	977	975
9	977	977	977	977	977	978	977	976	973	973	969	965	958	961	964	966	970	973	976	976	977	977	980	977	976	973
10 D	976	970	947	949	966	972	973	972	972	971	957	957	952	960	969	970	972	974	980	995	994	987	972	959	957	969
11 D	957	958	966	965	954	952	967	972	971	976	973	969	973	976	977	977	981	985	988	985	984	984	977	969	973	973
12	973	956	961	969	973	976	977	981	981	977	973	973	973	976	980	981	984	985	982	981	981	981	981	980	979	977
13	979	977	976	977	978	980	980	983	977	973	977	978	981	984	979	977	981	981	983	982	981	981	981	981	980	979
14 Q	980	981	981	981	981	981	981	980	981	977	969	964	963	969	973	976	977	980	977	977	976	977	977	977	979	977
15 Q	979	980	980	978	980	980	981	980	977	977	972	969	968	968	972	975	977	980	981	982	982	980	980	979	979	977
16	979	979	978	980	980	980	979	979	980	977	974	971	970	973	973	973	975	974	976	977	980	978	976	976	977	977
17	977	977	977	977	977	977	975	973	970	968	968	966	966	968	970	973	973	974	980	985	988	988	988	984	977	976
18 D	977	977	976	977	980	980	977	974	973	971	966	963	965	970	971	973	977	988	992	992	992	985	981	978	977	977
19	977	974	976	976	974	972	970	974	974	973	974	973	972	976	977	982	988	992	988	985	985	985	983	981	977	978
20	977	970	973	973	974	977	980	980	980	978	972	968	965	969	976	980	983	986	988	987	985	985	983	981	981	978
21 Q	981	981	981	982	984	987	985	984	984	981	977	976	970	972	977	977	979	984	983	984	984	981	981	981	981	981
22	980	979	980	980	980	981	983	986	980	975	972	971	969	968	973	972	976	984	984	983	980	980	979	979	964	978
23 D	964	960	956	956	957	938	938	952	960	964	967	971	971	969	972	978	987	988	989	987	988	987	984	984	984	970
24 Q	984	980	979	979	980	984	987	988	988	984	984	984	979	976	980	984	987	987	984	984	984	984	984	984	984	983
25	983	983	983	982	980	981	979	979	977	978	972	970	968	967	970	974	976	978	983	983	983	982	982	981	982	978
26	982	982	982	982	983	983	984	985	983	979	979	981	977	979	981	980	986	990	990	986	983	983	983	983	983	983
27	983	983	982	982	983	975	974	976	975	978	975	979	975	972	978	983	986	986	986	989	987	986	984	980	977	981
28	977	974	974	976	979	982	982	983	983	983	978	978	976	978	979	979	986	990	986	984	986	986	984	983	983	981
29	983	980	978	979	979	982	982	982	979	975	968	965	971	973	978	984	988	993	989	986	986	985	985	983	983	981
30	983	983	984	986	986	986	985	983	979	977	973	971	963	963	963	971	975	982	983	983	983	983	982	982	982	979
Mean.	982	983 974	983	983	983	985 974	983 975	983 976	978 975	971 974	971	971 969	965 968	961 969	967 972	975 975	983 978	986	986 983	986 984	$\frac{986}{983}$	$\frac{983}{982}$	983 980	979 978	981	9 79 976

DAILY EXTREMES OF EACH COMPONENT OF TERRESTRIAL MAGNETIC FORCE: MAGNETIC CHARACTER FIGURES: TEMPERATURE IN MAGNET HOUSE.

July, 1923.

Day.																		1	1
Day.						7	Te r re s tria	l Magnet	ic Force.								racter ures.§	Magnetic	Temperature in
Day.		Nort	h Compo	nent.			West	Compon	ent.		1	Vertic	al Compo	onent.		77		Character of Day	Magnet House
	Maxin	num	Min	nimum 200γ+	Range.	Maxin	num	Min	nimum 00 y +	Range.	Maxim			nimum 200γ+	Range.	ΣRª	ρ	(0-2).	200 +.
	h. m.	γ +	γ	h. m.	$\frac{Range.}{\gamma}$	h. m.	lγ	γ,υ	h. m.	γ	h. m.	γ	γ	h. m.	γ	100γ2			a.
1	21 50	1040	981	13 I	:59	14 0	681	636	10 9	45	17 3	976	957	I 2I	19	59	0.70	0 ,	84·7 84·7
2	16 58	1075	985	3 50	90	17 35	696	631	8 18	65	18 30	1000	949	6 21	51	149 36	1 · 77	0	84.9
3	16 12	1042	999	11 34	43	13 19	68 o	642	6 36	38 38	18 0	977	960 963	12 O 11 40	17	36 36	0.42	ŏ	85.3
4	19 25	1038	994	13 12	44	18 0	674 683	636	9 31 5 22	39	20 0 18 3 2	977 981	953	11 10	28	46	0.55	0	85.3
5	18 53	1043	995	10 50	40	14 18	003	644	5 22	39	10 32	901	933	1	1	7			0
6	22 35	1067	998	12 36	69	14 33	694	630	8 15	64	19 40	988	964	11 50	24	94	1.12	I	85·3 85·5
7	19 13	1043	993	9 0	50	15 51	683	629	6 58	54	21 30	984	926	2 3	58	88 48	1.04	0	85.5
8	19 14	1046	999	16 6	47	17 38	677	628	7 50	49	18 o	981	966	13 20	15	40 64	0·57 0·75	Ö	85.5
9	20 40	1052	988	12 40	64	20 40	679	638	6 9	4I 101	22 34 20 IO	981 997	957 937	12 2	60 60	320	3.79	ī	85.5
ю	¹ 7 47	1081	946	11 43	135	13 42	728	627	7 5	101	20 10	997	937	2 20		34.			
m	18 58	1083	959	12 8	124	15 9	691	622	1 10	69	18 30	989	945	4 36	44	221	2.61	' I	85.7
12	14 15	1046	1001	10 24	45	o 38	696	623	8 11	73	16 30	985	953	1 11	32	84 -	0.99	0	85·7 85·7
13	19 12	1044	1006	13 0	38	14 11	68o	638	6 19	42	12 58	985	973	8 40	12	34	0.40	. 0	85.8
14	18 25	1036	1007	9 52	Ž9	13 50	68o	631	8 1	49	4 10	982	961	11 26	21	37 60	0·44 0·71	ő	85.9
15	20 5	1055	1002	10 25	53	14 32	690	636	5 53	54	19 0	983	966	11 35	17	00	0 /1		
16	18 45	1052	1001	12 13	51	14 19	675	632	6 2	43	20 40	981	969	12 0	12	46	0.54	0	85.9
17	19 20	1056	1003	12 58	53	15 2	685	637	21 52	48	21 50	991	964	11 38	27	58	0.69	0	85.9
18	18 9	1072	989	12 54	83	14 32	708	627	2 16	81	19 25	995	961	11 30	34	146	1.73	0	85·9 85·9
19	0 50	1053	989	11 33	64	15 29	681	638	2 30	43	16 54	992	969	11 58	23 26	65 63	0·77 0·75	0	86.1
20	18 54	1044	991	10 38	53	14 59	691	638	8 o	53	17 40	990	964	11 40	20	03	0.75	ľ	
2.	19 29	1039	994	11 19	45	14 10	671	627	7 50	44	5 30	987	969	12 30	18	43	0.21	0	86∙1
2I 22	23 59	1087	1001	11 11	86	23 43	695	628	8 23	67	7 10	987	962	24 0	25	125	1.48	1	86·1
23	0 7	1087	986	12 0	101	13 50	697	580	2 51	117	17 30	991	933	5 32	58	273	3.53	I	86·1 86·3
24	20 58	1039	999	11 11	40	12 32	671	630	6 20	41	8 12	990	975	12 42	15	35	0.42	0	86.3
25	16 3	1041	1002	10 50	39	13 40	683	637	7 59	46	19 O	983	966	13 10	17	39	0.47	Ŭ	00 3
		70.6	7077	11 0	25	T4 55	6	600	9 50		18 o	990	975	12 20	15	34	0.40	0	86∙ 3
26	21 45	1046 1058	1011	14 36	35 60	14 55 13 52	677 699	633 628	8 52 5 53	71	19 12	989	973 971	12 32	18	90	1.06	1	86.5
1	22 56 19 51	1050	1012	II 2	35	15 J2 15 I	682	637	6 33	45	17 20	990	973	1 0	17	35	0.42	0	86.5
29	19 51 1 15	1046	998	11 23	48	14 20	692	634	6 48	58	17 0	994	963	10 58	31	66	0.79	0	86.5
30	19 33	1047	1003	10 40	44	13 21	681	623	7 30	58	4 30	986	962	12 15	24	59	0.70	0	86.5
J-	, 55	' '			'	_					18 30 }								06 -
31	19 40	1052	999	11 47	_53_	13 22	685	631	7 10	_54_	17 41	987	959	12 55		65	0.77	<u>°</u>	86.5
Mean.	_	1053	994		59		687	631		_56		987	960		27	84		0.59	85.8
No. of					,,		2.7			2.		27	27		31	31		31	31
Days used.	_	31	31		31	_	31	31		31		31	31		3*	٦-		1	

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TERRESTRIAL MAGNETIC FORCE: NORTH COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

239. Eskdalemuir. (X.)

15 000 v (:15 C.G.S. unit) +

August, 1923.

											15,0	ου γ (·	15 C.G.S). umit)	7											
Hour G.M.T.	О.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day.	γ		γ	γ	γ	γ	γ	γ	γ	γ	γ_	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ
1 ~	1 -	1035							1026	1015	1008	1002	1002		1015		1033	1038		1042		1039	1033	1028	1027	1028
2~	1027	1026		1037			1032	1028	1023	1016	1004	995	992			1031				1053			, ,,		1036	1027
3 D	1036	1052	1048	1052	1042	1041	1042	1032	1035	1037	989	964	1004	994	1018	1019		1 -	1	1044			,	1032	1028	1029
4 D	1028	1027	1028	1023	1019	1057	1027	998	994		1006	1005	1003	999	1003					1032			1032	1029	1028	1019
5	1028	1032	1026	1024	1024	1024	1024	1023	1019	1013	1008	1004	999	1004	1021	1029	1031	1024	1024	1033	1028	1031	1032	1029	1036	1022
	_			1	1	ļ	۰									7000		T 00 m	1005	1000	1022	1022	1032	1024	1027	1026
6 D	, J					1033			1023		1	1007	1008		1019	1032	1015		1027		1033	1033	1032		1027	1020
7		1028					. ,		1014		1000	1000	, -			1014		1028	1033				1033	-	1032	1024
0	, -	_	1 -			1027			1015	1005	999	1004	1005					1029	1035		1034	1034	1034	1034	1035	1024
9	1032	_	1			1033		,	1010			1004	1	1011				1034	1040				1033	1030	1028	1025
10	1035	1029	1030	1029	1034	1031	1025	1023	1019	1011	1004	1003	1014	1.011	1014	1020	1031	2034	1343	3/	34	34	- 33			
11	1028	1026	1025	1027	1028	1028	1024	1020	1013	1006	1005	1004	1006	1012	1014	1020	1024	1028	1030	1038	1039	1034	1033	1030	1030	1023
12	1030	1030		1030	1				1007	994	991	990	1000	1005		1014		1025	1029	1035	1034	1038	1044	1043	1034	1021
13 D						1038			1010	1000	993	1000	1016	1026	1033	1034	1043	1040	1044	1044	1062	1034	1038	1033	1030	1030
14	1030		1	1035		1026			1021	1009	999	999	999	996	1008	1029	1029	1041	1043		1030			1030	1039	1024
15	1039			1023		1023			1011	1000	995	996	997	1005	1018	1010	1015	1024	1019	1024	1032	1029	1025	1024	1024	1018
		_		-			l	1		i	1						ŀ			1						
16	1024	1023		1022	1021					994	991	992	1003					1031	1032			1035	1029	1033	1039	1019
17	1039	1029		1034	1024				1009	996	990	989	993	1001		1024	1 -	1030	1030		1028	1024	1024	1024	1024	1019
18 Q	1024	1022		1024	, .	1025			1015	1006	996	994	994	1000	1	1023	-	1030	1034		1033	1033	1033	1033	1033	1020 1025
19	1033	1030		1029	1029	1029			1018	1008	1000	1004	1009	1018	1020	1023		1029	1025	1031				1043	1043	1023
20	1043	1039	1029	1035	1038	1028	1029	1027	1023	1014	1005	1001	1009	1009	1012	1019	1020	1024	1020	1029	1020	1027	1025	1025	1023	1023
27.0	7000	1022	1022	1022	1920	1020	1000	1022	1019	1014	1008	1001	1009	1015	1017	1020	1025	1020	1027	1028	1033	1030	1028	1030	1034	1021
21 Q 22	9	1022	1	1		1025		l .	1019		1006	1001						1037	1034		1030	-	1033	1052	1028	1025
23	1034	1019		1023	1023	1 - 1		1	1010	1003	995	992	993	1001	1007	1013	1015	1020		1029		1030	1029	1029	1030	1017
24 D	1030	1029	1		1033		1033		1019	1005	985	976	986	996	1001		, -	1020			, ,		1032	1034	1033	1018
25	1033	1029			1025			1	1014	1006	999	1005	1010	1010	1010			1021	1024	1031	1031	1024	1024	1023	1026	1020
-3	33			1		'	1		1					I	1				1	1			1	1		1
26	1026	1030	1028	1028	1026	1024	1020	1019	1019	1016	1013	1008	1005	1011	1020	1024			1029	4	1030		1 -	1025	1025	1023
27	1025	1028	1025	1024	1024	1020	1021	1017	1010	1002	1001	1000	996	997	999	1010	1021		1034		, .,		1030	1028	1029	1019
28 Q		1025	1023	1024	1024	1024		1023	1014	1000	990	985	985	993	1004	1011	1020	1028	1032		1030	1028	1025		1024	1017
29 Q		1023		1022	1020			_	1011	1002	995	995	999	1004	1009				1033		1033			1029	1028	1019
30	1028	1028	1028	1028	1026	1028	1028	1024	1014	1000	990	991	995	1001	1009	1018	1024	1029	1035	1038	1040	1035	1033	1034	1035	1021
		l									-0.		-0-	006			7006	102:	1025	1024	1029	1029	1029	1029	1037	1021
31		1037				1034			1019	1000	981	981	981		l	1014		-1	1035		·					
Mean	1031	1029	1028	1029	1028	1029	1028	1022	1015	1007	999	997	1001	1006	1013	1020	1025	1029	1032	1035	1035	1032	1032	1031	1031	1022
<u> </u>	1	<u> </u>	<u> </u>	1	1	1 4	•	<u> </u>	1	<u> </u>	1	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	1	<u> </u>	1	<u> </u>		<u> </u>	1	<u> </u>	1	<u> </u>

TERRESTRIAL MAGNETIC FORCE: WEST COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

240. Eskdalemuir. (-Y.)

August, 1923.

											4,000	γ (·ο	4 C.G.S.	unit)	+											
Hour G.M.T.	о.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day. 1 Q 2 3 D 4 D 5	γ	γ	γ	γ	γ	γ	γ	9	9	γ	γ	9	γ	7	7	7	γ	γ	γ	γ	9	9	9	γ	9	9
	651	650	650	650	644	639	630	634	634	639	646	657	666	672	677	676	672	668	665	665	661	661	659	656	654	655
	654	649	646	640	645	648	649	646	644	640	636	646	662	677	680	679	676	672	669	671	670	664	661	661	657	658
	657	666	651	630	623	630	634	640	651	666	657	672	688	683	683	682	673	673	673	667	641	650	644	646	650	657
	650	647	650	666	680	656	640	625	650	645	646	654	661	672	670	666	666	668	677	672	666	656	661	659	656	659
	656	651	651	645	640	640	635	635	634	635	642	651	660	667	672	672	669	661	661	661	661	661	660	656	656	653
6 D 7 8 9	656 647 657 656 652	651 648 660 652 650	653 650 656 648 651	649 648 651 649 650	647 641 641 643 644	642 640 636 639 635	635 635 636 640 631	640 631 636 636 631	638 633 630 636 631	655 640 630 641 635	665 648 641 655 644	675 656 657 667 658	688 667 668 679 672	689 677 677 688 678	685 682 677 681 678	687 677 668 672 674	670 667 658 669 663	657 661 653 663 651	656 658 656 663 646	661 654 658 662 652	651 661 662 662 661	640 658 653 662 661	642 658 651 662 659	640 656 653 657 658	646 657 656 652 656	657 654 653 657 653
11	656	652	654	656	647	641	636	635	638	644	652	662	671	676	675	669	663	660	657	657	651	657	657	657	656	655
12	656	656	656	653	651	646	641	635	632	634	641	658	675	678	678	673	666	657	653	656	657	662	662	638	640	654
13 D	640	643	648	657	641	631	630	625	630	638	651	667	683	694	693	684	679	673	672	667	668	630	629	636	646	655
14	647	648	652	649	658	663	642	632	632	636	646	659	673	678	678	674	668	659	658	646	652	657	658	657	654	655
15	654	648	652	651	647	642	633	630	632	637	652	667	679	682	689	685	675	667	652	647	655	653	657	657	654	656
16	654	653	654	652	648	644	640	636	636	642	653	663	674	674	676	671	668	668	668	668	661	654	654	649	642	656
17	642	631	637	646	640	642	641	641	636	632	640	649	663	668	669	668	662	659	657	658	658	657	655	653	652	650
18 Q	652	651	649	649	648	644	637	636	637	643	649	658	668	672	671	668	662	658	658	659	662	659	658	657	652	654
19	652	648	648	648	647	643	641	637	636	641	648	657	663	674	675	674	677	669	666	663	662	662	659	648	641	656
20	641	637	636	642	637	637	636	633	638	642	653	661	674	682	678	670	659	654	657	657	653	653	653	645	647	651
21 Q	647	648	647	647	647	642	642	637	641	643	641	662	674	679	675	667	661	658	653	657	658	658	657	651	641	654
22	641	637	644	645	649	642	642	642	638	637	652	664	675	678	672	666	661	656	653	657	657	657	653	657	658	654
23	658	649	649	647	643	640	637	636	636	641	653	663	674	680	679	672	659	655	652	654	657	657	653	657	657	654
24 D	657	653	653	652	648	641	632	628	631	635	654	664	672	681	680	673	663	658	656	653	654	657	652	648	648	654
25	648	653	669	636	636	635	638	641	641	642	647	660	678	685	683	682	674	667	660	653	658	653	649	652	656	656
26	656	658	648	647	647	646	646	646	642	641	642	652	664	675	675	672	667	663	662	658	658	657	654	652	652	655
27	652	652	651	648	646	645	642	632	627	631	642	658	674	684	679	669	663	659	657	658	654	643	645	637	642	652
28 Q	642	642	642	642	643	642	637	636	631	626	633	653	670	679	675	669	663	657	653	652	652	652	652	649	650	650
29 Q	650	648	649	647	647	645	640	637	636	636	647	654	667	679	678	672	663	661	658	658	657	653	653	652	651	654
30	651	648	648	648	647	645	642	639	634	631	636	646	664	679	684	679	674	668	662	663	663	663	656	657	667	656
Mean Mean	663	663 650	658 650	652 648	649 646	651 642	652 638	649 636	639 636	640 639	650 647	662	674 672	680 679	679 678	670 674	665	664	663 660	66 <u>3</u> 6 <u>5</u> 9	658	664 656	659 654	654 652	638 651	659

083 01 BBHO TERRESTRIAL MAGNETIC FORCE: VERTICAL COMPONENT. B1923

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time. August, 1923. 44,000 y ('44 C.G.S. unit) + 241. Eskdalemuir. (Z.)Hour 14. 15. 16. 18. 20. 21. 22. 23. 24. Mean. Noon 17. 10. II. 13. 9. 2. 3. 4. G.M.T. Day γ 986 982 981 982 ı Q 982 988 3 D 4 D 5 96 i o83 **a**8a QQI 985 985 985 988 981 981 6 D 980 982 о8т αŠτ 982 10 o86 **o** 983 980 980 13 D 982 980 972 15 983 986 982 986 18 Q 982 982 981 982 o81 о8т о8т о8т 98<u>5</u> 981 21 Q 980 980 α8т 980 983 978 981 980 969 969 98 i 98o 98r 24 D

DAILY EXTREMES OF EACH COMPONENT OF TERRESTRIAL MAGNETIC FORCE:

9<u>57</u>

980

MAGNETIC CHARACTER FIGURES: TEMPERATURE IN MAGNET HOUSE.

976

August, 1923

976

976

976

242.	Eskdale	muir		MAGN	METIC	CHAR	ACTE	K FI	GURES); IF	MPERA	AIUR	E IN	MAGI	NICI I.	IOUSE.		Augus	it, 1923.
Z4Z.	Lakudie	mun.					Terrestr	ial Magne	etic Force.								racter ires.§	Magnetic	Temperatu in
							31/	t Compo	nont.		·	Verti	cal Comp	onent.				Character of Day	Magnet
Day.			h Compo			Maxin			nimum		Maxim			nimum		Σ R ²	lρ	(0-2).	House 200 +.
	Maxim			nimum 100 y +	Range.	4,000			00 γ +	Range.	44,000			οο γ +	Range.				[
	h. m.	Y	γ	h. m.	γ	h. m.	Ìγ	γ	h. m.	γ	h. m.	γ	γ	h. m.	γ	100γ2		ł	a.
_	20 28	1050	996	II 23	54	13 21	682	630	6 5	52	50	989	961	12 8	28	64	o·85	0	86.7
I 2	19 22	1059	989	12 0	70	15 16	684	635	9 32	49	19 I	986	970	12 25	16	76	1.01	0	86.7
_	1 31	1066	941	10 52	125	12 24	699	618	3 8	81	20 12	1002	958	2 41	44	241	3.22	I	86.7
3	ľ	1	989	1		3 38	683	614	20 11 S 6 59	69	20 20	993	941	4 50	52	128	1.71	1	86.8
4	4 52	1062	1	7 31	73	14 20	676	632	5 59	44	17 0	989	969	11 10	20	51	0.69	0	86.9
5	23 48	1047	994	12 4	53	14 20	0,0	032	1 3 39	1 77	-/ -		-	1		_	ł .		
_	27.20	TO42	994	11 10	49	12 26	697	629	8 20	68	16 22	997	972	10 20	25	77	1.02	I	86.9
6	21 39	1043	994	11 50	50	14 0	683	626	7 3	57	19 22	992	969	12 40	23	63	0.84	0	86.9
7	19 29	1047		11 10		13 10	678	620	8 10	49	16 20	988	975	12 28	13	50	0.66	0	87.0
8	20 45	1043	994	1	49 48		691	630	7 37	61	15 20	991	969	11 43	22	65	0.87	О	87.1
9	18 54	1043	995	9 42	48	12 57	683	629	7 2	54	17 11	987	963	12 2	24	58	0.77	0	87.1
10	18 29	1048	1000	10 17	40	14 7	003	029	/ -	34	-,) - 1	"		1 . 1	•			ł
	l	l		10.50	40	72 55	679	634	6 18	45	18 30	987	972	11 39	15	40	0.54	0	87.1
II	20 12	1044	1002	10 50	42 81	12 55	680	631	[49	17 10	987	967	12 30	20	94	1.25	I	87.1
12	21 7	1066	985	10 38	91	13 14 13 28	698	615	7 40 21 22	83	21 14	993	967	11 36	26	158	2.11	1	87 · 1
13	20 14	1081	990	9 59	1		685	626		59	16 10	998	963	5 30	35	83	1.11	r	87.2
14	17 59	1048	988	13 22	60	13 47			7 27	67	18 48 5	1006	967	11 40	39	108	1.44	I	87.3
15	0 10	1048	979	12 33	69	14 3	694	627	7 3	07	17 31	1000	907	11 40	3				
		1048	990	10 15	58	14 8	680	632	7 19	48	16 10	987	966	10 30	21	61	o·81	0	87.3
16	19 51		990	II 2	66	14 37	672	627	0 28	45	18 o	986	962	11 50	24	70	0.93	0	87.3
17	0 10	1052	989	11 33	1	13 18	674	635	7 2	39	16 40	988	977	11 1	11	37	0.49	0	87.3
18	20 13	1034			45	ľ		}	1		7 23	985	971	12 18	14	58	0.78	o	87.5
19	23 12	1051	999	10 1	52	15 59	685	631	23 33	54	17 22 \$	985	969	12 20	16	64	0.86	o	87.5
20	0 1	1050	997	11 10	53	13 44	684	626	1 43	58	16 45	905	909	12 20	10			_	''
			005	11 11	12	13 5	682	636	7 10	46	7 0}	984	961	12 10	23	45	0.60	o	87.5
21	23 58	1038	995	11 11	43				, .	1 1	17 50∫		960	11 58	25	68	0.01	o	87.5
22	23 5	1067	1004	10 36	63	13 0	679	632	0 29	47	17 0	985 988		11 1	19	56	0.74	o	87.5
23	21 10	1034	984	10 26	50	13 19	684	632	0 8	52	14 50		969	1	18	104	1.39	I	87.5
24	23 15	1038	971	10 57	67	14 4	695	620	8 21	75	16 19	985	967	12 40				ī	87.6
25	18 42	1038	995	9 50	43	13 0	689	631	4 33	58	21 30	984	957	11 40	27	59	o·79	•	, ,, ,
-	1	1	(1	00							070	961	11 6	18	34	0.45	o	87.6
26	16 21	1037	999	12 39	38	13 11	679	639	9 9	40	17 I	979 981	964	12 22	17	69	0.92	o	87.7
27	20 20	1049	993	12 31	56	13 17	685	626	8 36	59	18 30	-		12 22	18	58	0.78	o	87.7
28	18 6	1032	982	11 54	50	12 41	681	626	9 1	55	17 30	979	961	1	10	40	0.53	0	87.7
29	19 32	1034	994	10 59	40	13 23	68o	633	8 8	47	5 21	978	966	12 45	1	66	0.88	0	87.7
30	19 50	1045	989	10 15	56	14 13	685	631	8 48	54	17 40	981	958	13 16	23	00	0 00		1
31	0 35	1048	975	10 11	73	0 20	684	635	8 30	49	8 52	974	956	13 20	18	8r	1.07	I	87.9
an.		1048	990		59		684	629		55		988	965		23	75		0.35	87.3
o. of															1	24		31	31
Days	-	31	31		31	-	31	31	_	31		31	31		31	31 .		3.	3,
sed.	1			<u> </u>	1	1		l	<u> </u>		l		<u></u>	<u> </u>			<u> </u>	'	<u> </u>

[§] For explanation see page 105.

28 Q

29 Q

Mean

Q denotes an "International Quiet Day," while D denotes a disturbed day used for the computation of Tables 27"

TERRESTRIAL MAGNETIC FORCE: NORTH COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

243. Eskdalemuir. (X.)

15,000 y (15 C.G.S. unit) +

September, 1923.

September, 1923.

													J 0.0.D.						, +							
Hour G.M.T.	о.	ı.	2.	3⋅	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day.				~~~	γ		γ	γ_	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ
I ay.	γ 1037	γ 1024	γ 1025	γ 1025	1026			1018	1011	1001	994	992	994	1005	1009	1020	1022	1021		1028	1027	1025	1028	1027	1025	1018
2	1025				1	1	1024	1020	1035	1026	995	991	996	1008	1019	1023	1023	1030	1037	1037	1038	1034	1031	1035	1051	1023
3	1051				1023			1010	1004	995	989	990	992	999	1010	1018	1020	1024	1036	1038			1026	1033	1033	1019
4	1033	1027	- 32	r e					1016	1008	995	995	993	987	1001	1006	1014	1024	1028	1025	1028	1026	1028	1028	1030	1017
7	1030				1024		1021		1016	1013	1005	1003	1005	1004	1011	1017	1018	1024	1029	1023	1027	1025	1024	1024	1024	1019
)	3-			5					1					•	1					1			1		1	
6	1024	1024	1024	1023	1024	1023	1020	1016	1013	1011	1001	1000	1002	1005	1012	1016	1022	1020	1023			, ,	1029	1	1029	1019
7 Q	1029			1028			1024		1020	1013	1005	1000	1000	1002	1005	1013	1010	1020		1028	1 -		1028	1025	1027	1019
8Õ	1027	1024	1024	1025					1023	1018	1005	996	995	1004	1009	1015	1020	1022		1028	1029	_	1030	1029	1029	1020
$9\widetilde{\mathrm{D}}$		1028		1030		1025		1024	1019	1005	995	994	997	1001	1010	1020	1014	1029	J	1028	1029	, ,	1063	1034	1033	1022
10 D	1033	1028	1038	1024	8101	1020	1024	1005	1000	994	980	976	990	996	1006	1019	1016	1019	1020	1024	1030	1033	1028	1024	1023	1014
		1					·	1 7													ĺ					707#
11	1023	1020	1023	1022	1021	1023	1019		1010	996	990	985	985	994	1009	1018		1	1021		, ,	1034	-	1034	1024	1015
12	1024	1020	1020	1020	1020	1027	1028	1025	1018	1006	992	985	991	994	1004	1005	1	1015		1027	1 -	1029	1029	1032	1030	1010
13	1030	1024	1025	1027	1026	1025	1024	1022	1014	1010	1004	1002	1008	1002	996	999	, ,	1024	1032		1036		1025	1024	1024	1019
14	1024	1028	1033	1034	1032	1030	1029	1022	1014	996	989	990	986	992	1000	1 3	1012	5	1020		1 22		1024	1025	1024	1018
15	1024	1023	1021	1024	1023	1019	1020	1020	1014	1004	995	994	1000	1012	1012	1022	1029	1024	1024	1025	1027	1028	1026	1020	1025	1010
		1					_				1					l				7006	1006	1024	7024	1022	1023	1017
16 Q			1024			1025				1005	991	991	994	1003	1006			1025	1025	1			1024	1023	1034	1017
17	1023		1023	1022	1022		š.	1014	1001	999	992	991	995	1005	1014		1024		1				1027	1043	1025	1019
18	1034		1024		1033					1005	986	991	996			1015			1024	1029	1029	1	1030	1030	1038	1018
19		· ·	1020			1023		1016		-	1000	994	995	1001		1	1019		1024	1 -	_		1036	1033	1034	1023
20	1038	1024	1034	1029	1029	1029	1028	1025	1024	1015	1009	1005	1006	1009	1014	1015	1017	1010	1024	1032	1033	1031	1030	1033	1034	10-3
				0	0	0							7005	1000	1012	1016	TOTO	1020	1024	1028	1030	1029	1031	1030	1029	1021
21 Q	1034	1029				1028			_	1010	1 -	1002	1005	1009				1024	1024			_	1038	1037	1033	1022
22 Q	1 -	1		ľ		1029		1030	-	1013	996	990	991	1002	1015			1024	1019		1 00	1029	1 0	1028	1030	1022
23	1033	1030		1030		1034		1030	1024	1013	999	995	995 999	1000		1024	1020	i	1 -	1 ,	1 0	_	1024	1024	1025	1020
24	1030	1028		1030	1		1027		1013	1004	994 1008	1007	1000	1014	1 -	1			1029			, .	1030	1024	1028	1022
25	1025	1020	1025	1025	1033	1025	1024	1023	1010	1013	1.000	100/	1009	1.014	1.014		-023	3		1			"	'		l
26 D	1028	1028	1028	1028	1037	1048	1031	999	1010	1005	1001	994	975	971	985	1009	1016	1025	1019	1021	1020	1018	1018	1018	995	1013
27 D	995	948	946	990	1025	956	966	974	990	976	948	947	948	966	985	984	980	985	1009	995	971	980	980	1009	981	977
28 D	993	990		1010				1014	1004	994	986	986	986	989	1006	1005		1014	1013	1	1015	1017	1023	1019	1034	1006
29	1034	1009	1			1018			1010	1005	994	985	982	995	1006	1015	1018	1019	1019		1019	1019	1018	1004	1024	1010
30	1024		t .	5		1025		1	1009	1001	991	987	990	999	1005	1009	1015	1018	1020	3	1014	1017	1023	1021	1018	1011
I							1022					992	993	1000	1007	1013	1016	1020	1024	1026	1027	1026	1027	1027	1026	1016
Mean	1027	1021	1023	1023	1024	1024	1022	1010	1014	1005	994	772	993	1.000	1.007	1013	1010	1020	1024	4			'	i '		1
1	1	ı	ł	1	1	i 1	ļģ.	1	1	t .	1	t .	•		•	1						<u> </u>	-			

TERRESTRIAL MAGNETIC FORCE: WEST COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

244. Eskdalemuir. (-Y.)

				~							4,000	λ (.ο	4 C.G.S.	unit)	+											
Hour G.M.T.	0.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day. 1 2 3 4 5	γ	γ	9	γ	7	9	γ	γ	9	9	γ	γ	7	9	9	γ	γ	γ	γ	γ	9	9	γ	γ	9	9
	634	636	647	650	653	647	639	635	633	634	655	672	689	693	688	684	674	665	659	640	647	658	659	659	657	657
	655	654	653	650	650	647	642	640	637	641	653	662	676	683	681	675	667	664	663	662	669	661	656	657	655	658
	654	653	631	633	643	640	634	633	631	633	648	662	679	683	677	666	659	658	664	667	661	652	655	652	649	653
	648	647	648	646	646	646	640	632	629	633	639	648	668	676	669	666	654	654	652	653	653	653	653	652	647	650
	647	648	649	647	648	647	644	642	643	643	647	656	668	672	670	665	659	658	657	654	657	655	653	653	652	654
6	651	647	647	647	647	643	641	637	637	642	650	656	666	676	675	669	663	658	657	656	655	647	647	651	652	653
7 Q	652	651	651	651	647	646	644	637	631	633	635	646	663	673	671	662	656	657	654	654	652	651	650	651	650	651
8 Q	650	649	649	646	643	641	640	640	637	640	646	660	668	672	670	666	663	662	658	657	657	657	655	656	652	653
9 D	652	651	651	649	642	641	641	640	632	634	640	657	673	678	678	673	659	661	657	657	656	662	628	619	635	651
10 D	635	612	628	626	643	647	637	629	635	637	650	665	678	683	676	673	662	656	656	653	649	655	653	656	653	650
11	653	653	653	651	646	642	641	640	640	645	661	669	685	682	679	673	664	654	657	659	656	655	646	621	631	655
12	631	639	647	647	648	646	645	640	635	633	640	649	668	675	676	671	660	658	656	652	654	653	654	655	650	652
13	650	651	649	650	650	651	647	645	640	643	651	661	676	684	681	674	669	663	661	659	660	637	634	652	652	656
14	652	650	647	648	642	643	645	641	637	640	653	659	668	675	672	665	665	657	648	652	643	650	652	651	649	652
15	649	652	648	649	651	653	651	638	632	630	635	646	663	674	672	673	671	662	655	654	653	651	651	651	650	653
16 Q	650	651	651	648	647	644	637	636	631	639	643	658	673	677	677	669	657	651	652	655	652	652	653	651	649	652
17	648	648	647	646	646	645	638	630	628	634	645	659	668	668	664	662	662	656	655	658	665	657	651	662	645	652
18	645	639	650	645	644	645	645	640	636	638	645	655	661	670	671	668	667	663	661	660	653	649	645	652	654	652
19	654	646	646	646	646	646	641	637	636	638	643	647	656	663	665	658	656	656	657	660	656	654	653	653	647	650
20	647	646	650	641	645	645	645	640	636	640	646	658	665	668	667	664	657	656	654	653	651	644	648	649	648	651
21 Q	648	648	645	645	646	648	645	645	640	637	643	650	660	664	668	667	662	657	657	655	653	655	650	650	652	652
22 Q	652	653	652	653	653	651	649	643	634	630	635	652	672	676	674	667	660	656	655	659	658	652	653	649	644	653
73	644	642	638	637	641	649	642	638	637	638	644	658	676	681	675	669	665	659	652	656	654	651	651	650	650	652
24	650	645	645	636	650	643	639	637	636	639	647	656	666	669	667	660	653	654	658	660	657	655	646	645	646	650
25	646	646	645	650	638	640	644	640	638	641	648	653	659	667	665	668	666	660	661	660	656	640	641	650	650	651
26 D 27 D 28 D 29 30 Mean	650 525 584 655 652 642	651 500 641 623 632 640	651 537 684 634 639 644	660 609 616 633 637	657 629 626 638 644 645	672 662 631 640 645 646	662 677 636 641 645	661 624 632 641 641 638	666 631 632 637 636	649 633 631 634 633	645 653 642 636 638 645	658 668 652 644 642 656	665 682 665 654 651 669	680 671 667 666 660 674	671 668 669 669 659	677 675 663 663 658	680 671 650 657 658 662	682 668 652 656 657 659	656 584 651 656 661	656 554 647 653 659	635 591 642 652 646 651	560 610 636 651 647 647	546 626 640 647 645 645	514 589 638 648 645 643	525 584 655 652 640 643	643 624 644 647 647 651

245. Eskdalemuir. (Z.)

() B100 1093 01 TERRESTRIAL MAGNETIC FORCE: VERTICAL COMPONENT. Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

44.000 ν (·44 C.G.S. unit) +

September, 1923.

											44,000	γ (.44	C.G.S. 1	init) +	-											
Hour G.M.T.	О.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day. 1 2 3 4 5	964 966 954 954 954	γ 961 965 950 953 953	γ 962 965 944 953 953	965 965 953 953 953	965 965 954 955 953	γ 966 966 957 957 953	967 968 961 957 953	969 969 964 957 956	968 968 961 953 955	965 964 955 949 953	957 958 945 949 949	γ 955 954 941 945 942	955 953 941 944 941	954 956 942 945 941	957 960 951 949 946	965 965 957 953 953	976 965 957 959 956	981 965 956 959 957	983 965 953 957 957	985 965 954 957 957	981 961 957 957 957	972 961 960 957 957	968 961 958 956 957	966 961 956 954 956	966 954 954 954 955	967 963 953 953 953
6 7 Q 8 Q 9 D 10 D	955 953 953 953 945	955 953 953 953 938	954 951 953 952 938	954 953 953 950 942	953 953 953 950 942	954 953 953 950 941	957 953 952 952 945	957 953 953 950 948	953 952 952 950 945	949 951 950 950 945	950 949 950 949 944	950 947 946 944 942	949 942 941 938 942	946 946 937 940 946	950 950 941 943 954	953 953 945 949 961	953 953 949 950 961	953 955 950 950 957	953 953 950 950 955	953 953 949 950 954	953 953 950 953 955	954 953 950 952 953	955 954 952 949 953	953 954 953 944 953	953 953 953 945 953	953 952 949 949 948
11 12 13 14 15	953 949 948 953 949	953 949 950 952 949	953 949 950 950 949	953 950 951 950 950	953 950 950 950 950	952 949 950 950 949	952 950 950 952 950	950 950 950 950 952	948 949 949 948 949	945 946 945 945 945	942 944 941 942 943	944 940 937 941 940	944 939 937 938 933	945 941 942 942 934	946 945 949 949 938	952 950 949 952 942	957 953 949 954 949	957 954 950 960 953	953 953 952 962 953	950 953 953 958 953	952 953 953 953 953	953 953 960 952 950	954 952 957 950 950	952 949 953 949 950	949 948 953 949 950	950 949 949 950 947
16 Q 17 18 19 20	951 953 946 943 948	951 951 947 944 947	951 952 947 947 945	951 952 947 948 947	951 953 947 950 947	951 954 949 951 948	954 955 951 952 950	954 957 954 955 951	951 953 954 955 951	946 947 952 951 951	946 946 950 950 944	940 943 946 951 944	938 944 943 946 944	939 946 946 944 943	946 946 948 948 942	954 946 950 951 947	958 949 953 950 950	958 954 951 950 950	955 954 951 950 951	954 953 953 951 951	954 952 954 951 952	954 955 954 951 951	954 958 954 951 950	954 954 945 951 947	953 946 942 948 947	951 951 950 950 948
21 Q 22 Q 23 24 25	947 950 949 952 953	947 951 949 952 953	947 950 948 944 953	947 948 948 948 949	947 948 948 946 949	947 948 945 943 950	948 948 948 948 950	951 951 948 952 950	950 951 948 952 949	947 950 946 949 946	947 947 945 948 945	944 940 940 947 945	939 937 937 945 945	939 938 938 948 945	940 943 944 952 946	943 947 949 953 946	947 951 955 955 951	948 948 956 953 953	948 947 956 952 953	950 947 953 953 953	951 947 952 953 953	951 948 952 949 953	951 948 952 947 953	951 947 953 952 952	950 948 952 952 953	947 947 948 950 950
26 D 27 D 28 D 29 30	953 871 906 937 944	953 846 903 937 951	953 767 878 942 955	950 803 911 946 955	945 827 933 950 951	937 827 940 954 951	935 834 943 954 952	941 902 946 956 954	941 931 947 954 955	941 948 947 950 954	945 950 946 947 954	945 954 946 950 950	948 961 949 950 947	953 966 954 949 946	957 980 962 950 950	958 982 966 952 954	957 996 970 955 957	957 1026 971 958 958	967 1047 969 958 959	958 -962	969 981 966 958 969 957	961 973 962 958 967 956	933 918 951 958 962 952	899 874 946 958 959	905 937 944 958 947	947 924 946 952 955 950
Mean	947	946	942	945	946	947	948	952	951	949	947	945	944	945	949	953	957	930	000	337	557					

DAILY EXTREMES OF EACH COMPONENT OF TERRESTRIAL MAGNETIC FORCE: MAGNETIC CHARACTER FIGURES: TEMPERATURE IN MAGNET HOUSE.

246. Eskdalemuir.

September, 1923.

270.	Lonualt																		
							Terrest	rial Magı	netic Force.								racter ures.§	Magnetic Character	Temperature in
Day.		Nort	h Compo	nent.		1	Wes	t Compo	nent.		1	Verti	cal Comp	onent				of Day	Magnet House
7.	Maxim	um	Mir	imum	Range.	Maxim			nimum	Range.	Maxin			nimum	Range.	$\Sigma_{ m R^2}$	ρ	(o-2).	200 +.
	15,000	$\gamma +$		οο γ +		4,000 1			οο γ +	I	44,000			00 γ +					
	h. m.	γ	ν .	h. m.	γ	h. m.	γ	γ	h. m.	γ	h. m.	γ	γ	h. m.	γ	100γ²	0.45	0	a. 87·7
I	0 2	1041	990	11 8	51	12 37	698	625	0 40	73	19 12	988	953	12 30 12 20	35 16	92 85	0.45	0	87.7
2	23 54	1063	986	10 58	77	13 0	686	638	6 35	48	7 30	969	953 940	11 23	41	121	0.42	ī	87.7
3	ОІ	1058	985	12 7	73	12 53	690 681	619 621	2 20	71 60	20 53 16 53	961	940	12 10	19	102	0.50	î	87.7
4	20 50	1056	977	13 8 11 18	79 34	12 47 12 22	677	639	7 49 8 30	38	10 55	958	942	11 46	18	29	0.14	ō	87.7
5	18 19	1034	1000	11 10	9.4	12 22	0//	039	0 30	30	19 15	950	949	7. 7.		~9			, ,
6	20 48	1039	999	10 37	40	13 30	679	632	8 5	47	21 40	957	945	13 0	12	40	0.10	0	87.7
7	19 47	1039	995	11 4	37	13 29	677	630	10 10	47	17 0	956	941	12 10	15	38	0.19	0	87.7
8	20 II	1033	993	11 29	42	13 41	673	637	8 20	36	I 15	953	935	13 0	18	34	0.17	0	87.7
9	22 12	1096	991	11 32	105	13 20	683	600	22 42	83	20 28	953	938	12 0	15	181	o·89	I	87.8
IÓ	0 19	1051	972	10 52	79	13 20	690	603	0 52	87	15 22	964	937	1 45	27	145	0.41	I	87.7
11	22 40	1043	975	11 27	68	12 32	689	615	23 0	74	16 32	959	941	10 0	18	104	0.21	О	87.7
12	23 10	1037	980	10 55	57	13 42	678	628	8 41	50	16 40	956	939	12 30	17	6o	0.30	О	87.7
13	19 42	1045	989	14 29	56	12 29	688	628	21 49	60	21 20	961	935	11 13	26	74	o·36	0	87.7
14	19 50	1047	979	9 15	68	12 41	684	625	8 47	59	17 40	963	938	11 39	25	87	0.43	0	87.7
15	16 30	1035	991	10 40	44	13 6	680	629	9 5	51	17 32	956	933	12 25	23	51	0.25	0	87.7
16	18 45	1030	986	10 22	44	13 25	682	627	7 59	55	15 40	958	938	12 0	20	54	0.26	0	87.7
17	20 19	1046	987	11 16	- 59	20 19	669	627	7 8	42	22 20	962	943	11 32	19	56	0.27	0	87.7
18	22 40	1057	978	10 21	79	14 17	679	631	8 11	48	21 38	954	941	24 0	13	87	0.43	0 I	87·7 87·7
19	23 35	1042	990	10 59	52	13 53	670	635	7 44	35	7 50	955	942	0 I	13 13	41 39	0.10	0	87.7
20	22 11	1053	1003	10 30	50	15 31	670	635	8 0	35	21 5	953	940	13 48	13	39	0.19		
21	21 43	1036	1000	10 30	36	14 34	669	637	9 15	32	22 20	951	937	12 52	14	25	0.15	0	87.7
22	22 41	1049	988	11 14	61	13 20	677	628	9 22	49	8 o	952	936	12 30	16	64	0.31	0	87·7 87·7
23	15 38	1038	989	II 42	49	13 42	689	634	7 48	55	17 0	956	936	12 20	20 15	58 66	0.32	I	87.7
24	21 0	1058	990	11 0	68	12 15	674	632	8 48	.42	20 41	956	941	4 50 9 41	12	26	0.13	ō	87.7
25	21 3	1037	1001	10 40	36	12 59	669	635	7 22	34	20 50	954	942	9 41	12	20	0 15		1
26 .	20 53	1067	944 749	20 32	123	15 19	697	497	23 17	200	18 20	977	866	23 55	111	675	3.31	2	87.7
27	2 20	1097		1 42	348	22 16	745	443	1 36	302	17 33	1067	724	1 48	343	3300	16.17	2 I	87·7 87·7
28	23 49	1056	965	0 46	91	1 38	713	600	O I	113	16 32	974	871	1 59 0 28	103	295	1·45 0·21	0	87.7
29	24 0	1029	976	12 20	53	23 42	686	621	0 55	65	22 11	959	931	0 20	31	44 49	0.21	Ö	87.8
30	o 8	1040	985	10 40	55	13 10	671	621	0 45	50	20 0	970	939				<u>-</u>		87.7
Mean.		1048	978		70		684	616		68		964	928		37	204		0.37	
No. of Days	l	30	30		30	_	30	30	_	30	_	30	30		30	30		30	30
used.	-	30	ر ا		J-		J.	ي ا	1	"		"	"				1	[i
	<u> </u>	·	<u>'</u>				<u>. </u>	·	<u>' </u>										

[§] For explanation see page 105.

Q denotes an "International Quiet Day," while D denotes a disturbed day used for the computation of Tables 271-276.

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TERRESTRIAL MAGNETIC FORCE: NORTH COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

247. Eskdalemuir. (X.)

75.000 m/s 75.000 mi

October, 1923.

							1				15,0	00γ(•	15 C.G.	S. unit) +					,						
Hour G.M.T.	o.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day.	γ	Ιγ	Ιγ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ
Í	1018	1030	1026	1020	1 -	1020	8 -	1015	1010	1002	1000	995	996	1000	1000	1002	1009	1014	1 - :	1019		1019	1021	1016	1014	1012 1012
2 Q	1014	1015	1015	1015		1016		1016	1014	1005	996	995	996		1000	1001	1	1015	1020	•	4	1023	1021	1020	1020	1015
3 Q	1020	1019	-	1019			1019	ł .	1015	1009	1001	995	995 991	i .	1005	1015	1015	1023	1019		J	1020	1021	1021	1024	1013
4	1020	1020	1019	1019		1019	1019	1019	1015	1005	991	1000	1002	995 1005	1		1		1014			1018	1022	1020	1024	1016
5	1023	1023	1020	1017	1025	1025	1029	1027	1010	1013	1004	1000	1002	1005	1200,	1	13		' '	1 ′			ļ			
6	1024	1024	1023	1020	1023	1028	1023	1023	1020	1014	1009	1006	1003	1004	1008	1012	1017	1009	1018	1019	1018	1013	1017		1020	1016
7	1020	1021	1022	1023	1024	1037	· 1	1033	1025	1008	1004	996	994	995	999	1009		1017	1019	* -	I .	1019	1019	1019	1018	1017
8	1018	1019	1019	1024	1032	1043	1042	1132	1028	1017	999	985	980	985	981	999	-		1022			1023	1019	1021	1023	1015
9	1023	1023	1027	1024	1024	1029		1032	1022	1008	990	989	993	999	1003		1014	1014	1014			1019	1015	1020	1032	1015 1019
10	1032	1032	1020	1019	1022	1024	1023	1024	1028	1018	1007	1006	1009	1005	1013	1024	1019	1017	1019	1029	1027	1013	1010	1022	1019	1010
				7000	1007	1018			1018	1007	006	003	989	988	998	1005	1002	1004	1014	1018	1015	1020	1018	1021	1019	1012
11	1019	1015		1028		1010		1014	1011	997	996	992	999	· .	1009	1011	1013	1015		1024	1009	1009	1017	1017	1018	1012
12	1018		,			1024		1019	1014	1006	989	980	979	987	996	1007	1013	1018		1022	-	1026	1023	1022	1019	1012
13 14	1019	1018		1018	1022	1 3	re .	1023	1017	1003	987	980	984	998	1008		1	1027	1031	1032	1025	1022	1053	1024	1032	1017
15 D	1032	1023	ş.	1023	1 -	1 8	1023		987	955	973	980	983	966	936	978	970	994	965	998	1032	1007	974	969	1023	995
		`		_													1	0			000	007	045	054	921	981
16 D	1023	1032	1021	969	1017		1016	1022	1017	993	974	984	964	968	979	993	993	1018	944	925 1003	920	937	945	954	1008	991
17 D	921	979	989	978	995	959		974	984	999	1008	1002	993	990 1002	995	993	993	993		1013	1	1056	994	1003	1009	1000
18 D	1008	1013		1012			1007 1016		1008	984	988	993	999 1005	998	1003	1008	1008	1008	1	1007		1008	1012	1016	1017	1010
-	1	1013	1	1007			1015	1	1001	997	992	988	990		1002	1006	1005	1011		1021		1020	1035	1014	1012	1009
20	1010	1014	1013	1012	1012	1013	1015	1022	1001	997	992	900	334	99-				1		ĩ	1	ĺ				
21	1012	1011	1014	1016	1008	1011	1015	1017	1013	1008	998	993	993	993	997			1013		1019	,	1016	1017	1017	1018	1010
	1018	1017	1017	1016	1014	1015	1021	1016	1010	1002	996	992	993	996		1009			1014			1018	1025	1017	1019	1011
23 Q	1019	1012	1016	1016			1017		1016	1011	1003	1002	1003			1014		1016		1021		1021	1021	1021	1020	1015 1011
24 Q	1019	1016			1	- 1	1015		1009	997	988	987	994	1002	1008	1	1015	1015		1017	1	1019	1017	1018	1017	1016
25	1020	1017	1016	1020	1020	1020	1020	1020	1015	1010	1001	1001	1001	1006	1011	1020	1021	1022	1025	1024	1017	1014	101/	1010	101/	1010
-6		107/	T027	T027	1020	TOTO	1017	TOTE	1007	000	991	991	992	996	1005	1010	1014	1016	1018	1020	1021	1021	1020	1028	1020	1013
	1017	1014 1012	1031	1021	J	1019	1017	1015	997	999	1001	1000	1000					1015			l .	1025	1016	1016	1016	1014
27 28		1012	1		t	1	1016	1 ~	1011	1001	996	991	992	, ,,,		1	1017	1 -	1020		1020	1020	1019	1023	1027	1012
20	1026	1015	1015	1015		1017		1019	1010	1005	991	997	996	999	1005		1012		1019		1	1019	1019	1019	1019	1012
30 Q	1019	1019					1019	1 -	1014	1009	1000	999	1000	1004	1005	1010	1014	1019	1019	1023	1024	1023	1023	1022	1019	1015
3 ~	_	1	_				S S	İ							l				100	TOT 5	T004	1022	1021	1019	1011	1015
31	1019			1015		-	1020		1014	1006	996	992	1000			1			1024		1024		1	1		
Meant	1016	1017	1018	1015	1019	1018	1019	1020	1012	1003	996	994	994	997	1001	1008	1010	1014	1013	1015	1017	1017	1015	1015	1016	1011
•		l	L							1	<u> </u>	<u> </u>	<u> </u>					1	, ,	<u> </u>	1	l	<u> </u>		1	<u> </u>

TERRESTRIAL MAGNETIC FORCE: WEST COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

48. Eskdalemuir. (-Y.)

4,000 y (.04 C.G.S. unit) +

October, 1923.

248.	ESKQ	aiemi 5/	JIF. †	(—¥.	·)						4,00	ο γ (•	04 C.G.S	. unit) +											
Hour G.M.T.	0.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day. 1 2 Q 3 Q 4 5	9 641 646 646 646 647	9 639 646 646 642 646	γ 641 647 646 641 643	γ 641 646 646 641 651	9 636 645 646 641 647	635 645 645 640 645	9 639 643 641 641 649	γ 648 642 638 640 647	γ 639 637 636 636 643	γ 634 633 634 634 644	9 641 634 644 641 650	γ 646 640 647 652 660	γ 651 650 655 667 662	9 656 661 661 667 671	γ 656 662 660 665 671	9 656 659 658 663 671	γ 654 652 653 654 664	9 649 653 652 652 662	γ 651 655 652 652 662	γ 652 652 652 652 656	γ 652 652 652 652 651	9 652 652 652 652 648	γ 646 648 652 652 651	9 643 646 648 648 651	9 646 646 646 647 646	γ 646 648. 648 649 654
6 7 8 9 10	646 646 647 640 641	642 646 647 624 638	645 647 648 624 639	645 651 657 630 640	646 652 651 634 642	641 649 652 635 642	645 649 648 638 643	644 649 652 638 646	640 645 650 635 638	641 644 648 633 630	647 649 650 643 634	649 656 658 651 650	655 667 671 667 677	660 672 690 672 676	663 667 689 671 680	660 659 676 664 680	654 648 664 658 666	641 647 655 653 664	649 646 652 653 661	652 646 651 651 661	651 646 649 648 649	641 647 646 644 631	638 647 641 636 637	644 647 640 640 643	646 647 640 641 641	647 651 655 645 650
11 12 13 14 15 D	641 641 * 645 623	643 642 — 646 629	645 643 — 646 636	635 642 — 646 636	630 651 — 647 652	678 647 — 647 656	676 645 — 646 669	638 643 — 642 670	638 639 — 633 639	633 639 * 629 642	636 * 632 633 654	657 — 644 647 644	672 655 662 664	678 — 667 672 677	676 — 668 670 666	662 	660 657 663 661	656 	653 651 660 641	651 649 660 598	647 647 655 601	646 — 640 645 584	642 646 603 590	646 646 621 629	641 * 645 623 643	652 — — 647 640
16 D 17 D 18 D 19 D 20	643 568 633 644 638	614 574 642 646 638	624 582 637 647 637	630 611 634 654 642	662 661 627 653 638	684 688 631 641 637	694 668 638 642 640	668 665 658 641 636	658 662 649 638 632	647 637 648 642 629	648 637 649 650 640	657 645 650 665 643	652 661 661 672 653	666 662 661 661 656	669 672 664 656 657	662 669 657 650 656	620 657 640 648 650	587 648 630 648 649	585 645 643 655 650	567 642 647 627 640	558 624 612 627 641	566 610 581 637 640	505 618 614 644 635	530 635 640 643 630	568 633 644 638 637	623 641 640 647 642
21 22 23 Q 24 Q 25	637 645 637 641 646	648 644 642 643 647	642 643 643 646 647	638 642 643 645 646	641 642 643 644 646	648 647 643 644 646	647 641 646 643 646	647 641 647 642 645	637 636 642 638 642	632 629 639 636 638	634 635 643 649 643	643 648 654 664 655	656 660 658 673 660	661 659 659 671 661	661 664 658 663 659	659 655 648 654 657	654 648 646 647 652	652 652 647 647 652	652 652 646 647 655	648 648 647 647 652	649 647 647 645 648	644 646 646 646 636	644 640 646 646 631	643 638 642 646 630	645 637 641 646 634	647 646 646 649 ⁶ 47
26 27 28 29 30 Q	634 636 644 639 645	627 639 646 641 644	639 646 646 642 645	627 644 646 642 648	636 645 645 647 646	636 649 646 648 647	641 649 643 643 646	640 645 641 641 642	635 639 633 633 638	634 659 629 629 638	639 645 640 641 645	652 654 650 647 655	663 661 655 656 660	665 666 657 661 661	660 660 656 660 659	655 655 653 655 653	652 653 649 652 651	652 652 648 652 651	652 648 651 651 648	652 645 647 649 648	652 646 646 649 647	646 622 646 646 646	641 627 643 646 643	633 643 639 645 639	636 644 639 645 636	644 647 646 647 648
31 Mean†	$\frac{636}{639}$	642	643	642	642	640	637 648	637 646	637 640	$\frac{638}{637}$	650 643	657 652	667	672 666	664	670 661	656 653	656 647	656 649	652 645	605 640	630 635	630 632	632	638 638	645

* No trace; presumed defective paper. † Mean of 29 days; 12th & 13th omitted. Q denotes an "International Quiet Day," while D denotes a disturbed day used for the computation of Tables 271-276.



OB 1923/103/01/1940

TERRESTRIAL MAGNETIC FORCE: VERTICAL COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

October, 1923.

249.	Eskd	alemi	uir.	(Z.)	111 6	un ou	ines j	or por	, one		44,000	γ (·44	C.G.S. u	ınit) +										Octo	ber,	1923.
Hour G.M.T.	o.	r	2.	3∙	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day. 1 2 Q 3 Q 4 5	959 959 959 959 960 958	γ 955 959 959 960 957	γ 951 959 959 960 957	γ 954 959 959 960 956	γ 956 959 959 960 953	γ 956 959 959 960 954	γ 956 959 959 960 953	γ 953 962 959 960 953	955 964 959 960 956	955 964 958 956 956	953 959 951 956 952	953 955 949 952 951	955 951 948 949 949	956 951 950 952 949	958 955 955 952 953 952	959 959 956 956 956	963 960 959 960 960	γ 963 962 959 960 962	963 960 959 960 964	960 960 959 960 965	959 960 959 960 967	959 959 959 959 960 965	γ 959 959 959 960 962	959 959 959 959 960 961	959 959 959 959 958 959	957 959 957 957 958 957
6 7 8 9 10	959 958 960 958 955	957 958 960 954 950	956 957 959 951 954	956 957 957 951 955	956 957 953 952 956	956 953 949 953 956	956 949 942 953 955	956 949 945 954 955	957 950 949 954 954	955 951 953 954 955	952 951 954 950 954	952 952 955 950 946	952 950 953 950 942	952 950 953 951 946	952 957 958 955 947	954 961 962 962 953	959 965 966 966 955	964 964 965 966 962	961 961 961 963 962	960 961 961 962 959	960 961 961 962 962	961 959 961 962 970	961 959 961 966 967	960 960 961 962 963	957 960 957 955 963	957 956 957 957 956
11 12 13 14 15 D	963 963 960 959 946	962 963 960 960 948	958 963 960 960 952	956 962 960 960 952	955 957 960 960 947	942 955 959 960 945	927 955 959 960 943	942 956 959 962 938	946 959 963 963 952	946 959 963 964 957	947 960 963 959 956	944 959 960 955 956	946 955 958 952 957	947 955 955 955 966	951 956 958 956 988	969 963 960 959 1000	978 964 964 962 1020	974 963 963 960 1047	971 960 963 959 1035	967 960 963 959 1016	966 968 963 962 968	963 972 960 963 944	963 964 959 955 928	962 963 959 943 870	962 960 959 945 850	956 961 960 958 962
16 D 17 D 18 D 19 D 20	851 799 953 958 966	894 799 957 959 966	913 796 961 959 966	891 808 957 959 965	886 819 953 955 964	914 851 950 958 963	911 883 953 959 963	925 911 950 962 962	938 934 953 963 966	949 957 957 966 966	953 962 957 962 966	953 961 958 955 965	965 962 958 958 963	976 976 959 962 963	981 962 966 966	985 969 967 970	1049 992 981 970 971	1028 990 981 967 967	984 973 967 969	981 981 970 973 966	947 985 970 974 966	898 979 942 970 966	887 970 945 967 959	866 934 951 967 962	799 953 957 966 962	942 928 959 964 965
21 22 23 Q 24 Q 25	963 964 964 964 961	957 964 964 964 961	959 964 964 964 962	959 963 964 961 961	960 963 964 961 960	960 962 964 961 960	961 962 962 961 960	963 961 961 960	967 967 963 962 961	970 968 964 960 962	967 964 960 952 957	964 963 957 952 956	963 963 956 956 957	964 963 958 957 958	967 966 961 960 960	967 968 964 964 964	968 974 964 964 962	964 968 964 964 960	964 967 961 964 960	964 964 961 964 960	964 964 961 961 960	967 964 961 961 967	967 964 961 961 968	967 963 964 961 966	964 963 964 961 961	964 965 962 961 961
26 27 28 29 30 Q	962 961 963 963 965	962 962 964 962 964	953 962 964 963 964	950 962 964 964 963	954 961 963 964 963	957 958 963 962 963	960 958 963 962 963	961 958 966 963 963	965 965 966 966 964	962 961 966 963 963	960 958 962 962 960	958 957 962 962 960	957 957 963 964 963	961 959 965 966 963	965 964 966 967 967	966 966 967 970 967	967 967 967 969 965	965 967 966 966 965	965 968 966 966 965	962 968 966 966 964	962 966 966 966 964	962 965 966 964 964	964 965 966 964 964	965 962 966 964 965	961 962 963 964 964	961 962 965 965 964
31 Meant	964	963 952	963	964	963	964 952	964 952	964 955	964	964 959	960 957	959 956	959 956	960 958	963	964 967	963 971	964 971	964 969	967 966	975 964	968	963 958	963 954	963 951	964 959

DAILY EXTREMES OF EACH COMPONENT OF TERRESTRIAL MAGNETIC FORCE; MAGNETIC CHARACTER FIGURES: TEMPERATURE IN MAGNET HOUSE.

250.	Eskdale	muir.		MAGN	2110	0111111			TUKES									Octob	er, 1923.
							Terrestri	al Magne	tic Force.								racter ires.§	Magnetic	Temp erature
Day.		North	Compone	ent.		(West	t Compor	ent.		Ī .	Vertic	al Compo	onent.			1	Character of Day	Magnet
Luy.	Maxim	um	Mi	nimum	Range.	Maxin	num	Mi	nimum oo γ +	Range.	Maxii 44,00			nimum 000 γ +	Range.	$\Sigma_{\mathbb{R}^2}$.	ρ	(0-2).	House 200 +.
	h. m.	γΤ	γ	h. m.	γ	h. m.	γ	γ	h. m.	Ι γ	h. m.	γ	γ	h. m.	Ιγ	100γ2			a.
ı	0 35	1041	989	II 23	52	14 42	661	625	0 30	36	17 27	963	951	2 0	12	41	0.31	0	87.7
2	19 53	1025	991	10 52	34	13 23	666	629	9 16	37	8 55	965	949	12 40	16	28	0.14	0	87.7
3	18 55	1027	990	11 23	37	13 12	665	632	8 44	33	20 10	960	947	12 0	13	26	0.13	0	87.7
4	23 41	1026	987	10 59	39	13 17	672	633	8 20	39	22 30	961	949	12 10	12	32	0.19	, 0	87.7
5	6 10	1032	995	11 54	37	14 12	674	640	4 50	34	20 20	968	948	12 20	20	29	0.14	0	87.7
6	O 12	1032	999	16 40	33	14 14	664	635	1 6	29	17 4	964	952	12 5	12	21	0.10	0	87.7
7	5 41	1047	991	12 0	56	13 10	673	642	8 51	31	16 30	965	949	6 45	16	44	0.22	0	87.7
8	5 14	1051	975	11 42	76	13 16	696	637	23 0	59	15 53	969	941	5 40	28	100	0.21	1	87.7
9	23 58	1038	987	10 48	51	13 0	672	610	0 43	62	16 30	966	950	12 10	16	67	0.34	0	87.7
10	16 20	1041	1002	15 25	39	14 57	688	626	21 10	62	21 6	970	942	12 0	28	61	0.31	0	87.7
11	4 22	1043	980	12 51	63	5 18	691	627	4 4	64	16 o	978	923	6 0	55	111	o·56	1	87.7
12	5 50 } 18 42 }	1028	982	11 20	46	4 34	652	630	9 42	22	20 40	975	953	12 30	22	31	0.19	0	87.7
13	20 48	1032	975	11 29	57	13 47	672	629	9 45	43	16 20	964	955	13 30	9	52	0.26	0	87.7
14	22 0	1071	979	11 6	92	12 36	677	596	21 39	81	21 22	967	943	22 50	24	156	0.79	1	87.7
15	19 40	1110	901	13 49	209	15 20	732	525	16 33	207	16 28	1063	838	21 23	225	1372	6.92	2	87.7
16	16 50	1066	809	23 40	257	5 55	700	473	22 3	227	16 44	1061	770	23 42	291	2023	10.50	2	87.7
17	22 49	1060	906	0 42	154	5 12	712	524	0 45	188	16 10	993	791	1 38	202	999	5.04	2	87.7
18	20 38	1104	975	15 58	129	14 11	679	564	20 28	115	16 15	985	938	21 26	47	321	1.62	I	87.7
19	19 58	1025	969	12 29	56	12 22	682	600	19 26	82	19 48	978	954	4 5	24	104	0.23	I	87.7
20	21 48	1046	986	8 29	60	14 32	665	624	8 31	41	15 55	974	958	22 0	16	55	0.28	0	87.6
21	6 53	1025	992	12 53	33	13 39	663	628	96	35	9 0	971	956	1 5	15	25	0.13	0	87.6
22	22 12	1040	991	11 2	49	14 5	665	627	9 5	38	15 50	975	961	5 40	14	40	0.08	0	87.5
23	22 40	1026	1001	11 11	25	13 51	668	637	8 40	31	15 27	965	956	12 0	9	17 28	0.14	0	87.5
24	23 35	1020	986	10 47	34	11 50	673	634	9 10	39	15 30	965	952	II O	13	ľ	0.14	0	87.5
25	18 9	1030	1000	10 12	30	12 30	663	627	21 30	36	21 40	969	954	10 42	15	24	0.12	"	87.5
26	23 16	1051	990	10 48	61	12 20	667	620	2 50	47	15 40	969	948	2 34	21	64	0.35	0	87.5
27	20 33	1049	977	8 28	72	12 50	672	614	20 50	58	17 50	969	957	11 35	12	87	0.44	0	87.5
28	23 53	1031	990	11 10	41	13 56	660	628	8 55	32	15 50	968	962	10 58	6	27	0.14	0	87.5
29	20 25	1024	990	10 33	34	13 45	665	628	9 21	37	15 20	970	960	10 28	10	26	0.13	0	87.5
30	23 12	1027	996	10 30	31	13 2	665	637	8 30	28	15 0	967	959	9 38	8	18	0.09	0	87.5
31	20 22	1052	990	10 35	62	12 49	681	_594	20 20	87	19 58	979	959	12 0	20	118	0.60	I	87.5
Mean		1043	902		65		675	612	l —	63		976	901	<u> </u>	40	198		0.39	87.6
No. of Days	_	31	31	_	31	_	31	31		31	_	31	31	-	31	31	_	31	31
used.		3.	3.	 		of 29 day				1		1	1	tion see	1	1	<u> </u>	1	

TERRESTRIAL MAGNETIC FORCE: NORTH COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

251. Eskdalemuir. (X.)

November, 1923.

											15,	000 γ	(•15 C.G	.S. un	it) +											
Hour G.M.T.	о.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day.	Ι γ	Ιγ	γ	γ	Ιγ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ
Ĭ	1010	1019	1004	1011				1018	1014	1009	999	1000	1004	1011	1018	1019	1020	1023	1023		1022	1021	1021	1024	1027	1015
2 D	1027	1028				1038		995	1004	984	969	985	993	990	992	995		1002	1011		1011	1043	1004	1005	1012	1007
3	1012	1013				1012			1013	1000	999	991	980		1003					1017		1		1 _	1015	1008
4		1013				1019				1013	1005	1002	1008		1005		1012			1017	1	1	1018	1018	1018	1012
5 Q	1018	1017	1014	1017	1017	1021	1021	1021	1018	1018	1013	1008	1000	1012	1011	1009	1008	1012	1017	1017	1014	1013	1015	1017	1017	1015
6	1017	1016	1017	1021	1022	1024	1023	1021	1014	1012	1011	1008	1008	1012	1013	1013	1012	1015	1016	1022	1022	1025	1021	1022	1020	1017
7	,					1022		1022	1021		1	1005		1015			1013			1017		1016	1030	1025	1027	1017
8	_					1021		I .	1016		997	993				1012					1023	1022	1021	1021	1021	1014
9	,					1019			1019			1000	1002	1006	1011	1016	1017	1016	1021			1021	1021	1024	1021	1016
10 Q	1020	1020	1019	1020	1024	1025	1026	1025	1021	1015	1009	1006	1006	1007	1015	1020	1024	1026	1029	1029	1023	1022	1023	1025	1024	1020
~		l	1		1			_	l						İ	1		i					1			
II	1024					1030				1	1012	1009		1016		1024				1026		1023	1021	1023	1021	1023
12 D	í					1029		1		1 2	1016	1009	1012	ı	1022	1	1006		1000		1015	1	1030	1013	1011	1018
13	1				1016		9 -	1 -	l .	1	1005	1002	1002		1009	1010			1014			1 -	1008	1013	IOII	1013
14						1019		1020	1010	1002	994	994	1	1001		1009			1020	1021	1021	_	1016	1020	1019	1012 1017
15 Q	1019	1018	1017	1015	1019	1021	1024	1024	1022	1013	1009	1006	1004	1005	1000	1015	1019	1023	1023	1021	1021	1022	1021	1021	1020	1017
16	1019	8101	1018	1017	8101	1022	1023	1024	1024	1022	1019	1018	1016	1014	1014	1014	1008	1016	1014	1010	1016	1014	1007	1000	1000	1017
						1018					_										1018		1014	1017	1018	1016
18	_					1022				1017		1020		1018		1017			1021	1 -	1022	1021	1021	1018	1018	1020
19	1018		1		1026		1		1021	1017	1013	1012	1016	1018	1017	1016	1015	1017	1018	1018	1019	1021	1021	1018	1018	1018
20 Q	1017	1017	1017	1018	1020	1021	1021	1018	1015	1011	1006	1006	1007	1012	1017	1020	1018	1020	1021	1021	1021	1021	1021	1021	1019	1017
							i				[
21	_		1			1023			1018							1025					1	1	1022	1025	1022	1022
22 D	1021	1024				1020			1019				, ,			1021	1014						1004	996	996 1016	1016 1012
23	996		l .			1011			1015 1016			1010			1008				1018	5 ·	1016	1016	1015	1016	1018	1012
24 25 Ω	1015	1014 1016				1015						1			1019					1017			1019	1010	1010	1013
25 ₩	1010	1010	1017	1010	1019	1019	1020	1019	1010	1014	1010	1012	1015	101/	1010	1015	1013	1010	1019	1019	1010	1010	,	1019	1019	101/
26	1018	1018	1018	1018	1019	1021	1023	1023	1023	1017	1013	1009	1008	1013	1015	1014	1013	1014	1014	1014	1015	1014	1012	1013	1014	1016
	1014					1026					1024	1018	1017		1003	998	999	997		983	999		1014	1012	1027	1015
		1014	1011			1011			1004		نہ ا	1007	1002	1004	1002				1009			1008		1021	1016	1008
29 D	1016					1021			,	1008	999	996	997	990	1002	1013	1010	1007	1014		1016	F.		1032	1014	1013
30	1013	1015	1023	1036	1016	1015	1017	1014	1003	992	1003	1006	1003	996	1006	1011	1015	1016	1017	1015	1010	1018	1014	1013	1010	1012
Mean †	1017	1017	1016	1018	1019	1021	1022	1021	1018	1012	1007	1006	1007	1009	1012	1013	1014	1016	1017	1017	1017	1018	1017	1018	1017	1015
·	.	-			1	1	l							1		1		1	<u> </u>]	1	1	l			<u> </u>

TERRESTRIAL MAGNETIC FORCE: WEST COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

252. Eskdalemuir. (-Y.)

4,000 γ (·04 C.G.S. unit) +

November, 1923.

Hour G.M.T.	o.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20 .	21.	22.	23.	24.	Mean.
Day. 1 2 D 3 4 5 Q	9	γ	γ	γ	9	γ	γ	7	γ	γ	γ	9	γ	9	9	9	9	γ	γ	γ	γ	γ	γ	γ	9	7
	638	639	653	639	637	640	640	640	638	642	651	661	668	669	662	656	652	652	654	651	651	647	641	648	646	649
	646	649	642	647	650	643	664	714	681	662	655	662	656	655	655	650	647	649	648	646	642	605	590	612	606	648
	605	614	621	637	642	648	642	644	640	638	645	649	647	655	653	649	645	642	643	642	640	636	639	641	641	641
	641	640	641	645	640	637	639	638	637	636	642	649	650	648	647	642	646	646	646	645	642	641	641	640	640	642
	640	640	641	642	642	641	641	640	639	639	642	648	652	654	652	648	647	651	646	645	640	638	640	640	641	644
6	641	642	645	642	641	641	641	640	640	641	649	652	656	657	653	651	652	651	650	645	646	645	644	644	644	646
7	644	646	643	645	644	644	643	640	639	637	643	653	657	661	659	653	657	664	662	650	645	636	601	612	628	645
8	628	638	646	642	645	644	640	638	634	630	636	646	651	655	653	652	651	650	648	645	645	644	644	644	643	644
9	643	643	644	644	641	650	640	638	630	631	639	650	658	658	653	650	650	646	646	646	645	639	635	641	639	644
10 Q	639	644	645	650	651	650	649	645	639	636	640	647	654	658	657	655	652	650	649	649	646	640	642	640	640	647
11 .	639	640	644	644	647	645	644	644	643	637	640	646	653	659	655	650	650	648	648	647	644	639	642	635	638	645
12 D	638	644	644	648	647	643	642	641	637	639	643	645	655	659	654	655	655	657	650	636	617	617	593	611	627	640
13 .	627	637	639	644	645	644	642	642	641	640	647	654	660	662	661	656	647	653	641	645	633	622	610	608	634	642
14 .	634	642	644	645	645	643	643	640	635	635	642	649	654	654	653	646	645	644	644	638	639	639	639	639	642	643
15 Q	642	640	641	644	644	644	643	642	640	637	641	647	651	651	648	645	644	644	644	643	643	643	643	643	643	644
16	643	643	643	645	644	644	644	643	643	640	644	649	654	651	650	650	646	645	645	644	644	636	625	627	631	643
17	631	640	635	635	641	643	643	641	639	639	645	650	651	651	650	649	649	645	645	643	643	640	636	635	638	643
18	637	642	642	643	644	645	643	643	640	642	644	651	653	649	649	645	649	648	648	648	643	643	642	639	642	645
19	642	640	636	637	635	642	642	642	642	643	645	651	654	653	649	645	644	644	643	643	642	642	642	642	642	643
20 Q	642	644	644	643	644	643	642	639	638	640	645	655	655	655	649	643	643	643	643	642	641	639	639	639	639	644
21	639	639	643	644	647	646	643	642	642	641	648	654	651	649	648	648	652	652	652	648	643	642	643	642	639	646
22 D	639	639	642	642	640	642	642	641	639	638	641	645	648	651	648	648	649	659	657	659	656	634	636	601	600	642
23	600	609	628	638	639	642	640	640	638	635	638	645	652	652	650	646	644	644	643	642	641	638	638	638	638	639
24	638	638	638	638	639	643	638	637	638	634	640	646	653	653	648	644	644	644	643	640	638	638	638	639	642	641
25 Q	641	643	643	642	643	642	642	641	638	639	643	648	649	649	647	644	647	643	642	642	641	636	633	636	634	642
26 27 D 28 29 D 30	* 625 615 628 635	627 628 628 635	630 627 639 651	635 640 642 633	642 643 643 633	642 649 663 637	642 653 648 638	644 661 650 643	647 659 647 647	649 652 641 643	647 647 640 639	644 647 645 645 645	648 652 647 651 646	653 658 651 640 645	650 657 642 652 645	649 660 646 650 650	648 651 646 648 647 648	650 637 645 640 643 648	648 636 644 643 643	647 621 643 639 642 644	643 620 637 639 637 641	642 609 632 628 635	634 623 618 616 633	623 636 606 619 632	625 615 628 635 632	639 641 641 641 643
Mean †	634	638	640	642	643	644	643	645	642	640	643	649	653	654	652	649	040	040	040	044	"	033		~J~	~J 4	943

[†] Mean of 29 days; 26th omitted.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

253. Eskdalemuir. (Z.)

November, 1923.

				` ,							44	,000 y	(·44 C.G	S.S. un	it) +										•	
Hour G.M.T.	o.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day. 1 2 D 3 4 5 Q	963 960 958 963 966	955 956 945 962 964	951 957 935 962 964	952 957 947 961 962	960 956 953 961 962	964 957 951 961 962	γ 964 958 956 961 962	967 948 958 961 962	967 949 961 962 962	967 956 964 961 959	964 960 962 961 957	960 958 964 961 957	963 965 966 965 956	γ 963 968 966 966 958	γ 965 969 966 966	967 972 968 968 963	964 972 966 966 961	γ 964 972 966 966 965	963 970 965 965 965	γ 963 969 965 965 966	963 971 965 965 967	963 969 966 965 967	963 965 966 965 966	960 961 965 965 966	959 957 963 965 966	962 962 960 964 963
6 7 8 9 10 Q	966 965 957 965 964	963 964 959 964 964	962 964 962 964 964	962 964 963 964 964	962 963 963 964 961	962 963 963 962 961	962 963 963 961 961	963 963 963 963 961	963 963 964 964 962	963 964 965 965 964	962 964 963 965 962	962 964 963 965 962	962 964 967 965 964	963 963 971 968 964	962 966 971 969 965	963 965 970 970 965	963 966 967 969 964	963 968 964 968 964	963 971 963 967 962	966 972 963 965 961	966 970 963 964 962	965 971 963 965 962	966 974 964 965 961	965 966 964 964 961	964 957 964 964 961	963 966 964 965 963
11 12 D 13 14 15 Q	961 961 957 960 962	961 958 957 958 962	960 961 957 958 962	960 961 958 959 962	960 959 961 960 962	960 961 961 960 963	958 958 961 961 963	957 958 961 961 962	957 957 961 961 962	959 957 961 960 963	957 954 958 959 962	957 956 958 957 962	960 955 958 959 963	960 957 961 963 964	961 960 962 965 966	961 962 963 966 965	961 964 966 966 964	.962 968 966 965 964	961 972 967 965 963	961 977 965 965 962	961 974 969 965 962	960 969 967 962 962	960 960 964 963 962	960 957 963 962 962	960 957 960 961 962	960 961 962 962 963
16 17 18 19 20 Q	962 964 963 962 960	962 959 961 959 960	962 956 960 959 959	962 958 959 957 959	962 958 959 957 959	962- 959 959 957 959	962 962 959 957 960	962 962 959 959 961	959 962 959 959 961	959 959 959 959 963	956 958 955 955 958	956 958 955 955 957	957 959 956 957 957	958 962 958 959 959	959 962 959 963 961	962 962 959 961 961	965 962 959 960 959	966 962 959 959 959	966 962 959 959 959	964 962 959 959 959	965 962 959 959 959	966 962 961 960 959	967 963 963 960 959	966 962 963 960 959	964 962 962 960 960	962 961 959 959 959
21 22 D 23 24 25 Q	961 960 978 961 960	960 958 971 961 958	960 957 967 961 958	958 957 964 961 958	958 957 964 961 958	958 956 964 959 957	958 956 962 958 957	958 956 961 958 957	957 956 960 958 957	956 956 960 958 957	953 956 958 957 954	953 955 957 957 957	956 956 957 957 957	959 958 957 961 960	960 961 960 963 962	960 960 963 963 962	956 960 964 964 961	957 958 961 962 961	957 960 961 961- 959	957 960 960 961 959	960 967 960 961 959	960 972 960 961 958	960 975 960 959 959	960 980 960 959 957	960 978 960 960 957	958 961 962 960 958
26 27 D 28 29 D	957 961 938 955 946	955 957 938 955 948	955 957 941 955 946	956 954 943 953 938	957 954 947 951 936	955 953 949 947 943	954 951 950 943 947	954 948- 950 943 949	954 945 952 950 950	954 944 953 951 951	954 946 950 951 950	954 946 954 955 951	954 947 957 955 954	954 949 958 963 957	955 951 961 962 959	958 957 962 961 959	958 964 962 962 958	958 968 961 962 959	958 969 962 962 955	958 980 962 960 958	958 976 962 959 959	957 972 963 960 955	958 963 963 959 955	961 950 958 951 954	961 938 954 946 954	956 956 954 955 952
Mean †	961	959	958	958	958	958	958	958	959	959	957	958	959	961	963	963	963	963	963	964	964	964	963	961	960	961

DAILY EXTREMES OF EACH COMPONENT OF TERRESTRIAL MAGNETIC FORCE: MAGNETIC CHARACTER FIGURES: TEMPERATURE IN MAGNET HOUSE.

254. Eskdalemuir.

November, 1923.

	l						Terrestri	al Magne	tic Force.								acter ures.§	Magnetic	Temperature in
Day.			h Compo					t Compo					al Compo			Σ R²		Character of Day	Magnet House
	Maxim 15,000			nimum oooγ+	Range.	Maxim			imum oo γ +	Range.	Maxin 44,000			nimum oo y +	Range.	2 K-	ρ	(o-2).	200 +.
	h. m.	γ	γ	h. m.	γ	h. m.	Ι γ	γ	h. m.	γ	h. m.	Ιγ	γ	h. m.	Ιγ	100y2			a.
Ţ	18 32	1029	989	1 41	40	12 41	672	623	1 11	49	7 47	967	947	2 18	20	44	0.79	I	87.5
• 2	21 22	1082	941	9 48	141	6 55	728	564	21 48	164	16 38	973	945	7 10	28	476	8.51	2	87.5
3	I 29	1028	977	11 37	51	13 3	659	603	0 59	56	15 0	969	931	1 40	38	72	1.58	I	87.3
4	6 20	1022	998	11 53	24	13 13	653	635	8 30	18	15 20	969	961	10 0	8	10	0.17	0	87.4
5	6 45	1022	1004	15 49	18	12 36	657	637	20 40	20	20 50	967	955	11 50	12	9	0.19	0	87.3
6	21 28	1027	982	12 23	45	13 7	658	635	18 32	23	18 40	967	961	11 8	6	26	0.46	o	87.3
7	22 14	1040	993	17 25	47	18 o	670	588	22 30	82	21 55	975	955	24 0	20	93	1.67	I	87.3
8	19 25	1025	992	11 30	33	14 18	657	625	0 37	32	14 50	972	955	0 10	17	24	0.43	0	87.3
9	23 0	1027	999	11 0	28	12 34	662	629	8 48	33	14 28	971	960	5 33	II	20	0.36	0	87.3
10	19 16	1030	1003	11 40	27	14 19	660	635	90	25	14 30	965	960	6 40	5	14	0.25	0	87.3
11	6 34	1033	1007	11 21	26	13 32	666	633	23 15	33	17 5	963	956	7 40	7	18	0.32	o	87·1
12	21 40	1066	988	18 38	78	13 10	666	573	22 13	93	19 20	978	953	10 0	25	154	2.75	I	87.1
13	6 9	1029	995	15 50	34	13 6	668	599	22 30	69	20 0	970	957	I 45	13	6 i	1.09	I	87·1
14	19 50	1024	990	10 16	34	13 24	657	630	0 6	27	15 10	966	957	1 0	9	20	0.35	0	87.0
15	7 15	1025	1002	12 29	23	12 20	653	636	9 13	17	14 30	966	962	24 0	4	8	0.12	0	87·o
16	6 18	1025	1003	16 9	22	12 10	655	620	21 38	35	21 55	967	955	9 52	12	19	0.33	0	87.1
17	1 10	1034	1008	0 10	26	13 50	652	630	0 12	22	22 0	964	955	I 20	9	12	0.22	o	87.1
18	5 55	1027	1016	13 56	11	11 48	654	637	23 15	17	22 50	963	955	10 20	8	5	o·08	0	87.1
19	3 4	1027	1012	10 43	15	12 15	655	632	1 30	23	13 53	963	955	10 31	8	8	0.12	0	87.1
20	22 53	1022	1005	11 34	17	11 58	656	638	8 42	18	90	963	956	11 10	7	7	0.13	0	86.9
21	16 58	1047	1007	19 32	40	16 52	662	637	9 8	25	оі	961	951	10 42	10	23	0.42	o	86.9
22	16 49	1034	986	22 30	48	19 41	670	594	23 3	76	23 10	980	954	11 10	26	88	1.57	1	86.9
23	23 11	1021	987	0 29	34	12 22	659	604	I 20	55	0 I	978	956	11 40	22	47	o·83	I	86.9
24	22 0	1023	1009	10 42	14	12 52	654	634	9 10	20	14 20	965	957	12 50	8	7	0.13	0	86.9
25	23 27	1033	1009	10 28	24	11 50	652	630	23 43	22	14 10	962	954	10 0	. 8	11	0.50	0	86.8
26	7 30	1023	1004	12 3	19	13 20	653	621	23 32	32	23 50	961	953	8 5	8	14	0.26	o	86.8
27	7 59	1051	976	18 43	75	14 58	667	601	20 50	66	19 3	982	937	23 50	45	120	2.15	I	86.7
28	22 27	1041	992	9 58	49	7 18	665	599	22 22	66	21 59	965	937	O I	28	75	1.35	1	86.7
29	21 43	1066	978	12 30	88	5 17	682	609	21 50	73	13 25	968	940	5 33	28	139	2.48	1	86.7
30	2 32	1044	987	8 40	_ 57_	2 11	660	620	2 59_	40	13 59	962	935	3 50	27	56	1.00	I	86.7
Mean.		1034	995		40	_	663	618		44		968	952	· . —	16	56		0.43	87.1
No. of		1					1					1							1
days		30	30	_	30	_	30	30		30	_	30	30	_	30	30	_	30	30
used.	<u> </u>										•				<u>!</u>		<u> </u>	<u> </u>	<u> </u>

TERRESTRIAL MAGNETIC FORCE: NORTH COMPONENT.

124 0 0 6 Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

December, 1923. 15,000 γ (·15 C.G.S. unit) + Eskdalemuir. Mean. Hour 18. 21. 16. 19. 8. TT. Noon. 15. 17. 6. 9. 10. 5. 7. Ι. 3. G.M.T. Day. ν . 1017 τοτο TOTT 2 Q τοτο TOTO TOT 8 TOTO **TOT8** TOTO TOTO 1018 7 Q т008 1тот8 TOTO. aa8 TOT4 TOIL TOOT IOII TOTE IOII тот8 TOT 2 οτοτ TOT2 TOT2 т6 1012 IOII TOI 17 Q тотб 1018 1018 21 Q 1018 1016 1019 1019 22 Q 23 D 101Š TOT2 24 D 25 D 26 D тоо8 IOII 27 D 28 TOTE TOIT tot6 TOTE IOII

TERRESTRIAL MAGNETIC FORCE: WEST COMPONENT.

IOII

1014 1014 1013 1015

1013 1012

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

Meant

1014 1013 1013 1014 1018 1019 1019 1018 1016 1011 1008

256.	Eskd	alemu	ıir.	(Y .	.)			•			4,00	ο γ (·α	4 C.G.S.	unit)	+									ecem	ber,	1923.
Hour G.M.T.	о.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day. 1 2 Q 3 4 5	γ 631 632 639 637 633	γ 633 637 638 641 634	γ 643 639 642 641 633	γ 642 638 642 642 639	7 638 638 644 646 637	γ 639 639 642 647 631	γ 638 639 641 649 632	γ 638 638 639 650 634	γ 641 638 638 652 637	γ 634 638 637 648 634	7 638 639 640 648 638	γ 644 643 643 648 644	γ 648 648 649 657 645	γ 653 649 650 659 650	γ 651 648 651 673 648	γ 646 642 649 661 648	γ 643 642 643 646 648	γ 642 638 643 632 648	9 641 638 642 632 646	9 641 637 641 642 638	7 638 631 641 639 642	9 628 639 637 623 638	γ 631 639 633 632 637	γ 632 638 635 632 637	γ 632 639 637 633 637	9 640 640 642 645 640
6 7 Q 8 9	636 633 631 639 600	633 641 635 638 599	634 641 641 641 624	635 641 641 638 630	638 640 645 638 638	641 638 641 641 639		641 634 640 639 640	638 635 639 639 639	636 632 637 638 638	638 636 637 640 633	644 645 641 644 639	649 649 647 655 647	653 651 649 657 646	651 647 648 656 648	646 646 645 659 642	645 645 645 666 646	640 645 641 666 642	640 641 641 656 635	640 640 640 646 631	637 636 639 641 626	635 635 639 622 623	628 632 639 617 626	631 633 638 601 621	633 631 639 601 626	639 640 641 642 634
11 12 13 14 15	626 627 629 630 629	629 634 635 632 622	627 641 640 632 629	638 642 644 638 634	646 645 641 638 633	640 644 648 634 637	638 645 641	640 639 645 640 639	636 639 641 638 638	635 639 642 636 638	638 642 647 638 640	643 646 653 646 645	648 647 657 652 645	649 646 650 654 647	647 647 647 662 647	643 642 643 651 641	642 640 640 645 644	640 639 639 645 640	640 640 634 642 639	639 636 636 637 639	636 637 636 639 625	631 632 631 634 625	625 630 624 634 632	621 635 627 634 628	627 629 631 629 619	637 639 641 641 636
16 17 Q 18 19 20	619 635 634 633 629	622 636 635 631 638	632 639 636 628 638	635 640 639 633 639	635 639 639 633 638	639 639 639 641 637	638 638 638	639 638 638 641 637	638 638 638 640 636	640 637 638 638 630	639 639 638 639 636	641 640 639 643 640	641 640 643 645 645	641 644 645 645 647	641 641 644 645 644	640 639 643 643 639	637 638 639 639 637	636 638 639 629 637	635 638 638 628 637	635 638 642 631 636	635 637 642 632 633	634 634 631 633 633	634 636 625 631 629	634 635 637 632 628	635 634 634 629 629	636 638 638 636 637
21 Q 22 Q 23 D 24 D 25 D	629 633 633 634 617	628 633 632 635 628	633 634 635 638 632	638 633 636 638 637	633 634 637 637 634	633 636 637 638 636	636 636 638	636 634 634 638 635	636 633 633 641 633	637 635 632 635 628	639 635 633 644 629	643 642 638 639 635	645 644 644 641 638	647 643 648 638 640	645 642 648 656 643	644 639 647 652 640	638 638 648 647 626	638 638 652 627 631	637 637 646 636 635	637 637 640 639 633	633 634 595 627 605	633 632 624 624 628	632 633 629 623 622	632 633 631 622 610	633 634 618 614	637 636 636 637 630
26 D 27 D 28 29 30	614 616 622 632 628	621 629 623 634 631	642 629 623 635 631	623 633 639 638 631	644 651 645 634 632	638, 644 631 633 633	640 632 636	638 647 634 635 630	637 639 632 632 631	641 637 633 635 631	639 627 633 636 638	647 627 631 635 642	655 635 636 635 642	656 634 639 639 643	618 642 646 644 641	648 638 646 642 637	643 612 639 637 636	615 630 610 637 632	623 633 624 631 631	632 602 633 631 620	596 620 624 630 613	573 628 621 627 629	591 629 628 626 630	615 625 628 625 630	616 622 632 629 630	628 631 632 634 632
31 Mean†	630 629	632 631	642	632 637	631	630 638		632 638	630 637	631 636	636 638	639 642	643 646	648 647	647 647	642 645	639 641	$\frac{637}{638}$	637 637	631	630	631 629	630 629	630	631	635 637

† Mean of 29 days, 3rd and 4th omitted. Q denotes an "International Quiet Day," while D denotes a disturbed day used for computation of Tables 271–276.

TERRESTRIAL MAGNETIC FORCE: VERTICAL COMPONENT.

Mean values for periods of sixty minutes centred at the Hours of Greenwich Mean Time.

257. Eskdalemuir. (Z.) 44,000 γ (·44 C.G.S. unit) +

December, 1923.

201.	Laku	aiemi	air.	(2.)	`						44,00	λογ (.	44 C.G.S	. шис)	+										,	1323.
Hour G.M.T.	o.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Day. 1 2 Q 3 4 5	954 955 956 *	954 955 955 956	γ 951 955 955 - 956	γ 950 955 955 — 953	951 955 954 — 949	γ 954 955 955 946	γ 954 955 955 — 949	954 956 955 - 952	γ 953 955 955 - 952	954 955 955 955 *	953 951 * 952 952	γ 954 951 — 952 953	γ 954 951 — 953 953	954 955 — 956 953	955 955 955 953 956	955 955 955 — 959 956	958 955 955 960 956	γ 957 955 — 961 956	955 955 955 — 960 957	955 955 955 — 956 959	955 955 955 — 958 959	956 956 956 — 962 959	γ 956 956 — 961 958	γ 955 956 — 960 957	954 956 * 957 957	γ 954 955 — — 954
6 7 Q 8 9	958 957 953 949 963	957 954 950 949 958	954 954 949 949 951	954 953 949 950 950	953 953 946 949 947	953 953 946 946 946	953 951 946 946 946	9 53 9 51 9 46 9 45 9 47	953 952 946 945 947	955 952 949 946 947	954 951 950 946 950	954 953 950 946 951	957 953 950 946 951	957 953 950 948 951	958 953 950 950 950	957 953 951 950 956	957 950 950 953 953	957 947 950 957 955	955 947 949 962 955	954 948 948 962 954	956 949 947 968 954	955 949 946 975 956	957 950 946 973 955	958 950 947 969 954	957 953 949 962 951	955 951 948 954 952
11 12 13 14 15	951 948 944 952 950	948 946 944 949 945	947 944 944 940 943	947 945 944 942 945	947 946 944 944 946	950 946 944 945 946	950 945 944 945 946	950 944 944 945 946	949 944 944 945 946	947 941 944 945 945	945 938 943 944 942	946 938 944 941 943	947 942 944 941 945	947 946 947 945 946	951 948 948 948 949	952 951 951 949 950	954 952 952 952 950	951 952 952 953 950	951 952 955 953 949	950 952 955 953 950	950 952 955 953 954	951 952 956 949 954	951 951 955 949 952	950 948 955 949 951	947 944 951 949 944	949 947 948 947 947
16 17 Q 18 19 20	945 949 945 944 951	939 949 944 943 949	942 948 943 943 948	944 948 943 942 948	946 948 942 940 948	947 948 942 939 948	947 948 942 939 948	947 948 942 939 948	947 948 942 939 948	947 948 942 939 948	943 945 942 937 944	944 945 940 939 943	946 945 939 939 942	945 945 939 940 944	946 945 939 943 944	947 945 940 944 944	947 945 942 946 944	948 945 942 947 944	948 945 942 949 944	947 945 940 947 944	947 945 940 946 944	947 944 942 946 944	947 944 940 946 945	947 943 939 946 943	947 943 940 946 944	946 946 941 943 946
21 Q 22 Q 23 D 24 D 25 D	950 947 945 946 945	947 944 945 945 944	948 943 943 942 941	946 943 942 942 941	946 943 942 942 942	946 943 942 941 941	946 943 942 941 941	946 943 941 941 941	945 943 941 937 941	943 942 941 937 941	943 · 942 939 934 941	942 942 938 937 941	943 943 937 941 941	947 943 939 943 944	947 943 941 946 945	947 945 942 949 949	948 946 942 951 957	948 944 942 958 957	947 944 942 954 953	947 943 947 954 953	947 944 966 954 953	947 945 961 953 945	947 946 951 950 945	947 946 946 949 944	947 946 946 946 941	946 944 944 945 945
26 D 27 D 28 29 30	941 940 935 941 935	941 924 935 940 935	933 929 935 940 935	928 935 933 939 935	929 936 933 940 935	928 935 936 940 935	932 937 938 940 935	936 937 937 940 935	936 937 938 940 934	936 942 940 939 934	937 946 940 937 931	941 949 941 938 931	941 945 940 939 931	945 946 940 939 931	961 948 943 943 934	962 950 945 943 938	969 954 947 942 939	978 949 949 941 939	969 949 951 943 939	958 948 949 940 940	958 945 952 941 940	949 941 947 940 938	941 941 944 940 938	941 941 943 936 935	940 936 941 936 935	945 942 941 940 935
31 Mean†	935 948	934 946	934 944	931 944	934 944	934 944	935 944	935 944	935 944	935	935 943	936 944	935 944	935 945	938 948	939	939 950	939	939 950	939 950	939 951	938	$\frac{935}{949}$	935 948	934	936

DAILY EXTREMES OF EACH COMPONENT OF TERRESTRIAL MAGNETIC FORCE: MAGNETIC CHARACTER FIGURES: TEMPERATURE IN MAGNET HOUSE.

258. Eskdalemuir.

December, 1923.

																			.,
							Terres tria	al Magne	ic Force							Char Fig	acter ures.§	Magnetic	Temperature
Day.		Nort	h Compo	nent.		1	Wes	t Compo	ent.		<u> </u>	Vertica	al Compo	nent.				Character of Day	in Magnet
	Maxim			imum	1	Maxim			imum	í	Maxir			nimum	T	Σ R ²	ρ	(o-2).	House
	15,000	$\gamma + $		00γ+	Range.	4,000)			ογ+	Range.	44,000			ροο γ +	Range.		<u> </u>	·	200 +.
	h. m.	γ	γ	h. m.	γ	h. m.	γ	γ	h. m.	γ	h. m.	γ	γ	h. m.	γ 8	100γ ²			a.
I	15 28	1022	999	II 44	23	13 2	655	623	21 28	32	16 o	958	950	3 0		16	0.30	0	86.5
2 .	17 20	1019	1005	0 20	14	12 10	650	625	20 0	25	20 0	956	951	11 10	5	8	0.12	0	86.5
3	22 25	1023	1007	16 27 11 13	61	12 34 13 35	654 680	632 607	22 40 21 16	22	21 20	964	950	9 43	14	92	1.69	0	86·5 86·5
4	6 23	1037	976 1003	10 10	17	17 3	653	628	I 59	73 25	21 38	960	945	5 2	15	92	0.21	0	86.5
5	4 55	1020	1003	10 10	1 1	1 7 3	933	020	1 59	~3	21 30	900	943	3 2	13	-11	0 21	Ŭ	00.3
6	13	1022	999	11 20	23	13 10	654	623	22 28	31	22 16	959	953	4 30	6	15	0.28	0	86.5
7	19 16	1023	1002	10 32	21	12 39	652	630	23 48	22	0 10	958	946	17 20	12	ΙĬ	0.20	О	86.3
8	19 11	1031	1004	10 45	27	13 38	651	630	0 23	21	15 0	951	945	7 20	6	12	0.22	0	86·1
9	7 15	1030	967	20 13	63	16 26	676	596	22 40	80	20 20	977	944	7 20	33	115	2.10	I	86∙1
10	18 29	1036	993	9 43	43	11 46	649	583	0 20	66	ОІ	963	943	4 55	20	66	1.31	I	86.2
11	6 5	1010	995	3 13	24	12 19	652	619	22 49	33	15 50	955	945	9 50	10	18	0.32	o	86·o
12	23 52	1029	1007	19 55	22	13 33	651	626	0 30	25	18 35	953	937	10 32	16	14	0.25	o	85.9
13	5 42	1029	994	13 0	35	12 0	659	617	22 22	42	22 22	957	942	9 50	15	32	0.59	О	85.9
14	1 48	1036	979	13 42	57	14 8	666	618	2 18	48	19 4	953	938	2 0	15	58	1.06	1	85.9
15	23 43	1061	998	20 10	63	13 53	650	615	20 30	35	2Q 30	955	942	1 30	13	54	0.98	I	85.9
16	от	1026	1006	12 32	20	11 40	645	617	0 49	28	17 10	949	939	0 40	10	13	0.23	o	85.8
17	21 26	1028	1012	1 21	16	13 0	645	629	21 28	16	ог	949	942	23 4	7	6	0.10	0	85.9
18	21 43	1054	1011	1 21	43	13 11	647	616	21 58	31	0 1	946	939	12 40	7	29	0.52	0	85.4
19	8 31	1034	1009	17 26	25	12 20	647	619	17 36	28	17 43	950	936	10 0	14	16	0.29	0	85.3
20	22 28	1039	1008	23 40	31	12 19	648	623	23 13	25	0 10	951	941	22 32	10	17	0.31	0	85.3
21	8 53	1025	1000	13 12	25	12 29	651	626	1 10	25	16 o	949	942	10 50	7	13	0.24	o	85.3
22	0 16	1027	1012	13 0	15	11 25	645	627	0 39	18	0 1	947	940	9 30	7	6	0.11	0	85.3
23	18 6	1031	965	20 40	66	17 10	654	558	19 50	96	19 58	968	937	11 20	31	145	2.66	I	85.2
24	8 29	1042	969	12 58	73	14 20	666	620	17 3	46	17 8	962	934	10 9	28	82	1.20	I	85.1
25	20 3	1037	973	16 48	64	14 42	650	57 ⁸	19 51	72	16.50	959	940	9 55	19	96	1.76	I	85 ⋅ 1
26	20 51	1090	936	13 50	154	2 14	666	530	20 36	136	17 0	982	924	2 32	58	456	8.33	2	84.9
27	$\begin{bmatrix} 8 & 12 \\ 23 & 28 \end{bmatrix}$	1047	963	10 18	84	4 30	658	596	15 52	62	16 3	957	920	1 14	37	123	2.24	1	84.9
28	20 39	1028	987	12 48	41	3 50	650	587	17 12	63	20 23	953	932	3 52	21	61	1.11	1	84.9
29	23 0	1032	992	12 33	40	14 33	648	617	21 45	31	14 40	944	935	23 40	9	26	o·48	0	84.7
30	7 53	1022	1006	16 12	16	13 24	647	609	19 51	38	19 40	941	930	12 40	11	18	0.33	0	84.7
31	4 49	1021	1002	2 0	19	2 19	653	626	19 11	27	17 40	939	930	2 35	9	12	0.31	0	84.7
Mean.		1033	998		40		654	611		43		955	940		16	55	\ <u> </u>	0.39	85.7
No. of																			
Days	_	31	31		31	-	31	31		31	-	30	30	-	30	30		31	31
used.	<u> </u>		<u> </u>	<u> </u>	1	<u> </u>		l	1	1	l	}		1		l		1	l

^{*} No trace; lights out of adjustment.

[†] Mean of 29 days, 3rd and 4th omitted.

[§] For explanation see page 105.

DIURNAL INEQUALITIES OF THE GEOGRAPHICAL COMPONENTS OF MAGNETIC FORCE.—"ALL" DAYS.

 $(Not \ corrected \ for \ the \ effect \ of \ the \ North \ Force \ on \ the \ West \ Magnetograph, \ or \ \textit{vice versa}, \ or \ for \ the \ effect \ of \ the \ Horizontal \ Force \ on \ the \ V.F. \ Balance.)$

Mont	h		our.	G.M.T. 2.	3.		4.	5.		6.	7.		8.	9.		10.	11.	Noo	n 13	3.	14.	15.	16	. :	17.	18.	19	.	20.	21.	22.	23.	24.
and Seaso			259.	NOR Es l	TH kdal	CC)MP uir.	ON	EN	Τ (all da	ys	exce ₁	bt Ja	n.	1 7, 1	Marci	h 14,	15, A	pri	l 27,	28, ,	Tune	11, 1	12, 1	13, Oc	t. 12	2, 1.	3, N	ov. 26	, De	c. 3, 4). 923.
Jan. Feb. Mar. April May June July Aug. Sept. Oct. Nov. Dec.		-+++++++++++++++++++++++++++++++++++++	3.7 - 4.1 - 8.7 - 2.8 - 6.3 - 6.7 - 4.4 - 1.7 - 1.4 -	- 2·3 - 3·9 - 5·6 - 2·1 - 4·2 - 3·5 - 6·0 - 6·1 - 7·1 - 0·9 - 0·1	+ 3 + 3 + 4 + 4 + 6 + 4 + 2 o	·4+++ ·9++++ ·6++++ ·5++	3·9 4·2 4·7 3·6 5·0 3·3 5·5 7·8 7·7 3·6 1·3	+ 8 + 6 + 8 + 4 + 7 + 7 + 7 + 5 + 4	3·1 - 5·1 - 3·2 - 4·0 - 5·7 - 1·3 - 1·3 - 1·3 - 1·5·6 - 1·5·6 - 1·5 - 1·5 - 1·5·6 - 1·5 - 1 ·5 - 1 ·5 - 1 ·5	+ 9:4 + 7:7 + 10:1 + 2:6 + 3:5 - 5:8 - 8:1 - 5:6	9 + 8 7 + 6 7 + 6 7 + 6 7 + 6 7 + 6 7 + 7 8 + 7 8 + 7 8 + 7 8 + 7 8 + 7 8 + 7 8 + 7 8 + 7 8 + 8 8 + 7 8 + 8 8 + 7 8 + 8 8 8 + 8 8 + 8 8 + 8 8 + 8 8 + 8 8 + 8 8 + 8 8 + 8 8 + 8 8 + 8 8 +	·6 - ·6 - ·1 - ·1 - ·5 + ·9 +	+ 5·11 + 2·5 + 0·3 - 6·2 - 5·7 - 5·5 - 6·8 - 2·7 - 1·4 - 2·6 - 5·1	- 0 - 4 - 10 - 11 - 13 - 11 - 15 - 11 - 7 - 2 + 2	·9 - ·1 - ·2 - ·9 - ·3 - ·6 - ·9 - ·9 - ·9 - ·9 -	- 9·3 - 14·2 - 23·3 - 20·1 - 21·6 - 16·7 - 23·3 - 22·0 - 15·1 - 8·3 - 2·5		9 -14 3 -20 6 -28 4 -20 7 -25 3 -20 4 -21 7 -23 1 -16 2 - 8 9 - 6	·3 — I ·4 — 2 ·4 — I ·3 — I ·9 — I ·8 — I ·6 — (5·2 7·3 2·0 6·8 9·3 5·2 6·2 6·3 6·3 6·3	- 7·1 -11·0 -13·5 - 9·8 -10·5 - 9·3 - 9·0 - 8·8 -10·3 - 3·7 - 3·5	- 3° - 2° - 7' - 3° - 2° - 3° - 2° - 3° - 2°	9 - 19 - 19 - 19 - 19 - 19 - 19 - 19 -	1·1 — (·8 + + + + + + + + + + + + + + + + + + +	0·4 2·1 7·4 11·9 10·2 5·2 7·0 4·1 3·5 0·3 1·3	+ 1·3 + 4·4 + 9·1 + 17·4 + 14·3 + 12·1 + 9·8 + 7·9 + 2·5 - 0·0	+ 2 + 6 + 12 + 15 + 15 + 14 + 12 + 19 + 14 + 1	··3 + ··2 + ··9 + ··6 + ··6 + ··9 + ··6 + ··9 +	- 0.4 - 6.6 - 11.9 - 12.5 - 15.0 - 13.4 - 10.5 - 5.7 - 1.4 - 1.2	+ 4.7 + 8.3 + 13.1 + 10.1 + 10.1 + 10.1 + 9.9 + 10.1 + 6.0 + 2.6 + 1.1	+ 4 + 9 + 13 + 8 + 9 + 10 + 4 + 1 + 0	8 + 2. 8 + 3. 7 + 8. 3 + 10. 9 + 10. 1 + 7. 4 + 9. 5 + 8. 6 + 10. 2 + 4. 8 + 2. 5 + 0.	7 1 + 0. 1 - 0. 1 + 7. 2 + 10. 3 + 6. 8 + 8. 1 + 7. 8 + 8. 5 + 10. 5 + 1. 4 + 0.
Year																			ł													0 + 6.	
Winter Equinox			- (1					- 1		}					- 1			1									- 1	- 1		ĺ	4 + 8	
Summer		İ	-	1							ļ							İ		- 1		1	1	- 1				- 1	- 1		ì	ł	
260.	Esi	kda	lemu	ir.																										Dec.		1	923.
Jan. Feb.		 - -	1·0 —	γ 1·5 - 4·3 -	γ - 2·2	4 -	γ 0·4 3·8	- ο·	·1 +	γ 0·1	- ο·		γ 0·6	γ - 2·	3 -	ο.δ λ	γ + 2·6 + 4·2	+ 8·	1 + 11	·7 -	γ -10·9 - 16·3	γ + 8·1 + 11·5	γ + 5 + 8	4+	3.5	γ - 0.4	γ - ο· - 2·	6 _	γ 3·2 5·0	γ - 8·0 - 8·3	-11·3 - 8·	β — 10· — 9·	γ - 6.8
Mar. April		- 4	·6 -	5.6 -	- 7:3	3 -	5.8	- š·	·o —	5.2	- 7	3 -	10.0	$-11\cdot$	1 —	6.2	+ 4.3	+16.	7 + 23	.2 +	-22.2	+18.4	+12	8+	5.8 -	- 1.4	- o.	8 —	1.8	- 5.5	— 8⋅9	- 9·5	7.2
May June		2	ı·8 —	4.0	- 7:	1	9.0	-13.	·3 -	16.1	18.	3 -	19.3	- I7·	o —	10.6	+ 0.3	+12.	2 + 18	.3 +	-20.7	+19.1	+16	5 + 1	5.1 -	-11.2	十 7:	3 +	3.6	+ 1.3	+ 0.7	- 0·8 - 0·8	3 − 5·8
July Aug.		- 2	2·5 —	5·6 -	- 8·	5 -	8·6 9·2	-11·	· I —	16·7	-19·	3 -	20·5 18·5	19· 15·	4 — 5 —	7.6	- 2·9	+16·	0 +18 9 + 23	·1 +	- 22·1 -23·6	+20.1	+15 + 12	9+1 3+	1·4 -	-II·5 - 5·I	+ 9·	0 3 +	5·9 -	+ 4·8 + 1·0	+ 2·2 - 0·3	$\begin{vmatrix} -1 \cdot 3 \\ -2 \cdot 8 \end{vmatrix}$	- 2·0
Oct.	•••	- 7	·9 —	6.3 -	- 4.8	8	1.8	+ 1.	·6 +	1.8	o.	3 -	6.2	— 8∙	8	3.2	+ 5.5	15.	6 +19	∙9 +	- 18.7	+15.2	+ 6	6+	0.7 -	- 3.0	- I.	5 -	6.4	-10.5	—13 ·7	- 8·1 - 9·6	7:5
Nov. Dec.																																- 8·2	
Year	•	- 5	5.5	4.2	- 4.6	9	4.6	– 5·	-2	7.2	– 9·	2 -	11.4	-11:	8 –	6.5	+ 2:4	+12.	6 + 18	-3 +	18.9	+15.7	+11	3 +	7.5	- 4.7	+ 2.	2 -	o·8	- 3.7	— 6·c	- 6.5	— 6·ı
Winter		4	·8 –	2.5	- 1.8	3 -	0.7	– o.	3	0.3	+ 0.	6 –	1.0	- 2.0	5 –	0.3	+ 4.4	+ 9.	3 + 12	.0 +	-11-4	+ 8.3	+ 5	8 +	3.2	- 1.2	— 1·	0 -	4.7	- 8.2	—10 ∙(- 9.9	— 8·r
Equinox		- 7	·1 -	6.5 -	- 6.3	3	4.2	_ ₂ .	9-	4.6	– 8·	5 —	12.8	— 13 ·	9 —	7.5	+ 3.5	+16	3 + 23	· 3 +	22.7	+18.5	+11.	9+	6∙5 ⊣	- 2.9	+ o.	7	2.3	- 5.7	8.8	8.2	- 6.8
Summer	•••	— <u>3</u>	3.7	4.2 -	- 6.6	<u> </u>	8.4	-12	5	16.8	— 19·	8 –	20.6	— 18·	8 –	11.8	- o·7	+12.	1+19	.7 +	22.4	+20.5	+16	3 + 1	2.7	- 9.9	+ 7	0 +	4.6	+ 2.7	+ 0.8	- 1.4	- 3.3
261.			ΓIC <i>A</i> emu		COM	PO	NEI	T	(all	day	s exc	ept	Jan	. 17,	M	arch	14, 1	15, A ₁	pril 2	7, 2	28, J	une 1	1, 12	2, 13,	, Oci	2. 12,	13,	Nov	. 26,	, Dec.	3, 4		23.
Mar.		3 5	·7 — ·0 —	2·9 -	- 6·3 - 6·4		4·8 - 5·5 -	- 4·1	9 — 0 —	3·3	- 4·0	7 —	3.5	- 2·0		3.6	- 3·4 - 6·3	- 3·9	$- \frac{2}{6}$	7 + 7 - 0 -	0.8	+ 4·7 + 3·9	+ 6 + 8	$\begin{vmatrix} 6 + 1 \\ 8 + 1 \end{vmatrix}$	7·7 ∃ 2·4 ∃	- 7·9 - -11·5 -	+ 7°:	3 +	7·3 -	- 4·9 - 6·3	+ 1.6	γ + 2·1 + 0·5 + 0·2	- 2·2
May		- ž	4 -	3.6 -	- 2.8	-	1.0	+ o·:	2 +	0.5	+ 0.5	5 -	1.6	- 4.0	—	7.9	-10.2	-11.8	9	0	4.3	+ o·3	+ 3.	9 + 2	7:3 +	-11.5	+11:3	3 + 1	[0∙3]	- 7.7	+ 5.3	+ 1·1 + 2·1 + 1·5	- I.o
July		— І	·8 —	3.2	- 2.7	·	1.5	- I:	3 -	0.7	+ 0.6	6	0.4	– I.Ò) 	4.9 -	- 6.3	− 7·7	— 6·	3 -	3.7	— 1⋅3	+ 2.	5 + 6	6∙0 +	- 7.1 -	+ 7⋅6	3 +	7.4	- 6.0 -	+ 4.0	+ 1.5 + 1.7 + 2.1	+ o.6
Sept.		- 4	·5 —	8.3 -	- 5.3	-	3.8 -	- 3·6	6 –	2.1	+ 1.6	1	1.3	- o·€		2.6	- 4.9	- 6.3	- 4·	9 -	0.6	+ 3.3	+ 6.	6 + 8	8-4 +	- 9.0 -	+ 7·1	(+	6.9	- 6.0 -	+ 2.4	- 1·7 - 4·5	— 3⋅3
Nov.		— 2	.3	2.9 -	- 3.0) —	2.6 -	- 2.	4 -	2.3	- 2.4	1	2.1 -	- 1.5	:	3.1 -	- 3.0	- 1·4	ı[+ o⋅	7 +	2.2 -	+ 3.0	+ 2.	9 + 9	3·I +	- 2.9 -	- 3.3	3∤+	3.7/ →	- 3.4 -	+ 2.0	+ 1·2 + 1·8	— 0⋅3
Year		— 2	-8	3.8	- 3 ·8	-	3.1	- 2.7	7	2.3	— r ∙ı	-	1.0	– 1·ç	-	4.0	- 5.8	– 6 ⋅6	4.	7 -	1.1	+ 2.7	+ 5.0	5 + 7	7·3	7.9	⊦ 7·3	+	6.8	- 5.0	- 2.8	+ 0.7	- 1·4
Winter		– 1	-9	2.6	- 3⋅8	-	3.3	- 3:3	3	3.3	– 3·1	-	2.7	- 2:2	_	2.8	- 3.0	- 2.6	_ ı·	2 +	I · I	+ 3·3	+ 4.	2 + 4	1.7 +	4.8	⊦ ₄ .8	+	5·1 +	4.2	⊦ 2·7	+ 1.4	– o·3
Fquinox		- 5	- 0	6.3	5.5	-	4.9	- 4.1	1	3.0	- o·5	+	0.5	- 0.2	-	2.9	5.5	– 7 ·1	— 5·	2 -	0.4	⊦ 4·4	+ 8:	+10)· 1 +	10.0	⊦ 8∙3	+	7.4+	4.9	⊦ 1 ·9	- I·2	- 3 ⋅8
Summer		— 1	-5	2.5	2.1	_	1.1	- o·6	6 –	o·5	+ 0.3	-	0.7	- 3.2	-	6.3	- 8.7	10 ·1	- 7	8 –	3.9	⊦ o·3	+ 4.4	+ 7	··3 +	8.9	⊦ 8.7	+	7.7	5.9	F 3·7	+ 1.9	0.0

DIURNAL INEQUALITIES OF THE MAGNETIC COMPONENTS, DECLINATION, INCLINATION, AND HORIZONTAL FORCE.—"ALL" DAYS.

		Hour.	G.M.T.		T		7			l ,	<u> </u>	Ī	l	Noon	1		15.	16.	17.	18.	19.	20.	21.	22.	23.	24.
Mont	h	1.	2.	3.	4.	5	j.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	10.	1/.	10.	-9.					<u> </u>
and Seasor			DE	CLIN	ATIC	N (meas	sured	l posit	tive to	ward	s the	West)	(all de 3, Nov	ays ex	cept J	an. 17	, Mar	ch 14,	15, A	l <i>pril 2</i>	27, 28	, June	11, 12	2, 13,	
		262	. Es	kdale	muir.							Ocī.	12, 1	o, IV 00). 20,	Dec. o	·, ')·						 -	 , -	19	923.
Jan.		-0:74	-0.27	-0:4'	7-0:1	7 -0	,)·23 –	-0.30	-0.37	_0·42		+0.07	+0.03	1+2.07	+2.62	+2.28	+1.69	/ +1·14	+0.75	+o·46	_o·13	_o·68	8 -1.63	-2·40	-2.20	-1.36
Feb. Mar.	•••	—1. 03	-0.99	-0.9	-0.0	8 – 1	.10	- 1 • 04	-0.49	-0.72	-0.74	+0.34	+1.54	1+2.91	+3.78	+3.05	+2·49	+1.04	+1.03	-0.13	-0.50	-0.7	4 - 1.56	-2.32	-2.34	-1.82
April	•••	-1.59	-1.79	-1.3	4 - 1.2	8 -1	1.53	-2.10	-3.21	-4.00	-3.03	-1.05	T 1 34	1 4 30	1.60	1 A.R.	1 4 93	+3.13	+2.30	1 1.21	+0.57	0.00	0.32	2 -0.38	-0.75	-1.20
May June	•••																									
July Aug.	•••	0 ⋅83	-1.31	-1.89	9-1-6	8 – 2	2.44 -	-3.21	-3.77	-3. 73	3.10	-1.02	+0.00	7 + 3.10	T 4 43	T 7 01	1 2.84	1 3 1/	± T.O2	10.45	+0.15	-0.0	-0.36	o∙60	- I ·05	-1.17
Sept. Oct.	•••	-2.29	-1.67	-1.8	1 - 1.2	3 -1	1.20	-1.04	-2.44	-2.09	-2.01	+0.21	+ 2 40	7 4 91	1.75	14 //	T 3.30	± T.28	-0.07	+0.46	-0.53	-1.60	-2.44	ı —2·95	-2.17	-1.78
Nov.	•••	1.10	o·57	-0.38	3 -0.2	9 —	0.12	-0.35	-0·38	-0.43	-0.49	+0.24	+1.77	+2.45	+2.47	+1.89	+1.90	+1.07 +0.84	+0.83	+0·55	-0.36	-0·57	7 - 1.73	-2·49 -1·72	-2.38	-1.68
Dec.	•••		-o·33	[1							Į.		l	ļ				l	1	Į.			\	
Year	•••	-1.27	-1.09	-1.17	7 - 1 • 1	5 - 1	-38	-1.80	-2·0 8	-2·24	-1.92	-0.42	+1.24	+3.51	+4.43	+4.20	+3.30	+2.25	+1.24	+0.55	-0.02	-0.58	3 -1.17	-1.60	— 1 ·65	-1.21
Winter		-1.03	–o·54	-0.45	0.3	9 -0	.37 -	-0.49	-o·34	-o·45	o·52	+0.31	+1.37	+2.37	+2.79	+2.50	+1.77	+1.22	+o·65	+0.22	-0·28	-0.93	1.75	-2·13	-2.07	—1· 65
Equinox	c	-1·74	-1.61	-1.48	3 -1.2	5 -0	··98	-1.36	-2.01	−2·55	-2.27	-0.41	+2.01	+4.50	+5.62	+5.12	+3.89	+2.40	+1.03	+0.24	-o·33	-0.95	-1.68	3 -2.29	-2.10	I·8I
Summer	٠	-1. 05	-1.13	-1.57	-1.9	1 -2	·78 –	-3.55	-3 ⋅89	-3:73	-2.97	-1.16	+1.25	+3.67	+4.87	+4.99	+4.24	+3.12	+2.02	+1.19	+0.56	+0.17	4 -0.07	-0.37	-o·79	-1.00
			<u>. </u>	<u> </u>	1	·	<u>'</u>	•			<u> </u>	1	·		-							10 D	•	1 \)		
263.	E.I	I cdalen		NAT:	ION	(all	days	exce	pt Jar	n. 17,	Marc	h 14, .	15, A	pril 27	, 2 8,	June I	11, 12,	13, 0)ct. 1 2	, <i>13</i> , 1	Nov. z	26, D	ec. 0, 4	¥).	19	23.
200.	E-81			,	1 ,	1	1	,	,	,	,	,	,	Τ,	ı '	,	· [,	,	, , , ,	, ,		10.11	1		+0.11	+0.13
an. Feb.		+0.11	+0.01	-0.03	-0.3	6 — o	·35 –	-0·58 -0·69	0·48	0·4I 0·37	-0·14	+0·22 +0·57	+0.34	+0·32 + 0·63	+0·07 +0·41	-0.05 +0.15	+0.01 +0.12	+0.00	+0.08	+0.10	+0.08	+0.32	-0.03	+0·12 -0·12 -0·41	-0.01	+0.11
Mar.		-0.31	-0.33	-0·17	-0.3	0 0	··40 —	-0.48	-o·33	0.00	+0.44	+0.94	+1.01	+0.70	1 0.53	10.24	10.00	-0.10	-0.21	-0.20	-0.63	-0.53	-0.64	-0.64	-0.52	0.67
April May			-0·30		3 -0.0	7 – 0 9 0																				
June			-0.27		1	3 -0	.16	0.00	+0.40	+0.80	+1.21	+1.2	+1.64	+1.21	+0.71	+0.13	-0.30	-0.37	-0.40	-0.82	-0.92	-0.70	-0.50	-0.55	-0.52	-0.4
July Aug.	:::	-0.34	-0·31	-0·14	-0.1	9 -0	0.22	-0.03	+0.43	+0.79	+1.21	+1.51	+1.33	+0.78	+0.39	+0.05	-0.13	-0·28	-0.43	-o·58	-0·75	-0.79	-0·55	-0·53	-0 46	-0·4
Sept.	•••	-0.21	0.48	-0.40) — O·5	9-0	•47 -	-0.30	+0.50	+0.40	+0.95	+1.40	1.37	7 0 99	7031	1013	10.75	10.28	10.07	±0.05	-0.05	-0.11	-0.15	-0.01	-0.22	-0.3
Oct. Nov.		-0.42	—o·50 —o·08	-0·30	0.0	9 -0	·44 –	-0.47	-0.05 -0.45	-0.10	+0.70	+0.45	+0.40	+0.34	+0.22	+0.14	+0.10	+0.06	-0.03	-0.07	-0.05	+0.05	+0.07	+0·19	+0.08	+0.07
Dec.			١.	_0.05	-0.1	9 -0	.39 –	-0.44	U·40	_0·39	_0·19	+0.07	+0.20	+0.10	70.13	+00/	1000	, 0 00	,		'					
Year	•••	-0.25	-o·23	-0.22	-0.3	7 -0	-36	-o·33	-0.11	+0.22	+o·63	+0.99	+1.00	+0.75	+o·43	+0.15	—o·o2	o·o6	—o·23	o·32	-0·37	—o∙3¢	-0.28	-0.27	—o·28	-0.28
Winter		−0 ·05	– 0∙06	o·16	0.2	3 -0	.43	-0.55	o·51	-o·34	-0.01	+o·33	+0.38	+0.37	+0.21	+o·o8	+0.08	+0.08	+0.08	+0.07	+0.05	+0.21	+0.11	+0.09	+0.09	+0.10
Equinox		-0.37	0.40	-0.20	0 -0 4	3 -0	.51 –	-0.50	-0.22	+0.23	+0.79	+1.27	+1.26	+0.94	+0.57	+0.27	+0.03	+0.04	–o·15	-o·19	-0.32	-o·33	0.37	-0.39	-0.41	-0.49
Summer		-0.32	-0.23	0.23	-0.1	5 -0	·12 +	-0.05	+0.42	+0.76	+1.11	+1.38	+1.35	+0.94	+o·53	+0.10	—o·18	-0.31	– 0·61	-o·83	-0.85	-0.77	-0.59	-0.52	-0·51	-0.44
			<u> </u>		1			I	l				<u> </u>	1	<u> </u>					<u>'</u>	<u></u>					
264.				TAL	FOF	CE	(all	days	ехсер	t Jan.	. 17, N	1 arch	14, 1	5, Афп	ril 27,	2 8, J1	ine 11	, 12 , .	13, Oc	t. 12,	13, N	ov. 26	B, Dec.	3, 4).	19	923.
204.	F-91	cdaler v		1 v	- ν	1	<u> </u>	νΙ	νΙ	ν	ν	ν	ν	γ	ν	γΙ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ
Jan. Feb.	•••	— I·9	'o·8	- 'o·(5 + 1	3+	3.7 +	- 7·0 - 8·8	+ 5.7	+ 4.9	+ 1.0	- 4·3	- 6·1	- 5·7	— I·7	+ I·I	+ 0.8 - 0.5	+ 0·5 + 0·7	+ 1.6	+ 1.3	+ 1.6	- 2·c	+ 2.2	- 0.5 $+ 2.4$ $+ 6.8$	+ 0.4	- 2.
Mar.	•••	+ 2.7	+ 2.3	4 0.	1 + 2	4 +	4.4	- 5.9	+ 43	- O·4	- 7.0	-15.4	17.0	-14 3	10 1	7.7	0.7	2.2	- TO-2	+ TO:6	+12.7	+11.0	+11.7	+10.9	+ 8⋅2	+ 8.8
April May	•••	+ 0.9	+ 3.3	+ 2.	1 + 3.	11+	0.0	7'5	+ 2.4	- 5.2	10.0	-20.0	-20.1	-23 1	-13 /	3.6	7.8	6.0	± 15.7	19.8	+16.6	+13.0	10.1	+ 8.7	+ 9.7	+ 4.4
June	•••	+ 5.3	+ 3.I	+ 3.	2 + 2	9 +	1.9	- 0.7	- 0.2	-12.2	-19.3	-25.2	-27.8	-21.7	T-13 4	- 3 0	7.0	1 4.0	1 8.2	± 14.8	+16.5	+14.5	+11.0	+ 9.7	+ 8.4	+ 67
July Aug.	•••	+ 4.6	4 1.0	+ 1.	1 + 0	/ +	1.0	- 1.3	- 0.1	-11.0	-10.5	1-19.7	-20.0	-1/3	90	2.7	2.6	1 7.0	1 8.7	- TO:0	+13.1	+13.5	+9.8	+ 9.0	+ 7.7	+ 7.4
Sept.	• • •	+ I·4	+ 4.0	+ 3%	9 + 0	9+	5.7	- 3.2	- 2.3	6.7	-14.3	XX.0	-22.3	-17.1	ر و —ا	- 2 3	2.0	1 3.5	2.6	1 2.2	1 3.6	+ 3.7	+ 2.9	+ 0.2	+ 1.6	+ 2.7
Oct. Nov.	•••	+ 3.5	+ 5·1	十 2"	7 + 0	9 +	7.5	- 0.2	+ 0.1	- 0.4	-10.1	-19.4	14.0		- 0 2	4 /	1 0 9	0.0	1 7.5	⊥ 2·T	+ 2.0	+ 0.7	+ 0.3	- I·6	— 0.7	- 0.7
Dec.	•••	— o∙3	— o·6	0.0	0 + 1	7 +	4.7	- 5.6	+ 6.0	+ 4.9	+ 2.0	- 2.2	- 4·4	− 3·5	- 2.7	— o·6	0.0	+ 0·2	- I·I	+ 0.1	+ 0.1	- 3.2	_ 1.3	— 1 ·9	~ 3	
Year	•••	+ 2.6	+ 2.0	+ 1.	9 + 2	9+	4.3	- 4·I	+ 1.2	– 3 ⋅6	-10.1	-16.3	17·1	-13.6	– 8⋅3	– 2 ·6	+ 1.3	+ 3.0	+ 6·1	+ 7.6	+ 8.2	+ 6.9	+ 6.1	+ 5.1	+ 4.3	+ 3.6
Winter	•••	+ 0.1	- o.1	+ 0.	9+ 2	3 +	5.2	- 6.9	+ 6.4	+ 4.1	- 0.7	- 5·9	– 6.8	- 6· ₄	– 3·7	— o·7	0.0	+ 0.4	+ o·5	+ 0.7	+ 0.9	- 1.1	- o·1	- 0.4	– o ⋅8	- 1.6
Equino	ĸ	+ 3.7	+ 3.7	+ 2.	2 + 4	6 +	6.1	- 6∙3	+ 3.1	- 3.3	-11.9	-20.0	−20 ·8	_16·6	_10·4	- 4.2	+ 1.1	+ 2.5	+ 5.9	+ 6.5	+ 7.9	+ 7.7	+ 7.5	+ 6.6	+ 5.7	+ 5.9
Summer	r	+ 4.1	+ 2.5	+ 2.0	6 + 1	8 +	1.6	- 0.9	– 6∙1	-11.5	-17.7	-22.9	-23 ·5	-17.7	-10.7	– 3 ·o	+ 2.8	+ 6.1	+11.8	+15.7	+15.9	+14.2	+10.0	+ 9.1	+ 8.3	+ 6.6
	 -	l	1	i	1	<u> </u>		!			!	<u> </u>	!	1	<u>'</u>					<u> </u>		<u></u>	<u>'</u>			Q
(19889)																	•									

DIURNAL INEQUALITIES OF THE GEOGRAPHICAL COMPONENTS OF MAGNETIC FORCE.—INTERNATIONAL QUIET DAYS.

			our.	G.M.T.	3	.	4.	5	i.	6.	7.	8.		9.	10.	II.	Noo	n.	13.	14.	15	16.	17.	:	18.	19.	2	20.	21.	22.	23.	24.
Month and Season		_						<u> </u>			1	N	IOR	тн	COM	' IPOI	NENT	1 (0)uiet	Davs) <u>.</u>	!	<u> </u>		!		_!	'			1	· <u>·</u>
		:	265.	Es	kda	lem	uir.														, •	.,										1923.
Jan. Feb. Mar. April May June July Aug. Sept. Oct.		-+++++++	2·3 - 2·9 - 7·1 - 3·8 - 5·8 - 6·5 - 4·7 -	+ 3·1 + 4·6 + 2·3 + 5·6 + 4·9 + 6·6	++++++	1·4 - 1·3 - 4·8 - 4·8 - 4·6 -	- 1.4 - 4.3 - 6.2 - 7.0 - 5.7 - 4.0 - 6.6	+++++++	1.7 - 3.1 - 3.2 - 7.5 - 4.7 - 5.7 - 5.9 - 6.3 -	+ 6.9 + 7.3 + 6.7 + 6.2 + 6.9 + 7.3	+ 4.7 + 1.1 + 1.1 - 0.2 + 2.6 + 5.3	+ 4 + 5 - 3 - 5 - 4 + 0	·1	2·2 1·2 ·11·6 · 9·6 ·12·4 ·11·5 · 13·6 · 8·0	- 7:3 - 6:3 -24:2 -19:9 -20:5 -21:7 -19:6	3 — 13 4 — 28 5 — 25 5 — 25 7 — 25	$ \begin{array}{c c} \cdot 6 & -13 \\ \cdot 0 & -15 \\ \cdot 7 & -26 \\ \cdot 2 & -22 \\ \cdot 6 & -25 \\ \cdot 2 & -18 \\ \cdot 7 & -23 \\ \cdot 0 & -22 \end{array} $	3	- 9·5 -14·0 -18·5 -15·7 -20·6 -13·3 -17·4	- 5.6 - 10.3 - 9.6 - 9.8 - 13.1 - 8.4 - 10.3 - 11.1	- 2·3 - 4·3 - 2·2 - 1·5 - 1·9 - 5·0 - 2·1 - 5·3	0.0 - 3.2 + 3.8 + 4.3 - 2.7 + 4.9 - 2.7	0 + 2 $0 + 2$ $0 + 3$ $0 + 3$ $0 + 3$ $0 + 3$ $0 + 4$ $0 +$	·6 ++++++++++++++++++++++++++++++++++++	3.5 1.0 9.7 12.6 7.8 11.2	+ 4 + 2 + 12 + 14 + 13 + 12 + 11 + 8	·6 ·2 ·9 ·4 ·4 ·4 ·+ ·+ ·+ ·+ ·+ ·+ ·+ ·+ ·+ ·+ ·+ ·+ ·+	3.9 3.4 10.8 11.0 12.1 13.3 13.1 9.8	+ 4.0 + 4.1 + 9.6 + 10.1 + 11.8 + 9.1 + 11.1 + 8.9	+ 3.7 + 4.6 + 9.2 + 8.6 + 8.6 + 10.7	+ 4 + 7 + 8 + 7 + 8 + 7 + 7 + 9	7 + 0 + 2 + 4 + 7 + 8 + 7 + 7 + 7 + 7 + 7 + 7 + 7 + 8 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1
Nov. Dec.		+	I · I -	- 0.2	1+	0.9	- 3·I	:1+	4.6	+ 5.6	1+ 4.5	+ 2	+	· 2·8 · 1·0	- 7·3	$\begin{vmatrix} -9 \\ -3 \end{vmatrix} = 3$	· 5 — 9 - 6)·2 - - -	- 6·7	— 3·9 — 2·4	- 0.1 - 1.0	+ 0.8	3 + 2	·3 + ·5 +	4·3 2·1	+ 3	·8 + ·4 +	1.9	+ 1·5	+ 1.1	+ 2 - I	·0 — I
Year	•••						_				+ 3.8																					4 + 4
Winter Equinox			į.			- 1		1			+ 4.6	i		- 1		1	- 1	- 1	- 1		l	1		1		_			-		ł	0 + 6
Summer	•	+	5.2	⊢ 4·5	+	4.9	- 4.9	+	6.0	+ 5.0	+ 1.3	- 4	-5	11.8	—19·7	-24	-22	-4	-16.8	<u></u>	- 2.6	+ 2:3	3 + 7	+ 8	11.1	+12	+	12.4	+ 10.5	+ 8.3	+ 7	·9 + 7
266.	Esl	kda	ilem	uir.								V	WES	ST (COMI	PON	ENTS	(Q	uiet	Days)											•	1923.
Jan., Feb. Mar. April May June July Avg. Sept. Oct. Nov. Dec. Year			2·4 - 2·7 - 3·5 - 0·6 - 5·0 - 2·4 - 3·6 - 2·5 - 2·3 -	- 2·3 - 2·8 - 4·6 - 3·5 - 0·5 - 2·1 - 5·4 - 1·8 - 0·2	——————————————————————————————————————	1·3 + 2·1 - 2·8 - 4·6 - 4·9 - 5·1 - 3·9 -	- 2·2 - 3·1 - 4·3 - 7·9 - 8·3 - 7·1 - 5·4 - 3·0 - 0·7	- 3 - 1 - 1 - 10 - 10 - 0 - 0	0·5 - 2·1 - 4·3 - 7·0 - 1·5 - 3·2 - 0·6 - 6·6 - 3·0 - 0·4 - 0·6 -	- 2·2 - 4·1 - 9·0 -15·7 -17·6 -16·0 -15·8 - 9·6 - 4·0 - 1·0 - 0·7 - 8·0	- 4.0 - 5.9 - 14.3 - 18.9 - 17.9 - 17.1 - 12.2 - 5.6 - 2.9 - 1.7	- 4 - 9 -20 -19 -22 -18 -17 - 9 - 5 - 1	•5 — •5 — •7 — •1 — •9 — •6 — •5 — •5 —	7.6 11.0 22.2 17.3 22.1 16.4 15.8 16.6 11.8 6.0 2.1	- 5.9 - 8.4 - 14.1 - 11.9 - 16.1 - 12.5 - 10.6 - 12.6 - 4.8 - 1.9 - 0.3	+ 0 - 2 - 1 - 6 - 4 3 + 4 + 4 + 4 + 4	$ \begin{array}{c} \cdot 1 + 5 \\ \cdot 7 + 10 \\ \cdot 3 + 12 \\ \cdot 1 + 9 \\ \cdot 0 + 7 \\ \cdot 0 + 10 \\ \cdot 5 + 15 \\ \cdot 9 + 14 \\ \cdot 2 + 11 \\ \cdot 9 + 8 \\ \cdot 6 + 7 \\ \cdot 4 + 9 \end{array} $	·8 + ·3 + ·5 + ·5 + ·7 + ·9 + ·9 +	- 9.9 -16.5 -21.2 -16.9 -16.2 -17.3 -22.8 -20.1 -14.8 - 9.4 - 8.7	+ 9.8 + 15.0 + 20.7 + 17.3 + 18.9 + 19.4 + 21.8 + 19.8 + 12.6 + 6.7 + 6.4 + 14.8	+ 7·1 + 11·4 + 15·1 + 13·7 + 20·5 + 14·0 + 6·6 + 3·1 + 3·7	+ 1.5 + 4.0 + 11.1 + 15.5 + 10.7 + 7.5 + 2.0 + 1.9 + 1.9	6 + 1 $0 - 6$ $0 + 9$ $0 + 11$ $0 + 11$ $0 + 13$ $0 + 6$ $0 + 2$ $0 + 2$ $0 + 3$ $0 + 4$ $0 + 5$	·i + + + + + + + + + + + + + + + + + + +	1.9 0.7 7.1 11.1 8.0 5.9 3.8 1.1 0.3	+ 1 + 4 + 9 + 7 + 4 + 1 + 0 - 0	·2 — + + + + + + + + + + + + + + + + + +	1.2 0.8 4.0 2.7 5.3 5.6 4.3 2.4 0.8 1.3 4.4	+ 0·1 - 0·2 + 2·1 + 3·5 + 4·9 + 2·8 + 1·5 - 4·3 - 4·1 + 0·6	- 0.6 + 1.6 + 3.1 + 3.1 + 3.2 + 2.0 + 0.3 - 0.8 - 4.3	- I - I - 0 + 2 + 4 + I - 0 - 3 - 3 - 4	9 - 4 - 3 - 3 - 3 - 3 - 3 - 3 - 3 - 3 - 3
Equinox Summer		_	3.0	- 3.2		3.4	- 3.9		5.2	- 6.7	- 9.5	-14	.4 —	15-4	- 9.8	+ 0	.5 + 12	.3 +	-18·2	+17.0	+11.8	+ 6.4	+ 4	·o +	3.2	+ 2	.7 +	2.0	+ 1.0	+ o.1	- I	·6 — 2
					<u>'</u>						<u> </u>	VE	ERT	ICA	L CO	OMP	ONE	NT	(Qui	et Da	ys).											1923.
267.		_	1	٠, ١	γ	, 1	γ	γ	,)	γ	λ γ	Ι γ	-	γ	γ	Ιγ	γ	1	νΙ	γ	Ι γ	Ι γ	γ	 -	γ	γ	<u> </u>	γ	γ	γ	Ι γ	Ι γ
Jan. Feb. Mar. April May June July Aug. Sept. Oct. Nov. Dec.		1 + + + + + + +	0·3 - 0·7 - 2·0 - 1·9 - 0·8 - 1·1 - 1·8 - 2·1 - 1·2 -	- 0.9 - 0.6 - 0.5 - 2.7 - 2.9 - 1.8 - 1.1 - 1.1 - 1.5 - 1.2	++-++-	0·8 - 1·8 - 0·2 + 2·6 + 3·1 + 0·9 + 1·4 + 0·5 +	- 1·0 - 1·4 - 0·2 - 1·8 - 4·3 - 2·5 - 1·9 - 2·5 - 1·4 - 0·5 - 1·1	+ + + + + + + + + + + + + + + + + +	0·9 - 0·3 - 0·3 - 1·5 - 4·8 - 2·9 - 3·4 - 0·5 - 1·4 -	- 0·7 - 0·5 + 0·3 + 2·7 + 3·6 + 3·1 + 4·1 + 2·8 + 2·0 - 0·8	- 1·4 - 0·3 + 0·4 + 3·6 + 2·8 + 2·9 + 3·1 + 2·6 - 0·8	- I + 0 0 + I + 1 + 2 + 2 + 2 + 1 - 0	2.5 + + + + + + + + + + + + + + + + + + +	1.5 2.0 0.3 2.1 1.8 1.1 1.7 1.1 0.3 1.3	- 1.7 0.0 - 2.3 - 5.6 - 7.8 - 3.8 - 5.9 - 3.7 - 1.3 - 4.1 - 2.6	7 - 1 $7 - 1$ $7 - 1$ $7 - 1$ $7 - 1$ $7 - 1$ $7 - 1$ $7 - 1$ $7 - 1$ $7 - 2$ $7 - 3$ $7 - 5$ $7 - 5$ $7 - 5$ $7 - 5$ $7 - 5$ $7 - 5$ $7 - 5$ $7 - 5$	$ \begin{array}{c cccc} \cdot 6 & - & 1 \\ \cdot 1 & - & 2 \\ \cdot 6 & - & 9 \\ \cdot 2 & - & 10 \\ \cdot 2 & - & 14 \\ \cdot 0 & - & 10 \\ \cdot 8 & - & 10 \\ \cdot 8 & - & 9 \\ \cdot 9 & - & 5 \\ \cdot 6 & - & 1 \end{array} $	·8 - ·5 - ·8 - ·8 - ·1 - ·8 - ·8 - ·7 -	- 3·1 - 7 ·5 - 10·6 - 11·2 - 7·2 - 7·5 - 8·6 - 9·4 - 4·6 - 0·1	+ 0·5 - 2·0 - 4·3 - 5·2 - 6·8 - 3·7 - 5·5 - 5·2 - 1·4 + 2·2	+ 1.6 - 0.6 - 1.8 - 3.9 - 2.3 - 1.7 - 0.9 + 1.7 + 2.2	0 + 1.0 0 + 4.2 0 + 1.0 1 - 0.3 1 + 0.1 1 + 0.0 1 + 2.3 1 + 2.1 1 + 0.0	3 + 1 $4 + 4$ $3 + 3$ $3 + 1$ $4 + 3$ $4 + 4$ $4 + 3$ $4 + 4$ $4 + 3$ $4 + 4$ $4 + 3$ $4 + 4$ $4 +$	·1++++++++++++++++++++++++++++++++++++	1.9 2.9 2.8 4.5 5.5 3.3 1.5 0.8	+ 1 + 3 + 3 + 5 + 5 + 3 + 1 + 1	·1+ ·2+ ·5+ ·3+ ·7+ ·3+ ·4+ ·6+	3·6 5·7 4·5 2·9 2·5 1·6 0·8 1·1	$\begin{array}{c} + 1.2 \\ + 2.9 \\ + 2.8 \\ + 3.1 \\ + 2.1 \\ + 2.1 \\ + 0.7 \\ + 0.9 \end{array}$	+ 1·2 + 2·1 + 2·2 + 1·7 + 1·9 + 0·8	+ 2 + 2 + 2 + 1 + 2 + 1 + 2 + 1	·2
Year		+	0.4	+ o·7	+	o ·6	⊢ o ∙g	+	1.3	+ 1.4	+ 1.4	+ 1	ı ·o	· 0·4	— 3·	4 - 5	·8 - 7	·3 -	- 5.9	— 3·1	- o·2	+ 1.5	+ 2	+	2.4	+ 2	+	2.4	+ 2.1	+ 1.7	+ 1	·5 + 1
Winter Equinox Summer	x	+	1.5	+ 1.5	+	1.2	⊢ 1 •0	+	0.9	+ 1.3	+ 2.0	+ 1	1.4	0.2	- 3:3	6 - 6	·6 - 8	-7	- 8·o	- 4.0	0.0	+ 2.7	+ 3	· 3 +	2.1	+ 2	+3	2.3	+ 2.0	+ 1.8	+ 2	.0 + 1

DIURNAL INEQUALITIES OF THE MAGNETIC COMPONENTS, DECLINATION, INCLINATION AND HORIZONTAL FORCE— INTERNATIONAL QUIET DAYS.

Departures from mean of the day adjusted for non-cyclic change.

Hour. G.M.T.

	I.	2.	3.	4	١.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.
-	000	P	lede 1	<u> </u>	<u>'</u>		DEC	LINA	TION	(mea	sured	positi	ve to	wards	the W	/est) (Quiet	Days)	•				•		100
	268.	. Es	Kaale	emui	IF. 1	,	,	,	· ·	1 /	(,	1	,	,	,	,	. ,	,	,	1 ,	, ,	, ,	, ,	19	923.
-	-o·6o	-o·37	-0.1	8 +0	0.24	+0.01	-0.31	-o·57	-0.67	-1.00	-o·47	+0.47	+1.49	+2.17	+1.88	+1.05	+o·8o	+0.63	+0.28	+0.09	-0.52	-1.03	-1.30	-1.19	-0.91
	-0.01	-0·55	-0·4	18 — 0	0.51	-0.60	-0·84	-1.16	-1.12	-1.38	-0·75	+0.63	+1.94	+2·51	+2.26	+1.53	+0.30	+0.17	十0.17	+0.18	+0.03	-0.21	-0.34	-0.43	-0.85
: -	-1.10	-0.73 -1.18	-1.1	8 - 1	1.21	1·83	-1.23 -2.16	-3.11	-4.05	-3.73	-1.31	+1.21	+3.98	+5.27	+4.65	+3.13	+2.15	+1.38	+0.85	+0.13	+0.18	-0.14	-0·39	-0.60	-1.00
				4-1	1.75 -	-2.55	-3.36	-3.85	-3.57	-2.87	-1.22	+1.23	+3.19	+4.24	+3.98	+2.79	+1.94	+1.71	+1.46	+1.00	-0.10	+0.11	+0.14	+0.01	-0.10
		-		5 -2	2.05	-3.05	-3.84	-3.55	-4.22	-3.66	-2.01	+0.29	+2.92	+4.39	+4.50	+4.16	+2.98	+1.71	+o.86	+0.65	+0.35	+0.29	+0.27	+o·54	+0.17
- 1	-0.50	-o·73	-0.9	3 - 1	1.48	-2:49	-3.32	-3:5 2	-3.42	2 - 2.59	-1.50	+0.37	+3.05	+4.18	+4.33	+3.20	+2.19	+1.22	+0.72	+0.82	+0.34	+0.48	+0.18	-0.12	-0.49
	-0.85	-1.32	-1·4	0 - 1	·46 -	-2·43	-3.23	-2.74	-3.56	3 - 2.83	-0.74 -1.25	+ 1·55	+4.44	+4.89	+4.55	+3.40	+1.62	+0.74	+0.33	+0.30	-0.00	-0.22	-0.55	-0·62	-0.08
	91			7 -0	·8 ₂ -	-0·82	-I.06	-1.30	-1.92	-1 ⋅93	0.04	+1.86	+3.17	+3.51	+2.93	+1.57	+0.41	+0.22	+0.05	-0.13	-0.23	-0.29	-0.57	-1.07	-1.26
-	-o·35	+0.11	+0.1	2 -0	0.24	0.20	-o·30	_o·50	0.52	-0.47	+0.01	+1.08	+1.71	+z·00	+1.40	+0.74	+0.32	+0.05	-0·18	-0.23	-0.98	_o.88	-0.92	-0·85	-0.89
-	-0.63	−0 ·66	-0.7	7 -0	o·99 -	-1.43	-1.90	-2.23	-2.47	-2.17	-o·88	+1.10	+2.93	+3.75	+3·37	+2.33	+1.34	+0.75	+o·39	+0.25	-0.11	-0.27	-o·39	o·53	-0.77
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-	-0.89	–o.∂ı	-0.9	5 - 1	· ·0 9 -	-1.37	-1.69	-2.20	-2.94	-2.69	-1.00	+1.31	+3.58	+4.43	+3.93	+2.57	+1.29	+o·58	+0.33	+0.00	-0.04	-0.23	-o·43	-o·71	-0.96
-	-0•47	-o·77	— I·2	1-1	.73 -	-2.63	-3.21	-3.72	-3.60	2.87	-1.37	+1.01	+3.40	+4.58	+4.43	+3.40	+2.23	+1.36	+0.79	+0.67	+0.17	+0.20	+0.13	0 ∙04	-0.45
Esk	dalem	uir.								IN	CLIN	ATIO	N (Qı	uiet D	ays).			·····				,		19	923.
-	0.12	+0.11	+0.0	9 – 0	0.05 -	-0·14	_0·23	_0·30	-0.20	+0.03	+o·30	+0.31	+0.12	_0·01	-0·13	+0.03	_o·o2	_0·04	_o·o9	_o·15	-0.10	+0.13	+0.10	+0.08	+0.06
-	-0.11	-0.07	-0.0	9 - 0	·09 -	-0.17	-0.41	-0.37	-0.17	+0.34	+o.58	+0.85	+0.71	+0.35	+0.13	+0.04	+0.01	-0.17	-0.23	-0.28	-0.25	0.23	-0.50	0·I4	0.0
• -	-0.12	-0.13	-0.1	<u>5</u> — o	·2I -	-0.25	-0.38	-0.42	-0.20	+0.14	+0.21	+0.69	+0.57	+0.40	+0.27	+0.05	+0.25	+0.11	0.00	-0.13	-0.15	-0.19	-0.23	-0·23	-0.1
-	-0.35	-0·14	-0.1	0 -0	28 -	-0.31	—0·20 ⊥0:11	+0.02	+0.47	+1.11	+1.70	+1.09	+1.21	+0.53	+0.10	-0.12	-0.43	-0.01	-0.03	-0.92	-0.61	-0.59	-0.40	-0·43	-0.4
-	-0.45	o∙38	-0.3	9 —o	1.23 -	–o∙18	+0.01	+0.38	+0.83	+1.24	+1.53	+1.54	+1.24	+o.85	+0.32	-o·36	-0·46	-0.72	-o·83	-0.86	一0.77	o·78	0 ⋅63	o·51	-0.5
-	-o∙38 -	-0.29	-0.3	1 — o	·2I -	-0.07	+0.22	+0.43	+0.72	+1.01	+1.17	+1.17	+0.73	+0.35	+0.09	-0.01	-0.01	-0·27	-o·53	—o∙83	0.89	—o·63	− 0·53	-o·52	-0.4
				3 -0	0.06	-0.10	—o·o8	+0.21	+0.64	+1.15	+1.50	+1.40	+0.95	+0.48	+0.13	-0·22 ⊥0:06	-0.49 -0.49	-0.59	-0·71	-0·77	_ი.გ/ _ს.გნ	-0.71	-0·51	-0.4I	-0.3
-	-0.13	-0.22	-0.2	1 -0	19 -	-0.19	-0.23	-0.11	+0.20	+0.71	+1.00	+0.92	+0.67	+0.25	+0.21	+0.21	+0.02	-0.23	-0·35	-0·45	-0.45	−0 ⋅46	-0.44	-o·31	-0.3
-	-0.02	+0.01	-0.0	7 -0	.23 -	-0.32	-0.36	-0.25	-0.03	+0.20	+0.47	+0.46	+0.40	+0.25	+0.18	+0.10	+0.01	-0.15	-o·28	-0.24	0.0 6	+0.01	-0.02	-0.10	-0.0
-	⊦o·18	+0.17	0.0	0 - 0	- 00	-0.12	-0·19	-0.14	–0· 16	-0.04	+0.03	+0.06	+ 0.1 6	+0.17	+0.04	-0.0 4	—o·o7	–o·18	–o·14	—o·o8	-o·o3	+0.02	+0.04	+0.18	+0.2
-	-0.16	0·12	o·1	4 -0	·16	-o·17	—o∙17	-0·02	+0.26	+o·64	+0·9 6	+0.99	+0.72	+o·37	+0.14	—o∙o4	-o·13	-o·32	-0·42	-0 ·51	–0·4 6	– 0∙38	– 0∙34	-0.29	-0.2
-	-0.04	+0∙05	–o·o	2 -0	.11	- 0 ·19	-0.30	-0.27	-0.14	+0.15	+o·35	+0.42	+o·35	+0.19	+0.05	+0.03	-0.02	-o·13	-o·19	-0.19	-0.11	-0.02	—o·o2	+0.01	+0.0
-	-0.23	-0.21	-0.3	1 -0	.24 -	-0.25	-0.26	-0.13	+0.31	+0.60	∔1.17	⊥1.17	±0.85	+0.30	+0.30	+0.04	-0.02	-0.23	-0.35	0 ∙50	o·48	-0.45	-0.47	-0.37	-0.3
					- 1										i	i					1				į.
•• -	-0.29	−0·2I	-o.1	9 -0	.11	– o∙o 8	+0.07	+0.33	+0.41	+1.07	+1.38	+1.37	+o·96	+0.53	+0.17	-0.30	—o∙36	—o∙6o	-o·75	0.86	-0·78	-0·68	-o·54	-0.50	-0.4
Esk	dalem	nuir.							НС	RIZC)NTA	L FO	RCE	(Quiet	Days	;).								19	923.
\neg	γ	γ	γ	1)	y	γ	γ	γ	γ	γ	γ	γ_	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ	γ
•	- 2·I	- 2·0	- I.	7 +	0.4	+ 1.8	+ 3.2	+ 3.9	+ 2.3	- I.O	- 5.0	- 5·1	- 2.4	- 0·4	+ 2.2	+ 0.6	+ O.t	+ 1.5	+ 2.1	+ 2.9	+ 2.0	+ 2·0	+ 3.V	+ 2.3	
-	2.1	+ 2.1	+ 2.	2 +	3.2 -	+ 3⋅8	+ 5.8	+6.4	+ 3.0	- I·o	l 8·₄	-12.7	-11.8	 8⋅8	- 5.6	- I.O	- 2.0	+ 0.2	+ 1.1	+ 3·I	+ 3.5	十 3.9	+ 4·2	+ 4.1	+ 3
-	5.9	+ 3·I	+ 3.	3 +	4.8 -	+ 5.2	+ 3.0	+ 0.5	- 6.4	-17.3	-27.3	-28.2	-22.0	-11.8	- 3.4	+ 2.2	+ 7.0	+10.2	+11.3	+13.5	1+11.5	+ 9·8	+ 9.3	+ 7·2	1+ 7
-	3.4	+ 1.2	+ I.	3 +	0.8	+ 1⋅3	- 0.3	— 3·6	- 8•o	- T4.T	-22.4	-24.5	-10.3	-10.4	- 4.6	+ 2.4	+ 7.2	+11.2	十15.3	+16.5	+11.3	 10 ·7	1+ 8.0	+ 9.3	1+ 7
-	F 6·1∣-	+ 4.8	+ 5.	0 +	3.8 -	+ 2.4	- I·8	- 5.2	-10.0	- T5.6	- TQ.7	-20.5	14.6	- 7·0	- 2.7	- 0.7	+ 0.2	+ 5.4	+ 9.1	+13.7	+14∙ઇ	+ 10.5	1+ 8.5	+ 8.3	1+ 0
-	- 3·I ·	+ 3·I	+ 2.	81+	1.8 -	+ 2.7	+ 2.2	- 2.2	- 8·7	- T7.5	-23.6	-23.7	-18.1	- 10.4	- 3.8	+ 2.7	+ 7.6	+11.1	+11.8	十12・7	1+13.8	+II·4	+ 8.2	+ 0.9	1 + 0
-	- 5·6l	+ 5.4	+ 5.	2 +	4.9 -	+ 4.2	+ 4.3	十 エ・フ	I- 4.7	12.4	-22.2	- 22·8	- 17.7	— 0.5	- 5.2	→ T·2	- 0.3	+ 3.7	1+ 5.7	+ 9.2	+ 10·1	1+ 8.9	+10.9	4 0.0	1 + 7
:: <u>-</u>	- 2·3	+ 3.7 - 0.2	+ 3.	8 +	3.0	+ 4.5 + 3.0	+ 3.4 + 5.1	+ 1.8	- 2·3	-10.1	16·4	- 15·9	-12·I	5:4 2:8	- 3.6	- 2.4	+ 0.4	+ 4.3	+ 5.8	+ 2.8	+ 1.3	+ 0.2	+ 0.6	+ 1.6	+ 6
-	- 2.6	- 2·5	- o.	ī +	1.3	+ 2.2	+2.6	+ 2.0	+ 2.3	+ 0.4	- 1·4	- 1.6	- 3.0	- 2·5	- 0·5	+ 0.0	+ 1.3	+ 2.6	+ 2.0	+ 1.2	+ 0.6	0.0	- 0.2	- 2.3	- 2
	- 1																								
ı							 1.9	1 2 . 7	1-L T-0	- 2.3	- 5.7	- 6·9	- 5.9	- 3⋅3	- 0.7	+ 0.2	+ 0.8	+ 2.5	+ 3·I	1+ 3.1	1+ 2.0	1+ 0.7	1+ 0.7	+ 0.I	1- c
-	- o·7					1				i .									l	ì	-	1	i	l	1
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-	+ 4.0	+ 3.6	+ 3.	5 +	4.0	+ 4.1	+ 4.3	+ 2.6	- 2.6	-10.4	-18.6		-15.9	– 8∙9	— 4·5	— o ∙6	+ 1.3	+ 4.6	+ 6.0	+ 8.3	+ 8.0	+ 7.4	+ 7.7	+ 6.3	+ 5
	Esk.	2680.600.610.710.710.360.850.900.530.630.630.47 Eskdalen +0.120.16 +0.120.180.180.180.180.180.19 +0.21 +0.21 +0.31	268. Es 0.60 -0.370.61 -0.550.71 -0.731.10 -1.180.36 -0.83 +0.25 -0.190.50 -0.731.26 -1.350.85 -1.000.90 -0.730.55 -0.370.35 +0.110.63 -0.660.53 -0.290.89 -0.910.47 -0.77 Eskdalemuir. +0.12 +0.110.11 -0.070.12 -0.130.38 -0.290.16 -0.170.38 -0.290.16 -0.170.18 +0.170.18 +0.170.18 +0.170.19 -0.21 Eskdalemuir. +0.14 +0.050.29 -0.21 Eskdalemuir. +0.4 +0.050.29 -0.21 Eskdalemuir. +0.4 +0.050.29 -0.21	268. Eskdale 0.60 -0.37 -0.1 0.61 -0.55 -0.4 0.71 -0.73 -0.7 1.10 -1.18 -1.1 0.36 -0.83 -1.1 0.50 -0.73 -0.6 0.55 -0.73 -0.6 0.85 -1.00 -1.1 0.90 -0.73 -0.6 0.55 -0.37 -0.1 0.53 -0.66 -0.7 0.53 -0.66 -0.7 0.53 -0.66 -0.7 0.89 -0.91 -0.9 0.47 -0.77 -1.2 Eskdalemuir.	268. Eskdalemu 0.60 -0.37 -0.18 +0.10 -0.61 -0.55 -0.48 -0.10 -0.71 -0.73 -0.74 -0.11 -0.73 -0.74 -0.11 -0.75 -0.73 -0.75 -0.73 -0.75 -0.73 -0.75 -0.7	268. Eskdalemuir.	268. Eskdalemuir. -0.60	268. Eskdalemuir.	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DIURNAL INEQUALITIES OF THE GEOGRAPHICAL COMPONENTS OF MAGNETIC FORCE.—SELECTED DISTURBED DAYS. Departures from mean of the day adjusted for non-cyclic change.

Month		lour.	G.M.T 2.	3	.	4.	5.		6.	7.	1	3.	9.	1	o.	II.	Noon	1. 1	13.	14.	15.	16.	17.	I	8.	19.	20.	21.	22.	23	. 24.	
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Nov		+ 8.8 - 0.3 + 8.1 - 7.5 + 5.1 + 4.6 + 7.7 - 2.0 + 13.4 + 3.2	+ 5.8 + 6.9 + 1.6 - 7.1 + 5.2 + 7.3 + 1.3 + 1.5	8 +	0·6 - 7·4 - 2·1 - 0·2 - 9·5 - 1·1 - 8·4 - 0·6 - 4·2 -	+ 2·6 + 4·7 - 4·7 + 3·7 + 11·3 + 0·2 + 8·4 + 17·8 + 6 ·9	+10 + 3 + 3 + 2 + 7 + 6 + 15 + 6 + 10	·4 + ·7 + ·7 + ·2 + ·5 +	- 10·4 - 8·9 - 12·0 - 0·2 - 4·3 - 2·3 - 7·7 - 6·2 - 5·0 - 10·2	+ 4.8 + 1.1 + 3.0 - 9.0 - 7.2 - 3.2 + 15.1 + 7.2	3 + 5 - 5 - 5 - 5 - 2 - 1 - 2 - 7 +	2·0 2·7 5·9 16·6 16·3 12·5 8·8 1·8 4·9 7·4	- 8· - 10· - 13· - 24· - 21· - 17· - 12· - 11· - 10·	8 — 3 3 — 3 1 — 3 4 — 3 7 — 3 6 — 3 0 — 3	24.6 23.1 20.6 28.9 33.4 19.0 25.9 24.4 8.5 10.5	- 14·1 - 28·9 - 31·2 - 26·3 - 35·7 - 22·1 - 34·7 - 27·9 - 5·9 - 10·9	7 -21 -29 -29 -33 -20 -24 -21 -27 -27 -27	3 — •5 — •5 — •5 — •6 — •	11.7 24.3 24.1 16.5 23.3 17.8 17.9 21.8	- 4.13.4 - 13.4 - 3.4 - 10.6 - 11.5 - 9.5 - 8.6 - 13.6 - 5.6	7 + 6.3 7 + 6.3 6 - 10.2 8 - 1.8 6 + 20.3 8 - 4.6 9 + 1.6 9 - 2.7 1 - 3.5	3 + 2· 3 + 6· 3 - 1· 3 + 1· 4 - 5· 7 - 6· 7 - 4·	5 + 8 $3 + 13$ $4 + 15$ $5 + 29$ $7 + 19$ $9 + 9$ $4 + 5$ $8 + 8$ $1 + 9$ $0 - 5$	·7 + ·9 + ·3 + ·6 + ·5 + ·0 + ·6 - ·2 -	6·3 12·1 12·0 34·7 17·5 25·3 11·5 11·4 8·5 2·7	+ 5.1 + 22.1 + 18.1 + 17.1 + 25.1 + 13.1 + 9.1 - 7.1 - 5.1	9 - 4 $+ 9$ $+ 14$ $+ 15$ $+ 17$ $+ 19$ $+ 17$ $+ 17$ $+ 17$ $+ 17$ $+ 17$ $+ 17$ $+ 17$ $+ 17$	5 + 8· 9 + 11· 3 + 22· 7 + 17· 1 + 14· 0 + 9· + 11· 3 + 8· 7 + 5·	5 + 9 + 17 3 + 16 1 + 10 8 + 13 3 + 13 9 + 13 9 + 13 9 - 12 7 + 3	$\begin{array}{c} 7 + 3 \\ + 12 \\ + 6 + 14 \\ + 8 + 21 \\ + 8 + 13 \\ + 4 + 13 \\ + 7 \\ + 9 + 14 \\ + 9 + 14 \\ + 10 + 1$	7 -9 -2 -3 -8 -3 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1	3.7 3.5 3.7 2.0 1.8 3.9 5.6 5.8 3.1 2.0
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Summer	-	⊦ 2·5	+ 1.	4 +	2.6	+ 5.9	+ 6	•4	- 3.5	- 7:	5 -	13.6	−18 ·	8 -	26.8	–29 ·′	7 -24	.5	-18-9	— 8·	3 + 2.	+ o.	9+15	.9	22·3	+18	5 + 17.	2 + 14.	5 + 12	·8 + 12	· I	7.6
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Jan Feb Mar April May June June June Sept Oct Nov Dec Year Equinox		- 2·0 - 8·1 - 8·7 - 11·9 - 12·9 - 5·5 - 30·9 - 15·6 - 13·2 - 4·5 - 10·5	+ 5.6 - 4.1 - 3.2 - 11.3 - 7.2 - 19.1 - 12.5 - 6.2 - 11.5 - 1.5 - 7.5 - 1.6	5 - : : - : : : : : : : : : : : : : : :	2·9 - 1·7 - 6·3 - 7·3 - 7·3 - 7·3 - 5·6 - 5 - 6·5 - 6·5 - 6·2 - 6·1 - 7·3 - 5·2 - 6·	- 1·1 -14·2 -11·0 - 7·9 -20·7 -17·7 -17·3 - 9·4 - 2·7 +14·0 - 3·9 + 7·3 - 7·0	+ 0 - 9 - 3 + 4 -23 -12 -17 + 8 + 22 - 0 + 5	·8	- 7·7 - 5·8 - 8·4 -27·1 -17·3 -24·5 -22·8 - 8·4 -24·9 - 0·9 - 3·7	+ 6.4 + 2.2 - 8.5 - 16.6 - 30.0 - 23.5 - 25.5 + 23.0 + 12.1 + 5.2	++++++++++++++++++++++++++++++++++++++	4·5 2·2 9·2 9·2 10·4 17·6 12·6 25·9 16·7 3·1 11·7 5·1 3·7 8·2	- 2·6 + 6·9 - 22·1 - 19·1 - 23·1 - 8·1 - 5·1 + 1·1 - 7·1 + 2·1 + 1·1 - 7·1	0 - 9 + 1	2·1 12·1 1·7 14·0 11·2 12·7 16·3 1·9 3·6 9·9 1·6 1·6 2·6	+ 16 0 + 8 0 + 0 0 + 3 7 - 1 0 + 17 0 + 14 0 + 6 0 + 7 1	0 + 20· 0 + 23· 3 + 17· 7 + 20· 3 + 14· 10· 10· 10· 10· 10· 10· 10· 10	1 + 1 + 2 + 3 + 3 + 4 + 1 + 4 + 3 + 4 + 7 + 4 + 2 + 4	27.7 33.8 30.4 28.4 24.8 24.8 27.7 33.3 27.3 11.3 10.7	+25:2 +30:1 +36:1 +36:1 +32:1 +26:2 +29:1 +27:1 +12:1 +26:1 +15:1	+10·2 +31·6 +29·6 +36·8 +28·8 +28·8 +22·2 6 +27·4 +12·5 +12·5 +12·5	2 + 16· 5 + 30· 6 + 20· 8 + 21· 9 + 26· 6 + 21· 1 + 6· 9 + 11· 7 + 2· 3 + 18·	1 + 1 1 + 20 8 + 12 6 + 33 8 + 33 7 + 18 7 + 21 7 - 18 1 + 10 9 - 1 1 + 12	·5 — ·2 + ·9 + ·1 + ·1 - ·6 - ·2 + ·2 + ·6 + ·4 +	10·4 12·3 6·7 16·2 21·0 22·5 11·2 2·0 5·0 9·4 2·5	- 7 11. + 2. + 7. + 8. + 13. + 8 22 1.	1 — 15·66 — 9·73 — 11·88 + 6·40 — 8·75 — 11·88 — 23·	7 — 11· 3 — 16· 3 — 16· 1 — 2· 1 — 0· 9 + 6· 7 — 8· 3 — 18· 6 — 43· 1 — 16· 3 — 16· 3 — 12·	4 — 13 4 — 17 5 — 17 2 — 0 6 — 10 2 + 6 6 — 9 3 — 24 5 — 45 5 — 22 5 — 13 1 — 17	·8 — 15 ·5 — 20 ·3 — 11 ·5 — 3 ·1 — 3 ·4 — 3 ·4 — 3 ·1 — 22 ·7 — 17 ·8 — 12 ·9 — 17	1-1 - 11 1-1 - 12 1-1 -	1·2 5·5 2·2 3·5 4·2 9·6 3·1 5·7 2·7 4·3 5·1 5·8
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DIURNAL INEQUALITIES OF THE MAGNETIC COMPONENTS, DECLINATION, INCLINATION AND HORIZONTAL FORCE—SELECTED DISTURBED DAYS.

and Season. Jan Feb Mar April May June Juny		274	. Esi	cdaler	nuir			DECL	INAT	TION	(meas	ured	positiv	e tow	ards ti	he We	est) (I)isturh	ed Da	ws).					
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Mar April May June	- 1.	0:01	T.TE	-2.74	-2.07	-0.09 -2.53	2·T2	1+0.15	1-0.33	1-1 T · 87	1-2.83	1+3.08	1-4.85	1+6⋅16	1+5.26	1+2.33	4 3.04	-0.20	-2.42	: — I • 7 5	-2.84	-2.75	-3.20	-3 ⋅34	-2"
April May June		-T.58	-T.U3	-3.10	-2.45	-0.06	T·67	- T · 77	- I·67	I·37	+1.01	1+3.38	1+6.42	I+8·10	+6.75	1+5.77	+5.59	- +3⋅15	-3.14	ı 2·60	-2.42	-3.94	-4.50	-4·80	l 3∙:
June	- 1.	-2.10	-2.22	-2.02	- T + 20	140.67	-2.25	-2.22	-3.60	-2.63	I-T-58	1+ r • of	+ 5.34	+7.41	1+7.87	1+6.44	+4.17	-I-13	1+0.64	ıl— o∙ 76	−1. 63	-2.37	1-4 ⋅38	-3.20	- I •
	- 1	T.02	- T.OT	-2.06	4 · 2 T	4.72	5.35	-5.41	- 4·5T	-2.40	-0.55	1-2.25	11-5·18	I + b⋅57	→ 7・37	1 - 7 39	1+D.34	1-5.03	1+1.21	1-0.30	-0.00	-1.30	I0·72	.ı— I∙88	-2.0
inia	••	-2.85	-4.08	-0.65	-4.16	-4.79 -2.57	-3.68	-4.03	-3.53	-2.15	-0.58	+1.71	+4.23	+6.25	+7·07	+5.75	+5.20	+5.41	+3.14	+0.70	+0.10	-1.15	-2·81	-2.07	-2·
Áug	- 1.	_ T.E.	T •60l	T •77	-2.24	-4.25	_4.95	- 4.80	1-2·80	- T :05	1 T . T 2	1-13.05	1-5.50	(+6∙50	+ 5.71	(+ <i>a</i> ·71	1-2.03	1+I·7I	1+1.56	1+0.05	-0·84	-2.27	1-2.64	1-2.25	/ I ·
Sept	- 1.	-6.00	-2.54	-2.56	- T.55	- T . 22	1 T . 2 T	1-0.8r	-0.50	I-0.13	1+2.12	1 + 5.03	1 + 7.53	1-47-84	1+6.36	1-1-5-80	-4·4I	1+3.73	- I · O 5	1-2.43	-2.02	-4.27	15.74	-8.71	1-0.6
Oct	- 1.	-2.87	-2.06	-0.74	1 + T · 87	1-4.16	+4.65	1-13.66	1-2.04	I-1- 1 ⋅ 68	1-2.44	1-13.12	1 + 5.24	1+6.11	+6.12	1-1-5-58	1-1-68	-4.24	-0.40	14.08	-7.05	-9.13	J-8·22	I-4·64	-2.
Nov	••	-2.79	-2.14	-1.47	-1.16	-0·79 +0·52	-0.40	+1.98	+0.57	+0.30	+0.92	+1.76	+2.48	+2.69	+2.83	+2.73	十2:42	+2.33	+2.02	+1.00	_4.4Q	-3.59	-4.67	-3.58	-3.
Dec	.	-1.41	+0.09	—0∙2 0	+1.39	+0.52	+0.25	+0.40	+0.14	_0.05	+0.23	+1.22	7 2 35	T-2-74	T 2 31	72.00	T 02	7 53	, 00.	0 33	1 10	3 39	2 30	2 34	
Year		-2.31	-1.69	-2·08	-1.74	-1.17	–1. 60	-1.49	-1.48	0.96	+0.56	+2.51	+4.64	+5.78	+5.63	+4.88	+3.63	+2.04	+0.52	-0.72	-1. 89	-3·0 9	-3.63	-3.60	-2"
Winter	.	-1.54	–o·50	-1.26	_o·8o	-0·72	o·55	+o·85	+o·33	+o·36	+1.23	+2.00	+2.99	 +3·67	+3.35	+2.80	+2.15	+1.26	+0.35	o·53	-2.19	-3.26	-3.76	-3.58	-2.
Equinox		-3.41	-2.24	-2:11	_o·86	+1.30	+0.49	−0·5 6	_o·95	−0 ·94	+1.00	+3.37	+6.13	+7:37	+6.77	+5.90	+3.96	+1.04	-1.01	-2.47	-3.28	-4·93	-5.71	-5.34	-3.
Summer		1 •99	-2.31	-2.88	-3.56	-4·09	-4.74	-4 ⋅75	-3.81	-2.30	-o·53	+2.15	+4.81	+6.31	+6.77	+5.95	+4.77	+3.81	+2.23	+0.84	-0.31	-1.00	-1.41	-1.88	-2"
										INCI	LINAT	rion	(Dist	urbed .	Days).	•									
275. E	Esk	cdalen	uir.			,		,					,	. , .			, -	, ,	,	, , ,	, 1	-, -	, , , ,	79	923.
[an		+0.18	-0.16	0.22	_0:40	-o·39	-0.80	-0.83	n.q2	-0:41	-0:03	⊥0:2⊺	±0.25	-0.03	-0.16	-0.03	+0.04	+0.10	+0.89	+0.58	+0.43	+0.63	+0.49	+0.23	+0.
Feb		0.80	-0.52	0.94	1-0.24	0.72	O : 7T	-0.51	-0.24	140.28	⊥ 1 ⋅32i	10.47	1-0.50	1+0·17	-0·15	+0.50	-0.04	-0.07	+0.37	+0.20	+ I · I 0	—o∙oŏ	I-0.40	-0.02	1+0
1ar	.	-0.42	1.9R	-0.42	-0.83	-0.66	-0.82	-0.T4	10.22	1-0.76	1 T · 46	± 1.62	+ T . 2 T	+0.03	+0.54	-0.62	-0·36	-0·20	+0.44	+0.00	+0.231	0.00	-0.93	1-0.59	-0
pril		0.77	0.00	0.00	LICATO	0.66	0.82	الاميم ال	-L-0.81	⊥ T • 2 2	1 T. C.	1.ΩΩ	1 T.65	1-0.85	+0.10	+0.33	+∩∙ดงเ	-0.731	-0.371	- I · O 5 I	0.431	-1.17	-0.00	-0.70	1-0
lay		+0.43	+0.09	-0.73	-0.23	-0·05 -0·34	+0.33	+1.05	+1.47	+1.69	+1.72	+1.26	+0.57	+0.35	_0.40 -0.01	-0·33	-0.08	-Z·U1	-0.68	-0.62	-0.39 -0.83	-0.50	-0.42	-0.76	-0 -0
une		-0.20	0.70	10.08	140.05	O · T 2	10.T2	10.80	1.26	1 T . 50	T 1.12	± T ⋅ 28	⊥1.74 <i>1</i>	+0.61	+0.14	-0.23	-0.04	-0.7I	-1.72	-1.491	o·991	-0.72	-0.95	1-0.97	— 0
Aug	- 1	0.05	0.26	0.50	0.40	0.82	0.22	1-0.58	10.75	140.75	1 T . C T	1.7U	L 0.72	10.47	+0.111	0.00	0.03I	-0.201	-0.741	-0.011	U.90 I	-0.20	-0.74	1-0.25	1-0
Sept		1 0.07	T.T.	T.08	1.71	T • T 77	T.TO	LOTE	-L0.16	1.4.0.02	1 .60L	1.FO	- T • 2 T ■	T T .O.I	±0.38F	-0.10	+0.32 l	-0.10	+0.10	+0.17	+0.311	+0.00	-0.59	O·03	1-0
Oct	·• ·	-1.21	-1.48	-0.79	-2.22	-1·50 -0·81	-1.29	-1.77	-o·59	+0.71	+0.55	+0.20	+0.32	+0.70	+1.04	+0.00	+1.54	+1.00	+1.70	+1.09	+0.92	+0.10	+0.41	-0.30	1-0
Nov Dec	.	-0.63	+0.01 -0.21	-0.42 -0.42	-0.37	-0.92	-0.92 -0.42	-0.90 -0.90	0.89	-0.60	+0.08	+0.40	+0.37	+0.48	+0.53	+0.42	+0.70	+1.20	+0.32	+0.26	+o·86	+0.09	+0.30	+0.05	-0
Year		-o·37	–o·49	-0.43	-o·63	−0 ·68	–o·61	-0·12	+0.51	+0.40	+1.15	+1.11	+o·83	+0.55	+0.19	-0.10	+0.14	-0.22	–0·0 9	-0.03	+0.06	-0.31	0.22	-0.41	-0.
Winter		-o·33	-0.29	-0·43	_o·38	-o·71	−0 ·81	-0.79	-o·73	-0.23	+0.47	+o·41	+0.33	+0.23	+0.00	+0.23	+0.23	+0.41	+0.45	+0.41	+0.70	+0.31	+0.20	+0.14	+0.
Equino x	- 1	1			1			1			- 1			- 1		- 1	- 1	,	- 1	1				1	
	- 1				I										- 1		1	1	1		- 1			1	1
Summer	··	-0.13	– 0·16	0.19	–o·35	-o·33	0.00	+o·85	+1.50	+1.38	+1.69	+1.61	+1.01	+o·56	-0.03	−o·57	-0.19	— I ·04	-1.21	-o·88	-0·77	−0·5 9	-0.63	_0.81	-0.
270 =									ноі	RIZOI	NTAL	FOF	RCE (Distur	bed D	ays).								10	923.
276. Es			. 1	2/	1 2	1 22 1	2	2/ 1	12 l	12	2/ 1	2/	γΙ	ν 1	γ	ν	γ	γ	ν	νΙ	γΙ	γΙ	γ	ν	Ιν
an	. .	- 3.5	+'0.1	–′o∙3	+ 3.8	+ 3.7	+10.5	+'9.7	+11.5	+ 4.4	-γ 1·4	_ ^γ _{5·0}	_ 5.2	– ′o⋅4	+ 2.0	+ 1.7	∔ լ.յ	— o⋅6	- 9 ⋅3	- 4·I	- 2.7	- 5.7	- 4.1	- 2.0	- !
eb		1 ~	1 4 4 1	1 2.8	T . F	1 1 77.31	M.XI	L 5.01	0.5	6.61	1361.13	0.0	O:OI	2・41	+ 2.2	- 2.2	- O'u	- 0.0	T 3 1/1	T 3 01	- 0 71	7 4 9	1 .7 4		1 4.
Iar		2.6	~ 1	- h.h	1 T • 4	+ 2·7 + 4·8	⊥ 6.01	- T.O	= = .2	T2.71	22.6	― ソカ・31	-21.21	- 13·M	- 4.7	+ 14 "/	+-14-51	- TO 91	T 0 1	T 1 0	T 0 9	0 0	1	1 00	1 1
April May	- 1	TO.5	R.RI	L 4.2	2.2	4.2	7.7	T 77.01	22 .7	28.4	3V·0	-24.2	- T2 ·O	- 7·0	+ 6.5	→ 8.01.	+ 7:31	+37.5	+01.8	+ 19.0	+14'0	T 14 'O	7 10 3	7 40 0	_
une	- 1	1 7.0	_ 0.2	A-8	1 5.0	ام• تاسا	- 0.7	- T6.81	-22.0	-25.4	25.6	24.7	- TO: 4	T 5 · 1	- T.T	+ 29 2	+ Q·21	+ 20.11	+ 22.7	+10.01	+ 10.71	T 10.91	T 10.21	T 9'9	17
uly	- 1	1. 2.5	2.61	- 6·0	1 4·b	2.0	- 4·6	- T 4.2	- TO:2	-2215	22·XI	22.51	2:7·91	- TO:21	- 2.0	+ 4·11	+11'71	+ 14 2	T 00 0	T 40 3	T 40 31	T +3 31	1 *4 / 1	1 -3 ~	1 1
lug	1.	L 5.0	上 r・2	⊥ 6.2	1 5.4	+ 9·8 + 8·3	+ 1.0	- TO:2	- T2.T	T 4 · T	-25.4	—3U·U	- TA:0	— 0·51	- I·7	+ I · Q	+ 2.7	+ 7.71	+ 14.2	T 14 91	TO.O.	十 / 山	T10.1	7 4 0	lT.
Sept Oct	- 1.	⊥ 8.el	上 へっつ	_ 1.6	14 TO:0	1 12·6	T T ⋅ SI	+21.51	± 7.0	— 8 ∙τl	- 5.4	n·81	- 1.4	- 1.2	- 4·0	+ 5.11	- 4.0	+ 4.0	- 9.5	-13.2	- 0.41	_ 3 4	~~~~	- 0.3	_
JOZZ	- 1	0.6	_ T.C	1 2.2	11 5.6	I⊥ TO•Ol	⊥ to•o	10.9	X.e.	L-L- 0.21	0.7	- 7.0	4.2	4.3	- T·7	→ 0. 01	- 0·7I	- 2.21	0.0	- 3'0		T 0 91	3 31	- 3/	1
)ec		+ 7:4	+ 4.9	+ 3.6	+ 3.0	+ 10.0	+ 9.2	+11.3	+10.9	+ 7.1	− 3·o	- 9·2	— 6·8	- 7·4	- 6.5	- 4·o	- 6·6	−13·1	— I·2	− 0.9	- 8·6	+ 0.9	- 3·7	- o.o	+
Year		+ 0.9	+ 1.3	0.0	+ 3.8	+ 5.3	+ 5.1	— o·6	- 4·7	-11.6	−18 ·6	—18·3	-14.0	- 8.6	- 0.9	+ 5.6	+ 4.3	+11.3	+10.0	+ 7.9	+ 5.5	+ 7.0	+ 3.9	+ 4.3	+
Vinter		+ 2.8	+ 2.0	+ 2.3	+ 2.7	+ 8.0	+ 9·4	+ 9.1	+ 8.3	+ 1.3	 8 ⋅6	— 7·8	— 6·з	- 3.9	- o·5	_ r·o	+ 0.2	- 1·8	- 1·9	- I·3	- 5·5	+ 0.3	- 1·5	– 1 ·9	<u> </u>
	1	1			1	+ 7.1	Ì			i l			1	1	1			- 1		i i				1	1
xon mp:	- 1	! (1	f i	i	1 1		1 1	1			- 1	- 1	ì				1	- 1	1			ļ
ummer	,	ا ما			L + - +	11 0.0		+ ,	+^ -		00 m				انتميد	4.70.0	1 7.7	+21.0	+28.2	+20.5	+17.6	+13.6	+11.4	+12.0	1-

RANGE OF MEAN DIURNAL INEQUALITIES FOR THE MONTHS, YEAR, AND SEASONS OF 1923.

Note.—The ranges are those shown in Tables 259 to 276, in the preparation of which the non-cyclic change has been eliminated.

277. Eskdalemuir. 1923.

Month and Season.	" All " Days.			Quiet Days.			Disturbed Days.			" All " Days.			Quiet Days.		Disturbed Days.			
	N.	W.	V.	N.	w.	v.	N.	w.	v.	D.	I.	Н.	D.	I.	Н.	D.	I.	Н.
January February March April May June July September October November December Year Winter	7 15.6 24.2 29.7 42.9 40.8 43.6 35.5 38.4 35.5 35.6 15.6 12.0	23.0 25.5 34.3 50.6 40.0 48.2 42.6 42.6 42.6 33.6 22.8 18.5	γ 9.0 14.2 20.9 19.6 23.4 21.2 15.3 17.0 17.3 20.5 6.8 7.9 14.5	γ 10·1 20·5 23·7 41·4 39·6 38·9 33·5 38·8 34·7 25·1 15·1 8·0 25·6 12·8	γ 16·4 17·5 27·5 43·4 36·4 43·1 40·1 39·0 26·6 15·4 13·6 28·1 14·6	γ 4·4 5·1 13·9 14·2 20·5 15·7 14·2 13·1 8·4 4·8 4·1 9·8 3·6	γ 21·3 35·0 46·8 56·1 63·6 56·0 57·9 28·7 21·2 23·6 31·9	7 39·5 43·6 54·5 58·6 66·8 58·4 57·9 53·0 72·5 35·6 36·0 41·8	γ 21·4 46·6 75·8 38·0 53·6 46·9 30·1 20·5 82·2 98·7 21·1 20·2	5.02 5.79 7.93 10.56 8.26 9.69 8.36 9.36 8.32 7.70 4.96 4.06 6.67	0.92 1.32 1.49 2.40 2.35 2.54 2.12 2.30 2.02 1.71 0.92 0.79 1.37	γ 13·1 19·6 24·1 41·4 42·2 45·3 38·8 38·0 32·9 23·6 14·1 10·4 25·3 13·8 28·7	3:47 3:89 6:32 9:32 7:85 9:09 8:72 7:85 9:04 8:45 5:43 3:44 2:98 6:22 3:20	0.61 1.26 1.11 2.52 2.34 2.40 2.06 2.36 2.10 1.46 0.83 0.43 1.50	9.0 19.0 19.1 41.7 41.0 41.0 34.8 37.5 23.6 13.0 5.6	8·26 9·50 12·90 12·25 12·80 11·86 12·05 11·45 16·55 15·25 7·50 7·44 9·41 7·43 13·08	1.81 2.16 2.88 3.06 3.73 3.85 3.46 2.65 3.31 3.98 1.46 2.12 1.83	γ 20·8 29·0 44·2 52·2 68·8 64·8 58·5 46·5 38·7 45·8 19·9 24·4 29·9 18·0
Summer	38.7	43.0	19.0	37.1	38.8	15.9	52.0	57.9	33.8	8.88	2.23	39.4	8.30	2.24	38.1	11.52	2.90	55·o

NON-CYCLIC CHANGE (24h.—0h.).

Eskdalemuir.

MEAN VALUE OF THE SQUARES OF THE ABSOLUTE DAILY RANGES. (Unit, $100\gamma^2$.)

279. Eskdalemuir.

1923.

Month.	" All " Days.			Quiet Days.			Disturbed Days.			R_N^2	R _w ²	R_{v}^{2}	$R_N^2 + R_W^2$	$R_N^2 + R_W^2$	Mean Character
	N.	w.	v.	N.	w.	V.	N.	w.	v.	T/N	TCM		ICM ICW	$+ R_V^2$	Figure.
January February March April May June July August September October November December	γ 0·0 0·0 +0·4 -0·3 -0·1 +0·4 -0·2 -0·6 -0·1 +0·5 +0·9	γ -0·4 -1·0 +0·3 +0·5 -0·6 +0·8 -0·4 -0·4 +0·4 -0·3 +0·2 +0·2	γ -0·4 -0·5 +0·2 -0·1 +1·1 +0·5 -0·3 -0·4 -0·1 -0·8 -1·5	γ -0·6 +2·0 +2·2 -0·8 +1·8 +3·6 +1·0 -0·6 +1·4 +2·8	γ +1·6 -1·8 +0·8 -1·4 0·0 +0·8 +1·8 +1·2 -1·0 0·0 -1·4 +1·6	7 -1·2 -0·8 -1·2 +1·7 +0·2 -0·4 0·0 -0·8 +0·6 -0·8 -1·2 -2·6	7 -1·4 -4·6 0·0 -3·6 -9·0 -11·6 -11·2 -3·6 0·0 -7·8 +1·8	γ -2·2 -6·2 +2·6 -1·8 -7·2 -2·8 +1·2 +3·0 -18·6 -2·0	7 -2·4 -0·6 -6·4 -6·2 +3·2 +5·0 +0·4 -3·4 +3·6 -4·2 -1·6	17·2 60·7 55·4 55·1 45·4 56·9 41·0 37·3 80·5 70·8 22·8	26·2 45·5 86·2 48·0 41·3 54·5 34·5 31·7 72·7 66·6 29·5 25·2	4.0 18.2 37.51 12.72 17.3 15.63 8.9 6.0 50.9 60.9 3.6 3.8	43.4 106.2 141.6 103.1 86.7 111.4 75.5 69.0 153.1 137.4 52.3 49.5	47.4 124.4 187.41 118.12 104.0 129.03 84.4 75.0 204.0 198.3 55.9 54.74	0·35 0·54 0·52 0·47 0·45 0·40 0·29 0·32 0·37 0·39 0·43 0·39
Year 1923	_		_	-	–	_	_	_	_	47.3	46.8	20.0	94.1	115.2	0.41

1923.

1 Mean of 29 days; 2 Mean of 29 days; 3 Mean of 28 days; 4 Mean of 30 days.

MEAN MONTHLY AND ANNUAL VALUES OF TERRESTRIAL MAGNETIC ELEMENTS.

(All days except those noted in monthly tables.)

280. Eskdalemuir. errota 1964 1923.

Month.	North.	West.	Vertical.	Total.	Declination (West).	Inclination (North).	Horizontal Force.
January February March April May June July August September October November December Year 1923	γ 15999 16002 16000 16007 16012 16014 16024 16022 16016 16011 16015 16013	y 4687 4680 4675 4670 4665 4663 4658 4655 4651 4646 4643 4637	y 44935 44947 44949 44948 44946 44951 44976 44978 44950 44959 44961 44946	y 47928 47940 47940 47941 47946 47972 47973 47944 47950 47953 47938	0	69 38·7 69 38·9 69 39·2 69 38·8 69 38·6 69 38·6 69 38·6 69 38·8 69 39·3 69 39·1 69 39·0	7 16671 16672 16669 16674 16678 16679 16687 16685 16678 16671 16674 16671

Values of a_n , b_n in the series Σ (a_n cos 15 $nt^o + b_n$ sin 15 nt^o), t being reckoned in hours from midnight G.M.T.

281. Eskdalemuir.

(Longitude of Eskdalemuir Observatory, 3° 12' W.)

1923.

			No	orth Co	mponer	nt.					West	Comp	onent.				i		Verti	ical Cor	nponen	t.		
Month and Season.	a ₁ .	b ₁ .	a2.	b_2 .	a ₃ .	b_3 .	a4.	b ₄ .	a ₁ .	b_1 .	a_2 .	b_2 .	a_3 .	b_3 .	a4.	b ₄ .	a_1 .	b ₁ .	a ₂ .	b_2 .	a ₃ .	b ₈ .	a4.	b4.
											"All	" Da	ıys.											
Jan. Feb. Mar. Apr. May June July Aug. Sept. Oct. Nov. Dec. Year W. Eq. S.	7 + 2·4 - + 6·2 - + 10·5 - + 15·9 - + 12·2 - + 14·2 - + 13·7 - + 4·3 - + 2·0 - + 3·7 - + 12·4 - + 13·1 -	- 2·6 - 0·2 - 2·4 - 6·4 - 5·7 - 4·6 - 2·8 + 1·0 + 1·2 + 2·2 - 1·5 - 1·1	-5·5 -6·4 -9·5 -8·3 -9·2 -6·6 -7·5 -7·0 -6·3 -3·7 -2·8 -6·3 -3·8 -7·3	-0·6 -1·3 -0·9 +0·4 +0·9 -0·3 +2·2 +1·1 +0·8 +0·2 -0·9 0·0 -0·6 -0·1	+2·2 +3·2 +3·6 +1·5 +2·0 +0·9 +1·3 +1·9 +2·0 +1·1 +1·7 +1·9 +1·7 +2·7	-1·8 -2·1 -2·6 -0·4 -1·0 -0·7 -2·1 -2·6 -1·6 -1·7 -0·9 -1·6 -2·2	-0.4 -0.6 +0.3 +1.0 +0.1 +0.6 +0.4 +0.1 +0.3 0.0 +0.1 -0.1	+0·4 +0·4 +1·5 +0·1 +1·2 +1·0 +0·7 +0·5 +0·8 +0·5 +1·0	- 6·8 - 7·1 - 8·8	- 2·6 - 6·9 - 12·0 - 14·8 - 17·1 - 15·5 - 12·0 - 8·9 - 2·5 - 0·8 + 0·6 - 7·9 - 1·0 - 7·6	+1·2 - +3·2 - +2·8 - +3·1 - +3·2 - +3·1 - +6·0 - +2·8 - +0·9 - -1·0 - 0·0 - +2·1 - -0·1 - +2·4 -	+ 5.0 + 7.4 + 11.1 + 7.1 + 10.0 + 7.1 + 6.6 + 6.9 + 6.8 + 3.8 + 4.0 + 6.7 + 4.3 + 8.0	-0·5 -2·2 -3·2 -2·1 -2·4 -3·6 -4·1 -2·5 -2·1 -1·3 -2·3	-1·7 -3·5 -5·1 -1·5 -2·3 -2·3 -2·5 -3·2 -3·1 +0·5 -0·6 -2·2 -0·5 -3·7	+0·6 +1·1 +2·5 +0·7 +0·6 +1·6 +2·8 +1·5 +0·4 +1·1 +0·8 +2·0	+1.6 +2.1 +1.4 +0.3 +0.4 +1.1 +1.3 +0.6 +1.8 +1.2 +0.7 +1.2 +1.3 +1.5	+ 0·2 + 0·7 + 2·5 + 4·4 + 3·5 + 2·9 + 3·6 - 0·1 + 0·2 + 0·7 + 1·4 + 0·6	- 5.9 - 6.9 - 4.0 - 5.2 - 5.2 - 2.8 - 5.0 - 7.4 - 3.4 - 3.8 - 4.8 - 4.8 - 4.4 - 5.8	- 2· - 4· - 5· - 5· - 3· - 4· - 3· - 0· - 3· - 3· - 1· - 4·	6 -0·5 4 -0·8 8 -1·5 4 -2·3 8 -1·6 2 -1·0 7 -1·9 1 -0·2 4 -1·9 7 -0·2 9 -0·4 5 -1·0 1 -0·5 5 -1·5	+1·9 +1·8 +0·7 +1·3 +0·8 +2·0 +1·4 +1·6 +0·2 +0·5 +1·1 +0·4 +1·7	+0·5 +0·5 +0·3 -0·3 +0·8 0·0 -0·1 -0·2 +1·0 -0·9 -0·5 +0·1	-0.5 -0.5 -1.3 -0.2 -0.2 -0.1 -0.8 -0.7 -1.4 -0.4 -0.2 -0.5 -0.5	-0·2 -0·6 0·0 +0·1 +0·1 0·0 -0·2 -0·2 +0·1 -0·1 -0·1
0.	11131	33	19	100	1124		1100	100	1 43			iet De	·		1103	100	1 3 0		1 7	/	111		1 9 3	
Eq.	+ 8.8 - + 2.9 - + 10.8 - + 12.7 -	+ o·2 - o·8	-3.7 -6.6	-0.1 -0.6	+1.4	-1·0 -1·8	0·0 -0·3	+0.5 + 1.2	- 3·4 - 3·5	— 2·o — 8·o	+2·9 - +0·7 - +3·3 -	+ 5·1 + 3·0 + 5·6	-2·6 -1·8 -3·5	-3·5	+1.0	+0.8 + 1.5	+ o·5 + 3·2	- 1·1	- 0 - 2	·8 — 0·2	+0.6 +2.0	-o⋅3	-o.8	0.0 0.0 -0.2 +0.1
													Days											
Year W. Eq. S.	+11·2 - + 5·2 - +13·1 - +15·4 -	+ 3·9 - 2·6	-8·1	-0·5 +0·3	+3.1	-2.5 -2.2	-0·5 -0·5	+1.0 −0.3	-14·1 -12·3 -19·2 -10·6	+ 0.5 - 2.1	-0.8 - 0.2	+ 5·8 + 12·7	+0·5 -2·0	+0.3 -4.8	+0·8 +2·3	+2.5 + 0.9	- 0·1	3 - 22.6	- 3 - 10	·4 -1·4	+1·9	-0.1 + 2.0	-0·4 -0·6	+0.1 -0.1

HARMONIC COMPONENTS OF THE DIURNAL INEQUALITY OF MAGNETIC FORCE.

Values of c_n , α_n in the series $\Sigma c_n \sin (15nT^\circ + \alpha_n)$, T being Mean Local Time reckoned in hours from midnight.

1923. 282. Eskdalemuir.

2021	-oru	iloiliuli	•																					.020.
			N	orth Co	mpone	ent.					We	est Com	ponen	t.					Ver	tical Co	npone	n t .		
Month and Season.	c ₁ .	α1.	c ₂ .	α2.	c ₈ .	α _s .	C4.	α4.	c ₁ .	α1.	c ₂ .	α2.	c ₃ .	α3.	C4.	α4.	c ₁ .	α ₁ .	c ₂ .	α2.	C3.	α3.	C4.	α4.
											",	4 <i>ll"</i> L	ays.		· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·							
Jan. Feb. Mar.	γ 3·0 6·7 10·5	55·1 70·6 94·3	γ 3·3 5·5 6·5	258·3 269·6 265·0	γ 2·6 2·8 3·8	148·8 139·8 133·1	γ ο·7 ο·5 ο·7	331·1 330·7 319·7	γ 6·7 8·7 11·6	264·2 256·0 236·6	γ 4·4 5·2 8·1	0·6 19·9 29·5	γ 1·1 1·8 4·1	265·2 204·5 221·8	γ 2·0 1·7 2·4	37·9 33·2 40·9	γ 4·5 5·9 6·9	167·4 181·3 177·8	γ 0·8 2·5 5·0	238·3 256·7 258·4	γ 0·4 0·9 2·0	63·2 84·1	γ ο·5 ο·6 ο·8	272·5 256·7 231·5
April May June July Aug.	16·1 13·8 15·3 13·1 14·5	101.6 120.8 115.2 114.0	9·5 8·3 9·2 6·7 7·8	270·9 279·5 281·8 273·7 292·6	4·4 1·6 2·2 1·1 2·5	135·1 115·6 127·3 140·2 158·6	1.6 1.0 1.2 1.1	25·7 99·9 19·5 45·3 34·7	14.0 15.6 17.3 15.9		7·8 10·4 7·8 8·9	20·3 30·9 23·8 31·1 48·5	6·0 2·6 3·1 3·7 4·4	221·8 244·9 231·7 231·0 245·1	2·9 0·7 0·5 1·3 1·4	73.9 75.5 32.9 42.8	4·7 6·8 6·3 4·7 4·6	151·9 143·0 149·7 144·6 131·8	5·8 6·0 5·3 4·1 4·1	253·5 261·2 266·0 249·6 273·6	1·9 0·7 1·5 0·8 2·0	88·8 125·6 67·2 97·6 102·4	1·3 0·2 0·2 0·1 0·8	284·7 317·2 306·1 287·3 267·4
Sept. Oct. Nov. Dec.	13·9·7 4·5 3·0	104·6 87·4 77·3 45·3	7·I 6·4 3·7 2·9	285·3 284·0 279·8 257·9	3·2 2·5 2·0 1·9	153·1 138·0 158·3 127·1	0·9 1·1 0·8 0·5	343·7 20·0 35·9 8·9	12·7 9·9 7·1 6·6	228·7 258·8 266·5 278·1	7·5 6·8 4·0 4·0	28·3 14·3 352·1 6·0	5·2 4·0 2·2 1·5	241·5 228·3 291·8 254·1	1·7 3·3 1·9 o·8	81·4 70·0 63·8 40·3	5·0 8·2 3·4 3·9	184·4 207·6 179·7 172·5	4·8 3·6 0·7 1·0	252·5 275·1 260·5 253·3	1·4 1·9 1·0	107·0 69·0 177·4 145·7	0·7 1·4 0·4 0·2	270·9 274·6 296·4 251·3
Year	9.9	101.8	6.3	276.8	2.5	140.1	0.8	20.1	10.4	224 · 1	7.0	23.7	3.2	235.8	1.6	55.5	5∙0	167.4	3.6	259.7	1.1	95.1	0.6	272.0
W. Eq. S.	4·2 12·5 14·2	65·3 98·2 115·3	3·8 7·3 8·0	267·4 275·9 282·1	2·3 3·5 1·8	143·8 139·2 137·3	0·5 1·0	357·5 5·6 47·2	7·2 11·6 15·7	265·4 232·4 200·0	4·3 8·4 8·6	5·6 23·1 33·3	1·4 4·8 3·4	256·0 228·4 238·3	1·6 2·5 0·9	44·7 66·4 44·3	4·4 5·8 5·5	175·5 184·1 143·0	1·3 4·8 4·8	252·6 258·6 262·7	0·5 1·7 1·2	130·4 85·8 94·7	0·4 1·0 0·3	270·2 269·7 282·3
											Q	uiet Do	ays.											
Year W. Eq. S.	9·0 2·9 10·8 13·4	103·8 89·7 97·7	6·1 3·7 6·6 8·1	277·0 267·7 275·8 282·2	2·3 1·7 3·1 2·2	135·1 134·3 134·8 136·4	0·9 0·5 1·3	8·2 14·8 357·5 20·2	8·4 4·0 8·8 13·6	204·6 243·6 206·7 192·6	5·9 3·1 6·5 8·1	36·1 20·2 36·6 41·7	3.5 2.1 4.9 3.6	238·3 251·3 234·4 236·4	1·6 1·3 2·1 1·3	55:9 63·5 59·7 41·8	2·8 1·2 3·3 4·5	105·2 157·5 102·1 95·2	2·5 0·4 2·8 4·3	270·0 276·7 272·0 268·1	1·3 0·7 2·0 1·4	101·1 125·5 92·2 102·4	0·5 0·9 0·4	278·2 279·6 269·2 295·6
											Dist	urbed 1	Days.											
Year W. Eq. S.	11·6 6·4 13·4 18·3	107·8 56·5 104·6 126·2	7·3 3·9 8·2 9·9	281·0 269·1 278·6 287·7	2·9 3·0 3·8 2·2	150·8 154·6 134·4 174·0	0·1 1·1 0·5 1·4	88·9 343·8 252·0 130·9	15·9 12·3 19·3 23·5	245·1 275·4 267·0 210·1	5·8 12·7	12·8 358·1 7·1 28·7	2·2 0·6 5·2 2·0	216·3 66·7 211·8 236·1	1.8 2.6 2.4 0.9	59·0 31·9 82·1 74·8	16·1 10·4 26·5 13·7	197·9 183·6 214·6 176·3	7·5 3·7 11·4 7·3	253·3 252·3 254·9	1·5 0·2 2·8 1·8	59·8 263·6 52·5 72·9	0·5 0·4 0·6 0·7	315·5 272·7 294·6 0·7
(19889)																								Q 4

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263.	ESKUA									 -	1	1			
		Time.	Desiral	Ampli	tudes.		_	Date.	Phase.	Time.	Period	Amplit	udes.	Δ	Remarks.
Date.	Phase.	G.M.T.	Period	A _n .	A _R .	Δ	Remarks.			G.M.T.		A _N .	A _E .		Temarks.
	ļ	h. m s.	s.	μ	μ	km.		Feb.	e	h. m. s. 9 37 23	S.	μ	μ 	km.	
Jan.		to					Small disturbance.	10	L	9 57 23					
12	•••	2 39 to 3 15	•••	•••	•••				F	10 40	•••		•••	•••	·
								19		o to			•••		Very slight disturbance;
13	L M _R	10 30 10 36)		•••	2					I	•••		•••		confused by microseisms.
		37 }	25	•••	~	"		21		r to	•••		•••		Slight disturbance; masked
	M _n	10 38	24	3	•••	•••				2	•••		•••	•••	by heavy microseisms.
	M _E M _N	10 39 10 49 \	20	•••	3	•••		23	? P _n	6 18 31			•••		Conford to a signature
		50 ∫	18	2	•••				e (? S) e(? SR ₁)	6 26 35 6 30 9	•••		•••		Confused by microseisms.
	F	11 10	•••	•••	•••	***			L	6 42	•••		•••		
21	i (? S)	4 23 6			•••	(3600)	L irregular and confused by		M _N F	7 3 7 30	20		•••		
	L F	4 26 46 4 45		•••	•••		microseisms.							-6-0	
							Confused by microseisms and	24	i P i S	7 45 50 7 54 52	•••			7650	Value of A _x is the largest
22	? S L	1 37 2 5	•••		•••		wind effects.		SR ₁	8 0 6	•••		•••		recorded. Impossible to assign time owing to
-	F	3	•••	•••				1	L M _x	8 8	18	68	•••		overlapping of records.
22	i Pz	9 15 42		•••		(8160)	i Pz approximate only, ow-		F	11 30	•••		•••		
	i S _B	9 25 10		•••	•••		ing to partial failure of time marks.	28	e _x (? S)	22 27 8			•••	·	
	SR ₁ SR ₂	9 30 9 33		•••	•••				L M _N	22 28 28 22 31	 12	 5	•••		
	L M _r	9 36 9 42·5	22		-7I				F	22 50			•••		
	M _E	9 45 5	19		-64			Mar.	? e _n	8 37 48					Record defective.
	F	II	•••	•••	•••			1	F	10			•••		
27	L	8 34			•••		Slight disturbance; confused	2	s	17 14 45					Initial phase masked by
	F	9		•••	•••		by microseisms.		SR ₁	17 22 21	•••				microseisms.
Feb.				İ			Confused by microseisms and		SR ₂	17 26 21 17 37	:::				
I	L F	20 26 21 30	•••	•••	•••		wind effects.		M _N	17 42 43	36	+110			
ĺ		•					Greatly confused by micro-		M _N M _N	17 49 41	24 21	十70 十59	•••		
2	? S L	1 27 14 ?			•••		seisms and wind effects.		M _n F	17 56 56	18	+65	•••		
	F	3	•••	•••	•••	•••			1	19 30					
2	P_z	5 19		•••		(8000)		3	e _n	22 36 22 43					
	i S _z SR₁	5 28 17 5 33 11	•••	•••	•••	···			L	22 53					
	SR ₂	5 36 15	• • • •	•••	•••					23 25	•••	•••	•••		
	F	9	•••	•••	•••	•••	77 71 1 1	4	e (? S) L	0 27 12 0 34					
3	i P	16 12 58	•••	•••	•••		Very severe disturbance. Records too confused to	ĺ	F	1 30					
					•••	•••	allow of identification of other phases.			7 30 to					Small disturbance.
			•••	•••	•••	•••	-	4	'''	7 30 to 8 30			•••	•••	
4		13 to 14			•••	•••	Slight disturbance; confused by microseisms.	13		20 to					Very slight disturbance.
					•••		_			21				•••	
5		23 to 24		•••	•••		Small disturbance; con- fused by microseisms.	14		21 to					Disturbance with a well- marked L phase. Record
							Trace of waves; greatly			23	•••	•••		•••	confused by overlapping.
6	•••	15 31 to 15 33		•••	•••		confused by microseisms.	15	Pw	5 44 26				2010	
		i					Confused by microseisms.		P _z e _z	5 44 ² 4 5 47 45					,
11	i _m e _n	23 5 52 23 II	•••	•••	•••				S _x	5 47 5°					,
	L F	23 25 24 I5	•••		•••]	i _n L _n	5 47 55 5 48 50			•••		
	_	-	ĺ						M _N M _N	5 51 0 5 51 58	18 18	+29 -33	•••		
12	i (? S) ? SR ₁	2 18 57 2 23 37	•••						M _N	5 52 37	14	-38	•••		
	L	2 31	•••						F	7			•••		m 1-1-1-1-1-1-1
	M _z	$\left\{\begin{array}{c} 2 & 34 \\ 35 \end{array}\right\}$	20	•••	9			16	e P _z	22 15 39					Times somewhat doubtful.
	M _r	² 39 40 }	20	-10	•••				e _z (?PR)					1 .	P masked by microseisms.
	M _w	2 49	16	-12				24	e P S	12 51 (30)				(8120)	r masked by microscisms.
	F	3 30	•••	•••	•••			}	SR,	13 0 54 13 5 (40)				\	
15		23 to	•••	•••			Slight disturbance.		SR ₂	13 9 13 12	:::				
		24	•••	•••					M _m	13 19 18	26	150 100	•••		
16	e _m M	7 2 57 7 22	18		3				$M_{\mathbf{x}}$	13 24 38 13 27 22	20 20	-96			
	F	7 50							M _w	13 34 2	20	-48			
1	1	l		ĺ	İ	Į.	Į į	l .	F	16	1	<u> </u>	<u>,</u>	· · · · · ·	

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203.	ESKUAI		1	1		ı		!	<u> </u>		1	I			1923.
Date	Phase.	Time. G.M.T.	Period	Ampli	tudes.	4	D 1	Date.	Phase.	Time.	Period	Ampli	tudes.		
		G.M.1.		A _x .	Az.	Δ.	Remarks.			G.M.T.		A _N .	Az.	⊿.	Remarks.
Mar.		h. m. s.	S.	μ	μ	km.		May		h. m. s.	s.	μ	μ	km.	
26		4 24 to					Traces of feeble disturbance.	cont.	L M _N	16 59 17 2 29	 30	 —185	•••		,
		4 52					T		M _E M _N	17 2 19 17 5	28 25 18	 -174	-127 	•••	
26		6 o to 6 15				:::	Traces of feeble disturbance.		M _N F	17 10 4		+ 83	•••		Wave motion continued until 21h.
26		14 30 to					Traces of feeble disturbance.	4	e e	22 40 57 22 45 17					
									i _E (?S)	22 51 3 23 10					
April.	/T.\							5	F	1 0				•••	
5	e (L) F	22 54 23 10						5		15 35 to 15 55					Trace of slight disturbance.
13	e P _n i S _n	15 42 (0) 15 51 1				(7600)	e P _N indistinct. Time approximate.	8		19 42 to					Trace of L waves. Very feeble.
	i _N (SR ₁) L _N	15 55 31 16 4					promission ,			20					recone.
	M _N M _N	16 15 4 16 17 7	18 16	28 -29				10	e _s	4 12 14 4 14 4					
	M _n F	16 26 24 18 30	18	-23 					e _B F	4 20 18 5 45					
13		21 15 to					Traces of slight disturbance.	12	?e₅ ? L	I 45 2 8					
19		21 50	•••		""		No horizontal component		M _N M _N	2 8 2 21 50 2 26 49	26 22	 15 9			
19	i, F	3 ² 7 39 5					records available.		F	3					
23	e P _E	3 29 40 3 33 II				9340		12		23 8 to 23 35					Feeble disturbance.
	e _s e S _s e _z	3 40 7 3 41 17					* .	15	L	5 12					Very feeble.
	SR ₁	3 46 5 3 59			-28				F	5 40	•••		•••	•••	Cliche disturbance
	M _s M _s F	4 6 19 4 14 15 6	15		+20 			15	? e _n e _E L	21 53 22 10 30 22 45				•••	Slight disturbance.
23	e _s	7 4							F	23 30				•••	
	e, e L	7 IO 30 7 20				:::	Feeble.	22		13 to 13 30					Slight disturbance.
	F	7 35	•••	•••	•••			23	eP _N	22 48 20				8120	
24	e L F e L	22 38 22 52 23 16					Slight disturbances.		eS _N	22 57 46 23 13				•••	
24	F	23 25					J		M _N M _N F	23 23 19 23 29 9 2	17	-9 13		•••	
25	L F	20 0 20 30			:::			25	?e	22 41					
27	L	11 23							L M _N	22 50 22 54	17				Confused by microseisms. and wind disturbance.
70	F	12			•••				F	23 30		•••	•••		Destructive earthquake in Persia.
29	•••	3 to 3 30					Slight disturbance.	25		4 to 5		•••	•••	•••	Disturbance; confused by wind and microseisms.
29	?S L	9 45 30 9 50						28	i P _z	1396				9740	
	F	10 45					L phase irregular.		PR _{1z} eS _N	I 42 50 I 49 53					eS and L not clearly defined.
30	L F	20 55 21 15							L M _N	2 12 2 21 46	 22	 16			
									M _N F	2 26 26 3 30	20 	13 			
May.	? S	11 5 46					The most marked movement	30	eP _z	8 38 46					No horizontal component records. From Pand PR,
•	e (? SR) L	11 11 46 11 29				:::	began at 11h. 5m. 46s. on NS. L. not well devel-	30	$PR_{1\dot{z}}$ P_{z}	8 40 55 18 5 8	•••	•••		 4740	$\Delta = 5600 \text{ km}.$
	F	12 15					oped.	30	PR ₁ eS	18 6 59 18 11 36	•••			***	
2	•••	16 50 to 17 20				:::	Small disturbance.		F	19 30					
4	P	16 37 38				7560		31		6 40 to 7 20					Slight disturbance shown on vertical record. No hori-
	PR ₁ PR ₂ i S	16 40 15 16 41 49 16 46 36						31	eP_z	22 13 9					zontal component records. No horizontal component
	1.3	10 40 30	<u> </u>	<u> </u>											records.

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283.	Eskdal	muir.													1923.
Date	Phase.	Time.	Period		itudes.			Date.	Phase.	Time.	Period	Ampli	tudes.		
Date.	Phase.	G.M.T.	Period	A _n .	Az.	⊿.	Remarks.	Date.	rnase.	G.M.T.	renod	A _w .	A _R .	⊿.	Remar ks.
June		h. m. s.	S.	μ	μ	km.		July		h. m. s.	s.	μ	μ	km.	
I	P	17 37 16				9340	Compression.	12	e F	10 20					
	S L	17 47 43 18 5 58								II 20	•••	•••	•••	•••	_
	M _N M _N	18 12 40 18 19 41	20 18	36 43				13	i P PR ₁	11 26 16 11 29 37			•••	9280	Compression.
	M _s	18 22 18	- 16	42		•••			SR ₁	11 36 40		•••	•••	•••	
		(20 30)			•••	•••			L	11 43·5 11 54			•••	•••	
I	P S	20 28 16 20 38 42				9320	Epicentreapparently the same as that of previous shock.	[M _N M _N	12 1 22 12 6 48	26 21	+63 +69	•••	•••	
	L M _n	20 57 21 5 25	20	 -16			Initial movements of P and of S in the two cases were		M _n F	12 10 40 14 30	17	+69 	•••		
	M _s	21 10 11	17	18		•••	very similar in form.							ļ	
	r	23 30	• • • • • • • • • • • • • • • • • • • •		•••			14	?eP _z ?eS	o 9 o 19 33		•••	•••		
2	•••	2 to 2 50					Trains of L waves of small amplitude.		L M _N	0 36 0 48 \	 26		•••	···	
3	? e₂	11 50							M	49 { 0 53 {			•••	•••	
3	F	13 10							F	54 ∫	17	7	•••	•••	
7		23 30 to				•••	Trace of slight disturbance		F	1 15	•••	•••	•••	•••	
		23 35			•••		on vertical record.	23	$\mathbf{e}_{\mathbf{x}}$ \mathbf{F}	21 51 22 8	•••	•••	•••	•••	
17	e F	18 10 6 18 30						29		10 to		•••			Traces of slight disturbance.
18	P	_				1				10 30		•••			
10	i,	8 36 6						31	e	5 58 7					
	e _m ?L	8 38 29 8 58							F	6 40		•••			
	F	10 30			•••			31	e e	15 19 31 15 28 47		•••			
19	iP e _n (?PR ₁)	22 53 44 22 55 55			•••	6730			?L F	15 43 17					
	PR ₂	22 57 25							-	- /					
	eS SR ₁	23 I 59 23 6 I5										ļ			
20	L F	23 13 0 15			•••	:::									
21	e (?L)	12 56					Small disturbance.	Aug.						į	
	F	13 15						I	LF	5 2I 6 25					
22	iS	7 6 35					P masked by wind disturb-	_		_				2950	
	SR ₁	7 12					ance. ⊿ probably about 8000 km.	I	e P i S	8 22 21 8 27 0					
	L M _w	7 21			•••	•••			L F	8 30 9		•••		:::	
	M _w	7 27 28 7 30	28	190	•••				L	17 38					
	F	31 🖍	21	150	•••		(Record failed before end of	4	F	18 20					
)	•••	•••				` disturbance.)	5		2 30					Trace of waves of low amplitude.
28	e _s (?S) L	15 17 20 15 19					Very feebly developed.								ampheade.
	F	15 26	•••		•••			8	e _{z} (? P)	12 11 56 12 20 24					? Two earthquakes.
29		11 30 to					Trace of disturbance.		e	12 21 8					
		12				•••			e (?S)	12 35.5					
	ļ								L M	12 42 12 50 \	17		10		
									F	51 ∫ 13 45					
July 2	1				1		Earthquake recorded in	10	L	1 27					
•		•••	•••	•••			early hours (approx. 2h		F	I 45		•••			
							4h.), but time marks were lacking.	10	?e	2 28 (40)		•••			
2	e _s	23 42 14	•••	•••		•••			e e	2 34 (20) 2 38		•••		:::	
5	L	2 27 2 33							L M _s	2 43 2 47	23	 6	•••		
10	?e,		***	***		•••			F	3 10		•••			
10	e,	0 43 II 0 47 4						10	e	16 19 27		•••			
	e _x (?S)	o 53 54 o 56 38	•••						L F	16 36 17 5	•••	•••		:::	
	L M _m	1 14 1 27 42	20					10	e	22 37 23		•••	•••		
	F	3 30	•••					11	F	0 30	•••	•••	•••	•••	

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		Time.		Ampli	tudes.			D-4-	Diversi	Time.	Period	Ampli	tudes.		
Date.	Phase.	G.M.T.	Period	A _B .	A _z .	Δ.	Remarks.	Date.	Phase.	G.M.T.	Period	A _N .	A,	⊿.	Remarks.
Aug.		h. m. s.	s.	μ	μ	km.		Sept.		h. m. s.	s.	μ	μ	km.	
11	e e L M _n M _g F	1 13 1 19 12 1 45 1 51 59 1 52 40 3 20	28 26	28				2 cont.	PR ₂ iS SR ₁ SR ₂ L M _w	3 4 29 3 9 35 3 14 34 3 19 4 3 27·5 3 34 40 3 34 47		 —120	 -109		S was followed immediately by two or three large sinusoidal movements; for N-S component period was 20s. and amplitude 145 μ .
12	e L F	6 33 27 6 56 7 35							M _N M _B M _N	3 36 23 3 36 40 3 39 56 3 43 24	21 19 19 17	-136 -119 -110	 - 168 		An aftershock of the great Japan earthquake of Sept. 1.
12	? e P ? e PR ₁ e S e (?SR ₁) L F	10 19 3 10 22 37 10 29 29 10 36 10 50 12				?9310		2	M _E M _N F	3 43 19 3 49 35 7 30 9 39 25	17 16 	 104 	105 	9170	An aftershock of the great Japan earthquake of
12	e L F	17 34 3 ² 17 41 18 15							iS SR ₁ L M ₂	9 42 44 9 49 44 9 55 35 10 6 10 13 56			 -25		Sept. 1.
14	e (? S) L F	18 0 39 18 2·5 18 25							M _N M _N F	10 15 25 10 20 18 12 30	26 21 	-28 	•••		
16	?eP S	20 34 30 20 44 12				?8400 		2	L F	13 50 14 35					
	e (SR ₁) L F	20 49 40 ?21 0 21 45					Ldoubtful: changing paper.	2	L F	14 57 15 35					
17	e e L F	1 29 23 1 31 40 1 49 2 40						3	e P i S F	22 50 54 23 1 12 1 30				9150 	L irregular
17	•••	13 to 14					Slight disturbance.	9	e P S L	22 15 13 22 24 28 22 37				7910 	Epicentre N.E. of Calcutta.
19	L F	13 14 14 40			•••				M _N M _N M _N	22 42 4 22 46 4 22 48 19	30 21 21	- 73 - 61			
23		6 to 6 30					Traces of long waves.	10	F L	1 30		•••			
27	L F	11 58 12 25						10	F	9 44.5			•••		
28	?S L M _R	23 37 3 23 49 23 55 22	 21 20		 26			11	•••	9 15 to 9 25			•••	•••	Small disturbance.
29	M _n F	23 55 49 2 25		32			·	14		13 27 to 13 52		•••	•••	•••	Small disturbance: confused by microseisms.
Sept.						•••	The recording drums were under overhaul for two days prior to Sept. 1., and were not brought into	17	e _n e _n L F	4 2 27 4 8 52 4 23 4 50			•••		Disturbance with well de-
ı	 	 12 I to 12 12	•••			•••	action until after 9h. on that day. Traces of waves of small amplitude.	17		7 ^{to} 9	•••			•••	veloped L waves. Record defective.
ı		14 33 to					Waves of small amplitude.	21	e e L F	20 17 56 20 22 20 26 21		•••			
ı		22 35 to 23 5					Slight disturbance.	22		21 to 23					Fairly large disturbance. Record defective.
1 2		23 34 to 0 5		•••			Slight disturbance.	23	e L	17 48 18 18 o					
2		1 50 to 2 20					Waves of small amplitude.	26	F ?S	18 40				•••	
2	i P PR ₁	2 59 II 3 2 34				9200			L F	2 54 4	•••			•••	

SEISMOLOGICAL DIARY: Instruments.—Two horizontal and one vertical Galitzin Seismographs with galvanometric registration—continued Lat. 55° 19′ N. Long. 3° 12′ W. Height above M.S.L. 242 metres.

283. Eskdalemuir.

283.	Eskaai	oman.													
D-4	Dhoos	Time.	Period	_	itudes.			Date.	Phase.	Time.	Period	Ampl	itudes.		70
Date.	Phase.	G.M.T.	Penod	A _N .	A _E .	⊿.	Remarks.	Date.	T flase.	G.M.T.		A _N .	A _E .	Δ.	Remarks.
Sept.		h. m. s.	s.	μ	μ	km.		Nov.		h. m. s.	s.	μ	μ	km.	
26	e P S	8 37 8 46 49		•••				3	eP	16 32 0 16 3 6				9740	Confused by wind effects and microseisms;
	L M _n	9 2 9 7 55	30	•••	37				PR ₂	16 39 12 16 42 48		•••			
	M _x M _z	9 9 8	28 22	31	29				SR ₁	16 49 17					
	M _n F	9 11 34	22	-20					M _N M _N	17 7 II 17 10 I	26 24	45 46			
30							Considerable disturbance		M _N M _N	17 11 52 17 16 0	24 20	60 -41			
							in early hours. Time marks failed.		M _N F	17 17 6 18	20	60 	•••		
								4	· i _n	0 25 35					•
Oct.		8 to					Moderate disturbance. No	-	i _n e _n	0 35 34 0 37 12					
		9		•••	•••	•••	time marks.		e _n	o 43 o 48		•••	•••		
I 2		23 45 to					L waves: confused by wind disturbance and		L F	1 0 2 40	•••		•••		
3	L	16 35					microseisms.	5	P	21 40 51			 	(9380)	
	F	17 10	•••						PR ₁	21 44 26 21 48					
4	e F	17 54 19 18 30			•••				Si	21 51 20 21 51 30	•				
7	e	3 49 16							$\begin{array}{c} SR_1 \\ L \end{array}$	21 57 26 22 8	•••	•••			
	S ?SR	3 59 4 5							M _N M _N	22 20 23 22 2I 40	24 23	63			
	L M _n	4 20 4 32 3	24	 -157					M _N M _N	22 26 11 22 27 16	18 17	←76 −55			
	M _N M _N	4 34 23 4 40 52	24 20	- 105 - 96				6	F	0 10	•••	•••	•••		
	F	6 30		•••				6	e	17 34 40					
10	iP	7 15 11	•••	•••		•••	Record too faint for identification of later phases.		e e	17 41 17 44 10					
11	? L	12 43							e L	17 50	•••				
	F	13 10	•••	•••		•••		c	F	18 50	•••	•••			
13	e e	4 48 4 52 30		•••				6	e L F	19 4I 45 20 0	•••	•••			
	L F	5 0 5 20					·	8	L	20 50	•••	•••			
15		4 14 to					Traces of waves.		F	0 31 1 5					
		4 33						9	e (? S)	3 42 31 3 48 2				:::	
15	e	7 5 ² 8 2							e L	3 51 29 3 59·5					
	e e T	8 28							F	4 30					
	L F	8 54 10						0I 11		22 to 0		•••			Trace of waves.
20	e F	o 30 o 45													
20	L	3 55 30						II	•••	5 58 to 6 20		•••			Trace of disturbance.
	F	4 30						17	e (? P)	3 4 53	•••			?8200	
23	L F	16 43 17						•	e (? S) e	3 14 18 3 19 28					
Nov.	_	,						,	L F	3 28 4 25					
Nov.		7 30 to		•••			Traces of waves.	18	L	22 11	•••				Earlier phases confused by
		7 45							M _N	$22 \ 26 \ 27 $	17	21	•••		wind effects and micros- eisms
l t	L F	8 49 (9 10)							F	23		•••			
ı	? e	20 21	•••					19	e M _N	4 0 4 2 12	 10	 8			
•	L	20 35 21							F	4 5		•••			
2	e?P	21 29					Record confused. Felt in	21	L F	II 20 II 40					
	L F	22 5 0 30					Shortland Is. (155° E, 8° S.) at 21h. 15m.	21	L	14 5	•••	•••			
							G.M.T. (approx.).		F	14 23	•••	•••			
		'		·	 		[1		 						

SEISMOLOGICAL DIARY: Instruments.—Two horizontal and one vertical Galitzin Seismographs with galvanometric registration—continued.

Lat. 55° 19′ N. Long. 3° 12′ W. Height above M.S.L. 242 metres.

283. Eskdalemuir.

	Remar Slight disturbance confused
Nov.	Slight disturbance confused
Nov. 22 e 7 44 25	Slight disturbance confused
22	Slight disturbance confused
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Slight disturbance confused
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Slight disturbance confused
23 e 2 56 28	Slight disturbance confused
23	Slight disturbance confused
23	Slight disturbance confused
F 4 0	Slight disturbance confused
23	Slight disturbance confused
1 1 <td>Slight disturbance confused</td>	Slight disturbance confused
L 18 16 <td>Slight disturbance confused</td>	Slight disturbance confused
24 e 8 3 0	Slight disturbance confused
24 e 8 3 0 2 15 40 to	Slight disturbance confused
	Singific disturbance confused
16 30	by microseisms.
24 L 18 56	•
	(Slight uncertainty about
24 e 19 40 18 ? Seismic. S 21 6 3	absolute accuracy of
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	times.)
$oxed{25} \ \ \ \ \ \ \ \ \ \ \ \ \$	
L 17 43 F 22	
5 L 23 32	
20 7,33 to	
6 ?e 22 49	
26 e 12 43 4 L 22 53 F 23 10	
e 12 45 34 F 23 10	
L 13 7 II e 0 11 40	
L (0 24)	
26 14 13 to Traces of disturbance. F 0 50	
15 6 to	Traces of disturbance; con-
	fused by microseisms.
27 e 3 44 40	
F 4 35 14 L II II	Earlier phases masked by microseisms and wind
28 o 20 to Traces M _m II 15 20 7	effects.
28 0 20 to 11aces	
20 L 15 38	
28 e 0 38 47 ?2100 20 L 15 38	
e 0 42 19	
L 15 eS 15 150	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	
L 16 2 42	
SR 22 44 0	
29 L 4 5 L 22 48	
F 4 30 F 23 45	

1923.

				Janua	ry.				1			Feb	ruary.							Ma	rch.			
Day.	0 1	h.	61	n. '	12	h.	18	h.	0	h.	6	h.	12	2 h.	18	3 h.	0	h.	6	h.	12	h.		h.
	A. 1	T.	Α.	T.	A.	T.	Α. Ι	T.	A.	Τ.	A.	T.	A.	T.	A.	IT.	Α.	T.	A.	T.	A.	T.	A.	T.
1 2 3 4 5	μ 1·6 2·3 1·6	s. 5·5 6·5 5·5	μ 1·2 	s. 5·5 	μ 0·9 4·0 1·6	s. 5·5 7·5 5	μ 3.0 1.2	s. 6·5 6	μ 2·4 	s. 6 	μ 1·9 	s. 6 	μ 2·2 2·1 2·0	s. 7 5 	μ 2·4 2·7	s. 6 6	μ 2·8 1·6 1·9 1·6 0·9	s. 5·5 6 5 5·5	μ 1·6 1·9 1·8 0·9 2·0	s. 6 5 5 5.5	μ 1·6 1·7 1·6 1·1	s. 6 5·5 5·5 4·5 5·5	μ 1·7 2·3 1·4 1·0	s. 5·5 5 7 5·5
6 7 8 9	2·8 2·2 1·5 1·8 6·6	8 7 5 5.5	3·5 1·7 1·6 3·3 4·9	8·5 6 6 6 7	3·6 1·5 5·2 4·8	7 6·5 7·5 6	2·7 0·9 2·5 7·1 2·8	7·5 6 5·5 9 7	2·7 4·9 6·6	6 8 7	5·5 6·0 6·3	6 8 7	4·9 6·6 5·8 	6·5 8 7 	4·7 6·2 7·3 3·9	6·5 8 7·5 7	1·4 2·9 1·3 	5 7·5 7 	1·7 	6	1·6 2·2 	6 6·5 	3·1 1·6 	7 6
11 12 13 14	3·2 1·3 0·9 1·0	6 5·5 5 4·5	2·2 1·5 0·9 1·6	6 5 5 5.5 	2·3 1·5 1·0 2·3 5·4	6 5 5 6·5 7	2·4 1·1 1·1 4·1	5·5 5·5 4 7	 2·7 1·6	 6 6·5	2·9 2·1 1·5	6 7.5 7	3·9 1·9 2·3 2·3 0·9	6 6 8 6·5	3·5 3·4 2·3 2·0 1·2	6·5 6 6 7 6·5	1·2 1·2 2·3 1·5 1·1	6 6 5.5 6	 1·9 2·5 1·5	 6 6 5·5	1.6 3.0 2.1 	8 5 6 6	3·2 2·0 	5·5 6·5
16 17 18 19 20	2·1 1·2 1·4 7·1	7 6·5 7 6·5	1·5 1·4 6·8	7 7 6·5	1·6 2·4 1·5 6·7	6·5 6·5 7 6	1·0 1·4 1·5 2·7 5·5	6 7·5 6·5 8 6·5	1·2 1·6 1·6 2·7 2·9	5·5 6 6 6·5 7	0·9 1·7 1·6 3·4 1·6	6 5·5 6 6·5 6·5	1.6 1.8 2.3 3.6 1.9	6 5 6 6·5 6	0·8 1·7 2·1 3·3 1·8	6 5·5 6 6 6·5	0·9 0·9 0·8 0·5	6 6·5 6	0·9 0·7 0·6 0·3	6·5 6·5 6	0·6 0·4 	6 7 5.5	0·5 o·5 o·4	6 6 5·5
21 22 23 24 25	5·3 2·3 2·3 3·1 2·6	6·5 6 6 6	3·3 2·5 1·6 3·1 2·2	7 5·5 6 6 6 6	2·7 1·8 3·2 2·3	7 5·5 6 6	1·9 2·2 2·3 2·8 2·3	6 5·5 6 6·5	1·6 3·2 2·6 1·6 2·0	6·5 8 8 6·5 6·5	2·7 3·5 2·3 1·7 2·1	5 7·5 6 5·5 7	2·2 3·2 2·5 1·6 1·8	7 8 7 6 8·5	3·4 2·9 1·6 1·6 2·2	8 7 6 6 7	0·6 0·7 1·3 1·7 0·8	5·5 7·5 8 7 5·5	0·5 0·8 2·0 	6 5·5 8 7	 0·8 2·6 0·8 0·7	 6 8 7 5	 0·7 2·2 0·8 0·9	7.5 6.5 4
26 27 28 29 30	3.4 2.3	 6·5 6	 2·3 	6	2·5 3·5 2·4 	5·5 6·5 5·5 	2·3 2·3 	6	2·2 7·5 4·3	6·5 6 6	2·2 5·6 4·6	7 6 5·5	2·6 4·7 3·4	5·5 6·5 6	3·8 4·6 2·6	6 6·5 6	0·6 0·9 2·I 	5·5 5 7·5	o·8 	6	0·9 0·9 2·5	4 5 6 	0·7 2·7 	5 7
31					<u> </u>			<u> </u>	<u> </u>		<u> </u>	<u> </u>	<u> </u>	<u> </u>		<u> </u>	<u> </u>	•••	<u> </u>	ι·4μ;	т –	6.75		
Mean			A =	2·6μ;	<u>T</u> =	6·2 s.							T = 0											
Normal, 1911-22			A =	2·5μ;	T = 0	6∙o s.					A =	2·3μ;	T = 0	6∙o s.					A =	1·8μ;	T =	5.7 s.		\

1				Ap	ril.							Ma	ay.				1			Ju	ne.			
Day.		h. \	6	h.	12	h.	18	h.	0	h.	6	h.	12	h.	18	h.	0	h.	6	h		h		h.
,	A.	T.	A.	T.	A.	T.	A. 1	T.	A.	T.	Α.	T.	A.	T.	Α.	T.	A.	1 T.	A.	T.	A.	T.	A.	T.
1 2 3 4 5	μ Ι·ο ο·9 Ι·5	s. 8 6 7:5	μ 1·9 1·6	s. 7 6	μ 1·2 2·3 1·6	s. 7 8 6	μ 1·4 1·4	s. 8 6·5	μ ο·6 ο·6 ο·8	s. 5 4.5 4.5	μ ο·8	s. 4.5	μ ο· 7 ο· 9 	s. 4·5 4·5 	μ ο· 7 ο· 3 	s. 5 5 	μ ··· ··· ··· ···	s. 3·5 — 3	μ 	s. 	μ 0·2 0·0 	s. 4 — — …	μ 	s.
6 7 8 9	1·2 1·3 1·1 0·9	6 5·5 5 5 5·5	1·1 1·8 1·6 0·9 2·4	5·5 5 5·5 4·5 6	1·4 1·6 1·3 1·1 2·4	5·5 6 4·5 4·5 5	1·1 1·7 1·1 1·8 1·4	5 6 5 5 5.5	1·4 0·2 0·6 0·3	6 5·5 4·5 5	0·8 0·7 0·4 0·3	5·5 6 5·5 4	0·8 0·8 0·7 0·8 0·7	5 5·5 4·5 4·5	0·6 0·6 0·6	6 4·5 4·5 5								
11 12 13 14 15	1·0 0·2 0·1 1·6 0·9	4·5 5 4 5·5 6·5	0·6 1·6 1·0	5·5 6 5·5	0·8 0·1 0·4 1·7 1·5	3·5 4 3·5 5·5 5	0·2 0·1 2·0 1·8	4 4 6 5	1·6 1·5 0·7	5 4 5.5	2·2 I·0 	4·5 5 	1·8 1·0 0·9 0·5	4 4 4·5 5	1·2 0·8 0·7	5 4·5 5	0.9 0.6 0.9 0.5	6 6 5 5	 0·7 1·1 0·7	5·5 4·5 5	0·1 0·9 0·1	6 6 5 4.5	1·2 1·0 1·0 0·8 0·2	5 4·5 5·5 4
16 17 18 19	1·2 0·9 	6 4·5 	0·8 1·1 	5·5 4 	0·9 	5 	o·8	5.5	0·6 0·7 0·6 0·2 0·6	6 5·5 5 4 4·5	0·6 0·7 0·5 0·3 0·3	4 6 5·5 4 4·5	0·6 0·6 0·3 0·2 0·2	4 6 5·5 4·5 5	0.6 0.5 0.1 0.2	4 5 4·5 4·5	0·3 0·4 0·5 0·4	4 4·5 3·5 4·5	0·6 0·5 0·3 0·8 0·8	4 4 3 4.5 5.5	0·5 0·5 0·2 0·9 0·8	4·5 4 4 6 5·5	0·5 0·3 0·2 0·8 0·8	4.5 4.5 5.5 5
21 22 23 24 25	 2·5	 5.5	 3·2		 1.6 3.8	 6 4.5	 I·7	5·5	 0·2 1·0	4·5 4·5	0·5 0·3 0·2 1·2	5 4 4 6	0·7 0·9 0·3 0·5	4 4 4·5 5 5·5	1·1 0·2 0·2 0·8 1·5	4 4·5 5 5 6	0·5 0·5 1·0 0·7 0·4	5 5·5 4·5 4·5 5	o·5 o·8 o·3 	5 4·5 •··	0·3 0·7 	4 5 5	 o·8 o·8 	 5 5
26 27 28 29					0.3	 4.5	 0·7		1·7 0·5 0·0 0·1 0·2	5·5 6 5 5	o·8 o·3 	5·5 4·5 	0·7 0·1 0·1 0·1	5·5 5 4·5 5	0·6 0·3 0·2 0·2	6 3·5 5·5	0·7 0·7 0·4	6 6 4.5 	 0·7 	 4.5 	1·6 0·5 	5	0·8 	5·5
31			A -		 				0.1	6			т –				 		A =	o·6μ;	T =	4·8s.		
Mean Normal, 1911-22					T = 5 $T = 5$		······································						T = A	1·7s.						ο·5μ	T =	4·6 s.		

Note:—The symbol ... indicates that microseisms were not measured, either by reason of occurrence of earthquake or lack of record.

MICROSEISMS OF NORTH COMPONENT: AMPLITUDE ($\mu = .001 \text{ mm.}$) AND PERIOD (seconds). Derived from readings, for the period of thirty minutes centering at the exact hour, Greenwich Mean Time.

284. Eskdalemuir.

	1			Ju	ıly.							Aug	ust.							Septe	mber.			
Day.	o h	1.	6	5 h.	12	h.	18	h.	0	h.	6	h.	12	h.	18	h.	0	h.	6	h.	12	h.	18	
	A.	T.	- <u>A.</u>	T.	A.	T.	A.	T.	Α.	T.	Α.	T.	Α.	T.	Α.	T.	A.	T.	Α.	T.	A.	T.	A.	T.
1 2 3 4 5	μ ο·1 ο·3 ο·2	s. 4 4.5	μ ο· I	s. 4.5	μ 0·2 0·2 0·2	s. 4.5 4 4.5	μ 	s	μ 0·2 0·3 1·0 1·0	s. 4.5 4 4.5 4 5.5	μ ··· ··6 ··0 ··3 ··2	s. 5 4.5 4 5.5	μ 0·2 1·4 0·9 0·6	s. 4·5 5 4 4·5 5	μ 0·2 1·0 0·9 0·3 0·9	s. 4·5 4·5 4 4·5 6	μ ··· 0·2 ··· 0·5 0·9	s. 4 6 5.5	μ 0·5 1·2	s. 5.5	μ 0·2 0·6 0·8 0·8	s. 4 5 6 6·5	μ 0·3 0·5 0·8 0·9	s. 4·5 6 6 6
6 7 8 9	0·1 0·0 0·0	4·5 — — 4			0·0 0·0 0·0	4 4			0·7 0·6 0·3 0·1 0·2	6·5 6 5 6 4·5	0·7 0·3 0·2 0·4 0·5	6 4 5 4·5 5	0·9 0·3 0·2 0·2 0·2	6 5 5.5 5	0·8 0·5 0·4 0·5	5·5 4·5 4·5 5	1·1 0·9 0·8 	7·5 6·5 6	0·9 0·7 0·8 0·7	7 6·5 6 6·5	0·9 0·9 0·8 1·2	6·5 6 6 6 6	0·8 0·8 0·6 0·9 0·2	6 6·5 7 6 5·5
11 12 13 14 15	0·1 0·0 0·2 0·4 0·2	4.5 5.5 5 4.5			0·0 0·0 0·3 0·0	 4·5			0·3 0·1 0·2 0·1 0·2	4.5 4.5 4.5 5	0·2 0·1 0·2 0·2	4 4 5 4.5	0·3 0·2 0·2 0·1 0·2	3 4 4 5 4.5	0·I	4	0·2 0·8 1·4 	6·5 6 7 	0·4 1·3 1·5 	5·5 6·5 6 	0·7 2·5 	5 6 	0·8 1·7 	5 7·5
16 17 18 19 20	 0·2 0·3	 4.5 4.5			 0·2 0·7	 4 5.5	 0·2 0·8	 4.5 5.5	0·3 0·5 0·8 0·7 0·3	4.5 4.5 5 5	 o·2	 4	0·3 0·2 0·9 0·3 0·2	4 4 5·5 5 4·5	0·2 0·5 0·3	4·5 6 5	 o·6 i·o o·8 i·3	4.5 5 5.5 5.5	 0·9 1·0 0·8	4.5 4.5 5.5	1.3 1.0 1.0	5.5 4.5 8.5	 1·3 0·8 0·9 0·8	4.5 6 5 6
21 22 23 24 25	1·0 0·7 0·2 0·3 0·2	5·5 5·5 4 4 4·5	0·I	4	0·8 0·4 0·3 0·2 0·1	6 4.5 5 4.5 5	 0·2 0·2 0·1	 4.5 4 4.5	0·3 1·4 1·7 2·5 0·8	3·5 4·5 5·5 5·5	0·4 1·6 	3·5 5 	0·7 1·8 1·5 1·2 0·2	4 5 6 5.5 5	1.0 1.8 2.0 	4 5 5 4.5	0·8 0·8 1·6 0·7 0·9	6 4.5 6 6 6	 	 5	0·5 0·7 0·8 	5 4.5 6 6.5	0·7 0·9 0·9	4·5 6 5·5
26 27 28 29 30	0·4 0·6 0·2 0·3 0·2	4.5 5 4 3.5 4.5	0·8 0·8 0·2 0·2 0·1	4.5 4.5 4 4	0·2 0·2 0·2	 4 4 4.5	0·3 0·3 0·1	4.5 4 4 4.5	1·6 1·2 0·8 	5 6 6 	1·6 1·7 0·8 	5·5 5 	1·4 0·7 1·0	5 6 6	0·8 0·9	6	 o·3 	 5.5					 0·7 	6
31	0.6	4.5	^		0·4	4.5	0.3	5	1	<u> </u>	ļ	0.50	· T -			1	1		A -	0.04.	T =	1 5 · 8 s	l	<u></u>
Mean Normal				ο·3μ; ο·3μ;									T = T =			<u></u>					T =			

				Oct	ober.				1			Nove	mber.							Dece	mber.			
Day.	0	h.	6	h.	12	h.	18	h.	0	h.	6	h.	12	h.	18	h.	(h.	6	h.	12	h.		3 h.
	Α.	T.	A.	T.	Α.	T.	Α.	T.	A.	T.	Α.	T.	A.	T.	A.	T.	A.	T.	A.	T.	A.	T.	A.	T.
1 2 3 4 5	μ ο·7 ο·9	s. 5 5 5.5	μ o·8 o·7 o·8	s. 4.5 5 5.5	μ 0·8 0·9 0·9 0·9	s. 5.5 5 4.5 5	μ 1·7 0·8 0·9 0·9	s. 5·5 5 5	μ 1·6 0·9 2·7 3·1	s. 6 5 6 6	μ 1·6 0·8 1·4 3·1 2·7	s. 5·5 4·5 5 6 6	μ 1·2 0·9 1·7 2·8 2·4	s. 5·5 4·5 5·5 7	μ 0·8 0·9 2·6 1·6	s. 5·5 4·5 6 6	μ 1·1 1·6 2·8 1·6 3·6	s. 4.5 6 6 6	μ 1·6 2·5 2·0 1·9	s. 5 6 6 6.5	μ 1·4 2·7 2·7 1·8 1·7	s. 5·5 5 6 6	μ 1·6 2·7 1·7 2·7 1·6	s. 6 5 5.5 8
6 7 8 9 10	3·1 1·0 	5 5 6	3.3	5.5	1·5 0·9 5·6 0·9	6 5·5 6·5 6	1·4 0·8 4·4 1·6	6 6 6 6	1·2 1·0 1·9 1·1	 6 5 4.5 4.5	1·6 1·4 1·1 1·7 1·1	6 4 4.5 5 4	1·2 1·0 1·1 1·5 1·0	5·5 5 4·5 4·5	1.0 1.8 1.0	5·5 5 4·5 4·5	 1·4 2·5 4·9 1·2	5 6 5.5 5	0·8 1·8 3·9 2·5 1·1	6 5 6 5·5 5	0·9 2·6 4·3 2·0 1·0	5 5.5 6 5 5.5	0·9 3·0 1·0 1·1	5 5·5 5·5 6
11 12 13 14 15	1·7 0·8 1·0 0·7 1·0	5·5 5·5 5·5 4 5	1.0 1.0 0.3 0.9	5 4·5 4·5 4 5	1·1 1·0 0·3 0·8 0·2	5 5·5 4 5 4	1·0 1·2 0·2 0·7 0·2	5·5 4·5 4 5 4	1.0 0.9 2.5 2.5 4.5	4·5 4·5 6·5 5	0·9 4·8 3·4 4·3	5.5 6 5.5 6	0·9 4·6 2·5	4·5 5 5·5	0·9 1·9 2·9 4·6 3·7	4·5 6 5·5 5·5 5·5	1·9 1·9 2·8 2·2 3·9	6 6 6·5 6·5	1·6 2·3 2·5 4·6	6·5 6 6 6	2·3 2·2 2·5 2·3 4·6	6 6·5 7 6 6·5	2·1 2·8 2·2 4·1	5·5 6 7 6
16 17 18 19 20	0·2 0·9 0·9 0·8 1·9	4·5 4 4·5 5 5·5	0·6 0·5 1·1 1·6 1·7	4 4·5 4 4 5·5	0·7 0·8 1·0 2·0 1·9	4·5 4·5 4·5 6	0·8 0·5 0·8 1·7 1·9	4 5 5 5.5 5.5	4·1 1·8 2·6 2·7 1·7	6 5 5 5.5 6	4·I 1·9 2·I 1·7 1·6	5.5 4.5 5 6	3·3 2·1 3·2 1·8 1·6	5·5 4·5 6 5 5·5	1·9 3·1 2·7 1·7 1·1	6 4·5 5 5 5·5	3·9 2·8 3·0 4·3	6 7 6 6 	2·8 3·1 3·3 3·0 1·6	6 6 6 6	3·5 2·2 4·1 2·7 1·2	5·5 6·5 6 6	3·6 2·7 4·9 2·4 1·6	6·5 6 7 6 6
21 22 23 24 25	2·1 1·1 1·1 1·1	5 5 4 5	1·7 1·0 1·1	5·5 4·5 5	2·7 1·0 1·0 2·6	5 5 5 5.5	3·I 1·0 	4·5 4·5 4·5 4·5	0·9 0·9 0·6 0·7 0·7	5·5 5 5 4 4	0·9 0·8 0·4 0·7 0·6	5 5 4.5 4	0·9 0·7 0·5 0·6 0·5	4.5 4.5 4 4 3.5	1·0 0·4 0·5	4·5 5 4	1·3 0·8 3·9 2·3 0·9	5·5 5·5 4·5 4 4·5	I·4 o·8 4·0 I·7 o·7	5·5 5 4·5 5·5 5·5	1·1 1·0 2·3 1·5 1·0	6 5 5 5 4.5	0·9 2·5 2·2 0·8 1·1	6 5 5·5 5·5 4·5
26 27 28 29 30	2·7 2·7 2·7 1·5 1·7	5 6 5 5.5	2·3 2·5 2·5 1·0 1·7	6 5·5 5·5 5·5	2·8 2·4 2·5 1·3 1·7	5 5.5 5.5 5 5.5	2·8 2·5 2·4 1·8 1·7	5 5 5·5 5 5·5	0.6 1.0 1.0 0.9	4·5 5·5 4·5 4·5 4·5	1.0 0.9 1.0	5 5 4.5 4.5 	1.0 1.1 1.0	6 4·5 4 4·5 5	I·2 0·9 I·2 I·0 I·I	6 5 4 4.5 4.5	1·1 0·9 2·0 2·3 1·4	4·5 5 4·5 6 7	1·1 0·7 2·3 1·7 1·6	5 6 6 5·5 5	1·4 1·0 2·3 1·6 1·8	4 4.5 6 6 5	1·2 1·0 1·8 1·2 2·1	4.5 4.5 5.5 6 6
31	1.9	5	2.5	5.5	1.5	6.5	1.2	6									1.8	5.2	1.8	5	1.6		1.6	6
Mean			A =	1·5μ;	T =	5·1 S.					A =	ι ·6μ;	T =	5·1 s.					A =	2·1μ;	T =	5·7 s.		
Normal 1911–19, 1921–22*			A =	1·2μ;	T ==	5·2 s.					A =	ı·8μ;	T =	5·7 s.					A =	2·3μ;	T =	5·9 s.		

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M.O. 279
Cahirciveen

Air Ministry

METEOROLOGICAL OFFICE

OBSERVATORIES' YEAR BOOK 1923

Comprising the results obtained from autographic records and eye observations at the observatories at Lerwick, Aberdeen, Eskdalemuir, Cahirciveen (Valencia Observatory), Richmond (Kew Observatory), and Benson.

CAHIRCIVEEN (Valencia Observatory)

Published by the authority of the METEOROLOGICAL COMMITTEE



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PRINTED AND PUBLISHED BY HIS MAJESTY'S STATIONERY OFFICE

CAHIRCIVEEN (VALENCIA OBSERVATORY).

Latitude Longitude			10°	56' N 15' W 41m.
Heights in metres	above Se	a Level	<i>!</i> .	
Barometer				13.7
Rain-gauge				9·i
Robinson Cup Anemograph.		• •		26
Dines Tube Anemograph .	• • •			30
Heights in metre	es above G	round.		
Thermometer Bulbs				1.3
Sunshine Recorder				
Robinson Cup Anemograph .				14
Dines Tube Anemograph .				13

INTRODUCTION.

SITE.

Valencia Observatory derives its name from the fact that it was originally established on Valencia Island in 1867. It was removed to the mainland in March, 1892, and now lies in a direct line between the old site on Valencia Island and the town of Cahirciveen, about 2½ miles (4 km.) north-east from the former, and threequarters of a mile (1 km.) south-west of the latter. It is quite remote from any other buildings. The general character of the country surrounding the Observatory is hilly. The eastern bank of the Cahir river is about 150 metres to the westward, and in that direction there is no very high ground between the Observatory and the open sea, some $3\frac{1}{2}$ miles (6 km.) away. To the north-west, however, are hills varying in height from 400 (120 m.) to 900 feet (275 m.), the highest being less than 3 miles (5 km.) distant. These are only separated by a narrow gully running in a N N W direction from other hills equally high, which stretch away to the northward: the nearest of these is but little more than a mile $(1\frac{1}{2}$ km.) from the Observatory. Beyond the town of Cahirciveen to the north-east the river opens out considerably, and the country in this direction becomes an open boggy basin, rising by only a gentle gradient. Southward of this, however, it soon rises again, and at about a mile southeast of the Observatory it culminates in a hill upwards of 1,245 feet (380 m.) in height. Still further south it opens out once more to a distance of nearly 5 miles (8 km.) from the Observatory, where there is a range of hills running east and west. and varying in height from 400 (120 m.) to 1,300 feet (400 m.). To the south-west there is an opening to the sea, between Valencia Island and the mainland; and the circle of hills is completed by those on the island itself, the highest of which is about 800 feet (240 m.) high, and bears about west-south-west from the Observatory. For general views of the Observatory building, see Figs. 16 and 17. A site plan showing the disposition of the various instruments is reproduced in Fig. 15.

METEOROLOGY.

The elements dealt with in the following tables are: atmospheric pressure, air temperature, humidity, rainfall, sunshine, wind speed and direction, minimum temperature on the grass, together with a diary of cloud and weather.

Pressure and Temperature.—The photographic barograph and thermograph are installed in a room on the ground floor of the Observatory tower. The standard Fortin barometer (M.O. 463), from which the control readings at 9h, 15h and 21h are taken, is mounted in the same room beside a window which faces the north-east. The stems of the dry and wet bulb thermometers pass out into the screen placed against the north wall of the tower. Close to the bulbs of these thermometers are the bulbs of the standard thermometers (dry, M.O. 1701; wet, M.O. 1702) from which the control readings at 9h, 15h and 21h are taken.

Rainfall.—The Beckley raingauge and the 8-inch (20.3 cm.) check gauge (M.O. 402) are placed in a railed-off enclosure about 40 metres to the north of the tower.

Sunshine.—The recorder (M.O. 5) is cemented to a wooden rail on the roof of the tower. The exposure is satisfactory.

Wind Speed and Direction.—The Robinson Cup Anemograph (Beck, 46) is placed on the roof of the Observatory tower (see Fig. 16). It will be seen from Fig. 15 that the exposure is satisfactory except for winds between south and south-west. Winds from these directions are liable to be deviated and reduced in speed because of the sheltering action of the roof and chimney. The Dines Tube Anemograph stands in an open field, about 250 metres S E by E of the Observatory tower. The field slopes northwards to the river Cahir. About I mile (1½ km.) to the south-east and in an approximately direct line with the highest point (1,245 feet) is the hill Bentee which extends for some little distance in a northerly and south-westerly direction. description of the surrounding country has already been given on p. 221.

The Robinson Anemograph was damaged by the gale of February 26th-27th; for the period it was out of action data were obtained from the records of the Dines Tube Anemograph. Such values are printed in italic type.

Minimum Temperature on the Grass.—The grass minimum thermometer (N. and Z. 2497) is of the type described on p. 14. It is exposed over short grass in the field enclosure. It is set at 18h and read at 9h on the succeeding day, the reading being entered to the day of reading.

Notes on the Meteorological Summaries.

Pressure.—The mean pressure for the year was 0.5 millibars below normal, and the mean monthly pressures differed from the corresponding normal values by amounts varying from excesses of 11 millibars in January and 10 millibars in June, to a deficiency of 17 millibars in February. In six months out of the twelve, the mean pressures were within 2 millibars of the corresponding average values. The highest pressure recorded was 1,041 millibars on the 20th December, while the lowest, on the 26th February, was 950 millibars; a low pressure of 954 millibars was also registered on the 7th February. Both of these low pressures were accompanied by destructive gales.

The hourly differences between the mean diurnal inequality for the year and the normal annual diurnal inequality follow approximately the curve given by the formula $0.1 \sin (15t + 135^{\circ})$, the amplitude being expressed in millibars.

In Table A are given the details of the harmonic analysis of the mean diurnal inequalities for each month and the year.

The inequality is represented by either of the equivalent formulae:—

- (a) $a_1 \cos 15t + b_1 \sin 15t + a_2 \cos 30t + b_2 \sin 30t + \dots$ (b) $c_1 \sin (15t + \alpha_1)^\circ + c_2 \sin (30t + \alpha_2)^\circ + c_3 \sin (45t + \alpha_3)^\circ + \dots$

where t is the time in hours after midnight, Local Mean Time. In Table A only the coefficients for formula (b) are given.

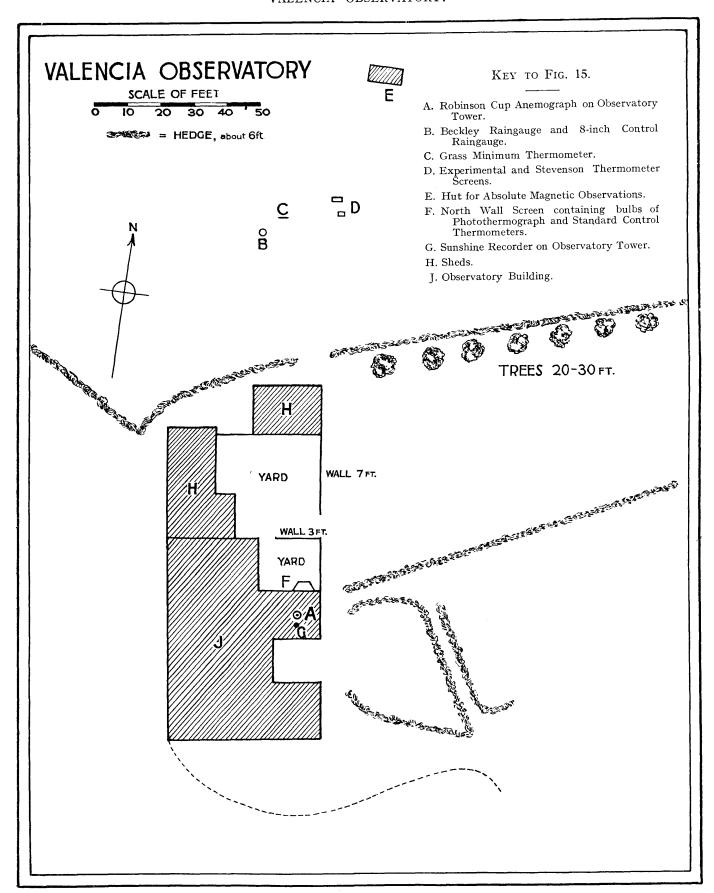


Fig. 15. Site Plan.

VALENCIA OBSERVATORY.

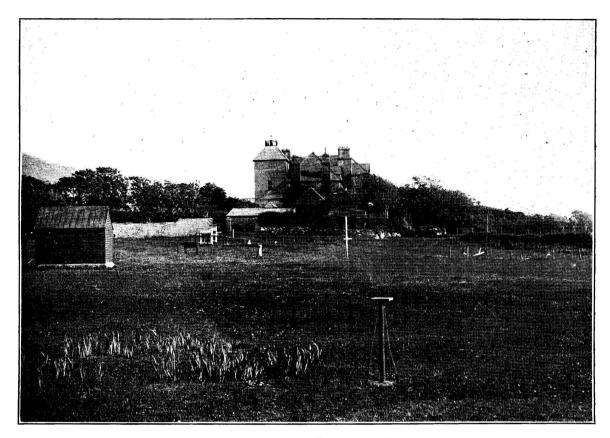


Fig. 16. General View from North.

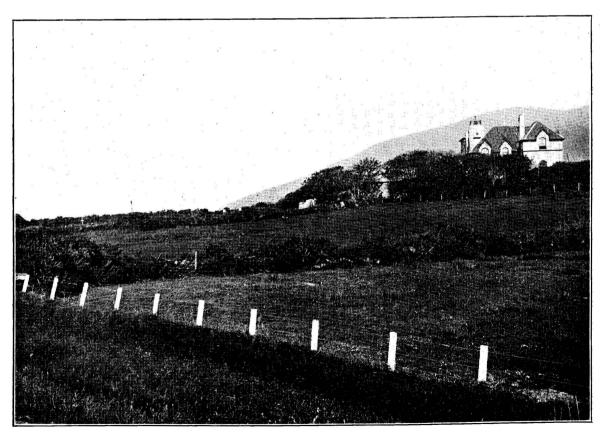


Fig. 17. General View from West.

To face p. 223.]

The four values given in the line immediately below the monthly values are the arithmetic means of the monthly amplitudes; on account of the changes in phase from month to month these give a better idea of the average conditions for the year

in some respects than the amplitudes computed from the annual inequality.

Notable features of Table A are the wide and irregular variations, both in amplitude and phase, of the 24-hour term, in particular the very large amplitudes in August, February and October, and the very low ones in March and May; the comparative uniformity throughout the year of the 12-hour term; the regular change in the 8-hour term with its high amplitudes in summer and winter and lower ones at the equinoxes, accompanied by a change in phase of 180° in passing from winter to summer. The 6-hour term shows no great regularity in its amplitude changes but there appears to be approximate opposition in phase as between winter and summer.

Comparing the coefficients for the year with the normal values, the amplitude of the 24-hour term is high and the maximum occurs rather early; the 12-hour term agrees very closely both in amplitude and phase; the 8-hour term, with an amplitude not much greater than half the normal value is early as regards phase; the 6-hour term has an extremely high amplitude and in phase is late by about a

quarter of a period.

Normal values for the individual months are not available, but for purposes of comparison we may refer to Official Publication, No. 93, of the Meteorological Office, which gives the monthly co-efficients obtained from the mean inequalities for the period 1871-1882, but omitting the 6-hour term. The arithmetic means of the monthly amplitudes of the 12-hour and 8-hour terms for 1923 do not differ greatly from the 12-year averages but the mean of the 24-hour terms is very much in excess, being, in fact, higher than the highest value found in any one of the twelve years of the comparison period considered separately. The wide variations in the amplitude and phase of the 24-hour term, noted above, constitute a not unusual feature, and are to be found, though naturally in a much smaller degree, in the 12-year averages. The changes in the 12-hour term are in reasonably good agreement with those for the comparison period. The range, both in amplitude and phase, is very much greater in 1923, but the general sequence of values throughout the year follows that of the average values fairly closely. The highest amplitude is in March and values generally tend to be higher at the equinoxes than in summer or winter; comparatively high values of the phase angle also appear at the equinoxes, though compared with the other terms the variations are small. The 8-hour term changes also correspond fairly closely with those found for the comparison period, the winter values being on the whole higher than the summer values and these, again, considerably higher than those for the equinoxes; the phase angles for this term show the normal features of very rapid reversal in passing from winter to summer and vice versa with comparatively minor changes during the course of these seasons themselves.

Temperature.—The highest temperature of the year was 294·5a (70·7° F.) on the 6th July, and the lowest was 270·4a (27·3° F.) on the 25th November. This latter temperature occurred during a cold period of ten days, on seven of which the minimum was below the freezing point, the remaining three having minima only a fraction of a degree above it. In no other month was the temperature at any time below 273a. The mean temperature for the year was only o·1a below average, but the individual months show differences from the corresponding normals varying from an excess of 1·7a for December to a deficiency of 2·5a for November. With the exception of November all the winter monthly means were higher than normal by more than a degree absolute; three of the equinoctial months had mean temperatures lower than normal, March alone showing an excess of about one degree absolute; the July mean was about a degree above, and those for the remaining summer months all less than normal. The mean daily ranges of temperature for the individual months were, without exception, below average, the deficiency being more than a degree absolute in eight of the twelve and in two of these more than two degrees absolute.

(19889)

The mean diurnal variation of temperature for the year does not differ greatly from normal; the amplitude is about 0.5a low, and the maximum is about an hour early. The harmonic analysis of the monthly and annual variations is given in Table B. For purposes of comparison we may utilise the mean inequalities for the period 1871–1882 as was done for the harmonic coefficients of the pressure inequalities. The means given on the line immediately below the monthly values are the arithmetic means of the monthly amplitudes. These are all below average, the 24-hour term mean by some 10 per cent., the 12-hour term mean by about 15 per cent. and the 8-hour term mean by about 5 per cent. The mean inequality for the year also gives low amplitudes for all terms; in particular the 8-hour term has only half the average amplitude. In phase the 24-hour and 12-hour terms show no striking departure from the average values the first having its maximum 43 minutes late and the second 8 minutes early. The difference from the average of the 8-hour term phase is proportionally rather greater.

The monthly values show some irregularity in amplitude, particularly in the 24-hour term, the normal regular increase in going from winter to summer being conspicuously disturbed by the high values for March, April and November and the abnormally low value for October. The phase angles for this term show considerable departures from the 12-year averages in the winter months, January having its maximum about $2\frac{1}{2}$ hours and each of the remaining three months about an hour late. The equinoctial and summer months have phase angles agreeing fairly well with average values with the exception of March which also has its maximum rather more than an hour late. The sequence of the 12-hour term amplitudes has the same general features as are found in the monthly values for the 12-year period, with high values at the equinoxes, lower values in winter and still lower ones in summer, with the exception that the autumn equinoctial maximum, usually occurring in October, is found instead in November, normally regarded as a winter month. The lowest amplitude, occurring in May, is abnormally low and would ordinarily be found in June. The 12-hour term phase angles show no great departure from the average, the only month in which the time of maximum differs by more than half-an-hour being April, in which month it is rather more than an hour early. For the 8-hour term amplitudes tend to be high in winter and low in summer as compared with the corresponding averages. The highest values are found in summer and the lowest at the equinoxes accompanied at the latter season by considerable changes in the phase angles. Winter and summer phases are nearly opposite. Similar phenomena are to be observed in the average values for the 12-year period. The 6-hour term amplitudes are at their highest at the equinoxes. Summer amplitudes appear on the whole to be higher than winter ones, but the difference is by no means well marked. The phase changes in the 6-hour term throughout the year are very wide and

Relative Humidity.—The highest daily mean value of the relative humidity was 97.5 per cent. on the 7th January, and the lowest 65.8 per cent. on the 31st May. The 8th August had a notably high mean relative humidity for a day in summer, namely, 96.3 per cent. The highest mean daily vapour pressure was 17.7 mb. which occurred on the 12th and 13th August, while the lowest was 5.2 mb. on the 24th November. The mean relative humidity for the year was 1.7 per cent. below average. The only months with relative humidity higher than average were June and July in each of which the excess was 1.5 per cent. For March the relative humidity was 5.5 per cent. and for November 4.2 per cent. below normal.

irregular, particularly in the summer months. On the average, the winter and equinoctial phases seem to be nearly opposed. No data are available for purposes

of comparison in the case of this term.

Rainfall.—The total rainfall for the year was 7 per cent. higher than normal, the actual excess being 108 millimetres. The wettest month was February, which had 275 millimetres of rain, or more than twice the normal amount, and only two days in the whole month on which no rain was recorded. August had an excess over normal of 60 per cent., and only four completely dry days. The month with least rainfall

was June, with a total of 24 millimetres, only 30 per cent. of the normal amount. January and May had each about half the average amount of rain. The greatest hour's rainfall was 8.7 millimetres, which fell between 15h and 16h on the 24th September.

Bright Sunshine.—The total amount of bright sunshine for the year 1923 was about 12 per cent. less than normal. Only March, August and November had more than average sunshine, the excess for November being about 30 per cent. and for the other two months 8 per cent. The most notable deficiencies were in February and June, both of which months had barely half the average amount of sunshine. The maximum recorded sunshine for any one day was 14.9 hours, on the 13th July. Records of 14.8 hours on the 29th May, and 14.5 hours on the 7th May, were also obtained, the last-mentioned being the day with the greatest proportion of possible sunshine recorded on any day during the year, namely, 95 per cent.

Wind Speed.—The mean monthly wind speeds were higher than average in the summer months, more particularly in May and August. In the winter months, on the other hand, wind speeds were, on the whole, below normal, the notable exception being February, which had an unusually large proportion of high winds, including three gales. Two of these, on the 5th and 7th, were of short duration, but in the third, on the night of the 26th–27th, the mean hourly winds were of gale force for 12 hours continuously. The gales of the 7th and the 26th–27th were responsible for a great deal of destruction. The year, as a whole, was not remarkable for the number of gales, one occurring in each of the months of August, September and November, besides those of February.

The highest hourly wind speed recorded was 24 metres per second (54 miles per hour) on the 7th February, with which was associated the highest gust of the year, 43 metres per second (96 miles per hour); this is the highest gust recorded by the Observatory anemometer since the commencement of its records in 1917. On this occasion two gusts of approximately the same strength occurred within a few seconds of each other and caused a considerable amount of damage to the Observatory buildings.

Cloud and Weather.—The mean amount of cloud at all observation hours was 7.7. The most cloudy month was December, with a mean amount of 8.5, but January and June each had 8.4. The least cloudy months were November, 6.5, and March, 6.6. During the year the most cloudy of the observation hours was 7h with an average of 8.1; the least cloudy was 21h with 7.4. The mean values for the individual observation hours for the year show a steady fall from 7h to 21h except that cloud amount at 15h is slightly higher than at 13h or 18h. There were very few occasions of cloudless sky, these amounting in all to no more than 28 in more than 2,000 observations; on no day throughout the year was the sky without cloud at all six observation hours, and the only near approaches to this were on the 22nd and 23rd November, on which days the average cloud amount was less than 1.0. The 24th November was also a very fine day, cloud amount at the observation hours having a mean value for the day of 1.0.

(1989) R 4

TABLE A.

Harmonic Analysis of Diurnal Variation of Pressure, 1923.

Cahirciveen (Valencia Observatory), Longitude 10° 15′ W.

							Pha	se, Local	Mean T	lime.		
Month.		Amplit Milli				Hour rm.		Hour rm.		Iour rm.	6-H Ter	
	c ₁	c ₂	c_3	c4	α ₁	Max.	α₂	Max.	α3	Max.	α_4	Max.
January February March April May June July August September October November December	·232 ·729 ·045 ·225 ·076 ·252 ·407 ·972 ·260 ·700 ·133 ·482	·341 ·388 ·453 ·239 ·340 ·276 ·271 ·207 ·305 ·328 ·381 ·290	· 190 · 108 · 057 · 040 · 102 · 110 · 100 · 035 · 018 · 030 · 122 · 098	.075 .060 .046 .062 .040 .038 .008 .050 .061 .055	259·7 143·9 318·2 279·7 226·7 201·3 144·3 181·9 238·5 240·9 34·7 322·3	h m 12 41 20 25 8 44 11 21 14 53 16 35 20 22 17 52 14 6 13 57 3 39 8 31	0 164·4 142·0 164·7 161·1 139·6 141·9 148·0 118·8 149·1 159·6 165·6 150·2	h m 9 56 10 16 9 30 9 38 10 21 10 16 10 4 11 2 10 2 9 41 9 29 10 0	358·9 9·7 16·5 167·7 180·7 163·9 149·3 176·1 251·3 316·1 27·5 6·1	h m 2 2 1 47 1 38 6 17 5 59 6 21 6 27 6 5 4 25 2 59 1 23 1 52	235·6 101·9 29·7 1·2 327·8 343·0 55·0 316·7 3·4 357·5 166·8 214·4	h m 3 355 5 48 1 0 1 299 2 2 1 47 0 355 2 14 1 27 1 33 4 43 3 56
Mean Year *Normal	 ·376 ·196 ·151	·318 ·310 ·307	·084 ·019 ·034	·047 ·020 ·004	 200·9 188·1	 16 16 17 28	 152·4 151·5	9 55 9 57	30·7 2·8	 1 19 1 56	347·9 83·5	 I 42 O 7

^{*} From the mean diurnal inequality for the period 1871-1915.

TABLE B.

Harmonic Analysis of Diurnal Variation of Temperature, 1923.

Cahirciveen (Valencia Observatory), Longitude 10° 15′ W.

							Ph	ase, Local	Mean 7	lime.		
Month.		Amplitu Jegrees A				Hour rm.		Hour erm.	8-H Ter			lour rm.
	c ₁	c ₂	c ₃	c.	α ₁	Max.	α2	Max.	α3	Max.	α4	Max.
•					0	h n		h m	0	h m	0	h m
January	495	170	.103	.015	207.1	16 1		0 59	241.1	4 39	77.9	5 46
February March	1.879	·344 ·484	·084 ·084	·051	227.1	14 52	1 5	0 53	305.2	4 24 3 I3	178.8	4 31
April	1.746	435	170	.100	221.5	15 IA		11 46	53.5	0 49	254.2	3 16
May	1.574	.098	.153	.053	242.7	13 49	1 - 0	I 4	63.5	0 35	15.4	1 15
June	1.393	.208	148	.030	241.1	13 50		0 35	71.0	0 25	201 4	4 9
July	1.719	.134	192	.042	246.9	13 32	,	0 33	72.9	0 23	342.4	1 48
August	1.340	.225	.094	059	247.9	13 28		0 36	35.7	I I2	267.4	3 3
September	1.112	·280	052	.106	243.3	13 47	83.8	0 12	100.1	7 38	276.4	2 54
October	.676	.326	.065	.025	249.5	13 22	58.1	I 4	310.2	3 6	237.3	3 33
November	1.034	.438	.174	.020	237 · 1	14 12	48.4	I 23	270.1	4 0	351.9	1 38
December	.367	284	.072	.065	231.3	14 35	33.2	I 53	240.9	4 39	62.8	0 27
Mean	1.164	·285	.116	.060							••	
Year	1.117	.273	.027	.021	239.3	14 3	64.6	0 51	37.1	1 11	248.4	3 22
Period 1871-1882	1.251	•328	.054		244.9	13 40	1 -	0 59	54.4	0 47	• •	٠٠.

TERRESTRIAL MAGNETISM.

Notes on the Magnetic Observations for the Year 1923.

Absolute observations of declination, horizontal force and inclination were made weekly at the Valencia Observatory during the year 1923. The instruments in use were the same as in previous years, namely, the Dover unifilar, No. 139, with collimator magnet 139A and mirror magnet 139C, and the Dover dip circle, No. 118. The needles of the dip circle were sent to the Kew Observatory early in the year for testing, and during the interval from the 13th March to the 18th July, inclusive, a pair of needles, No. 33B, belonging to a dip circle at Kew, was used. The tests at Kew having proved satisfactory, the Valencia needles were brought into use again in July without alteration. Comparisons carried out before and after the period during which the needles 33B were used showed no sensible difference between the readings of the two pairs of needles so that no instrumental discontinuities were introduced by the changes in March and July. The mean times of observation were 10.20 for the declination, 11.38 for the horizontal force and 14.29 for the inclination, all according to Greenwich Mean Time. In the individual observations the only departures of note from the mean times were one of 6 minutes and one of 7 minutes for inclination. The deflection of the mirror magnet was measured for two distances of the collimator magnet, namely, 30 cm. and 40 cm., and a single distribution constant, P, was calculated. The complete deflection observation consisted of eight readings of the mirror magnet as in the latter part of the year 1922. It had been found in 1922 that the extreme variation in P was equivalent to about 6γ in the value of H as compared with 3γ in the previous year, but it did not appear to be necessary to attribute this increase in what must be presumed to be casual error to the change in the routine of the deflection observation, and this is borne out by the extreme variation in P found for the year 1923 which is 3γ in the value of H, or the same as in the year preceding that in which the change was made. The mean value of P was 7.66. The moment of the collimator magnet has decreased at the rate of about I units per annum as compared with 3 units per annum in the previous two or three years.

The values of the declination, horizontal force and inclination obtained in the absolute observations are given in detail in Table C. All the observations made are included in this table, but in Table D the mean monthly values are computed from only such of the absolute observations as were taken at times subsequently found, by reference to the Kew magnetograph curves and the quarterly list of daily "magnetic characters" published by authority of the International Meteorological Committee, to be free from serious disturbance. Observations in Table C taken at disturbed times, and not, therefore, utilised for the mean values in Table D, are marked with an asterisk. The north, west and vertical components and the total force for each month and the year are computed from the corresponding mean values of the observed elements.

Westerly declination has diminished by 10'·5 as compared with 1922. From 1921 to 1922 the decrease was 9'·5 and in the previous 12 months 11'·4. The average annual decrease for the five years 1915–1920 was 9'·2, and for the five years 1910–1915 it was 8'·2. During the three years ending in 1923 the average annual decrement is 10'·5 so that the rate of the eastward movement of the magnetic needle appears to be increasing slowly.

Northerly inclination decreased by $1' \cdot 5$ from 1922 to 1923. The corresponding change for the preceding year was $-0' \cdot 4$, and for the year previous to that $-1' \cdot 9$. From 1910 to 1915 the average yearly decrease was $1' \cdot 0$ and from 1915 to 1920 $0' \cdot 5$. For the three years 1920–1923 the average change per year is $-0' \cdot 8$. Inclination, therefore, continues to diminish at a slow rate.

It was remarked in these notes for the year 1922, that since the year 1920 the horizontal force had appeared to be increasing slowly whereas previously it had shown a steady decline from year to year. For the five-year period 1910–1915 the average annual decrease was about 5γ and for the period 1915–1920 about 6γ , while from

1920 to 1921 an increase of 8γ appeared, followed the next year by a further increase, but only of 1γ . The mean for 1923 shows a further increase of 3γ over that for 1922, so that the steady fall in the horizontal force would seem definitely to be checked and to have given place to a slow annual rise.

The horizontal force, however, is merely a component, and to consider its changes apart from the corresponding changes in the total force might give rise to misleading conclusions. Reference to the last column of Table D shows that the reversal of the annual change in the horizontal force from 1920 onwards is not accompanied by any such reversal in the total force. From 1910 to 1915 the average yearly change in the total force was -49γ , and from 1915 to 1920 it was -33γ . From 1920 to 1923 the mean annual change is again -33γ , so that the total force continues to decrease at a fairly uniform rate. The individual changes from year to year as shown in the table are somewhat irregular, but this may be due in considerable measure to instrumental uncertainties. The total force is computed from the horizontal force and the inclination, using the formula $T = H \sec I$, so that an error of o' $\cdot I$ in I would give an error of approximately 47 in T at Valencia. In addition, it is to be remembered that the secular change data for Valencia are obtained from absolute observations made at fixed hours at any of which the value obtained for an element may differ, by an amount which is not necessarily constant, from its true mean value for the day of observation. It is by no means improbable that owing to this and errors of observation, uncertainties to the extent of several tenths of a minute of arc may be introduced into the mean value of I for the year. For the average change over a series of years these possible errors are naturally much diminished and the average fall of 33 y per annum in the total force obtained from the values in Table D is probably a close approximation to the true change. This continued decrease in the total force indicates that the rise in the value of the horizontal force observed since 1920 is not a true increase in the magnetic field but merely a component increase arising from the continued fall in the inclination, which becomes proportionally more effective in the horizontal component as the actual inclination angle itself becomes smaller. magnetic field in the Valencia district continues to become less year by year, therefore, although without observations of inclination the opposite would have appeared to

be the case for the last three years.

TABLE C.

Cahirciveen (Valencia Observatory), Absolute Magnetic Observations, 1923.

Latitude 51° 56'. Longitude 10° 15'W.

Da	te.	Westerly Declination	Horizon- tal Force	Northerly Inclination	Date.		Westerly Declination	Horizon- tal Force	Northerly Inclination
January	3 ··	8 52·5 18 52·6	γ 17864 17860	67 59·I 68 0·7	July	3 4	° ', 18 44·2	γ 17853	68 o·1
13	17 19 24	18 51·2 18 52·0	17861	68 0·9 68 2·4	,, ,,	11 18 25	18 45·8 18 44·7 18 42·9	17844* 17867 17848	68 3·2 68 0·3* 68 1·1
,,	31	18 51.2	17846	68 3.0	August	I	18 43·I	0.6	67 59.9
Februar	8 16	18 50·8 18 51·3	17863	68 3.4))))	2 8 9	18 46.0	17846 17858	68
"	21 23 28	18 49·5 18 52·7	17850 17853	68 1.8	"	15 16 22	18 44·7 18 45·5	17851 17878	68 0·9 68 1·1
March	2			68 3·4 68 1·6	,,	29	18 45.4	17849	68 2.0
,, ,,	6 9 13	18 50.0	17862	68 2.6	September ,,	5 6 12	18 43·9 18 43·3	17852 17842	68 I·7 68 I·8
"	14 20 21	18 48·7 18 47·8	17863	67 59.2	,, ,,	19 26 27	18 44·3 18 43·9	17847 17836*	68 2.9
"	27 · · · 28 · · ·	18 51.5	17833	68 2.9	October	4	18 44.0	17847	
April	4 · · · 5 · · ·	18 46.8	17829	68 I·6	"	6 11 17	18 42·3 18 42·3	17845 17837	68 3·0 68 3·5
"	11 18 19	18 49·1 18 45·8	17860 17839	68 0·5 68 1·9	"	18 24 31	18 44·8 18 42·2	 17846 17840	68 1·6 68 0·7
))))	20 24		17843	68 0.4	November	7 8	.,		68 0.4
May	25 ··· I ···	18 48.5		68 1.5))))	14 21	18 42·2 18 42·7 18 43·4	17848 17829 17822	68 1·9 67 59·5
"	2 8 9	18 50·7 18 47·4	17865 17861	68 	,, December	28 4	18 43.7	17860	$\frac{68}{68} 1.8$
"	15 16 18	18 47.5	17854	68 2.4	"	12 19 21	18 41·0 18 42·1	17869 17878 17866	67 59·6 ·· 68 0·5
"	23 29	18 44.1	17857	68 1·2 68 0·7*	"	26 27 28	18 46.4	17847	68 1.7
June	8	18 46.9	17848	68 1.5	,,	20	••	1/04/	••
" "	13 20 21	18 49·7* 18 49·1	17829 * 17857	68 o·3* 68 o·3					
"	27	18 45.4	17850	68 1.8					·

^{*} Disturbance at these times. Values not utilised in computing means given in Table D.

TABLE D.

Valencia Observatory, Cahirciveen.

Magnetic Data for the Year 1923.

1923	Declination (West).	Inclination (North).	Horizon- tal Force.	North.	West.	Vertical.	Total.
January February March April May June July August September October November December Year, 1923	(West).	(North). 68	γ 17858 17855 17847 17843 17857 17852 17856 17847 17843 17840 17865 17852 17849	7 16899 16897 16892 16892 16905 16909 16908 16902 16896 16919	y 5774 5769 5759 5748 5752 5749 5737 5726 5726 5725 5736 5746 5796	y 44245 44288 44244 44204 44246 44230 44251 44231 44266 44237 44189 44247 44242 44289	γ 47712 47753 47768 47669 47713 47697 47717 47700 47729 47700 47654 47718 47707
Year, 1921	19 6·5 19 17·9 19 27·2 19 36·2 20 3·8 20 44·6	68 3·4 68 5·3 68 6·1 68 6·5 68 7·9* 68 13·0	17848 17840 17842 17844 17869	16865 16837 16823 16810 16785	5842 5896 5942 5987 6130 6337	44299 44353 44385 44407 44519* 44771	47760 47806 47837 47858 47972* 48215

^{*} Mean of II months only.

Readings in millibars at exact hours, Greenwich Mean Time.

285. Cahirciveen (Valencia Observatory): Hb (height of barometer cistern above M.S.L.) = 13.7 metres.

January, 1923.

Da	y.	ı.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
1	I	mb.		mb.		mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	Lamb	1 1	1
																										004·1 996·3
	4	017.9	018.4	019.1	019.4	019.8	020.2	020.7	020.0	021.1	021.3	021.4	020:0	007.1	000.4	009.4	018.6	011.0	012.4	013.0	014.0	015.1	015.7	016.7	017.0	006.7
	5	006.9	004.9	003.4	001.0	001.7	000.9	001.0	001.9	003.0	003.7	004.6	004.9	005.6	006.1	007.0	008.0	009.1	009.4	010.3	011.2	014.1	012.9	013.3	013.0	018.1
	6	014.3	014.7	015.3	or 5.5	015.7	016.3	017.2	017.4	018-4	018-5	018-4	018.2	017.5	016.8	016.2	015.5	014.3	013.6	013.0	013.0	013.0	012.8	012.7	012.3	015.5
	8	009.3	009.9	010.9	011.0	012.6	013.6	015.0	016.3	017.8	018.6	020.6	013.0	013.1	012.0	012.1	011.5	011.0	011.0	010.5	010.2	009.9	009.2	008.6	008.5	011.0
																										009.9
																										018·6 023·3
Level	14	024.1	024.0	023.9	023.0	023.8	023.5	023.7	023.9	025.4	026.2	025 0	025.2	024.7	024.2	024.3	024.5	024.7	025.0	024.9	025.0	024.9	024.6	024.4	024.3	025 1
	15	032.0	032.1	032.7	032.5	032.4	032.5	032.6	032.9	033.2	033.4	033.6	033.2	032.9	032.3	032.2	032.2	032.4	032.9	032.8	032.7	032.4	032.3	032.1	032.2	032.6
Station	16 17	031.9	031.8	031.4	031.2	030.5	030.4	030.4	030.2	030.2	030.0	029.6	029.0	028.2	027.9	027.6	027.2	027.3	027.0	026.7	026.5	026.3	026.2	026.1	026.2	028.9
tat	18	034.4	034.6	035.0	035.5	035.6	035.4	035.9	036.4	02/5 037·I	027.9	020.4	037.3	020.5	020.7	029.2	029.7	030.6	031.5	032.2	032.9	033.0	033.5	033.6	034.3	029.0
ഗ		-3/ 2	1 ~ J / J	(J) -	IV.)/ 4	10.30	1030 2	IU JU I	10 10 2	030.3	1035.0	() () (034.4	1033.7	10.23	102T+2	U31.1	1020 · h	ILO 2O · N	1020.2	0.20.0	1028.8	1008.4	1008.1	1000.0	033 · 4
																										033.0
	24	034.5	034.2	034.3	034.5	034.5	034.6	034.8	035.0	035.6	036.0	036.6	036.2	035.8	035.2	035.0	034.9	035.6	035.3	035.4	035.0	035.5	035.1	035.0	034.7	035.6
	3	3, -	37 -	03/ 1	03/ 0	03/ 0	037 0	03/1	03/4	03/19	030.2	037.9	037.0	037.5	037.1	030.9	037.0	037.1	037.3	037.5	037.2	037.2	037.1	037	037.3	037-3
	26 27	037·0 032·8	036.7	036.8	036.7	036.6	036.4	036.2	036.3	036.7	036.8	036.9	036.4	036.0	035.4	035.1	034.9	034.6	034.7	034.5	034.3	034.1	034.0	033	6 033.2	035.7
	28	030.1	029.8	029.7	029	028.7	028.5	028.3	028.3	028.8	028.0	028.0	028.7	1028.2	027.4	1029.0	029.7	029.7	029.0	7026.2	029.9	030.1	030.1	030	2 030.4	1030.7
	_			~~ 7	V-4 -	,,,,,	1023 1	044 7	1022 4	1044 4	10222	10221	1021.0	MO21 * 5	10771 *6):O2I :C	1020.7	1020.	71020.2	SIO 20.2	102110	NO2T.	(O) T . (COST	0027.5	022.3
\		1	1	ı	1	1	1	1	1	i	1		1			1	1	1	1		1	1		1	1	
Mean		1022	1022	1022	1022	TOXZ	1022	1022	1023	1023	1023	1023	1023	1023	1022	1022	1022	1023	1023	1023	1023	1023	1023	1023	1023	018·9 1023
(Station Mean			1 33	, 00	1 00	- U.	1 33	1 /3	1 .02	1 '55	1 .00	. 99	.01	1 .23	1 197	71 •99	99 199	.00	•24	.31	1 .43	i •46	13.1	tl •20	1 .28	l ∙oo
(Sea lev	el)	.30	.22	31	.31	•22	1024	.43	.72	.25	35	•54	.30	•92	1024	68	68	.78	93	1025	1025	1025	1025	1024	1024	
286.	Cahi	rcive	en (V	alenc	ia O	bserva	atory)) : H	b =	13.7	metr	es.											Fe	brua	rv. 19	23.
286.		mb.	mb.	mb.	mb.	mb.	atory)	mb.	mb.	mb.	l .mb	l mb.	mb.	mb.	mb,	l mb.	l mb.	mb.	l mb.	l mb.	l mb.	l mb.	Lmb	1 mh	ry, 19	Lmb
286.	1 2	mb. 018·1 012·6	mb. 017·5 012·2	mb. 016·6 012·3	mb. 015·5	mb. 014·4	mb.	mb. 013·9	mb. 013·9	mb. 014·4	.mb 014·4	mb. 014·5	014.1	013.2	012.1	010.8	010.8	010.5	010.6	010.1	010.7	010.5	mb.	mb.	mb.	mb.
286.	1 2 3	mb. 018·1 012·6 012·6	mb. 017·5 012·2 012·5	mb. 016·6 012·3 012·5	mb. 015·5 012·2	mb. 014·4 012·0	mb. 014·1 011·6	mb. 013·9 011·1	mb. 013·9 011·0	mb. 014·4 011·1	.mb 014·4 011·2	mb. 014·5 011·4	014.1	013.2	012.3	010.8	011.0	010.5	011.1	011.1	010.7	010.5	mb. 011·5	mb.	mb.	mb. 013·3
286.	1 2 3 4	mb. 018·1 012·6 012·6 016·5	mb. 017·5 012·2 012·5 016·7	mb. 016·6 012·3 012·5	mb. 015.5 012.2 012.2	mb. 5 014·4 2 012·0 2 011·9	mb. 014·1 011·6 012·3	mb. 013·9 011·1 012·3 018·6	mb. 013.9 011.0 012.3	mb. 014·4 011·1 012·9	.mb 014·4 011·2 013·1	mb. 014·5 011·4 013·0	014.1	013·2 011·5 012·6	012.1	010.8	010.8	010.5	010.0	013.3	010.7	010·5	mb. 011·5 012·1	mb. 012·4 015·8	mb. 012·6 012·7	mb. 013·3 011·6
286.	1 2 3 4 5	mb. 018·1 012·6 012·6 016·5 010·6	mb. 017·5 012·2 012·5 016·7 009·7	mb. 016·6 012·3 012·5 017·2 009·1	mb. 015.5 012.2 012.2 017.3 007.9	mb. 5014.4 2012.0 2011.9 3017.8	mb. 014·1 011·6 012·3 018·1 006·3	mb. 013·9 011·1 012·3 018·6 006·0	mb. 013·9 011·0 012·3 018·9 005·3	mb. 014·4 011·1 012·9 019·2 004·7	.mb 014·4 011·2 013·1 019·4 004·2	mb. 014·5 011·4 013·0 019·4 003·5	014·1 011·7 013·0 019·0 002·4	013·2 011·5 012·6 018·4 001·3	012·1 011·3 012·2 017·8 999·7	010·8 011·2 011·7 017·1 998·0	010·8 011·0 012·1 016·8 996·8	010·5 011·0 012·6 016·4 995·5	010·6 011·1 012·9 016·5 994·1	010·1 011·1 013·3 015·2 992·8	010·7 011·2 013·8 014·7 991·5	010·5 011·4 014·4 013·7 989·9	mb. 011·5 012·1 015·1 013·2 988·7	mb. 012.4 015.8 012.4 987.0	mb. 012·6 012·7 016·2 011·6	mb. 013·3 011·6 013·0 016·8 000·4
286.	1 2 3 4 5	mb. 018·1 012·6 012·6 016·5 010·6	mb. 017·5 012·2 012·5 016·7 009·7	mb. 016·6 012·3 012·5 017·2 009·1 982·8 968·4	mb. 015.5 012.2 012.2 017.3 007.9	mb. 5014.4 2012.0 2011.9 3017.8 9007.1	mb. 014·1 011·6 012·3 018·1 006·3 982·2	mb. 013·9 011·1 012·3 018·6 006·0	mb. 013·9 011·0 012·3 018·9 005·3	mb. 014·4 011·1 012·9 019·2 004·7 982·6	.mb 014·4 011·2 013·1 019·4 004·2 982·8	mb. 014·5 011·4 013·0 019·4 003·5	014·1 011·7 013·0 019·0 002·4 982·3	013·2 011·5 012·6 018·4 001·3	012·1 011·3 012·2 017·8 999·7 981·4	010·8 011·2 011·7 017·1 998·0	010·8 011·0 012·1 016·8 996·8	010·5 011·0 012·6 016·4 995·5	010·6 011·1 012·9 016·5 994·1	010·1 011·1 013·3 015·2 992·8	010·7 011·2 013·8 014·7 991·5	010·5 011·4 014·4 013·7 989·9	mb. 011·5 012·1 015·1 013·2 988·7	mb. 012·2 012·4 015·8 012·4 987·0	mb. 2 012.6 3 012.7 3 016.2 4 011.6 985.3 3 980.7	mb. 013·3 011·6 013·0 016·8 000·4
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Note.—When pressure exceeds 1000 mb. the leading figure 1 is not printed, i.e., 1001.7 mb. is written 001.7. This rule does not, however, apply

PRESSURE.

Readings in millibars at exact hours, Greenwich Mean Time.

287. Cahirciveen (Valencia Observatory): H_b (height of barometer cistern above M.S.L.) = 13.7 metres.

March, 1923.

Day.		ı.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Me
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A	r	998.3	998.4	998.5	998.6	998.7	998.5	997.8	996.9	996∙0	994.6	992.5	990.0	987.0	982.8	980.7	981.3	982.1	983.5	984.6	985.5	986.1	987.1	988.4	989.0	1999
	2	389.3	989.4	989.2	989.0	988.8	988∙1	987.9	988.4	988.6	988.7	988.8	988∙6	988∙0	987.9	987.4	987.1	987∙0	987.4	987.6	987.3	987.4	987.8	988.3	988.5	PA
i	2 1	280.0	080.2	080.4	080.8	000.7	002.4	004.1	laa6·3	1998.7	0000	1001.7	002.9	004.2	005.7	007.1	008.6	0009.6	0.110	012.8	013.8	015.1	015.7	010.4	017.2	loc
	4	21.7.0	018.3	018.7	010.2	010.7	020.5	020.7	021.0	021.6	021.6	021.9	021.8	021.7	021.1	020.9	020.5	019.9	019.6	018.8	018.4	017.1	016.3	015.0	014.2	Ю
	5	213.3	012.3	011.7	012.1	012.7	013.4	014.0	014.9	015.7	016.4	017.0	017.7	018.0	018-4	018.3	018.2	018-2	018∙3	017.9	017.2	016.7	016.2	015.6	014.7	01
1 ,	6	712.7	012.2	0.010	008-6	007:3	006.1	006.4	007:3	007:3	007.6	008-1	008.2	008-1	008.1	008-1	007.8	007.6	008.0	008.2	008.3	008.7	008.9	009.2	009.4	oc
	7	200.6	000.0	000.0	010.3	010.6	011.4	011.6	012.3	013.2	013.5	013.5	014.0	014.2	014.2	014.6	014.7	015.5	016.0	016.5	016.7	017.1	017.5	017.9	018.0	О
	8	318.T	018.0	018.0	018.3	018.4	018.7	010.1	010.6	020.1	020.0	020.3	020.2	020.4	019.0	020.0	020.0	020.1	020.1	020.3	020.3	020.3	020.3	020.1	019.9	01
1		210.0	010.7	010.3	018.6	018.6	018.6	018.3	018.4	018.2	018.0	017.6	017.2	016.7	015.7	015.3	014.6	014.3	014.5	014.2	013.8	013.9	013.3	012.6	011.8	oı
10	9 (011.5	010.6	009.9	008.4	007.4	006.7	006.4	005.4	004.4	003.1	002.4	001.4	000.6	999.4	998.7	999.4	999.9	000.5	001.7	002.4	003.3	004.0	005.2	005.9	oc
_	_]		00=10	00=.0	008.5	008.7	000.4	000.0	010:0	011.7	011.8	012:1	012.0	011.0	011.4	011.4	011.0	010.4	000:4	000.5	000.3	008.8	008.7	008.7	008.0	oc
I	1 19	0000	007.2	007.8	000.7	000.7	009 4	009 9	010 9	011 /	011 0	007.5	006.1	006.6	006.7	007:1	007.8	008.0	010:0	012.2	012.8	014.8	016.0	016.0	017.0	loc
I	2	008.7	008.4	007.9	007.3	007.1	000.7	000-2	005.7	005.0	004 9	005	0001	006.0	000 7	036.1	026.0	026:0	026.5	026.7	026.8	026.8	026.0	026.0	026.7	02
I	3 ^c	018.4	010.1	019.9	021.0	021.0	022.5	023.4	024.1	025.5	025.0	020.0	026.0	020.0	020-3	0201	020 0	020 0	020 5	020 /	022.5	022.7	022.7	022.7	023.6	lñ9
evel	4	026.6	026.3	025.9	025.5	025.3	025.1	025.2	025.3	025.0	025.0	025.0	024.8	024.4	024.0	023.0	023.3	023 4	023 3	023 0	023 3	023 /	023 /	023 /	021.1	02
ē r	5	023.7	023.3	023.2	022.8	022.7	022.8	022.8	022.8	022.9	022.0	022.0	022.6	022.2	022.0	021.9	02,1.5	021.5	021.5	021.7	0217	021 0	021 0	021 2	021 1	٦
Station	6	020.8	020.3	019.8	019.4	019.3	019.3	019.7	019.9	020.1	020.1	020-1	020.1	019.9	019.6	019.6	019.1	019.5	019.9	020.3	020.7	021.1	021.0	021.2	021.0	02
.≌ 1∶	7 🛚	0.120	020.8	020.3	020.2	020.3	020.6	021.0	021.4	022.0	022.1	022.2	022.2	021.9	021.9	021.7	021.0	021.8	022.0	022.7	023.5	023.4	023.0	023.5	023.2	02
ta at	8 (023.3	023.8	023.5	023.4	024.0	024.2	024.3	024.7	024.9	024.2	024.4	023.9	024.0	023.8	023.5	023.2	023.0	023.3	023.4	023.2	023.0	023.3	022.9	022.7	02
# 19	പ	12 T · 8	021.3	020.7	020.5	020.3	OTO-8	010.0	O10.8	010.7	010.3	018.0	018.01	018.0	017.5	017.2	017.0	017.0	017.3	017.7	017.8	017.9	017.0	017.5	017.1	lσr
1 20	0	217.1	017.0	016.8	016.7	016.4	016.6	016.9	017.3	017.4	017.4	017.1	017.0	017.0	016.8	016.7	010.8	017·1	017.8	018.1	018.0	019.1	019.3	019.4	019.4	lo,
2	1	o19·3	019.6	019-9	019.8	019.7	019.8	020.0	020.3	020.9	020.8	020.9	020.7	020.5	020.1	020.0	019.7	019.5	019.6	019.5	019.5	019.6	019.3	018.7	018-4	01
2:	2 1	218.2	017.7	017.2	Ιστά·8	016.3	016.1	016.1	lo16·2	016.2	015.8	015.4	015.0	014.0	014.1	013.4	012.9	012.5	012.0	012.0	012.7	012.0	012.3	012.1	011.0	lοι
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2	4 10	212.5	012.4	012.2	012.1	012.2	012.3	1012.6	012.0	012.5	OI 2 · I	012.3	1012.0	012.0	OII · 7	011.1	010.0	010.3	000.9	009.5	1000.3	1000.2	1007.0	1000.3	005.2	10^{1}
2	5	004.3	003.7	003.0	003.2	003.7	006.1	008.7	010.3	011.6	012.8	014.2	014.9	015.7	016.1	016.3	016.5	016.9	017.3	017.4	017.5	017.3	017.0	016.8	016.5	01
2	6 l	016-0	015:2	014.7	014.0	013.2	012.8	012.0	012.2	012.2	011.5	011.3	010-8	0.00	009.5	008.8	008∙0	007:3	006.5	006·0	005.4	005.1	004.4	003.7	003.2	01
2	~ L	ററാ ന	002:1	002:0	002.3	002:3	002.4	1002.8	0.200	003.5	1003.3	003.3	002:9	002.7	1002:5	002.4	002:3	002.5	002.0	00312	004.0	1004.0	005.7	1007.0	0000	ľ
2	Я I	000.2	010.4	OTTE	012.4	013.7	014.7	ιοτό·ο	lo16·a	018-4	0.010	010.5	020.2	020.8	020.0	02I · I	02I · I	021.5	021.3	021.5	021.4	021.7	021.0	021.0	021.5	lΟī
2	^ I	021.2	020.7	020.4	0.010	010.7	010.4	0.8±0	lo i 8 · a	018.7	1018.3	lot8:o	017.0	017.7	1017.2	010.0	010.0	010.2	010.2	010.7	010.9	010.0	010.0	010.0	017.0	IJΙ
3	2	017.0	017:0	017:4	017.7	018.0	018.6	010.3	010.6	010.0	020 I	020 1	020.0	019.9	019.5	019.1	018.9	019.3	018.8	019.4	019.3	019.4	019.0	019.0	o18.8	OI
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tion le	vel)	.50	.30	.10	: ∙01	.03	.22	47	{ ·80	•12	0.5	.07	95	•79	48	.30	{ .21	32	1 '57	1 .07	1 .02	1 17	. 10	1 12	12	<u> </u>
an			1014												1	1	1	1-07.	1.0.	ITOTE	LIOTE	LTOTE	17015	LIOTE	TOTE	ITC

Gahirciveen (Valencia Observatory): $H_b = 13.7$ metres.

April, 1923.

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mb	mh I	mb	mb	mb	mb	mh	l mb	mb	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.					
2.6	014.3	07.4.0	014.0	0.12.0	014.0	074.2	014.4	014.6	014.7	015.1	015:0	0.14.0	0.14.0	015.0	015.1	015.3	015.6	016.2	010.0	017.2	017.5	017.9	o:810	015
0 * Q . O l	A+ Q . + 1	0 + R . 0	OT S.T	OT S. A	OTX:O	OTX O	MOIO:7	IOTO:X	OTO · N	ยดวกเก	IIOTO · XI	10·20 · I	1020 O	O O O	OTO:71	1010.01	0.610	1019.0	1019.91	1019 9	019 9	1019 7	019 4	POTO
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009.4	008.8	008.0	007.3	006.4	005.9	005.3	004.6	003.8	002.9	002.0	001.3	000.1	999.0	998.1	996.7	995.5	994.8	994.1	993.5	993.0	991.9	991.0	992.1	000
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996·6	996.5	996.3	996.2	996.2	996.4	996.5	, 996.6	996.9	996.8	996.7	996.8	996.0	996.8	990.9	990.0	990.0	990.0	280.7	280.3	080 F	088.2	087.7	087.2	, 000
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003.0	003.2	003.6	004.2	004.7	002.1	002.8	000.1	006.5	000.0	007.3	007.7	008.0	009.1	000.3	000.2	204.6	000 7	003.0	003.6	003.2	002.0	003.4	002.2	, 00
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008.0	007.9	008.0	000.2	008.4	000,0	009.0	009.5	009.4	207.5	2008.0	008.4	208.6	208.8	008.0	000.0	000.4	000.0	010.6	011.1	012.0	012.4	012.6	013.0	3000
000.9	000.0	000.2	000.4	000.4	000.	000.9	007.3	007.0	275.6	0000	000.4	000.0	000	010.0	016.1	016.6	017.4	018.1	018.6	019.0	019.4	019.8	020.2	:016
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002:0	004:2	005.6	007:0	008:2	000.7	001.2	002.5	003.7	004.2	004.6	005.2	005.8	006.3	006.9	007.1	007.2	007:3	008.0	008.3	009.0	009.2	009.4	009.5	:00ر
000.56	000.7	LOOO · X	010.1	1010.2	POTT:	0 0 1 1 . 2	OTTIX	MOT2 T	012.5	1012.5	OT2 - 4	012.2	1012.51	1012.2	012.4	O14:31	OLA N	O1-4	1012 4	10 91	1 7	/		
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007:6	007.1	007.5	00/ 3	007	1006.0	1006.1	006.2	006.4	006.4	006.6	200.8	007.0	007.4	007.7	007.8	008.2	008.3	008.4	008:8	009.5	009.6	009.9	010-2	.007
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Note.—When pressure exceeds 1000 mb. the leading figure 1 is not printed, i.e., 1001.7 mb. is written to monthly means.

Readings in millibars at exact hours, Greenwich Mean Time.

289. Cahirciveen (Valencia Observatory): H_b (height of barometer cistern above M.S.L.) = 13.7 metres.

May, 1923.

Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
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31	018-5	018.7	018.7	018.8	019-1	019.6	020.0	020-1	020.3	020.0	021.0	021.1	021.2	020.7	020.4	020-1	019.7	019-6	019.7	019.9	020.5	020.6	020 - 2	020-1	020.0
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Mean (Sea level)	1017			.06	.02	20	42	51	.72	.70	80	81	.83	.74	.64	•44	32	.28	38	·61	•04	.08	.04	1 .02	.56

290. Cahirciveen (Valencia Observatory) : $H_b = 13.7$ metres.

June, 1923.

290.	Uanii	CIVOE	n (V	aienc	ia U	Serva	itory)	: n	, =	13.7	men	es.														
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Note.—When pressure exceeds 1000 mb. the leading figure 1 is not printed, i.e., 1001.7 mb. is written 001.7. This rule does not, however, applied monthly means.

PRESSURE.

Readings in millibars at exact hours, Greenwich Mean Time.

291. Cahirciveen (Valencia Observatory): H_b (height of barometer cistern above M.S.L.) = 13.7 metres.

July, 1923.

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	3	007.8	007.4	007.1	007.0	0071	[007·2	2 007.5	008.0	008.6	008.0	009:	2 009.5	009.7	009.8	009.8	009.9	009.8	010.0	010.1	010.0	010.2	010-2	010	2 010.	3001
	4	010.1	009.9	009.8	009.0	010.0	010-2	010 4	010.0	010.9	011.1	011.	3 011.6	011.9	012.3	012.4	012.5	012.6	012.8	013.4	013.5	013.0	014.4	014	6014.	6011
	5	015.1	014.9	015.0	015.1	015.2	015	015 6	015.8	016.0	016.2	016.6	016.7	016.7	017.0	016.8	017.0	017.0	017.2	017.2	017.4	017.8	017.8	017	6017	4016
ł			İ	1	1		1	1	1	ļ	ł	İ	1	i	1		!		1		1	i		1		1
	6	017.3	016.9	016.2	016.2	015	015.1	014.5	014.2	013.9	013.4	013.2	012.8	012.8	012.8	012.6	012.8	012.8	012.7	013.2	013.6	013.7	013.0	013	8013.	7014
1	7	013.6	013.4	012.9	012.6	012	012.8	013.0	013.0	013.3	013.4	013.6	013.6	013.6	013.7	013.7	013.9	014.2	014.4	014.7	014.0	015.2	015.6	015	7015	8013
- 1	8	015.7	015.4	015.0	014.8	014.5	014.3	014.1	014.0	013.4	012.9	012.4	011.6	010.9	010.6	010.3	009.9	009.6	009.7	009.7	009.9	010.2	010.2	010.	3010.	0012
	9	009.8	009.4	008.8	008.7	008.5	009.0	008.9	009.0	009.3	009.5	009	009.5	009.9	010.5	010.5	010.5	010.7	011.0	011.1	011.4	011.8	012.3	012	5012	8010
1	10	012.8	012.6	012.8	012.9	013.2	013.8	014.1	015.0	015.3	015.5	015.6	015.7	015.9	016.4	016.8	017.1	017.7	018.0	018.7	019.2	010.6	010.0	020	0020.	3016
1				1	-			1				-					'		1	1 ′	_] -			
1	II	020.5	020.4	020.4	020.5	020.7	021.1	021.4	021.9	022.2	022.3	022.6	022.7	023.1	023.2	023.5	023.5	023.4	023.4	023.4	023.4	023.7	023.9	023.8	8 024.0	0022
l	12	023.5	023.4	023.3	023.3	023.4	023.5	023.7	024.0	023.8	023.9	024.4	024.6	024.4	024.2	024.1	024.0	024.0	023.6	023.6	024.0	024.4	024.2	023.0	023.0	6023
-	13	023.7	023.2	022.9	023.0	022.8	023.0	023.0	022.9	022.8	022.5	022 2	021 4	021.3	020.9	020.9	020.9	020.8	020.4	020.3	020.3	020.7	020.0	021.0	020.8	8021
Š	14	020.3	019.8	019.4	019.3	019.4	019.6	019.5	019.3	018.8	018.6	018.7	018.7	018∙6	018.4	0.810	017.8	017.6	017.4	017.1	016.0	016.0	016.5	016.2	2015-8	8018
Level	15	015.2	014.5	013.6	012.6	012.1	011.6	010.8	010.5	009.7	009.2	009.0	009.0	009.2	009.4	009.4	009.6	009.8	009.8	010.1	010.2	010.3	010.7	010.8	8010.8	8010
	,		, ,			İ	ì	1			_					[-	_			J	,	1		1
Station	16	010.8	010.0	010.0	010.8	010.8	011.0	011.2	011.2	011.0	011.1	011.1	011.1	011.1	011.0	010.7	010.6	010.3	010.1	010.2	0.00	010.2	010.3	010-2	2010-2	2010
Ĕ	17	010.1	009.7	009.4	008.9	008.7	008.8	008.9	009.0	009.0	009.2	009:3	009.8	009.9	010.2	010.5	010.7	010.8	011.2	011.6	011.8	012.1	012.7	013.0	013.2	2010
त्त्	18	013.2	013.3	013.5	013.8	014.3	014.6	014.9	015.5	015.9	016.7	017.0	017.3	017.6	018∙0	018.1	018.3	018-2	018.5	018∙6	018.8	010.0	OT8.8	018.8	3018·	5016
St.	19	018.1	017.9	017.4	017.4	017.0	016.9	017.0	017.2	017.6	017.9	018·1	018·8	018.9	019.4	019.8	019.9	010.0	020.0	020.1	020.5	021.1	021.3	021.	1021.2	2 018
1	20	021.1	021.1	021.1	021.4	021.6	021.0	022.2	022.6	023.3	023.4	023.6	023.7	023.8	023.8	023.7	023.7	023.6	023.7	023.0	024.0	024.5	024.4	024	3024.	1023
- 1					•		1	[[00	۱' '	J	"		۱ ا	3 /	,		, ,	-5					7	73
-	21	024.4	024.3	024.4	024.6	025.0	025.2	025.7	026.1	026.4	026.5	026.7	027.0	027.1	027.3	027.3	027.4	027.4	027.3	027.5	027.7	028.0	028.0	027.0	027.8	31026
	22	027.7	027.4	027.2	027.1	026.9	026.8	026.9	026.6	026.4	026.0	026.1	026.2	025.7	025.2	024.9	024.2	023.7	023.2	022.5	021.0	021.6	021.4	020	010.8	3025
l	23	018.7	017.5	016.3	015.4	014.9	014.6	014.6	014.5	014.5	014.5	014.5	014.4	014.5	014.5	014.4	014.4	014.5	014.5	014.7	014.0	015:2	015.2	015	3 015:2	2015
- 1	24	014.8	014.2	013.8	013.7	013.5	013.5	013.6	013.5	013.6	013.3	013.4	013.5	013·8	013.7	013.3	013.3	013.2	012.9	012.0	012.0	013.3	013.4	012.8	3012.4	1013
	25	011.0	011.1	010.6	010.1	010.3	010.7	010.9	0.110	011.3	011.6	012.0	012.4	012.8	012.8	013.0	013.1	013.5	013.7	013.8	014.0	014.8	014.0	014.0	014.8	3012
1							'				1		'	l				,	-5 /	-3					17	1
	26	015.0	014.9	014.9	014.9	015.2	015.5	015.9	016.1	016.3	016.7	017:4	017.7	017.9	018.1	018.0	018.0	018∙1	017.9	018.0	018.2	018.3	018-1	017.0	017.	8016
	27	016.8	015.7	014.9	014.1	013.4	013.0	013.0	012.6	012.5	012.6	012.5	012.1	011.5	011.2	010.2	010.1	009.2	008.5	008.0	007.7	007.7	007.0	006	1005.8	богт
	28	005.5	005.1	001.3	004.1	003.7	003.0	004.0	004.2	004.3	004.6	005·0	005.2	005.4	005.6	005.7	005.7	005.7	005.9	006.0	006.2	006.5	006.5	006.	006.6	005
	29	006.1	006.2	006.1	006.1	006.0	006.0	006.1	005.9	005.7	005.1	004.8	004.2	003.3	002.3	002.4	002.8	003.1	003.3	003.5	004.1	004.5	004.5	004	004.1	1004
1	30	003.6	003.1	002.7	002.2	001.6	001.4	000.8	000.2	000.0	998.3	997·I	996.8	996.4	995.9	995.8	995.9	996.1	996.7	997.0	997.2	997.9	997.9	997.8	997	1008
	Ĭ			<u>'</u>			'	ŀ	1	i	آ' 'ا				,,,,		,,,,		,	/	,		, -	1	1337	1
\downarrow	31	997.2	996.4	995.5	995.0	994.2	993.8	993.7	993.3	992.9	992.8	992.6	992.7	992.7	993.0	993.5	994.0	994.7	995.4	996.2	99 7·o	998.1	998.7	999.5	000.2	995
Iean		1014	1014	TOTA	1012	1012	1013	TOTA			1012	TOT 4	TOTA	TOTA	TOTA	TOTA	TOTA	TOTS	1012	TOLA	TOTA	TOTA	TOTA	TOT	TOT	1
							1013	1013	1014	1014	1013	1014	1014	1014	1014	1013	1013	1013	1013	1014	1014	1014	1014	1014	1014	
Station :				131		·87							.03													<u> </u>
ean										1015	1015	1015	1015	1015	1015	1015	1015	1015	1015	1015	1015	1010				
ea leve	1)	-51	.14	.78	.63	52	.56	·6o]	.67	.66	.62	•65	•66	.64	1 .05	1 .00	1 .00	1 .28	1 .02	•73	·85	.10	•22	.16	oc 0c) '

292.	Cahir	civee	n (Va	alenci	ia Ob	serva	tory)	: H	b=1	3.7	metr	es.												Augu	st, 1	923.
<u></u>		mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.		mb.		mb.	mb.	mb.	mb.	mb.
1	I	001.0	001.5	001.9	002.1	002.7	003.3	003.9	004.7	005.3	005.4	005.8	006.0	006.2	006.4	006.5	006.2	006.1	006.0	005.5	004.7	004.0	002.9	002.0	999.7	004 • 2
1	2	995.0	992.8	989.7	986.9	983.2	981 6	979.4	978·o	978.1	978.7	1981.1	985.8	990.3	994.5	997.4	999.5	001.2	002.6	004.2	005.8	007.3	008.2	000.1	009.7	/ 1993 ⋅ 2
-	3	010.7	011.2	011.9	012.7	013.5	014.3	015.1	016.3	016.8	017.5	018-4	019.0	019.7	020.6	020.9	021.1	021.6	021.9	022.2	022.3	022.2	022.7	022.5	022.5	018.0
	4	022.4	021.7	021.1	020.4	020.7	020.2	019.9	019.4	019.3	018.8	3 018·5	018.1	017.4	017.0	o16·8	016.1	015.2	014.4	013.6	012.9	012.5	012.0	011.0	010.4	017.3
	5	009.4	008.8	008.7	008.8	008.9	009.6	010.1	010.5	011.3	011.5	012.0	012.5	012.7	013.2	013.2	013.7	013.8	013.7	014.0	014.2	015.2	014.9	014.6	014.3	012.0
																										011.8
ĺ	7	009.3	008.7	007.8	007.8	008.0	008.4	009.2	010.0	011.5	011.7	012.2	012.0	012.8	012.8	013.0	012.9	012.8	012.8	012.8	012.0	012.6	012.3	012.0	012.1	011 1
	8	011.8	011.2	011.3	010.0	010.6	010.9	010.7	010.2	010.7	010.6	010.4	010.2	010.0	010.0	010.8	011.0	011.1	011.0	011.7	012.1	012.5	011.7	012.1	012.3	011 • 2
	9	012.5	012.6	012.8	013.4	013.0	014.2	015.0	015.8	010.0	010.6	017.4	017.7	018.0	018.4	018.4	018.7	019.1	019.0	019.8	020.4	021.0	021.4	021.4	021.3	017.1
	10	021.4	021.7	021.3	021.6	022.0	022.2	022.5	023.1	023.0	023.0	024.3	024.2	024.3	024.0	024.0	023.9	023.9	023.9	024.0	024.1	024.0	024.2	024.2	024.3	023.3
1																										022.3
																										016.5
,e																										018.0
ē																										023 · 1
Station Level	15	025.1	025.0	024.9	025.0	025.0	025.3	025.6	026.1	026.4	026.0	026.8	026.6	026.8	026.4	026.5	026.5	020.0	020.7	020.0	020.6	020.7	026.7	026.4	026.4	026 · 1
Ю	16	026.3	025.8	3025.2	024.0	024.6	024.4	024.4	023.0	023.6	022.8	3022.6	021.7	021.3	020.2	019.5	018.4	017.8	016.2	015.7	014.4	013.5	012.3	010.7	000.5	020.3
. .	17	008.4	008.0	007.6	007.3	3006.8	3006.3	006-4	006.4	006.4	006.2	006.4	006.5	006.2	006.4	006.4	006.2	005.9	005.8	005.7	005.8	006.0	005.9	005.7	005.5	006 · 5
ţ,	18	005.3	005.1	004.9	004.8	3 004.0	005 1	005.8	006.3	007.0	007.4	1007.9	008.7	009:5	009.9	010.7	011.3	011.0	012.2	012.9	013.4	014.1	014.3	014.4	014.3	1.000
Ś	10	014.2	014.4	014.0	014.2	014.0	014.3	014.6	014.8	015.1	014.8	014.3	014.7	014.4	014.1	013.7	013.2	012.7	011.7	011.1	010.4	010.4	010.5	010.3	010.0	013.4
	20	009.7	009.5	009.1	008∙€	008.8	008.7	009 2	008.9	008.8	008.0	007.8	006.9	005.3	003.8	002.9	001.9	001.0	000.0	999.5	998.5	997.6	996.4	994.9	993.3	004 · 5
1	21	994.4	994.7	995.8	996.3	997.0	998.2	999.1	999.8	000.4	000.8	8000.8	001.0	000.0	001.0	001.1	000.8	000.6	000.8	000.9	001.7	002 0	002.5	003.0	003.3	999 • 7
- 1	22	003:4	003.7	004.1	004.4	004.9	005.5	006.2	006.8	007.8	008-2	: oo8·8	009.2	009.5	009.7	010.1	010.1	010.3	010.1	010.1	0.010	010.1	009.7	000.3	008.2	007.8
- 1	23	007.0	005.8	004.0	001.5	999.2	996.9	994.0	992.7	992.7	993.5	993.7	993.8	993.7	993.6	992.7	992.4	991.9	991.5	991.3	991.0	991.1	991.6	992.6	993.7	995.4
	24	995.0	996.4	1997.6	998.5	000.0	001.5	002.9	004.9	006.7	008·c	008.7	009.9	011.5	012.8	013.6	014.6	015.5	016.0	016.4	016.8	017.0	016.4	016-1	016.0	008.4
	25	015.5	015.1	014.3	013.6	012.4	011.0	009.5	009.1	008.6	007.4	006.4	005.8	005.2	005.1	005.0	004.6	004.7	004.7	004·0	003.9	003.8	003∙8	∞3.1	002.9	007 · 8
	26	002.5	001.7	001.3	000.7	000 • 2	000.1	999.8	999-6	999.5	999+5	999.2	999.0	999.0	998.9	999:2	999.2	999•4	999 [.] 4	999.7	999.8	999.9	00012	000.1	999.7	000.0
1	27	999.7	999.5	999.5	998.9	998.7	998.5	998-6	998.3	998.5	998.5	998.2	998.7	999.5	000.1	001.0	002.0	002.8	003.7	004.5	005.4	ооб∙о	006.2	007.0	007.4	001 · 1
	28	007.8	008.0	008.2	008.2	008.4	008.9	009.0	009.5	010.2	010.4	010.6	010.0	0.110	011.0	011.0	011.2	010.8	010.5	010.3	0.010	009.4	008.3	006.9	006.2	00015
1	20	004.4	002:3	3 999-8	997.8	995-6	992.9	992.0	992.1	993.0	994.2	996.2	998.0	999.5	001.4	003.5	004.9	006.3	007.4	008.5	009.9	010.9	011.3	011.8	012.2	001·8
	30	012.3	012.2	012.4	012.5	012.5	012.8	013.5	013.5	013.8	013.8	013.9	014.0	014.0	014.1	014.0	013.8	013.8	013.7	013.6	013.8	014.0	014.0	013.7	013.4	013.4
\downarrow	31	013.2	013.1	012.9	012.6	012.6	012.7	012.9	013.1	013.4	013.5	013.6	013.7	013.7	013.8	013.8	013.9	014.0	014.3	014.4	014.6	015.3	015.4	015.6	015.8	013.8
Mean		1010			1009	1009	1009	1000	1009	1010	1010	1010	1010	1011	1011	1011	1011	1011	1011	1011	1011	1011	1011	1011	1011	1010
(Station	n level)	.70	.38	01.	82	.62	-60	-66	∙83	1.17	.32	-60	-90	.16	.41	.59	.62	•69	∙68	.75	∙87	.99	∙86	.67	.46	-89
Mean		1012	1012	1101	1101	1101	1011	1011	1011	1101	1011	1012	1012	1012	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1012
(Sea lev		•36				.28	·26	.32	.48									.34		.40		-64	.51			
G.M.T.		Ι,	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
Not	E.—Wh	en pr	essure	e exce	eds 1	000 1	nb. th	e lead	ling f	gure	ı is n	ot pri	nted.	i.e., 1	001.7	mb. i	s wri	tten o	001 · 7.	Thi	s rule	does	not,	howe	ver,	l apply

Note.—When pressure exceeds 1000 mb. the leading figure 1 is not printed, i.e., 1001.7 mb. is written 001.7. This rule does not, however, apply to monthly means.

Readings in millibars at exact hours, Greenwich Mean Time.

293. Cahirciveen (Valencia Observatory): H_b (height of barometer cistern above M.S.L.) = 13.7 metres.

September, 1923.

Day		I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
A		mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.
	1	015.9	015.8																							018.9
	2	023.6	023.7	023.8	023.9	024.3	024.7	025.2	025.6	026.2	026.3	026.6	026.7	027.1	027.2	026.9	026.9	026.9	027.0	027.1	027.6	027.9	027.5	027.4	027.1	026 • 1
	3	026.5	026.1	025.6	025.6	025.0	024.5	024.3	024.1	024.0	023.7	022.8	022.6	022.0	021.6	020.7	019.9	019.2	018∙8	018∙6	o18·7	018.6	018∙0	017.8	or8∙o	022 · I
	4	019.4	019.9	020.6	021.3	021.8	022.8	023.4	024.1	025.5	025.5	026.2	026.4	026.9	027.1	027:3	027.4	027.5	027.5	027.6	027.8	028-2	028.2	028-2	028.2	025 · 2
	5	028∙0	028.0	027.8	027.8	027.6	027.8	027:9	028.3	028-8	028.9	028.9	029.4	029:4	029.0	028.9	028.9	028-5	028.5	028.7	028.7	028.8	028.7	028.7	028.5	028 · 5
	_								_		_	1										'		0		
																										025.5
																										026 · 6
	8	027.0	027.0	020.5	020.1	025.8	025.8	025.0	025.7	025.4	025.2	024.9	024.8	024.4	024.2	023.3	022.7	021.9	021.5	021.0	021.0	021.0	020.0	020.3	019.9	024.0
1	9	010.0	019.3	017.4	010.0	010.5	010.2	010.7	010.0	010.2	010.7	010.7	010.5	010.4	010.4	010.2	010.2	010.5	010.7	010.7	017.4	017.7	010.0	019.1	010.2	017.1
	10	010.5	010.5	010.2	019.4	018.4	018.9	019.4	019.9	020.3	020.9	020.7	020.7	020.5	020.4	020.1	019.9	020.1	02013	020.5	021.0	021.2	021.2	021.2	020.9	019.9
	11	020.7	020.2	οτο-8	010.3	010.3	018-8	018-7	018.5	018.3	018.2	017.7	017.4	οτάνο	016-7	015.0	015.5	015.0	014.7	014.4	014.5	014.1	013.7	013.5	012.8	016-2
	12	013.0	011.6	011.2	010.8	010.2	010.6	010.8	011.3	011.3	010 2	010.0	010.0	011.1	010.8	010.6	010.6	010.6	010.1	0.010	0.0.0	8.000	000.1	008.8	008.0	010.6
, e	13	007:4	006.6	005.5	004:0	003.8	003.3	003.3	001.4	000.8	000.0	000.7	000.4	000.0	008.5	008.0	000.0	000.5	000.7	000.0	000.3	000.4	000.1	000.4	000.3	001.2
e é																										000.9
H																										006.9
Station Level	-3	203 2	203 2	200	005 2	1003 4	304 1		305	ر دی	4	00, 1	50, 3	55, 3	30, 0	00, 9		JJJ 7		-				5		
ij	16	011.6	011.6	012.0	012.4	012.8	013.2	013.9	014.3	014.5	014.6	014.8	014.7	014.7	014.6	014.3	014.1	013.2	012.6	012.1	011.0	010.9	010.0	008.9	007:3	012.8
ल																										994.5
∞	18	995.2	995.5	996∙0	996.4	996.7	997.3	998.2	998.8	999.5	000.5	001.2	002·I	003.0	003.7	004.6	004.9	005.4	005.9	006.5	007.3	007.9	008.3	008.4	008.5	001.0
1	19	008.5	008.4	008.2	008.4	008.3	008.2	008.7	∞8∙9	009.0	009.0	008.9	009.3	009.4	009.3	009.1	009.1	009.2	009.2	009.4	009.9	010-2	010.3	010.4	010.7	009 1
1	20	010.9	010.0	011.1	011.1	011.1	011.6	012.0	012.7	013.4	013.4	013.6	012.9	013.2	012.9	011.2	009.5	007:4	005.9	005.0	005.1	004.9	∞4.7	∞4∙9	005∙0	009.9
			_			l					_				_						_	_			1	
ı																										006.2
	22	∞3.8	002.9	002.1	001.8	000.9	000.7	000.6	000.3	000.1	999.9	999.2	998-6	997.7	997:3	996.5	995.6	994'7	994.3	993.6	992.4	991.2	990.8	990.2	989.6	997.6
	23	990.0	990.6	991.8	993.4	994.6	996.3	997:3	998∙1	998.9	000.0	000.0	001.8	002.6	003.1	003.4	004.4	004.8	005.2	000.0	006.2	000.6	000.0	000.0	000.8	000.3
1	24	006.4	006.5	005.2	004.4	003.3	003.1	002.5	001.4	000.4	999:4	997:7	990.1	993.4	991.5	989.4	986.8	987.5	987.7	987·5	987.6	987.1	986.4	985.9	985.0	995.6
Ì	25	985.9	986.2	986.4	987.2	988.3	989.7	991.4	992.2	993.0	994.2	995.9	997:3	998.6	000.0	001.3	003.0	004.4	005.8	000.9	008.2	008.9	009.6	010.0	011.2	997.6
	26	017.8	01214	012.7	012.1	012.5	014:3	OT 4 · 7	07.5.0	015.5	015.5	015.8	07.5.7	015.8	016.0	016.6	016.2	016.2	016.4	016.3	016.5	016.3	015.0	015.7	015.3	015.1
																										014.5
																										022.0
1																										025.3
. ↓																										020 4
· · · · · · · · · · · · · · · · · · ·	J-				/																					
Mean		1012	1012	1012	1012	1012	1012	1012	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013
(Station		•99					∙68	.91																		
Mean		1014	1014	1014	1014		1014								1015	1014	1014	1014	1014	1014	1015	1015	1015	1014	1014	1014
(Sea leve		•66					•35										.74							•92		.77

294. Cahirciveen (Valencia Observatory) : $H_b=13\cdot7$ metres.

October, 1923.

		mb.											mb.										mb.		mb.	
A	I	019.1	o18·9	018.9	019.3	019.7	020.2	020.9	021.3	022.1	022.4	022.5	022.9	023.0	023.1	023.0	023.1	023.1	023.1	023.3	022.9	022.8	022.5	022.1	021.6	021.7
1																										019.7
	3	009.5	007.5	006.7	007.0	000	011.0	012.4	013.2	012.3	015.9	016.3	017.2	017.9	018∙4	019.1	019.4	019.8	020.3	020.8	021 .4	021.9	022.4	022.7	022.9	016.0
	4	023.2	023.5	023.5	023.6	023.6	023.9	024.1	024.2	024.5	024.4	024.3	024.1	023.7	022.9	022.4	021.8	020.9	020.4	020.2	019.0	019.0	017.0	017.2	015.7	022 2
	5	014.8	013.4	012.5	011.0	0.110	010.3	010.0	010.9	011.3	011.5	011.0	011.8	011.7	011.8	012.1	012.2	012.5	012.9	013.2	013.7	013.9	014.2	014.2	014.2	012.5
	_			l								6							6					07.5.4	075.5	074.8
	6	014.3	014.2	013.9	013.0	013.0	013.7	013.0	013.9	014.3	014.4	014.0	014.9	015.1	015.1	015.3	015.1	015.4	015.0	015.0	015.0	015.9	015.7	015.4	015 5	014.8
	7	015.0	014.8	014.4	014.0	013.3	012.0	012.1	011.0	011.5	011.3	011.2	010.9	010.7	010.2	009.9	019.5	009.0	009.8	010.1	010.5	010.0	011.0	005:4	005:4	000.2
	8	012.0	011.9	011.7	012.0	008.0	000:4	012.3	012.7	012.1	011.9	011.1	010.3	009.1	007.6	0071	000.0	000.3	005.0	005.0	005.0	005 4	015.7	015:3	015.1	009·2 012·5
	9	005.7	000-2	007 2	012.5	012.4	011.7	010.8	011 3	000.8	008.0	008.4	008.8	000.0	000.6	010.7	015 4	010.5	015.7	013.0	010.8	011.3	011.0	011.2	011.5	011.1
I	10	014.7	013.0	013.2	012 3	012 4	011 /	0100		009 0	000 9	4	000 0	009 0	009 0	010 /	010 0	010 3	010 /	011 0	0.00	011 2		J J	3	
- 1	11	011.0	011.6	011.7	011.6	OTT-8	011.6	011.7	012.1	012.2	012.0	011.7	OTT 5	0.11.0	010.5	0.010	000.3	000.0	008.8	008∙1	007.2	006.5	005.8	004.9	003.9	0.010
ì	12	002.4	001.3	000.0	000.0	998.3	997.5	997.0	996.8	997.2	997.4	998.1	998.4	998.2	998.2	998.4	998.4	998.3	998.6	998.6	998.6	998.6	998.5	998.5	998.7	998.7
1	13	000.0	000.0	000.3	999.6	999.9	000.3	000.7	001.4	002.1	002.6	003.0	003.3	003.6	003.6	003.0	004.1	004.3	004.5	004.7	004.8	005.0	005.3	005.4	005.6	002.6
e.	14	005.2	005.7	005.9	006.1	006.3	006.5	006.9	007.5	008.1	008.5	000.1	000.6	009.8	0.010	010.3	010.4	010.7	011.2	011.7	012.1	012.5	013.0	013.4	013.3	009.2
ev	15	013.6	013.6	013.5	013.7	013.8	013.8	014.1	014.8	015.0	015.2	015.3	015.3	015.2	014.9	014.9	014.8	015.0	015.1	015.3	015.6	015.6	015.6	015.7	015.7	014.7
Station Level		1			1	1	i		ł		ŀ	I	1 1						1	1				1	Į.	l i
g	16	015.6	015.7	015.3	015.4	015.5	015.6	015.8	016.5	017.1	017.4	018.0	018.3	018∙3	018·4	o18·5	018∙8	019.0	019.4	020.1	020.4	020.6	020.8	021.0	021.5	017.9
.0	17	021.2	021.3	021.1	021.0	021.2	021.3	021.5	022.0	022.3	022.3	021.9	021.7	021.4	021.0	020.6	020.3	019.8	019.7	019.4	018.0	018.3	019.1	017.4	010.5	020.5
at .	18	015.1	014.2	013.1	011.0	0.110	0009.8	000.1	008.5	007.6	006.0	006.3	005.8	004.9	004.0	003.3	002·I	001.2	999.9	998.3	996.8	994.3	99I ·8	989.8	1907.0	004.5
<u> </u>	IQ	991.7	993.8	995.8	997·I	998-5	999.6	000.8	002.0	003.1	003.5	003.9	003.9	003.9	003.9	004.0	004.0	003.9	003.9	003.9	003.2	003.4	002.9	002.2	001.7	1001.2
1	20	001.0	000.3	999.3	998.2	997.3	996.5	995.9	995.2	994.3	992.8	992.0	990.6	988.8	987.2	985.3	983.2	981∙1	981.7	980.7	979.1	978.8	979.3	979:4	979.9	989.5
			_	٠ .				0.5	0.5		_	1			_	٠ .				. 00	-00 -	-00 -	000.0	00.0	088.0	086.5
1	21	980.9	981.9	982.6	983.7	984.8	985.6	986.1	1986.6	987.1	987.2	987.3	987.5	987.4	987·5	987.6	987.7	987.9	988.0	988.4	988.5	988.7	989.0	082.0	085.6	986.5
	22	989.2	988.9	988.8	988.8	988.9	989.8	990.4	991.4	992.3	992.5	992.7	992.9	992.7	992.6	992.2	992.0	991.7	991.6	991.0	990.1	989.2	900.3	907.0	074.6	990.5
	23	983.0	981.1	978.6	975.7	975.1	975.0	975.8	970.4	977.0	977.2	977.2	977.1	970.8	970.5	976.1	975.0	975.8	975.5	975.2	975.1	975.1	078.0	078.0	070.8	976.7
	24	974.4	974.0	974.0	974.0	974.3	974.2	974.2	974.3	975.3	974.8	974.0	974.5	974.0	974.7	974.7	974.0	975.3	970.0	970.7	087.0	086.6	086.2	085.6	085.0	975.4
	25	900.3	900.0	901.4	961-7	1902.0	903.9	904.4	905.3	900.1	900.9	907.4	907.0	907.9	900.2	900.4	900.2	988.0	967.7	987.0	907.2	900 0	900 2	9050	303 -	985.5
	26	084.5	082.4	082.7	082.2	082.2	082.2	084.5	08=.6	086.5	086.2	086.6	085.0	084.4	082.7	08010	076.5	072.6	070:0	070.1	070.0	070.4	070.2	970.2	970.1	979.6
- 1	27	904.2	068.0	068.2	067.5	066.8	965.0	063.8	062.4	067.8	062.0	062.6	905.9	065.8	067.2	068.4	068.8	060.0	070.3	073.7	076.6	978.7	980.2	980.9	982.2	969·1
1.	28	083.0	085.1	086.5	088.2	989.8	901.4	992.8	004.4	005:0	006.2	007:0	008.8	903.4	907.3	000.8	001.2	002.3	003.0	003.8	003.0	004.3	004.3	004.0	003.9	996.7
	29	003.6	002.0	002.4	001.6	001.1	000.1	999.7	999.6	990.6	990 /	000.6	000.5	000.6	000.5	000.7	000.8	000.0	999.9	999.8	999.3	999.1	998.1	997.4	997:3	000.1
	30	997.2	998.3	998.8	999.1	999.8	000.4	001.3	002.4	003.6	004.0	004.6	005.3	005.8	006.2	006.7	007.3	007.9	008.7	009.7	010.7	011.2	011.9	012.7	013.3	005.0
ĺ					1		1	1		1	l		1	l	1		1		1	1	İ		1		l	
\	31	013.9	014.6	014.9	015.5	016.1	016.7	017.4	018-1	019.3	019.7	020.2	020-1	020-1	020.2	020.5	020.7	020.9	021.2	021.6	021.7	021.9	021.8	021.4	021.2	019.0
			ļ		-\								l			l				·						
Mean		1002	1002	1002	1002	1002	1002	1002	1003	1003	1003	1004	1004	1004	1003	1003	1003	1003	1003	1003	1003	1003	1003	1003	1002	1003
(Statio	n level)	·81	l .ei	1 .43	.99	•50	1 .00	•93	•33	۱ • 7 8	¹ •8 ₇	¹ ∙o3	J •14	•07	96∙ ا	J ∙89	-65	1 .52	.57	1 .70	1 .00	1 .00	1 '44	•22	1 '95	30
Mean		1004	1004	1004	1003	1004	1004	1004	1004	1005	1005	1005	1005	1005	1005	1005	1005	1005	1005	1005	1005	1005	1005	1004	1004	1005
(Sea le	vel)	•46	•26	•08	.98	15	.31	•58	.98	'43	.52	.ĕ8	.79	.72		•54		•17		•35	.31	.25	.09	-87	•60	.01
<u> </u>								 -						ļ		<u> </u>										Mean
G.M.T.		ı.	2.	3.	4.	5.	6,	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
				<u> </u>	<u> </u>	<u> </u>	<u> </u>	l				<u> </u>		<u> </u>	<u> </u>	l	l .			<u> </u>	<u> </u>			<u> </u>		

Note.—When pressure exceeds 1000 mb. the leading figure 1 is not printed, i.e., 1001.7 mb. is written 001.7. This rule does not, however, apply to monthly means.

Readings in millibars at exact hours, Greenwich Mean Time.

295, Cahirciveen (Valencia Observatory): H_b (height of barometer cistern above M.S.L.) = 13.7 metres.

November, 1923.

Day.		ı.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	M
		- la 1	1-	l mala	Lanh	l mb	l mb	l mb	l mb	 mb	l mb	l mb	mb.	mb	mb	mb	l mb	mb	mb	mb	mb.	mb	mb.	mb.	l mb.	l In
人 .	. In	nb.	mb.	mb.	mb.	IIID.	IIID.	1110.	1110.	1110.	018.8	1110.	017.5	016.5	016:4	017:0	017:4	017:7	018.2	018.6	018.0	010.2	019.7	019.7	020.1	01
$T = \frac{1}{2}$	0.	1.4	021.1	020.0	020.4	020.1	019.0	019.0	019.5	019 4	018.4	017.5	017.1	016.1	015.5	015.7	015.6	015.7	015.6	015.6	015.7	oı ´ 5∙8	015.4	014.8	014.6	0
1 3	. [0]	2.8	OT2.5	OTO.E	012.0	OTTO	10TO-8	010.2	looo.X	looo•6	$1000 \cdot 0$	noro-t	1010.7	1010.7	oii.i	1011.51	011.7	o_{11}	012'4	013.0	013 2	013.2	013.0	013.0	0.5.0	10.
3		- 2 - 0	222	0126	012.5	1012.6	012.7	012.7	012.0	014.2	0.13	JUL 3 . C	NOT 2 · 51	O. C. TOI	012.0	1012.4	1011.7	011.4	011.0	010.7	010.2	010.1	000.1	000.7	100/4	., 0
1 4	0,	3.9	013.0	013.0	013.3	013	003.6	003.3	002.3	002:4	003.3	003.4	002.1	001.6	001.6	001.5	001.7	00I · 0	002.1	002.7	002.9	003.5	003.7	003.9	004.1	o
:		- 1			1	i		ł .	l	1	1	1	1 1							1					1	
1 6	.	4.6	005.2	005:6	006.6	007.5	008.3	000.2	010.7	012.2	012.8	013.0	014.4	014.8	015.1	015.8	016.0	016.4	017.6	017.4	017.3	017:5	017:3	016.7	016.4	o:
	- lo:	·6. +	015.0	015.6	OT 2 . 2	1015.3	OTEVE	015.6	015.7	1015.7	015:0	10TA - 5	1013.3	012.2	011.1	10000.01	0000.1	007'4	007.2	007.0	000.0	007.0	007.4	007.7	OOO.T	ĮV.
	≥ too	اد. ۹	008.4	008.7	008.7	1008.7	1008 <i>-</i> 8	വഹവംവ	1008.7	1.000	1008.3	:l007-8	10000 • 0	005:91	005.5	1005:2	004.9	004.0	005.3	005 4	000.1	000.0	000.7	000.7	1000.7	ĮΨ
		S. 21	006.0	006.8	006.2	loof. T	1005.6	005.5	1005.0	00001	0.000	1007.3	1007:0	OO8*41	008.8	1009:41	000.71	010.9	012.7	01315	014 3	014.2	טואיט	017.0	019.1	lo
10		10.4	021.3	022.7	023.2	024.2	025.4	026.0	028.2	028.6	028.7	029.2	029.5	029.9	029.8	029.7	029.6	030.0	030.3	030.4	030.8	030.8	030.7	030 6	030.6	0:
	1	- 1			1		1		i		i	1	1 1			1	- 1									1
T:	1 0:	ю.т	020.0	020.6	020-1	029.0	028.6	028.2	028.1	028.1	027.7	027.7	026.9	026.0	024.9	024.1	023.8	023.0	022.6	022.2	021.8	021.8	020.8	o19·8	019-2	0:
1		01	0.0	017.6	016.7	0.76.0	JOYE.E	OTAIT	OTAGE	012.7	012.2	1012.0	IOTT:XI	ดาดาชเ	0.000	000.41	000.01	ooo o	007.0	000.01	000.01	005.2	003"/	002.0	001.7	IV.
ම <u>ව</u>	. 100	NO. T	008.0	007:0	006.7	006.0	1004.8	002.7	002.6	1001.7	000.7	1080-3	loss.ol	980151	904 9	903.01	003.0	902.5	902.3	902.0	903.0	904 2	9051	900-7	900.4	19
e r	109	20.2	റ8റംറ	000.4	001.5	1002:0	1002.5	0.00	005:0	1005:0	QQD+7	1000.0	1007:31	997.41	990.0	990.31	990.41	990.0	990.0	990.0	9901	990.0	997.1	995.0	1995 0	יכוי
Level	go	1.3	987.9	984.1	980.8	979.7	979.8	980.3	980.7	980.8	979.7	980∙0	979.9	980.2	981.2	982.9	984.8	986.5	988.4	989.9	991.1	991.9	993.3	993.9	995.3	19
					ł		1	1				1	; I		i		1			1					l	
5 10	5 90	96.1	996.3	996.8	997.2	997.6	998.1	999.1	999.6	000.4	000.8	001.0	001.1	000.4	999.6	998.3	996.7	996.5	996.0	995.4	995.7	995.6	995.2	990·I	996.8	9
H H	- 100	اء ، ہ	006.8	007.4	1007.8	1000.6	loon•ol	002:4	003:5	004.5	006.2	1007.2	1007.8	007.0	007:0	008.1	008151	008·5	002.0	000.9	000.3	000.2	007.0	007.0	1000.0	v
Station	3 100	\~.=l	00714	1.800	000.2	000.5	$ \alpha \cdot \alpha - \alpha $	loto ol	OTO:T	1.010	0.000	10000.0	10009:41	009:51	000151	000.0	000.0	009.1	009.4	009.9	OTOLI	010.3	010.4	010-4	010.3	ľ
∞ 16	· •	1	010.0	010.2	010.2	OTOT	0.00	010.3	0.110	011.7	012:0	012.2	012.7	012:21	012:11	012.2	012.0	012·8	013.2	1013.2	013.0	014.0	014.0	013.0	013.0	V.
20	01	13.1	012.8	012.4	012.1	011.0	011.3	0.110	010.9	010.8	010.4	010.0	009:4	008.7	008.7	008.7	008.9	008.5	008.8	008.4	008.4	008.5	000.3	007.9	007.0	ľ
										0 -	0 -	0 -		~~=		206.8	206.0	007.0	007.3	00712	007.2	007.2	007.5	007.6	007.6	L
2	1 00	7.8	007.5	007.3	007.2	007.1	007.3	007.0	007.9	008.0	008.2	000.2	007.6	007.5	007.1	000.0	000.4	0070	010.8	007.2	010:0	011.0	011.1	011.1	010.8	ľ
22	5 00	7.8	007.9	008.0	008.3	008.6	008.9	009.1	009.8	010.4	010.5	010.0	010·5 013·6	010.2	010.2	010.3	010.4	010.5	015.5	016.0	016.4	017.1	017.6	018.1	018.7	0
2	3 01	0.0	010.8	010.0	010.9	010.9	011.1	011.5	011.9	012.0	012.9	013.3	022.9	023.7	022.6	013 9	022.7	022.8	023.1	023.1	023.5	023.2	023.1	023.1	023.0	0
24	01	8.9	019.1	019.0	019.9	020.0	020.4	020.0	021.5	022.2	022.4	078.8	017.9	016.8	015.0	015.0	014.1	013.3	012.7	011.8	011.0	010.2	000.4	000.1	008.2	6
2	5 02	2.0	022.2	021.8	021.3	021.0	020.5	020.3	019.7	019.0	010.9	010.0	01/9	010 0	015 9	015 0	014 1	0133	012 /	011 0	022	J	1	, -		1
1 0	; _c ,		007.0	006.5	005.5	00510	004.4	004:0	002·8	003.7	002.6	003.4	002.7	002.7	002.3	002.0	001.0	002.0	002.1	002.1	002.1	002.0	001.0	002.0	001.0	o
20	, 100		00 T	COTIL	OOTIT	OO T .O	$ \alpha \alpha \alpha \cdot \lambda $	000.71	റ∩∩∙XI	OOI •31	വാം	1002.4	1002 • 2	002.01	001.0	1002.0	1002.2	002.4	1002.9	003.7	1003.4	003.7	004 2	004 4	1004 0	"IV
27	l oc		004.0	002:01	വവാ എ	002.61	002.4	002·21	വാംപ	UU3 - D	บบ з ∙ b	1003.0	1002 °Q	002.41	001.0	1001.0	0021	002-4	003.4	003.7	1003.0	004 2	004 5	0050	∞ 5 5	ıv
1	٠ I		~~ ~ !	006.01	006.4	006.6	007.01	വെ ജ പ	റവ്യാപ്പ	$ \alpha \alpha \alpha \cdot \alpha $	$\alpha\alpha\alpha\cdot X$	Into:s	OTO: O	വസ്	011.3	orr o	1012.0	013.3	1014.2	1014'0	017.7	010.0	0174	017.0	1010.7	IV.
30	, 00	2 4	005.4	010.2	010.3	010.5	010.5	010.7	020.0	020.1	010.2	010.5	018.3	017:3	016.3	015.7	014.7	013.8	013.3	011.9	011.0	010.8	010.4	010.6	010.8	0
y 30		- 1		- 1		4																				1-
ın	10	00	1000	1000	1000	1000	1000	тооо	1000	1009	1000	1009	1009	1009	1008	1008	1008	1008	1009	1009	1009	1009	1009	1009	1009	10
ution lev	zel\ I	-681	.40	•36	-181	.18	.22	.35	-60	86	•78	1 .84	5.51	.13	. 707	10.		•02	1 .10	10	1 -25	42	41	42	1 .50	1_
n	(01)	001	491	1011	10)	10)		ارر		1011		'				Iroro	1010	zoro.	LOTO	Izoro	Izozo	TOTE	TOTT	TOLL	LTOIT	İ

296. Cahirciveen (Valencia Observatory): $H_b = 13.7$ metres.

December, 1923.

296	. Cahir	civee	n (V	alenc	ia Ol	bserva	atory) : F	$\mathbf{I}_b =$	13.7	met	res.											Dec	;emp	er, is	123.
		l to b	mb	l mb	Lmb	Lmb	l mb	lmb	l mb.	l mb.	l mb.	l mb.	l mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.		
*	_	mb.	mb.		1	1000	000.0	1000.0	1008.7	1008.8	1008.0	1007.1	1006.2	004.7	003.1	LOOT O	1000.3	laaa 7	1005.7	1992 • 9	laat •a	IOO4 · I	1.007.1	993.9	994.2	003.4
	_	!	001.1	004.0	LOO ALT	002.7	002.5	1002 - 5	1004.3	[004 • 4	1005-1	[[005:4	1000.2	1990-7	1997.0	1997.4	1990.4	1999'9	000.3	0.000	1, 100	1001.4	001.2	OOT 3	001.7	990.9
1																										
- 1	- 1		(laar a	1000 · T	1080.6	1088.0	1088.2	I0X7.7	けいおん・ん	IOX6 • 2	こうしょう	1083.5	1082 °Q	IOOT '8	100010	1000.4	979'7	1979.9	1900'2	1900.2	900.4	901.7	1902 3	90.5	002.0
	5	081.7	086.0	088.2	990.0	992.2	994.0	995.4	996.7	998.4	999.8	3001.2	002.9	004.0	005.1	006.3	007.6	009.0	010.2	011.7	012.7	013.9	014.6	015.1	015.8	001.7
1	-			1	1	1	1	1	i .	1		1	1			i	1		1	ĺ	i	1		t l	1	
.	6	016.3	016.5	016.6	016.7	016.9	017.2	016.9	017.0	017.3	017.1	016.5	015.8	015.0	013.3	012.4	011.4	009.9	008.5	007.0	005.8	004.6	003.1	001.4	999.9	012.2
		0 1		1	000 -		1000.5	000.4	IOOO I	10×0.0	IOXO · ·	IOXO • 7	1080.2	OXXX	വര്മ∙വ	ロのカフ・マ	1020.4	u05'0	1005.2	1405'4	140710	1909.0	991 1	1994 1	9910	1990 1
	ò	00.0	المما	005.2	1000.0	1006.7	1007.6	IOOX+5	1000.2	1000.5	1001.0	0002 • 2	1002.5	100219	1003.3	1004.4	1004 9	000.0	000.0	1007.0	1000.3	1009.1	1009 3	icog g	010 /	004.2
- 1				10.00.0	0.70.0	OTOT	OT 4.0	OT 4 .7	OT E . 2	IOTh I	1010.2	21017.0	מימוחו	010.2	юто.з	CHOG	1010.5	010.7	1010.4	1010. \	101/0	101/0	01/0	O1 / 1	O1 / 4	ור. כיי
- 1	10	017.2	016.9	017.0	017.1	017.0	017.0	017.2	017.5	018.1	018.3	3 018-8	018.8	018∙5	018.2	018.1	018.1	018.2	018.2	018.5	018.0	018.7	019.0	019.3	019.2	018.0
1				1	1	1	1	1	I .	1	[1				I				j .	}			1		
	11	018∙1	018-2	018.3	018.2	017.6	017.2	017.3	017.4	017.4	017.3	017.4	017.1	010.3	010.1	010.1	010.1	010.1	010.0	015.6	015 3	015.3	020.5	015.0	013.3	017.6
į	12																									
e	13		0	100-0	1005.0	1006.6	1000.	100×.5	1020.4	1020.0	1020.0	いつつエ・ク	O2 I . O	10.3 I .OI	()27.	() 42 '2	1032.2	0 12 0	1032 0	1077 1	1 U J J ~	(\sim, \sim, \sim, \sim)	I	I~.3.3 II	\circ	U3U 1
2	14	032.8	032.3	032.0	032.0	031.4	031.7	031.6	031.0	031.4	031.0	031.1	030.2	029.8	029.3	020.3	020.2	0201	027.8	022.8	023.6	029 0	029 9	032.2	030.8	030.5
	15	031.0	031.2	031.2	031.6	031.1	031.8	032.1	032.5	033.3	o33·4	o33·7	033.9	033.2	033.1	032.0	032.6	032.0	032 0	032 0	032	032 3	032 4	032 2	031 0	032.4
Station Level																										029.0
.9	16	031.4	031.4	031.0	030.3	1029.9	029.5	029.4	029.2	029.3	029.6	029.8	029.0	029.3	026.1	026.0	026.2	026.3	026.6	026.7	027.2	027.4	027.5	027.6	027.7	026.3
ıt.	17	026-1	025.7	025.4	025.3	025.0	025.0	025.0	025.7	020.3	020.0	020.8	020.7	020.1	020.8	020.0	020 2	020.3	030.7	030.0	031.0	031.2	031.8	031.5	031.8	026.3
, ;	18	027.5	027.3	027.6	027.6	027.7	027.7	028.2	028.0	029.2	029.5	030.2	030.0	029.9	029 0	029 9	033.0	034.7	035.3	035.8	036.0	036.4	036.0	037.4	038.0	029·5 033·7 030 ·5
0,	19	031.4	031.0	031.7	031.6	031.0	031.0	031.0	032.0	032.9	033.1	033.0	033.7	033.0	040:3	030.8	030.8	030.0	030.0	040.0	030.0	030.8	030.2	038.5	038.2	039.5
	20	038.5	038.4	038.7	038.8	039.0	039.0	039.0	039.5	040.5	040.3	1040.0	040.4	040 3	040 2	039 0	0390	039 9	-35 5		-37 7	-35 -	-35 -	3- 3	-3-	ا ت
									001.0	020.2	020.2	020.2	028.2	027.4	026.3	025.3	024.2	023.8	023.6	023.5	023.6	023.5	023.6	023.2	022.7	028.8
1																										
1			1	1 6	1	1 0	1 0	1~	0.76.7	Inth.X	OT TAKE	· I 🔾 T X · 🔾	iotx.	O L A . S	mioro	ww	1019.1	0190	019 /	019.7	O19 4		OIO 3	OT / / /	01/0	010.01
	24	015.7	014.7	014.2	013.9	013.2	012.0	012.4	012.0	0114	011.0	1010.8	000.2	008.0	006.8	006.2	005.8	005.4	005.5	005.5	005.7	005.9	006.2	006.0	006.3	010.3
	26	006.	007.0	006.8	006.0	007.2	007.5	007:0	008.2	008.0	008.5	7 008.7	008.3	007.4	006.7	005.7	005.0	004.7	005.1	005.2	005.9	006.5	006.9	007.6	007.9	006.9
		0 -	00	1 0 0	1~~0 0	المممال	1000.0	1000.7	100014	$10000 \cdot 1$	IOO A ' I	M(X)7.5		IOOZ O	10030	IOOZ L	1000	990 0	199/4	1994 /	1447 I	1991 9	994 /	1993 0	997	~~.n
ı	~0			1	0.00	10 * * . 0	1010.8	OT 4 1 4	OTh.I	1017.0	OIA *2	210110.3	1020.1	102014	1021 4	1022 4	1044 9	0430	044 0	024 9	1047 4	020 2	020.5	020 0	020 0	P . / 4
i			1 / 0	1 / /	1	16 -	1 6 - 7	1006.0	1025.5	102E - X	1025.	11025.2	1024.0	11.17.4.1	R)ZA·1	ICYZA U	11123	023.0	10230	1023.3	1022 0	U44 I	1040 0	040.0	DIG I	1V44 7
	29	027.0	020.0	016.1	020 5	015.0	016.0	016.6	017.3	017.8	018.	019.3	019.8	020 2	020.8	021 .5	022.3	023.1	023.8	024.2	025.1	025.2	025.7	025.6	026.3	020.3
				1		1		1		1	1										1			1 1		
	7 31	026.8	027.1	026.0	027.2	027.1	027.3	027.4	027.9	028.5	028.6	028.6	028.5	028.4	028.3	028.4	028.5	028.7	029.2	029.3	029.5	029.6	029.6	029.6	029.8	028.3
			1	1	1	1		.																		
Mean		1015	1015	1015	1015	1015	1015	1016	1016	1016	1016	1016	1016	1016	1016	1015	1015	1015	1015	1015	1015	1016	1016	1016	1016	1016
	ion level)	-60	-60	.73	.75	51 .78	31 −89	12	35	.71	1 .77	7 .90	1 .08	•37	1 .02	1 .02	1 '75	.70	75	1 73	1 .01	.02	.03	.07	•23	•07
Mean		1012	HOLZ	11017	11017	11017	11017	11017	11018	1018			1018	1018	1017	1017	1017	1017	1017	1017	017	1017	1017	1017	1017	
(Sea l		29						82	.05	.41	.47	√ .59	.37	•06	.74	.54	.44	.47	•44	.42	.50	.71	.72	.76	.92	.76
(Sed)	CVCIJ				44	-									<u>-</u> -		·									1.
G.M.	т .	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
					1			1		1	1	1	1	1	1	1	l			<u> </u>	!	1	<u> </u>			J
	VOTE.—W						m h +4	a los	ling f	aure	r ie n	ot pr	inted	i.e.	1001.	mb.	is w	ritten	001.7	7. Th	ais ru	le doe	s not	, how	ever,	apply
7	OTE.—W	nen p	ressu	re exc	eeas	1000 1	nd, to	ie ieac	mirg ii	Rais	ווכויו	or br		,	/		/··		,	-					•	•

Note.—When pressure exceeds 1000 mb, the leading figure 1 is not printed, s.e., 1001/ mb. is written to monthly means.

PRESSURE AT STATION LEVEL AND AT SEA LEVEL. ANNUAL MEANS OF HOURLY VALUES.

From readings in millibars at exact hours, Greenwich Mean Time.

297. Cahirciveen (Valencia Observatory) : $H_b = 13.7$ metres.

1923.

G.M.T	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.
Chation	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.
Station	011.77	011.57	011.40	011.26	011-21	011.32	011.48	011.68	011.95	011.98	012.09	012.06	011-95	011.84	011.76	011-67	011.68	011.76	011.86	011.99	012-15	012.11	012.04	011.98	011.78
Sea Level	013.45	013.25	013.08	012:94	012-89	013.00	013·16	013·36	013·52	013.65	013·76	013.73	013·62	013.21	013-43	013·34	013·35	013-43	013.53	013.66	013-83	013.79	013.72	013.66	013.45

PRESSURE AT STATION LEVEL: MONTHLY MEANS AND DIURNAL INEQUALITIES.

The departures from the mean of the day are adjusted for non-cyclic change.

298. Cahirciveen (Valencia Observatory): $H_b = 13.7$ metres.

1923.

	Month.	Mean.	Hour.	G.M.T. 2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.
	Tan.	mb.	mb. 0·26	mb. -0.26	mb. 0:31	mb. 0:33	mb. 0·44	mb. -0.44	mb. 0:35	mb. 0∙00	mb. +0·52	mb. +o·61	mb. +0.80	mb. +0·51	mb. +0·12	mb. -0·16	mb. -0·17	mb. -0·19	mb. -0·11	mb. +0.03	mb. +0.08	mb. +0·18	mb. +0·18	mb. +0.05	mb. -0.03	mb. -0.06
	Feb.	993.95 1013.65	+0.65	+0.28	+0.01	o·55	-0.84	-o⋅81	-o.8r	-0.71	-0·49	− 0·39	0.10	-0.04	-0.23	−0.35	-0.44	-0.10	-0.03	+0.26	+o·59	+0.74	+0.77	+0.92	+0.94	+o·85
	Apr. Mav	1003·83	-0·10	-0·25	-0·41	-0.36	–0·36 – 0·45	-0·14 -0·29	+o·o8 o·o9	+0·24 0·00	+0·42 +0·20	+0·36 +0·17	+0·35 +0·27	+0·33 +0·26	+0·24 +0·27	+0·20 +0·16	+0·10 +0·05	-0·16	-0·21 -0·29	-0·20 -0·35	-0·14 -0·26	-0.03 -0.06	+0·17 +0·35	+0·02 + 0·37	-0·07 +0·32	-0.08 +0.29
	June	1023·98	+0.03	—o∙18	-o·43	0 ⋅60	o·54	-0.43	−0·25	-0.0 7	+0.05	+0.07	+0.11	+0.20	+0.25	+0.23	+0.23	+0.06	0.05	-0. 06	–o·o5	+0.11	+0.38	+0.40	+0.34	+0.23
	Aug.	1014·17 1010·89 1013·11	+0.05	-0.29	-o·59	-0.90	-1.11	-1.16	-1.12	-0.96	-0.65	-0.52	-0.26	+0.02	+0.25	+0.49	+0.64	+0.65	十0.70	+0.67	十0.73	+0.81	+0.92	+0.77	+0.56	+0.32
1000	Oct.	1003.36	0.52	-0·73	-0.01	-1·01	–o·85	o·68	-0.42	-0.02	+0.43	+o·52	+0.67	+0.78	+0.71	+0.59	+0·52	+o·28	+0.15	+0.19	+0.32	+o·28	+0.22	+0.06	-0.17	-0.44
	Nov. Dec.	1009.33	-0.19	+0·02 -0·19	-0.00 -0.10	-0.09	-0·25 -0·08	0.00	-0·05 +0·20	+0.51 +0.41	+0.49 +0.49	+0·42 +0·78	+0·49 +0·88	+0.52	+0·30	-0.43 -0.04	-0·48 -0·27	-0·39	0·44 0·39	-0·15	-0·05 - 0·49	+0.04 -0.43	+0·22 -0·26	+0·22 -0·27	+0·25 -0·25	+0·34 -0·12
1	Year	1011.78	+0.03	-o·18	-o·35	-o·49	-0 ·54	-o·44	-o·28	-0.08	+0.10	+0.51	+0.32	+0.29	+0.12	+0.06	-0.02	-0.11	-0.11	0.03	+0.07	+0.30	+0.35	+0.31	+0.24	+0.17

ABSOLUTE EXTREMES OF PRESSURE AT STATION LEVEL FOR EACH DAY.

Maximum and minimum for the interval 0 h. to 24 h., Greenwich Mean Time.

299. Cahirciveen (Valencia Observatory) : $H_b = 13.7$ metres.

	Month	Ja	in.	F	eb.	М	ar.	Ap	ril	Ma	ay	Ju	ne	Ju	ly	Aı	ıg.	Se	pt.	0	ct.	N	o v .	D	ec.
	Day.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
Section of the sectio	1 2 3 4 5	017.0	997·2	mb. 018·8 012·7 016·3 019·5 011·6	011.7	mb. 997.7 989.5 017.2 021.9 018.4	986·9 988·5 013·9	020·1 019·3 007·3	017·9 005·1 005·4	mb. 019·6 020·2 018·6 017·2 012·9	017·4 017·2 012·9	027·3 026·4 021·9	024·4 021·8 019·1	018·1 010·3 014·7	007·0 009·7	009·7 022·8 022·5	977.9 009.7 010.4	027·I 028·3	018.0	021·6 022·9 024·5	012·4 006·2 015·7	mb. 021·2 020·6 014·6 014·3 007·4	014·6 009·6 007·4	001.6	mb. 991.0 993.4 992.4 979.7 983.5
	6 7 8 9 10	013·7 020·6 011·8 015·9	009.7	980·7 991·7 993·0 993·0	980.9	020·4 020·0 011·8	009·3 017·9 011·8 998·5	001·9 005·0 002·0 000·9	991·9 998·0 996·0	019.9	019·7 017·7 014·9 007·3	023·I 013·9 010·0 025·7	013·9 006·6 005·7 009·9	015·8 015·8 012·8 020·3	012·7 009·6 008·4 012·5	013·2 012·5 021·5 024·4	007·6 010·2 012·3 021·2	029·0 028·3 019·8 021·2	023·6 019·8 016·2 018·1	015·5 012·7 015·9 015·1	009·5 005·1 005·4 008·2	030·9 019·1 019·1	006·8 004·6 005·3 019·1	999·9 010·7 017·2 018·9	999·9 985·0 993·0 010·7 016·7
The second secon	11 12 13 14 15	025·9 026·0 032·1 033·7	020·3 024·I 023·4 032·0	012·2 018·3 018·5 005·0	008·7 010·6 005·0 994·9		004·4 017·9 023·2 021·0	996·2 987·2 988·2 002·5	987·2 982·2 984·3 984·5	008·9 011·4 011·5 009·6	005·3 004·9 002·1 002·1	036·2 028·4 028·0 020·5	028·4 025·7 023·6 018·9	024·7 023·8 020·8 015·8	023·2 020·1 015·8 008·8	020·0 021·8 025·1 026·9	013·9 013·5 021·5 024·9	012·8 008·0 003·1 011·6	008·0 998·4 999·1 003·1	003·9 005·8 013·4 015·7	996·7 998·7 005·3 013·3	019·2 001·7 998·9 995·3	982·1 988·4 978·9	033·5 033·0 033·9	015·2 013·2 022·4 027·8 030·8
	16 17 18 19 20	034·3 038·6 038·3	025·9 025·8 034·3 028·0 028·2	003·0 999·1 003·3	985·1 982·0 999·1 986·5	022.7	020·0 022·7 016·9 016·3	008·7 002·2 000·4 008·2	002·2 000·2 996·2 999·7	020·7 011·3	016·8 020·6 010·6 006·2	026·0 024·8 026·9 030·2	024·7 022·7 023·5 026·5	013·2 019·0 021·4 024·6	008·6 013·2 016·7 020·9	009·5 014·5 015·2 010·0	005·5 004·8 010·0 993·3	007·3 008·3 010·7 013·8	990·0 994·7 008·1 004·2	022·3 016·2 004·2 001·7	987·1 987·6 978·4	008·9 010·4 014·1 013·6	996·1 007·2 010·1 007·7	027·7 031·8 038·0 040·6	038.0
	21 22 23 24 25	034·8 036·9 037·5	031·8 032·3 034·7 034·1 036·8	986·4 985·2 993·9	981·0 972·0 973·0	012.4	011·9 010·6 005·2 002·9	013·0 020·2 020·4 999·6	006·2 012·9 999·6 991·6	015·2 025·2 027·4 021·3	013·1 013·2 021·3 018·9	030·8 030·6 029·6 027·I	029·2 029·5 027·1 024·0	027·9 019·8 015·2 014·9	019·8 014·3 012·5 010·1	010·2 008·2 017·3 016·0	003·3 990·9 993·7 002·9	004·2 007·0 006·8 011·2	989·6 989·7 985·5 985·6	992·9 985·6 979·8 988·4	985·6 974·5 973·8 979·8	011·2 018·7 023·2 023·0	007.6 010.8 018.7 008.2		012·4 012·2 009·4 005·3
	26 27 28 29 30	033·2 030·4 026·0 022·9		990.3	949·7 966·0 986·3 	021·9 020·1	001·9 008·0 016·4 016·8	012·9 012·7 008·7 010·2	009·4 008·4 007·0 005·8	022·I 025·4 025·6 022·8	019·2 021·7 022·3 017·3	025·3 025·8 025·8	023·8 024·6 024·7	017·3 006·8 006·7 004·1	005·8 003·6 002·3 995·8	007·4 011·2 012·2 014·2	998·0 006·2 991·8 012·2	016·9 024·5 026·3 023·9	019.0	982·2 004·3 003·9 023·3	982·2 997·3 997·1	004·0 005·3 018·2 020·1	000.0 001.8 002.1 010.3	009·I 009·7 026·9 027·I 026·3	995.8
	Mean	021·8 1026 ·18	1020	 1000 •41		1017			1000		1013		1022	1016		1015	1006	1017		1008	1 ' a	1013	··· 1004 ·90		1010

300. Cahirciveen (Valencia Observatory): North Wall Screen: ht (height of thermometer bulbs above ground) = $1 \cdot 3$ metres.

January, 1923.

Day.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mea
1 2 3 4 5	a. 76.0 84.2 81.9 81.1	84·2 81·4 80·8	84·3 81·6 80·6	84·4 81·7 80·5	84·5 81·8 81·2	83·5 81·3	83·2 81·8 81·1	82·8 81·9 80·4	82·8 81·3 80·8	82·9 81·6 80·7	83·3 81·3	a. 79·6 83·3 81·7 81·6 80·5	82·5 82·1 81·9	82·7 81·7 82·1	82·5 81·6 82·0	82·5 81·6 81·8	82·4 81·7 81·5	82·3 81·5 81·5	82·5 81·6 81·4	81·8 81·7	82·3 81·7 82·0	81·6 81·5 82·1	80·6 81·5 82·3	81·2 81·4 82·5	80 · 3 82 · 6 81 · 6 81 · 6
6 7 8 9	80·0 83·6 83·2 81·7	79·4 83·6 82·7	79·8 83·5 82·5 80·6	80·4 83·6 82·4 80·1	79·9 83·6 82·4 79·9	80·6 83·6 81·8 80·1	80·5 83·8 81·5 79·7	80·2 83·7 81·7 79·9	80·6 83·7 81·4 79·1	80·4 83·6 81·7 79·4	80·9 83·5 82·0 79·6	81·3 83·5 82·1 79·0 79·6	81·5 83·5 81·7 78·3	81·3 83·5 81·6 78·3	81·4 83·5 81·5	81·4 83·5 81·4 78·5	81·4 83·4 81·1 79·1	81·8 83·5 81·5 78·5	82·4 83·7 81·7 79·1	83·0 83·8 81·9 79·3	83·4 84·0 82·2 78·7	83·4 83·8 82·1 78·0	83·5 83·7 82·4 79·6	83·5 84·3 81·4 79·8	81 · : 83 · : 82 · : 79 · :
11 12 13 14	74·3 78·7 82·5	74·8 79·1 82·5	75·I 79·2 82·4	74·6 79·5 82·5	74.4 79.6 82.6	74·5 79·9 82·7	73·9 79·9 82·9	74·6 80·1 82·9	74·0 80·2 82·3	74·3 80·6 82·2	75.4 81.3 82.1	80·3 76·5 81·6 82·1 80·5	77·6 81·9 82·1	78·6 82·4 82·0	78·9 82·1 81·9	79·0 82·4 81·5	78·7 82·5 80·6	78·I 82·6 79·9	78·2 82·2 80·7	78·1 82·3 80·8	78·0 82·1 80·6	78·3 82·2 80·4	78·9 82·3 80·3	78·9 82·5 80·0	81 · 81 ·
16 17 18 19 20	80·9 79·1 81·4	80·9 78·7 81·3	81·0 78·4 81·4	80·7 77·9 81·4	80·9 77·1 81·8	80·9 76·9 81·8	80·9 75·6 81·8	80·9 75·2 81·8	81·9 81·9	80·9 76·5 82·4	81·7 78·4 82·5	81·7 82·1 79·4 82·8 81·4	82·3 81·3 83·2	82·4 81·5 83·4	82·4 81·4 83·7	82·3 81·4 83·3	82·0 80·7 82·9	81·8 81·3 82·9	81·7 81·4 82·9	81·3 83·1	81·3 81·0	83·3 81·3	79·9 81·2 83·1	79·6 81·4 82·7	81 · 79 · 82 ·
21 22 23 24 25	82·5 79·1 82·0	82·5 79·1 81·9	82·3 82·1	82·3 78·0 81·8	82·5 77·5 82·0	82·6 77·5 81·6	82·5 77·9 81·4	78·3 80·9	81·6 79·0 81·1	80·0 82·0	80·5 82·4	83·2 82·3 81·4 82·6 82·0	82·9 82·2 83·2	83·0 82·3 83·3	82·4 83·1	82·6 82·2 82·6	82·5 82·1 82·4	82·3 81·6 82·3	82·4 81·2	82·1 82·1	82·5 81·9 82·0	81·7 81·9	81·4 81·8 81·6	81·7 81·6	80 82
26 27 28 29 30	81·6 80·2 82·8	81·7 79·5	81·8 79·5	81·5 79·4	81·5 79·7	81·9 79·8 82·8	81·9 80·4 82·8	81·9 80·7 82·8	82·2 80·9	82·3 81·5	82·4 81·5	82·1 82·5 82·4 83·5 84·3	82·3 82·3	81·9 82·7 83·5	82·0 82·8	82·2 82·5	81·9 82·5 83·5	81.6 82.5 83.5	81·7 82·6 83·5	81·7 82·6 83·7	81·5 82·6 83·6	81·5 82·7 83·6	80·6 82·7 83·5	80·4 82·7 83·6	81 83
31 an			l	l	-l	.	·	84·2 81·6		-	·	-	-	-	-	-			-	-	-[

301. Cahirciveen (Valencia Observatory): North Wall Screen: $h_t = 1 \cdot 3$ metres.

February, 1923.

1 2 3 4 5	84·6 82·5	84·5 82·5 81·8	84·5 82·7 81·6	84·4 82·6	84·4 83·0	84·4 82·4	a. 84·7 84·4 82·0 80·9 82·5	84·4 82·5	84.3	84·3 82·8	84·5 83·4	83.9	84·5 84·1 82·3	84·9 82·5	84·9 83·1 82·6	84·8 82·6 81·8	84.6 82.3 81.7	84·4 82·2 81·7	81·9 80·9	81·7 81·5	82·0 81·4	82·2 81·4	81·9 81·4	81·5 81·6	a. 84·9 84·3 82·6 81·5 82·5
6 7 8 9	77.9	77.5	77.3	76.9	70.3	76.2		77.3	78.1	79.7	79.5	79.3	81.0	79.0	78.0 83.1	83.5	83.2	83.2	82.7	82.8	82.7	82.6	81.4	82.5	79·7 79·4 78·8 81·4 81·7
11 12 13 14 15	80·1 79·9 83·3 77·7 82·6	80·3 80·4 83·4 77·4 82·6	80·7 79·6 83·5 76·6 82·6	81·4 80·7 83·5 76·4 82·2	81·5 81·3 83·5 76·4 82·4	81·3 80·9 83·3 75·5 82·5	81·5 81·1 83·1 75·1 82·9	81·1 81·3 83·0 74·9 82·6	80·6 81·5 83·0 75·1 82·5	81·3 81·6 83·4 76·4 81·4	81·7 82·3 83·4 78·7 81·4	82·3 83·1 83·5 81·0 81·4	82·2 82·5 83·7 81·6 81·5	82·3 83·4 83·4 82·0 81·7	82·3 83·6 83·9 82·0 81·9	81·5 83·5 83·5 82·0 81·7	80·9 83·4 82·2 81·9 81·3	80·9 83·1 81·3 81·7 80·4	81·4 83·3 81·6 81·6 79·6	80·6 83·3 80·4 81·7 79·6	80·3 83·4 79·9 81·7 79·8	80·3 83·5 79·5 81·2 79·4	79·9 83·4 79·5 81·9 79·6	80·1 83·4 78·5 82·6 79·2	81 · 1 82 · 2 82 · 5 79 · 2 81 · 4
16 17 18 19 20	79·1 81·0 83·1	80·1 80·8 81·2	81·3 80·5 80·5	81·5 80·4 80·6	81·7 79·5 79·7	81·7 78·9 80·6	81·7 80·8 80·8	81·8 81·1 79·9	82·0 81·3 80·3	82·2 81·5 81·4	81·9 81·9 82·3	81·6 82·3 81·8	81·4 83·1 80·8	80·4 83·4 80·6	80·1 83·9 81·3	80·4 83·8 81·4 80·8	81·4 83·8 81·5	81·8 83·6 81·0	81·7 83·9 80·5	81.6 83.9 80.5 78.6	81·1 83·7 79·8 78·0	80·9 83·2 79·9	80·8 83·2 79·6	80·8 83·3 79·6 76·9	81·2 82·1 80·9 79·1 78·0
21 22 23 24 25	78·7 77·8	78·7 77·3	78·2 77·3	78·2 76·5	78·2 78·6	78·3	77·6	77:9 77:4	78·0 76·5	78·5 76·5	76·9 76·7	78·I	80·3 78·1	80·0 78·7	79·9 78·5	79·I	78·9 79·1	78·9 78·1	79·3 76·8	79·7 75·8	79·2 75·1 81·6	79·2 75·5 81·5	78·7 77·9 81·6	78·1 78·5 81·5	
26 27 28	82.2	83.5	83.7	84.2	83.6	81.9	80.7	81.2	81.8	81.4	81.5	81.8	81.9	81.7	80.9	80.4	80.3	80.4	80.3	80·5	80·6 81·5	80·5	80·6 81·3	80·4 81·2	81 · 6 81 · 6
	8o·8	80.8	80.6	80.5	80.5	80.5	80.3	80.3	80.5	80.8	81.2	81.7	81.9	81.9	81.8	81.7	81.5					1		,	81 · o Mean
G.M.T	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean

302. Cahirciveen (Valencia Observatory): North Wall Screen: h_t (height of thermometer bulbs above ground) = $1 \cdot 3$ metres.

March, 1923.

																								;n, 11	
Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mear
1 2 3 4 5	80·4 79·5 79·9	80·0 79·9	70.3	80·5	77.9	80·9 81·3	81·9 76·4	80·8 81·0 76·5	81·3 77·3	80·6 82·4 79·4	81·1 82·5 80·4	80·5 82·8 81·5	82·2 82·9 81·4	80·9 82·9 81·5	81·9 81·6	81·5 81·4 81·5	81·5 82·3 81·3	80·9 81·7 80·6	a. 81·5 80·5 81·4 80·6 82·3	80·6 81·2 80·6	80·4 81·2 80·8	80·5 80·6 80·9	80.3	80·3 80·8	81 · 4 79 · 9
6 7 8 9 10	81·7 80·9 79·5	80.0	81·8 80·6 79·6	81·3 80·7 79·4	81·4 80·6 79·2	78.4	81·4 80·6	80·1 76·0	82·I 81·0	82·5 82·2 80·1	82·5 82·7 81·2	82·4 83·1 81·7	83·1 82·9 82·2	82·9 83·3 82·9	82·8 83·2 83·0	82·6 83·1 82·3	82·3 82·6 81·8	82·1 81·5 81·1	81·9 81·8 80·7 80·5 79·9	81·8 79·9 79·8	81·6 79·8 79·0	81·4 79·6 79·6	81·1	79·3 79·3	80·1 81·3 81·9
11 12 13 14	83·3 80·7	83·5 80·5	78·5 83·3 80·5 75·3 80·6	83·4 79·7	83·4 80·1	80·2	83·4 79·9 78·9	83·6 79·1	83·8 79·9 80·4	83·6 81·5 81·5	83·4 81·9 82·5	84·1 82·0 82·8	84·3 82·6 82·9	84·1 82·8 83·3	83·7 83·0 83·6	83·5 82·7 84·1	82·8 82·3 83·1	82·4 81·7 82·4	80·7 81·5 80·9 80·7 78·5	81·1 79·6 80·2	81·7 78·3 80·8	81·6	80·5 76·6 80·5	80·5 76·3 79·0	79·8 83·0 80·5 79·9 80·1
16 17 18 19 20	79·6 79·9 78·8	79.8	78·5 79·5	79·0 78·5	77.7	78·9 76·9	79·3 77·4	79·2 76·9	80·0 79·3	80·4 80·3 80·0	81·2 81·6 80·3	81·3 82·3 80·4	81·9 82·4 80·6	82·8 82·9 81·3	83·2 83·6 81·4	83·2 83·3 80·6	83·4 82·6 80·5	82·5 81·9 80·5	80·6 81·4 80·7 80·4 81·4	81·5 81·1 79·9	81·3 80·2 79·8	80·4 81·0 79·4	80·0	80·6 79·3 78·6	80·0 80·6 80·4 79·7 79·4
21 22 23 24 25	79.2	78·9 79·2	78·3	79.4	79.6	78·1 79·9 80·4	78·2 79·9 80·4	77·8 80·1 81·5	78·9 80·7 81·8	79·8 81·5 82·6	81·2 82·2 83·1	81·8 83·1 83·5	81·8 84·0 83·2	82·3 83·6 83·4	82·5 83·9 83·4	82·4 83·3 83·4	82·6 83·1 83·1	81·6 82·4 82·7	81·1 80·5 81·3 82·3 81·9	79·9 81·3 82·4	79·3 81·0 82·5	79·2 80·3 82·4	79·3 79·1 82·7	79·4 78·7 83·3	81.7
26 27 28 29 30	82.1	83·6 82·1	83·4 82·3	83·4 82·3	83·4 82·4 82·5	82.5	83·0 82·2 82·6	82·5 82·8	83·6 82·9 83·2	83·9 83·5 83·6	84·3 84·1 84·4	85·2 84·3 84·4	85·0 84·5 84·4	85·3 84·5 84·5	85·1 84·4 84·3	84·4 84·4 84·2	84·3 84·2 84·1	83·6 83·5 83·4	83·5 82·7 82·4 83·2 82·1	82·4 81·6 83·1	82·1 81·6 83·1	83.0	81·5 83·0	82·1 82·3 82·9	83 · 2
31	_	<u> </u>	77·3				Ī		l			ļ						ļ	81·3				79·3 80·5		
Mean	100 3	00 2	00 1	00 0	100	79.0	000		000)		1		<u> </u>	<u> </u>	<u> </u>
	ircive	en (V	alenc	ia Ok	serva	atory)	: N	orth	Wall	Scre	en:]	h <i>t</i> =	1.3	metre	es.]					il, 19	
	a. 76.6 77.6 79.2	a. 76·2 76·8 79·5	alenc a. 75.5 77.0 79.7 80.0	a. 75.2 76.4 79.7	a. 74.4 75.6 80.3 80.6	atory) a. 74.9 75.5 80.4 80.3	a. 74.3 75.1 80.6	orth a. 78.7 77.4 81.6 80.4	Wall a. 80·3 79·4 82·2 80·7	Scre a. 81.5 80.5 82.3 81.5	en:] a. 82.5 82.4 82.2 81.7	$ht = \frac{a}{82.6}$ 82.6 83.3 81.6 82.2	1·3 a. 82·9 83·2 81·5 82·1	metro 83.3 83.5 81.8 82.4	es. a. 83.3 83.5 82.0 82.6	a. 83·0 83·3 81·7 82·2	a. 82·5 83·3 81·4 82·6	a. 81·6 82·6 80·8] a.	a. 79·7 79·9 80·9	a. 79·6 79·5 81·3	a. 79·2 79·3 81·9	a. 78·9 79·3 80·7 80·3	a. 77·8 79·1 80·9 79·9	a. 79·4 79·8 81·0 81·2
303. Cah	a. 76.6 77.6 79.2 81.0 79.0 79.6 79.0 78.3	a. 76.2 76.8 79.5 81.0 78.6 78.9 78.5 77.2	alenc a. 75.5 77.0 79.7 80.9 78.9 78.9 78.2 76.3	a. 75.2 76.4 79.7 80.9 79.4 78.3 78.0	a. 74.4 75.6 80.3 80.6 79.2 78.6 78.0 74.9	atory) a. 74.9 75.5 80.4 80.3 79.1 78.0 77.9 74.9	2. No. 1	orth a. 78.7 77.4 81.6 80.4 79.9 78.6 77.9 78.5 80.7	Wall a. 80·3 79·4 82·2 80·7 80·0 79·4 80·9 81·3	Scre. a. 81·5 80·5 82·3 81·5 81·1 80·7 79·9 81·4 81·6	en:] a. 82·5 82·4 82·2 81·7 81·4 81·5 81·1 81·9 82·1	$ht = \begin{bmatrix} a \\ 82.6 \\ 83.3 \\ 81.6 \\ 82.2 \\ 81.6 \\ 81.7 \\ 82.1 \\ 83.4 \\ 82.5 \end{bmatrix}$	a. 82.9 83.2 81.5 82.1 81.3 82.1 82.2 83.9 81.8	metro 83·3 83·5 81·8 82·4 81·6 81·9 82·3 81·8	a. 83.3 83.5 82.0 82.6 82.0 81.1 82.2 83.7 81.5	a. 83·0 83·3 81·7 82·2 81·6	a. 82·5 83·3 81·4 82·6 80·4 81·1 82·0 82·7	a. 81.6 82.6 80.8 82.2 80.5 79.7 81.5 82.9	a. 80·7 81·6 80·7 81·5	a. 79.7 79.9 80.9 80.5 79.1 80.1 81.9	a. 79.6 79.5 81.3 80.7 80.3 79.1 80.1 82.1 79.5	a. 79·2 79·3 81·9 79·6 79·8 79·3 79·5 82·2 79·4	a. 78·9 79·3 80·7 80·3 79·6 79·7 79·5 81·7	a. 77.8 79.1 80.9 79.9 79.4 79.1 79.3 82.1 79.1	a. 79.4 79.8 81.0 81.2 80.2 79.8 80.0 80.5 81.1
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304. Cahirciveen (Valencia Observatory): North Wall Screen: h_t (height of thermometer bulbs above ground) = $1 \cdot 3$ metres.

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31	82.1	82.2	<u> </u>	82.6	83.4	84.1	85.4	86.4	88·o	88·o	<u>-</u>	89.2		90.0	90.3	89.9	89.5	88·o	87.4	86.4	-	84.4	- <u>-</u>	84.6	┢
Mean	81.7	81.6	81.5	81.4	81.4	81.6	82.3	82.8	83.1	83.6	83.8	84.1	84.3	84.5	84.5	84.4	84.3	83.9	83.5	83.0	82.5	82.1	81.9	81.8	8:
)5. Gah	ircive	en (V	alend	ia O	bserv	atory) : N	orth	Wall	Scre	en:	$h_t =$	1.3	metr	es.								Jun	e, 19	23
1 2 3 4 5	a. 84.6 82.8 83.7 83.5 83.6	82·5 81·8 83·6 83·6 83·3		80·4 80·4 82·9 83·5 83·5	79·9 82·3 83·5	84.1	a. 81·9 83·4 83·6 84·5 82·9	82·8 85·9 83·9 84·6 83·1	84.8	a. 84·3 88·6 87·4 85·1 83·5	a. 84·8 88·6 88·4 85·6 84·2	88∙o	a. 85·8 89·2 87·4 85·9 84·1		a. 86·5 88·6 86·0 86·1 84·6	a. 86·8 88·6 85·6 86·9 84·9	85·5 86·5	87·5 85·3 85·6	a. 86·3 87·0 84·7 84·7 84·5	a. 85.8 86.5 84.5 84.3 84.4	83.9	a. 84·7 85·2 83·4 83·6 83·9	83·5 83·5	84·5 83·5	8.
6 7 8	84·0 82·5 84·5	82·T	81.7	83·6 82·8 84·5	83·5 83·2 84·5	183.6	84.5	184.7	84·3 85·9 85·3	85.0	185.0	85·2 85·9 86·9	85.4	185.6	185·0	86·3 85·5 87·7	85.4	85·1 84·9 86·4	84.5	84·3 84·5 85·7	84·5 85·6	83·5 84·5 85·5	84.5	83·1 84·5 86·1	84

						,	, • •	OI th																•	
1 2 3 4 5	84.6 82.8 83.7 83.5 83.5	82·5 81·8 83·6 83·6	81·2 83·3 83·5	80·4 82·9 83·5	79·9 82·3 83·5	a. 80·8 80·8 82·9 84·1 83·4	83·4 83·6 84·5	85·9 83·9 84·6	85·9 84·8	85.1	88.4	a. 85·4 88·0 87·7 85·9 84·2	89·2 87·4	86.4	86∙1	88·6 85·6 86·9	88·3 85·5 86·5	87·5 85·3	87·0 84·7 84·7	86·5 84·5 84·3	84·1 83·9	85·2 83·4	85·2 83·5 83·5	83.6	84·6 84·8 84·7
6 7 8 9 10	82 · 84 · 86 · 8	84.5	81·7 84·4 87·0	84.5	84·5 86·9	83·5 83·6 84·6 86·4 84·1	84·9 86·3	85·3 86·3	85.3	85.5	86.4	86·a	87.4	88.3	87.7	87.7	87.3	186.4	86.2	85.7	85.0	85.2	85.2	80.1	86.6
11 12 13 14	84·2 83·9 85·1 83·8	83.7	83·8 85·1 83·9	84·I 85·I 83·9	85·2 84·0	84·5 85·3 84·2	85·2 85·3 84·9	85·4 85·1	85·5 85·5	85·4 85·5	85·5 85·0	86·3 86·5	86·9 85·8 87·2	86·3 86·0	86·3 85·7 85·9 87·3 86·3	85.8 85.8	85·4 86·9	85·2 86·2	84·6 85·8	84.2	83·9 85·5	83·9 85·8	83·8 86·0	83·8 85·9	85·0 85·4 85·1 85·6 85·3
16 17 18 19 20	83·2 83·2 85·2 84·2 83·9	83·0 85·2 84·0	83·I 84·9 83·8	84·6 83·8	83·0 84·5 83·7	83.7	82·9 84·3	83·7 84·5 85·3	84·0 84·7	84·6 85·2 85·4	85·9 85·4	85·9 85·9 86·2	86·7 86·2	86·7 86·5	86·2 87·4 86·4	87·7 86·8	86·8 86·9	105.0	86·5 85·5	86.1	85·7 84·5	85·0 84·1	85·2 84·1 84·3	85·2 84·2	85·5 85·0
21 22 23 24 25	85·2 86·4	86·4 86·3	85·3 86·6 86·3	86·6 86·3	85·6 86·8	86.4	85·4 86·9 86·8	85·1 87·1	86·1 87·5 87·8	87·3 88·3	88·3 88·6 80·3	88·4 88·1	89·4 88·4 80·2	88·5 88·6 88·7	87·9 88·9 88·8	89·2 89·1	88·5 88·9	87·5 88·2 88·2	87·2 87·8 87·9	87·4 87·3	87.1	86·6 86·5	86.5	86·5 86·4	87.5
26 27 28 29 30	86·2 85·2 85·3 86·8 85·1	85·2 84·3 86·6	85·3 84·4 86·4	85·4 84·1 86·2	83·9 86·0	85·7 84·6 86·2	86·4 86·6	86·6 88·5	87·7 88·3 86·8	188 - 5	88·5 89·6 87·5	89·3 89·9	89·1 88·1	89·1 90·3 88·7	89·0 90·4 88·0	80.2	87·9 90·0 88·3	87·3 88·9 87·6	88·0 86·5	87.7	87·4 85·8	87·2 85·5	85·4 85·4	87·0 85·3	86·2 86·8 87·5 87·0 86·4
Mean .	84.8	84.6	84.4	84.4	84.4	84.5	84.9	85.4	85.9	86.2	86.7	86.8	87.1	87.1	87.1	87.2	87·o	86.5	86·o	85.6	85.3	85.0	85·o	84.9	85.7
G.M.T.	τ.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mea

306. Cahirciveen (Valencia Observatory): North Wall Screen: h_t (height of thermometer bulbs above ground) = $1 \cdot 3$ metres.

July, 1923.

Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	IO.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Ме
1 2 3 4 5	a. 84·7 86·7 87·3 86·6 86·9	86·7 87·4	86·6 87·4 86·6	86.6	a. 83·9 86·7 87·4 86·5 86·2	87·4 86·6	87·4 87·3	87·5 86·8 88·5	88·0 86·4 80·5	88·4 86·6 80·5	88·2 88·5	89·8	88·9 89·8 90·4	88·4 89·7	89·7 90·4	89·2 89·4 89·7	88.6 89.1 88.8	87·9 88·8 88·4	87·5 88·4 88·5	87·4 87·9 88·1	87·3 87·2 87·8	87·2 87·0 87·4	87·3 86·9 87·2	86·8 87·1	87 87 88
6 7 8 9 10	87·2 88·0 87·3 88·5 87·9	88·6 86·9 88·5	88·9 86·9 88·4	88·7 86·8 88·3	86·9 88·3	88·9 87·5 88·3	89·3 88·4 88·8	89·5 89·4 88·8	90·1 90·1	89·5 89·7	89·5 90·2 89·9	90·2 89·6 90·5	90·4 89·2 90·9	90·3 89·3 90·5	89·7 89·2 91·2	90·2 89·0 91·4	91·8 91·6	90·9 90·9	89·5 88·8 90·9	89·2 88·7 89·9	88·7 88·4 88·4	88·5 88·4 88·4	88·3 88·4 88·3	87·9 88·4	89 88 89
11 12 13 14	86·4 87·2 88·1	87.1	86·9 87·7 87·1	87·2 87·6		88·2 88·7 87·7	88·7 89·9 89·7	90·8 91·1	90·9 91·2	90·3	90.6	91·I	90·9 92·9 80·0	91·I 92·9	90·9	93·1 93·1	93.3	91·2 93·2 88·6	90·2 91·9 88·0	90·7 87·6	88·9 90·2 87·6	89·8 87·3	86·9	88·9 86·9	90
16 17 18 19 20	86·3 85·8 87·1	85·8 86·3 87·3	86·2 85·4 87·5	86·0 85·9 87·1	86·9 85·8 86·2 86·4 88·5	86·0 86·9	86·8 87·2 87·9	88·4 87·3 90·2 88·5 89·3	89·4 89·8 88·6	89·1 89·4 88·7	89·5 89·4 80·0	90·1 89·4 89·7 89·9 90·7	90·4 89·5 90·1	89·2 89·6	89·9 89·2 90·2	89·9 89·5	89·6 89·4 89·7	89·2 88·6 89·5	87·9 88·2 89·0	87·5 87·9 88·6	87·2 78·3 88·5	86.9 87.2 88.4	88.5	86·5 86·9 88·6	88 88 88
21 22 23 24 25	88·9 89·2 87·4	88·5 89·3	88·5 89·5 87·2	88·5 89·5 87·1	88·8 88·5 89·1 87·1 88·6	89·0 89·3	89·1 89·5	89·7 89·6 88·1	90·2 89·4 88·5	91·0 89·5 80·1	91·2 89·3 80·0	91·1 89·4 90·4	91·3 89·4 90·3	89·9 81·9	90·8 90·0 90·2	90·6 89·5 90·3	89·6 89·9	89·9 89·4	90·2 89·1 89·4	88·3 89·0	89·4 87·4 88·5	89.2	89·2 87·5 88·4	87.4	8
26 27 28 29 30	86·2 87·4 86·7	86.2	86·4 87·1 86·7	86·3 86·4 86·6	86·6 86·4 86·0 86·6 87·4	87·2 86·6 86·8	88·8 87·4 87·1	89·5	89·9 88·6 88·2	90·0 88·5 89·3	89·9 89·0 88·6	89·9 88·9	90·8 89·4 88·6	100.6	90·7 89·9 89·6	190.3	89·5 89·4	88·7 89·0	88·3 88·7	87·8 88·1	87·2 87·7	87·2 87·7	86.6	87·8 86·6 87·5	8 8 8
31					84.8		l							1		ļ			ļ						
lean .	87.3	87.2	87.1	87.1	87.0	87.3	88·o	88.7	89.1	89.4	89.8	90·I	90.3	90.3	90.4	90.3	90.2	89.6	89.0	88.6	88·o	87.8	87.6	87.5	188

307. Cahi																August, 1923									
3 4	86·3 85·9 86·7	86.9	87·3 85·9 86·7	88·2 86·0 86·7	88·9 85·9 86·9	88·0 85·9 87·7	87·5 86·7 88·0	87·9 88·4 89·6	88·4 88·5 90·6	88·5 88·8 90·3	87·9 89·5 90·6	a. 90·1 87·2 90·1 90·9 90·9	86·5 89·8 90·9	90.9	88·4 90·0 90·3	90.0	89·9 89·9	88·3 89·4	88·4 87·6 88·4 89·2	a. 87·6 87·3 87·7 88·9 89·2	86·9 87·0 88·9	86·7 86·1 89·1	86·1 88·6	85·9 86·5	87·6 87·9 89·0
7 8	88·5 88·7 87·9	88·4 88·6	88·5 88·4 87·9	89·1 88·5 87·9	88·9 88·3	88·8 88·0 87·6	88·5 88·5	88·5 89·2 88·7	88·4 89·3 80·4	88·5 89·5 90·8	89·4 89·3	89·3 90·2 89·3 91·5 91·3	90·2 89·4 91·4	90·6 89·5 91·4	90·0 91·4	90·6 90·6	89·5 89·6 90·5	89·6 89·6 90·2	88·5 89·4 89·4	88·6 87·9 89·4 88·8 88·5	87·3 89·0 88·5	87·5 88·8 88·4	87.8	88∙6 88∙o 88∙1	89·1 89·3
1 14	89·6 88·2	88·6 89·6	88·8 89·6 87·8	89·0 89·3	88·9 88·2	88·9 89·0	89·I	89·3 89·4 88·8	89·3 89·8	89·6 90·5	89·8 91·6 80·7	91·6 89·6 90·9 89·8 88·5	90·0 90·5 80·7	90·4 90·4	90·0 91·5	90·6 89·9	90·8 89·4	90·3 88·9	89·6 88·3	89.7	88·7 87·3	88·6 87·2	89·2 89·4 88·5 86·9 86·8	88·4 86·9	89·8 88·6
16 17 18 19 20	86·4 88·8 87·4 86·9 87·5	88·5 87·4 87·3	88·3 87·2 87·3	87·5 87·2 87·3	87·8 87·1 87·2	87·8 86·6 87·2	87·8 87·2 87·6	87·9 87·4 88·7	88·6 80·1	88·6 88·9	89·3 88·8 80·3	89·5 89·5 88·7 89·9 88·3	90·2 88·5 89·6	89·3 89·0	89·4	87·9 87·7	88·4 87·4	87·6 87·7 88·1 87·3 89·6	88·0 87·3	87.1	87·3 87·6	87·2 88·2	10/ I	86·9 87·8	87·8 88·0
21 22 23 24 25	86.4	86·4 85·4	86·5 85·8	86·5 86·2	86.3	86·2 86·4 85·0	86·8 86·8	87·5 87·3	87·3 88·2	87·6 87·7	87·8 88·1 87·0	87·8 88·2 89·4 87·9 88·3	88·5 89·9 87·0	88·1 88·1	88·5 89·8 88·0	89·4 89·8	88·2 88·9 87·8	88·3 87·4	86·8 87·6 86·8	86·0 86·0 86·9 85·8 87·6	85·0 86·5 85·5	84·5 85·6 84·2	86·2 84·5 85·3 83·9 87·6	84·3 84·5 83·7	86 · 8 87 · 3 86 · 5
28 29	86·6 85·6 84·9 82·9 84·0	85·1 85·2 83·2	85·4 85·2 82·9	85·5 85·2 82·9	84·5 85·0 83·0	85·4 84·4 82·6	85·6 85·4 82·5	85·8 86·4 82·0	86·1 85·0 82·4	86·2 86·3 82·8	86·0 87·1 83·1	88·9 86·7 87·6 83·3 86·4	86·3 87·1 85·4	86·0 87·4 85·3	86·7 87·5 85·0	86.7	86·5 86·6 85·6	86·6 86·2 84·6	85·3 85·2 85·1	84·8 84·4	84·5 84·5	84·9 84·7	85·2 85·2 84·9 84·3 84·5	84·2 83·8	85·8 83 ·9
31												86.4	<u> </u>		·								84.5		85·1 87·7
Mean G.M.T	86·6 1.	2.	86·6 3⋅	86·7 4·	86·6 5.	86·6 6.	86·9 7·	87·5 8.	88·o 9.	88·3 10.		89·0 Noon		14.	15.	16.	17.		19.	20.	21.	22.	23.	<u>-</u>	Mean
•	I					1	1	1	1	1	1	İ	1	1	1	1	ł	{	1	1	1	1	1	1	1

308. Cahirciveen (Valencia Observatory): North Wall Screen: h_t (height of thermometer bulbs above ground) = 1.3 metres.

																						Sep	temb	er, 19	923.
Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	Io.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	М
	a.	a.	a.	a.	a.	a.	a.	a.	a.	a. 84.6	a. 85·7	a. 86·4	a. 86∙8	a. 86·8	a. 87·1	a. 86.8	a. 86∙6	a. 86·2	a. 85·5	a. 84.7	84·1	a. 83.6	83·4	a. 82·3	85
I 2	84·6 81·7		84.4	84·2 80·9	84·3 80·5	80.3	80.9	84·2 83·9	85·7 84·9	86.6	87.1	87.4	87.5	87.6	86.8	87·1	87.4	86.9	85.9	84.3	85.2	85.3	84.1	84.1	84
3	84.5	83.9	83.9	83.8	84·5 84·5	84·8 84·4	85.7	86·3 85·5	86·5 86·1	86·5 86·5	86·9 87·0	86·9 87·3	86·5 87·5	86.8	87·1	87·2 87·6	87·3	87·2 86·7	87·2 86·1	87·5 85·7	87·6 85·3	87·5 85·2	86·5 85·5	86·0	86 86
5	85·4 85·9	85·5 86·3	84·6 86·4	84·5 86·4	86.3	86.3	84·4 86·3	86.6	87·o	87.4	87.9	88.1	88.4	87·5 88·8	88.7		87.9	87.5	87.1	86.9	86.8	86.8		86.4	8
6	86·o		86·1	86.2	86.3	86.4	86.6	86.9	87.2	87.3	87.6	87.9	88.3	88.9	89·0 87·6	88.7	88.3	88·3 86·7	88·2 85·9	88·o 84·3	87·8 83·5	87·9 82·5	88·1 81 6	88.2	8/ 8/
7 8	88∙3 80∙6		86·9 80·7	86·6 8o·o	86·6 80·4	86·1	85·9 83·2	86·o 85·1	86.2	86·5 87·0	87.7	87·1 88·3	88·4	87·3	87.9	88∙1	87.5	86.9	86.3	86∙0	86.2	86.2	86.2	86.3	8
9	86.2	86.3	86.4	86.5	86.5	86.3	86.5		87.2	87.2	87.8	88·o	87.9	87·6 87·5	86·3 87·5	86·5 87·4	86·5 87·1	86·4 86·7	86·2 85·8	86.3	86·3 84·8	85·9 83·4	85·7 82·5	1 2 1	8
10	85.1		1_	84.5		_	1	1	1	85.7	ĺ	1	88.8	1	88.1		1	87.6	L	Í	87.1	1	86.9	1	8
II I2	80·4 86·9	80·I	80.3	80·1 87·4	87.4	80·7 87·4	80·8 87·3	83·4 86·8	86·8 87·2	86·9 88·1	88·4 89·0	88·7 89·4	89.1	88·4 89·9	80.8	88·3 89·5	87·7 88·6	88.2	87·3 87·6	87·1 87·5	87.5	87.6	86.9	86.9	8
13	86.8	86.6	86.6	86.7	86.7	86.8		87.1	87.6	87·2 85·6	87.2	87·4 85·2	86.0	87.8	87·2 85·8	86.8	86·6 85·3	86·o 84·8	85·6 84·1	85·5 82·9	85.4	85·0 82·6	85·4 83·1		8
14 15	84·8 82·1	84·8 81·9	84·3 82·1	84·7 82·4	84·4 82·0	84·5 82·4	84·4 82·0	85·1	85·5 83·5	84.3	82.5	83.2	83.3	85·9 84·4	83.8	84.4	84.2	83.3				82.4	82.1	82.4	8
16	83.9		82.0	83.1		83.2	83.1	83.7	84.4	84.6	84.4	85.4	86·o	85.9	85.7	85.7	84.9	84.4	83·9 82·3	84.1	84.4	84.6		85.0	8
17 18	84·4 83·1		84·5 83·7	84·5 83·5	84·6 83·6	84·8 83·4	85·2 82·5	85·9 83·8	85·6 84·0	84·6 85·1	83·5 84·1	83·5 84·7	83·9 84·5	84·8 85·1	8 ₄ ·5 8 ₅ ·4	84·9 85·4	83·1 84·9	83·3 84·2	84.2	83·9 83·3	83.8	84·1 83·6	83·9	83.9	8
. 19	83.0	84.5	84.5	84.3	84.5	84.8	84.9	84·4 84·7	85.4	85.9	86.4	84.9	86.9	86·I	86.2	86·2 86·0	80.1	85·7 85·3	85.3	85·1 86·7	84·9 86·3	85·4 85·8	85·2 86·2	85·I	8
20	84.9	84.7	84.9	84.5		84.5	l_	ł.		85.6	l	85.9	l	86.0			l_	1		ĺ		*	1		8
2 I 2 2	86·3 84·6	86·1 85·2	86·1 84·4	86·1 83·8	86·1	85·8 84·2	85·9 83·5	85·7 83·9	86·1 85·0	86.2	86·7 84·6	87·3 85·6	87·4 85·9	87·3 85·5	87·5 85·6	87·3 85·6	87·0 85·1	86·5 83·9	86·4 83·3	86·3 83·3	86·2 83·6	83.5	85·5 83·9	83.9	8
23	83.9	83.7	83.4	83.6	83.5	83.9	84.1	84.1	84.5	85·5 84·6	185.2	85.7	85.3	85.7	85.7	85.6	85.3	84.7	84.2	83·7 84·8	83·3 84·9	81.7	80.6	80·2 85·1	Į۷
24 25	80·7 85·1	80·9 85·2	82·7 85·2	83·3 85·2	83·9 84·1	83·9 84·4	84·1 84·4	84·5 84·8	85·2 84·9	85·5 84·6	85·3 84·7	85·0 85·1	85.4	85·4 85·6	85·3 86·1	85·3 86·3	86.3	85.9	85.9	85.9	86.2	86.4	86.3	86.4	8
26	86.3	85.9	85.6	85.8	86∙1	86·1	86·o	86∙1	86.9	87.4	87.4	87.7	87.7	87.7	87.5	87.5	87.5	86.9	86.5	86.6	86.8	86.8	86.6		8
27 28	86·7 86·5	86.7	86.8	87.1	87·1 84·6	87.1	87.2	87·5 84·5	87.6	87.5	87.5	87·6 87·1	87·5	187.5	87·4 88·o	87·5 87·9	87·5 87·7	87·5 87·7	87·4 88·o	87·7 87·8	88·3 87·9	87·8 88·1	87·8 88·1	87·5 88·2	8
20 29	88.1	88∙0	88·o	85·0 87·9	87.7	87.7	187·a	l88∙o	188.5	80.3	89.5	89.2	89.5	90.3	90.2	88.2	87.0	86.5	86·o	86·o	86.7	87.9	88.5	88.7	8
30	89.5	-	89.4	89.0	88.3	88.0	88.1	88·1	89.5		 	88.5		l	88.7	88∙0	·	87.4	87.3	87.3	87.4		87.4		8
lean .	84.9	84.9	84.7	84.7	84.7	84.7	84.8	85.4	86∙0	86.3	86.5	86.7	8 ₇ ∙o	87.1	87.0	86.9	86.5	86.1	85.8	85.6	85.6	85.4	85.3	85.1	B
		-							*** 11			•	1 0									0)ctob	er, 19	19
09. Ca	hircive	en (V	alene	ia U	DSOTV	atory): N	ortn	wan	Scre	en:	$n_t =$	1.3	metr	es.									···	_
ı	a. 87·2	a. 86·8	a. 85.8	85.0	a. 84.9	a. 84.9	a. 84.9	a. 84.8	<i>a</i> . 85∙o	85·4	a. 85·7	a. 86∙o	a. 86∙4	a. 86⋅6	a. 86·4	a. 86∙3	a. 86∙o	a. 85·5	a. 85·3	a. 84·5	a. 84·6	a. 84·6	a. 84·8	a. 85·2	8
2	85.5	85.7	85.9	86.3	86.4	84.5	84.3	84.4	84.8	85.2	85.2	85·I	85.8	85.4	85.6	85.4	84.8	84.5	83.9	83.8	83·8 82·7		83·0 82·4	82.9	8
3 4	84·0 82·0	86·1 81·7	86·0 81·7	84·8 81·5		83·5 81·3			83·2 82·4	82.9	84.4	83.7	84·2 84·5	84.3	84·1 84·0	83·0 83·5	83·5 83·6	83.2	82.7	83.0	83.5	83.7	84.1	84.2	8
5	84.4	84.5		84.5	84.7	85·o	85·ŏ	84.9	84.9	85.3	85.5	85.7	86·ŏ	85.4	85·o	85·o	84.9	83.6	83.8	83.6	83.7	83.4	83.5	83.8	8
6	84.2		83.7	84.3	84.4	84.5	84.6	84.9	84.4	85.4	86.0		86·0		85.0	85·7 86·7	85·6 86·3	85·1 85·6	85·2 85·6	85·2 85·6	85·3 85·9	85·4 85·8	85·5 85·8	85·4 85·9	8
7 8	85·4 85·7	85·4 85·6		84·9 85·0	84.9	85·5 84·4	84.3	84.4	84.9	85.8	86.8	86·o	86.6	87.1	87.5	87.7	87.7	87.6	87.4	87.5	87.6	87.7	87.7	87.9	8
9	87.9	87.2	86.3	86∙0	85.7	85.5	85.4	85.4	85.4	85.6	86.2	86.5	86.5	86.4	86∙3	85.7	85.4	85·0 85·0	84·7 85·3	84·8 85·1	84·8 84·8	84.5		84·9 84·0	8
10	85∙0	02.1	05.0	05.1	85.4	05.2	85.3	85.3	05.2	04.7	84.9	84.6	04.0	05.2	02.1	3.0	المارين	اري ر	ر ر	1	1	'	1	1	ľ

l .		a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	8 c. c	85.3	84.5	84.6	84.6	84.8	85.2	82.6
I		87.2	86.8	85.8	85.0	84·9	84.9	84.9	84.8	85.0	85.4	85.7	80.0	86.4	80.0	80.4	85.4	84.8	84.5	82.0	83.8	83.8	83.2	83.0	82.0	84.0
2																									82·9 81·9	
3		84·0 82·0	87.7	87.5	87.5	87.8	03.2	87.0	03.3	80.4	83.9	82.4	82.7	84.5	84.2	84.0	82.5	83.6	83.2	82.7	83.0	83.5	83.7	84 1	84.2	82.8
4		84.4	84.5	84.4	84.5	84.7	85.0	85.0	84.0	84.0	85.3	85.5	85.7	86.0	85.4	85:0	85.0	84.0	83.6	83.8	83.6	83.7	83.4	83.5	84·2 83·8	84.6
5																										
6		84.2	82.5	82.7	84.2	84.4	84.5	84.6	84.0	84.4	85.4	86.0	85.0	86.0	86∙T	85.0	85.7	85.6	85.1	85.2	85.2	85.3	85.4	85.5	85·4 85·9 87·0	85∙0
7		85.4	85.4	85.3	84.0	85.2	85.5	85.0	86.3	86.8	86.0	86.0	86.7	86.8	87.0	87.0	86.7	86.3	85.6	85.6	85.6	85.9	85.8	85.8	85.9	86·o
8																						- / -	-//		1-12	00 0
9		0	0	96.0	106.0	10	10	10	10	10	10 - 2	106.	104	106	196.4	186.2	1X = .7	125.4	105.0	104.7	104-0	104.0	104.5	104 7	84.9	85.8
IÓ		85·ó	85.1	85.0	85.1	85.4	85.5	85.3	85.3	85.5	84.7	84.9	84.6	84.6	85.2	85.1	85·o	85·o	85.0	85.3	85.1	84.8	84.9	84.3	84.0	85·0
1																										
11		84.2	84.3	84.3	84.2	84.0	84.0	83.6	83.4	83.5	84.0	84.4	84.2	84.7	84.8	84.9	84.6	84.5	84.2	83.9	83.8	83.9	84.0	83.1	82·9 82·6 80·6	94.1
12		82.9	82.4	82.6	83.3	83.0	8 3 ·o	82.8	83.4	83.4	82.9	82.3	83.4	83.5	83.3	82.9	83.0	82.8	82.7	82.7	82.8	02.0	01.9	02.3	02.0	82.6
13		82.4	82.6	82.5	82.7	82.5	83∙0	82.4	82.6	83·o	82.7	82.5	83.5	83.6	83.9	83.2	83.4	83·I	81.8	02.1	02.0	01.0	01.9	01.9	76.5	80.6
14		81.1	80·0	80.3	79.8	80.7	80.3	80.2	80.3	80.7	81.4	82.0	82.1	82.9	82.0	83.1	83.1	82.4	81.9	80.3	80.2	80.0	80.2	87.0	80·6 76·5 81·9	70.0
15		77.1	77.2	70.0	70.0	70.1	70.0	70.0	77.0	78.7	90.9	02.0	02.0	03.2	03.4	03.3	03 2	-	-	100	1 3	,	1		-	
		٥.												0	0	00	8	84.7	84.4	82.0	84.0	84.0	82.0	83.8	83.0	83·8 84·2 84·6 83·2 84·4
16		81.7	81.8	82.3	82.7	82.9	83.0	83.4	83.6	83.8	83.9	84.5	85.0	85.3	85.3	05.0	04.9	84.2	84.0	82.7	83.6	83.8	83.5	83.7	83.0	84.2
17		84 0	84.0	84.0	84.0	83.9	84.2	84.0	83.9	84.3	84.3	84.4	84.9	05.1	05.2	05.0	84.7	84.8	85.0	85.6	85.0	86.0	87.3	87.3	87.5	84.6
		03.7	03.2	82.9	03.0	93.3	83.7	83.9	83.0	83.0	03.0	04.2	04.5	94.9	82.0	84.5	82:7	82.5	82.3	82.2	82.2	82.3	81.7	82.9	83.1	83.2
19 20		92.4	03.0	03.3	93.0	84.0	82.9	02.5	82.7	02.5	03.0	03.2	85.6	85.8	85.7	85.1	85.2	85.2	84.3	84.0	84.4	83.9	82.7	82.6	82.2	84.4
20		05'4	03.2	03.2	03.9	04.0	04.2	04.2	05.0	05.4	05.4	05.5	05.0	V3 V	°5 /	ء ری	3 -	-3 -	1-4.3	1		ر ا	'	l	1	1 ' '
21		82.2	82.6	82.8	82.6	82.4	82.2	81.5	82.4	82:0	82.2	82.6	82.7	82.1	82.0	83.2	82.8	83.0	82.4	82.2	82.5	82.3	82.0	82.5	82.6	82·6 83·2 82·4 81·9
22		81.0	82.4	82.0	82.4	82.6	82.5	83.3	83.4	82.6	84.0	83.8	83.5	84.5	84.5	84.3	83.7	83.4	82.6	82.5	82.6	82.6	82.6	82.5	82.7	83.2
23		82.8	83.0	83.4	83.0	84.4	83.0	83.7	83.3	83.4	83.5	83.3	83.3	83.6	82.5	83.2	82.2	81.4	80∙1	80.6	80.5	80.5	79.9	80.4	80∙6	82.4
24																										
25		81.5	82.2	82.5	82.7	82.8	82.4	81.5	81.9	82.6	81.9	83.3	83.8	82.5	83.0	83.4	82.7	82.4	80.7	80.5	80∙8	8o·6	80.2	79·I	79·I	81.9
		l.	I	I	1	ł .	1	Ī.	1			1	1			1	1	1		1		1	l	I .		
26		79.2	80.3	81·o	80.7	81.3	82.4	82.6	82.3	82.3	83.5	83.0	83.5	83.4	83.5	82.6	83.4	83.8	84.3	84.3	83.8	83.8	83.2	81.2	80.5	02.5
27 28		83.4	83.6	83.6	83.6	83.9	83.1	83.4	83.5	83.7	83.8	84.2	84.1	84.4	83.7	82.8	83.6	83.4	83.1	82.9	02.0	01.9	86.5	86.5	82·3 86·9	85.3
29		83.2	83.5	83.6	83.3	83.2	83.5	83.7	84.3	84.6	84.9	85.2	86.5	86.8	86.6	86.6	86.5	80.1	80.1	80·I	80.2	80.3	82.3	80.8	82.7	84.4
30		86∙9	85.5	84.8	84.7	84.9	84.2	83.7	83.2	83.6	84.2	84.7	85.5	85.4	85.3	84.6	84.2	83.7	83.4	93.0	03.4	03.4	03.3	02.0	82.7	4
		0				0	0	0	0			1_						00.5	90.6	80.8	82.7	82.7	82.7	82.8	82.8	83.2
31		82.0	82.4	82.6	83.1	83.1	82.9	82.0	83.3	83.2	83.8	83.2	84.4	84.8	84.3	84.2	93.9	02.5	02.0	02.0	02 /	02 /	<u> </u>		82.8	3 -
Mean		83.3	83.3	82.2	82.2	82.2	82.2	93.1	82.2	82.4	82.8	8412	84.4	94.77	84.6	84.5	84.2	84.0	83.6	83.4	83.4	83.3	83.1	83·1	83.1	83.6
	•••	V3 3	03.3	03.3	3.2	3 3	3 2	30 1	23 3	3.4	03.0	04.2	94.4	02.7	04.0	94.2	04 3	34 0	350	-57	-			<u> </u>	1 1	
G.M.T.		1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
1				١,	٦.	1	1	, '	1	J.	1	١	-10011	٦,	1 -4.	٠,٠				1	1	!		l	j '	1 !

Readings in degrees absolute, at exact hours, Greenwich Mean Time.

310. Gahirelveen (Valencia Observatory): North Wall Screen: he (height of thermometer bulbs above ground) = $1 \cdot 3$ metres.

November, 1923.

																							emb	•	
Day.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
1 2 3 4 5	81.9	82·3 85·3 81·5	82.2	81.7	81·9 85·5 81·5	81·1 85·6 81·7	81·6 85·9 80·7	82·0 86·0 80·9	82·5 86·1 80·6	82·8 85·1 81·8	83·0 84·5 81·7	84·1 81·7	84·9 84·0 82·6	83·6 82·6	84·8 83·6 82·1	a. 81·6 84·8 82·5 82·4 80·7	84·8 81·9 81·9	84·8 81·7 81·5	81·5 81·5	84·9 81·5 81·3	84·9 82·0 81·0	81.2	85·0 82·0 80·2	80.2	83.6
6 7 8 9 10	78·9 80·8	81.1	12 .	79·6 81·3	80·1 82·0 81·8	81·4 81·6	79·9 81·6 81·0	80.9	80·4 80·9 81·3	80·1 81·3 81·5	80·8 81·4 82·1	81·7 82·2	81·8 82·2	80·6 81·3 82·3	80·9 81·2 82·1	81·3 80·5 82·0	81·3 80·9 81·4	80.5	80·4 80·8	81·4 80·2 80·6	81·3 79·9	76·4 81·4 79·6 79·9 79·0	81·3 80·1 79·4	77.0 81.2 80.4 79.0 78.4	81.1
11 12 13 14 15	84.6	77.9 83.3 85.0 80.3 79.9	77·8 83·5 85·0 80·6 80·9	77·7 83·4 85·1 78·8 81·7	83·7 85·2	83·6 85·0 78·2	78·5 83·6 85·0 79·3 81·5	83·7 84·9 78·2	83·7 84·9	83·8 85·0 78·6	83·9 85·0 70·8	84·2 85·1 79·8	84·5 85·3 80·4	82·6 84·5 85·4 80·3 82·2	84·5 85·0 79·7	84·2 84·4 79·6	84·1 83·4 78·3	82·5 84·1 82·8 79·3 81·3	83·9 82·5 79·4	84·0 81·3 79·5	84·0 80·5 77·8	82·7 84·2 80·9 77·7 80·8	84·3 80·5 78·1	84·4 80·5 78·7	79.3
16 17 18 19 20	78.7	79·5 79·6 78·7 79·5 78·1	79.2	77.8	78·2 78·5	77·7 77·6	78·4 77·4 78·9 79·4 78·1	78·6 79·2	79.4 80.1	78·2 79·9	77·7 81·0	77·8 80·5	79:3 80:6 70:6	79.4 80.8 80.7	79·6	79·2 79·7	79·6 80·7 79·4	78·4 80·1 78·9	78·5 79·5 79·2	79·3	78·5 79·5 78·5	79·2 77·6	78·5 79·1 78·1 78·5	77°4 78°1	78·7 79·4 79·1 78·6
21 22 23 24 25	73·6 74·9	73·5 75·3		73·5 75·1	72·9 75·I	72.8	75·8 72·9 74·9 73·4 72·7	73·0 74·7	73·7 75·0	75·7 76·2	76·7	77·5	78·3 77·9	79·6 78·1 77·9 76·3 78·0	77·8 77·8	77.4	76·4 76·2	76·5 75·6 75·6 72·8 78·6	72.2	75·I 74·6 71·5	75·I 74·I 70·9	74·2 74·9 73·5 71·4 78·6	74·9 73·1 71·4	73·6 74·4 72·9 70·5 78·4	75·1 75·5 73·2
26 27 28 29 30	75·4 75·4 72·5	76·3	72·6 74·6 75·6 71·5	73·3 74·4 75·6 71·5	74·4 76·3 71·4	72·5 73·7 75·5 71·2	76·1	72·8 73·5 75·8 71·6	73·9 73·4 76·5 72·2	73·7 76·8 73·9	76·2 75·1 76·4 75·8	76·3 75·3 77·4	76·8 75·7 78·7 78·3		77·1 75·8 78·8 79·7	77·2 75·4 78·3 80·1	77·2 74·6 77·4 80·2	74°4 76°5 80°5	77·8 75·1 76·6 80·9	74·8 75·4 81·3	77 ² 74 ⁴ 74 ³ 81 ⁹	74·2 81·6	73·7 81·4	72·5 80·6	76·7 75·3 74·8 76·2 76·4
Mean	78.4	78.5	78.5	78.4	78.4	78-2	78.2	78.2	78.5	79·I	79.6	80.1	80.5	80.6	80.4	80.1	79.7	79.4	79.2	79.0	78.7	78.6	78.4	78.3	79.1
		45.0							TY7 11	· C		1.	1.9	o t =	.00							Dac	emb	ar. 19	123.
311. Cahi	ircive	· ·	,													1 a	1 a	1 a.	1 a.	1 a.	1 a.	Dec	embe	er, 19	923.
311. Cah	a. 80·4 80·5 79·3 81·3	a. 79·8 79·6 79·1 80·6	a. 79·8 79·6 79·5	79.5 79.2 78.6 80.6	a. 79·6 79·3 78·9	a. 79·2 79·2 79·5 79·7 79·7	a. 79·5 78·7 79·3 79·8 79·5	a. 78·9 77·7 78·6 79·1 80·0	a. 78·9 79·1 78·3 80·0 80·2	a. 78·8 78·2 77·9 79·7 80·4	a. 79·9 79·8 79·5 80·4 79·9	a. 80·3 78·8 79·9 81·3 80·1	a. 80·7 79·5 79·8 80·4 80·5	a. 81·1 79·1 79·8 80·4 80·8	a. 80·8 80·0 79·4 79·9 80·7	79·5 78·8 79·5 81·2	79·2 81·2	79·3 79·3 78·8 80·9	80·0 79·8 78·9 80·5	79·9 80·4 78·4 80·7	78·7 80·9 78·0 80·6	a. 80·6 79·4 81·5 78·3 80·8	a. 80·6 78·4 82·0 78·9 80·3	a. 80·3 78·8 81·5 78·6 79·1	a. 80·0 79·3 79·5 79·8 80·2
1 2 3 4	a. 80·4 80·5 79·3 81·3 79·9 80·4 81·0 80·5	a. 79.8 79.6 79.1 80.6 79.6 80.0 81.7 80.9	a. 79·8 79·6 79·5 81·2 79·4	a. 79.5 79.2 78.6 80.6 79.3 78.2 82.5 80.4	a. 79.6 79.3 78.9 79.8 79.5 76.9 82.7 80.0	a. 79·2 79·2 79·5 79·7 79·7 77·0 83·1 80·4	a. 79.5 78.7 79.3 79.8 79.5 76.4 82.8 79.0	a. 78.9 77.7 78.6 79.1 80.0 75.0 82.8 79.6 78.2	a. 78·9 79·1 78·3 80·0 80·2 75·2 82·9 78·8	a. 78·8 78·2 77·9 79·7 80·4 75·3 83·0 79·5	a. 79.9 79.8 79.5 80.4 79.9 77.4 82.5 78.8	a. 80·3 78·8 79·9 81·3 80·1 78·7 81·9 79·8 78·8	a. 80·7 79·5 79·8 80·4 80·5 79·2 81·5 79·7 80·0 83·3	a. 81·1 79·1 79·8 80·4 80·8 79·4 81·6 79·6 80·9 83·3	a. 80·8 80·0 79·4 79·9 80·7 79·5 81·6 79·2 81·1 83·3	80·5 79·5 78·8 79·5 81·2 79·9 82·1 78·7 81·0 83·2	79.9 79.5 78.9 79.2 81.2 79.9 82.1 78.3 81.2 82.8	79·9 79·3 79·3 78·8 80·9 80·3 82·3 79·1 81·5 82·7	81.0 80.0 79.8 78.9 80.5 80.4 81.9 79.3 81.6 82.8	80·9 79·9 80·4 78·4 80·7 80·3 82·0 78·7 81·6 82·8	79·9 78·7 80·9 78·0 80·6 80·2 81·6 77·5 81·7 82·9	a. 80.6 79.4 81.5 78.3 80.8 80.2 81.5 77.4 81.9 82.8	a. 80·6 78·4 82·0 78·9 80·0 81·2 77·9 82·2 82·8	a. 80·3 78·8 81·5 78·6 79·1 80·4 81·0 78·0 81·9	a. 80·0 79·3 79·5 79·8 80·2 78·7 82·0 79·3 79·7
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TEMPERATURE: ANNUAL MEANS OF HOURLY VALUES.

From readings in degrees absolute at exact hours, Greenwich Mean Time.

312. Cahirciveen (Valencia Observatory): North Wall Screen: ht = 1.3 metres.

1923.

1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
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82.51	82.45	82.38	82.30	82 · 26	82.27	82 · 47	82.80	83.19	83 · 56	8 3 ·98	84.29	84.51	84 · 57	84 · 55	84 · 42	84 · 18	83.81	83.47	83.21	82.98	82.83	82.69	82.60	83.26

TEMPERATURE: MONTHLY MEANS AND DIURNAL INEQUALITIES.

The departures from the mean of the day are adjusted for non-periodic change.

313. Cahirciveen (Valencia Observatory): North Wall Screen: $h_t = 1.3$ metres.

1923.

1 1	1	Hour.	G.M.T.	1			1	1		1	1	1	1	1	[1	1	1	1						1
Month	Mean.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.
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1.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.
Jan. 2	281.32	-0.20	-0.35	-0.35	-o·35	-0.42	-0.21	-0.55	-0.54	-0.48	-0.30	+0.01	+0.33	+0.21	+0.61	+o·56	+0.53	+0.30	+0 ⋅26	+o·28	+0.27	+0.18	+0.13	+0.01	-0.04
Feb. 2	280.97	-0.22	o·26	-0.39	-0.52	-0·50	-o·53	-0.66	-0.66	-0.51	-0.19	+0.23	+o.69	+0.95	+0.92	+o∙86	+0.72	+0.53	+0.30	+o·02	+0.03	-0·12	-0.23	-0·24	-0.23
Mar. 2	281.15	-o⋅88	- I ·04	-1.13	-1.18	-1.37	-1.34	-1.10	-1.17	-0.30	+0.30	+1.04	+1.42	+ r · 62	+1.76	+1.83	+1.60	+1.35	+0.77	+0.17	-0.12	-0.28	-o·38	-o·61	-0.71
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Apr. 2	81.12	T ·00	_ r · 28	T · 5 T	T .75	_T.87	_1.06	_ T.60	-0.68	1.0.22	1.0.66	J. T. 24	+1.53	L T .772	± x.77	עלי. 1 ו⊥ ⊥	L T.74	L T . 4 T	ـــــــــــــــــــــــــــــــــــــ	اعم. مدا	±0.03	-0.16	-0.28	-0.58	-0.72
May 2	82.00	-1.22	_ T : 28	T.42	- 1.46	1.40	1.20	0.63	-0 00	10.23	1 0.66	1 24	T 1 33	T 1 /2	1.60	1 7.67	T 1 /4	1 7.27	1 7.04	0.55	10.00	-0.46	-0.76		7.73
Inay 2	02.90	-1.23	-1.20	-1.43	1.40	1.40	-1.29	-0.03	-0.11	+0.24	+0.00	+0.93	+1.23	+1.41	+ T.02	+1.01	+ 1.50	+1.37	+1.04	+0.55	+0.09	-0.40	-0.70	-1.01	-I·I2
June 2	:05.09	-0.93	-1.14	-1.24	-1.91	-1.31	-1.19	-o·79	-o·32	+0.18	+o·55	+0.99	+1.10	+1.38	+1.43	+1.44	+147	+ I·27	+0.83	+0.33	-0.00	-0.41	-0.05	-0.72	-o·77
		_											1							_	_				
July 2	288 66	-1.38	- I ·44	-1.21	-1.53	-1.65	-1.34	-o·66	+0.10	+0.48	+0.78	+1.12	+1.49	+1.65	+ 1 ·65	+1.74	+1.68	+1.20	+0.92	+o·38	-0.08	0.63	-0.90	-1.08	-1.23
Aug. 2	87.68	-1.07	-1.03	-1.10	-1.01	-1.00	-1.15	-0.75	-0.14	+0.31	+0.61	+1.08	+1.20	+1.43	+1.44	+1.38	+1.24	+1.08	+0.60	+0.17	-0.31	-0.47	-0.65	-o·85	-r·00
Sept. 2	85.74	-o.8i	-0·84	-0.97	-0.00	-1.02	-0.08	-0.80	-0.32	+0.26	+0.55	+0.73	+ T .00	+ T · 23	+1.35	+ T · 26	I + T · T 6	+0.78	+0.37	+0.02	-0.22	-0.10	-0.35	-0.21	-0.66
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Oct. 2	82.62	0.40	0.40	-0.41		0.26	0.45	0.50	0.00	0.70	10.01	10.00	10.80	1.00	10.06	1 0.00	10.50	10.45	1.0.01	0.78	-0.22	-0.24	_0.46	-0.46	-0.44
Nov.	מים מיבו	-0 40	-0 40	-0 41	-0.44	-0.30	0.45	0.09	-0.30	-0.19	+0.21	-0.55	+0.02	+1.00	+0.90	+0.92	+0.70	TU-45	+0.01	10.70	10.07	-0 24	-0 40	-0.40	-0.44
Nov. 2	V. A. 09	-0.71	-0.50	-0.59	-0.09	-0.04	-0.99	-0.85	-0.84	0 ⋅53	+0.01	+0.55	+1.08	+1.47	+1.04	+1.30	+1.10	+0.70	+0.37	+0.10	+0.01	-0.30	-0.41	-0.59	-o.77
Dec. 2	81.53	-0.15	−0. 05	-0.10	-0.25	-0.24	-0.51	-0.31	-0.42	-0.30	-0.31	+0.08	+0.34	+0.62	+0.71	+0.65	+0.46	+0.59	+0.18	+0.02	-0.0 7	-0.58	o·23	-0.22	-0.29
 																									
Year 2	83.26	-o·75	-o·81	o·88	-0.96	-1.00	-0.99	-0.79	-0.46	-0.07	+0.30	+0.72	+1.03	+1.25	+1.31	+1.29	+1.16	+0.92	+0.55	+0.21	-0.05	–o∙28	-0.43	-0.57	-o·66
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ABSOLUTE EXTREMES OF TEMPERATURE FOR EACH DAY.

Maximum and minimum for the interval 0 h. to 24 h., Greenwich Mean Time.

314. Cahirciveen (Valencia Observatory) : North Wall Screen : $h_t = 1 \cdot 3$ metres.

1923.

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Month	Ja	ın.	Fe	eb.	М	ar.	Ap	ril	M;	ay	Ju	ne	Ju	ly	Aı	ug.	Se	pt.	0	ct.	No	ov.	D	ec.
Day.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
1 2 3 4 5	a. 84·6 84·6 82·3 82·5 83·6	a. 75.6 80.4 80.2 80.2 78.5	a. 85·5 85·0 84·3 82·7 83·1	a. 84·4 82·5 81·5 80·1 81·6	a. 83·3 82·3 83·2 81·6 84·5	a. 78·5 79·1 79·5 76·2 80·8	a. 83·5 83·6 82·4 82·8 82·1	a. 74·3 74·9 78·6 79·5 78·5	a. 87·3 90·3 87·5 87·5 87·7	a. 82·5 82·1 84·1 84·0 83·1	a. 86·9 89·3 88·5 87·0 85·6	a. 80·2 79·9 82·2 83·4 82·8	a. 89·7 89·3 90·2 90·5 90·3	a. 83·5 86·5 86·2 86·5 87·2	a. 90·9 89·0 90·4 91·3 91·6	a. 85·8 85·9 85·6 86·5 87·2	a. 87·1 87·6 87·6 87·8 89·0	a. 82·3 80·1 83·8 84·2 85·9	a. 86·6 86·5 86·2 84·8 86·1	a. 84·4 82·9 81·9 81·1 83·3	a. 84·9 85·1 86·1 82·8 81·6	a. 81·0 81·1 81·4 80·0 77·1	a. 82·5 80·5 82·2 81·4 81·3	a. 78·8 77·5 77·4 77·9 78·9
6 7 8 9 10	84·0 84·3 84·3 81·8 80·5	78·6 83·4 80·9 77·3 77·4	83·3 81·9 80·7 83·5 83·6	76·4 76·4 76·1 78·2 78·7	83·9 83·2 83·5 83·3 81·1	80·9 80·6 79·0 76·8 78·6	82·4 82·7 84·9 82·5 80·1	76·5 77·8 74·6 78·8 75·7	83·7 84·4 85·3 83·4 84·0	79·6 77·2 80·4 79·6 78·7	86·7 87·1 88·4 87·6 87·6	83·1 81·7 84·4 84·9 83·7	94.5 91.8 90.8 91.9 93.8	87·0 87·5 86·7 87·9 86·2	90·0 90·7 90·8 91·9	87·4 87·3 87·9 87·4 84·9	89·0 88·3 88·5 88·1 87·7	85·8 80·7 79·7 85·4 81·4	86·3 87·1 87·9 87·9 85·6	83·2 84·7 84·2 84·4 83·7	81·4 81·5 82·1 82·4 81·2	76·0 77·0 79·5 79·0 76·6	80·5 83·1 81·0 82·2 83·4	74·5 80·4 77·3 76·7 81·9
11 12 13 14	80·3 79·2 82·6 83·0 83·1	74·9 73·7 78·6 79·8 79·4	82·3 83·7 84·0 82·6 82·9	79·7 79·6 78·5 74·9 79·1	83·1 84·3 83·0 84·3 81·7	76·5 80·0 76·2 75·1 77·0	84·0 84·7 80·6 83·0 83·5	76·3 76·1 77·3 78·3 80·8	81·9 81·4 82·7 81·8 83·9	77:4 77:4 77:7 79:9 79:4	87·2 87·2 86·3 88·2 86·5	83·8 83·7 83·7 83·7 83·4	92·2 91·9 94·1 91·5 91·8	83·4 86·2 86·9 86·7 86·9	92·2 90·3 92·0 90·2 90·0	83·4 88·4 88·4 86·8 86·1	89·4 90·0 88·0 86·3 84·9	79·9 86·5 84·5 81·6 81·4	85.0 83.9 84.0 83.3 83.9	82·8 81·3 80·0 76·3 75·9	82·8 84·6 85·4 80·6 82·4	77·5 83·0 80·4 77·1 78·7	83·4 83·4 80·4 82·8 81·5	82·3 79·6 75·7 79·2 79·6
16 17 18 19 20	82·0 82·4 81·5 83·7 82·7	80·4 79·5 74·9 81·2 79·4	82·2 84·1 83·3 80·9 80·7	78·9 78·6 78·7 76·4 73·7	82·2 83·5 83·6 81·7 83·2	78·5 77·5 76·3 77·0 74·9	85·5 85·1 84·0 84·8 84·6	81·3 82·9 78·3 77·5 79·6	83·6 85·4 84·6 85·1 85·3	79·6 80·1 81·6 81·4 82·3	85·9 87·4 87·7 87·1 87·7	83·2 82·6 84·1 83·4 83·9	91·0 90·3 90·3 91·8	86·5 85·4 85·3 86·4 88·4	90·2 90·4 89·5 90·0 90·1	85·5 86·8 86·1 86·5 87·0	86·1 86·0 85·7 86·9 86·9	81·9 81·9 82·5 83·0 84·4	85·5 85·4 87·5 87·6 86·0	81·6 83·3 82·7 81·4 82·2	82·1 80·2 81·1 80·9 80·1	77·4 77·0 77·0 77·4 77·4	83·2 83·5 83·5 81·5 79·5	80·8 81·8 80·0 78·3 75·0
21 22 23 24 25	83·4 83·0 82·4 83·4 82·6	79·0 80·6 77·1 80·6 79·8	80·4 79·3 82·3 83·7 82·6	76·8 74·9 78·4 79·7 80·2	83·2 82·7 84·0 84·2 84·6	75·6 77·8 78·4 77·9 81·5	80·5 85·7 83·6 83·8 84·5	77·1 75·9 77·7 75·3 81·5	86·9 87·4 85·2 84·5 84·0	82·5 82·6 81·0 77·4 80·0	87·3 89·5 89·3 89·4 88·8	85·1 85·1 86·4 86·3 86·0	92·1 91·9 90·1 90·6 90·6	88·7 88·4 87·3 87·0 87·3	88·9 88·8 90·9 88·3 89·6	84·5 84·3 84·3 83·5 83·7	87·7 86·1 85·9 85·9 86·5	85·4 82·9 80·1 79·9 84·1	83·7 84·7 84·6 83·9 84·0	81·4 81·8 79·8 79·1 79·1	79·9 78·3 78·2 76·3 79·1	73·4 72·7 72·5 70·5 70·4	84·4 84·3 83·2 83·6 84·2	75·4 82·4 80·5 80·2 80·0
26 27 28 29 30	82·4 82·6 82·8 83·7 84·3	81·5 80·4 79·3 82·7 83·3	84·3 82·0 82·5 —	80·0 79·7 77·9 —	84·9 85·6 84·8 83·7 83·8	81·9 81·5 80·9 81·9 78·9	83·0 84·2 84·2 85·5 86·0	79·0 78·2 79·5 81·0 83·5	83·7 85·4 85·5 88·3 86·0	79·2 80·0 81·3 79·6 81·3	88·6 89·6 90·9 89·5 88·6	85·4 84·7 83·6 85·3 84·5	90·1 90·9 90·2 90·0 90·7	86·1 86·1 85·9 86·4 86·0	89·5 87·6 87·9 86·0 86·9	85·0 84·2 84·2 82·0 83·4	87·9 88·3 88·4 90·4 89·9	85·5 86·6 84·2 85·9 87·2	83·9 83·4 84·5 86·9 87·1	79·1 79·4 81·7 82·3 82·7	79·0 78·1 76·3 78·9 82·2	73·1 71·9 73·4 72·5 70·7	84·5 84·9 84·1 83·6 83·8	82·2 81·6 78·3 78·4 82·1
31 Mean	85·2 82·9	83·o 79·4	82 · 8	 78·6	83.4	75·9 78·4	83.6	78·2	90·3	81.5	<u> </u>	83.8	91.1	84·7 86·5	87·4 89·8	82·4 85·6	87.6	83.3	8 ₄ ·8 8 ₅ ·4	82.4	81 · 2	- 76·4	84.2	79.3

315. Cahirciveen (Valencia Observatory): North Wall Screen: h_t (height of thermometer bulbs above ground) = $1 \cdot 3$ metres.

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Day.	ı.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure
1 2 3 4 5	% 89 93 79 75 95	% 90 95 78 77 93	% 89 95 78 76 95	% 89 95 79 80 96	% 88 95 78 79 91	% 89 92 80 79 93	% 89 91 76 78 91	% 90 85 77 82 84	% 89 79 77 79 69	% 87 78 75 84 71	% 87 75 73 81 71	% 87 70 71 82 68	% 90 79 71 82 69	% 89 80 73 79 65	% 95 72 74 81 68	% 95 75 73 78 66	% 93 75 72 84 66	% 92 76 76 84 67	% 92 77 73 87 70	% 96 76 79 91 73	% 95 77 71 91 68	% 96 84 72 92 76	% 93 86 73 92 71	% 96 80 69 93 74	% 90·8 82·8 74·7 82·3 77·5	mb. 9·3 10·0 8·4 9·0 8·1
6 7 8 9	69 99 96 83 68	73 97 97 87 71	75 97 95 78 74	74 97 84 77 64	76 97 79 74 66	73 97 78 63 69	76 95 72 62 71	79 96 72 63 67	78 96 77 71 67	80 97 77 72 73	77 99 72 68 76	78 99 71 77 66	79 99 75 80 61	80 99 81 77 71	84 96 76 84 73	85 99 76 73 69	92 99 79 71 73	93 99 83 76 72	93 97 79 71 67	96 97 82 69 75	97 96 82 76 77	99 97 89 79 73	97 99 92 66 76	97 96 83 65 68	82·9 97·5 81·4 73·8 70·2	9·0 12·3 9·2 7·1 6·5
11 12 13 14	69 89 89 97 76	69 91 91 96 77	72 89 91 96 79	66 93 93 96 81	67 91 94 95 81	81 91 94 95 81	80 91 95 93 81	71 93 95 95 82	76 91 95 91 83	72 93 96 88 87	72 91 93 81 91	73 91 95 73 92	72 88 97 71 95	76 86 97 71 99	81 82 99 70 96	81 86 99 70 96	81 81 97 73 93	79 79 97 76 95	81 84 100 72 95	83 85 100 73 96	87 84 100 72 95	88 83 100 74 93	89 83 97 73 95	91 83 97 75 95	76·9 87·6 95·6 82·4 88·5	7·0 6·9 10·3 9·2 11·0
16 17 18 19 20	95 95 90 92 74	95 95 91 92 65	96 95 87 93 74	96 95 88 95 76	96 95 88 93 78	97 95 88 93 73	95 95 90 93 72	95 96 89 93 77	96 95 91 95 77	96 96 91 92 79	96 93 91 92 73	97 91 93 71	97 91 78 91 71	96 93 68 91 71	96 93 69 89 71	93 93 72 89 76	92 95 79 93 73	89 97 72 95 75	91 96 72 96 79	91 87 78 96 80	93 83 80 96 80	95 85 84 95 82	95 86 85 89 87	95 90 86 82 85	94.7 92.8 83.3 92.5 75.7	10·3 10·1 7·9 10·9 8·1
21 22 23 24 25	85 87 91 91 87	80 82 91 91 84	79 87 91 89 84	79 87 91 93 83	84 87 91 89 86	92 85 91 93 89	93 75 94 93 89	95 81 94 95 93	93 85 95 93 93	93 91 94 93 91	91 89 97 91 93	88 81 93 89 92	87 80 95 85 87	86 79 95 88 88	87 83 93 83 88	82 87 92 86 89	81 83 92 87 93	86 84 91 88 85	87 85 91 79 83	87 85 91 78 84	84 87 91 83 82	87 89 93 83 82	88 87 93 89 85	87 91 93 87 85	86·7 84·8 92·6 88·3 87·3	10·0 9·5 10·1 9·6
26 27 28 29 30	84 83 91 86 92	84 84 91 87 93	83 84 93 86 93	84 83 93 83 92	81 86 91 86 91	83 84 91 86 92	77 83 91 86 92	81 85 92 87 93	79 79 91 87 92	82 81 89 88 91	82 78 92 91 91	79 82 87 93 81	77 83 85 95 85	79 84 82 96 87	78 84 81 96 91	78 83 82 96 92	82 82 86 96 93	83 83 85 96 93	81 79 86 97 95	85 83 87 95 97	84 83 88 95 97	85 83 87 95 97	84 95 87 93 95	83 91 86 93 93	81·6 83·4 88·2 91·1 92·0	9·4 9·4 11·2 11·7
31	93	93	93	93	96	96	96	96	95	92	91	91	91	91	93	95	95	96	93	91	93	92	91	92	93.3	12.3
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	100.2	86.5	86.6	86.3	86 · 1	86.5	85.6	86.2	85.6	86 · 1	85.1	83.6	83 · 4	83.8	84.1	84.1	84.9	85.2	84.8	85.7			87.5		·	†9.5
apour ressure*	mb.	mb.	mb.	mb.	96·1	mb.	mb.	mb.	mb.	mb.	mb.		mb.	mb.	mb.	84·1 mb. 9·5	mb.	mb.	mb.	mb.	mb.	mb.	-	mb.	mb.	1 19.5
ressure*	mb. 9·3	mb. 9·1	mb. 9·2	mb. 9·1	mb. 9·1	mb. 9·2 /ator	mb. 9⋅0 y):	mb. 9·0	mb. 9·1 th V	mb. 9·2 Vall	mb. 9·3	mb. 9·3 en: h	mb. 9·4	mb. 9·5	mb. 9·5 metr	mb. 9·5	mb. 9•5	mb. 9·5	mb. 9°5	mb. 9·6	mb. 9·6	mb. 9·6	mb. 9·5	mb. 9·4	mb. ‡9·3	y, 1923
ressure*	mb.	9·1	mb. 9·2	mb.	9·1	mb. 9·2	mb. 9·0	mb. 9 ∙0	mb. 9∙1	mb. 9·2	mb.	mb. 9·3	mb. 9·4	mb. 9·5	mb. 9·5	mb. 9·5	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb. 9.4	mb. ‡9·3	mb. 13·0 12·2 9·9
6. Cahire	mb. 9·3	mb. 9·1 (Va 92 93 83	mb. 9·2	mb. 9·1 ia 0	mb. 9·1	mb. 9·2 /ator	mb. 9·0 (y): % 96 95 88 85	Mb. 9.0 Nor % 95 93 87 85	mb. 9·1 th V	mb. 9·2 Vall % 95 96 83 90	mb. 9·3 Scree % 96 95 81 85	mb. 9·3 en: ha	mb. 9·4 = : % 96 96 81 71	mb. 9·5 1·3 1 % 96 91 87 70	mb. 9·5 metr % 96 90 81 73	mb. 9·5 es. % 95 89 85 74	% 93 90 76 75	mb. 9·5 % 93 89 77 76	% 9.5 9.5 89 88 78	% 93 89 88 76	% 93 90 84 76	% 9.6 9.6 9.6 9.2 87 82 77	mb. 9·5 % 93 85 82 79	% 93 83 87 79	mb. ‡9·3 abruar : % 94·3 91·8 83·3 80·5	mb. 13·0 12·2 9·9 8·9 10·3 8·0 7·6
6. Gahire 1 2 3 4 5 6 7 8 9	mb. 9·3 9·3 9·3 9·3 9·3 9·5 8·5 8·7 7·7 9·1 7·4 8·7 8·6 8·6	% 92 93 83 87 78 89 76 88 85	mb. 9·2 slenc % 95 93 85 85 78 91 82 83 85	mb. 9·1 % 95 95 83 86 79 89 82 81 84	mb. 9·1	mb. 9·2 /ator % 96 93 83 85 76 91 86 83 77	mb. 9·0 9·0 % 96 95 88 85 77 81 77 82 79	Mb. 9·0 Nor % 95 93 87 85 85 79 76 85	mb. 9·1 th V % 95 82 89 92 86 74 81 76	mb. 9·2 Vall % 95 96 83 90 91 81 73 77 75	mb. 9·3 Scree % 96 95 81 85 92 82 65 83 82	mb. 9·3 en: h % 96 95 83 72 93 77 66 85	mb. 9.4 % 96 96 81 71 93 75 66 82 82	mb. 9·5 L·3 I % 96 91 87 70 93 75 64 87 85	mb. 9·5 metr % 96 90 81 73 93 79 83 89 85	mb. 9·5 % 95 89 85 74 93 72 85 68 80	% 9.5 % 93 90 76 75 92 83 85 64 83	% 93 89 77 76 92 79 89 67	% 9.5 % 989 88 78 92 79 89 73 80	% 9.6 9.6 93 89 88 76 92 79 89 77	% 93 90 84 76 92 82 83 76	% 92 87 82 77 92 77 88 77	mb. 9.5 % 93 85 82 79 93 81 91 78	mb. 9·4 F(93 83 87 79 92 75 88 82 80	mb. ‡9·3 bruar : % 94·3 91·8 93·3 80·5 87·4 82·2 79·7 80·0 80·7	mb. 13·0 12·2 9·9 8·9 10·3 8·0 7·6 7·3 8·8 8·8 8·5 10·7 10·9 7·9
1 2 3 4 5 6 7 8 9 10 11 12 13 14	mb. 9·3 1 1 1 1 1 1 1 1 1	mb. 9·1 (Va 9·2 9·3 8·7 7·8 8·9 9·3 8·9 9·3 9·5 9·2	mb. 9·2 9·2	mb. 9·1	mb. 9·1	mb. 9·2 9·2 // ator % 96 93 85 76 91 86 83 77 72 79 93 95 95 95	mb. 9·0 9·0 9/0 9/0 9/0 9/0 9/0 9/0	% 95 93 87 85 85 77 77 75 93 96 95	mb. 9·1 th V % 95 82 89 92 86 74 81 76 79 77 92 95 93	mb. 9·2 Vall % 95 96 83 90 91 81 73 77 77 71 96 96 91	mb. 9·3 Screet % 96 96 95 81 85 92 82 65 83 82 79 72 95 97 91	mb. 9·3 en: ha % 96 95 83 72 93 77 66 85 83 78 70 95 96 76	mb. 9·4 9·4 9·4 9·4 9·4 9·6 96 8i 7i 93 75 66 82 82 7² 67 95 93 74	mb. 9·5 9·5 1·3 1 % 96 91 87 70 93 75 64 87 85 72 70 96 89	mb. 9.5 metr % 96 90 81 73 93 79 83 89 85 69 68 95 92 73	mb. 9·5 es. % % 95 89 85 74 93 72 85 68 80 70 73 95 89	% 93 90 76 75 92 83 85 64 83 73 79 92 88	mb. 9·5 %6 93 89 77 76 92 79 89 67 79 78 83 92 87	mb. 9·5 % 9·3 88 88 78 92 79 85 91 91 78	mb. 9·6 % 9.3 89 88 76 92 79 80 87 79 80 87 79 75	mb. 9·6 % 93 90 84 76 92 82 83 76 78 86 87 92 91	mb. 9·6 % 92 87 82 77 88 77 77 88 87 92 91 83	% 93 85 82 79 93 81 91 78 79 86	mb. 9·4 F(6) 93 83 87 79 92 75 88 80 86 91 95 94 81	mb. \$\dagger*29\cdot3 94\cdot3 91\cdot8 83\cdot3 80\cdot5 87\cdot4 82\cdot2 79\cdot7 80\cdot0 80\cdot7 79\cdot3 93\cdot4 93\cdot3 84\cdot4	13.0 12.2 9.9 8.9 10.3 8.0 7.6 7.3 8.8
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	mb. 9·3 1 1 1 1 1 1 1 1 1	mb. 9·1 (Va 9/2 93 83 78 89 76 88 85 89 93 95 92 80 86 80 87 71	mb. 9·2 llenc	mb. 9·1	mb. 9·1	mb. 9·2 9·2 9·2 9·2 9·2 9·2 9·2 9·2 9·2 9·2 9·3 8·3 7·7 7·2 9·3 9·5 9·5 8·9 8·9 8·9	mb. 9·0 9/0 9/0 9/0 9/0 9/0 9/0 9/0	mb. 9·0 Nor % 95 93 87 76 85 77 75 93 96 95 92 88 91 82 78	mb. 9·1 th V % 95 95 95 82 92 86 74 81 76 79 92 95 93 88 93 88 83 81	mb. 9·2 Wall % 95 96 83 90 91 81 73 77 75 77 96 96 91 93 88 89 83 83	mb. 9·3 Screen % 96 95 81 85 92 82 65 83 82 79 95 97 91 93 92 93 77 78	mb. 9·3 en: ha % 96 95 83 72 93 77 66 85 83 78 70 95 96 76 93	mb. 9·4 9·4 9·6 96 96 81 71 93 75 66 82 82 72 67 95 93 84 92 89 93 87	mb. 9·5 9·5 1·3 I % 96 91 87 70 93 75 64 87 85 72 70 96 89 74 88 94 93 78 77	mb. 9·5 metr % 96 90 81 73 93 89 85 69 68 95 92 73 91 97 77 73	mb. 9·5 % 95 89 85 74 93 72 88 80 70 73 95 89 74 88 90 97 69 97	mb. 9·5 % 93 90 76 64 83 73 79 92 88 75 83 85 83 86 67	mb. 9.5 9.6 93 89 77 79 89 67 79 79 79 77 77	mb. 9·5 % 93 89 88 78 92 79 85 91 78 90 76 95 72	% 9.6 93 93 89 77 79 80 87 92 90 77 95 90 77 96 72 83	mb. 9·6 % 93 99 84 76 78 88 87 92 91 75 86 80 96 75 84	mb. 9·6 % 92 87 77 77 88 77 77 83 87 92 91 83 87 92 91 75 85 87	mb. 9·5 % 93 85 82 97 93 81 78 79 86 93 95 93 84 78 96 73 87	mb. 9·4 For the second	mb. \$\frac{1}{2}9\cdot 3\\ 94\cdot 3\\ 91\cdot 8\\ 83\cdot 3\\ 80\cdot 5\\ 87\cdot 4\\ 82\cdot 2\\ 79\cdot 7\\ 80\cdot 7\\ 93\cdot 4\\ 87\cdot 5\\ 85\cdot 4\\ 91\cdot 2\\ 79\cdot 4\\ 77\cdot 2\\ 77	mb. 13.0 12.2 9.99 10.3 8.00 7.6 7.3 8.8 8.8 8.5 10.7 10.9 9.5 9.2 10.5 8.3 7.2 7.5 7.1 9.0 9.8
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	mb. 9·3 1 1 1 1 1 1 1 1 1	mb. 9·1 (Va 9/2 9/3 8/3 8/7 7/8 8/9 9/5 8/2 8/6 8/	mb. 9·2 llenc 9/95 93 85 78 91 82 83 85 82 86 94 96 95 79 87 85 89 76 87 88 82 88 82	mb. 9·1	mb. 9·1	mb. 9·2 /ator // 96 93 83 85 76 91 86 83 77 72 79 95 85 89 83 68 85 83 77 89 84	mb. 9·0 9/0 96 955 88 85 77 81 77 82 79 75 70 93 96 93 88 88 89 78 72 85 84 88 90 87	mb. 9·0 95 93 87 76 85 77 75 93 96 95 92 88 91 82 87 88 87 88 88 88 88 88 88 88	mb. 9·1	mb. 9·2 Vall % 95 96 83 90 91 77 77 77 76 96 91 93 88 89 83 87 99 87 87 85	mb. 9·3 Screet % 96 95 81 85 92 82 65 83 82 79 72 93 97 91 93 92 93 77 89 92 78 79	mb. 9·3 en: ha 96 95 83 72 93 77 66 85 83 78 70 95 96 76 93 92 92 92 78 80 77	mb. 9·4 9·4 9·4 9·4 9·6 96 96 81 71 93 75 66 82 82 72 67 95 93 74 92 89 93 81 79 77 81 91 79 80	mb. 9·5 9·5 1·3 I % 96 91 87 70 93 75 64 87 72 70 96 88 94 93 78 77 81	mb. 9.5 metr % 96 90 81 73 93 79 83 89 85 69 68 95 92 73 91 97 77 73 79 82 78 83 88	mb. 9·5 es. % 95 89 85 74 93 72 85 68 80 70 73 95 89 74 88 90 97 79 79 84 87	mb. 9.5 93 90 76 83 85 64 83 73 79 92 88 87 77 87 86 67 71 87 88 83 87	mb. 9·5 % 93 89 77 76 92 79 88 83 92 87 77 87 77 87 79 97 77 88 99 77 89 97 77 89 91	mb. 9·5 % 93 89 88 88 92 79 89 70 85 91 91 76 95 77 98 88 88 88 88 89 88 88 89 89	79 89 77 79 80 87 99 77 96 72 83 83 84 89	mb. 9·6 % 93 90 84 76 92 82 83 76 78 86 87 99 1 75 86 80 96 75 84 84 85 85 87 99 87	mb. 9.6 92 87 82 77 88 87 77 83 87 77 83 87 77 95 77 85 87 87 87 88 87 87 88 87 88 87 88 87 88 88	mb. 9.5 9.5 9.5 9.5 9.5 9.5 9.5 9.7 9.7 9.7 9.7 9.7 9.7 9.7 9.7	mb. 9·4 9·4 9·4 9·4 75 88 80 86 91 95 94 81 85 77 87 87 87 87 87 88 88 88	mb. ‡9·3 ***spring** **spring** ***spring** ***spring** ***spring** ***spring** **spring** ***spring** ***spring** ***spring** ***spring** **sprin	mb. 13.0 12.2 9.9 8.9 10.3 8.0 7.6 7.3 8.8 8.8 8.5 10.7 10.9 7.9 9.5 9.2 10.5 8.3 7.3

 $5|86 \cdot o|86 \cdot 4|86 \cdot o|$ **86 · 6** $|84 \cdot 3|84 \cdot 9|85 \cdot 8|86 \cdot 3|85 \cdot 4|84 \cdot 9|$

Vapour Pressure*

Hour G.M.T.

86

mb.

9.2 9.2 9.0

mb. | mb. |

9.0 9.2

10.

mb.

9 4

Noon.

mb. mb. mb. mb. mb. mb. mb. mb. mb. 8.9 9.0 8.7 8.7 8.8 8.9 9.0 9.2

mb.

20. 21. 22.

 $|82 \cdot 1| |81 \cdot 7| |83 \cdot 0| |81 \cdot 7| |82 \cdot 1| |82 \cdot 7| |84 \cdot 0| |84 \cdot 2| |84 \cdot 3| |84 \cdot 1| |84 \cdot 8| |84 \cdot 6|$

mb.

8.9 8.9 8.9

18.

9.1

mb. mb. mb.

9.4 9.2

15.

9.3

14.

mb. mb.

6.3

mb. | mb. | mb. | mb. | mb.

8.9 8.8

8.9 8.9

23.

84 · 4

mb.

‡9·o

Mean

†9·1

Computed from the mean temperatures and the mean relative humidities.

[†] Mean of the column.

RELATIVE HUMIDITY.

Percentages at exact hours, Greenwich Mean Time. Determined as explained on page 16.

317. Cahirciveen (Valencia Observatory): North Wall Screen: ht (height of thermometer bulbs above ground) = 1.3 metres.

March, 1923.

																									marc	h, 1923.
Day.	r.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
1 2 3 4 5	% 79 72 78 63 92	% 80 72 77 67 97	% 75 82 79 69 92	% 76 81 79 69 96	% 74 81 80 70 92	% 78 75 78 73 91	% 81 73 74 80 91	% 79 75 81 79 87	% 76 70 76 83 85	% 76 77 74 77 81	% 78 79 75 75 80	% 82 78 73 70 78	% 85 70 73 68 79	% 82 80 75 69 76	% 89 77 72 67 77	% 83 73 77 68 76	% 81 75 75 69 78	% 76 72 75 71 82	% 76 77 73 78 81	% 76 77 71 77 85	% 72 76 71 73 88	% 72 71 75 78 85	% 67 73 71 83 87	% 65 76 64 91 84	% 77·6 75·3 75·1 73·1 85·1	mb. 8·4 7·9 7·7 7·3 10·3
6 7 8 9 10	84 77 85 68 69	85 77 85 69 70	84 70 92 73 69	86 76 91 73 74	86 69 91 70 77	91 71 91 75 76	89 73 86 79 81	84 73 85 85 82	84 70 84 77 83	77 69 77 71 81	76 70 75 67 86	76 69 67 67 86	79 67 68 66 89	77 68 65 66 87	73 68 67 68 87	73 69 67 68 87	78 69 71 73 86	76 73 75 72 89	82 76 73 73 91	85 76 81 73 90	75 79 79 76 89	75 80 72 73 91	74 84 68 72 86	73 84 68 69 85	80·3 73·0 78·0 71·8 82·6	9·5 8·3 8·5 7·3 8·2
11 12 13 14	86 95 73 87 70	87 96 67 85 73	91 93 68 85 73	91 95 73 87 66	92 93 72 85 65	91 92 67 87 65	91 92 73 70 63	89 91 78 67 66	93 93 81 68 67	93 96 65 64 67	89 81 66 62 64	89 76 68 62 61	87 71 62 59 59	86 69 65 56 63	89 74 67 58 60	89 71 70 62 60	87 73 67 75 65	87 75 72 81 66	89 77 76 85 72	89 72 79 82 76	93 73 84 7 ² 75	92 63 85 71 79	95 68 87 70 77	96 73 85 79 81	89·8 81·8 72·7 73·4 68·0	8·9 10·0 7·5 7·3 6·8
16 17 18 19 20	83 73 76 72 76	85 77 76 75 78	86 75 77 80 79	85 76 81 75 80	86 81 83 83 83	87 76 85 77 85	86 73 83 74 83	78 73 85 73 85	79 72 83 71 87	77 74 80 71 80	75 68 75 67 77	71 70 73 67 78	70 71 74 68 71	69 67 72 63 70	66 65 72 63 71	65 65 73 69 70	68 65 80 72 76	68 71 82 73 79	70 75 84 72 77	69 73 69 73 85	72 76 72 69 86	72 77 64 69 85	72 79 68 73 82	74 72 70 73 83	75·7 72·7 76·6 71·7 79·2	7·6 7·6 7·9 7·1 7·6
21 22 23 24 25	88 82 87 89 82	87 85 87 88 83	87 85 87 91 82	87 86 87 89 87	87 85 87 82 92	85 88 87 79 85	87 87 86 81 81	89 91 86 77 81	93 90 85 74 81	86 86 79 72 68	76 75 73 69 68	70 72 68 68 68	76 73 71 69 65	76 71 78 70 65	76 69 76 68 64	75 71 78 70 65	75 65 78 68 65	73 71 77 69 72	77 75 85 72 76	72 77 86 71 75	79 82 85 72 74	80 82 87 77 73	78 85 89 83 70	85 85 90 81 72	81·0 79·9 82·4 76·4 74·9	7·9 8·0 8·8 8·5 9·1
26 27 28 29 30	74 91 87 89 95	72 91 83 91 95	72 93 82 89 92	73 95 76 88 95	73 95 78 87 93	72 93 77 87 95	71 95 77 87 95	76 95 76 87 92	77 95 77 83 89	72 95 78 84 87	74 91 73 81 79	74 84 77 78 76	73 83 76 79 75	74 80 75 80 71	76 81 73 81 75	76 83 74 79 73	74 78 75 81 72	76 84 76 85 73	83 89 82 86 78	86 89 85 87 82	87 89 83 88 83	89 88 85 91 84	89 87 89 91 89	89 85 88 92 89	76·8 88·8 79·2 85·4 84·5	9·7 11·3 9·5 10·5 9·8
31	91	91	92	92	89	93	89	90	89	85	78	82	89	88	75	72	73	67	70	70	73	72	76	78	82 · 1	8.2
Mean						82.3							73.1	72.7	72 · 3	72.6	73.8	75:4	78.4	78.6	78.9	78.6	79:4	80.0	78·2	†8•5
Vapour Pressure*	mb. 8·3	mb. 8·3	mb. 8·3	mb. 8·3	mb. 8·2	mb. 8·1	mb. 8·2	mb. 8·2	mb. 8·5	mb. 8·6	mb. 8·7	mb. 8·7	8·8	mb. 8·8	8·8	mb. 8·7	mb. 8·7	шъ. 8∙5	шо. 8·5	8·4	8·3	8·3	8·1	8·2	mb. ‡8·4	
318. Cahirci	veen	(Val	enci	a Ob	serv	ator	y) :	Nort	th W	all S	Scree	en: ht	= I	·3 n	netre	es.									Apri	il, 1923.
1 2 3 4	% 85 87 86 84	% 84 89 86 83 78	% 87 88 87 78 76	% 88 87 87 76	% 87 89 81 75 78	% 87 89 82 76 79	% 87 89 85 75	% 73 91 82 77 71	% 67 82 82 77 69	% 63 80 79 69 66	% 63 76 81 69 65	% 59 75 87 66 68	% 59 7 ² 83 67 70	% 59 69 78 65 68	% 65 69 82 65 68	% 66 70 84 70 70	% 69 71 86 67 73	% 73 76 86 67 75	% 83 78 91 68 69	% 82 85 87 75 68	% 79 85 91 73 65	% 82 85 92 79 73	% 83 82 87 73 74	% 88 87 84 72 76	% 75·5 81·3 84·9 73·0 71·8	mb. 7·2 8·0 9·1 7·9 7·3
5 6 7 8 9	76 74 87 75 75 63	82 89 79 73 69	76 87 84 73 69	73 74 88 85 73 72	76 88 87 76 71	80 81 83 80 73	77 83 88 87 79 76	81 81 79 78 72	73 77 71 72 71	67 74 67 71 67	64 72 64 67 69	64 67 66 62 65	61 69 64 66 62	61 67 65 66 61	70 67 69 63 61	67 69 69 60 60	68 71 72 59 67	76 71 75 58 82	79 70 75 61 85	82 72 78 61 85	83 68 72 58 85	82 73 74 54 85	83 72 83 57 85	86 73 78 60 85	74·5 76·1 74·9 67·1 72·0	7·4 7·4 7·7 7·1 6·1
11 12 13 14 15	88 87 85 75 89	85 89 88 77 89	87 88 88 79 85	87 89 89 79 84	88 87 88 81 83	88 85 86 85 84	88 83 89 81	89 78 86 86 86	90 71 85 79 79	90 70 91 82 83	87 69 89 83 82	87 67 89 85 83	87 70 87 81 80	79 72 87 89 78	81 75 87 91 79	82 70 83 87 80	82 72 78 89 82	84 71 73 91 83	83 79 76 93 83	84 83 73 91 82	89 84 70 92 82	86 86 71 91 81	85 82 76 91 82	86 83 75 93 81	85·9 78·8 83·0 85·1 82·7	8·5 8·4 8·0 9·0 9·4
16	83	83	84	81	84	84	86	8 ₅ 86	82 85	79 85	79	81	79	78 85	79 87	75 89	73 89	68 87	76 87	76 87 84	65 87	72 87	68 87 89	66 89 89	78·1 82·7 89·1	9·6 10·7 10·3
17 18 19 20	68 91 91 76	75 95 93 74	79 96 83 75	78 95 82 75	73 96 82 77	7 ⁸ 95 80 7 ⁸	83 96 75 76	95 72 76	95 70 70	93 67 74	84 92 65 72	84 87 63 72	79 78 86 61 70	81 61 70	82 61 68	80 57 72	81 59 69	81 59 66	81 64 68	84 68 71	89 71 70	90 72 69	73 65	74 67	71.8	8·2 8·5
18 19	68 91 91	75 95 93	96 83	95 82	82	95 80	96	95 72	95 70	93 67	92 65	87 63	61	81 61	82 61	80 57	59		64	68	71	72		74	71·3 71·8 65·9 71·8 72·5 74·1 82·9	_
18 19 20 21 22 23 24	68 91 91 76 67 73 77 76	75 95 93 74 73 77 76 74	96 83 75 75 81 69 71	95 82 75 76 81 73 76	82 77 79 81 75 76	95 80 78 75 82 71	96 75 76 74 84 69 78	95 72 76 74 86 71	95 70 70 68 80 73	93 67 74 67 80 68 60	92 65 72 60 71 76 59	87 63 72 60 65 83 60	61 70 61 64 76 61	81 61 70 60 63 73 62	82 61 68 57 57 72 67	57 72 57 59 72 72	59 69 59 61 68 73	59 66 58 60 71 84	64 68 58 60 75 86	68 71 60 61 73 87	71 70 63 70 70 91	72 69 62 74 68 89	73 65 69 79 68 92	74 67 71 77 68 95	71·8 65·9 71·8 72·5 74·1	8·5 6·1 7·7 7·7 7·5
18 19 20 21 22 23 24 25 26 27 28 29 30 Mean	68 91 91 76 67 73 77 76 95 82 78 84 89 96 81 · 4	75 95 93 74 73 77 76 74 92 77 86 87 92 96	96 83 75 75 81 69 71 92 75 84 89 91 96	95 82 75 76 81 73 76 91 77 76 90 91 96 82·3	82 77 79 81 75 76 91 76 76 85 91 95	95 80 78 75 82 71 70 89 85 87 86 95	96 75 76 74 84 69 78 82 77 83 88 89 97 82·8	95 72 76 74 86 71 70 84 75 82 79 88 96	95 70 70 68 80 73 63 78 75 77 80 84 97	93 67 74 67 80 68 60 87 73 72 80 83 97	92 65 72 60 71 76 59 81 66 60 82 83 97	87 63 72 60 65 83 60 77 72 69 85 85 96	61 70 61 64 76 61 74 71 67 81 95 73.0	81 61 70 60 63 73 62 85 65 71 91 89 93	82 61 68 57 57 72 67 75 64 69 86 93 94	80 57 72 57 59 72 73 65 73 83 95 90	59 69 59 61 68 73 77 65 79 95 88 73.7	59 66 58 60 71 84 75 64 73 81 93 88	64 68 58 60 75 86 76 62 74 83 93 88 76.8	68 71 60 61 73 87 77 62 76 87 93 90 78.0	71 70 63 70 91 81 69 77 89 95 89 78.4	72 69 62 74 68 89 85 71 79 89 96 92 79.6	73 65 69 79 68 92 83 76 82 87 96 92 80·0	74 67 71 77 68 95 83 75 86 89 95 91 80·7	71·8 65·9 71·8 72·5 74·1 82·9 71·8 75·9 85·9 90·4 93·5 78·1	8·5 6·1 7·7 7·5 10·0 7·7 8·2 9·8 11·3
18 19 20 21 22 23 24 25 26 27 28 29 30	68 91 91 76 67 73 77 76 95 82 78 84 89 96	75 95 93 74 73 77 76 74 92 77 86 87 92 96 83·0 mb.	96 83 75 75 81 69 71 92 75 84 89 91 96 82·4 mb.	95 82 75 76 81 73 76 91 77 76 90 91 96 82·3 mb.	82 77 79 81 75 76 91 76 76 85 91 95	95 80 78 75 82 71 70 89 85 87 86 95 82·7	96 75 76 74 84 69 78 82 77 83 88 89 97 82 8	95 72 76 74 86 71 70 84 75 82 79 88 96	95 70 70 68 80 73 63 78 75 77 80 84 97 77:4 mb.	93 67 74 67 80 68 60 87 73 72 80 83 97 76·1	92 65 72 60 71 76 59 81 66 60 82 83 97 74·2	87 63 72 60 65 83 60 77 72 69 85 85 85 96 74.3	61 70 61 64 76 61 74 71 67 81 89 95 73.0	81 61 70 60 63 73 62 85 65 71 91 89 93 73.0	82 61 68 57 57 72 67 75 64 69 86 93 94 73.4	80 57 72 57 59 72 73 65 73 83 95 90	59 69 59 61 68 73 77 65 79 95 88 73.7 mb.	59 66 58 60 71 84 75 64 73 81 93 88 75.0	64 68 58 60 75 86 76 62 74 83 93 88 76.8	68 71 60 61 73 87 77 62 76 87 93 90	71 70 63 70 91 81 69 77 89 95 89 78·4 mb.	72 69 62 74 68 89 85 71 79 89 96 92 79.6	73 65 69 79 68 92 83 76 82 87 96 92 80.0	74 67 71 77 68 95 83 75 86 89 95 91 80·7	71·8 65·9 71·8 72·5 74·1 82·9 71·8 75·9 85·0 90·4 93·5 78·1 mb.	8·5 6·1 7·7 7·7 7·5 10·0 7·7 8·2 9·8 11·3 12·6

^{*} Computed from the mean temperatures and the mean relative humidities.

⁺ Mean of the column.

[‡] Mean of the row.

Percentages at exact hours, Greenwich Mean Time. Determined as explained on page 16.

319. Cahirciveen (Valencia Observatory): North Wall Screen: ht (height of thermometer bulbs above ground) = 1.3 metres.

May. 1923

																										y, 1923.
Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	1	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
1 2 3 4 5	% 91 93 83 89 87	92 92 88 87 84	% 92 93 87 87 87	% 92 92 88 86 86	% 92 91 91 87 89	% 91 91 92 85 88	% 90 82 91 89 89	% 87 83 91 90 81	% 85 81 90 91 80	% 82 76 85 88 77	% 80 73 81 83 85	% 80 72 85 83 78	% 81 71 87 78 75	% 80 71 87 74 72	% 80 69 83 78 72	% 81 73 82 81 70	% 80 70 85 82 73	% 80 70 88 86 75	% 84 72 89 88 80	% 1 87 76 89 89 87	% 90 77 92 90 88	% 89 79 90 89 91	% 92 85 90 88 90	% 91 82 89 89 86	% 86·2 79·9 87·5 85·7 82·3	m.b. 11 · 8 12 · 1 12 · 5 12 · 2 11 · 5
6 7 8 9 10	87 81 86 85 71	88 81 85 85 72	87 80 81 79 79	91 83 85 73 77	92 83 82 75 77	92 84 87 72 82	91 77 88 70 77	92 70 86 71 75	92 67 81 72 64	89 66 77 80 66	89 64 72 67 69	80 60 72 80 64	76 62 73 81 69	73 61 71 86 64	66 62 71 74 72	67 66 70 67 79	66 68 69 59 87	68 73 71 66 91	70 73 72 62 89	71 77 77 68 88	72 79 79 65 89	71 81 82 68 88	75 83 82 62 89	77 84 82 61 80	80·3 73·4 78·4 72·4 77·0	9·5 8·0 9·6 7·9 8·6
11 12 13 14 15	75 73 83 68 79	69 80 79 76 81	73 80 76 63 80	79 83 81 66 76	75 77 69 71 76	71 72 75 71 77	70 75 83 75 78	67 77 76 83 77	59 87 73 83 73	69 71 70 81 65	69 78 69 83 70	73 78 70 87 69	71 85 65 84 64	79 76 64 83 65	75 83 65 84 64	64 83 77 86 65	60 85 75 86 78	66 86 71 81 76	67 87 70 83 73	64 80 70 76 73	75 81 71 74 78	76 79 73 71 77	75 81 72 74 77	75 79 68 73 76	70·8 79·7 72·9 80·6 73·6	7·2 7·5 7·5 8·4 8·1
16 17 18 19 20	76 80 87 81 93	77 76 89 81 93	80 77 87 76 95	83 80 89 79 93	81 76 89 81 93	72 76 88 87 93	77 72 86 85 93	74 68 85 75 92	70 65 80 78 87	69 68 77 72 81	67 66 79 75 81	67 66 7 ² 73 78	69 69 72 73 78	73 70 74 75 78	65 72 76 77 78	68 72 82 79 79	70 77 79 82 82	69 81 75 82 83	67 87 79 81 78	66 85 79 85 85	75 83 84 88 87	80 87 83 85 86	75 87 85 91 87	78 88 83 91 86	72·8 76·0 81·7 80·3 85·9	7·7 9·1 9·9 9·8
21 22 23 24 25	72 91 86 76 91	78 92 89 76 79	78 92 82 79 75	75 92 88 79 70	80 93 85 83 71	75 95 83 81 75	81 93 78 81 71	83 95 75 73 70	80 93 72 68 75	81 92 68 66 72	83 92 67 65 78	82 91 · 65 60 73	82 88 65 68 71	80 84 62 72 70	83 86 63 74 68	87 89 63 73 65	88 89 60 76 64	92 89 65 79 64	91 90 68 81 67	85 89 68 88 71	82 91 72 92 69	83 89 66 95 67	89 87 76 93 70	89 83 77 92 74	82·4 90·3 72·7 77·6 72·0	10·9 12·1 8·7 8·9 8·5
26 27 28 29 30	76 75 85 72 76	79 71 81 68 73	77 73 83 76 75	74 72 78 77 78	74 75 82 82 77	79 80 81 85 78	79 73 77 72 71	74 71 77 73 68	70 73 77 68 68	68 75 76 65 66	66 73 73 64 67	69 71 70 66 66	64 67 70 61 66	65 69 61 65	63 69 65 59 65	64 68 61 67 67	76 66 62 64 70	71 66 69 56 72	76 73 70 61 70	78 75 71 59 71	71 78 68 57 76	80 80 69 72 78	79 81 70 75 78	79 83 68 77 80	72·9 72·9 73·3 68·0 71·6	7·9 8·5 9·2 8·9 8·9
31	78	77	74	72	66	66	69	66	61	65	64	63	63	57	53	55	55	61	6 1	63	73	71	71	74	65.8	10.0
	81 · 5	81 · 2	80.7	81.3	81 • 1	81 · 4	80.1	78.2	76.2	74.3	7 3 ·9					72.6	_			77.1	_					†9· 4
Vapour	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.j	mb.	mb.						mb.	mb.	
Pressure*	9.0	9.0					9.3			9.4	9.5	9.6	8.6	9.7	9.5	9.8	9.8	9.7	9.6	9.4	9.3	9.2	9.1	9.0	‡9.3	
Pressure*			8.9	8.8	8.8	9.0	9.3	9.4	9.4	9.4							9.8	9.7	9.6	9.4	9.3	9.2	9.1	9.0		e, 1923.
	% 74 82 89 89	% (Va) % 70 84 90 91	8·9 % 73 86 91 93	8·8 ia Ol 77 87 91 92	8·8 58erv 79 89 91 91	9.0	9.3	9.4	9.4	9.4	% 67 72 73 73			.3 n % 67 73 79 68		% 65 69 77 68	% 67 69 78 69	9·7 % 66 74 78 73 74	9·6 % 69 76 79 77 75	9·4 % 73 76 78 76 77	9·3 % 75 81 83 77 82	9·2 % 76 82 83 79 84	9·1 % 72 84 83 80 76	9.0 % 74 88 87 79 70		m.b. 9·4 10·4 11·4 10·8 10·5
320. Gahirci	% 74 82 89	% 7° 84 9°	8·9 lenc % 73 86 91	8·8 ia Ol 77 87 91	8·8 8·8 8 79 89 91	9.0 /ator % 81 87 93 85	9·3 % 75 86 96 82	9·4 Nor % 7 ² 74 92 79	9·4 th W	7all \$ % 66 69 78	% 67 72 73	en: h <i>t</i> 66 63 69 71	= I % 66 68 70 71	% 67 73	% 66 72 77	% 65 69	% 67 69 78	% 66 74 78 73	% 69 76 79 77	% 73 76 78 76	% 75 81 83 77	% 76 82 83	% 72 84 83 80	% 74 88 87 79	Jun % 71.0 77.3 83.0 78.9	m.b. 9·4 10·4 11·4 10·8
320. Gahirci 1 2 3 4 5 6 7 8 9	% 74 82 89 89 84 79 88 91 95	% 70 84 90 91 87 72 89 91 95	8·9 % 73 86 91 93 89 75 92 92 94	8·8 % 77 87 91 92 91 76 92 92	8·8 % 79 89 91 91 90 91 91 92 94	9.0 /ator % 81 87 93 85 88 80 92 93	9·3 % 75 86 96 82 87 82 93 95	9·4 Nor % 7² 74 92 79 82 79 90 95	9·4 th W 67 72 86 79 82 79 88 95 95	7all 9 % 66 69 78 75 83 75 78 93 95	% 67 72 73 73 79 81 82 94	en: ha % 66 63 69 71 78 80 80 80 89 94	= I % 66 68 70 71 81 74 87 88 92	·3 n % 67 73 79 68 77 78 89 84 92	netre 66 72 77 72 78 78 87 84 93	% 65 65 69 77 68 74 77 91 83 91	% 67 69 78 69 75 81 90 84 91	% 66 74 78 73 74 82 91 88 91	% 69 76 79 77 75 84 92 88 92	% 73 76 78 76 77 85 90 90 83	% 75 81 83 77 82 87 90 91 83	% 76 82 83 79 84 87 88 92 82	% 72 84 83 80 76 87 88 93 83	% 74 88 87 79 70 89 90 94 82	% 71.0 77.3 83.0 78.9 81.2 79.9 88.6 90.3 91.5	m.b. 9·4 10·4 11·4 10·8 10·5 10·7 12·0 13·2 14·0
320. Gahirci 1 2 3 4 5 6 7 8 9 10 11 12 13 14	% 74 82 89 89 84 79 88 91 95 83 95 81	% (Va 70 84 90 91 87 72 89 91 95 85 77 86 95 83	8·9 lenci % 73 86 91 93 89 75 92 94 84 78 87 95 83	8·8 % 77 87 91 92 91 76 92 93 82 78 89 95 85	8·8 bserv % 79 89 91 91 91 80 91 92 94 83 65 89 93 85	9.0 yator 81 87 93 85 88 80 92 93 94 84 65 88 89 88 88	9·3 % 75 86 96 82 87 82 93 95 83 71 87 95 82	9·4 North % 72 74 92 79 82 79 90 95 95 81 72 87 95 82	9·4l th W % 67 72 86 79 82 79 88 95 77 69 82 96 81	9·4 7all 9 % 66 69 78 75 83 75 78 93 95 81 95 80	% 67 72 73 79 81 82 94 95 78 69 80 95 77	en: h _t 66 63 69 71 78 80 80 89 94 76 70 82 87 77	= I % 66 68 70 71 81 74 87 88 92 79 70 82 82 76	*3 n % 67 73 79 68 77 78 89 84 92 79 68 85 78 75	72 77 72 78 78 87 84 93 77 71 93 80 76	% 65 69 77 68 74 77 91 83 91 78 69 93 78 71	% 67 78 69 78 67 78 67 78	% 66 74 78 73 74 82 91 88 91 82 74 92 76 81	% 69 76 79 77 75 84 92 88 92 83 78 93 79 83	% 73 76 78 76 77 85 90 90 83 85 79 95 77 87	% 75 81 83 77 82 87 99 91 83 85 81 96 81 91	% 76 82 83 79 84 87 88 92 82 85 79 96 81 95	% 72 84 83 80 76 87 88 93 83 83 96 79	% 74 88 87 79 70 89 90 94 82 81 82 95 78	% 71.0 77.3 83.0 78.9 81.2 79.9 88.6 90.3 91.5 81.2 73.4 88.4 86.8 82.3	m.b. 9·4 10·4 11·4 10·8 10·5 10·7 12·0 13·2 14·0 11·8 10·2 12·2 11·9
320. Gahirei 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	74 82 89 89 84 79 88 91 95 83 95 83 97 76 86 93	70 84 90 91 87 72 89 91 85 77 86 89 95 83 96 76 89 93 84	8·9 lene: %	8·8	8 · 8 	9.0 // vator % 81 87 83 85 88 80 92 93 94 84 84 96 83 88 89 60 79 79 10 10 10 10 10 10 10 1	9·3i % 755 86 96 82 87 82 93 955 83 71 87 955 82 96 89 89 89 89 87	9·4 Nor 72 74 92 99 82 79 95 81 72 87 95 82 87 95 82 87 95 87 97 88	9·4l th W % 67 72 86 79 88 95 77 69 82 96 81 97 83 75 93	9·4 Vall 5 % 66 69 75 83 75 78 93 95 77 69 81 95 80 95 79 74 90 76	% 67 72 73 81 82 945 78 80 95 77 794 77 73 90 74	en: h# 66 63 69 71 78 80 80 89 94 76 70 82 87 77 95 77 72 88 74	= I % 66 68 70 71 81 74 87 79 70 82 82 76 95 77 76 86 72	*3 n %67 733 79 68 77 78 88 89 92 79 68 85 78 77 76 85 74	78 87 77 72 78 87 77 84 93 77 71 93 80 76 93 78 83 77	% 65 69 77 68 74 77 91 83 1 78 69 93 78 79 1 93 84 80 85 70	% 67 69 78 69 75 81 90 84 91 78 82 90 81 83 88 70	% 66 74 78 82 91 82 74 92 78 88 89 171	% 69 76 79 77 75 84 92 83 88 81 92 92 75	% 73 76 78 76 77 85 90 83 85 79 95 77 87 82 74 95 93	% 755 81 83 777 82 87 99 91 83 85 81 96 81 91 77 77 93 95 80	% 76 82 83 79 84 87 88 85 79 96 81 92 92 92 93 82	% 72 84 83 80 76 87 88 93 83 83 95 79 95 78 80 93 93 77 94	% 74 88 87 79 90 94 82 81 82 95 78 99 99 99 95 75 78 86 79	% 71.0 77.3 83.0 78.9 81.2 79.9 88.4 90.3 91.5 81.2 73.4 88.4 88.8 82.3 91.4 79.7 83.2 91.3 77.0	m.b. 9·4 10·4 11·4 10·8 10·5 10·7 12·0 13·2 14·0 11·8 10·2 12·6 12·9 12·9 10·5 11·3 13·1 10·7
320. Gahirci 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	% 74 82 89 84 79 83 95 83 95 81 97 76 86 93 85 78 94 93 92 91	(Va % 70 84 90 91 87 72 89 91 95 85 77 86 95 83 96 76 89 93 93 93 93 93 93 93 9	8·9 8·9 73 86 91 93 89 75 92 94 84 78 87 95 81 79 96 84 74 95 91 91	8·8	8·8i % 79 89 91 91 91 92 94 83 65 89 93 85 96 79 80 96 82 74	9.0 // rator % 81 87 93 85 88 80 92 93 94 84 96 83 88 96 96 97 70 95 91 93 93	9·3i % 755 86 96 98 82 87 82 93 95 83 71 87 95 82 96 89 86 95 78 89 89 89 89 89 89 89 89 89 89 89 89 89	9·4 Nor 72 74 92 79 82 79 95 95 81 72 87 95 82 97 88 77 93 73 67 94 92 83	9·4l th W 67 72 86 79 82 79 82 95 97 69 82 96 81 97 83 75 93 77 68 99 91 79	9:4 % 66 69 78 75 83 95 77 77 69 81 95 80 95 79 74 90 94 84 89 81	% 67 72 73 73 79 81 82 94 955 78 69 80 95 77 94 77 73 80 87 77 73 80 87 71	en: h _t 66 63 69 71 78 80 80 89 94 76 77 95 77 72 88 74 72 81 86 77	= I % 66 68 70 71 81 74 87 88 92 79 70 82 82 76 95 77 76 86 72 79 91 79 84 75	*3 n % 67 73 79 68 77 78 89 84 92 79 68 85 75 94 77 76 85 77 77 76 85 77 77 78 85 85 85 77 77 77 78 87 78 87 78 87 78 78	78 87 88 77 77 77 78 88 77 77 77 77 78 88 77 77	93 78 69 79 83 91 78 69 93 78 79 84 80 85 70 70 94 85 78 67	% 67 69 78 69 75 81 99 84 91 78 67 76 78 70 71 92 84 80 70	% 66 74 78 73 74 82 91 88 91 82 76 88 91 77 92 78 88 91 77 92 78 88 91 77 79	% 69 76 79 77 75 84 92 88 92 83 78 93 79 83 88 81 92 92 92 75 81 93 86 84 76	% 73 76 78 76 77 85 90 83 85 77 87 82 74 95 93 77 87 87 87 88 87 81	% 755 81 83 777 82 87 99 91 83 85 81 96 81 91 77 77 93 95 80 89 95 92 87 85	% 76 82 83 79 84 87 88 89 95 75 82 92 93 82 91 94 92 85	% 72 84 83 80 76 87 88 83 83 83 96 79 95 78 80 93 91 74 90 95 93 92 86	% 74 88 87 79 70 89 90 94 82 81 82 95 78 93 86 79 93 86	71.0 77.3 83.0 78.9 88.6 90.3 91.5 81.2 73.4 88.4 86.8 82.3 91.4 79.7 83.2 91.3 77.0 75.5 93.2 87.7 87.5 82.1	m.b. 9·4 10·4 11·4 10·8 10·5 10·7 12·0 13·2 14·0 11·8 10·2 12·6 12·2 11·9 12·9 10·5 11·3 13·1 10·7 10·7 14·2 13·4 13·4
320. Gahirci 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Mean	% 74 82 89 84 79 83 95 81 97 76 86 93 95 87 88 85 89 82 85 88 86 · 5	(Va % 70 84 90 91 87 72 89 91 95 85 86 95 83 96 76 89 93 84 71 93 99 93 86 85 86 \cdot 4 85 85 86 \cdot 4 85 85 86 \cdot 4 85 85 86 \cdot 4 85 85 85 85 85 85 85	8·9 lone % 738 86 91 93 89 75 92 94 84 78 87 95 83 97 81 79 96 84 74 95 87 89 87 87 82 87 87 87 87 87	8·8 ia Ol % 77 87 91 92 91 76 92 93 82 78 89 95 85 96 79 86 96 96 87 88 90 86 87 80 80	8 · 8 % 79 89 91 91 92 94 83 85 65 89 93 85 65 89 80 80 80 80 80 80 80	9·0 /ator % 81 87 93 85 88 80 92 93 94 84 96 83 88 96 97 70 95 91 86 91 85 87 · 1 85 87 · 1	9·3i % 755 86 96 98 82 87 93 95 83 71 87 95 88 94 91 93 88 82 86 95 88 82 86 95 88 88 88 88 88 88 88 88 88 88 88 88 88	9·4 Nor % 72 74 92 79 82 79 95 95 81 72 87 95 88 77 93 83 81 91 84 84 84 84	9·4l th W 67 72 86 79 82 79 88 95 97 69 82 96 81 97 83 75 93 77 88 96 89 97 80 98 83 72 88 83·2	9·4 Vall 5 % 66 69 78 75 83 75 77 69 81 95 80 95 79 74 90 94 84 89 81 82 91 77 87 81 10	% 67 72 73 73 79 81 82 94 955 78 69 80 95 77 94 77 73 90 74 70 93 80 87 71 82 91 78 70 76 89 80 · 3	en: h# 66 63 69 71 78 80 89 94 76 70 82 87 77 95 77 72 88 74 72 91 81 86 77 80 91 82 68 74 79 91 87 79 91	= I % 66 68 70 71 81 74 87 88 92 79 70 82 82 76 67 77 76 86 87 77 79 89 79 77 73 94 79 1	*3 n % 67 73 73 78 89 84 92 79 68 85 78 77 76 85 74 77 76 87 76 67 73 86 77 78 88 77 77 78 88 77 78 88 77 78 88 77 78 88 77 78 88 77 78 78	78 87 88 87 77 77 78 84 78 83 88 76 77 84 75 66 79 92 79 3	85. % 655 669 777 77 668 74 77 83 91 78 69 93 84 80 85 70 70 94 85 77 86 72 70 69 92 78:5	% 67 69 78 69 75 81 90 84 91 78 67 78 87 70 77 82 75 82 75 82 75 84 82 75 75 87 75 87 75 87 75 75 75 76 76 77 76 77 77 77 77 77 77 77 77 77	% 66 74 78 73 74 82 91 88 91 82 76 81 77 79 89 84 81 76 79 82 77 71 75 78 80 4	% 69 76 79 77 75 84 92 88 92 83 78 93 79 83 88 81 92 92 75 81 93 86 84 76 74 86 79 77 77 76 82 · 2 · 2	% 73 76 78 76 77 85 90 90 83 85 79 95 77 82 74 95 93 77 87 81 80 85 79 78 76 82 93	% 755 81 83 777 82 87 991 833 85 81 96 81 97 77 77 93 980 89 952 87 85 83 86 81 80 77 81 84 77	%6 82 85 79 682 91 94 92 85 83 85 85 85 86 86 87 88 86 86 86 86	% 72 84 83 80 76 87 88 83 83 83 83 83 83 83 96 79 95 78 80 93 91 74 90 95 88 88 88 88 88 88 88 88 88 88 88 88 88	% 74 88 87 79 90 94 82 81 82 95 78 93 86 86 89 84 84 82 95 52 85 2 85 2 85 2 85 2 85 2 85 2	71.0 77.3 83.0 78.9 88.6 90.3 91.5 81.2 73.4 88.4 86.8 82.3 91.4 79.7 83.2 91.5 91.5 91.5 82.7 77.0 75.5 82.1 82.7 76.9 79.9 82.7 76.9 76.9 82.7 76.9 82.7 76.9 82.7 76.9 83.2	m.b. 9.4 10.4 11.4 10.8 10.5 10.7 12.0 13.2 14.0 11.8 10.2 12.6 12.2 11.9 12.9 10.7 10.7 10.7 14.2 13.7 14.3 13.1 13.1 13.1 13.1 13.1 13.2 13.1 13.2 14.0 15.0 16.0 17.0 17.0 18.0 1
320. Gahirei 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Mean	% 74 82 89 84 79 83 95 81 97 76 86 93 85 78 94 93 92 85 88 86 5 8 8 86 5 5 mb.	70 84 90 91 87 72 89 91 95 85 77 86 89 93 84 71 93 99 193 89 86 85 86 85 86 4 mb.	8·9 lenc % 738 86 91 93 889 75 92 94 84 78 87 95 87 89 91 89 87 82 87 \cdot on mb.	8·8	8·8i % 79 89 91 91 91 92 94 83 85 96 96 82 74 93 91 91 90 88 88 87 87 00 mb.	9.0 rator % 81 87 93 85 88 80 92 93 94 84 65 88 96 83 88 96 87 97 97 95 91 86 91 91 85 87.1 mb.	9·3i % 755 86 96 98 82 87 93 95 83 71 87 95 88 94 91 93 88 82 91 89 82 85 82	9·4 Nor' % 72 74 92 79 82 79 95 81 72 88 77 95 88 77 93 37 67 94 92 92 83 81 91 84 44 94 92 96 96 97 88 88 88 88 88 88 88 88 88 88 88 88 88	9·4l th W % 67 72 86 79 82 79 82 95 97 83 75 93 77 68 96 89 91 79 80 95 83 72 82 88 83·2	9:44 7all 5 % 66 69 78 75 83 75 89 95 77 69 81 95 80 95 79 74 90 94 84 89 81 82 91 77 87 81 90 mb.	% 67 72 73 73 73 77 81 82 94 95 78 69 80 95 77 94 77 73 90 74 70 93 80 76 89 80 3 mb.	en: h 66 63 69 71 78 80 80 89 94 76 70 82 87 77 95 77 72 88 74 72 91 81 86 77 80 91 82 68 74 87 79 92 mb	= I % 66 68 70 71 81 74 87 88 92 79 70 82 82 76 95 77 76 86 72 79 91 79 89 79 79 79 79 79 79 79 79 79 79 79 79 79	*3 n % 67 73 79 68 77 78 89 89 89 77 76 85 77 76 87 76 87 76 77 76 87 76 77 76 77 76 77 78 77 78 78 78 79 79 79 79 79 79 79 79 79 79	78 87 88 87 79 83 80 76 93 83 72 74 93 88 80 76 77 88 83 80 76 77 84 75 66 70 92 79 3	98. % 65, 69, 77, 76, 68, 74 77, 91, 83, 91, 78 69, 33, 78, 71, 93, 84, 80, 85, 70, 70, 69, 92, 77, 77, 86, 72, 70, 69, 92, 78, 58, 78, 77, 77, 78, 78, 77, 77, 78, 78, 7	% 67 69 78 69 75 81 99 84 91 78 67 76 78 82 76 75 85 78 85 78 78 82	% 66 74 78 73 74 82 91 88 91 82 76 81 92 76 88 91 71 77 9 88 89 84 81 76 79 82 77 77 75 78 80 4 mb.	% 69 76 79 77 75 84 92 88 92 83 78 93 79 83 88 81 92 92 92 75 81 93 86 74 86 77 77 76 82 2 2 mb.	% 73 76 78 76 77 85 79 99 83 85 77 87 82 74 89 83 87 87 87 87 87 87 87 88 80 85 79 78 87 88 80 85 79 78 81 80 85 79 78 81 80 85 79 78 78 78 78 78 78 78 78 78 78 78 78 78	% 755 81 83 777 82 87 991 83 85 81 96 81 91 77 77 93 95 80 88 9 95 92 87 85 83 86 81 86 77 81 84 7 mb.	%6 82 83 79 84 87 88 89 82 82 85 75 82 92 93 82 91 94 92 85 83 87 88 87 88 87 88 88 88 91 91 91 91 91 91 91 91 91 91 91 91 91	% 72 84 83 80 76 87 888 83 83 83 96 79 95 78 80 93 91 74 90 95 93 92 86 85 78 82 85 2 85 2 mb.	% 74 88 87 79 70 89 90 94 82 81 82 95 75 78 93 86 79 93 86 86 89 84 82 79 85 2 mb.	## ## ## ## ## ## ## ## ## ## ## ## ##	m.b. 9.4 10.4 11.4 10.8 10.5 10.7 12.0 13.2 14.0 11.8 10.2 12.6 12.2 11.9 10.5 11.3 13.1 10.7 10.7 14.2 13.7 14.8 13.4 13.1 13.3 13.0 12.6 12.5 12.8

^{*} Computed from the mean temperatures and the mean relative humidities.

[†] Mean of the column.

[‡] Mean of the row.

RELATIVE HUMIDITY.

Percentages at exact hours, Greenwich Mean Time. Determined as explained on page 16.

321. Cahirciveen (Valencia Observatory): North Wall Screen: h_t (height of thermometer bulbs above ground) = $\mathbf{1} \cdot \mathbf{3}$ metres.

szi. Ganirci	148811	(v a					3 / -	-110-						Ü								Ü	•		Jul	y, 1923.
Day.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure
1 2 3 4 5	% 83 91 93 89 93	% 86 91 94 91 93	94 93 94	% 86 91 94 93 93	% 90 91 94 93 93	91 89 94 93 93	% 89 88 94 87 96	% 82 88 95 83 95	% 83 90 94 78 96	% 81 85 92 79 94	% 83 85 82 74 94	% 79 83 76 78 89	% 81 81 73 74 86	% 77 85 73 81 89	% 78 84 73 75 89	% 76 82 71 78 92	% 75 82 77 84 93	% 78 87 78 85 91	% 81 91 79 84 89	% 88 91 81 86 83	% 90 92 85 87 86	% 91 92 86 88 87	% 93 92 87 91 86	% 92 93 88 91 85	% 83·9 88·1 85·4 84·7 90·9	mb. 13·1 14·6 14·3 14·7 15·5
6 7 8 9	86 90 89 97 83	81 88 93 95 82	82 89 93 96 82	83 91 93 97 80	83 91 94 97 79	87 91 89 95 75	85 89 85 95 75	80 93 81 93 70	75 97 76 88 64	76 93 80 86 69	75 89 81 87 68	81 86 88 91 73	81 86 91 87 73	79 86 92 83 73	77 89 95 80 72	79 83 95 78 67	74 79 97 73 72	79 81 95 75 75	86 84 97 78 80	85 85 97 81 81	91 88 96 86 84	89 89 96 85 85	89 91 97 87 87	89 91 97 87 86	82·1 88·3 91·0 87·6 76·5	15·7 16·2 15·9 16·6 14·8
11 12 13 14 15	83 90 85 86 86	87 92 84 91 86	89 93 80 91 87	90 93 85 91 90	89 94 85 91 93	89 95 78 93 94	88 94 73 86 93	84 94 70 77 94	81 89 70 75 97	73 86 69 77 95	79 82 69 78 95	81 81 65 79 92	79 79 66 77 91	79 75 68 77 91	75 78 65 76 91	78 76 68 77 90	75 71 67 77 87	75 71 65 81 82	75 77 70 82 85	81 75 75 83 90	84 76 76 81 91	87 77 80 82 92	89 79 85 85 93	91 83 85 87 93	82·4 83·5 74·3 82·5 90·6	14·6 15·2 14·7 14·8 16·4
16 17 18 19 20	86 83 89 86 98	85 85 83 89 98	83 82 82 89 98	85 83 77 87 97	87 87 76 93 98	86 89 78 95 98	82 85 75 96 98	77 84 69 97 95	81 71 71 98 94	84 68 67 98 93	76 70 65 94 93	74 69 67 91	68 72 77 91 91	67 69 69 91 87	71 69 72 92 85	73 69 70 91 87	72 72 75 93 90	72 69 78 93 91	77 69 80 95 92	76 69 82 97 91	82 75 84 95 90	83 82 84 96 91	81 86 84 97 88	83 82 84 97 89	79·0 76·6 76·5 93·1 92·9	13·7 12·8 13·0 16·4 17·5
21 22 23 24 25	91 95 92 92 98	92 95 91 93 97	93 94 91 92 97	94 95 92 92 98	94 95 95 91 99	95 94 95 91 97	95 94 97 87 95	93 91 95 89	93 90 97 93 93	93 85 98 94 84	91 78 97 94 80	86 77 98 97 77	86 79 98 94 75	87 77 95 92 79	85 81 92 94 73	85 82 89 90 74	84 85 85 90 69	91 85 84 92 74	91 84 81 91 69	94 88 81 93 70	94 89 87 93 74	95 92 87 92 66	93 91 87 91 73	95 90 92 93 70	91·1 87·9 91·5 92·1 82·8	17·4 16·7 16·5 16·3 14·9
26 27 28 29 30	69 82 92 88 88	68 83 93 88 89	71 82 94 91 84	78 88 90 92 85	74 91 94 91 87	70 93 92 86 87	73 95 88 87 88	73 95 84 84 87	66 94 83 85 87	69 93 83 80 91	71 93 79 88 94	69 94 77 85 87	68 93 79 91 86	70 91 76 91 80	67 89 77 93 76	68 91 78 92 75	69 92 79 89 79	71 92 79 87 79	73 93 80 84 83	75 94 84 82 84	75 94 85 85 86	79 93 87 84 87	82 94 86 86 87	81 94 89 87 88	71·8 91·1 84·6 87·4 85·1	12·0 16·1 14·4 14·7 14·4
31	88	90	89	91	91	91	91	91	90	90	86	86	83	79	82	77	71	79	79	80	81	82	82	78	84.7	13.2
Vapour	88·4	mbi	mb	mb	mbl	mbi	mb !	mbil	mh I	mh	mb	mb	mb	mb	mb	mb l	mb	mb.	mb.	mb.	mb.	mb.	87·7 mb.	mb.	mb.	†15·1
Pressure*	14.2	14.3	14 · 2	14.2	14.3	14.6	14.9	15.2	15.4	15.5	15.7	15.8	16.0	15.9	15.8	15.7	15.6	15.2	15.0	14.7	14.5	14.5	14.5	14.4	1+15.0	t, 1923.
322. Cahirc		(Va					· · · · · · · · · · · · · · · · · · ·	Nor				%	= 1 %	%	%	%	%	%	%	%	%	%	% 82	%	1 %	mb.
1 2 3 4 5	78 83 86 82 93	79 86 87 81 95	% 81 84 86 81 95	% 82 85 85 77 96	% 86 87 85 81 96	% 84 87 87 77 95	% 78 92 83 81 96	79 94 78 78 78 92	% 76 92 75 74 91	% 85 90 78 73 87	% 78 84 76 74 85	75 88 77 70 83	72 87 77 70 80	73 83 76 69 79	73 74 75 73 78	71 73 75 73 76	65 75 73 73 78	70 78 75 76 75	79 80 77 79 77	81 80 84 79 79	77 84 86 79 84	% 78 84 89 80 91	82 82 90 89 92	85 87 82 91 93	77.6 84.1 81.0 77.3 86.9	13·4 13·8 13·6 13·9 16·1
6 7 8 9	93 95 95 96 94	94 96 97 96 95	94 97 96 96 96	94 94 97 96 96	93 95 95 95 95	93 95 96 96 94	92 95 98 96 90	92 95 97 94 85	94 95 95 94 78	95 90 95 89 79	95 85 94 87 76	93 83 95 86 75	94 77 97 81 76	90 78 97 84 77	91 79 97 84 75	92 78 98 87 76	92 78 98 85	95 76 97 86 80	95 80 95 88 81	95 87 94 90 87	95 84 97 91 88	97 85 98 92 88	94 90 97 93 89	94 91 95 93 91	93·7 87·5 96·2 90·7 84·9	16·5 15·5 17·4 16·7 15·3
11 12 13 14	91 91 97 89	92 93 97 91	92 95 97 91	93 95 95	92 97 98	92 97 97	93 95 97 90	92 95 97 87	83 97 97 81	79 97 97 81	80 95 97	79 94 93	77 95 93	77 95 92	76 95 87	75 95 86	79 97 84 79	88 97 86 78	88 98 86 77	88 97 87 79	83 97 91 81	79 97 90 80	81 98 90 80	87 98 87 76	84·9 95·6 92·6 81·6	14·7 17·7 17·7
15				91 76	90 78	91 76	- 1	72	68	66	79 67	77 66	76 67	64 69	73 69	71 63	68	7I	69	71	71	76	76	76 78	71.7	14·4 11·8
15 16 17 18 19	77 75 92 88 86 97	79 75 91 89 85 97	75 80 87 84 84 96	76 79 88 87 85 97	78 85 90 86 88 99	91 76 81 89 87 85 96	74 85 89 82 86 94						76			79 84 90 89	78 92 84 93 94		82 93 84 95 93		71 86 92 86 96 90	76 89 91 85 96 90	76 89 92 83 96 92	78 90 92 85 97 93	80·1 88·5 84·4 87·4 93·8	14.4
16 17 18	77 75 92 88 86	79 75 91 89 85	75 80 87 84 84	76 79 88 87 85	78 85 90 86 88	76 81 89 87 85	74 85 89 82 86	72 85 90 88 82	68 82 89 80 82	75 85 79 83	67 72 83 80 81	77 66 71 80 80 77	76 67 73 83 85 80	77 84 79 84	75 84 79 85	63 79 84 90 89	78 92 84 93	71 84 93 86 94	82 93 84 95	71 81 91 86 95	86 92 86 96	89 91 85 96	89 92 83 96	90 92 85 97	80·1 88·5 84·4 87·4	14·4 11·8 13·3 15·3 14·0 14·7
16 17 18 19 20 21 22 23 24	77 75 92 88 86 97 93 81 89 86	79 75 91 89 85 97 94 82 90 83	75 80 87 84 84 96 89 81 86 88	76 79 88 87 85 97 81 82 86 85	78 85 90 86 88 99 86 80 88 80	76 81 89 87 85 96 81 78 89 83	74 85 89 82 86 94 85 79 89	72 85 90 88 82 94 77 71 92 75	82 89 80 82 94 76 74 94 75	75 85 79 83 90 77 74 94 72	72 83 80 81 90 77 72 91 71	77 66 71 80 80 77 90 79 70 79	76 67 73 83 85 80 93 74 72 78 73	77 84 79 84 95 77 74 77 72	75 84 79 85 94 89 77 77 68	63 79 84 90 89 95 79 82 74 69	78 92 84 93 94 78 73 76 70	71 84 93 86 94 94 89 76 79	82 93 84 95 93 88 79 83	71 81 91 86 95 93 87 82 81 78	86 92 86 96 90 83 85 82 81	89 91 85 96 90 82 89 83 86	89 92 83 96 92 82 87 83 90	90 92 85 97 93 79 87 88 90	80·1 88·5 84·4 87·4 93·8 82·9 78·5 84·5 78·0	14.4 11.8 13.3 15.3 14.0 14.7 16.4 12.8 12.3 13.8 12.0
16 17 18 19 20 21 22 23 24 25 26 27 28 29	77 75 92 88 86 97 93 81 89 86 87 88 76 79 87	79 75 91 89 85 97 94 82 90 83 87 80 74 86	75 80 87 84 84 96 89 81 86 88 90 91 77 77 86	76 79 88 87 85 97 81 82 86 85 92 91 76 75 87	78 85 90 86 88 99 86 80 88 80 95 88 83 80 86	76 81 89 87 85 96 81 78 89 83 94 88 78 85 91	74 85 89 82 86 94 85 79 89 77 95 86 80 78 89	72 85 90 88 82 94 77 71 92 75 93 82 81 72 88	82 89 80 82 94 76 74 94 75 92 83 80 84 84	66 75 85 79 83 90 77 74 94 72 91 89 80 74 80	72 83 80 81 90 77 72 91 71 92 86 85 71 80	77 66 71 80 80 77 90 79 72 92 83 85 73 72 69	76 67 73 83 85 80 93 74 72 78 73 94 81 89 66 69 67	77 84 79 84 95 77 74 77 72 95 79 85 70 72 70	75 84 79 85 94 89 77 77 68 95 70 65 77	63 79 84 90 89 95 79 82 74 69 93 81 77 73 64 73	78 92 84 93 94 78 76 70 91 76 76 76 76 68	71 84 93 86 94 94 89 76 79 73 88 77 75 75 71 79	82 93 84 95 93 88 79 83 75 80 69 79 69 77	71 81 91 86 95 93 87 82 81 78 89 75 70 82 71 76	86 92 86 96 90 83 85 82 81 91 79 73 81 77 78	89 91 85 96 90 82 83 86 87 79 69 83 78	89 92 83 96 92 87 87 87 81 74 77 71 79	90 92 85 97 93 79 88 90 84 78 72 84 74 85	80·1 88·5 84·4 93·8 82·9 78·5 78·0 91·0 82·7 78·3 76·2 77·2 74·3	14.4 11.8 13.3 15.3 14.0 14.7 16.4 12.8 12.3 13.8 12.0 14.7 13.3 11.5 11.2 9.9 10.4
16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	77 75 92 88 86 97 93 81 89 86 87 88 76 79 87 75 85	79 75 91 89 85 97 94 82 90 83 87 80 74 86 71 83 87.5	75 80 87 84 84 96 88 86 88 90 91 77 77 86 69 82 87 87 87 80 80 80 80 80 80 80 80 80 80	76 79 88 87 85 97 81 82 86 85 92 91 76 75 87 72 82 87	78 85 90 86 88 99 86 80 88 80 95 88 83 86 75 87	76 81 89 87 85 96 81 78 83 94 88 78 85 91 74 89 87 89 87 89 89 89 80 80 80 80 80 80 80 80 80 80	74 85 89 82 86 94 85 79 87 95 86 80 78 89 70 88 89 89 88 89 89 80 80 80 80 80 80 80 80 80 80	72 85 90 88 88 82 94 77 71 92 75 93 82 81 72 88 73 75 85 · 3	82 89 80 82 94 76 74 94 75 92 83 80 84 84 72 74 84 0	75 85 79 83 90 77 74 94 72 91 89 80 74 80 75 72 82 9	72 83 80 81 90 77 72 91 71 92 86 85 71 80 73 70 81·5	77 66 71 80 80 77 90 79 72 92 83 85 73 72 69 72	76 67 73 83 85 80 93 74 72 78 73 94 81 89 68 69 71	69 77 84 79 84 95 77 74 77 72 95 79 85 70 71 79:5	75 84 79 85 94 89 77 77 68 95 75 80 70 65 77 72 79 •4	63 79 84 90 89 95 79 82 74 69 93 81 77 73 64 73 69 79.4	78 92 84 93 94 78 73 76 76 76 76 76 68	71 84 93 86 94 94 89 76 79 73 88 77 75 71 79 72 81 • 72	82 93 84 95 93 88 79 83 75 80 69 79 69 77 77 82:5	71 81 91 86 95 93 87 82 81 75 70 82 71 76 76 83.6	86 92 86 96 90 83 85 82 81 91 79 73 81 77 78	89 91 85 96 90 82 89 83 86 87 79 76 79 69 83 78	89 92 83 96 92 82 87 83 90 87 81 74 77 71 79 81	90 92 85 97 93 79 88 90 84 78 72 84 74 85 82	80·1 88·5 84·4 93·8 82·9 78·5 84·5 78·0 91·0 82·7 78·3 76·2 77·2 74·3 77·4	14.4 11.8 13.3 15.3 14.0 14.7 16.4 12.8 12.3 13.8 12.0 14.7 13.3 11.5 11.2 9.9 10.4
16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Mean	77 75 92 88 86 97 93 81 89 86 87 88 76 79 87 75	79 75 91 89 85 97 94 82 90 83 87 86 71 83 87.5 mb.	75 80 87 84 84 96 88 86 88 90 91 77 77 86 69 82 87·2 mb.	76 79 88 87 87 85 97 81 82 86 85 92 91 76 75 87 72 87 90 mb.	78 85 90 86 88 99 86 80 88 80 95 88 87 87 88·4	76 81 89 87 85 96 81 78 89 83 94 88 85 91 74 89 87 91 74	74 85 89 82 86 94 85 77 95 86 80 78 89 70 88 87 22 87 89 70 88 87 88 88 89 70 70 89 80 70 80 80 80 80 80 80 80 80 80 8	72 85 90 88 82 94 77 71 92 75 93 82 81 72 88 73 75 85·3 33 33 34 35 36 37 37 38 38 38 38 38 38 38 38 38 38	82 89 80 82 94 76 74 94 75 92 83 80 84 84 72 74 84 00 mb.	75 85 79 83 90 77 74 94 72 91 89 80 74 80 75 72 82·9 90 mb.	72 83 80 81 90 77 72 91 71 92 86 85 71 80 73 70 81·5	77 66 71 80 80 77 90 79 70 79 72 92 83 85 73 72 69 72 79 90	76 67 73 83 85 80 93 74 72 78 73 94 81 89 69 68 69 71 79.7	77 84 79 84 95 77 74 77 72 95 79 85 70 71 71 79:5	75 84 79 85 94 89 77 768 95 75 80 70 65 77 72 79•4	63 79 84 90 89 95 74 69 93 81 77 73 64 73 69	78 92 84 93 94 78 73 76 70 91 76 76 76 76 64 76	71 84 93 86 94 94 89 76 77 75 75 77 79 72 81 · 7	82 93 84 95 93 88 79 80 69 77 77 82·5 mb.	71 81 91 86 95 93 87 82 81 78 89 75 70 82 71 76 83.6	86 92 86 96 90 83 85 82 81 91 73 77 78 84·5 mb.	89 91 85 96 90 82 89 83 86 87 79 76 79 69 83 78 85.4	89 92 83 96 92 82 87 83 90 87 81 74 77 71 79 81 86.0	90 92 85 97 93 79 87 88 90 84 74 85 86.7 mb.	80·1 88·5 84·4 93·8 82·9 78·5 78·0 91·0 82·7 78·3 76·2 77·2 77·4 83·9	14·4 11·8 13·3 15·3 14·0 14·7 16·4 12·8 12·3 13·8 12·0 14·7 13·3 11·5 11·5 19·9 10·4

Computed from the mean temperatures and the mean relative humidities.

323. Cahirciveen (Valencia Observatory): North Wall Screen: h_t (height of thermometer bulbs above ground) = $1 \cdot 3$ metres. September, 1923.

																										r, 1923.
Day.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
1 2 3 4 5	% 79 84 89 88 82	% 77 86 91 82 79	% 76 87 93 89 77	% 77 86 92 85 79	% 77 90 91 81 79	% 77 90 91 77 81	% 79 89 87 79 82	% 78 81 86 74 81	% 77 82 87 69 83	% 79 76 89 67 82	% 76 71 88 68 79	% 68 70 89 69 79	% 69 71 95 71 78	% 67 73 95 72 78	% 70 74 94 69 79	% 67 75 95 73 79	% 71 75 96 76 78	% 69 78 96 75 81	% 71 81 97 78 82	% 77 87 96 79 80	% 81 88 96 80 78	% 81 88 96 81 80	% 78 89 93 82 81	% 82 91 95 81 79	% 75·1 81·6 92·3 77·2 79·9	mb. 10·5 11·1 13-8 11·4 12·8
6 7 8 9	82 94 91 86 85	85 95 91 90 84	88 95 89 89 84	90 92 94 88 83	93 89 90 88 85	95 88 89 91 86	96 95 91 92 85	95 94 91 95 81	96 90 86 93 81	97 82 81 93 77	96 69 77 92 69	95 67 76 92 64	95 64 74 93 68	97 64 77 94 72	97 66 80 93 68	98 63 80 92 73	95 69 83 89 70	96 73 85 90 74	95 74 86 90 79	96 79 88 82 85	95 83 87 83 84	95 87 88 83 88	94 88 89 80 88	93 89 85 82 89	93·6 81·3 85·4 89·2 79·1	15·4 12·1 12·9 13·7 11·3
11 12 13 14	91 94 93 81 84	93 93 94 82 87	93 93 92 85 85	93 93 91 79 83	96 93 88 82 84	95 93 87 80 81	93 93 93 79 84	93 95 91 80 71	85 95 90 77 69	84 93 93 76 65	80 91 95 75 76	79 90 94 74 76	76 89 93 70 77	78 86 92 69 70	80 85 92 67 71	79 85 87 69	81 89 81 68 63	81 91 87 68 71	83 92 86 68 73	84 91 75 80 66	85 92 78 76 66	88 90 76 79 75	92 91 75 73 72	95 94 88 80 74	86·4 91·3 88·1 75·9 74·5	12·2 15·3 13·6 10·4 9·1
16 17 18 19 20	66 83 77 86 71	65 86 78 84 77	78 78 75 87 67	72 80 75 85 64	73 82 77 87 69	70 81 79 83 68	75 80 86 84 66	73 94 81 85 64	65 95 76 85 67	67 93 67 82 68	75 89 77 82 66	65 82 75 88 69	69 84 78 82 72	69 85 70 83 76	69 88 67 80 76	71 84 67 81 81	7 ² 87 68 83 83	75 79 72 87 93	78 82 76 88 95	78 74 78 89 93	75 73 73 85 93	77 73 81 82 91	76 77 79 74 85	76 76 82 69 80	72.0 82.7 75.5 83.6 76.2	10·9 11·0 9·6
21 22 23 24 25	80 88 86 91 85	86 82 89 92 84	83 79 88 92 84	83 86 78 87 84	86 87 78 85 86	86 85 73 84 90	85 87 71 82 89	85 83 73 84 89	81 76 74 80 87	83 76 78 79 88	85 90 72 85 87	86 78 72 91 81	87 75 73 90 78	89 80 69 89 80	88 75 64 91 81	84 77 71 90 82	80 74 69 90 82	84 77 73 91 88	85 85 73 89 93	83 91 78 85 94	85 91 80 87 93	89 91 83 88 91	85 90 89 85 91	84 89 87 85 91	84·6 82·6 76·7 87·2 86·5	13.0 11.1 10.1 11.5 12.4
26 27 28 29 30	91 94 95 99 79	93 95 96 99 79	95 96 95 100 78	95 94 96 99 79	93 94 97 99 82	93 94 97 97 80	93 94 95 96 80	93 94 93 97 82	92 94 95 97 81	88 94 93 95 84	88 95 96 94 90	87 95 93 93 90	87 96 90 93 90	87 96 85 82 92	87 97 85 82 91	86 97 89 89 93	87 96 92 93 94	96 95 94 95	91 95 96 95 96	92 96 96 94 96	91 95 97 92 96	91 96 97 84 96	93 96 99 84 96	93 97 97 84 96	90·5 95·2 94·1 93·2 87·9	14·1 15·5 14·5 15·8 15·3
Mean							86·o								80 · 2							86.2			84.0	†12.4
Vapour Pressure*	mb.	mb.	mb.	mb. 11 · 6	mb. 11•7	mb. 11·6	mb. 11·8	mb. 12•1	mb.	mb.	mb. 12·6	mb. 12·6												mb. 12·1	mb. ‡12·2	
324. Cahirci													: = :	1.31	metr	es.								(Octobe	r, 1923.
1 2 3 4 5	97 84 95 60 89	% 96 89 95 62 90	% 96 93 93 62 92	93 93 82 63 93	91 95 82 66 95	% 89 93 77 65 95	% 84 87 80 66 95	% 81 82 72 65 93	% 76 73 62 64 92	% 72 75 63 63 84	% 69 65 65 62 87	% 67 64 67 64 83	% 64 61 66 66 81	% 67 71 67 67 83	% 73 69 67 67 87	% 78 71 75 72 83	% 82 74 66 74 81	% 87 78 64 75 89	% 85 79 61 78 86	% 88 78 64 81 86	% 87 79 59 83 84	% 85 82 59 86 88	% 85 88 60 89	% 83 91 61 89 86	% 82·6 79·6 71·5 69·8 87·8	mb. 9·9 11·0 9·1 8·4 12·1
6 7 8 9	85 88 94 96 88	88 84 93 93 87	90 82 87 90 90	87 89 87 89 90	85 92 89 86 90		88 95 91 80 95	84 96 93 79 95	83 96 89 79 95	81 99 88 80 95	77 97 89 78 95	79 95 93 78 97	81 96 94 76 96	83 97 95 76 96	88 99 95 80 93	85 96 96 78 93	87 96 95 79 91	85 96 95 80 92	89 97 96 81 90	88 97 96 83 92	88 95 96 85 92	89 97 95 85 92	89 97 96 88 92	89 88 96 87 91	85·5 94·5 92·7 83·1 92·3	11 · 8 14 · 1 14 · 1 12 · 1 12 · 8
11 12 13 14	89 92 74 76 89	86 89 73 85 87	89 91 73 83 89	93 88 72 83 90	82 89 76 80 90	79 87 70 83 89	90 81 74 83 90	89 81 73 82 87	92 70 72 84 90	90 77 71 80 89	87 76 78 73 86	87 62 68 72 83	88 65 74 67 78	90 65 67 73 78	90 67 65 66 77	91 66 68 65 81	90 65 69 67 81	91 66 76 73 87	91 65 73 76 87	92 65 71 85 91	91 69 69 85 91	91 77 72 91 93	96 79 71 88 91	93 72 78 89 88	92·7 75·6 71·8 78·5 86·8	9·2 8·6 8·2 8·6
16 17 18 19 20	84 89 76 91 92	91 89 77 87 91	88 89 79 81 91	83 91 79 76 91	81 91 77 77 87	87 91 78 71 85	86 93 81 79 85	90 93 83 75 83	92 93 84 75 82	93 96 86 72 82	93 95 87 72 77	88 92 88 76 80	83 90 87 77 78	88 88 88 70 79	88 88 90 70 90	84 88 91 73 90	90 92 91 81 91	91 91 92 77 90	91 92 93 84 92	93 92 95 84 93	93 81 93 87 92	91 89 94 87 93	90 82 95 88 93	91 77 94 88 85	88·6 90·0 86·2 79·2 87·2	11·5 11·9 11·7 9·7 11·6
21 22 23 24 25	89 84 92 86 87	87 84 91 84 84	81 82 92 81 88	73 80 95 85 88	70 81 92 84 85	70 85 86 81 81	80 71 83 84 87	75 72 78 86 81	76 70 71 86 76	77 76 76 85 81	77 81 79 83 70	85 85 77 78 68	85 78 78 83 73	87 83 81 86 70	82 79 80 80 65	86 81 84 80 70	79 85 81 82 74	84 91 77 83 84	85 89 91 88 85	81 87 85 85 83	84 88 87 83 85	84 88 89 84 86	78 91 86 84 85	79 88 86 87 86	80·7 82·3 84·1 83·6 80·1	9·6 10·1 9·8 9·5 9·0
26 27 28 29 30	86 87 79 82 95	79 81 77 85 93	80 77 77 86 95	89 78 77 87 93	91 85 74 91 92	87 77 79 92 91	86 83 75 93 92	88 85 73 91 89	89 82 72 93 85	78 81 71 93 84	86 85 73 92 84	80 83 72 93 81	81 72 96 78	82 80 74 97 74	87 81 76 99 83	83 87 75 95 81	85 91 71 95 82	87 88 70 95 81	89 82 73 96 83	89 78 76 94 82	89 78 78 95 83	78 82 82 95 82	83 88 82 95 83	86 75 82 96 86	84·9 82·5 75·3 92·5 85·7	10·1 9·4 9·3 13·1 11·5
31	86	85	88	82	8o	79	83	76 ——	76	65	76	75	75	78	81	81	85	86	85	86	86	86	86	86	81.3	10.0
												79:4	79 · 0	8o·0	80 · 7	81.5	82.3	83 · 9	84 · 9	85.2	85.0	86.2	86 · 5	85.6	83·4	†10.7
Vapour Pressure*	mb. 10·8	mb. 10·7	mb. 10·7	mb. 10·5	mb. 10·6	mb. 10·3	mb. 10·5	mb. 10·3	ть. 10·2	mb. 10·5	mb. 10·5	mb. 10·6	mb. 10·8	mb. 10·8	mb. 10·9	mb. 10·9	mb. 10·7	mb.	mb. 10.7	mb.	10.6	10·6	10.6	mb. 10·6	mb. ‡10·6	
Hour G.M.T.	r.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	_

^{*} Computed from the mean temperatures and the mean relative humidities.

[†] Mean of the column.

[‡] Mean of the row.

RELATIVE HUMIDITY.

Percentages at exact hours, Greenwich Mean Time. Determined as explained on page 16.

325. Cahirciveen (Valencia Observatory): North Wall Screen: ht (height of thermometer bulbs above ground) = 1.3 metres.

November, 1923.

							· y / ·																		vembe	r, 1923.
Day.	ı.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
1 2 3 4 5	% 83 74 92 73 85	% 85 73 90 70 86	% 85 75 90 71 87	% 85 74 90 70 86	% 83 76 91 75 83	% 83 83 91 74 87	% 83 83 88 81 89	% 84 85 88 79 86	% 86 92 88 77 89	% 81 93 89 78 86	% 78 95 82 73 85	% 79 97 81 75 79	% 82 95 75 72 76	% 87 95 71 73 71	% 88 96 69 73 71	% 88 95 77 73 73	% 84 95 81 77 79	% 76 95 74 79 85	% 78 96 76 80 83	% 74 96 69 79 82	% 75 96 71 84 79	% 80 96 75 80 81	% 76 95 71 85 84	% 73 93 64 86 79	% 81·8 88·9 81·1 76·1 82·3	mb. 9·8 11·3 10·5 8·4 8·0
6 7 8 9 10	84 81 96 68 71	88 76 95 72 76	85 76 96 71 72	87 80 93 69 76	85 76 88 70 80	82 75 86 76 80	79 69 82 83 82	79 71 85 87 83	80 71 85 80 79	71 80 83 77 75	63 80 79 69 73	61 78 76 66 75	60 79 76 69 77	59 92 79 67 70	59 93 79 63 76	69 93 84 65 71	63 93 79 63 79	77 93 78 62 81	84 93 76 63 85	88 93 71 67 82	89 96 74 69 83	90 96 77 73 83	90 96 72 73 88	93 96 68 72 88	77·4 84·4 82·1 70·5 78·2	6·9 8·7 8·7 7·6 7·3
11 12 13 14 15	88 96 97 60 82	87 95 96 58 87	88 97 97 61 91	88 96 96 75 92	87 95 95 64 91	85 97 93 75 91	86 97 92 67 75	86 97 93 79 75	83 96 93 68 81	83 96 93 82 78	86 96 93 66 80	84 96 95 75 72	83 97 93 67 73	86 99 93 68 70	85 99 95 74 76	87 97 92 72 70	92 97 91 75 71	92 97 91 72 70	95 97 86 76 66	96 96 83 73 70	96 99 80 83 72	96 96 79 84 70	95 96 77 84 79	99 96 70 85 82	88·6 96·7 90·7 72·3 77·7	9·3 12·5 11·7 6·9 8·4
16 17 18 19 20	88 72 73 81 71	81 72 72 83 74	74 73 71 82 71	79 72 80 81 72	73 74 76 73 79	75 81 84 71 74	83 81 73 68 79	71 77 73 70 79	79 68 73 75 79	73 77 67 77	71 83 71 75 76	70 84 75 78 76	75 81 73 73 76	68 71 75 67 81	69 66 77 68 73	71 70 78 67 81	87 74 73 67 82	89 80 79 73 81	87 81 78 69 81	85 81 81 80 77	79 83 77 73 83	76 75 78 81 81	82 78 71 73 82	79 87 67 78 83	77·7 76·5 75·2 74·1 77·7	7·8 7·1 7·2 7·0 7·0
21 22 23 24 25	83 87 83 85 83	80 87 83 87 86	83 87 85 83 77	82 85 82 85 77	83 87 81 85 83	88 87 81 85 83	90 87 82 83 83	89 85 85 80 81	88 85 82 80 81	87 81 75 85 82	88 78 79 85 87	81 74 73 82 79	75 71 74 81 85	74 68 74 80 87	76 70 71 83 85	82 78 72 85 86	83 77 77 85 90	88 83 77 87 94	88 82 77 81 89	88 81 79 80 91	89 79 80 80 91	87 81 81 80 91	87 81 83 83 90	89 81 85 83 89	84·4 81·1 79·1 83·1 85·3	6·6 5·7 5·2 6·2
26 27 28 29 30	93 91 83 81 87	93 89 76 80 83	93 91 81 85 83	91 87 77 89 83	91 91 75 85 83	91 91 77 89 77	90 91 75 90 80	90 89 75 90 83	90 91 77 85 79	87 90 81 85 80	88 90 77 90 81	82 90 77 83 81	87 89 80 78 84	93 91 76 77 82	93 88 77 78 81	91 87 82 79 81	89 88 83 81 89	89 87 81 83 95	89 83 82 79 96	89 83 82 83 96	91 81 81 81 97	91 81 82 83 99	89 81 83 85 92	91 77 83 87 93	90·0 87·7 79·2 83·5 85·9	7·1 6·3 5·5 6·3 6·7
Vapour	mb.	mb.	mb.	mb.	mb.	mb.	82·4 mb.	mb.	mb.	mb.	mb.	mb.	78·5 mb.	mb.	mb.	mb.	mb.	82·9 mb.	mb.	mb.	mb.	mb.	mb.	mb.	8r·6	†7·8
Pressure* 326. Cahirci			7·3 lenci		7·3 bserv		·	7·2 Nor			7·9 Scree	7·9					7.9	7.9	7.0	7.7	7.5	7.3	7.4			r, 1923.
I	% 93	%	% 95	% 94	% 95 82	%	% 89	% 91	% 90	% 91	% %	% 90	% 91	% 85	% 87	% 89	% 93	% 93	% 92	% 92	% 89	% 89	% 85	% 85	% 90·8	mb. 9·1
2 3 4 5	76 79 84 80	94 83 82 91 80	79 78 80 82	77 82 83 83	82 79 77 79	93 78 67 81 77	82 69 81 81	88 77 87 80	76 77 81 76	81 87 85 73	73 72 85 72	78 72 78 67	73 72 85 71	73 75 86 71	73 78 87 73	75 85 85 70	72 82 87 69	70 87 93 73	59 90 91 77	60 93 91 73	77 95 94 73	78 96 93 72	85 95 90 74	83 91 99 77	76·3 81·5 86·3 75·6	7·3 7·8 8·5 7·5
6 7 8 9 10	75 93 76 82 92	80 95 67 80 92	82 95 68 80 91	87 93 69 76 92	85 95 74 78 89	88 96 66 75 91	87 97 76 78 91	88 96 72 80 92	89 95 78 85 91	88 93 76 85 92	88 96 83 84 92	85 95 71 87 92	86 91 72 87 89	81 89 64 92 91	82 85 70 92 89	83 83 76 91 88	83 84 75 91 89	85 85 68 91 92	89 89 69 92 92	87 82 72 92 92	90 81 83 92 91	91 72 85 93 89	91 71 81 91 88	91 71 81 91 87	85·6 88·8 73·6 85·8 90·7	7·9 10·2 7·1 8·4 10·9
11 12 13 14 15	88 92 83 89 82	87 92 82 89 79	88 89 89 90 75	83 89 90 87 68	87 89 91 86 68	87 89 91 84 68	88 89 93 83 75	89 88 92 83 72	87 92 93 82 68	87 92 91 83 69	86 92 91 83 72	83 92 89 81 73	82 92 90 82 77	86 93 91 84 72	86 93 91 86 72	89 93 90 88 72	88 95 91 93 75	89 93 94 95 77	88 95 89 93 76	85 90 93 84 76	83 89 91 83 77	86 87 93 84 78	88 83 91 79 78	88 77 90 80 81	86·6 90·4 90·1 85·7 74·1	10·5 10·7 8·0 9·5 7·8
16 17 18 19 20	83 93 93 73 63	83 96 93 78 64	87 95 95 73 63	93 92 95 85 64	96 93 96 83 64	95 92 97 83 61	96 93 95 80 62	96 93 96 87 62	97 95 93 87 64	97 93 95 80 58	96 93 92 77 65	96 95 87 80 66	95 95 77 73 66	96 93 78 73 68	93 92 79 66 70	93 91 75 65 71	91 93 83 64 73	91 93 80 67 79	92 93 78 65 82	93 92 75 69 84	91 95 79 66 85	89 95 81 63 87	91 95 80 62 87	92 92 80 63 87	92·4 93·4 86·6 73·8 70·1	10·6 11·1 9·8 7·4 6·1
21 22 23 24 25	79 83 93 95 89	73 84 93 97 94	74 80 93 95 94	75 82 89 93 95	77 87 74 93 95	81 70 95 97	89 81 67 96 95	92 87 69 95 97	93 85 69 96 96	92 87 70 96 97	93 82 71 96 97	91 85 69 96 97	93 83 75 95 97	93 83 76 97 96	95 87 77 96 97	95 86 79 92 99	92 88 75 89 97	92 88 75 91 97	92 86 76 87 97	92 91 76 86 91	95 92 84 86 88	88 95 91 87 85	82 95 93 90 87	78 96 93 89 85	87·5 86·0 79·1 92·9 94·2	9·7 10·6 8·7 10·9
26 27 28 29 30	87 86 92 88 92	85 86 83 87 93	85 86 75 89 91	85 85 74 89 89	81 92 77 91 87	81 93 76 93 87	83 95 75 93 85	86 95 76 91 82	86 95 71 93 82	91 93 72 95 91	93 91 74 95 88	95 96 71 93 88	96 93 75 96 81	96 92 72 96 80	96 95 70 99 81	95 96 77 97 81	95 95 81 97 81	95 95 84 97 83	97 92 83 96 81	93 91 87 96 81	93 92 86 95 83	91 93 89 92 83	91 91 87 92 88	89 89 87 92 88	90·1 92·0 79·0 93·3 95·3	11·1 11·4 8·6 10·5 11·4
31	92	92	92	92	92	93	92	93	95	96	93	95	95	93	97	96	96	96	99	96	96	96	97	99	94.5	11.3
Mean Vapour	85·3 mb.	85·6 mb.	84·8 mb.	mb.	mb.	mb.	mb.	86·2 mb.	mb.	mb.	85·6 mb.	84·9 mb.	84·7 mb.	mb.	mb.	85·3 mb.	mb.	mb.	86·4 mb.	mb.	mb.	86·8 mb.	mb.	mb.	85·5 mb.	<u>†9·4</u>
Pressure*	9.2	9.3	9.2	<u>6.1</u>	9.1	8.9	9.0	9.1	9.1		9.4	9.5		9.5	9.6	9.5	9.5	9.5	9.4	9.3	9.3	9.3			‡9·3	
Hour G.M.T.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	_

[•] Computed from the mean temperatures and the mean relative humidities.

[†] Mean of the column.

From the monthly means for exact hours, Greenwich Mean Time.

Cahirciveen (Valencia Observatory): North Wall Screen: $h_t = 1.3$ metres. 327.

1923.

G.M.T.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
Relative Humidity	% 84·9	% 85·1	% 85·0	% 85·0	% 85·2	% 84·9	% 84·6	% 83·8	% 82·6	% 81·6	% 80·6	% 79·5	% 79·0	% 78.8	% 79·0	% 79·1	% 79·7	% 81·1	% 82·2	% 82·7	% 83·5	% 84·1	% 84·4	% 84·4	% 82·5
		mb.	mb.	mb.	mb. I	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb. 1	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	

RELATIVE HUMIDITY: MONTHLY MEANS AND DIURNAL INEQUALITIES.

The departures from the mean of the day are adjusted for non-cyclic change.

Cahirciveen (Valencia Observatory): North Wall Screen: $h_t = 1.3$ metres.

1923.

Month.	Mean.		G.M.T. 2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.
Jan. Feb. Mar.	84.4		% +1·0 +1·3 +3·5		+1.4	+2.0	-0.3	+0.4	% +0·7 +1·3 +3·6	+1.0		+0.5	% -2·0 -0·9 -4·7	-2.3	-2·7	-1.4	_	% -0.8 -2.2 -4.5	-1.2	% -0·9 -0·2 +0·1	+0.1	% +0·4 +0·1 +0·6	-0.1	% + 1·8 +o·6 +···	% +0·8 +0·5 +1·7
April May June	77.2	+4.0	+3.8	+4·4 +3·3 +3·9	+3.9	+3.7	+4.1	+2.8	+0.9	-1.1	-1·9 -3·0 -2·1	-3.3	-3·8 -4·2 -3·9	-4.7	-5.4	-5.7	-4.6	-4·5 -3·5 -4·4	-2.2	-1·5 -1·0 -1·1	0.0	+1.9	+2.8	+1·9 +3·9 +1·7	+3.5
July Aug. Sept.	83.9	+3.4	+3.6	+3·6 +3·3 +2·5	+3.1	+4.5	+4.0	+3.3	+1.4	+0.1	-1·1 -1·0 -1·7	-2.4	-2·9 -4·0 -3·1	-4.2	-4·3 -4·4 -3·5	-4·7 -4·5 -3·9	-4.6	- 5·3 - 4· 5 - 3· 0	-2.2	-I·4	-0.4	+0.6	+1.4	+2·6 +2·1 +1·3	+2.7
Oct. Nov. Dec.	81.6	+2·9 +o·8 -o·1	+o·5	+2·1 +0·5 -0·7	+1·6 +1·1	+0.4	+1.5	+o·8	+0.0	-2·2 +0·4 +0·2	0.0	I · I	-4·I -2·5 -0·6	-3.1	-3.5		-1.8	-0.2	+1.2	+1.6 +0.8 +0.7	+o·8	+1.3	+1.7	+3·2 +1·6 +0·7	+1.4
Year	82.5	+2.4	+2.6	+2.5	+2.5	+2.7	+2.4	+2·1	+1.3	+0.1	-1.0	-1.9	-3·o	-3.2	-3.8	-3.6	-3.4	2.8	-1.4	-0.4	+0.3	+0.9	+1.6	+1.0	+1.9

RAINFALL: ANNUAL TOTALS OF HOURLY VALUES.

Amounts, in millimetres, for periods of sixty minutes between the exact hours, Greenwich Mean Time.

Cahirciveen (Valencia Observatory): H_r (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + h_r (height of receiving 1923. surface above ground) = $9 \cdot 1$ metres + $0 \cdot 5$ metres.

G.M.T.	-	,	to I.	to 2.	to 3.	3 to 4.	to 5.	5 to 6.	6 to 7.	7 to 8.	8 to 9.	9 to 10.	to	to Noon	Noon to 13	13 to 14.	14 to 15.	15 to 16.	16 to 17.	17 to 18.	18 to 19.	19 to 20.	20 to 21.	2I to 22.	to 23.	23 to 24.	o to 24.
Amount			mm. 84·5	mm. 84·4	mm. 76·9	mm. 70·0	mm. 61·4	mm. 69·5	mm. 68·8	mm. 64·9	mm. 51 ·6	mm. 55·2	mm. 55·1	mm. 55·6	mm. 61·5	mm. 60·1	mm. 61·4	mm. 60·9							mm. 55 [.] 9		mm. 1522 · O
Duration	•••	•••	hr. 38·2	hr. 34·2	hr. 36·1	hr. 33·1	hr. 33·3	hr. 35 [.] 9	hr. 33·5	hr. 31·9	hr. 32.0	hr. 32·8		hr. 27·1	hr. 31·5	hr. 30·9	hr. 30·5	hr. 30·0	hr. 29·1	hr. 34'7	hr. 36·7	hr. 37·2	hr. 34·I	hr. 33°2	hr. 35·2	hr. 37 [.] 5	hr. 796·2

330. Cahirciveen (Valencia Observatory).

interval was experienced from the 22nd June to the 1st July.

NOTES ON RAINFALL.

1923.

Notable Falls of the Year.—There were no occasions of very remarkable rainfall during 1923. The heaviest hourly rainfall shown in the tables is 10.2 mm., experienced between 19 h. and 20 h. on the 20th October. On the 24th September, 28 mm. fell in the six hours between 11 h. and 17 h.; on the 16th February, 26 mm. were registered in the

five hours from 11 h. to 16 h.; on the 23rd August, between 4 h. and 9h. 20 mm. were recorded, of which 17 mm. fell between 6 h. and 9 h. Dry Periods.—Absolutely dry periods were few and of no great length. For the ten days from the 14th to the 23rd March inclusive, no rain was recorded and a similar dry

-Rain fell on every day from the 15th February to the 8th March, an interval of 22 days; from the 11th September to the 3rd October, 23 days; and again from the 18th October to the 9th November, 23 days. In this last period only three days had less than 1 mm. of rain.

Amounts in millimetres, for periods of sixty minutes, between the exact hours, Greenwich Mean Time.

331. Cahirciveen (Valencia Observatory): Hr (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + hr (height of receiving surface above ground) = 9·1 metres + 0·5 metres.

January, 1923.

Day.	0-1	1-2	2-3	3-4	4-5	5–6	6-7	7-8	8–9	9–10	10–11	11–12	12–13	13–14	14-15	15–16	16–17	17–18	18–19	19–20	20-21	21-22	22-23	23-24	0-24	tion 0-24
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm. 5·9	hr.
I 2								·6	1.0	1.4	2.4			• 2			••2					1.2	8	.3	5.0	3.2
3 4	·r								·6 			•••							·6 		•2	•4	٠	··· ··7 ··2	3.4 1.4 9.0	1.8
5	1.2	•5	• 5	⋅8	2.2	2.3	.1	.3		•••	•••	•••		.1	• 2	•••			•••		•6		•••	·1	7.2	5.5
6 7								:::			• • • • • • • • • • • • • • • • • • • •						.1 1.0	·1	2·1	1.3	·1	.1	• 2	•4	1.6	2.2
8	1.0	•4					•••						 ·6		• • • • • • • • • • • • • • • • • • • •	···	•••	• • • • • • • • • • • • • • • • • • • •		·		1.4	1.2		4·7 5·8	3.6
10 9	·5	1.3		•2		• 2	•••	•6		•4				.6	1.8	•2	.7	.1			.0	•••	•2	.1	6∙0	2.8
11	٠1		•6			•6			•4								•••								2.1	1.:
12 13						• • 2	••2	•4	• • 2		.1	.1		.3	.1		•••				:::	···			2.3	3.
14 15			:::									••2	• 5	• • 2	:::		٠		• 2	•••					1.3	2.
16					•4													1.3							0.4	0.
17 18							-::																			٠.
19 20											:::			:::		••2	•••								0.3	0.
21						.1	•т																		0.5	٥٠
22													:::	:::					:::				• 1	•4	0.5	0.
23 24	:::					.1	•••		•••																0·1	0.
25						•••	•••	•••	•••	•••	***															
26 27						:::	•••										•••				l		· 4		0.6	0.
28 29							•••			:::		·				•4		••2							1.0	1.
30			·I			•••	•••		•••	•••						.3	1.1	.8	.3	.3					1	2.
31		<u></u>			.2				.3	-3		.3	·1	1.0	.6			4.8		2.2	2.3	3.7	3.2	3.1	98·1	3.
Sum.	3.1	2.5	2.3	1.5	4.3	4.7	0.4	1.9	2.8	2.8	3.6	1.6	1.2	2.4	3.6	2.7	3.5	<u> </u>	3.9		hr.	hr.	hr.	hr.	hr.	-,,,
Total Dura-	hr. 2·6	hr. 1 · 6	hr. 2·4	hr. 1 · 7	hr. 2·1	hr. 2·5	hr. 0.7	hr. 1 · 8	hr. 2·4	hr. 2·0	hr. 1·9	hr. 1·4	hr. 1•9	hr. 2·3	hr. 2·8	hr. 2.8	hr. 2·4	hr. 3.7	hr. 2.5	hr. 2·1	1.4	2.4	2.8	1	23.1	
tion.			[1			'					l	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	1	<u> </u>	1	<u></u>	1	<u> </u>
332.	Cah	ircive	en (V	/alenc	ia Ob		•	: Hr	= 9.	ı me	tres -	- o·5	meti	res.	i	<u> </u>				<u> </u>	1,		F	ebrua	ry, 19	23.
332.	Cah	ircive	en (V	alenc	mm.	serva	tory)	: Hr	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	ebrua	mm.	hr
						serva	tory)					,		mm.	mm. 1·3	mm.							mm.	mm.	mm. 5:3 1:8	3 ·
332. 1 2 3	mm.	mm. 	mm.	mm. 	mm. 1·8 	mm. 1 · I 	tory)	mm. I·I	mm.	mm. .4 	mm.	mm.	mm.	mm.	1.3					 I·I			mm.	mm2	mm. 5:3 1:8 2:7	1 · · · · · · · · · · · · · · · · · · ·
332.	mm.	mm.	mm.	mm.	mm. 1 · 8	mm.	mm4 -2	mm.	mm. '3 '5	mm. '4	mm.	mm.	mm.	mm. .8	1.3					1 · 1	3.3		mm.	mm2	mm. 5·3 1·8 2·7 	hr 3. 1. 6.
332. 1 2 3 4 5	mm.	mm 7.3	mm.	mm	mm. 1·8 	mm. I·I ·3 I·2	tory) mm. '4 '2	mm I·I	mm. '3 '5 I·I '2	mm.	mm.	mm.	mm	mm. .8 	1·3 ·2	·	···· ··· ··· ··· ··· ··· ··· ···		•2	 I·I			mm.	mm2	mm. 5:3 1:8 2:7	3. 1. 6. 6.
332. I 2 3 4 5	mm.	mm.	mm.	mm.	mm. 1·8 	**************************************	mm4 -2	mm. 	mm3 -5 1-1	mm.	mm	mm 1.6	mm	mm. .8 	1·3 ·2 .3 1·7	··· ··· ··· ··· ··· ··· ··· ··· ···	··· ··· ··· ··· ··· ··· ··· ··· ··· ··	··· ·· ·· ·· · · · · · · · · · · · · ·	 •2 4•9	··· ··· ··· ··· ···	3·3 ·8 ·1	 I·9 2·0	mm67	mm ·2 1·8	mm. 5·3 1·8 2·7 10·5 23·2 21·9 5·0	hi 3: 1: 6: 6: 6:
332. I 2 3 4 5 6 7 8 9	mm 3.5	mm 7.3	mm 5.3 2.1	mm 1.8 5.8	mm. 1·8 1·8 3·9	mm. 1 · I 3 1 · 2 1 · 3	mm4 -2	mm I·I	mm3 -5 1-1 -2	mm.	mm	mm.	mm	mm. .8 	1·3 		··· ··· ··· ··4 ··ɪ ···	 .1 .2 .2	··· ··· ··· 4·9	··· ··· ··· ··· ···	3.3 .8	 1·9	mm6	mm2 I.8	mm. 5.3 1.8 2.7 10.5	hi 3: 1: 6: 6: 4:
332. I 2 3 4 5 6 7 8 9	mm	mm 7:3	mm 5:3 2:1 .3	mm 1.8 5.8	mm. 1·8 1·8 3·9	**************************************	tory) mm. '4 '2 '7 '5	mm I·I	mm.	mm.	mm	mm 1.6	mm 3.1	mm. .8 4 2·3	1·3 .2 .3 1·7 2·5	··· ··· ··· ··· ··· ··· ··· ··· ··· ··	··· ··· ··· ··· ··· ··· ··· ··· ··· ··	 .:I .:. .:1 .:2 .:2 .:.	 ·2 4·9	··· ··· ··· ··· ··· ··· ··· ··· ···	3·3 ·8 ·1 ···	 1·9 2·0	mm. 	mm	mm. 5°3 1°8 2°7 10°5 23°2 21°9 5°0 13°3 0°3	6. 6. 6. 4.
332. 1 2 3 4 5 6 7 8 9 10 11 12	mm	mm 7.3	mm 5'3 2'1 '3	mm 1.8 5.8	mm. 1·8 1·8 3·9	**************************************	**************************************	mm I·I	mm3 -5	mm.	mm	mm 1.6 3.5 .3	mm 3.1 4	mm8	1·3	··· ··· ··· ··· ··· ··· ··· ··· ··· ··	···· ··· ··· ··· ··· ··· ··· ··· ··· ·	 .:I .:. .:I .:2 .:2 	 .2 4.9 	 I·I ·4	3.3	 I·9 2·0	mm. .6 .7 	mm2 1.8	mm. 5'3 1'8 2'7 10'5 23'2 21'9 5'0 13'3 0'3	6.66662.4.00.2.
332. 1 2 3 4 5 6 7 8 9 10 11	mm	mm 7:3	mm 5:3 2:1 .3	mm 1.8 5.8	mm. 1·8 1·8 3·9	mm. 1 · I 3 1 · 2 1 · 3	**************************************	mm I·I	mm3 -5	mm. '4 '4 '4 ' ' '	mm	mm 1.6 3.5 .3	mm 3.1	mm8	1·3	··· ··· ··· ··· ··· ··· ··· ··· ··· ··	··· ··· ··· ··· ··· ··· ··· ··· ··· ··		 .2 4.9 		3·3 ·8 ·1 ··· ···	 1·9 2·0 	mm	mm	mm. 5°3 1°8 2°7 10°5 23°2 21°9 5°0 13°3 0°3 0°8 3°0	6.6.6.6.2.4.0.0.0.2.3.
332. 1 2 3 4 5 6 7 8 9 10 11 12 13	mm	mm 7.3	mm	mm 1.8 5.8	mm. 1 · 8 1 · 8 3 · 9 4 · 4 · 5	mm. 1·I 3 1·2 1·3	mm. · 4 · 2 · · · · · · · · · · · · · · · ·	mm I·I	mm3 -5	mm.	mm	mm 1.6 3.5 .3 2.6	mm 3.1 4 2.9	mm8	1·3	 	······································		 .2 4.9 		3·3 -8 -1	1·9 2·0	mm.	mm 1.8	mm. 5·3 1·8 2·7 10·5 23·2 21·9 5·0 13·3 0·8 3·0 2·4 22·9	hi 3: 1: 6: 6: 6: 4: 0: 2: 4: 0: 3: 0:
332. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	mm	mm	mm 5.3 2.1 .3	mm 1.8 5.8	mm. 1·8 1·8 3·9	**************************************	**************************************	mm 1·1	mm3 -5	mm.	mm	mm 1.6 3.55 .3 2.6	mm 3.1	mm84 2.34 2.3	1·3	··· ··· ··· ··· ··· ··· ··· ··· ··· ··	··· ··· ··· ··· ··· ··· ··· ··· ··· ··		 .2 4.9 	 1·1 ·4 	3·3 -8 -1	 1·9 2·0 	mm	mm	mm. 5'3 1'8 2'7 10'5 23'2 21'9 5'0 13'3 0'3 0'8 3'0 2'4 22'9 32'0 18'2	6 6 6 6 2 2 4 0 0 0 2 2 3 3 2 2 9 8 8 8
332. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	mm	mm	mm 5.3 2.1 .3	mm 1.8 5.8	mm. 1·8 1·8 3·9	**************************************	**************************************	mm 1·1	mm3 -5	mm.	mm	mm 1.6 3.5 .3 2.6	mm 3.1 4 2.9	mm8	1·3	 	··· ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·		 -2 4.9 -4 		3·3 -8 -1	 I·9 2·0 	mm	mm 1.8	mm. 5 · 3 1 · 8 2 · 7 10 · 5 23 · 2 21 · 9 5 · 0 13 · 3 0 · 3 0 · 8 3 · 0 2 · 4 22 · 9 32 · 0 18 · 2 9 · 8	hi 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
332. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	mm	mm	mm 5.3 2.1 .3	mm 1.8 5.8 1.2	mm. 1 · 8 1 · 8 3 · 9	mm. 1·I 3 1·2 1·3	**************************************	mm 1·1	mm3 -5	mm. '4 '4 '6 2'9	mm	mm 1.6 3.55 .3 2.6	mm 3.1 2.9 6.2 3.5	mm84 2.3	1·3	 	 		 .2 4.9 	 1·1 ·4 ·4 	3·3 -8 -1	2·0	mm	mm2 1.8 4.0	mm. 5'3 1'8 2'7 10'5 23'2 21'9 5'0 13'3 0'3 0'8 3'0 2'4 22'9 32'0 18'2	hi 3. 1. 6. 6. 6. 6. 6. 6. 7. 9. 9. 8. 3. 9.
332. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	mm	mm 7.3	mm 5.3 2.1 .3	mm 1.8 5.8 1.2	mm. 1·8 1·8 3·9	### SOFVA Mmm. I · I	**************************************	mm 1·1 3·6	mm3 -5	mm. '4 '4 '6 2'9	mm	mm 1.6 3.5 .3 2.6 4.0	mm 3.1 4 2.9 6.2 3.5	mm8	1·3	 			 -2 4.9 -4 4.3	 1·1 · 	 3·3 ·8 ·1 	 1.9 2.0 	mm.	mm2 1.8 4.0	mm. 5'3 1'8 2'7 10'5 23'2 21'9 5'0 13'3 0'3 0'8 3'0 2'4 22'9 32'0 18'2 9'8 0'3 14'7 7'1	h: 3: 1: 6: 6: 6: 6: 6: 2: 4: 0: 0: 2: 3: 3: 0: 4: 3: 3: 0: 4: 3: 3: 3: 0: 4: 3: 3: 3: 3: 3: 3: 3: 3: 3: 3: 3: 3: 3:
332. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	mm	mm	mm 5.3 2.1 .3	mm 1.8 5.8 1.2	mm. 1·8 1·8 3·9	**************************************	**************************************	mm 1·1 3·6	mm. '3 '5 I'I '2 I'8 '7 I'5 '2 1.8	mm.	mm	mm 1.6 3.55 .3 2.6 4.0 1.5 2.2	mm 3.1 2.9 6.2 3.5	mm8	1·3	 		 	 4.9 4.3	 1·1 ·4 3·0	 3·3 ·8 ·1 	 1·9 2·0 	mm	mm	mm. 5 · 3 1 · 8 2 · 7 10 · 5 23 · 2 21 · 9 5 · 0 13 · 3 0 · 3 0 · 8 3 · 0 2 · 4 22 · 9 32 · 0 18 · 2 9 · 8 0 · 3 14 · 7 7 · 1 5 · 3 17 · 7	6.6.6.2.4.0.0.2.3.3.0.4.3.3.9.
332. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	mm 3.5	mm 7.3	mm 5.3 2.1 .3	mm 1.8 5.8	mm. 1·8 1·8 3·9	**************************************	**************************************	mm 1·1 3·6	mm. '3 '5 I'I '2 I'8 '7 I'5	mm. '4 '4 '6 2'9 I'7 '1 '9 '2	mm	mm 1.6 3.5 .3 2.6 4.0 1.5	mm 3.1 2.9 6.2 3.5	mm84 2.342 7.3 3.0 .6	1·3	 			 4.9 4.3	 1·1 ·4 3·0 	3·3 -8 -1	 1·9	mm	mm	mm. 5 · 3 1 · 8 2 · 7 10 · 5 23 · 2 21 · 9 5 · 0 13 · 3 0 · 8 3 · 0 2 · 4 22 · 9 32 · 0 18 · 2 9 · 8 0 · 3 14 · 7 7 · 1 5 · 3	hi 3: 1: 6: 6: 6: 6: 6: 6: 6: 6
332. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	mm	mm 7.3	mm 5.3 2.1 .3	mm 1.8 5.8 1.2	mm. 1·8 1·8 3·9	### SOFVA Mm. 1 · 1	**************************************	mm 1·1 3·6	mm. '3 '5 I'I '2 I'8 '7 I'5 '2 1.8	mm.	mm	mm 1.6 3.5 .3 2.6 4.0 1.5	mm 3.I 2.9 6.2 3.5	mm8	1·3	 			 4.9 	1·1 ·4 3·0 1·3 7	 3·3 ·8 ·1 2·3 2·3	 1·9 2·0 i i i	mm	mm	mm. 5 · 3 1 · 8 2 · 7 10 · 5 23 · 2 21 · 9 5 · 0 13 · 3 0 · 8 3 · 0 2 · 4 22 · 9 32 · 0 18 · 2 9 · 8 0 · 3 14 · 7 7 · 1 5 · 3 17 · 7 0 · 3 8 · 8	hi 3: 1: 6: 6: 6: 6: 6: 6: 6: 6
332. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	mm 3.5	mm 7.3	mm 5.3 2.1 .3	mm 1.8 5.8	mm. 1·8 1·8 3·9	**************************************	**************************************	mm 1·1 3·6	mm. '3 '5 I'I '2 I'8 '7 I'5	mm. '4 '4 '6 2'9 I'7 '1 '9 '2	mm	mm 1.6 3.5 .3 2.6 4.0 1.5	mm 3.1 2.9 6.2 3.5	mm84 2.342 7.3 3.0 .6	1·3	 			 4.9 4.3 2.6 	1·1 1·4 3·0 1·3 7	 3·3 ·8 ·1 	 1·9 2·0 i i i	mm	mm	mm. 5 · 3 1 · 8 2 · 7 10 · 5 23 · 2 21 · 9 5 · 0 13 · 3 0 · 3 0 · 8 3 · 0 2 · 4 22 · 9 32 · 0 18 · 2 9 · 8 0 · 3 14 · 7 7 · 1 5 · 3 17 · 7 0 · 3 8 · 8 33 · 3 11 · 4	hi 3.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1
332. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	mm 3.5	mm 7.3	mm 5.3 2.1 .3	mm 1.8 5.8	mm. 1·8 1·8 3·9	**************************************	**************************************	mm 1·1 3·6	mm. '3 '5 I'I '2 I'8 '7 I'5 '7 I 3 I 2	mm.	mm	mm 1.6 3.5 .3 2.6 4.0 1.5	mm 3.1 2.9 6.2 3.5	mm	1·3	 			 4.9 4.3 2.6 9	1·1 ·4 3·0 1·3 3·0 1·3 7	 3·3 ·8 ·1 2·3 2·3 2·3 	 1·9 2·0 1·4 	mm	mm	mm. 5:3 1:8 2:7 10:5 23:2 21:9 5:0 13:3 0:3 0:8 3:0 2:4 22:9 32:0 18:2 9:8 0:3 14:7 7:1 5:3 17:7 0:3 8:8	hit 3: 6: 6: 6: 6: 6: 6: 6: 6: 6: 6: 6: 6: 6:
332. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	mm 3.5	mm 7.3	mm 5.3 2.1 .3	mm 1.8 5.8	mm. 1·8 1·8 3·9	**************************************	tory) mm.	mm 1·1 3·6	mm. '3 '5 I'I '2 I'8 '7 I'5 '7 I 13 '7 I 2 I 2 I 2	mm.	mm	mm 1.6 3.5 .3 2.6 4.0 1.5	mm 3 2.9 6.2 3.5	mm	1·3	 			 4.9 4.3 2.6 9 2.2 	 1·1 ·4 3·0 3·0 1·3 7 8·3	 3·3 .8 .1 	 1·9 2·0 6·3	mm	mm	mm. 5 · 3 1 · 8 2 · 7 10 · 5 23 · 2 21 · 9 5 · 0 13 · 3 0 · 3 0 · 8 3 · 0 2 · 4 22 · 9 32 · 0 18 · 2 9 · 8 0 · 3 14 · 7 7 · 1 5 · 3 17 · 7 0 · 3 8 · 8 33 · 3 11 · 4 3 · 4 275 · 4	htt 3: 6: 6: 6: 6: 6: 6: 6: 6: 6: 6: 6: 6: 6:
332. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	mm 3.5	mm 7.3	mm 5.3 2.1 .3	mm 1.8 5.8	mm. 1·8 1·8 3·9	**************************************	**************************************	mm 1·1 3·6	mm. '3 '5 I'I '2 I'8 '7 I'5 '7 II -3 I'2 '7 II -3 I'2 I'2 I'2 I'2	mm.	mm	mm 1.6 3.5 .3 2.6 4.0 1.5	mm 3.1 2.9 6.2 3.5	mm	1·3	 			 4.9 4.3 2.6 9	1·1 ·4 3·0 1·3 3·0 1·3 7	 3·3 ·8 ·1 2·3 2·3 2·3 	 1·9 2·0 1·4 	mm	mm	mm. 5:3 1:8 2:7 10:5 23:2 21:9 5:0 13:3 0:8 3:0 2:4 22:9 32:0 18:2 9:8 0:3 14:7 7:1 5:3 17:7 0:3 8:8 33:4 3:4	hr 3: 1: 6: 6: 6: 6: 2: 3: 3: 9: 8: 3: 9: 12: 12: 12: 12: 12: 12: 12: 13: 14: 15: 16: 16: 16: 16: 16: 16: 16: 16

Amounts in millimetres, for periods of sixty minutes between the exact hours, Greenwich Mean Time.

333. Cahirciveen (Valencia Observatory): Hr (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + hr (height of receiving surface above ground) = 9.1 metres + 0.5 metres.

March, 1923.

							of re	ceivin	ig sur	face	above	e grou	ind) =	= 9.1	meti	res +	0.21	netre	s.					mar	ch, 19)ZJ.
Day.	0-I	1-2	2-3	3-4	4-5	5–6	6-7	7-8	8–9	9–10	10–11	11-12	12–13	13-14	14-15	15–16	16–17	17–18	18–19	19–20	20–21	21-22	22-23	23-24	0-24	Dura- tion 0–24.
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	hr.
I												.3	1.7	4.1	2.2	1.0									9.5	3.9
3			•6		·1	• • 2		1.9	·]				•1	.1								2.6	1.3
4									•••		•••]		•••	•••	•••	•••		•••	:::					0.9	3.9
5	4.4	5.0	3.8	I.I	.3	•••	•••		•••					•••	•••			•••								1
6						1.8	1.7						•2		•••	.3	•••	•4		1.2			:::	•••	7.3	2.2
7 8					.2																				0.2	0.2
9									•••							2.2				 •6	•••		:::		30·5	10.3
10			•••				.3	1.3	2.3	1.3	4.2	4.6	4.6	4.2	3.0		.7	_ ′	~			ļ				1
11			• • • •						•••					.1	•9	٠9	 I .0	1.0	1.2	1.9	1.1		1.2		10.4	8.9
12	:::	:::	•••					·1		1.3											• • • • • • • • • • • • • • • • • • • •			•••	0.4	0.4
14								'	•••								•••	•••			•••	•••		•••		
15	•••		•••	•••			•••	***	•••		•••	•••							•••		•••	•••	•••	•••		
16									•••									•••			•••	•••				:::
17			•••						•••																	
19		:::	•••						•••												•••	•••	•••	• • • •		
20			•••		•••				•••	•••	•••	•••	•••		•••				•••	•••	•••		•••	•••	•••	
21																			•••	•••	•••			•••		
22			•••	•••				•••	•••									:::		•••	•••			• • • • • • • • • • • • • • • • • • • •		
23 24		:::	•••																	•••	•••		•6	•••	0.6	0.3
25	1.1	1.7	.3		.3		•••	•••	.3					•••	••••		•••			•••	•••	•••	•••	•••	3.7	1.9
26		 																		1.2	2.0	.8	.8	٠1	5.2	3.6
27	1.6	3.4	1.6	2.0			.1				•••		•••		:::				2.0	·5	 I.I	1.8	1.4		15.9	8.4
28 29		:::	•••													\			•6	1.0	1.3	2.3	2.2	2.3	9.8	6.1
30	4.0	•6	2.4	4.8	•6	2.0	٠7	•2	•••					•••	•••	•••	•••				•••	•••		•••	15.3	6.5
31										•••			2.4	٠6					•••		•••				3.0	1.3
Sum.	11 · 1	10.8	8.7	8.1	1.8	4·1	2.9	3.9	3.0	2.7	4.5	5.2	8.9	9.8	6.2	4.2	1.8	2.2	4.9	7.0	6.4	5.7	6.6	3.7	134.8	63.3
Total			hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr	
Dura-	hr. 4 [:] 0	hr. 3•1	3.3	2.6	2.4	2.1	2.0	2.2	1.2	2.0	1.2	1.5	3.1	2.7	2.7	2.6	1.6	1.6	3.5	4.2	4.0	3.4	3.9	2·I	63.3	
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tion.									!			!			!		1							A ===	:1 10	02
334.	Cah	ircive	en (V	/alenc															mm !	mm		l mm	mm		il, 19	
334.	Cah	mm.	en (V	mm.	mm.	serva	mm.	: Hr		I me			metr	es.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	Apr	il, 19	23.
<u>'</u>												mm. 	mm. 	mm. 							•••			mm.	mm.	hr.
334. I 2 3	m m .	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm. 	mm.	mm.	mm. 1.5	mm. I·2	mm. 			•••		 •8	•••	•••			mm.	mm.	hr.
334.	m m .	mm.	mm. 	mm. 	mm.	mm. 	mm.	mm.	mm.	mm. 	mm.	mm. 	mm. 	mm. 		 I·4	 .4	 		 I·4	 .5	 		mm.	mm. 8·9	hr. 6·2
334. I 2 3 4 5	mm.	mm.	mm	mm.	mm.	mm.	mm. 	mm. 	mm.	mm.	mm.	mm 1.5	mm. I·2 	mm		 I·4 	 :4 	 .6	 •8	 I·4 	 :5	··· ··7	···	mm.	mm 8.9 0.1 1.3	hr 6·2 0·2
334. 1 2 3 4 5 6 7	mm.	mm.	mm. 	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm. 1·5	mm. I·2	mm. 		 I·4 	··· 4 ··· ·· ··	 .6 	 .8 	 I·4	 .5 	··· ·· ·· ·· ·· ·· ·· ·· ··	··· ·3 ··· ··· ··2	mm.	mm 8.9 0.1 1.3 5.5	hr 6·2 0·2 0·7 4·5 0·7
334. 1 2 3 4 5 6 7 8	mm.	mm.	mm	mm.	mm.	mm.	mm.	mm	mm.	mm	mm.	mm 1·5	mm I • 2	mm		 I·4 	··· ··· ··· ··· ···	··· ··6 ··· ·· ··2	 •8 	 I·4 	 .5 	 .7 	··· ·3 ··· ···	mm.	mm 8.9 o.1 1.3 5.5 1.8 1.2 1.0	hr. 6·2 0·2 0·7
334. 1 2 3 4 5 6 7	mm.	mm.	mm	mm.	mm.	mm.	mm. .9	mm. .2	mm.	mm	mm.	mm 1·5	mm I • 2	mm		 I·4 	··· ··4 ··· ···	 .6 	 •8 •9 	1·4 	 	··· ··· ··· ··· ··· ···	··· ·3 ··· ··· ·2 ··· ·4	mm	mm 8.9 0.1 1.3 5.5 1.8 1.2	hr 6·2 0·2 0·7 4·5 0·7 1·1
334. I 2 3 4 5 6 7 8 9 10	mm.	mm.	mm	mm.	mm.	mm	mm.	mm.	mm.	mm	mm.	mm I·5	mm I·2	mm		 I·4 	'4	··· ··6 ··· ··2 ··· ··· ···	 ·8 ·9 	I·4 	··· ··· ··· ··· ··· ··· ···	··· ·· · · · · · · · · · · · · · · · ·	··· ··3 ··· ··2 ··· ··4 ···	mm	mm 8.9 o.1 1.3 5.5 1.8 1.2 1.0	hr 6·2 0·2 0·7 4·5 0·7 1·1 1·2
334. 1 2 3 4 5 6 7 8 9	mm.	mm	mm	mm.	mm.	mm	mm	mm.	mm.	mm	mm	mm 1.5	mm 1·2	mm		 I·4 	··· ··4 ··· ··· ··· ···	 	 .8 .9 	 I·4 I·4 	 	 .7 	 .3 .4 .7	mm	mm 8.9 0.1 1.3 5.5 1.8 1.2 1.0 1.8	hr 6·2 0·2 0·7 4·5 0·7 1·1 1·2 2·7
334. 1 2 3 4 5 6 7 8 9 10 11 12 13	mm	mm	mm	mm	mm	mm	mm	mm.	mm	mm	mm	mm I · 5	mm 1·2	mm	 	 I·4 	'4	 	 .8 .9 	 I·4 I·4 	 	 	 .3 .2 .4 .7	mm	mm 8.9 0.1 1.3 5.5 1.8 1.2 1.0 1.8	hr 6·2 0·2 0·7 4·5 0·7 1·1 1·2 2·7
334. 1 2 3 4 5 6 7 8 9 10	mm	mm	mm	mm	mm	mm	mm	mm.	mm.	mm	mm	mm 1.5	mm 1·2	mm		 I·4 	'4	 	 .8 .9 	 I·4 I·4 	 	 .7 	 .3 .4 .7	mm	mm 8.9 0.1 1.3 5.5 1.8 1.2 1.0 1.8 3.3 10.4	hr 6·2 0·2 0·7 4·5 0·7 1·1 1·2 2·7 2·7 5·0
334. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm 1.5	mm I·2 3.0	mm	 	 I·4 3·5		 .6 .2 		 I·4 	 	'7 1·1	 .3 .2 .4 .7	mm	mm 8.9 0.1 1.3 5.5 1.8 1.2 1.0 1.8 3.3 10.4 9.7 4.2 0.1	hr 6.2 0.2 0.7 4.5 0.7 1.1 1.2 2.7 2.7 2.7 5.0 3.9 2.1
334. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm I · 5	mm 1·2	mm	 	 I·4 3·5			 .8 .9 	I·4 I·4 i·4	 .5 		··· ·· ·3 ··· ·2 ·· ·4 ·· ·7 ·· ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1	mm	mm 8.9 0.1 1.3 5.5 1.8 1.0 1.8 3.3 10.4 9.7 4.2 0.1 30.2	hr 6.2 0.7 0.7 1.1 1.2 2.7 2.7 5.0 3.9 2.1 0.1 10.8
334. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm		mm I.5	mm	mm	 	 1·4 3·5 4·0			 .8 .9 	I · 4 I · 4 I · 4	 .5 	'7 1·1	···· ··3 ··· ··2 ··· ··4 ··· ··7 ··· ·· ·· ·· ·· ·· ·· ·· ·· ··	mm	mm 8.9 0.1 1.3 5.5 1.8 1.2 1.0 1.8 3.3 10.4 9.7 4.2 0.1	hr 6.2 0.2 0.7 4.5 0.7 1.1 1.2 2.7 2.7 2.7 5.0 3.9 2.1
334. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17	mm	mm.	mm	mm	mm	mm	mm	mm	mm	mm		mm I · 5	mm 1·2 3·0	mm	 	 I·4 3·5 			 .8 .9 	I'4			··· ·· ·3 ··· ·2 ··· ·4 ··· ·7 ··· ·7 ··· ·7 ··· ·1 ··· 3.0 ···	mm	mm 8.9 0.1 1.3 5.5 1.8 1.0 1.8 3.3 10.4 9.7 4.2 0.1 30.2 4.2	hr 6.2 0.2 0.7 4.5 0.7 1.1 1.2 2.7 2.7 2.7 5.0 3.9 2.1 0.1 10.8 2.8
334. 1 2 3 4 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	mm		mm	mm	mm		mm	mm	mm	mm		mm I · 5 I · 5	mm	mm	 	I·4 4·0			 .8 .9 2.4 	I · 4 I · 4 2 · 7	 		··· ·· ·3 ··· ·2 ··· ·4 ··· ·7 ··· ·· ·7 ··· ·3 ·0 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1 ·1	mm	mm 8.9 0.1 1.3 5.5 1.8 1.2 1.0 1.8 3.3 10.4 9.7 4.2 0.1 30.2 4.2	hr 6·2 0·2 0·7 4·5 0·7 1·1 1·2 2·7 2·7 5·0 3·9 2·1 10·8 2·8
334. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm		mm I · 5	mm	mm 2.1 2.3	 	I·4				I'4 I'4 2.7			 	mm 3.8	mm 8.9 0.1 1.3 5.5 1.8 1.2 1.0 1.8 3.3 10.4 9.7 4.2 0.1 30.2 4.2	hr 6.2 0.7 4.5 0.7 1.1 1.2 2.7 2.7 5.0 3.9 2.1 10.8 2.8
334. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	mm	mm	mm	**************************************	mm	mm	mm	mm	mm	mm		mm 1.5	mm 3.0	mm 2.1 2.3		I·4	··· ··· ··· ··· ··· ··· ··· ··· ··· ··			I'4			 .3 .2 .4 .7 .7 .7 	mm	mm 8.9 0.1 1.3 5.55 1.8 1.2 1.0 1.8 3.3 10.4 9.7 4.2 0.1 30.2 4.2 0.3 10.5	hr 6.2 0.2 0.7 4.5 0.7 1.1 1.2 2.7 2.7 2.7 2.7 5.0 3.9 2.1 0.1 10.8 2.8 0.1 6.1
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334. 1 2 3 4 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 5	mm	mm	mm	**************************************	mm	mm	mm	mm	mm	mm		mm	mm 3.0	mm 2·1 2·3		I·4 3·5				I·4			 .3 .2 .4 .7 .7 .3.0 	mm 3.8	mm. 8.9 0.1 1.3 5.5 1.8 1.2 1.0 1.8 3.3 10.4 9.7 4.2 4.2 0.1 30.2 4.2 0.3 10.5 3.0 2.1	hr 6.2 0.7 4.5 0.7 1.1 1.2 2.7 2.7 5.0 3.9 2.1 10.8 2.8 0.1 6.1 1.6 1.4
334. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	mm		mm	mm	mm	mm	mm	mm	mm	mm		mm	mm 3.0	mm		I·4 3·5 4·0	··· ··· ··· ··· ··· ··· ··· ··· ··· ··			I·4			··· ·· ·3 ··· ·2 ··· ·4 ··· ·7 ··· ·7 ··· ·3 ·0 ··· ·3 ·0 ··· ··· ·· ·· ·· ·· ·· 2 ·4 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	mm 3.8	mm. 8.9 0.1 1.3 5.5 1.8 1.2 1.0 1.8 3.3 10.4 9.7 4.2 0.1 30.2 4.2 0.3 10.5 3.0 2.1 0.7	hr 6.2 0.2 0.7 4.5 0.7 4.5 0.7 1.1 1.2 2.7 2.7 5.0 3.9 2.1 0.1 10.8 2.8 0.1 6.1 1.6 1.4 0.3
334. 1 2 3 4 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm		mm 1.5 1.5	mm 3.0	mm		I·4	··· ··· ··· ··· ··· ··· ··· ··· ··· ··			I'4 I'4 2.7				mm 3.8	mm. 8.9 9.1 1.3 5.5 1.8 1.2 1.0 1.8 3.3 10.4 9.7 4.2 0.1 30.2 4.2 0.3 10.5 3.0 2.1 0.7 1.7 2.4	hr 6.2 0.2 0.7 4.5 0.7 1.1 1.2 2.7 2.7 2.7 2.7 5.0 3.9 2.1 0.1 10.8 2.8 0.1 6.1 1.6 1.4 0.3 1.5 1.2
334. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm		mm I · 5 I · 5 I · 5	mm 3.0	mm		I·4 3·5 4·0				I·4 2·7				mm 3.8	mm. 8.9 0.1 1.3 5.5 1.8 1.2 1.0 1.8 3.3 10.4 9.7 4.2 0.1 30.2 4.2 0.3 10.5 3.0 2.1 0.7 1.7	hr 6.2 0.2 0.7 4.5 0.7 1.1 1.2 2.7 2.7 2.7 2.7 5.0 3.9 2.1 0.1 10.8 2.8 1.6.1 1.6
334. 1 2 3 3 4 4 5 5 6 7 8 9 10 11 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm		mm I · 5 I · 5 I · 5	mm 3.0	mm		I·4 4·0	··· ··· ··· ··· ··· ··· ··· ··· ··· ··			I'4 I'4 2'7				mm 3.8	mm. 8.9 9.1 1.3 5.5 1.8 1.2 1.0 1.8 3.3 10.4 9.7 4.2 0.1 30.2 4.2 0.3 10.5 3.0 2.1 0.7 1.7 2.4	hr 6.2 0.2 0.7 4.5 0.7 1.1 1.2 2.7 2.7 5.0 3.9 2.1 0.1 10.8 2.8 0.1 6.1 1.6 1.4 0.3 1.5 1.2 3.0
334. 1 2 3 4 4 5 5 6 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum.	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm		mm I.5 I.5	mm 3.0	mm		I·4 3·5	··· ··· ··· ··· ··· ··· ··· ··· ··· ··			I'4 I'4 2'7				mm 3.8	mm. 8.9 0.1 1.3 5.5 1.8 1.2 1.0 1.8 3.3 10.4 9.7 4.2 0.1 30.2 4.2 0.3 10.5 3.0 2.1 0.7 1.7 2.4 3.0	hr 6.2 0.2 0.7 4.5 0.7 1.1 1.2 2.7 2.7 5.0 3.9 2.1 0.1 10.8 2.8 0.1 6.1 1.6 1.4 0.3 1.5 1.2 3.0
334. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm		mm I · 5 I · 5 I · 5	mm 3.0	mm		I·4	 4.9 			I·4				mm 3.8	mm 8.9 0.1 1.3 5.5 1.8 1.2 1.0 1.8 3.3 10.4 9.7 4.2 0.1 30.2 4.2 0.3 10.5 3.0 2.1 0.7 1.7 2.4 3.0 107.4	hr 6.2 0.2 0.7 4.5 0.7 1.1 1.2 2.7 2.7 5.0 3.9 2.1 0.1 10.8 2.8 0.1 6.1 1.6 1.4 0.3 1.5 1.2 3.0
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334. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum. Total Dura-	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm		mm I · 5 I · 5 I · 5 I · 5 I · 5 I · 5 I · 5 I · 6 I · 7 I · 7 I · 7 I · 7 I · 7 I ·	mm 3.0	mm		I·4				1·4				mm 3.8	mm. 8.9 0.1 1.3 5.5 1.8 1.2 1.0 1.8 3.3 10.4 9.7 4.2 0.1 30.2 4.2 0.3 10.5 3.0 2.1 0.7 2.4 3.0 107.4 hr. 59.9	hr 6.2 0.2 0.7 4.5 0.7 1.1 1.2 2.7 2.7 2.7 2.7 5.0 3.9 2.1 0.1 10.8 2.8 0.1 6.1 1.6 1.4 0.3 1.5 1.2 3.0 59.9

Amounts in millimetres, for periods of sixty minutes between the exact hours, Greenwich Mean Time.

Cahirciveen (Valencia Observatory): Hr (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + hr (height of receiving surface above ground) = 9·1 metres + 0·5 metres.

May, 1923.

Day.	0-I	1-2	2-3	3-4	4-5	5–6	6-7	7-8	8-9	9–10	10–11	11-12	12-13	13-14	14-15	15–16	16–17	17–18	18–19	19–20	20-21	21–22	22-23	23-24	0-24	tion 0.24
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	hr.
1			•••	•••		•••	•••		•••			•••	•••				٠	••••						•••		•••
2 3								:::			•••			•••				•••								
4											•••		•••			• • • •	•••		•••	•••						
5	•••	•••		•••	•••	•••		•••	•••		•••						•••	•••	•••	•••	•••		•••			
6				• 1	٠ı	• • •		•2			•••							•••	•••	•••	•••				0.4	0.6
7 8									:::												•••				0.1	0.1
9 10		•••				.1		.1		•4	•••	•5	.1					···	 •9		1.3	·1	···		6·0	1·4 5·6
10	'''	""	.2	.1				•••	'''			•••]	•••												
11 12	.3			.3		.1		1.0	•2			••2	·4 ·4		.5	·1		·4 ·4	·		'4 '1	3			4·2 5·4	3.0
13			'				••2	1.1				•4					.5	'	•••	•1					1.0	0.7
14 15								.3				r·8					·5								5.8	3.3
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16 17] :::	:::		.7		:::	:::			:::												·1 ·4			0.6	0.4
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19 20					•4			·								:::									2.4	2.6
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23 24					.1			•••		•••						:::								.3	0.5	0.8
24 25	:::											·1	:::											.3	0.2	0.7
26	.2	 	.3			.3	•4	.3					١					.2	.3				.2	.3	2.5	2.5
27 28						1.1	'				•1			•••		•••	•••				•••				0.2	0.4
20 29	:::	:::																•••								
30									•••	…								•••	•••	•••			•••	•••	'''	
31																		•••						<u> </u>		
Sum.	0.9	1.3	2.0	2.7	I · 2	1.9	I.0	2.7	1.4	1.4	1.4	3.0	1.5	1.1	1.0	0.8	3.0	2.6	1.7	2.5	3.5	1.4	1.8	1.6	43 · 4	35∙0
Total	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	
																1	1.8	2.2			1 O.O.			T . 6	35.0	1 1
Dura-	0.0	0.7	1.4	2.0	1.0	1.7	0.0	2.4	1.7	1.5	1.1	1.2	1.1	0.7	1.0	0.2	1.0	2.2	1.6	1.8	2.9	1.7	1.6	1.6	133	
Dura- tion.	0.0	0.7	1.4	2.0	1.0	1.7	0.9	2.4							1.0	0.5	1.8		1.0	1.0	2.8	1.7	1.0	<u> </u>	<u> </u>	23.
Dura-	o·9 Cah	o·7	ı·4 en (V	2·0	ia Ob	1·7	o·9 tory)	2·4	= 9	ı me	tres -	+ 0.5	met	res.							mm.	1·7	mm.	<u> </u>	ne, 19	23.
Dura- tion.	0.0	0.7	1.4	2.0	1.0	1.7	0.9	2.4							mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	Jui mm.	ne, 19	hr.
Duration. 336.	Cah	o·7	mm	alenc	ia Ob	mm.	o·9 tory) mm. 	2·4 : H ₇ mm	= 9 · · · · · · · · · · · · ·	I me	tres -	+ 0.5	met	res.	mm. 	mm. 		mm.	mm.	mm.	mm.	mm.	mm.	Jui	ne , 19 mm.	hr.
Duration. 336.	Cah	o·7	oen (V	alenc	ia Ob	serva	o·9 tory) mm.	2·4 : H _r	= 9 ·	mm.	tres -	+ 0·5	meti	res.	mm.	mm.	mm.	mm. 	mm. 	mm. 	mm. 	mm.	mm.	Jui	me, 19	hr. o·1
Duration. 336.	Cah	mm.	mm. 	2:0 /alenc	ia Ob mm. 	mm. 	tory) mm	2·4 : H ₇ mm.	= 9 · · · · · · · · · · · · · · · · · ·	mm	tres -	+ 0 · 5	metrone mm.	mm.	mm. 	mm. 	mm.	mm. 	mm.	mm.	mm. 	mm. 	mm. 	Jui mm. 	me, 19	hr.
Duration. 336.	Cah	mm.	mm	2.0 /alenc	ia Ob	**************************************	mm	2·4 : H ₇ mm	= 9°	mm	mm.	+ 0·5	mm.	res.	mm	mm	mm.	mm.	mm.	mm.	mm.	mm.	mm.	Jui	me, 19	hr o·1 o·4
Duration. 336.	Cah	mm.	mm	2·0 mm.	mm	mm	mm	* H ₇	= 9°	mm	mm.	+ 0·5	metronia met	res.	mm	mm. 	mm.	mm.	mm.	mm.	mm.	mm.	mm. 	Jui mm.	mm o.i o.4 i.6 9.1	hr o·1 o·4 1·6 5·6
Duration. 336. 1 2 3 4 5 6 7 8 9	Cah	0.7	mm	2·0 /alenc mm	mm	mm	mm	* Hr mm	= 9°	mm	mm	+ 0.5	mm	res.	mm.	mm	mm	mm	mm	mm	mm.	mm.	mm.	Jui mm.	mm o.r. o.r. o.4 r.6	hr o·1 o·4 1·6
Duration. 336. 1 2 3 4 5 6 7 8	Cah	0.7	mm	mm	mm	mm	mm	* Hy mm	= 9°	mm	mm	+ 0·5	mm	res.	mm	mm	mm	mm	mm	mm	mm.	mm	mm	mm.	mm o·1 o·4 1·6 9·1 o·6	hr
Duration. 336. 1 2 3 4 5 6 7 8 9 10 11	Cah mm	0.7	mm	2 · 0	ia Ob mm 2.3	mm	0·9 tory) mm	2 · 4	= 9° mm	mm	mm	+ 0.5	mm	mm	mm.	mm	mm	mm	mm	mm	mm.	mm	mm	Jun mm.	mm o·1 o·4 i·6 9·1 o·6	hr o·i o·4 i·6 5·6 o·7
Duration. 336. 1 2 3 4 5 5 6 7 8 9 10 11 12 13	Cah mm.	0.7	mm	2·0 /alenc mm	mm	mm	0·9 tory) mm	2·4 : H ₇ mm	= 9° mm	mm	mm	+ 0.5	mm	res.	mm	mm	mm	mm	mm	mm	mm.	mm	mm.	Jui mm	mm o·1 o·4 1·6 9·1 o·6 2·1 o·8	hr 0·1 0·4 1·6 5·6 0·7 1·2 1·3
Duration. 336. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14	Cah mm	0.7	mm	2.0 /alenc mm	ia Ob mm 2 · 3	mm	o·9 tory) mm	2 · 4	= 9° mm	mm	mm	+ o·5	mm	res.	mm	mm	mm	mm	mm	mm	mm	mm	mm	Jui mm	mm	hr o·i o·4 i·6 5·6 o·7 i·2
Duration. 336. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 15	Cah mm 2.6	0.7	mm	2·0 /alenc mm	ia Ob mm 2·3	mm	o·9 tory) mm	2·4	= 9° mm	mm	mm	+ o·5	mm	res. mm.	mm	mm	mm	mm	mm	mm	mm	mm	mm	Jui mm	mm o o i o i o i o i o i o i o i o i o i o i o i o i o o i o i o o i o i o i o i o i o i i o i i i i i o i	hr 0·1 0·4 1·6 5·6 0·7 1·2 1·3 3·4
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Duration. 336. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	©ah mm.	0.7	1·4 pen (V mm	2·0 /alenc mm		mm	mm	2·4 : Hr mm	= 9· mm	mm	mm	+ o·5	mm	res. mm.	mm	mm	mm	mm	mm	mm	mm	mm	mm	Jui mm	mm o.1 o.4 1.6 9.1 o.6 2.1 o.8 1.4 6.5	hr o·i o·4 i·6 5·6 o·7 i·2 i·3 i·3 ·
Duration. 336. 1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 15 16 17 18 19 20 20 21 22	0 · 9 Cah mm	0.7	1 · 4 mm.	2·0 /alenc mm	ia Ob mm 2 · 3	mm	o·9 tory) mm	2 · 4	= 9° mm	mm	mm	+ o·5	mm	res. mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	Jui mm	mm	hr 0·1 0·4 1·6 5·6 0·7 1·2 1·3 1·3 3·4
Duration. 336. 1 2 3 4 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21	©ah mm.	0.7	1·4 pen (V mm	2·0 /alenc mm	1·0 ia Ob mm 2·3	mm	mm	2·4 : Hr mm	= 9· mm	mm	mm	+ o·5	mm	res. mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	Jui mm	mm	hr 0·1 0·4 1·6 5·6 0·7 1·2 1·3 1·3 3·4
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Duration. 336. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	©ah mm.	0.7	1·4 pen (V mm	2·0 /alenc mm		mm	mm	2 · 4	= 9· mm	mm	mm	+ o·5	mm	res. mm.	mm.	mm	mm	mm	mm	mm	mm	mm	mm	Jui mm	mm	hr 0·1 0·4 1·6 5·6 0·7 1·2 1·3 1·3 3·4
Duration. 336. 1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	©ah mm	0.7	1·4 pen (V mm	2·0 /alenc mm	1.0 ia Ob mm 2.3	mm	o·9 tory) mm	2 · 4	= 9· mm	mm	mm	+ o·5	mm	res. mm.	mm.	mm	mm	mm	mm	mm	mm	mm	mm	Jui mm	mm	hr 0·1 0·4 1·6 5·6 0·7 1·2 1·3 1·3 3·4
Duration. 336. 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	0 · 9 Cah mm	0.7	1·4 Den (V mm	2·0 /alenc mm	1.0 ia Ob mm 2.3	1·7 SSOFVA MM 2·2	o·9 tory) mm	2 · 4	= 9° mm	mm	mm	+ o·5	mm	res. mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	Jui mm	mm	hr 0·1 0·4 1·6 5·6 0·7 1·2 1·3 1·3 3·4
Duration. 336. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	0 · 9 Cah mm 2 · 6	0.7	1·4 pen (V mm	2·0 /alenc mm	1.0 ia Ob mm 2.3	mm	o·9 tory) mm	2 · 4	= 9· mm	mm	mm	+ o·5	mets mm.	res. mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	Jui mm	mm	hr 0·1 0·4 1·6 5·6 0·7 1·2 1·3 3·4
Duration. 336. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 S.m.	0 · 9 Cah mm	0.7	1·4 pen (V mm	2·0 /alenc mm	1.0 ia Ob mm 2.3	mm	o·9 tory) mm	2 · 4 : Hr mm	= 9° mm	mm	mm	+ o·5	mm	res. mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	Jui mm	mm	hr 0·1 0·4 1·6 5·6 0·7 1·2 1·3 1·3 3·4
Duration. 336. 1 2 3 4 5 5 6 6 7 8 9 10 11 12 13 14 15 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 S.im. Total Dura-	0 · 9 Cah mm 2 · 6	0.7	1·4 pen (V mm	2·0 /alenc mm	1.0 iia Ob mm 2.3	mm	o·9 tory) mm	2 · 4	= 9· mm	mm	mm	+ o·5	mets mm.	res. mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	Jui mm	mm	hr 0·1 0·4 1·6 5·6 0·7 1·2 1·3 3·4
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Amounts in millimetres, for periods of sixty minutes between the exact hours, Greenwich Mean Time.

337. Cahirciveen (Valencia Observatory): Hr (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + hr (height of receiving surface above ground) = 9 · 1 metres + 0 · 5 metres.

July, 1923.

							01.10		15 Du	Tacc		- 6.00				res +									ıy, 19:	
Day.	o-1	I-2	2-3	3-4	4-5	5–6	6-7	7-8	8-9	9-10	10-11	11-12	12-13	13-14	14–15	15–16	16–17	17–18	18–19	19–20	20-21	21-22	22-23	23-24	0-24	Dura- tion. 0–24
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	hr.
I 2									···	•••								•••	••2	• • • 5		1.3	1.1		3.2	4.3
3	.3	•4	• 2	.7	•••			.1	•••							:::						•••			1.7	3.0
4 5	···	1.4	1.3		·					•2	.3				•2	·ı	.9	•2	·1			•••		•••	7.1	7.1
6	.		l		l	 												•••								
7 8				•4			·ı									1.0	3.1	1.1	···8		···			•••	0·6 7·4	3·8
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10									•••							•••		•••	•••	•••						
II I2								•••										•••							0.5	1.3
13	•••																	•••								
14 15	:::		:::			1.3	2.0	5.7	3.2	• 2												•••		•4	13.5	5.4
16	ĺ				 			 	l	.1		·													0.1	0.2
17			:::			• 5	.3		•••		•••														0.8	0.3
18 19			:::				3.0	1.3												•••	•••	·1	.1	.1	5.3	4.8
20	•2	.1		.1	.1	·I	·1		•••	•••	•••			• • • • •	•••	•••	•••	•••	•••	•••	•••	•••	•••	•••	" /	
21											•••								•••						0.1	0.1
22 23					2.5	6.2	3.1	•4	••2									•••	•••	•••		•••		•••	0.6	3.3
24				3.9		 '4	1.4								•••				•••						6.7	2.3
25	.3	.3	'4	39	1														,						 	
26 27						• • 2	··.	٠.								•2	•6	•4		٠1	1.3	2.6			6.3	2·6 1·3
28		.8	∙8	.9	1.3	•2			•••	:::		:::			·1	•••									0.7	0.6
29 30						···	.1		.3	2.8	1.6							•••		•••	.1	•2		.9	6.2	2.3
31	.3	1.1	 	1.1	1.4	1.7	1.7	.7	1.5	.2		•2				•••								•••	9.9	3.1
Sum.	2.7	4.2	3.5	8.4	·	11.8	12.7	8.6	6.2	3.8	2.3	1.0	o·8		0.3	1.3	4.6	1.7	1.1	0.9	1.6	4.3	1.2	1.7	92 · 4	50.6
Total Dura-	hr. 3·0	hr. 3·6	hr. 2·5	hr. 3'4	hr. 3·1	hr. 4.5	hr. 5·1	hr. 3·0	hr. 2·8	hr. 2·7	hr.	hr. o·6	hr. 0·7	hr.	hr. 0·4	hr. o·5	hr. 1 · 6	hr. 1·5	hr. 0·9	hr. 1·7	hr. o·8	hr. 2·5	hr. 2·3	hr. 2·4	hr. 50·6	
tion.	<u> </u>	<u> </u>	<u> </u>	<u> </u>	1	<u> </u>	1	<u> </u>	<u> </u>	1	<u> </u>		·	<u>. </u>		1					<u>'</u>	<u> </u>			•	
																								_		
338.	Cah	ircive	en (V	/alenc	cia Ot	serva	tory)	: Hr							1		l m m	mm	l mm	lmm	mm	mm			st, 19	
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	= 9	mm.	tres -	+ 0·5	meti	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm. 5.5	hr. 1.8
I 2					mm. ·6	mm. 	mm. 	mm. 	mm. .5	mm. •9	mm. 	mm.	mm. 	mm. 					1	\$	1	1	mm.	mm. 3·6 ·2	mm. 5.5 19.6	hr. 1·8 6·9
I 2 3	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.		•••	•••						mm. 1.0 	mm. 3·6 ·2 ···	mm. 5·5 19·6 o·8	hr. 1·8 6·9
I 2	mm. 2·6	mm. 3.9	mm. 6·9	mm. 2·2	mm. .6	mm. 1.0	mm. .7	mm. .9	mm. .5	mm. •9 •••	mm. 	mm.	mm. • 1	mm. 				 					mm. 1·0 ·2	mm. 3·6 ·2 ··· ·6	mm. 5·5 19·6 o·8 14·3	hr. 1·8 6·9 0·9 2·0
1 2 3 4 5	mm. 2·6 	mm. 3.9 	mm. 6·9	mm. 2 · 2	mm6	mm i.o	mm7	mm. .9 	mm. .5 	mm.	mm 3.2	mm.	mm	mm.					 	1.6			mm. 1.0 	mm. 3·6 ·2 ···	mm. 5·5 19·6 o·8	hr. 1·8 6·9
1 2 3 4 5	mm. 2·6 6·2	mm. 3·9 7·7	mm. 6·9 	mm. 2·2 	mm. .6 	mm. I·0 	mm. .7 	mm. .9 	mm. .5 	mm9	mm.	mm.	mm	mm.					 1.5	1.6 	1.6	1.4 	mm. 1 · 0 · 2 1 · 2 2	mm. 3.6 ·2 ·6 1.0 ·6	mm. 5.5 19.6 0.8 14.3 15.5 2.6 9.5	hr. 1·8 6·9 0·9 2·0 7·7 2·6 5·1
1 2 3 4 5 6 7 8	mm. 2·6 6·2 ·4 ·2	mm. 3·9 7·7	mm. 6·9 ·4 ·4	mm. 2·2 I·3 .2	mm6	mm. 1·0 	mm7	mm	mm58	mm.	mm 3.2	mm.	mm	mm.					 1.5	 	1.1 	 I.4	mm. I · 0 · 2 I · 2	mm. 3·6 ·2 · ·6 ·	mm. 5.5 19.6 0.8 14.3	hr. 1·8 6·9 0·9 2·0 7·7 2·6
1 2 3 4 5 6 7 8 9 10	mm. 2·6 6·2 	mm. 3·9 7·7	mm. 6·9 '4 '4	mm. 2 · 2 I · 3 · 2	mm. .6 	mm. 1·0 	mm7	mm	mm. .5 	mm 3.7	mm 3.2 I.4	mm.	mm 2 · 9	mm					 	···	 i.6	1·4 	mm. 1 · 0 2 1 · 2 2	mm. 3·6 ·2 · ·6 · ·6 · ·6	mm. 5.5 19.6 0.8 14.3 15.5 2.6 9.5 0.3 0.8	hr. 1·8 6·9 0·9 2·0 7·7 2·6 5·1 0·3 0·8
1 2 3 4 5 6 7 8	mm. 2·6 6·2 ·4 ·2	mm. 3·9 7·7	mm. 6·9 '4 '4	mm. 2·2 I·3 .2	mm6	mm. 1·0 	mm7	mm	mm. .5 .8 	mm.	mm 3.2 1.4	mm 4	mm1 2.9	mm				 	 	 	 1.6 	 1.4 1.4 	mm. 1 · 0 · 2 1 · 2 2	mm. 3·6 ·2 ·6 1·0 ·6	mm. 5:5 19:6 0:8 14:3 15:5 2:6 9:5 0:3 0:8 15:9	hr. 1·8 6·9 0·9 2·0 7·7 2·6 5·1 0·3
1 2 3 4 5 5 6 7 8 9 10 11 12 13	mm. 2·6 6·2 ·4 ·2 ·2 3·2	mm. 3.9 7.7 	mm 6·9 ·4 ·4 1·0	mm. 2·2 1·3 ·2 6 ·1	mm6	mm I · 0	mm7	mm 9	mm. .5 	mm.	mm 3.2 I.4	mm	mm 2.9	mm				 	 	1.6 	 1.0 	I · 4 I · 4 I · 6	mm. 1 · 0 · 2 1 · 2 2 · 8	mm. 3·6 ··· ··· ··· ···	mm. 5'5' 19'6 0'8 14'3 15'5 2'6 9'5 0'3 0'8 15'9 3'7	hr. 1·8 6·9 0·9 2·0 7·7 2·6 5·1 0·3 0·8 12·0 1·4
1 2 3 4 5 6 7 8 9 10 11 12	mm. 2·6 6·2 ·4 ·2	mm. 3·9 7·7 	mm. 6·9 '4 1·0	mm. 2·2 I·3 ·2	mm6	mm I · 0	mm7	mm9	mm.	mm.	mm 3.2 I.4	mm	mm 2.9	mm			 		 	 	 1.6 	 1.4 1.4 	mm. 1 · 0 · 2 1 · 2 2 · 8	mm. 3·6 ·2 · ·6 · ·6 · ·1·0 · ·1·8 · ·	mm. 5·5 19·6 0·8 14·3 15·5 2·6 9·5 0·3 0·8 15·9 3·7	hr. 1·8 6·9 0·9 2·0 7·7 2·6 5·1 0·3 0·8 12·0 1·4
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14	mm. 2 · 6 6 · 2 '4 '2 2 3 · 2	mm 3 · 9 7 · 7	mm 6·9 ·4 ·4	mm. 2·2 1·3 ·2 6 ·1	mm6	mm I · 0	mm7	mm	mm	mm.	mm 3.2 I.4	mm 4	mm 2.9	mm					 	 	 I·I I·6 	I · 4 I · 4 I · 6	mm. 1 · 0 · 2 1 · 2 2 · 8	mm. 3·6 ··· ··· ··· ···	mm. 5'5' 19'6 0'8 14'3 15'5 2'6 9'5 0'3 0'8 15'9 3'7	hr. 1·8 6·9 0·9 2·0 7·7 2·6 5·1 0·3 0·8 12·0 1·4 1·8 3·9
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17	mm. 2.6 6.2 2.3.2 2.7	mm 3 · 9 7 · 7	mm 6·9 ·4 1·0 ·3	mm 2·2	mm6	mm 1 · 0	mm7	mm	mm.	mm.	mm 3.2 1.4	mm	mm 2.9	mm			 		 	 	 	 	mm. 1:02 1:2 2:8	mm. 3 · 6 · 2 ·	mm. 5·5 19·6 0·8 14·3 15·5 2·6 9·5 0·3 0·8 15·9 3·7 2·1 7·8 1·0	hr. 1·8 6·9 0·9 2·0 7·7 2·6 5·1 0·3 0·8 12·0 1·8 3·9 0·4
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	mm. 2 · 6 6 · 2	mm 3.9 7.7	mm 6·9 ·4	mm 2·2	mm	mm	mm7	mm	mm58	mm.	mm 3.2 I.4	mm	mm 2 · 9	mm					 	 	 I·I I·6 	 1.4 1.4 	mm. 1 · 0 2 1 · 2 2 · 8	mm. 3·6 ··· ·· ···	mm. 5·5 19·6 0·8 15·5 0·3 0·8 15·9 3·7 17·8	hr. 1·8 6·9 0·9 2·0 7·7 2·6 5·1 0·3 0·8 12·0 1·4 1·8 3·9
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18	mm 2.6 6.2 2.4 2.2 2.7	mm 3.9 7.7	mm 6·9	mm	mm	mm 1 · 0	mm7	mm	mm58	mm.	mm 3.2 I.4	mm.	mm 2.9	mm		 2·4 				 		 1.4 1.4 	mm. 1 · 0 · 2 1 · 2 2 · 8	mm. 3·6 ··· ·· ···	mm. 5:5 19:6 0:8 14:3 15:5 2:6 9:5 0:3 0:8 15:9 3:7 2:1 7:8 1:0 4:2	hr. 1·8 6·9 0·9 2·0 7·7 2·6 5·1 0·3 0·8 12·0 1·4 1·8 3·9 0·4 3·9
1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21	mm 2.6 6.2 2.3.2 2.7 2.7 2.7	mm 3.9 7.7	mm 6·9	mm	mm	mm	mm7	mm	mm58	mm.	mm 3.2 I.4	mm	mm 2 · 9	mm					 	 			mm. 1 · 0 · 2 1 · 2 2 · 8 · 1 · 6	mm. 3 · 6 · 2 ·	mm. 5·5 19·6 0·8 14·3 15·5 2·6 9·5 0·3 0·8 15·9 3·7 2·1 7·8 1·0 4·2 8·0 15·7 0·7	hr. 1·8 6·9 0·9 2·0 7·7 2·6 5·1 0·3 0·8 12·0 1·8 3·9 0·4 3·9 3·8 4·2 0·3
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	mm 2·6 6·2 · · 2.3 2·7	mm 3.9 7.7	mm 6·9	mm	mm	mm 1.0	mm	mm	mm	mm.	mm 3.2 I.4	mm	mm 2 · 9	mm						 		I · 4 I · 4	mm. 1:0 1:2 2:8	mm. 3.6 .26 1.0	mm. 5·5 19·6 0·8 15·5 0·3 0·8 15·9 3·7 2·1 7·8 1·0 4·2 8·0 15·7 20·1	hr. 1·8 6·9 0·9 2·0 7·7 2·6 5·1 0·3 0·8 12·0 1·4 1·8 3·9 0·4 3·9 3·8 4·2 0·3 4·2 0·2
1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	mm 2.6 6.2 2.3.2 2.7 2.7 2.7	mm 3.9 7.7	mm. 6·9 '4 1·0 '3	mm	mm	mm	mm	mm	mm58	mm.	mm 3.2 I.4	mm	mm 2.9	mm									mm. 1:0 2:2 2:8	mm. 3·6 ·2 · ·6 · ·6 · · 1·8 · · · 4·6 · ·	mm. 5·5 19·6 0·8 14·3 15·5 2·6 9·5 0·3 0·8 15·9 3·7 2·1 7·8 1·0 4·2 8·0 15·7 20·1 0·4 13·5	hr. 1·8 6·9 0·9 2·0 7·7 2·6 5·1 0·3 0·8 12·0 1·4 1·8 3·9 0·4 3·9 3·8 4·2 0·3 4·2
1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	mm 2.6 6.2 2.7 2.7 2.7	mm 3.9 7.7	mm 6·9	mm	mm	mm	mm7	mm	mm	mm.	mm 3.2 I.4	mm	mm	mm									mm. 1 · 0 · 2 1 · 2 2 · 8 · 1 · 6 · 4	mm. 3.6 .26 1.0 1.8 4.6 4.6	mm. 5·5 19·6 0·8 14·3 15·5 2·6 9·5 0·3 0·8 15·9 3·7 2·1 7·8 1·0 4·2 8·0 15·7 20·1 0·4 13·5 4·8	hr. 1.8 6.9 0.9 2.0 7.7 2.6 5.1 0.3 0.8 12.0 1.4 3.9 0.4 3.9 3.8 4.2 0.3 4.2 0.2 8.4 1.3
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	mm 2.6 6.2 2.3.2 2.7 2.7	mm 3.9 7.7	mm 6.9	mm	mm	mm I · 0	mm	mm	mm	mm.	mm 3.2 1.4	mm	mm	mm								I · 4 I · 4	mm. 1:0 2:2 2:8	mm. 3.6 .2 66 1.0 1.8 4.6 1.1.8 1.1.8	mm. 5·5 19·6 0·8 14·3 15·5 2·6 9·3 0·8 15·9 3·7 2·1 7·8 1·0 4·2 8·0 15·7 20·1 13·5 4·6 2·3	hr. 1.8 6.9 0.9 2.0 7.7 2.6 5.1 0.3 0.8 12.0 1.4 1.8 3.9 0.4 3.9 3.8 4.2 0.3 4.2 0.2 8.4 1.3 2.1 1.1
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	mm 2.6 6.2 2.3 2.7 2.7	mm 3.9 7.7	mm 6·9	mm	mm	mm	mm	mm	mm	mm.	mm 3.2 I.4	mm	mm	mm								I · 4 I · 4	mm. 1 · 0 · 2 2 · 8 · 1 · 6 · 4	mm. 3.6 .2 6 1.0 1.8 4.6	mm. 5·5 19·6 0·8 14·3 15·5 2·6 9·3 0·8 15·9 3·7 2·1 7·8 1·0 4·2 8·0 15·7 20·1 0·4 13·5 4·8 4·6	hr. 1·8 6·9 0·9 2·0 7·7 2·6 5·1 0·3 1·8 3·9 0·4 3·9 3·8 4·2 0·3 4·2 0·3 4·2 0·3 4·2 0·3 4·2 0·3 4·2 0·3
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	mm 2.6 6.2 2.7 2.7	mm 3.9 7.7	mm 6·9	mm	mm	mm 1.0	mm	mm	mm	mm.	mm 3.2 1.4	mm	mm	mm									mm. 1 · 0 · 2 1 · 2 2 · 8 · 1 · 1 · 6 · 4	mm. 3 · 6 · · · · · · · · · · · · · · · · · ·	mm. 5·5 19·6 0·8 14·3 15·5 2·6 9·5 0·3 0·8 15·9 3·7 2·1 7·8 1·0 4·2 8·0 15·7 0·7 20·1 13·5 4·8 4·6 2·3 16·6	hr. 1.8 6.9 0.9 2.0 7.7 2.6 5.1 0.3 0.8 12.0 1.4 1.8 3.9 0.4 3.9 3.8 4.2 0.3 4.2 0.3 4.2 0.3 4.1 1.1 6.2
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	mm 2.6 6.2 2.7 2.7	mm 3.9 7.7	mm 6.9	mm 2·2 1·3	mm	mm	mm	mm	mm	mm.	mm 3.2 1.4	mm	mm 2.9	mm								I · 4 I · 4	mm. 1 · 0 · 2 2 · 8 · 6 · 4	mm. 3.6 .2 66 1.0 1.8 4.6 1.4	mm. 5·5 19·6 0·8 14·3 15·5 2·6 9·3 0·8 15·9 3·7 2·1 7·8 1·0 4·2 8·0 15·7 20·1 0·4 13·5 4·6 2·3 16·6 0·2	hr. 1.8 6.9 0.9 2.0 7.7 2.6 5.1 0.3 1.8 3.9 0.4 3.9 3.8 4.2 0.3 4.2 0.3 4.2 0.3 1.1 6.2 0.3 1.2
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mm 2.6 6.2	mm 3.9 7.7	mm 6.9	mm	mm	mm	mm	mm	mm	mm.	mm 3.2 1.4	mm	mm	mm								1·4	mm. 1 · 0 · 2 1 · 2 2 · 8 · 1 · 1 · 6 · 4 6 · 6	mm. 3 · 6 · · · · · · · · · · · · · · · · · ·	mm. 5·5 19·6 0·8 14·3 15·5 2·6 9·5 0·3 2·1 7·8 1·0 4·2 8·0 15·7 20·1 0·4 13·5 4·6 2·3 16·6 0·2 3·0 193·5	hr. 1.8 6.9 0.9 2.0 7.7 2.6 5.1 0.3 1.8 3.9 0.4 3.9 3.8 4.2 0.3 4.2 0.3 4.2 0.3 1.1 6.2 0.3 1.2
1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	mm 2.6 6.2 2.7 2.7	mm 3.9 7.7	mm 6.9	mm 2·2 1·3	mm	mm	mm	mm	mm	mm.	mm 3.2 1.4	mm	mm 2.9	mm								I · 4 I · 4 I · 4 I · 6 I · 3	mm. 1 · 0 · 2 1 · 2 2 · 8 · 1 · 6 · 4	mm. 3 · 6 · · · · · · · · · · · · · · · · · ·	mm. 5·5 19·6 0·8 14·3 15·5 2·6 9·3 2·1 7·8 1·0 4·2 8·0 15·7 20·1 0·4 13·5 4·6 2·3 16·6 0·2 3·0 193·5	hr. 1.8 6.9 0.9 2.0 7.7 2.6 5.1 0.3 1.8 3.9 0.4 3.9 3.8 4.2 0.3 4.2 0.3 4.2 0.3 1.1 6.2 0.3 1.2

Amounts in millimetres, for periods of sixty minutes between the exact hours, Greenwich Mean Time.

339. Gahirciveen (Valencia Observatory): H_r (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + h_r (height of receiving surface above ground) = $g \cdot I$ metres + $o \cdot 5$ metres. September, 1923.

							of re	ceivii	ıg sur	race	above	grou	ina) =	= 9.1	meti	es +	0.21	metre	5.				Joh		er, 19	
Day.	0-1	I-2	2-3	3-4	4-5	5-6	6-7	7-8	8–9	9-10	10-11	11-12	12–13	13–14	14–15	15–16	16-17	17–18	18–19	19–20	20-21	21–22	22-23	23-24	0-24	Dura- tion. 0–24
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	hr.
1	•••		•••			•••			•••		:::	•••		•••	:::		•••			•••			•••		0.4	0.2
3												•8	3.3	1.8	1.0	1.0	.3			2.0	• 5	•5	3.3	• 5	16.0	9.1
4	•••	•••	•••	•••	•••	•••								•••	: ::		•••			•••			•••			:::
5	•••	•••	•••			•••		'''		***					Ì										1.8	2.1
6 7	• • • • • • • • • • • • • • • • • • • •		···					···							1.0			•••	•••					:::	0.9	1.0
8												•••	•••	•••	•••	•••	•••				• • • • • • • • • • • • • • • • • • • •		•••		 o·6	 o∙8
9 10						:::								·6												
							1			ĺ														·1	0.1	0.3
11	 ·6										:::	•••			•••					•••				٠ı	2.8	4.4
13	•2	.5	•4	· 1						1.1	1.2	•2	٠ı	•••	.7	•••	•••		•••	···		···	• 1	1.0	4·7 3·3	3·4 1·7
14	···	.1	.7		1.3		2.1	1.8				2.3	··6		٠		•••		•••				•••		11.1	4.2
-										ļ	ļ										l			 	0.2	0.2
16	• • • 5		2.5	2.4	2.0	5.4	4.1	5.6	3.1	3.6	4·I	1.7	٠6		•4		1.5	·1	2.0	·ı			•••			12.2
18 19	1.3	•••	···	1.1		1			•••			···	.6			·	•••	·1							3.1	1.0
20						:::	:::										•••	1.0	•4	·I	•2		•••		1.7	1.8
21						l																.1	•2		0.3	0.3
21				.1	•4		1.5	•2			1.3			.3			•••	•••	•6	1.1	.3	٠1	•2	•2	6·2 4·2	3.0
23	. I	1.2		1.0						•••		2.8	3.3	2.2	4·6	8·7	6·3						• • • •	• 2	28.7	6.9
24 25	•4				•6	1.4		•5	1.2	•2								•••		.9			•••		5.2	2.1
26																							•1	.1	0.2	0.2
27	٠9	2.0	•4	•••		· 1	1.1	•5	•••	•6	•••	•••				···· ˈ	•••			:::				· · I	6·5 0·5	3·8 0·7
28 29	•••		·1		. I	2.0				:::						•••	• • • •								2.6	1.2
30	•••				•••	•••			•••	•••		•••			•••	•••	•••	. I	•••	•••			···		0.1	0.2
Sum.	4.9	4.2	5.8	5.6	6.2	9.9	9·1	9.4	4.8	6.1	7.4	7.9	9.5	5.2	8.7	9.9	8.2	1.6	3.3	4.9	1.7	1.6	4.1	2.2	142.8	65.5
Total Dura- tion.	hr. 3·6	hr. 2·9	hr. 4·2	hr. 3·0	hr. 3'4	hr. 3·2	hr. 2·5	hr. 2·9	hr. 1•9	hr. 2·7	hr. 2·8	hr. 3·0	hr. 4·0	hr. 3·8	hr. 3'4	hr. 2·3	hr. 1·6	hr. 1·6	hr. 1·8	hr. 2·4	hr. 2.0	hr. 1·9	hr. 2·1	hr. 2·5	hr. 65·5	
340.	0-L																						_		- 4-	00
	Gan	ircive	en (V	/alenc	ia Ob	serva	tory)	: Hr	= a ·	I me	tres -	- 0.5	meti	es.									(Octob	er, 19	23.
340.							tory)			I me		mm.	meti	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	er, 19 mm.	23. hr.
ı	mm.	mm.	mm.	mm.	mm.	mm.	mm.	Hr	mm. 9		mm.			mm.			•••			•••		•••	mm.	mm.	mm.	hr. 0·2
I 2	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	l .				i	i	mm.	i	mm.	mm.	mm.	hr.
1 2 3 4	mm. 	mm. 	mm. 	mm2 -2 -2	mm. .5 	mm.	mm.	mm.	mm. 	mm.	mm.	mm.	mm.	mm. 	•••	•••				•••			mm. 8 	mm. 1.0	mm. 0·2 2·8 6·1	hr. 0·2 3·0 2·3
1 2 3	mm. 2·6	mm. .2 2.6	mm. • · · · · · · · · · · 6	mm. ·2 ·2 ·2	mm. .5	mm.	mm. 	mm. 	mm. 	mm.	mm.	mm.	mm. 	mm. 	•••	•••	•••						mm. •8	mm. 1.0	mm. 0·2 2·8 6·1 2·2	hr. 0·2 3·0 2·3 3·7
1 2 3 4 5	mm. 2·6 	mm2 2.6	mm1 .6	mm2 -222	mm. ··· ··· ··· ···	mm6	mm24	mm11	mm.	mm	mm.	mm.	mm.	mm.				···					mm. 8 	mm i.o	mm. 0·2 2·8 6·1	hr. 0·2 3·0 2·3
1 2 3 4 5	mm. 2·6 	mm2 2.6	mm1 .6	mm2 -222	mm. .5 .6	mm. 	mm24	mm. 	mm.	mm. 	mm.	mm.	mm.	mm.									mm. 8 	mm. 1.0 1.1	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0
1 2 3 4 5 6 7 8	mm 2·6	mm2 2·6	mm ·1 ·6 · · · · · · · ·	mm2 -22	mm ·5 ·6 ·2	mm6 .1 .2	mm ·2 ·4 ·1	mm	mm	mm.	mm.	mm	mm	mm	 i.i i.o	 1.8		 I·2	 				mm. 	mm. 1.0	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2
1 2 3 4 5 6 7 8	mm 2·6	mm2 2.6	mm1 .6	mm2 -2	mm562	mm6 .1 .2	mm ·2 ·4 ·1	mm	mm	mm	mm.	mm	mm	mm	1.0 1.1 		 	 I.2	···	···			mm	mm I · 0 · I · 2 · I	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 12·6	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7
1 2 3 4 5 5 6 7 8 9 10 II	mm 2.6	mm2 2.6	mm1 .6	mm2 -2	mm ·5 ·6 ·2	mm	mm	mm111	mm	mm	mm	mm	mm	mm	 	 		 I·2	 	···			mm. 	mm 1.0	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2
1 2 3 4 5 6 7 8 9	mm 2·6	mm2 2·62111	mm1 .6	mm.	mm562	mm	mm	mm11111	mm	mm	mm.	mm I · 0	mm	mm	 	 		 I.2 	 	 		 I · 0	mm8	mm I · 0 · 1 · 1 · 2 · 1 2 · 1	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 12·6 1·5 3·3 3·4	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7 0·5 1·5 0·9
1 2 3 4 5 6 7 8 9 10 11 12 13 14	mm 2.6	mm2 2.6	mm	mm2 -22	mm56	mm6 .1 .2 1.46 1.0	mm	mm	mm	mm	mm 1.6	mm	mm	mm	 	 		 I.2 	 			 I · 0	mm8	mm I · O · I · I · I · I · I	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 12·6 1·5 3·3	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7 0·5 1·5
1 2 3 4 5 6 7 8 9 10 II 12 13 14 15	mm 2·6	mm2 2.6	mm1 .6	mm2 -22	mm56	mm	mm	mm11	mm	mm	mm 1.6	mm	mm	mm	 	 		 	 	 		 I · 0	mm	mm	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 I2·6 I·5 3·3 3·4 2·2 0·3	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7 0·5 1·5 0·9 0·8 0·3
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	mm 2.6	mm2 2.6	mm	mm2 -22	mm56	mm6 .1 .2 1.46 1.0	mm	mm	mm	mm	mm 1.6	mm	mm	mm		 		 I'2 		 		 I.0	mm8	mm I · O	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 12·6 1·5 3·3 3·4 2·2 0·3 0·9	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7 0·5 1·5 0·9 0·8 0·3 0·5
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	mm 2.6	mm2 2.6	mm1 .6	mm2 -2	mm56	mm	mm	mm	mm	mm	mm 1.6	mm	mm	mm				 				 I.o	mm	mm 1 · 0	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 12·6 1·5 3·3 3·4 2·2 0·3	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7 0·5 1·5 0·9 0·8 0·3
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	mm 2.6	mm2 2.6	mm	mm2 -22	mm56	mm	mm24 I.o	mm	mm	mm	mm 1.6	mm	mm	mm	 	 				 		 	mm	mm I · 0 2 · I I · 9	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 12·6 1·5 3·3 3·4 2·2 0·3 0·9 2·3	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7 0·5 1·5 0·9 0·8 0·3 0·5 1·3
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	mm 2.6	mm2 2.6	mm	mm2 -2	mm56	mm	mm	mm	mm	mm	mm 1.6	mm	mm	mm	 		3.1 3.1 			 	 	 	mm.	mm 1 · 0 2 · 1 1 · 9	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 12·6 1·5 3·3 3·4 2·2 0·3 0·9 2·3 2·8	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7 0·5 1·5 0·9 0·8 0·3 0·5 1·3 1·1
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	mm 2.6	mm2 2.611	mm1 .6	mm2 -2	mm562	mm	mm241	mm	mm	mm	mm	mm	mm	mm			3.1 3.1 			 	 		mm	mm 1.0 2.1	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 12·6 1·5 3·3 3·4 2·2 0·3 0·9 2·8 31·8 6·7 3·9	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 2·2 11.7 0·5 1·5 0·8 0·3 0·5 1·3 1·1 9·8 3·7 1·9
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	mm 2.6	mm2 2.61111	mm	mm2 -2	mm562	mm	mm	mm	mm	mm	mm 1.6	mm	mm	mm			 			 	 	 	mm	mm I · O	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 12·6 1·5 3·3 4 2·2 0·3 0·9 2·3 2·8 6·7	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7 0·5 1·5 0·9 0·8 0·3 0·5 1·3 1·1 9·8 3·7 1·5 5·5 2·8
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	mm 2.6	mm2 2.6	mm	mm2 -2	mm56	mm	mm	mm	mm	mm	mm 1.6	mm	mm	mm						 	 		mm	mm 1.0	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 12·6 1·5 3·3 3·4 2·3 0·9 2·3 2·8 31·8	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7 0·5 1·5 0·9 0·8 0·3 0·5 1·1 9·8 3·7 1·9 5·5
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	mm 2.6	mm2 2.6	mm	mm2 -2	mm	mm	mm	mm	mm	mm	mm 1.6	mm	mm	mm						 	 		mm	mm 1.0	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 12·6 1·5 3·3 3·4 2·2 0·3 0·9 2·8 81·8 6·7 3·9 15·4 11·5 5·6 18·8	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7 0·5 1·5 0·9 0·8 0·3 0·5 1·3 9·8 3·7 1·9·8 2·2 7·4
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	mm 2.6	mm	mm	mm2 -2	mm56	mm	mm241	mm	mm	mm	mm 1.6	mm	mm	mm									mm	mm 1.0 2.1	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 12·6 1·5 3·3 4 2·2 0·3 0·9 2·3 31·8 6·7 3:9 11·5 5·6 18·8 7·2	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7 0·5 1·5 0·9 0·8 0·3 0·5 1·3 1·1 9·8 3·7 1·9 5·5 2·8 2·2
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	mm 2.6	mm2 2.6111	mm	mm2 -2	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm									mm	mm 1.0 2.1	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 3·4 2·2 0·3 0·9 2·3 2·3 3·4 2·2 0·3 1.5·6 17.6	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 2·1 1·7 0·5 1·5 0·8 0·3 1·1 9·8 3·7 1·9 5·8 2·2 7·4 4·8 9·5
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	mm 2.6	mm	mm	mm2 -2	mm	mm	mm241	mm	mm	mm	mm	mm	mm	mm							 		mm	mm 1.0 2.1	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 12·6 1·5 3·4 2·2 0·3 0·9 2·38 31·8 6·7 3·9 15·4 11·5 5·6 18·8 7·2 1·6	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 2·2 11·7 0·5 1·5 0·9 0·8 0·3 0·5 1·3 19·8 3·7 1·5 5·8 2·2 7·4 4·8 0·6
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	mm 2.6	mm2 2.6	mm	mm2 -2	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm									mm8	mm 1.0	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 3·4 2·2 0·3 0·9 2·3 2·8 81.8 6·7 3·9 15·4 11·5 5·6 17·6 3·7 0·4	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7 0·5 1·5 0·9 0·8 0·3 1·1 9·8 3·7 1·9·8 3·7 1·9·8 2·2 7·4 4·8 9·5 2·6 0·3
1 2 3 4 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mm 2.6	mm2 2.611	mm	mm2 -2	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm		1·8				 			mm	mm 1.0	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 0·2 12·6 1·5 3·3 3·4 2·2 0·3 0·9 2·8 31·8 6·7 3·9 15·4 11·5 5·6 18·8 7·2 1·6 3·7 0·4 176·9	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7 0·5 1·5 0·9 0·8 0·3 1·1 9·8 3·7 1·9·8 3·7 1·9·8 2·2 7·4 4·8 9·5 2·6 0·3
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	mm 2.6	mm	mm	mm2 -2	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm		1·8 3·2 2·2							mm8	mm 1.0	mm. 0·2 2·8 6·1 2·2 0·4 6·2 5·3 3·4 2·2 0·3 0·9 2·3 2·8 81.8 6·7 3·9 15·4 11·5 5·6 17·6 3·7 0·4	hr. 0·2 3·0 2·3 3·7 0·3 6·6 3·0 0·2 11·7 0·5 1·5 0·9 0·8 0·3 1·1 9·8 3·7 1·9·8 3·7 1·9·8 2·2 7·4 4·8 9·5 2·6 0·3

Amounts in millimetres, for periods of sixty minutes between the exact hours, Greenwich Mean Time.

341. Cahirciveen (Valencia Observatory): Hr (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + hr (height of receiving surface above ground) = 9·1 metres + 0·5 metres.

November, 1923.

									 -		 _			1	1	1	1	1	1	1	}	1	ī	1	Ī	Dura-
Day.	0-1	1-2	2-3	3-4	4-5	5-6	6–7	7–8	8–9	9–10	10-11	11-12	12–13	13-14	14-15	15–16	16-17	17–18	18–19	19–20	20-21	21-22	22-23	23-24	0-24	0-24
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm. 4.3	hr. 2·4
1 2					:::								٠1		•2	.9	.3	· I	·2	·3					3·4 0·8	3 4
3 4					• • • • • • • • • • • • • • • • • • • •				٠	·					:::			•••			•••		• 5	• 2	2·0 6·0	1.1
5			•5	•••	1.9	•••	• 5		.6	•4						•••	• 2	.1	1.0		•4]			1	
6 7	• 5															1.0		·1	1.1	·I					3.3	3.6
8			•8			.1			.7		·6				4			•••							3.3	1.6
9 10																	•••	•••	•••							
11																1.3		·3	·6	·6	.0	·2			2·6 9·9	3·9 10·0
12	·1	1.7						1.7	·2 ·9	.3	·2 ·6	·9 ·4	1.0 .5	1.7	1.5				•••	·4 ·8			.2		10.5	8·5 1·3
14			1.9	2.4	3.0	2.9	·2 ·4		·2 ·4	·6	·			:::				•••	•••	•••				*	12·6	2.3
16	1.0											.2	٠ı				1.3	5:2	٠6	٠9	•5	·2		٠i	10.1	3.5
17		.1	•••				·6			1.0	·9			•2	 ·6	 I·2		·5	1.3					·6	5·8 4·7	2.7
19		1.0	1.0	.5	•6					•••		·6	•9		 '4	·		·5	.3	·2	 •9	. I			4·9 5·2	3.1
20	•••	.1	.7		'4		.3	•2	•5	•••			•••												2.8	1.1
2I 22						1.6	·6			•••	•••					···										
23 24			•••											•••					•••	•••	•••				0·3 7·8	0·2 3·8
25			•••		•••		•••			.3	•4	·ı	•••	•••	•••	•••	•4	1.4	•5	•••	•••	2.7	1.9		1	2.8
26			3.0	٠9	.3						2.9	 '7	·1	2.5	·2					• • • •			•••		5·9	4.6
27 28	•••						•••		•••			•••								•••	•••				0.2	 0·4
29 30	•••	•••	,														.9	2.0	2.9	•8	1.4				8.0	4.3
Sum.	2.5	3.9	8.8	4.4	7.1	6.1	3.3	3.7	4.3	4.1	6.2	4.4	3.2	7·1	6.6	5.9	6.2	11 · 0	9.5	4.8	4.7	4.2	3.2	2.0	127.5	76.4
Total	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr. 2·6	hr.	hr. 1 · 6	hr. 76•4	
Dura- tion.	1.7	1.9	3.2	1.9	2.2	2.3	2.4	1.9	2.3	3.0	3.4	3.7	3.4	4.2	4.7	4.3	4.5	4.9	5.7	5.0	3.5	2.0	1.5	1.0	104	
342.	Cab	iroivo	on (V	/alanc	ia Ob	earva	tory)	: Hr	<u> </u>	T me	tres -	L 0.5	metr	es.									Dec	cemb	er, 19	23.
772.	Vali								7																	
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	hr.
I 2			mm.	mm.	mm.	mm.	mm.	mm.			•••		mm. • 2 • 1	mm. 	mm. 	mm. 	mm. '4	.3 mm.	3.0	2.2	1 · 0 · 2			 •5	7·8 4·8	3·7 2·8
2 3		 	mm. .3	mm. 	mm.	mm.	mm.	mm. .3	 .1	 1·7 ·7	•••	 *5 	·2 ·1 ···	··· ·2 ···		 '4 	'4 	1.0	3.0	2.2	1.0				7·8 4·8 8·8 8·7	3·7 2·8 5·3 3·8
2			mm. 	mm. 	mm. 	mm. 	mm. 	mm. 		 1·7		 •5	·2 ·1	• • 2		 '4	·4 ···	3 1.0	3·o 3·o	2·2 ·7	1·0 ·2 2·2	2.2	 1·7 	 •5 	7·8 4·8 8·8	3·7 2·8 5·3
2 3 4 5	 	 •4 •6 •1	mm3 .25	mm27	mm.	mm3	mm	mm. ·3 ·2 ·7 ·1	 •1 •6	 1·7 ·6	 1·2 ·9	 .5 	·2 ·1 · ·1 ·	···· ···· ···· ····	 •1 •6 	 '4 '3 	·4 	1·0 ·3 2·2 	3·0 	2·2 ·7 I·0 	1·0 ·2 2·2 	 2·2	 •1 1•7	 .5 	7·8 4·8 8·8 8·7	3·7 2·8 5·3 3·8
2 3 4 5	 	 •4 •6 •1	mm3 .25	mm27	mm.	mm. .3	mm1 .2	mm. ·3 ·2 ·7 ·1	 ·1 ·6 ·1	 1·7 ·7 ·6 	 1·2 ·9	 •5 	·2 ·1 · ·1	···· ··2 ··· ··3 ··· ··· ··· ···	 •1 •6 	 '4 '3 	'4 	1·0 ·3 2·2 	3·0 .3 .9 .1	2·2 ·7 I·0 2·I ·3	I·0 ·2 2·2 I·0 	2·2 2·6 	 •1 1•7 ••• 1•8 	3·3	7·8 4·8 8·8 8·7 2·6 11·7 23·9 1·2	3.7 2.8 5.3 3.8 2.0 5.4 7.5 0.7
2 3 4 5 6 7 8	 5.6 	 •4 •6 •1 6•9	mm3 .25 4.8	mm27 2.0	mm	mm	mm1 .24	mm3 .2 .7 .13	 ·1 ·6 ·1	 1·7 ·6 	 1·2 ·9	 .5 	·2 ·1 · ·1 · ·1	···· ··2 ···3 ···	 •6 	 '4 '3 	·4 	1·0 ·3 2·2 	3·0 .3 	2·2 ·7 I·0 2·I ·3	I · 0 · 2 2 · 2 · · · · · · · · · · · · · · ·	2·2 2·6	 1·7 1·8	 3.3	7·8 4·8 8·8 8·7 2·6	3.7 2.8 5.3 3.8 2.0 5.4 7.5
2 3 4 5 6 7 8 9	 5.6 	 •4 •6 •1 6•9 	mm3 .25 4.8	mm27 2.0	mm I · 9	mm3 I·I	mm1 .24	mm3 .2 .7 .13	 ·6 ·1 ·1	 1·7 ·6 	 I·2 ·9 ·4 ·1	 .5 .7 	·2 ·1 · ·1 · ·1 · ·1 ·	···· ··· ··· ··· ··· ··· ···	 .1 .6 	 '4 '3 		1·0 ·3 2·2 	3·0 ·3 ·9 ·1 	2·2 ·7 I·0 2·I ·3 	I·0 ·2 2·2 ··· ··· I·0 ··· ·2 ··· ··· ···	2·2 2·6	 1·7 1·8 ·I	3·3 	7.8 4.8 8.8 8.7 2.6 II.7 23.9 I.2 0.5 0.2	3·7 2·8 5·3 3·8 2·0 5·4 7·5 0·7 0·5 0·2
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For periods of sixty minutes, between the exact hours, of Local Apparent Time.

343. Cahirciveen (Valencia Observatory): h_s (height of recorder above ground) = 12.8 metres.

January, 1923.

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DURATION OF BRIGHT SUNSHINE.

For periods of sixty minutes, between the exact hours, of Local Apparent Time.

345. Cahirciveen (Valencia Observatory): h_s (height of recorder above ground) = $12 \cdot 8$ metres.

March, 1923.

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346.	Cahi	rcive	en (V	alenc	ia Ol	bserva	atory) : h:	; = 1	1 [2·8]	metre	es.	ı			J	1	<u>'</u>	April,	
346.	Cahi	rcive	en (V	alenc	ia Ol	bserva	atory) : h:	s = 1	1 2 · 8 1 hr.	metre	es.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	%
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For periods of sixty minutes, between the exact hours, of Local Apparent Time.

347. Cahirciveen (Valencia Observatory): h_s (height of recorder above ground) = 12.8 metres. May, 1923.

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Day.	3 to	4 to	5 to	6 to	7 to	8 to	o to	ro to	II to	Noon	ra to	ra to	15 to	16 to	17 to	18 to	to to	20 to	Total for	Per cent of
Day.	4.	5.	6.	7.	8.	9.	10.	11.	Noon		14.	15.	16.	17.	18.	19.	20.	21.	Day.	Possible.
	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	%
I			•••	•3	٠1	•5	.9	.7	1.0	1.0	.9	-8	1.0	1.0	1.0				9.2	62
2	-	•••	1.0	1.0	•2	•6	.9	1.0	٠1	ι.	·I	•2	-8	I.0	-8	. 1	•••		7.9	53
3	-		• • •	•••	•••	•••	•••	•••			•••		•••	•••	•••	•••	•••	_		•••
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7 8		•2	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	.2	_	14.4	9 5
8	-		• • • •	٠ı		٠ı	•2	.9	.3	·6	.3	•9	1.0	.7	1.0	·4	•2		6.4	42
9			-8	.7	•5	.7	.9	•6	•6		.7	∙8	1.0	1.0	.9	-8	•••		10.6	70
10	-		•••	∙8	∙8	.7	.9	•6	•6	•5	•5	•••	•••		••••	•••	•••		5.4	35
11				.,			-6	.,	.2	٠,	.,	.6	•5	-6	-6	-6			6.7	44
12	I		·3 ·7	·4 ·5	·3 ·6	·7 ·7	.8			·3		l							3.2	23
13	l	•2	·1	•4	.5	.9	.7	.8	1.0	.9	•9	.7	·1		.3	.5			8.0	52
14	l —															·ī	٠ı	'	0.2	I
15	I —	•••	·1	∙8	1.0	1.0	1.0	.7	I.0	1.0	1.0	1.0	-8	'4	∙6	•••	•••	_	10.4	67
-6	}			_	'	_			_	١.	_	١.							8·o	
16	_	•••	∙6	-6	1.0	1.0	1.0	.3	.7	4	:7	.4	'1 '2		•2	·4	•••	_	2.0	51 13
17 18					•••	···	.8	.7	·3	·5	.2			••2			•••		4.4	28
19	l				.1	.2	.1	.3	.5	ī		l'							1.3	8
20	l —												·I	.3	٠ı	•4	•••		0.9	6
	[}	1		_]	
21			•••		•5	•2	•••	•••		•5			•••				•••		1.2	8
22		•••	•••							1.1	1.2	 T:0		··.	7.0	···	•••	_	0.3	2
23			···	·8	·9 ·2	·6 ·2	.9	1.0	1.0	1.0	1.0	1.0	1.0		1.0	•6	•2	_	3.0	70 19
24 25				.0	·2	·2	•1	·9 ·5									••2		7.5	47 ·
23	{ · _		•••	1	1	•	-	3)	۱	9	′	′	9	2	פ ו	_		' '	T' · '
26	_		•2	•5	.7	·4	∙8	-8	-8	.9	1.0	1.0	1.0	1.0	•4		•••		9.5	59
27						.3	•2	·ı	·2	1.0	•5	1.0	•6	1.0	-8	.7	•2		6.6	41
28			∙8	.9	.1	.1	·ı	٠6	·4	.9	⋅8	•5	1.0	1.0	.9	.3	• • • •		8.4	52
29		'4	1.0	1.0	1.0	I.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	•4	•••	14.8	92
30	••••		.7	•6	I.O	1.0	1.0	1.0	•6		• • • •	•••		•••	•••	•••	•••	•••	5.9	36
31	l	.2	1.0	1.0	1.0	1.0	1.0	1.0	1.0	.8	1.0	1.0	1.0	1.0	1.0	1.0			14.0	86
]																			<u> </u>
Sum.		1.0	9.2	12.2	11.8	14.7	15.5	16.1	13.2	15.6	14.8	14.3	13.9	13.8	13.7	8.9	1.6	•••	190.3	
Mean.		0:00		0:22	0:00		0.55	0.52	0.43	0:50	0.48	0.46	0.45	0.45	0.44	0.29	0.05		6.14	39
Mean.		0.03	0.30	0.39	0.38	0.47	0.20	0.9%	0.43	0.20	0.40	0.40	0.45	0.45	0.44	0 29	003		0 14	39
	<u>'</u>			1						<u> </u>	l		<u> </u>				<u>'</u>		-	<u></u>
				1							<u> </u>	<u>'</u>	<u>'</u>				<u>'</u>			·
348.	Cahi	rcive	en (V	alenc	ia Ol	serv	atory) : h.	s = 1	12.8	metre	es.					<u>'</u> -		June,	1923.
348.													hr	l hr	l hr.	l hr.	hr	hr.		
	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	%
348.			hr.									hr.	1	hr. 1.0	1	hr. 	hr	hr		
I	hr.	hr.	hr.	hr. ·6	hr. '7	hr. •9	hr.	hr. '4 1.0	hr. •5 •9	hr. •5	hr ·2	hr	·2 I·0	1.0	·2 I·0 ·2	 .7 			hr. 4·2 12·1 7·4	% 26 74 45
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DURATION OF BRIGHT SUNSHINE.

For periods of sixty minutes, between the exact hours, of Local Apparent Time.

349. Gahirciveen (Valencia Observatory): h_s (height of recorder above ground) = $12 \cdot 8$ metres. July, 1923.

349.										1	1	1			ī —	1			Total	Per cent.
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11	l	.2	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	•9	•4	1.0	.7	.3		13.2	82
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31						<u> </u>													TO5.5	
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Mean.		0.03	0.19	0.20	0.25	0.23	0.22	0.22	0.27	0.30	o·33	0.37	0.40	0.39	0.33	0.53	0.13	•••	4.05	25
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For periods of sixty minutes, between the exact hours, of Local Apparent Time.

351. Gahirciveen (Valencia Observatory) : h_s (height of recorder above ground) = $12 \cdot 8$ metres.

September, 1923.

																		Sehr	ember	1323.
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9	-		•••				•••				···	7.0	1.0	1.0	···8	•••	_	_	 II·2	86
10	-			.7	1.0	-8	.9	1.0	1.0	1.0	I.O	1.0	1.0	1.0		•••			1 ** ~	50
11				.6	1.0	1.0	1.0	1.0	1.0	1.0	.2	.2	.2						7.3	56
12	l —										•4	٠ı	•1						0.6	5
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15	-		•••		'4	•5	-8	•6	•5	•4	1.0	٠6	.9	.9	.3	•••		-	6.9	54
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Mean.	-		•••	0.11	0.27	0.35	0.32	0.32	0.42	0.43	0.41	0.41	0.40	0.31	0.22	0.01	_	_	4.00	32
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1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	hr.	hr.	hr	hr	hr	hr '4	hr. 1·0	hr92 .8 .1 .326 .6 .6 .1 .0 .8 .2774 .9 .9 .9 .1 .02 .1 .9	hr9 .2 .8 .5 .2	hr. 1 0 5 7 1 0 2 5 4 1 0 6 7 9 9 9 3 8 4	hr. 1 · 0 · 6 1 · 0 · 9 · 4 ·	hr. 1.0 ·6 ·7 ··· ·4 ··· ·1 ·1	'46	·5	·2 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··			hr.	hr. 6·9 2·3 5·7 6·4 1·8 1·0 1·4 6·3 5·57 6·7 0·5 1·7 6·2 4·8 3·7 4·0 1·2 1·6 2·7	% 59 20 50 56 16 9 13 58 51 722 63 5 64 17 61 47 37 40 12 16 27
1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	hr.	hr.	hr	hr	hr	hr '4	hr. 1·0	hr92 .8 .1 .326 .6 .6 I .0 .8 .274 .9 .9 I .0 I .0 I .0 I .0 I .0 I .0 I .0 I .0 I .0 I .0	hr9 .2 .8 .5 .2	hr. 1.0 .5 .7 1.0 .2	hr. 1 · 0 · 6 1 · 0 · 9 · 4 ·	hr. 1.0	·4 ·6	·5	·2 ·· ·· ·2 ·· ·· ·· ·· ·· ·· ·· ·· ·· ·			hr.	hr. 6·9 2·3 5·7 6·4 1·0 1·4 6·3 5·57 6·7 0·5 6·7 1·7 6·8 3·7 4·0 1·2 1·6 2·7 5·7	% 59 20 50 56 16 9 13 58 51 72 63 5 64 17 61 47 37 40 12 16 27 59
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	hr.	hr.	hr	hr	hr	hr '4	hr. 1·0	hr92 .8 .1 .326 .6 .6 .1 .0 .8774 .9 .9 .9 .1 .01 .01 .01 .01	hr9 .2 .8 .5 .2	hr. 1.0 .5 .7 1.0 .2	hr. 1 · 0 · 6 1 · 0 · 9 · 4 · · · · · · · · · · · · · ·	hr. 1.0 ·6 ·7 ··· ·4 ··· ·1 ·1		·5 ·2	·2 ·· · · · · · · · · · · · · · · · · ·			hr	hr. 6·9 2·3 5·7 6·4 1·8 1·0 6·3 5·5 7 6·7 0·5 6·7 1·7 6·2 4·8 3·7 4·0 1·2 1·6 2·7 5·7 0·9 91·4	% 59 20 50 56 16 9 13 58 51 72 63 5 64 17 61 47 37 40 12 16 27 59 9 ————
1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	hr.	hr.	hr	hr	hr	hr '4	hr. 1·0	hr92 .8 .1 .322	hr9 .2 .8 .5 .2	hr. 1.0 .5 .7 1.0 .2	hr. 1 · 0 · 6 1 · 0 · 9 · 4 ·	hr. 1.0	.4	·5	·2 ·· ·· ·2 ·· ·· ·· ·· ·· ·· ·· ·· ·· ·			hr	hr. 6·9 2·3 5·7 6·4 1·8 1·0 1·4 6·3 5·57 6·7 0·5 1·7 6·8 3·7 4·0 1·2 1·6 2·7 5·7 0·9	% 59 20 50 56 16 9 13 58 51 72 63 5 64 17 61 47 37 40 12 16 27 59
1 2 3 4 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Sum.	hr.	hr	hr	hr	hr	hr	hr. 1·0	hr92 .8 .1 .322	hr9 .2 .8 .5 .2	hr. 1·0 ·5 ·7 1·0 ·2 ·5 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	hr. 1 · 0 · 6 1 · 0 · 9 · 4 ·	hr. 1.0	.4	·5 ·.2 ·.2 ·.3 ·.2 · · · · · · · · ·	·2 ·· · · · · · · · · · · · · · · · · ·			hr	hr. 6·9 2·3 5·7 6·4 1·8 1·0 6·3 5·5 7 6·7 0·5 6·7 1·7 6·2 4·8 3·7 4·0 1·2 1·6 2·7 5·7 0·9 91·4	% 59 20 50 56 16 9 13 58 51 72 63 5 64 17 61 47 37 40 12 16 27 59 9 ————
1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Sum. Mean.	hr.	hr.	hr	hr	hr2 .5	hr '4		hr92 .8 .1 .326 .6 .6 .1 .0 .8771 .9 .9 .9 .9 .1 .01 .91111	hr9 .2 .8 .5 .2	hr. 1·0 ·5 ·7 1·0 ·2 ·5 ··· ·· ·4 ··· ·9 ··· ·8 ·7 ·9 ·· ·8 ·7 · ·8 ·4 ·12·9 0·42	hr. 1 · 0 · 6 1 · 0 · 9 · 4 · · · · · · · · · · · · · ·	hr. 1.0 -6 -7 4			·2 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··			hr.	hr. 6·9 2·3 5·7 6·4 1·8 1·0 1·4 6·3 5·5 7·7 6·7 0·5 6·7 1·7 6·2 4·8 3·7 4·0 1·2 1·6 2·7 5·7 0·9 91·4 2·95 Total	% 59 20 50 56 16 9 13 58 51 72 63 5 64 17 61 47 37 40 12 16 27 59 9 —— 28 Per cent. of
1 2 3 4 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Sum.	hr.	hr	hr	hr	hr	hr		hr	hr9 .2 .8 .5 .2	hr. 1·0 ·5 ·7 1·0 ·2 ·5 ··· ·· ·4 ··· ·9 ··· ·8 ·7 ·9 ·· ·8 ·7 · ·8 ·4 ·12·9 0·42	hr. 1 · 0 · 6 1 · 0 · 9 · 4 · · · · · · · · · · · · · ·	hr. 1.0 -6 -7 4		·5 ·.2 ·.2 ·.3 ·.2 · · · · · · · · ·	·2 ··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··			hr.	hr. 6·9 2·3 5·7 6·4 1·8 1·0 1·4 6·3 5·5 7·7 6·7 0·5 6·7 1·7 6·2 4·8 3·7 4·0 1·2 1·6 2·7 5·7 0·9 91·4 2·95 Total	% 59 20 50 56 16 9 13 58 51 72 63 5 64 17 61 47 37 40 12 16 27 59 9 — 28 Per cent.

For periods of sixty minutes, between the exact hours, of Local Apparent Time.

353. Cahirciveen (Valencia Observatory): hs (height of recorder above ground) = 12.8 metres.

November, 1923. Total |Per cent. 9 to 10 to 11 to Noon 13 to 14 to 15 to 16 to 17 to 18 to 19 to 10. 11. Noon 13. 14. 15. 16. 17. 18. 19. 20. 3 to 6 to 8 to 20 to for of Day. 4 to 5 to 7 to 21. Day Possible 8. 10. II. Noon 13. 14. 15. 17. 9. hr. hr hr. hr. hr. hr. hr. hr. hr. hr. hr. hr. hr. hr. hr. hr. hr. hr. hr. ٠ı 1.3 14 ٠4 ٠4 0.9 10 ٠6 ٠١ ٠2 ... 3 ٠8 43 .3 •2 ·7 ٠Q ٠7 3.3 35 ٠4 ٠7 ٠9 ٠4 • • • 7.0 0.1 1.0 1.0 ٠9 75 I .0 •7 • • • 7 8 ... ٠6 ٠6 59 28 I •0 ... 1.0 ٠9 ... ٠ı ٠6 2.5 ٠5 .3 ٠4 10 ... •5 ... 11 ... • • • 12 13 38 •2 3.4 • • • 14 ... ٠7 3.3 38 ٠4 ٠8 ι·ö •7 ٠1 • • • 15 47 27 30 ٠8 ٠8 ٠8 16 •2 ٠5 .7 2·3 2·6 ٠Ğ .2 ·6 •7 17 18 ·5 ·5 ·7 ٠2 .9 .8 ٠ı ٠2 ٠ı ... ·3 ·7 3.5 .3 ٠2 ... 4 I .7 .6 ... IQ •2 ٠ī •2 •2 ... 20 65 **83** 1.0 1.0 1.0 5·5 **7·0** 21 ٠I 1 ·0 ı.o ı.o 1 ·O 1 ·0 22 ... 82 1.0 I .O ·9 ·8 6.9 1.0 1.0 1.0 1.0 ... 23 ٠8 6.4 77 ·9 ·8 1.0 1.0 ı.o ٠9 ... 24 ... 42 3.5 ٠6 25 •т 1.0 1.0 26 ... 27 28 48 .8 3.9 ٠9 1.0 1.0 •2 . . . ٠ı 54 12 ٠8 .2 4.4 ·7 1.0 •9 . . . 298 30 84.4 8.5 4.8 11.5 **15.5** 12.9 0.3 Sum. ... 14.0 14.9 2.81 32 0.52 0.28 0.16 0.01 o.38 0.50 0.43 Mean. 0.07 0.47 December, 1923. Cahirciveen (Valencia Observatory) : $h_s = 12.8$ metres. 354. hr. hr. hr. hr. hr. hr. hr. hr. hr. hr. hr. 1.6 20 ٠8 ٠4 ·4 ·6 ٠8 2.6 32 •2 ٠4 ... 39 8 3.1 ٠7 ٠4 3 .3 .3 ·2 ·8 ٠т8 33 .3 ... ٠4 5 0.2 3 •2 6 0.1 •т . . . 41 •2 ٠I •5 .8 I .0 •6 3.2 ... ŏ·8 ٠ı ٠43 ٠.. ... 10 ٠.. ٠.. ... TI ... 12 ... -8 6.1 79 .3 1.0 1.0 1.0 1.0 1.0 13 14 ... 8 0.6 ٠ı 15 ٠ı 16 I · 2 16 .2 •2 ٠7 ٠ı 17 18 2.2 20 ٠ı ٠6 .7 19 ... •3 ... o·8 10 ٠4 ... 20 21 22 •6 2 · I 27 •7 23 ... •5 .3 _ 24 • • • • • • • • • • • • ... 25 ٠.. 26 ... 27 28 ... ٠.. ... 2.3 30 ٠ı .3 1.0 •5 ... •4 • • • 29 1.7 22 ٠ı ٠9 30 .7 31 31.8 Sum. 2.7 6.4 1.3 4.7 4.3 1.03 14 0.22... 0.00 0.18 Mean. 0.15 0.21 0.14 0.04 Annual 86·o 6.8 24.8 Total. 2.7 21.1 40.5 60.2 116·2 134·0 135·5 **144·4** 139·1 124·1 103·6 78·4 56.9 ... 274.3 Annual 0.16 20 0.06 0.11 0.24 0.32 0.36 0.40 0.38 0.28 0.21 0.19 0.07 3.49 0.37 0.34 Mean. 6 to 8 to 10 to 11 to Noon 13 to 14 to 15 to 16 to 17 to 18 to 19 to 20 to Total Per cent a to Hour 3 to 4 to 5 to 7 to for of í8. Noon to 13. 6. 9. 19. 20. L.A.T. 5. 7. 10. II. 14. 15. 16. 17. Possible. Day.

Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$): Speed in metres per second.

355. Cahirciveen (Valencia Observatory):

 H_a (height of anemograph above M.S.L.) = Height of ground above

Day.	1	ι.	2	2.	3	3.	4	·		5.	,	5.	2	,.	8	8.	ç).	1	о.	1	I.	No	on.
	1 .	m/s.	0	m/s.		m/s.	0	m/s.	1 0	m/s.		m/s.	0	m/s.	°	m/s.	·	m/s.	٥	m/s.	۰	m/s.	0	m/
I	25	2.3	30	1.6	30	2.3	30	2.0	30	1.6		1.0	130	2.0	165	3.3	165	6.2	140	7.5	140	9.5	155	10.
2	185	8.5	185	9.8	180	10.8	180	10.8	190	10.2	225	10.8	225	8.9	225	9.8	225	9.8	220	11.2	220	12.2	220	13.
3	250	16.7	255	16.4	260	14.1	270	14.8		13.8	270	12.8	270	13.4	265	13.1	285	14.8	285	14.8	280	14.8	285	12.
_	325	6.6	325	3.6	325	3.6	325	2.6	305	5.6	310	3.3		1.3	1	0.7		0.3		1.3	205	1.6	200	2.0
4 5	175	9.2	180	8.5	180	8.9	190	10.2	245	10.2	280	2.0	260	6.6	285	10.3	295	10.8	290	12.8	295	11.2	290	11.
J	1 1/3] -	1.00	ر	1	-)	- ,-		'	1	Į.						_		_				250	1
6	285	10.8	285	9.5	285	9.8	290	9.5	285	9.8	285	8.9	280	7.9	265	5.6	260	8.2	265	5.9	255	4.9	250	4
7	240	9.8	240	10.5	240	10.2	240	10.2	240	9.5	240	9.8	240	9.8	240	8.2	240	6.9	230	5.6	230	5.6	225	5
8	260	9.8	270	4.6	280	8.2	290	9.2	290	9.2	290	10.2	295	10.2	295	9.5	295	7.9	295	8.5	290	9.8	285	7:
9	220	11.1	230	14.1	240	18.4	255	16.7	245	15.4	255	17.7		16.7	255	18.4	255	17.4	250	17.7	240	17.4	245	17
10	255	18.4	260	18.4		16.4	275	15.7	275	14.8	280	14.4	285	15.4	285	13.8	285	12.5	290	12.8	285	12.8	290	II.
			i	1							i	0 -		6.0	220	6.0	340	7.5	325	6.9	325	7.2	330	6.
11	315	10.2	305	8.9	325	8.5	330	9.8	325	8.5	340	8.5	340	6.9	330	6.9	340	7.5	50	2.3	3~3	0.7	330	0.
I 2	25	1.6	30	2.6	-	0.7	30	1.6	-	1.3	30	2.0	35	3.0		0.3	7.70			3.3	170	2.0	170	2.
13	160	3.6	175	3.3	170	4.3	170	5.6	170	4.3	170	3.6	170	1.6		1.3	170	2.3	170 320	3.6	335	5.6	345	5.
14	230	5.9	230	6.6	230	7.5	235	9.8	235	9.2	230	9.2	240	10.2	250	10.5	310	2.0	205	2.0	180	2.0	90	1.
15	290	4.3	280	3.6	260	3.9	260	4.3	250	3.3	255	3.6	245	2.3	230	2.0	220	2.0	205	2.0	100	20	90	1
16	1	0.0		0.3		0.7		0.3		0.7		1.3	185	3.3	180	3.6	180	2.6	180	2.3	180	3.0	180	3.
	160	4.6	7.55	3.9	155	3.6	160	2.6	150	4.6	155	4.6	155	4.6	155	4.3	155	4.3	155	4.6	150	4.3	160	4.
17 18	100		155	0.7	155	0.7	_	0.3	130	0.7	-55	0.7	-33	0.7		1.3		1.0	_	0.3	_	0.0		0.
		0.3		0.7	_	1.3		1.3	215	2.6	215	3.0	215	3.6	220	4.6	230	5.9	235	7.5	235	7:5	235	7.
19 20		8.5	27.5	9.8	315	9.2	320	10.8	330	10.8	330	11.1	330	12.8	330	10.2	330	9.8		11.5	340	11.8	340	11.
20	315	0.3	315	9.0	313	92	320	100	330	100	330		33-		33					_				
21	330	2.0	295	4.9	285	5.2	285	6.2	290	6.2	295	3.6		1.0		1.3	285	3.3	275	3.6	300	5.2	320	4.
22	305	3.9	300	4.6	300	3.9	300	3.0	300	4.3	290	6.6	295	6.2	300	6.9	295	4.6	280	4.9	285	6.2	280	5.
23	J	0.7	<u> </u>	0.3		0.3		0.3		0.3		1.0	_	0.7	-	1.0		0.7	150	4.9	170	4.9	175	3.
24	240	4.3	245	5.9	245	7.5	260	3.6	255	4.3	255	3.9	255	4.6	255	3.3	255	4.6	250	3.9	250	5.9	250	6.
25	240	2.3	225	2.6	220	2.3	220	2.3	215	2.6	205	3.3	200	3.3	195	3.6	195	3.9	190	3.9	190	3.9	190	4
•	1		ľ	ĺ	l			-	l											6	225	1.6	225	2.
26	200	2.3	200	2.0	200	2.0		1.3	200	3.0	210	3.3	230	2.6	230	2.6	230	2.3	235	1.6	235	6.6	225	6.
27	220	3.9	225	5.6	230	5.6	235	3.9	235	3.6	235	5.2	240	6.6	240	5.9	245	5.9	245	6.9	245		245	6.
28	-	0.3		0.3		1.3		0.7	_	I.0		0.3	220	3.3	190	3.0	195	2.0	240	2.3	225	1.3	240	11.
29	225	4.9	225	4.3	225	4.9	230	5.6	230	4.6	225	3.6	225	4.6	225	4.9	235	6.6	235	7.2	235	11.5	235	
30	240	8.5	240	9.2	240	8.5	240	9.5	240	8.5	240	5.6	230	3.3	225	3.3	225	4.6	225	5.6	230	4.9	220	7.
31	220	3.0	200	3.6	200	3.6	185	4.9	175	5.6	175	5.9	180	5.9	180	6.2	185	6.9	185	7.9	180	7.5	190	8.
																5.8		5.8		6.3		6.6	_	6.
ean	—	5.8		5.8		6.1		6.1	-	6.1	_	5.8	_	5.9		2.0		2.0		0 3	İ		l	1

356. Cahirciveen (Valencia Observatory) : $H_a = 12$ metres + 14 metres.

			•			_																		L t.
	0	m/s	0	m/s	0	m/s	٥	m/s	٥	m/s	٥	m/s	°	m/s	0	m/s	٥	m/s	0	m/s		m/s 9·8	200	m/s 9·8
1	225	8.5	195	5.2	190	6.2	190	7.2	190	8.5	195	9.8	210	10.2	220	12.1	225	12.5	215	11.1	205	4.6	220	7.5
2	220	6.9	220	7.9	220	7.2	225	6.6	225	5.6	225	6.2	215	5.2	210	5.9	195	4.9 8.2	185	4.9 6.2	195 225	6.6	220	7.9
3	225	6.9	225	7.2	225	8.2	225	8.2	225	10.2	225	8.5	225	6.2	225	7.5	230	0.3	230	1.0		0.7	205	2.6
4	285	6.6	285	6.9	295	4.3	295	2.6	310	2.3	315	2.0	305	3·3 9·8	l	9.7	175	10.8	175	10.3	175	8.9	175	10.5
5	175	9.8	175	9.8	175	9.5	175	9.2	175	9.5	175	9.2	175	9.0	175	92	1/3		-73		,,,		, ,	
ء ا			700	8.5	185	5.6	180	6.6	220	5.9	185	6.2	215	8.5	215	7.5	220	8.9	200	6.9	195	7.2	190	7.5
6	175 160	14.1	190	12.8	135	5.6 14.8	130	21.0	150	24.3	195	14.4	220	14.8	230	13.4	230	12.8	210	8.2	220	8.9	220	8.5
7 8	185	3.3	140 170	4.3	160	4.6	175	4.3	185	3.3	190	3.9	180	3.9	165	5.2	170	3.9	160	6.2	175	5.6	160	5.2
9	205	4.3	190	3.9	170	4.9	170	3.6	170	4.9	155	6.6	145	8.9	150	8.9	145	11.1	135	13.8	145	13.4	135	15.1
10	175	9.2	175	9.2	175	10.2	175	10.5	175	9.8	175	9.8	180	8.9	175	8.3	180	6.9	180	4.9	175	5.3	185	5.6
11	230	2.3	240	3.3	265	4.6	275	8.9		10.8	275	9.8	280	10.2	275	10.5	290	8.5	275	9.2	280	6.9	255	8.2
12	-30	0.3		0.3		0.0	-/3	1.3	205	1.6		0.7		0.3	-	0.0		0.0		0.7	145	2.0	180	2.6
13	190	5.2	190	4.6	190	3.9	190	4.3	190	3.9	200	2.3	200	2.0	i —	1.3		0.0		0.3		1.0	T-20	1.3
14		0.7		1.3		1.3	l —	1.3		1.0	l	1.3	30	2.0	-	1.3	30	2.6		1.0		0.7	120	3.9
15	130	10.5	130	8.01	135	11.5	130	10.8	130	10.2	135	10.2	140	10.2	155	8.2	175	5.6	165	3.3	190	4.6	155	39
-6	180	4.2	1.70	5.2	170	7.5	170	8.2	165	9.2	160	10.5	165	10.2	160	10.8	160	12.1	155	11.5	160	11.5	160	9.8
16	260	4.3	170 260	5.2	170 270	7.5	265	3.3	220	1.6	85	2.0	155	4.9	155	5.9	165	6.6	155	7.2	155	8.5	155	9.2
17 18	175	6.6	230	15.4	250	16.1	250	13.1	255	11.8	250	13.4	240	11.5	230	8.2	230	6.2	255	8.5	255	9.2	250	10.8
	280	7.2	285	6.9	280	6.6	295	3.6	300	2.0	300	3.3]	1.0		1.0	40	2.3	35	1.6		0.3		0.0
19 20		1.0	35	1.6		1.0	-53	1.0	35	2.0	35	2.0	35	2.0	75	1.6	135	5.2	150	7.2	150	7.9	155	8.9
20			1				ł								225	9.2	235	5.9	235	6.6	260	6.6	210	4.3
21	235	6.9	230	7.9	230	9.2	230	8.5	235	8.9	235	9.8	215 185	3.3	225 145	2.0	160	3.6	110	2.3		1.3		1.3
22	215	2.6	195	3.3	180	3.0	80	1.6	135	5.2	135 200	4.6	180	3.0	180	3.6	180	3.9	160	5.2	155	7.2	155	8.9
23	160	3.6	210	3.9	245	3.3	190	3.0	190	1 -	85	3.3		0.7		1.0	_	1.0		0.3	_	0.7		1.3
24	160	4.9	145	4.9	140	5·6 6·8	115	3.3	75	5.3	230	$6 \cdot I$	230	7.6	225	7.8	230	9.6	230	6.1	220	6.5	215	7.0
25	205	6.4	235	5.6	245	0.8	240	0.5	235	3.3	230	0.1	230	, ,	1 223	/ "	-30	, ,	-3			-		
26	755	8.4	160	8.7	170	10.6	185	11.8	185	13.4	180	13.5	175	13.5	175	9.6	210	$II \cdot o$	225	11.9	225	11.0	225	8.3
!	155 270	17.9	275	18.0	280	17.2	280	16.4	280	15.0	280	15.0	280	15.0	280	15.5	285	14.8	285	14.5	285	14·1	285	14.2
27 28	260	9.6	255	7.2	240	5.7	210	3.7	200	2.7	200	3.5	210	1.9	125	2.2	45	2.9	35	2.1	_	1.5	290	4.3
		ļ		<u> </u>	<u> </u>			ļ				6.8		6.6		6.3		6.5		6.2		6.2	_	6.7
Mean	_	67	_	6.8		6.8		6.8	_	6.9		0.8		0.0	_	0.3						<u> </u>	<u> </u>	
	<u>'</u>				<u>'</u>	,	i	i		<u> </u>	'										l ,	Ι.	N	oon.
G.M.T.	1. 2.		:.	3	3.	4	١.	5	j.	6		7	7.	8	3.	و ا).	I 1	o.	, '		1		
			<u> </u>				<u> </u>		l				<u> </u>		<u> </u>		!				<u></u>		·	

Averages for periods of sixty minutes, centered at the exact hours, Greenwich Mean Time.

M.S.L. $+ h_a$ (height of anemograph above ground) = 12 metres + 14 metres.

January, 1923.

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13.		I	f ·	I	5.	16	5.	17	7.	18	3.	19	9.	20).	2	I.	22	2.	23		24	f -	Mean	Day.
155 12 225 13 290 12 190 3	n/s. 2 · I · 3 · 8 2 · 8 3 · 3 0 · 2	225	m/s. 10·8 14·4 11·1 3·0 10·8	180 230 305 195 290	m/s. 6·9 14·1 10·2 3·6	215 230 310 190 295	m/s. 7.5 14.8 10.5 4.3 10.5	215 235 315 190 300	m/s. 7·5 15·1 10·2 4·6	210 235 325 185 290	m/s. 7·5 16·7 9·8 5·2 9·5	325 175	m/s. 7·5 16·7 10·2 5·9	220 240 320 175	m/s. 8·9 16·4 11·1 6·9	220 245 325 175	m/s. 9·8 16·7 11·5 7·2	210 250 330 175	m/s. 8·5 16·1 10·5 7·2 8·2	210 250 330 175 280	m/s. 8·5 14·8 7·5 8·5	325 175	8·5 9·2	m/s. 6·2 12·9 12·5 4·2	1 2 3 4
235 5 225 4 275 4 250 17	5·2 4·9 4·9 3·1	205 215 265 250 290	4·3 4·9 3·3 18·0	190 215 250	5·2 5·6 5·2 17·0 9·8	180 220 230 260 295	6·2 6·6 4·3 16·4 8·9	175 220 200 260 300	6·9 5·9 4·3 18·4	175 215 190 260 300	8·5 6·6 5·2 17·7 10·2	175 205 190 250 300	7.5 6.2 7.5 18.7 9.8	305 195 200 185 250 305	9·5 6·2 5·9 8·2 18·7 7·5	290 225 210 180 270 325	9·5 5·2 8·2 9·5 17·0 8·9	295 235 205 180 250 315	5·9 7·9 10·8 18·4 7·9	235 205 195	9·2 5·6 7·5 11·1 16·7	295 235 230 225 260 325	6.6 10.8 12.1 17.0 9.8	9·7 7·1 7·5 7·9 16·9 12·5	5 6 7 8 9
200 3 330 3	7·2 0·0 3·3 5·2 1·0	335 225 335 210	3·9 0·7 4·3 5·6 3·9	20 50 230 335 235	2·6 1·6 3·6 5·6 6·2	235 315 245	1.0 1.0 2.3 4.3 6.2	- 135 - 315 250	1·3 2·6 1·0 2·6 4·9	350 135 — — 250	1.6 2.3 1.3 1.0 4.3	100 235 300 250	0·7 2·0 2·0 3·3 1·6	 235 300 	0·3 0·7 1·6 3·9 1·3		1·0 1·3 2·3 4·3 0·0	220 305 245	1.0 1.3 3.6 3.6 2.3	110 225 300	1·3 1·6 4·9 3·3	20 225 285 	2·0 1·3 6·2 3·6 0·3	5·2 1·4 3·0 5·6 2·9	11 12 13 14 15
170 330 235	4·3 5·2 3·6 9·2 0·8	175 175 325 235 345	3·9 5·2 3·9 9·5 9·5	175 175 3 ² 5 230 345	2·6 4·6 4·3 7·9 8·5	175 170 325 245 360	3·6 3·6 2·6 11·1 8·5	180 130 — 245 360	3.6 3.0 1.0 9.8 6.2	180 — 300 240 360	4·3 1·0 3·9 11·1 5·9	170 — 300 245 5	3·9 1·0 4·6 10·5 5·6	165 5 300 250 5	4·6 3·6 3·0 10·2 4·9	165 360 295 260 5	4·3 3·3 2·3 8·5 3·6	170 360 — 270 345	3.6 2.3 1.3 10.8 3.9	165 360 — 290	4·9 1·6 0·7 8·9 0·3	165 — — 310 —	2·3 1·0 1·0 8·9 0·7	2·7 3·6 1·7 6·6 8·3	16 17 18 19 20
280 225 245	4·6 5·9 3·3 3·3 5·2	310 280 235 240 200	5·6 6·6 5·2 4·9 4·6	300 280 245 240 205	4·3 7·9 5·6 5·2 4·6	300 280 245 240 205	4·6 8·5 5·2 4·3 3·9	310 295 245 240 215	4·3 6·9 4·3 3·0 3·0	300 300 245 240 215	5·6 5·9 3·9 3·6 3·0	295 300 245 240 215	5·2 5·2 3·9 4·3 3·3	300 310 245 240 215	5·6 5·2 3·0 3·6 3·3	310 320 245 240 215	4·3 3·9 4·3 2·0 2·6	310 315 245 240 215	2·3 5·2 4·9 3·3 3·0	310 5 250 240 210	2·6 3·0 3·0 2·0 2·0	310 — 245 240 205	2·6 1·3 4·3 2·3 2·3	4·I 5·3 2·8 4·2 3·3	21 22 23 24 25
245 3 230 2 240 10	2·3 3·9 4·3 0·8 4·6	215 245 225 240 190	2·6 4·6 5·2 11·1 4·6	215 245 225 240 185	3·3 4·9 6·2 10·2 5·2	215 250 230 240 180	3·3 3·9 5·6 10·5 4·9	215 250 235 240 185	2·3 4·9 4·6 10·2 5·2	215 250 240 245 190	2·6 5·2 5·9 9·5 5·9	215 250 240 240 215	2·3 5·2 5·2 11·1 6·9	215 250 235 240 220	2·6 3·3 3·6 11·5 5·2	215 255 235 245 220	2·6 4·3 4·6 8·5 3·9	215 255 235 245 220	3·6 4·6 8·9 3·3	220 255 230 245 220	2·6 1·6 4·6 7·9 3·0	220 — 225 240 220	3.6 1.0 5.2 9.2 3.3	2·5 4·7 3·3 8·0 5·7	26 27 28 29 30
	9·2 6·6	200	9·8 6·7	200	9·8 6·6	210	9·5 6·4	215 —	9·2 6·0	210	9·5 6·3	220 —	9·8 6·4	220	6·1	220	8·5 5·9	220 —	7·9 6·0	220	8·9 5·4	225 —	7·9 5·7	7·4 6·1	31

February, 1923.

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200	8.5	195	10.2	200	10.2	205	10.8	205	12.5	215	12.8	215	13.8	220	11.8	220	12.5	220	10.5	220	8.5	220	9.2	10.1	I
220	7.9	215	7.5	215	8.2	215	8.2	220	9.2	220	8.5	220	8.9	220	9.2	220	8.9	230	9.5	230	9.2	230	6.9	7.3	2
230	7.9	235	8.5	230	9.5	250	7.5	265	9.2	260	6.9	265	7.2	270	7.2	275	7.9	290	8.2	290	6.6	290	6.2	7.7	3
185	3.3	175	4.9	170	5.6	175	5.9	175	6.2	175	5.6	175	6.9	175	7.9	175	7.9	175	8.2	175	8.2	175	8.9	4.6	4
175	10.2	175	11.8	175	12.1	175	13.4	175	13.8	175	13.4	175	14.8	175	14.4	175	14.8	175	14.8	175	14.4	175	15.4	11.5	5
195	8.2	195	7.2	210	9.2	220	8.5	200	6.2		6.	20-	6.0	20-		-0-	6 .			-0-					_
200	6.6	190	7.2	180	6.2	175	6.6			225 170	6.9	205	6.2	225	9.2	185	6.6	190	5.9	185 180	5.2	175 180	7:5	7.7	6
155	3.6	250	7.9	295	5.9	295	10.2	170 285	7.5	285	7.5	190 260	5·2 7·2	175 250	4·6 6·2	195 250	6.2	240	5·6 5·2	230	4.3	210	4.3	9·9 5·6	8
135	18.4	140	17.7	160	16.1	170	11.5	170	11.8	170	10.5	170	9.8		10.2	170	9.8	175	10.2	175	4·3 9·5	175	3.3	10.1	9
185	6.2	195	5.6	185	5.2	195	4.9	185	3.6	200	3.6	190	3.3	210	4.3	195	2.6	215	4.3	210	3.3	215	2.3	6.3	10
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245	7.2	235	6.6	230	5.9	220	3.3	200	3.0	190	3.0	195	3.3	195	2.6		0.3	175	1.6	155	2.0	155	1.6	5.6	11
190	3.0	190	3.6	195	4.3	195	4.6	195	4.9	190	4.9	190	4.6	185	5.2	185	4.9	185	5.6	185	5.6	190	4.6	2.7	12
235	3.0		1.0	235	3.0	240	3.3	265	2.6	_	0.0		0.3		0.3		0.0		0.0		0.0		0.0	1.9	13
120	2.0	110	3.3	110	4.3	110	5.9	110	4.9	105	6.6	100	6.9	100	7.9	110	10.2	105	11.5	130	8.5	130	11.1	3.9	14
170	3.9	170	5.9	230	6.6	230	8.9	235	6.6	235	5.9	235	3.3	230	4.6	220	3.9	190	3.6	185	3.9	185	3.9	6.9	15
165	6.6	220	2.6	200	2.0					. 0															- c
165	7.5		5.6	300 185	3.0 6.2	345 180	3.3	290	7.5	280	10.2	275	9.2		10.2	260	9.8	255	9.8	260	8.5	250	8.5	8.3	16
280	15.1	175 290	15.4	280	16.4	285	5.2	180 280	6.2	175	5.9	180	5.6	180	5.2	185	4.6	180	5.2	165 280	5.2	165	6.2	5.7	17
	0.0	15	1.6	350	2.0	335	14.8		13.8	275	12.1	275	11.8		II.I	280	II.I	275	12.8		9.8	295 —	10.5	11.8	
155	9.8	160	9.8		11.5	160	10.8	335 160	11.1	7.50	I.0		0.7		0.3	345	1.6	240	1·3 8·9	240	8.2		6.2	2·3 6·5	19 20
33						100	1.0 0	100	11 1	150	11.5	150	12.5	155	9.5	255	7.2	240	0.9	240	0 2	235	0 2	٠ ₃	20
230	8.5	240	9.5	240	10.2	240	10.8	240	8.9	250	11.8	250	10.2	250	11.8	250	7.9	245	9.5	240	4.9	215	3.6	8.2	21
	.0.3	290	2.6	330	3.6	275	4.6	280	4.6	260	3.0	225	2.0	140	2.3		1.3	80	2.0	150	5.6	155	6.6	3.0	22
145	9.5	135	9.5	135	10.8	135	9.8	135	10.2	135	11.8	125	12.8	115	10.5	120	7.9	120	4.9	155	4.3	155	5.2	6.6	23
280	3.3	280	2.6	275	2.3	260	2.0		1.0	250	2.6	240	7.9	255	5.9	255	3.6	230	3.0	215	3.9	200	4.3	3.0	24
210	6.0	185	5.2	165	5.7	165	7.5	180	6.3	190	6.0	175	6.0	145	7.1	130	7.7	110	9.5	100	10.2	125	9.7	$6 \cdot 9$	25
245.	.7.6	0.45	ا ر و	255	T7.0	260								"										1 1	
245· 280	·7·6 13·2	245 280	8·4 13·6	255 280	17.2	260	22.1	260	23.5	260	23.3	265	23.3	270	20.3	275	18.4	275	18.8	275	18.2	275	18.0	14.4	26
290	7.3	290	9.5	285	9.3	285 285	13.3	285	12.6		12.3	285	12.2	285	10.8	285	10.2	280	10.0	275	9.6	265	10.0	13.9	27
	/ 3	290	9.3	405	9.3	205	9.9	280	10.2	280	10.0	275	10.0	280	9.7	285	10.7	270	$IO \cdot I$	265	10.8	275	11.3	6.9	28
_	7.0		7.3		8.0		8.2		8.2		8.1		8.1		7.0	_	7.2		7.5		6.9		7.0	7.1	
										!	~ 1		0.1		7.9		7.3		7.5				'	′ -	
	1	_			Ī				i		i	<u> </u>			`	 		 	·	i	·!	1		i i	
13	.]	14	14. 15.		. 1	16	·	17	٠. ا	18	. [19).	20	o.	2	I.	2:	2.	2	3.	2	4.	Mean	Day.
			1		1		!				!		- 1		- 1	l		1		i)			

Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$): Speed in metres per second.

357. Gahirciveen (Valencia Observatory):

 H_a (height of anemograph above M.S.L.) = Height of ground above

Day.	1.		2	•	3		4	•	5	j.	6		7		8		g).	ı	0	ı	1.	No	oon.
1 2 3 4 5	280 240 265 10 170	m/s. 9·0 13·5 8·2 7·4 10·9	275 240 275 10 185	m/s. 8·7 13·8 7·5 5·9 11·0	285 5	m/s. 7·4 13·7 6·7 6·7	260 235 290 55 235	m/s. 7 · 4 13 · 3 7 · 5 1 · 6 9 · 8	240 235 330 50 245	m/s. 5·1 11·8 7·4 1·9 9·1	210 245 350 — 255	m/s. 3·7 12·6 8·7 1·4 10·0	185 245 350 — 240	m/s. 3·3 12·7 10·5 1·2 7·9	160 245 255 — 255	m/s. 4·I 10·8 9·7 1·5 8·3	155 255 340 — 260	m/s. 6·2 11·5 11·2 1·0 7·3	150 240 245 175 265	m/s. 7·6 9·4 10·8 2·4 7·6	150 245 340 130 265	m/s. 8·8 9·0 12·1 1·9 7·3	150 255 345 185 265	m/s. 10·2 10·7 13·3 2·8 6·9
6 7 8 9 10	190 275 340 90 95	8·0 10·9 5·0 5·0 7·0	190 285 340 85 100	8·7 9·5 4·0 4·8 6·5	190 290 350 85 105	10·3 10·2 5·0 5·0 6·5	195 285 355 90 135	11·3 9·6 4·0 5·0 8·8	200 295 350 85 140	11·2 10·5 3·6 5·0 10·3	205 290 5 130 140	12·3 10·4 2·1 2·0 10·3	240 290 5 — 150	9·9 10·7 2·2 1·3 11·0	260 295 — — — 150	6·7 9·5 1·0 0·5 11·5	245 300 - 85 150	8·0 9·4 1·0 2·5 11·7	250 310 50 90 150	9·3 7·2 4·1 4·0 10·9	250 310 60 100 155	9·7 8·1 4·3 4·7 11·5	250 310 60 100 155	9·7 9·2 4·0 4·0 12·5
11 12 13 14 15	195 285 65 90	0·5 7·5 7·9 1·7 4·4	190 290 50 100	0·5 7·4 8·2 I·7 5·0	185 295 50 100	1·0 6·7 7·1 2·3 5·7	180 330 — 95	1·3 9·1 6·2 0·5 5·8	80 180 315 — 85	2·0 9·8 5·7 0·5 6·3	180 335 120 90	1.0 10.3 5.8 2.7 5.4	65 185 335 105 90	2·2 10·6 4·4 5·7 5·8	190 — 95 100	0·5 12·7 1·2 5·0 6·6	185 90 100	0·5 13·3 0·5 3·5 7·7	195 335 105 90	1·2 13·0 5·2 3·4 6·5	160 210 335 90 100	3·3 11·2 4·0 3·8 5·3	160 215 335 105 100	4·2 12·4 2·6 3·2 7·7
16 17 18 19 20	70 75 75 80 90	2·0 3·0 5·7 4·0 4·1	75 65 80 70 60	4·2 4·3 3·0 4·5 2·7	70 85 80 60 120	1·9 5·9 3·3 3·2 2·0	75 75 90 85 85	3·5 4·4 2·5 3·7 4·0	65 70 - 85 55	2·9 3·7 1·0 3·1 2·0	85 100 — 90 55	3·5 3·6 0·5 3·2 2·7	95 95 70 90	2·1 3·8 1·9 4·3 1·5	95 60	4·6 2·7 2·1 4·2 2·1	95 20 85	4·0 1·7 1·7 4·5 1·2	100 85 70 100	5·4 1·8 3·5 4·9 1·2	90 65 90 85	3·8 3·6 2·1 4·0 1·3	90 55 235 80	4·5 3·5 1·7 4·8 0·5
21 22 23 24 25	 140	0·5 0·5 0·5 1·2 10·3		0·5 0·5 0·5 2·8 10·3	 	0·5 1·0 0·5 3·3 9·7	55 — — 140 165	2·0 0·5 0·5 4·1 9·2		1·3 1·5 0·5 4·7 8·6		0·5 1·3 0·5 5·0 9·7		1·0 0·5 1·5 4·9 10·3	 45 140 240	1·0 1·5 1·6 5·0 9·2	 55 140 240	0·5 0·5 2·9 5·2 7·6	— 80 140 255	0·5 0·5 3·8 5·8 9·0	315 80 155 250	2·8 1·1 3·6 6·0 8·5	340 20 110 160 235	3·0 2·5 2·6 7·2 8·3
26 27 28 29 30	150 160 345 170 165	7·9 13·3 5·8 4·8 4·5	150 165 330 160 160	9·1 12·7 5·8 5·4 3·3	150 170 315 160 255	10·1 12·8 6·7 5·4 5·1	150 180 310 160 345	10·5 7·7 6·7 5·7 7·0	150 185 305 160 340	10·3 5·3 6·5 5·9 7·0	155 170 310 155 335	10·8 4·3 5·7 6·6 6·5	150 180 305 160 350	11·4 4·5 5·5 6·6 5·3	160 175 305 160 350	11·8 2·8 4·7 6·8 4·7	160 175 285 165 340	11·9 2·5 5·0 7·4 5·8	160 170 285 165 340	12·5 1·7 3·8 8·5 6·6	160 170 280 165 345	12·9 2·1 3·7 9·6 6·7	160 175 270 165 340	12·8 2·3 4·3 10·1 6·8
Mean	60 —	2·I 5·7		2·3 5·6		5.7	105 —	5.6	_	1·5 5·4	_	o·5 5·3	55 —	2·2 5·4	110	2·7 5·1	175 —	4·0 5·2		5.8	——————————————————————————————————————	8·5 6·o	180 —	9·1 6·4

358. Cahirciveen (Valencia Observatory): $H_a = 12 \text{ metres} + 14 \text{ metres}$.

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1 2 3 4 5	45 — 300 65	m/s 1·9 1·3 0·5 3·0 6·3	60 175 310 60	m/s 1·2 2·3 5·1 5·0 6·6	65 175 315 40	m/s 2·9 I·4 5·I 4·2 6·0	60 185 320 30	m/s 1·1 1·7 4·2 5·4 6·2	60 60 185 330 30	m/s 2·2 1·7 5·5 5·2 5·6	60 — 175 350 15	m/s 2·9 0·5 3·7 4·0 7·2	60 175 360 30	m/s 3·7 1·3 5·6 4·3 6·4	90 — 175 360 15	m/s 4·2 1·0 6·2 4·6 6·8	95 175 25 15	m/s 4·0 1·3 6·9 4·2 7·0	100 170 30 355	m/s 3·7 0·5 7·3 4·6 8·2 4·6	135 280 175 20 355	m/s 3·8 1·6 7·2 4·2 9·1	125 265 170 30 350	m/s 2·9 2·7 7·2 5·3 10·6
6 7 8 9 10	350 180 135 125 85	4·9 2·8 3·1 9·6 8·1	20 — — II5 70	3·8 1·0 1·1 10·9 7·6	360 45 50 110 65	2·0 3·0 2·7 10·5 7·3	360 50 40 110 65	2·3 1·9 3·0 11·7 9·2	60	1·3 2·1 12·3 9·1	95 110 60	0·5 2·1 1·4 12·9 9·0	50	1·3 1·5 2·0 13·2 8·5	95 40 110 50	1·3 2·8 2·9 13·3 10·0	100 35 110 50	3·3 2·2 14·6 10·0	50 110 60·	0·5 1·9 12·5 10·3	190 15	2·3 1·6 11·8 9·3	190 265 110 55	5·0 2·0 14·6 10·2
11 12 13 14 15	75 140 70 285	7.0 2.5 1.7 8.0 0.5	85 — 285 300	6·4 0·5 1·0 7·2 4·1	55 275 330	5·7 1·2 1·7 6·3 8·4	75 90 55 275 325	4·9 1·6 1·8 6·4 9·0	80 90 55 255 325	4·3 2·9 1·8 6·1 8·8	85 100 40 225 315	2·3 2·3 1·6 4·8 8·2	100 45 225 325	1·3 3·0 1·7 4·6 7·1	120 260 330	1.0 3.2 1.5 5.2 6.4	40 135 — 245 325	2·4 4·2 0·5 5·5 6·9	75 140 — 285 325	3·5 4·4 0·5 6·3 6·5	145 310 285 315	4·7 2·7 7·2 7·2	155 310 275 325	4·2 7·4 7·2 7·2
16 17 18 19 20	340 175 190 75 100	5·0 7·9 9·7 3·0 5·9	330 185 230 125 110	5·3 9·1 3·9 2·7 6·8	325 190 265 150 115	4·8 9·7 2·4 3·5 6·5	310 185 — 140 90	4·2 10·5 1·3 4·5 4·7	315 185 — 150 90	3·4 10·8 0·5 5·7 4·9	315 185 — 140 85	2·3 10·6 0·5 6·0 5·2	190 — 125 90	1.0 10.6 0.5 4.9 8.0	190 — 125 90	1·2 10·8 0·5 4·4 5·3	315 185 — 140 75	1·8 11·0 0·5 5·8 5·4	310 190 — 140 45	2·0 12·2 0·5 6·8 6·7	310 190 145 40	2·7 11·5 0·5 7·9 6·8	310 190 315 150 40	3·3 11·5 3·0 9·2 7·2
2I 22 23 24 25	70 35 50 45 240	6·9 7·6 6·3 4·1 II·2	55 80 20 75 255	8·8 5·2 4·3 4·6 11·0	55 60 30 80 260	8·5 7·2 3·5 4·4 8·4	45 65 30 55 265	6·8 5·9 4·2 1·6 7·8	45 45 40 — 270	6·8 4·1 3·5 1·2 7·0	60 35 40 — 265	7·3 1·8 4·1 1·2 6·6	65 65 25 —- 270	7·8 3·2 3·8 0·5 7·1	60 65 15 — 265	8·6 5·7 3·8 0·5 8·0	50 60 10 175 260	8·5 6·7 3·5 2·0 8·4	45 60 340 185 260	9·6 7·1 3·7 2·5 8·7	40 55 340 185 260	9·6 7·7 5·2 4·1 10·0	40 50 350 180 260	10·3 8·3 6·7 5·5 10·2
26 27 28 29 30	340 — 260 175 225	10·2 0·5 3·5 2·3 10·1	340 — 230 170 225	11·3 0·5 2·8 2·7 10·5	340 230 145 220	11·7 1·0 2·3 1·8 11·0	220 75	10·6 0·5 4·1 2·2 11·2	345 230 65 210	10·5 0·5 3·8 2·2 10·8	340 235 100 215	10·3 0·5 3·5 1·6 11·2	235	11·3 0·5 4·3 0·5 11·5	350 — 240 — 210	8·9 0·5 5·0 0·5 10·7	340 — 250 — 210	8·5 1·1 5·6 0·5 10·4	345 250 190 210	9·7 1·1 5·3 3·0 10·6	340 315 230 190 210	10·0 2·8 5·0 4·5 10·7	340 270 260 180 215	9·0 3·3 5·3 6·4 II·2
Mean	_	— 5·2 — 5·1		5·1	_	5.2		5·1	_	4.9	_	4.5	_	4.7		4.8		5.2		5.5	_	6.0	_	6.8
G.M.T.	I	-	2			3.	4		5		6		7		8	3.	9		I	о.	1	Ι.	No	on.

WIND: DIRECTION AND SPEED.

Averages for periods of sixty minutes centered at the exact hours, Greenwich Mean Time.

M.S.L. $+ h_a$ (height of anemograph above ground) = 12 metres + 14 metres.

March, 1923.

13.		14	.	I,	5.	16	5.	17	7.	18	8.	1	9.	20).	2	ſ.	23	2.	2	3.	2	4.	Mean	Day.
160 II 255 IO 340 I3 190 3	n/s. 1·6 0·7 3·2 3·4 7·3	° 155 260 345 185 260	m/s. 13·1 8·5 12·5 5·0 7·0	175 260 345 190 260	m/s. 13·1 8·7 12·3 6·0 7·1	215 255 255 255 185 255	m/s. 13·1 9·3 11·2 6·5 6·3	235 250 355 180 235	m/s. 14·2 9·2 10·0 6·8 5·7	250 255 355 175 230	m/s. 14·0 7·9 11·2 6·7 5·5	245 275 360 175 215	m/s. 13·9 6·2 10·7 6·4 5·9	240 280 360 165 210	m/s. 12·5 6·4 9·5 7·5 6·0	245 285 360 165 210	m/s. 14·1 5·9 8·5 9·7 6·8	255 285 5 170 200	m/s. 15·4 7·1 7·6 11·0 7·2	260 290 360 170 200	m/s. 16·0 6·8 7·6 11·7 8·2	280 10	m/s. 15·0 8·2 8·1 11·7 8·2	m/s. 10·2 10·0 9·8 5·3 7·9	1 2 3 4 5
315 9 20 4 135 3	0·0 9·6 4·8 3·3 1·8	255 320 25 160 150	10·4 9·7 4·5 4·5 10·0	255 325 35 160 150	10·7 9·5 3·6 5·2 8·1	255 325 30 140 285	11·5 8·8 4·2 5·3 4·3	260 320 45 120 360	10·8 7·0 4·4 6·5 3·2	260 325 40 110 360	7·7 3·6 7·0 2·3	270 335 65 105	11·1 7·0 3·6 7·2 0·5	265 335 80 85	10·3 6·7 5·4 6·5 0·5	270 340 85 85 —	10·8 6·2 5·2 5·9 0·5	275 340 85 120	10·0 4·6 5·0 7·1 0·5	285 350 85 110	9·2 4·4 5·0 7·8 1·2	275 355 90 100	10·3 4·7 5·1 7·4 0·5	10·0 8·5 3·9 4·8 6·9	6 7 8 9 10
215 12 295 2 115 3	5·2 2·2 2·5 3·6 5·9	190 215 290 115 105	6·2 13·5 2·5 3·6 5·9	180 225 280 130 105	6·3 12·2 3·5 2·1 5·2	160 235 280 190 110	7·5 12·9 3·0 4·7 3·4	150 245 310 220 95	8·7 11·5 1·9 3·5 3·7	150 260 — — 70	10·5 10·8 1·0 1·5 4·3	160 270 — — 75	9·1 0·5 0·5 4·8	160 285 — 120 85	8·9 0·5 3·3 2·6	160 280 — 105 80	12·0 8·8 1·5 4·6 2·2	165 285 — 100 65	8·7 1·3 4·3 3·7	165 285 — 100 80	8·0 8·3 1·1 4·0 4·0	200 285 60 80 70	7·3 7·5 1·7 3·5 2·3	5·0 10·3 3·4 3·0 5·1	11 12 13 14 15
55 3 280 2 75 4	3·4 3·7 2·1 4·5	110 60 - 100 330	6·3 3·5 1·0 4·4 1·7	110 60 260 100	5·7 3·1 2·0 4·8 1·3	100 35 265 90 330	4·7 3·3 2·5 4·1 3·2	110 55 265 85 320	5·5 3·0 2·3 3·2 1·8	70 85	5·7 3·8 1·5 3·4 0·5	55 - 85 -	5·9 2·7 0·5 4·0 0·5	110 80 105 85	5·0 5·7 4·0 5·3 0·5	105 85 105 85 —	4·I 5·I 2·7 5·0 0·5	95 90	4·8 5·1 4·7 4·9 0·5	85 75 65 90	3.6 6.3 6.1 0.5	90 80 80 85	2·0 8·4 3·2 6·3 0·5	4·1 3·9 2·6 4·3 1·7	16 17 18 19 20
50 2 - 1 165 7	3·4 2·7 1·4 7·8 7·8	315 	2·7 1·3 2·8 8·3 6·5	330 345 275 155 225	3·7 2·4 3·8 7·0 6·4	335 275 155 190	6·3 1·3 2·8 6·7 6·2	335 50 220 140 185	6·5 2·7 2·8 6·0 5·6	355 75 175 145 180	5·8 3·6 3·7 7·2 5·3	355 80 175 135 160	4·4 3·4 3·3 6·2 4·8	350 80 170 135 155	5·8 4·2 2·7 7·0 6·6	355 85 — 115 150	3·7 4·6 1·3 8·5 6·9	360 80 110 150	3·0 4·0 1·2 8·3 7·1	25 — — 130 150	2·2 1·5 0·5 9·9 7·2		1·3 1·2 1·3 9·8 7·9	1.6 1.9 1.9 6.0 7.9	21 22 23 24 25
260 2 275 4 165 10	2·0 2·9 4·0 0·3	155 270 275 165 335	13·1 2·2 3·5 9·9 6·9	155 275 275 165 335	12·2 2·7 3·7 10·1 6·6	155 290 260 165 335	12·3 1·6 3·7 9·5 6·5	155 335 260 160 335	13·0 1·8 2·8 9·4 5·8	150 325 235 155 340	12·7 2·2 3·7 9·1 5·4	155 320 195 155 335	13.6 1.8 3.2 8.1 3.6	155 25 165 155 340	14.0 1.7 3.8 8.3 2.8	160 — 165 155 360	14·3 1·0 3·4 7·7 3·0	160 350 175 155 10	14·4 3·6 3·6 7·7 1·8	160 350 185 155	14·2 3·1 2·4 7·4 0·5	160 355 165 160 —	13·7 4·6 5·0 5·6 0·5	12·0 4·3 4·5 7·7 5·1	26 27 28 29 30
	8·4 B·4	275	8·1 6·4	290 —	6.4	285 —	7·2 6·3	290 	6.0	300	5.8	305	5.0	305 —	5.8	295	3.4	310	5.8	_	5.6		5.6	5.8	31

April, 1923.

																								•	
140 2 265 3 175 3 15	m/s 2·9 3·6 7·6 5·7 0·5	165 275 165 30 350	m/s 3.6 3.2 8.2 5.0 II.I	90 280 165 25 345	m/s 4·6 3·5 7·9 4·6 12·0	210 280 170 35 345	m/s 4·5 4·0 9·1 5·8 11·5	190 260 180 25 355	m/s 3·7 4·0 9·0 6·4 10·7	25	m/s 3·0 3·3 10·0 5·8 11·0	200 160 25 350	m/s 0·5 2·5 11·0 5·6 9·8	35 355	m/s 0.5 3.0 II.0 5.3 8.7		m/s 0·5 3·2 12·5 5·8 8·0	160 215 60 350	m/s 1·1 3·5 8·5 4·2 7·7	160 305 55 340	m/s 1·0 3·7 6·0 4·4 7·0	65 160 330 60 5	m/s 1·7 3·2 2·3 6·2 5·2	m/s 2·6 2·4 7·0 4·9 8·3	1 2 3 4 5
175 0 230 1 110 1	8·8 6·7 2·2 3·2 2·0	170 175 245 110 45	9·3 7·7 4·0 13·4 12·7		8·9 7·9 4·1 13·2 12·0	165 175 270 105 50	9·7 7·2 2·5 10·7 11·5	160 180 — 95 60	9·8 6·6 0·5 8·0 10·8	165 180 — 90 45	11·1 6·0 0·5 8·5 9·6	160 145 — 85 60	5·4 0·5 8·5 9·6	140 90	10·8 4·7 0·5 9·6 10·7	150 110 90 90 65	9·8 3·6 3·1 8·7 9·3	145 115 100 90 65	11·0 4·3 5·7 8·2 10·3	160 125 110 85 60	8·5 4·5 7·5 8·2 10·3	200 135 135 85 65	2·9 3·7 8·8 7·6 8·8	6·3 4·0 2·6 II·I 9·8	6 7 8 9 10
140 315 270	1·8 4·5 0·0 7·0 7·8	185 160 310 275 315	5·5 4·7 10·4 5·3 7·3	185 175 310 260 315	5·3 6·3 10·6 5·2 8·4	190 180 310 235 325	4·5 7·0 10·8 4·7 7·8	195 185 315 265 325	4·2 6·3 10·0 8·7 8·2	200 165 310 285 340	2·8 6·0 11·0 10·3 7·7	180 165 310 280 350	2·7 3·8 9·4 9·7 8·1	165 155 305 285 350	2·7 3·5 9·7 8·5 7·7	160 305 290 350	3·2 1·5 9·6 5·9 7·2	160 95 300 260 350	2·8 2·0 9·6 4·1 6·8	155 135 300 240 350	2·6 3·0 8·0 3·8 6·7	140 120 285 225 340	2·4 3·0 7·5 1·6 5·9	3·6 3·6 5·8 6·4 7·0	11 12 13 14 15
180 I. 310 145	3·5 2·8 3·2 8·6 7·7	315 185 350 130 40	3·2 12·5 3·9 8·2 7·2	315 185 355 125 40	3·0 11·8 3·5 8·0 7·0	285 180 320 135 40	2·8 11·6 3·2 9·6 7·7	230 180 310 135 50	2·6 11·8 3·5 8·5 6·5	220 185 325 130 40	4·2 12·5 3·0 7·5 7·2	210 185 355 85 40	4·5 12·8 1·7 6·2 5·8	185 180 320 90 35	4·8 13·2 1·8 5·7 5·0	175 180 — 85 35	5·9 13·3 1·3 7·7 6·8	185 180 — 100 50	5·9 12·0 1·1 6·5 7·4	165 185 135 75 55	5·7 12·0 1·6 6·0 8·0	160 190 75 65	7·3 10·7 1·1 6·2 7·3	3·7 11·3 2·4 6·3 6·5	16 17 18 19 20
335 190	0·6 8·3 6·5 6·8 9·5	35 35 330 180 260	10·0 8·5 7·4 8·5 10·4	35 40 335 180 260	10·3 9·0 7·7 9·3 10·8	35 40 355 185 255	10·8 9·0 7·9 10·0 10·6	35 35 5 190 255	10·5 8·7 8·0 10·2 10·9	40 35 15 190 250	9·4 9·0 8·5 10·4 10·7	35 35 10 190 255	7·8 7·3 7·7 11·5 10·1	30 40 25 185 250	6·8 5·5 5·6 11·8 10·3	20 20 35 195 245	7·5 4·5 5·8 12·3 10·4	30 20 45 200 260	9·0 5·2 5·5 13·7 10·2	35 20 50 215 285	7·7 5·6 5·3 13·1 8·7	40 40 45 235 305	8·3 6·4 4·0 11·2 8·2	8·7 6·6 5·6 6·6 9·4	21 22 23 24 25
270 260 185	9·2 5·0 5·4 6·9	330 275 265 215 220	9·0 4·7 3·6 6·1 10·3	310 275 275 275 215 225	7·5 4·3 3·5 6·6 9·7	310 270 275 230 225	7·0 3·8 4·0 7·9 7·8	315 280 275 235 225	5·9 3·5 4·0 9·6 8·0	325 275 275 275 235 220	5·3 3·8 3·3 9·8 7·3	325 275 285 240 220	5·1 2·8 2·7 9·3 6·7	340 285 290 235 205	4·0 2·8 1·6 8·4 6·0	340 285 — 235 195	2·5 4·2 0·5 8·8 6·0	350 250 — 230 200	3·3 3·0 0·5 7·9 6·0	25 190 — 225 200	2·4 2·7 1·0 8·2 6·0	340 280 — 225 200	1·7 3·2 1·5 9·0 6·0	7·8 2·3 3·5 5·1 9·2	26 27 28 29 30
	7.3	_	7.5	7.5 - 7.		_	7.5	_	7.3	_	7.3	-	6.7	_	6.3	_	6.3	_	6.3		6.0		5.4	6.0	
13.		1	4.	1	5.	1	6.	1	7.	1	8.	1	9.	2	o.	2	1.	2	2.	2	3.		24.	Mean	Day.

Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$): Speed in metres per second.

359. Cahirciveen (Valencia Observatory):

 H_a (height of anemograph above M.S.L.) = Height of ground above

Day.	I		2		3		4		5	.	6		7		8		9		10	0.	1	1.	No	on.
1 2 3 4 5	200 55 125 205 205	m/s. 6·1 1·6 4·1 4·0 5·9	195 — 145 205 205	m/s. 5·5 0·5 3·6 4·2 5·3	90 65 — 200 205	m/s. 5.5 1.8 1.1 4.3 5.2	90 40 205 195 220	m/s. 5·8 2·0 1·6 4·7 5·2	190 60 175 185 215	m/s. 5·9 2·4 2·0 4·3 4·7	195 60 185 195 190	m/s. 6·2 3·0 3·0 4·3 4·2	° 195 85 190 195 175	m/s. 5·7 3·3 2·1 4·7 4·0	200 85 210 210 190	m/s. 5·3 2·7 1·7 5·4 4·5	210 60 210 210 215	m/s. 5·9 1·9 2·2 6·1 5·5	210 65 225 215 215	m/s. 6·5 5·1 2·5 7·2 5·1	210 65 230 220 215	m/s. 6·5 4·2 2·5 7·7 5·5	210 85 230 225 215	m/s. 6·7 2·7 3·7 8·3 5·2
6 7 8 9 10	60 290 5	1·0 2·2 0·5 5·6 7·6	 60 305 5	0·5 2·0 0·5 7·0 7·1	55 320 360	0·5 2·5 1·2 6·3 5·2		0·5 2·5 1·7 6·4 6·3	55 - 330 320	1·2 2·5 1·0 7·0 5·0	50 330 325 340	0·5 2·5 2·7 7·5 6·8	40 355 325 335	0·5 2·0 2·3 7·6 6·8	330 30 335 325 345	2·5 3·5 3·3 7·7 5·8	335 30 15 325 315	4·4 4·2 4·5 8·7 6·7	335 355 355 340 295	5·9 3·7 4·7 8·7 5·9	335 340 345 320 290	6·2 4·2 5·7 9·3 7·2	340 345 335 320 290	6·3 4·6 6·6 9·5 7·9
11 12 13 14 15	335 360 10 325 295	8·5 8·0 3·3 5·9 6·9	335 10 10 280 300	9·3 6·2 2·6 6·2 7·9	340 5 10 305 290	7·8 6·5 2·3 5·9 6·6	345 5 290 290	9·3 6·8 1·3 7·5 7·5	350 355 300 270 295	9·3 6·6 3·0 8·9 6·9	345 355 290 255 310	9·5 6·0 6·9 8·5 6·6	340 345 300 250 310	9·7 6·3 4·3 11·1 6·6	350 325 300 250 305	9·5 6·6 6·6 10·2 6·9	340 360 315 255 315	9·7 5·0 6·6 9·5 6·9	330 320 300 260 320	10·3 5·9 11·8 7·5	335 290 305 250 320	10·1 4·7 5·9 12·5 7·2	335 270 335 255 330	10·5 7·3 7·2 12·1 7·2
16 17 18 19 20	305 305 300 315 230	8·2 4·3 6·2 4·6 7·2	300 305 320 315 230	8·5 4·9 4·3 5·2 6·9	305 330 305 315 230	9·8 8·2 4·6 5·2 6·2	325 355 295 300 230	10·2 6·9 3·9 5·6 6·9	325 355 310 295 230	9·8 5·6 3·6 5·6 6·9	330 355 315 285 240	9·8 6·2 4·9 5·6 8·5	320 355 315 285 255	9·9 5·9 5·9 8·2 5·9	335 355 315 290 265	10·2 6·2 6·6 5·6	340 345 330 285 290	5.9 6.2 7.2 5.9	335 340 330 285 285	10·2 4·9 7·5 6·6 4·6	330 320 330 275 285	9·2 4·6 6·6 7·2 5·6	335 300 330 270 285	8·9 4·9 7·2 8·5 5·2
21 22 23 24 25	3 ² 5 ² 75 300 35 305	3·9 4·3 4·9 3·6 9·8	325 275 315 35 325	3·6 4·6 7·2 3·3 9·2	310 270 340 35 325	4·3 6·2 9·2 2·0 8·5	305 260 350 — 335	4·3 5·6 7·5 0·7 9·5	305 260 15 — 335	4.9 6.2 7.5 1.3 8.9	300 250 20 — 335	3·9 5·6 7·9 o·3 10·5	290 250 20 — 335	3·3 3·9 8·9 0·0	290 250 20 — 340	5·2 6·6 10·5 0·7 11·5	290 245 25 350 350	5.6 8.2 10.5 3.6 10.8	275 240 25 320 345	5·6 10·2 7·9 4·6 10·8	275 245 30 300 345	5·6 8·9 8·5 3·9	270 240 25 295 335	6·6 8·9 7·5 4·9
26 27 28 29 30	360 30 355 60 30	10·8 5·6 2·0 4·9 6·2	355 30 10 65 40	9·8 5·2 4·3 4·3 6·2	360 30 45 65 50	8·9 4·3 4·3 2·0 5·9	5 25 30 — 45	7·9 3·9 4·9 0·7 4·9	5 15 45 — 45	8·5 4·9 2·6 0·7 4·9	5 10 — — 45	7.5 5.9 1.0 0.7 3.9	355 10 30 — 55	7·2 6·2 2·3 1·3 5·9	360 10 20 30 50	9·2 6·6 6·2 5·6 5·6	360 15 15 35 45	9·2 6·6 4·6 7·5 7·5	360 5 25 35 50	8·2 7·2 3·9 6·2 6·2	360 15 10 30 50	10·5 6·2 4·9 5·9 6·9	5 20 10 20 40	9·5 6·2 5·2 6·6 6·6
Mean	75 —	5.3	75 —	5.2	75 —	6·2 5·1	75 —	6·9 5·1		5·1	90	4·3 5·3	90	3.9	8 ₅	4·9 6·1	8 ₅	4·9 6·5	60	5·9 6·7	60	7·2 6·9	60	7·1

Note.—The values printed in italics are taken from the records of the Dines tube anemograph, the Robinson cup anemograph being out of action. The monthly means are computed from the hourly values as printed.

360. Cahirciveen (Valencia Observatory): $H_a = 12 \text{ metres} + 14 \text{ metres}$.

	0	m/s.	· ·	m/s.	0	m/s.		m/s.	0	m/s.	0	m/s.	°	m/s. 1	°	m/s.	٥	m/s.	0	m/s.	l °	m/s.	۰	m/s.
I	50	5.2	70	4.3	75	4.3	80	5.9	80	6.2	8o	3·3 1·6	75	4.9	55	6.2	55	6.6	55 265	7.5	55 290	7.2	55 340	3.6
3	_	0.7	_	1.0	_	0.7		1.0	_	0.3	55 —	0.3	320	0·7 4·9	345	4.6	320	2.6	330	3.3	350	7.2	350	9.2
4	360	7.2	355	8.5	350	8.9	345	9.5	345	10.2	5	6.9	20	7.2	25	6.6	20	9·5 6·6	20	7.9	20 350	7.2	10 350	7:2
5	5	5.6	350	5.6	355	5.6	355	5.6	350	6.9	350	7.5	350	7.2	350	7.2	350	0.0	350	0.9	350	/ 9	330	7.5
6	340	5.2	340	5.2	330	6.2	330	3.6	330	3.3	330	3.0	330	2.6	330	2.3	330	3.3	320 185	4.3	300 185	5.2	295	4·9 5·6
7 8	185	2·0 8·5	175	9.5	175	1.0	165	9.8	170 175	2.3	165 175	9.8	180 180	3·0 9·5	205 180	3.3	190	4.9	195	4·9 6·6	215	5.9	190 225	7.2
9	220	10.5	215	9.5	220	9.8	220	9.8	210	9.2	195	6.6	195	7.2	190	6.9	190	6.9	190	6.2	185	7.2	185	7.2
10	225	9.8	225	9.2	225	9.6	225	8.5	225	9.2	230	9.2	230	10.8	235	12.1	240	11.5	240	11.1	240	11.1	240	10.2
11	280	8.2	280	7.5	280	7.2	285	8.2	295	6.6	295	6.2	315	6.2	325	5.9	315	7.9	310	7.2	310	7.5	310	7.5
12	300	3.3	295	3.3	290	3·9 6·6	290	3.6	280	4·3 8·5	260	3.3	260 280	4·6 9·8	250 285	3.6	² 45 300	7.9	245 310	5·2 8·2	240 320	7.9	240 315	7·9 8·5
13 14	255 335	4.6	270 335	5·2 6·2	² 75 335	5.6	²⁷⁵	3.9	275 335	4.6	²⁷⁵ 335	3.9	335	4.9	335	4.3	335	4.6	335	5.9	330	5.2	325	4.9
15	265	2.0	270	3.0	270	2.6	270	1.6	270	3.6	270	4.9	265	5.2	265	5.9	265	7.9	280	9.8	285	12.1	295	8.9
16	345	7.2	345	7.5	350	6.6	360	5.6	360	5.2	350	5.6	345	4.3	345	4.6	345	5.9	350	6.2	340	7.5	335	8.5
17	355	3.9	355	4.6	350	3.9	340	4.6	360	3.6	360	4.3	350	4.6	345	4·3 5·6	345 310	3.3	340 310	3.9	335 310	3.9	320 310	3.3
18	275 350	3·6 7·5	275 360	3·9 5·6	²⁷⁵	4·3 5·2	285 355	4·3 5·2	295 360	3.9	305 360	4·9 5·2	310 360	3.6	310 360	3.9	355	4·9 5·9	345	4.9 6.2	330	7.5	330	7.9
20	360	5.9	355	6.2	5	5.6	5	5.3	5	5.6	5	6.6	10	4.6	10	4.6	360	4.9	335	6.6	330 .	7.2	325	8.2
21	300	2.0	_	0.3	_	0.3	300	2.0	300	2.6	285	2.0	285	1.6	280	2.3	280	1.6	300	3.0	300	1.6	300	3.9
22	- 1.3 -			1.3	10	2.0	360	3.3	355	2.3	325	4.3	320	5.6	320	4.9	320	3.0	310	3.6	275 300	5.9	280 300	3.3
23 24	_	1.0	315	3.3	310 320	4.6	295 —	3.6	295 320	3.3	295 320	3.6	295 320	3.6	295 —	3.0	295 320	3.0	300 315	3.3	315	4.3	315	5.6
25	335	3.3	335	2.6	335	3.3	335	2.6	335	3.0	335	4.3	335	2.6	335	2.6	335	3.9	335	4.3	335	5.2	335	6.6
26	335	5.6	335	5.6	335	4.6	335	4.3	335	5.9	335	7.9	335	7.5	335	7.9	335	7.9	335	7.5	340	7.9	345	7.2
27	360	2.3		1.3	360	2.0	360	2.0		1.0	360	2.0	355	3.0	350	4.6	345	4.6	340	4.6	330	5.6	330	7.9
28 29	50	3.0	50	2.6	_	0.7		0.3	_	0.3	_	0.7		0.3	315	3.6	70 320	3.6	320	3.9	65 320	2·0 5·2	5 320	3.3
30		0.0	5	1.6	5	3.0	355	2.3	_	1.3		0.7		0.3		1.3	_	1.3	285	3.9	280	3.9	280	3.6
Mean	_	4.2	_	4.3	_	4.4		4.3	_	4.4	_	4.4		4.6		4.8		5.0		5.2	_	6.0	_	6.4
G.M.T.	1	.	2	.	3		4	.	5		6		7	·.	8		g).	I	о.	I	1.	No	on.

Averages for periods of sixty minutes centered at the exact hours, Greenwich Mean Time.

M.S.L. $+ h_{\alpha}$ (height of anemograph above ground) = 12 metres + 14 metres.

May, 1923.

ı	3.	r	4.	1	5.	I	6.	ı	7.	1	:8.	1	9.	2	ю.	2	I.	2	2.	2	3.	2	24.	Mean	Day.
225 65 225 215 230	m/s. 7.0 2.8 4.3 8.7 5.5	225 70 230 210 235	m/s. 6·4 3·7 4·3 8·2 5·7	225 85 225 210 235	m/s. 5·3 4·3 4·0 8·0 5·3	230 60 225 205 230	m/s. 4·2 5·0 3·8 7·2 5·4	225 75 230 205 235	m/s. 4·I 4·2 3·4 6·8 4·9	200 105 215 205 235	m/s. 3·2 4·1 3·1 6·0 4·4	90 225 200 220	m/s. 3·7 4·0 3·3 5·7 4·2	90 235 210 230	m/s. 1·5 4·2 3·3 5·8 2·8	95 235 200 225	m/s. 0·5 3·6 3·7 5·3 2·7	100 225 200 225	m/s. 0·5 1·9 2·8 5·5 2·3	° — 210 205 240	m/s. 0·5 1·5 2·5 6·0 2·3	0 — 125 200 210	m/s. 1·1 4·3 3·2 6·0 0·5	m/s. 4·7 3·1 3·0 6·0 4·5	1 2 3 4 5
350 325 340 325 290	5·5 6·0 7·0 10·5 8·4	340 330 335 335 275	5·8 6·4 6·8 10·9 9·3	345 330 335 340 275	6·7 6·6 7·1 11·0 9·5	340 325 335 355 270	6·3 6·6 7·3 12·3 10·7	350 325 340 355 265	6·3 6·2 7·2 12·0 11·2	355 320 340 355 270	6·8 5·4 7·3 11·9 10·0	355 330 345 355 285	5·8 4·2 6·6 11·7 10·7		4·5 3·0 5·2 10·8 10·9	10 350 10 280	5·7 1·4 2·3 9·7 10·9	15 5 280	5·1 0·5 1·4 8·5 11·5	40 — 295 360 325	2·8 0·5 4·7 8·5 8·3	60 — 300 360 320	2·5 0·5 4·9 7·9 7·2	3·9 3·5 4·2 4·8 8·2	6 7 8 9
335 280 320 250 340	9·6 7·1 8·2 13·1 7·9	340 295 320 250 335	10·0 6·1 8·9 13·8 8·9	340 285 310 245 330	10·9 5·5 10·5 13·4 10·2	340 265 330 255 335	11.8 5.5 10.2 12.5 9.5	340 290 330 270 340	11·7 5·4 11·5 9·8 8·2	345 285 340 290 345	11·7 4·0 8·2 6·6 11·5	350 265 340 300 345	10·4 4·7 8·5 5·9 10·2	350 310 350 295 350	11·0 4·7 9·5 5·6 9·8	350 325 345 305 350	9·4 5·4 9·5 5·2 9·8	360 350 330 305 340	8·9 4·6 7·5 4·9 9·2	360 5 325 295 345	7·7 3·5 6·6 6·6 7·9	360 10 345 290 330	7·5 2·8 6·9 7·9 7·9	9·7 5·7 6·7 9·0 8·2	11 12 13 14 15
330 290 325 270 295	8·2 3·9 5·2 7·5 6·2	310 280 315 270 310	7·2 3·9 6·6 7·9 4·6	305 280 310 265 305	7.5 3.9 6.2 7.5 5.2	310 275 315 260 300	5·9 4·6 6·6 7·5 5·6	310 265 325 260 300	5·6 4·9 6·2 7·5 5·2	315 265 320 260 305	6·2 5·2 5·9 7·2 4·6	325 260 315 260 310	6·2 4·6 6·6 7·2 4·9	325 280 315 260 310	6·9 5·6 4·9 8·9 5·6	335 290 310 260 310	4.6 5.2 5.9 7.9 3.9	330 295 305 245 310	4·9 4·6 3·9 6·2 4·3	325 295 315 240 315	6·2 5·6 4·3 5·6 4·6	320 295 315 230 325	4·3 5·6 4·3 6·6 3·3	7·9 5·3 5·6 6·8 5·6	16 17 18 19 20
265 235 5 280 335	5·9 8·5 8·2 5·2 12·8	260 235 5 280 335	6·6 8·9 8·5 5·6 12·8	250 240 5 275 335	7·9 8·2 8·9 5·6 13·4	245 240 30 280 335	4.9 8.2 8.2 7.2 13.8	240 240 30 275 340	6·6 6·9 7·5 7·5 13·4	245 240 15 270 335	9·5 5·6 7·5 7·2 14·1	260 245 20 270 340	7·9 6·2 7·2 8·2 13·4	280 305 10 270 350	7·5 4·6 6·9 7·9 10·5	285 305 10 270 345	8·5 3·0 5·9 8·2 10·2	285 295 20 280 350	6·6 4·3 5·9 7·9	280 295 30 280 355	4.9 2.6 3.9 10.8 9.5	275 300 35 285 5	5·2 4·9 4·6 10·8	5·7 6·3 7·6 4·9	2I 22 23 24 25
5 10 5 40	11·8 6·9 6·9 8·2 7·5	355 360 10 360 50	10·8 6·6 6·9 7·5 7·2	360 10 25 350 50	10·5 6·6 5·9 7·9 6·2	5 15 15 345 50	9·2 6·6 6·9 8·9 5·2	10 360 10 345 50	10·8 6·9 10·2 8·9 5·2	15 350 360 360 50	8·9 6·2 9·5 10·5 5·6	15 360 5 5 55	7·5 3·0 7·9 9·2 4·9	15 355 20 15 60	4·9 4·3 6·9 8·5 5·2	5 355 40 25 60	4·6 2·3 3·9 7·2 4·3	20 50 25 60	4·6 1·0 2·0 5·2 2·6	25 — — 45 60	5·2 1·0 1·3 8·2 2·6	25 — 55 40 60	4·9 0·7 3·0 7·2 5·6	8·5 5·1 4·8 5·9 5·6	26 27 28 29 30
55	6·6 7·5	45 —	6·9 7·5	30	7·7	15 —	7.6	5 —	8·5 7·6	10	9·8 7·5	10	7·2 6·8	15 —	5·9 6·4	30 —	5.7	40 —	3·6 5·0	45 —	3·9 4·8	45 —	5·1	6.1	31

Note.—The values printed in italics are taken from the records of the Dines tube anemograph, the Robinson cup anemograph being out of action. The monthly means are computed from the hourly values as printed.

																							Ju	ne, 19	923.
,	1 m/c 1		m/s.		m/s.	0	m/s.	· ·	m/s.	0	m/s.		m/s.	1 0	m/s.	0	m/s.	, ,	m/s.	•	m/s.	·	m/s.] m/s.	1
45	m/s.	45	6.6	45	5.2	50	4.9	50	4.3	50	4.6	55	4.3	60	2.6	80	2.3	90	3.6	90	3.3	90	1.6	4.9	I
295	3.6	295	2.6	300	2.0	300	5.2	310	6.6	325	7.2	345	4.3	350	3.6	_	1.3	-	1.0	_	0.7		1.0	2.3	2
340	8.5	330	9.2	340	10.5	345	9.2	345	8.9	345	8.2	350	2.9	10	4.3	5	5.2	360	7.9	360	7.5	360	6.6	5.3	3
5	5.9	10	6.2	20	5.9	10	8.5	15	8.5	15	9.2	15	6.9	15	6·9 6·2	10	3.0	10	4.3	10 340	2.3	10 340	4.3	7·1	4 5
350	7.5	350	8.2	350	7.9	350	7.2	340	8.5	340	8.5	340	6.2	340	0.2	340	0.2	340	5.9	340	5.2	340	1		
295	4.9	280	4.6	275	5.2	275	5.6	270	4.6	270	4.3	270	3.3	270	3.3	230	2.0	235	2.3		1.0		1.3	3.9	6
185	5.6	180	7.2	175	7.2	175	7.2	185	6.6	180	7.2	270 180	7.5	180	8.2	180	7.2	175	8.5	175	9.2	175	9.8	5.2	7 8
225	7.2	225	8.5	225	7.2	225	7.2	220	6.9	200	5.2	200	5.5	195	5.3	195	5.6	190	6.2	185	5·9 8·9	190 220	7.5	7·8 8·7	9
185	8.2	185	8.2	190	9.2	185 245	8.9	185 250	9.2	185 260	9.5	195 260	9·5 7·5	220 260	9·8 7·9	220 265	8·9 7·5	220 270	8·5 7·5	220 280	7.9	280	8.2	9.6	10
240	11.5	240	11.2	250	9.0	445	10.2	250	9.2	200	0.2	200	1.2	200	7.9	203	/ 3	~/0	1 3	200	19				
310	8.2	310	7.5	305	7.2	310	6.6	310	6.9	315	5.2	315	4.6	315	4.6	315	3.0	315	3.9	300	3.6	300	4.3	6.4	11
245	9.2	245	9.5	250	8.2	250	7.9	250	5.9	250	4.3	245	4.9	250	4.9	250	4.6	250	4.3	250	4.3	250	3.9	5.3	12
325	6.9	320	7.2	320	6.6	330	7.2	335 280	7.5	335	8.2	335	7.5	335 280	7.9	335	5.6	335	3.9	335 265	3.9	335 265	4.9	3.9	13 14
305	4·9 7·2	300	6.2	310	3.9	300	3.3	315	4·3 8·9	280 315	3·o	320	8.9	340	7.5	340	7.9	340	6.6	335	6.9	345	7.9	6.4	15
310	/ 2	310	" -	3.5	" -	3.3	1 ' 3	3,3	0 9	313	1 3] ~~	0 9	340	1 3	340	' "	34.		333		0.0		1 . 1	
325	8.2	330	8.5	330	7.9	330	7.5	330	7.9	330	7.2	335	6.9	350	6.9	345	6.6	345	5.2	345	6.2	355	5.6	6.7	16
285	4.3	275	4.6	275	3.3	275	3.0	275	3.3	² 75	1.6		0.7	275	3.3	275	3.3	275	3.3	275	6.9	275	2.3	3.5	17
305	3.9	305	3.9	310 320	3.6	290 320	4.3	280	3.9	280	3.6	280	9.8	280	3.3	300	3.6	320 340	6.6	330 360	5.9	330 360	7·9 5·6	4·4 6·7	19
330 330	7.5	325 330	8.5	325	6.9	325	8.2	325 325	6.9	335 320	4.6	340 305	4.6	340 300	3.6	340 300	2.0	340	0.7		1.0		1.3	5.4	20
330	' 3	330				3 3		1 3-3		320	7 "	3-3	т *	J	, ,	3		l	,						
300	3.9	305	3.3	310	4.6	310	5.2	310	5.9	310	5.2	325	5.2	330	3.9	330	2.6	l —	1.3	330	3.3	330	3.0	2.9	2I 22
295	4.9	305	5.6	305	4.9	305	4.6	305	4.6	305	3.6	305	3.0	310	3.6	315	3.0	315	1.6	-	0.7		0.3	3.2	23
300	4.3	315 320	3.6	320 330	3.9	320 335	5·2 6·2	320 335	5.2	320	3.6	320	2.6	320	2.3	320	3.3	320 335	3.3	335	3.3	335	3.3	3.3	24
315	5·2 7·5	335	6.0	335	6.2	335	7.2	335	4·3	335 335	4·9 6·9	335 335	3.9	335 335	3·9 5·6	335 335	5.2	335	4.9	335	4.6	335	4.9	4.8	25
333		333		555			'	000		333		333		333		333		333	' -	000				li	-6
345	8.2	340	7.9	340	7.5	340	5.9	350	6.9	340	7.9	340	7.9	340	4.3	350	3.9	350	3.3	355	3.3	360	4.3	6.3	26
330	6.2	335	5.9	335	6.6	330 315	7.5	335	7.9	335	6.2	335	5.6	335	4.6	335	4.9	335	4.6	340	3.9	40	2.3	4.2 1.9	27 28
360 320	3.0	360 320	3.9	320 320	3.3	310	3.3	315 280	3.3	315 285	3.6	315 320	3.3	315 325	2·0 4·6	325	3.9	325	3.9	340	3.0	5	2.3	2.9	29
280	3.9	280	3.9	285	3.9	305	5.2	320	4.9	330	5.2	330	5·2 5·6	330	4.3	330	3.0	330	2.6	330	2.6	340	2.6	2.9	30
ļ			6.4		6.0		6.3		6.4										4.2		4.0		4.2	5·I	
-	6.3	_	0.4		0.0		0.3		0.4	_	5.9	-	5.4	_	5.0	_	4.3		4.3	_	3.0		" ~	,	
	1	14. 15. 16.							, 1	1	. 1			_	<u> </u>		_		_		,	2	4.	Mean	Day.
13	·	14	1 .		"	10	٠.	I	'·	1	o.	I). 	2	^{9.}	2	I.	2	2.	2	3.		4.		,
																									II 2

Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$): Speed in metres per second.

361. Cahirciveen (Valencia Observatory):

Ha (height of anemograph above M.S.L.) = Height of ground above

Day.	1.		2		3		4		5	i.	6		7		8		9		10). 	11	ι.	No	on.
	0	m/s.	0	m/s.	0	m/s.	0	m/s.	i °	m/s.	•	m/s.	U	m/s.	0	m/s.	Ö	m/s.	0	m/s.	٥	m/s.	0	m/s
r		1.3		1.0		1.3		0.7	-	0.0		0.0		0.0	_	0.3	-	0.7	÷	1.0	_	0.3	_	1.3
2	195	2.0	200	3.3	205	3.0	210	3.9	210	3.3	210	3.3	210	3.6	205	3.3	200	4.3	195	4.3	200	4'9	200	4.0
3	210	6.2	220	7.2	220	7.5	220	7.5	225	6.6	225	5.6	225	3.3	230	4.3	245	4.3	270	3.0	270 190	2.3	270 190	3.6
4	190	2.6	190	1.6	190	1.6	190	1.6	190	2.0	190	2·0 1·6	190	2.6	185	3.6	190 165	1·6 5·9	190 175	5.2	175	6.6	160	6.2
5	_	0.0	_	0.3		0.0	-	0.3		1.3	240	1.0		0.7	105	3.0	105	39	1/3	3 2	1/3		100	"
6	125	2.3	110	3.0	110	3.0	_	1.0	110	2.3	—	1.0	_	0.7		1.0		1.3	230	2.6	290	2.3	285	3.0
7	180	3.9	150	3.6	135	2.6	150	4.3	135	3.6	140	6.2	150	4.6	155	5.2	165	4.6	175	4.9	175	5.6	175	5.0
8	195	3.3	190	3.3	185	4.6	180	3.9	180	4.3	165	4.9	160	5.2	155	6.6	150	8.5	145	8.2	160	8.5	155	8.6
9	175	5.6	175	5.6	170	6.2	175	6.6	175	6.6	175	6.9	175	6.2	170	6.2	165	6.9	175	7·2 3·6	170 165	5.6	175 170	4:3
10	150	4.3	145	4.9	145	4.3	125	3.3	110	4.6	115	4.3	110	4.6	125	4.6	140	3.9	150	3.0	105	3.9	1 , ,	4
11	_	0.7		1.0		1.3	_	1.0	360	1.6	l	1.0	_	0.3		0.7	320	1.6	300	3.0	285	3.3	280	4.6
12	15	2.0		0.7	15	2.0		1.3	_	1.3	 —	0.7		1.3	10	2.3	340	3.9	325	5.2	325	4.3	335	4.6
13	55	1.6	55	3.0	30	3.9	60	2.3	45	3.0	55	5.2	30	5.2	40	5.2	55	7.2	40	6.2	25	6.2	30	5.6
14		0.7	<u> </u>	0.3		1.0	_	1.3		1.3		1.0		0.3	25	2.0	50	2.0	350	6.6	345	7.2	335	6.6
15		1.3	180	2.0	170	3.0	170	3.0	170	3.3	170	4.9	170	4.6	170	5.2	170	5.9	170	5.6	175	3.3	220	3.3
16	275	5.9	290	3.6	270	4.9	270	5.2	255	3.9	245	3.6	245	5.2	245	6.9	245	5.9	235	6.9	235	8.2	240	7:5
17	245	5.6	240	4.3	235	4.9	235	3.9	255	4.3	240	4.3	245	5.6	245	4.9	245	5.6	245	6.6	240	7.2	240	6.2
18	285	2.0	290	2.3	290	2.0	290	3.6	290	3.6	290	4.3	290	2.6	290	2.6	290	4.9	280	5.6	275	5.9	280	5.3
19	250	3.0	245	3.0	240	3.3	240	5.2	190	4.6	180	4.6	185	3.6	230	5.2	240	5.2	250	5.2	255	5.2	255	5
20	220	3.3	240	3.9	250	4.9	250	3.9	250	4.6	250	3.3	250	3.3	250	3.9	250	5.6	235	4.9	235	5.2	235	5
21	220	4.6	220	4.3	220	3.6	220	3.9	220	3.6	230	4.3	230	3.6	230	4.9	230	4.6	230	5.2	235	4.9	235	5.6
22	225	4.9	230	4.9	230	3.9	230	3.3	230	3.0	225	4.9	220	5.2	220	4.9	220	5.9	220	6.2	225	6.9	215	5.0
23	210	7.2	210	7.2	220	8.5	220	8.9	225	6.9	230	9.5	240	9.8	240	10.5	240	9.5	240	9.5	240	6.9	240	5
24		0.3	_	0.7		0.7		I.0	_	0.7		0.7		1.0	130	1.6	150	3.3	160	4.6	165	3.9	190 285	3:
25	200	3.9	215	4.9	235	7.5	240	2.9	245	4.3	275	5.2	280	3.3	280	4.6	280	3.6	300	5.9	285	7.2	205	7.
26	290	7.9	295	6.6	290	8.5	295	5.9	300	6.2	300	6.2	300	4.9	295	5.9	295	5.9	295	7.9	300	6.6	300	5.
27	195	2.3	195	2.3	185	3.0	175	4.9	170	5.9	160	7.2	205	5.9	240	5.2	230	5.2	225	5.6	225	5.6	225	2.
28	240	6.6	255	3.9	255	4.6	250	6.2	260	4.6	265	5.6	275	5.9	275	4.9	265	7.2	270	6.6	275	6.9	265	6.
29	250	3.9	255	5.6	260	6.6	270	5.6	280	3.3	260	5.2	255	3.3	255	4.3	250	3.6	230	4.6	210	3.6	190	8.
30	245	4.9	240	6.6	240	8.2	240	5.5	240	3.9	240	4.9	240	3.3	210	3.6	200	3.9	195	3.9	175	5.2	215	"
31	240	3.9	235	2.6	210	3.0	210	2.3	205	2.6	200	2.6	215	3.3	190	3.3	255	5.2	265	3.0	260	7.5	245	7.
Mean		3.2		3.2		4.0		3.8		3.6		4.0		3.8		4.2	_	4.8		5.2		5.3	_	5.

362. Cahirciveen (Valencia Observatory): $H_a = 12 \text{ metres} + 14 \text{ metres}$.

1	285	m/s.		m/s.		m/s.		m/s.		m/s.		m/s.		m/s.		m/s.		m/s.		m/s.		m/s.		
1		4.6	285	4.6	285	5.2	285	4.3	280	3.3	275	3.0	275	3.0	275	2.3	270	2.6	250	3.3	240	5.2	240	4.9
	- 1	12.5	120	11.8	120	14.8	135	15.1	140	15.1	150	15.4	155	13.1	165	10·8	180	8.2		12.8	240	20.0	240	21.3
3 2	245	8.2	245	7.9	245	8.2	245	7.5	250	7.2	250	5.9	250	7.2	250	6.9	245	7.9	245	8.9	240	8.9	245	8.5
_	145	4.9	145	5.9	155	5.9	150	7.2	150	5.2	150	6.2	150	7.5	155	9.5	150	9.5	145	8.9	150 205	5.2	150 210	6.6
5	150	8.5	160	7.9	175	7.9	180	5.2	180	4.9	185	4.3	190	3.6	195	4.3	205	4.9	205	0.2	205	3 2	210	0.0
6	180	6.6	180	6.6	180	6.6	180	7.2	180	7.5	180	7.2	180	8.2	180	7.2	180	7.5	185	6.2	190	5.9	185	6.9
1 1	175	7.9	175	7.9	175	7.5	180	7.5	185	5.6	195	4.6	225	5.2	235	5.2	280	4.6	285	4.3	285	3.0	280	3.6
	165	5.6	170	5.9	170	5.9	170	7.2	165	8.9	170	8.2	170	7.9	170	8.2	170	9.5	165	9.5	170	9.5	170	9.5
9	_	0.7	<u> </u>	0.3	<u></u>	1.0	245	3.3	245	3.3	245	2.0	245	2.3	245	3.6	245	2.6	215	3.3	225	5.6	225	4.9
10	240	3.6	240	3.6	240	2.3		1.3		0.7	_	0.7	—	0.3		0.3	255	2.0	290	2.0	295	2.0	295	2.6
1		[6		0.0	4.5	2.2		2.3		0.7	105	2.0	155	3.3	165	4.6	170	4.6
1	T	1.3	45	1.6	7.50	5.6	45 160	1·6 5·9	45 165	5.9	45 170	6.2	45 175	5.9	175	6.6	165	6.9	160	7.2	170	7.5	160	5.6
	145 180	7·5 4·3	140	3.6	150 210	3.6	215	2.0		1.3	215	2.0	1/3	1.3	-/3	1.0	_	0.3		0.0	220	1.6	240	3.6
· 1	315	2.0		0.7		0.7	315	1.6	315	2.3	315	1.6		0.7	360	3.0	360	3.0	355	2.6	345	3.0	340	4.9
, ,	330	3.9	320	4.3	310	5.2	310	5.6	320	4.3	325	3.9	310	4.9	330	5.9	330	5.2	310	5.9	310	6.2	315	5.6
															1		0.70	7.6	240	2.2	225	E.2	220	F:0
1	290	3.0	290	2.0	l —	1.3	285	3.3	255	4.6	250	3.0	270	4·6 8·9	245	8.9	270 245	9.5	240 245	3.3	225 245	5·2 9·8	230 240	5.9
à 1	215	9.5	240	9.5	240	8.9	240	5·9 8·9	240 265	5·6 10·2	240 270	8·5 7·9	245 270	9.8	245 270	8.2	275	10.5		10.8	285	9.8	285	9.5
	245 280	8·5 5·2	255	10.2	270	7.9	250 275	4.9	275	4.6	275	4.3	275	3.9	275	3.3	265	4.6	255	4.3	255	4.3	245	5.6
- 1	250	4.6	275 250	4.9	275 250	4·9 5·6	250	5.2	260	6.6	280	5.6	315	4.3	320	3.3		i · 3	310	1.6	200	2.3	175	4.6
	-3-	·	-3-	' -	-3-		3.	Ĭ																0 -
21 2	240	10.2	280	10.3	300	8.2	290	8.9	285	9.2	285	9.2	285	8.2	280	7.9	275	7.9	260	7.2	250	8.5	240	8.5
		10.5	255	10.2	260	9.8	260	9.2	265	9.2	270	9.2	265	8.5	265	9.2	260	9·5 8·2	255	9.5	265 215	6.3	260 220	9.2
~ 1	180	4.3	180	4.6	165	5.6	150	8.9	155	9.8	150	12.1		13.8	160	13.1	190	12.2	220 330	11.1	330	12.5	330	11.1
24 25	5	3.3	330	3.6	315 180	4.6	320	6·9 5·2	325 170	9·5 6·9	325 170	7.5	330 170	9.2	335 175	8.2	335 180	8.2	180	7.9	180	8.9	190	7.2
²³ 1	175	3.6	175	3.9	100	3.9	175	3 2	1,0	0 9	1/0	/ 3	1,0	9-	-73		100			, -				1
26	225	6.2	220	7.2	225	6.2	220	6.9	220	8.2	225	7.5	220	7.2	220	8.5	220	8.2		10.2		10.5	225	10.2
27 2		11.8		11.5		11.8	245	12.5		12.5	245	13.8		13.1		13.8	250	14.1		14.4		15.4	245	13.1
28 2	, ,	10.5	270	10.2	275	10.2	270	9.8	265	9.5	265	9.2	270	8.9	265	8.9	270	8.2	275	7.2	265	6.9	260	7°5
	80	5.2	90	5.2	80	6.9	70	7.5	55	8.9		14.1		14.8	35	14.8		15.7	10 265	9·8	5 260	15·1 9·5	260	9.2
30 2	275	10.2	270	10.5	275	10.2	270	10.2	265	10.5	260	11.1	275	10.8	270	9.5	275	11.1	4 05	9.0	200	9.5	200] -
31 2	285	5.6	295	6.2	280	6.2	285	6.6	300	4.9		1 · O		1.3	330	4.6	300	4.3	310	6.2	300	5.9	290	5.6
Mean	_	6.3		6.2		6.2	_	6.5		6.7	_	6.7		6.9		6.8	_	6.8		7.0		7.7	-	7.9
<u> </u>						<u> </u>		<u>'</u>		<u>'</u>	!					 i		<u>'</u>					No	on
G.M.T.	I.	ı	2.	.	3.	.	4		5.	. [6.		7	.	8	.	9	.	10	э.	13	1.	140	on.
		1		i		1		1																

Averages for periods of sixty minutes centered at the exact hours, Greenwich Mean Time.

 $M.S.L. + h_{\alpha}$ (height of anemograph above ground) = 12 metres + 14 metres.

July, 1923.

13	3.	14	.	15	.	10	5.	17	7.	18	3.	ıç).	20).	2	1.	2:	г.	23	3.	2.	4.	Mean	Day.
0	m/s.	0	m/s.	0	m/s.	0	m/s.	1 0	m/s.	ı °	m/s.	0	m/s.	i °	m/s.	°	m/s.	, ,	m/s.	i °	m/s.	0	m/s.	m/s.	í
335	2.0	255	2.3	245	3.3	230	3.3	230	3.6	220	3.6	215	3.3	215	2.6	215	2.6	200	3.9	195	2.6	195	2.6	1.8	r
200	6.2	195	5.6	195	5.6	195	6.2	195	5.2	190	5.6	200	4.9	190	5.6	190	4.6	190	5.2	190	5.6	200	5.2	4.5	2
265	3.9	265	3.6	245	3.6	240	4.3	240	3.6	240	3.9	240	3.0	240	2.0		1.0	—	1.3	220	2.0	190	1.6	4·I	3
210	3.0	220	2.6	220	1.6	220	2.3	220	2.6	235	2.0	240	1.6		1.0		1.0	T.45	2.0	7.45	0.3	T25	0.3	1.7	4
165	6.6	165	6.2	155	5.6	165	6.6	155	6.9	160	4.9	155	4.6	155	4.3	135	3.6	145	2.0	145	2.0	135	3.0	3.6	5
275	3.9	265	3.3	265	3.9	250	3.3	180	4.3	165	3.9	175	4.6	175	6.6	175	6.2	170	5.6	160	3.3	160	2.6	3.1	6
175	6.9	175	6.6	185	4.9	205	4.6	200	4.3	205	4.3	205	3.3	205	2.6	205	3.0	205	3.3	205	2.3	205	3.0	4.3	7
155	8.9	160	8.5	155	7.5	175	5.9	175	5.9	180	5.6	180	6.2	180	6.9	180	7.2	180	6.6	180	5.9	175	6.2	6.2	8
175	7.2	175	6.6	175	6.9	175	5.9	175	5.9	175	5.6	170	4.9	160	3.9	160	4.3	160	3.3	160	3.6	160	3.6	5.8	9
170	4.3	175	3.6	175	4.3	180	2.3	255	2.6	310	3.6	315	3.3	_	0.7	_	0.7	_	0.7	_	0.3	-	0.7	3.3	10
275	4.6	275	3.6	275	3.6	275	3.9	275	2.3	275	1.6	275	2.0	275	3.0	275	1.6		0.7		0.3	275	1.6	2.0	11
335	6.9	335	7.9	335	8.2	335	8.5	340	7.5	355	6.9	350	4.9	20	4.9	20	5.2	35	4.9	20	4.6	45	2.3	4.3	12
35	6.2	30	5.9	40	5.6	15	6.2	35	6.6	25	5.2	10	6.6	15	4.9	45	2.0		i · 3		o.3		1.3	4.5	13
330	7.9	330	5.9	325	5.9	320	5.2	320	4.6	315	5.6	315	5.2	315	3.9	315	2.3	l	0.7	255	1.6	210	1.6	3.4	14
240	5.2	245	3.6	245	3.9	250	5.2	270	5.9	285	6.2	290	3.6	285	3.3	280	3.0	275	3.3	260	3.9	260	3.0	3.9	15
240	9.8	240	8.5	240	8.9	240	8.5	240	9.2	240	8.5	255	6.2	250	5.9	250	5.9	245	5.2	250	5.2	250	4.3	6.4	16
245	6.6	265	6.6	270	6.6	265	7.2	265	7.2	280	8.5	285	7.2	290	5.2	290	3.6	265	5.9	265	3.9	280	3.6	5.7	17
255	7.9	265	6.2	265	5.6	265	5.2	265	5.9	265	5.2	265	4.3	265	4.3	265	3.9	265	3.3	260	3.0	255	2.6	4.3	18
255	4.6	255	4.9	255	4.3	255	3.9	255	3.0	255	4.6	255	4.3	250	4.6	245	4.9	245	3.3	245	3.3	240	3.0	4.3	19
235	5.6	220	3.9	215	4.6	220	5.6	230	5.9	230	5.2	230	3.6	210	3.9	210	4.3	205	4.9	210	4.9	215	5.2	4.2	20
235	6.2	235	5.2	240	6.2	240	5.6	240	6.6	240	5.6	240	4.3	240	3.6	235	3.6	230	3.9	230	3.3	225	3.3	4.6	21
220	5.6	220	6.9	220	5.9	220	5.9	215	5.6	215	6.2	210	5.6	200	4.6	200	3.9	195	4.9	215	4.9	215	5.9	5.2	22
260	4.3	295	4.9	305	5.2	305	3.9	305	3.9	305	3.6	305	3.6	305	2.6	305	1.6	_	0.7		0.7		1.0	5.7	23
230	5.2	240	5.9	245	5.9	245	6.9	250	5.2	250	4.6	250	4.9	250	5.2	250	4.9	250	4.9	245	3.3	220	3.3	3.3	24
280	6.6	275	7.2	285	6.9	280	8.5	285	8.9	290	8.2	300	6.9	305	5.6	290	7.5	295	6.6	295	7.2	290	6.9	6.2	25
300	6.6	310	5.6	295	5.2	305	4.6	290	4.3	300	4.3	310	2.3	310	2.6	310	2.0		0.3	_	0.7	200	1.6	5.0	26
225	5.6	225	5.9	220	5.9	225	6.9	225	7.5	225	7.2	225	6.9	220	5.6	250	4.9	245	2.3	240	2.6	230	3.9	5.1	27
270	6.6	270	6.6	270	6.2	260	5.6	260	4.6	260	4.9	285	2.6	285	2.3	<u> </u>	0.7	<u> </u>	1.0	245	3.9	245	2.6	4.9	28
180	5.2	170	5.9	220	6.6	250	6.9	260	5.9	265	6.2	260	6.9	265	6.6	270	6.2	270	4.6	250	6.2	245	5.6	5.2	29
225	7.9	225	10.2	235	12.8	240	13.1	240	11.8	255	9.2	250	7.9	250	8.5	260	7.5	270	6.2	255	4.9	250	5.2	7.0	30
250	7.9	260	6.6	280	6.2	285	7.5	280	7.9	285	7.9	285	7.5	280	8.2	280	6.9	280	5.6	300	3.9	300	4.9	5.3	31
_	6.0		5.7	_	5.7		5.8	_	5.7		5.4	_	4.7		4.4	_	3.8	_	3.4		3.2	-	3.3	4.2	

August, 1923.

																							~ug.	•	
-	m/s	0	m/s	١٠	m/s	٥	m/s	0	m/s	0 1	m/s	0 1	m/s	0	m/s	0	m/s	0	m/s	0	m/s	0	m/s	m/s	
235	6.2	225	5.6	225	5.6	220	4.9	205	4.3	200	3.6	190	3.6	160	3.9	140	4.6	130	5.2	140	6.2	120	8.5	4.4	I
250	22.6	_	20.3		17.4	250	15.4		13.1	- 1	12.5	250	11.2	٠ ١	10.8	245	9.2		10.8	245	8.9	245	7.9	13.8	2
250	7.2	250	6.2	255	5.6	255	5.2	255	3.3	255	3.3	255	2.3	_	1.3	250	1.6	185	3.3	180	3·0 8·5	155 145	3·6 8·9	5·9 8·7	3
150	10.8	155	10.8	160 215	5.6	155	6.2	145 210	10.2	150	9.8	150	10.2	145 200	10.8	145 200	3.6	200	3.6	140	4.3	185	5.6	5.5	5
215	5.9	215	5.9	215	3.0	215	0.2	210	5.9	220	5.9	215	4.6	200	4.3	200	3 0	200	3 "	190	4 3	100	,	, ,	
185	7.2	190	6.9	185	7.5	185	6.6	180	6.2	180	6.6	180	6.9	180	6.9	180	6.9	180	7.2	180	6.6	180	7.2	6.9	6
280	2.3	280	2.6	280	2.3	280	1.6		1.3		0.7		0.7		0.3	215	1.6		1.0	130	2.0	150	3.3	3.7	7 8
170	9.2	170	7.9	180	7.2	175	6.6	170	5.6	180	4.6	185	3.6	190	3.0	185	2.0	165	2.3		1.3	210	2.6	6.3	9
225	6.2	225	6.2	230	6.2	230	4.9	235	5.6	240	5.2	240	3.9	240	3.6	240	2.3	240	2.0	240	2.0	240	2.6	3.2	10
275	3.9	270	3.0	270	3.9	270	3.9	270	3.9	270	2.3	275	2.3	_	0.3		0.3		1.0	45	2 3	45			
180	3.3	185	5.2	170	5.6	160	5.9	165	5.2	155	5.2	140	4.6	130	5.6	130	6.6	150	7.5	155	7.2	150	8.2	3.9	11
160	7.5	165	7.2	170	7.5	165	7.2	165	5.9	165	5.6	165	3.9	165	4.3	165	3.9	165	3.9	165	5.2	170	4.9	6·1	12
250	3.9	250	2.3	280	2.6	310	4.9	310	5.2	315	3.6	315	3.6	315	2.6	315	2.3	-	1.3	315	2.0	315	2.6	2.6	13
330	5.9	325	6.6	330	6.2	330	6.2	330	5.9	330	5.6	330	4.6	330	4.3	330	4.3	330	4.3	330	3.3	330	3.9	3.6	14 15
305	7.2	305	6.6	310	5.6	310	5.6	305	5.2	300	4.3	295	4.9	295	4.3	290	3.9	300	3.3	300	3.3	295	3.6	5.0	-5
220	5.6	210	5.2	220	5.6	200	5.2	195	5.6	190	5.6	185	5.6	170	6.9	170	6.9	175	7.2	190	7.9	195	8.5	4.7	16
240	10.5	240	9.5	245	9.2	250	7.5	255	8.5	255	6.2	255	7.5	250	8.2	260	7.9	265	7.5	255	7.9	250	8.5	8.5	17
285	9.8	290	8.5	295	8.2	310	5.9	295	6.9	295	6.2	285	5.9	285	6.9	290	5.9	290	5.9	280	5.9	285	6.2	8∙1	18
245	5.2	240	4.3	235	4.9	220	3.3	200	3.9	185	5.2	180	5.9	175	6.9	175	5.2	220	3.9	230	4.3	240	4.9	4.7	19 20
165	5.9	165	8.5	175	7.9	185	7.5	190	7.5	190	8.2	195	8.2	185	9.8	185	10.8	180	11.1	180	9.8	185	10.2	6.4	20
240	9.2	240	7:5	250	5.9	275	3.9	275	7.5	255	7.0	255	9.8	260	0.5	255	8.9	255	9.2	255	9.2	255	9.5	8.4	21
255	8.9	240	9.5	240	9.2	250	7.5	275 250	7·5 8·5	255 245	7.9	255 240	5.6	240	9.5	²⁵⁵ ²³⁵	2.3	215	3.3	200	3.6	190	3.9	7.9	22
215	7.2	200	7.2	185	6.9	185	6.2	180	5.9	170	5.2	170	3.0	150	3.0	135	2.6	90	3.3	_	0.7	65	1.6	6.4	23
330	10.3	330	10.3	330	9.2	335	8.5	320	5.9	315	5.6	315	4.3	315	2.3	315	1.6	310	I · 6		1.0	230	1.6	7.3	24
195	8.5	210	9.2	220	8.5	220	7.2	220	6.2	220	5.2	220	5.2	220	6.6	220	6.6	220	6.9	220	7.5	220	8.2	6.8	25
235	11.5	240	10.8	250	10.2	245	10.5	245									1		8.9	250	9.5	250	10.5	8.9	26
260	12.1	270	11.5	280	11.8	280	12.8	245 280	13·1 9·5	250 280	9.2	250 280	8.5	250 280	10.2	245 285	9.5	245 275	10.2	275	10.2	275	11.5	12.5	27
265	7:5	260	5.6	260	6.6	260	5.6	250	4.3	250	3.3	250	1.6	220	2.3	175	2.6	155	3.0	130	3.9	110	3.9	6.7	28
350	14.4	335	14.8	330	15.1	320	14.8	320	12.5	320	11.1	320	10.8	315	10.5	300	9.2	290	10.8	285	10.2	290	11.1	11.7	29
260	10.2	265	10.2	255	9.8	260	11.1	260	10.5	270	7.9	270	8.9	275	8.2	285	7.9	290	6.2	280	7.2	275	5.6	9.6	30
280	7.5	280	7.5	310	7.5	320	7.0	225	6.6			l								200	1	305	4.3	5.5	31
200		200	1/3	1310	1 3	320	7.9	325	6.9	325	7.5	330	7.2	330	4.6	335	4.3	340	4.3	320	4.3	303	4 3		
-	8.2	-	7.9	_	7.6	-	7.1	-	6.8	— ·	6.3	-	5.8	-	5.7	-	5.4	-	5.5	-	5.2	-	6.0	6.6	-
	<u> </u>	<u> </u>	!	<u> </u>		<u> </u>		<u> </u>	<u> </u>	1	<u> </u>	<u> </u>	<u> </u>	!	<u> </u>	!	1	 		 	1	1-	!	`	ì
1	3.	r	4.	ľ	5.	1	6.	1	7.	l 1	8.	,	9.		20.		21.	1 2	22.	1 :	23.		24.	Mean	Day.
	-	<u> </u>		<u> </u>			72	<u></u>	·	-	- *		<i>J</i> .	1		'								<u> </u>	<u> </u>

Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$): Speed in metres per second.

363. Cahirciveen (Valencia Observatory):

Ha (height of anemograph above M.S.L.) = Height of ground above

Day.	1	.	2	.	3		. 4		5		6	.	7		8	.	ç		1	o.	1	r.	No	on.
	0 1	m/s.	0	m/s.	0	m/s.	0	m/s.	٥	m/s.	0	m/s.	0	m/s.	0	m/s.	۰	m/s.	۰	m/s.	0	m/s.	0	m/s.
1	305	3.9	330	3.0	330	3.9	330	4.3	330	4.3	330	3.6	335	4.3	355	1.6	355	2.0	340	4.9	345	4.6	330	5.6
2		0.3	-	0.3	-	0.7	33	0.7		1.0		1.0	_	i.3		0.7		0.3	<u> </u>	i.3	320	2.3	280	3.0
3	180	3.6	180	3.6	180	2.6	180	3.6	180	3.6	180	3.9	175	6.2	170	5.6	170	6.9	170	5.9	170	7.9	170	7.5
4	325	4.9	320	6.6	330	6.9	360	3.3	360	3.9	360	3.6	360	2.6	350	2.6	310	4.3	295	4.3	285	4.3	275	5.2
5	245	6.6	245	6.9	250	7.9	250	7.5	250	7.2	250	6.9	250	6.2	250	5.9	250	6.2	245	5.6	245	6.6	245	5.9
6	255	2.3		1.3	225	1.6	200	3.0	170	3.9	165	4.6	165	4.9	160	6.2	170	5.6	170	7.2	170	6.9	175	5.6
7	235	8.5	240	8.2	280	6.6	290	4.9	290	4.9	290	3.9	290	2.0	305	4.3	355	6.2	350	6.6	345	6.6	330	7.5
8		1.3	۱ <u>-</u>	1.3	_	0.3	! —	1.3	90	1.6	<u> </u>	1.0		0.7	150	3.6	160	5.6	170	6.6	170	5.9	170	6.6
9	175	5.2	175	4.9	175	4.6	180	5.6	180	4.9	180	4.3	180	3.9	180	3.9	180	3.9	180	5.2	175	5.2	170	5.9
10	55	1.6	30	2.6	30	3.0	30	2.6	25	2.0	—	1.3	25	2.0	25	2.3	20	3.3	20	2.3	20	3.3	10	3.0
11	_	1.3	15	2.0	15	1.6	15	1.6		1.0	_	1.0		0.7	-	1.0	230	4.6	215	4.9	210	5.6	215	6.2
12	225	5.6	225	5.6	225	5.6	235	6.9	240	6.2	240	6.2	245	6.9	255	5.2	255	4.9	250	5.9	245	5.2	240	4.6
13	185	4.9	180	5.9	175	6.2	175	6.9	175	6.9	175	6.6	175	7.2	175	7.5	175	8.9	175	9.8	180	8.2	185	7.5
14	260	7.2	250	5.2	240	5.9	260	6.2	255	6.6	260	5.9	260	3.9	270	3.9	295	4.3	285	4.9	280	4.9	295	5.2
15	330	7.5	335	7.5	340	5.6	330	6.3	350	6.6	345	7.2	340	6.9	335	9.2	335	10.2	330	9.8	340	8.5	330	9.5
16	295	4.9	330	4.3	280	4.6	310	5.6	300	5.2	315	4.9	300	3.6	295	3.6	315	5.2	310	4.9	280	4.9	280	3.0
17	175	7.5	170	8.5	170	9.2	165	11.1	165	11.8	165	12.1	165	12.8	180	10.8	210	4.6	250	3.6	320	7.5	305	4.3
18	285	7.5	280	8.2	280	9.5	285	10.2	280	10.8	275	9.8	280	8.2	280	10.2	280	10.2	295	10.2	285	9.2	290	8.5
19	260	3.9	245	7.2	245	6.9	260	7.5	245	8.2	250	9.2	250	8.9	260	6.9	250	8.2	250	10.8	250	10.2	250	10.2
20	280	10.3	295	8.9	295	10.5	290	9.8	295	9.8	290	9.2	290	9.5	290	9.5	290	8.9	285	8.2	285	6.2	280	5.9
21	280	12.1	275	9.5	280	12.5	280	12.1	280	12.5	285	12.5	295	9.8	305	7.9	305	6.2	290	6.2	285	4.9	265	3.9
22	270	5.9	260	8.2	250	5.9	255	7.2	245	7.5	255	6.9	260	7.5	245	6.6	245	9.2	240	9.2	235	7.5	235	8.9
23	275	12.1	295	11.8	305	13.8	320	13.1	325	12.1	325	10.5	310	10.2	300	8.5	305	8.2	300	10.3	305	9.8	305	9.8
24	80	1.6	80	1.6	135	3.3	145	4.3	150	6.2	150	6.2	150	6.9	155	8.2	155	9.5	150	9.5	155	11.1	155	12.1
25	220	13.8	225	14.1	225	13.1	230	15.1	235	15.7	230	13.8	230	12.8	240	16.1	235	20.7	235	19.0	240	18.4	240	19.0
26	235	8.2	240	5.6	225	3.9	215	4.3	205	4.6	185	4.6	180	5.2	175	4.6	180	4.9	180	6.6	170	6.9	170	7.5
27	170	9.5	170	9.5	170	9.8	170	9.8	170	9.8	170	9.2	170	9.5	170	9.2	170	10.2	170	10.2	170	9.5	170	9.8
28	250	5.2	275	3.6	285	2.6	I —	1.3	_	1.0	I —	0.7	_	0.0		0.3	l —	0.3	_	0.7	I —	0.3	70	2.0
29	165	5.6	165	6.6	170	6.3	170	5.9	165	6.9	160	6.6	165	4.6	160	5.2	160	4.3	165	4.6	170	6.9	170	5.9
30	130	5.6	135	5.6	140	6.6	150	4.3	150	5.9	160	6.2	165	7.2	165	5.2	165	3.9	170	5.2	170	5.9	155	9.5
Mean	. -	5.9	I —	5.9		6.0	_	6.2	_	6.4	_	6.1	_	5.9	_	5.9	[6.4		6.8		6.8	-	7.0

364. Cahirciveen (Valencia Observatory): $H_a = 12$ metres + 14 metres.

	0	mla	-	I m la	0	1 /- 1	0	l /- 1		· · · · ·	0	 , -	-	 		1 /		1 /		1 /	0	1 10		1 1
1		m/s.	255	m/s.		m/s.		m/s.		m/s.		m/s.		m/s.		m/s.		m/s.		m/s.		m/s.	22.	m/.s
2	220	0·3	255	8.9	310	3.9	335	6.6	335	7.5	345	5.2	360	5.2	355	6.2	355	5.9	350	5.2	335	6.2	335	5.6
	230 180	i 1	230		230 260	8.5	235	11.1	265	8.9	335	6.9	345	6.2	340	4.9	340	4.3	340	6.2	335	1	325	5.2
3		7:5	240	13.1		16.1	285	16.1	315	16.4	330	15.7	340	13.8	340	13.4	340	12.8	335	13.1	335	2.3	330	1
5	350	7.2	355	5.6	350	5.2	360	5.2	360	3.9	360	3.3	360	3.9	360	3.3	360	3.3	340	3.0	325		l	1.3
3	175	4.3	175	0.0	170	5.6	175	2.9	170	5.9	175	5.6	275	5.6	310	3.6	305	2.5	310	4.3	295	4.9	300	5.9
6	280	5.6	285	4.6	280	5.6	280	4.6	265	6.6	280	6.2	260		260	8.5	280	8.9	280	6.9	275	7.2	275	7.9
7	240	5.9	240	6.2	240	5.2	220	3.9	215	1	i	1		7.5	1	6.6	225	6.6	235	5.9	240	8.2	245	5.2
8	300	3.9	300	3.0	300	3.0	300	3.0	300	3.9	210	4.3	195	1.0	215	2.0	200	3.0	190	3.9	180	5.2	175	5.6
9	230	12.8		11.8	250	10.8	250	7.9		3·0 6·6	255	8.3	260	8.9	260	8.5	260	7.2	255	8.9	255	7.9	255	8.9
ΙÓ	220	3.6	220	4.6	205	3.3	190	3.6	255 195		255 200	2.0	200		200	2.6	200	1.6	~55	1.0	260	1.6	320	4.3
	220	3 0	1 220	" "	1203	3 3	190	30	195	3.0	200	2.0	200	2.3	200	2.0	200	1 0				1 0	320	4 3
11	255	6.6	265	5.9	275	5.2	270	3.6	280	3.9	285	2.3	_	1.0	l	0.3	280	1.6	_	0.7		1.3		1.3
12	215	2.6	215	3.3	230	2.6	270	3.6	270	3.6	270	4.3	285	6.2	290	6.2	300	6.9	315	8.2	325	9.2	305	9.8
13	305	10.8	305	10.2	320	10.5	325	9.8	325	9.8	325	9.8	325	8.9	325	8.5	335	8.9	330	8.5	320	8.2	320	7.9
14	300	6.2	285	2.3	350	3.9	325	3.3	340	5.2	360	3.9	360	3.3	360	3.6	15	3·ó	35	2.0	345	1.6	_	1.3
15		0.7		0.0	33	0.7	30	2.0	J4°	1.0	30	2.0	30	1.6	300	1.0		1.0	_	0.7	155	1.6	220	3.0
		,	Ì	1	1	' /	J-	~ "		1	30	~ 0	30	1]		l		l	'	"			
16	255	5.2	250	3.9	250	5.2	255	4.6	270	4.9	270	3.9	270	4.3	270	3.6	275	3.9	270	3.3	270	4.3	270	4.9
17	265	3.3	255	3.0	255	3.0	255	3.3	255	2.6	255	3.9	-/-	1.3	255	1.6	235	1.6	225	2.0		0.7	195	2.6
18	125	3.9	115	3.6	125	4.3	125	4.3	115	3.3	105	3.6	115	4.9	115	2.6	105	1.6		1.0		1.0	130	2.0
19	235	10.5	245	13.4	255	13.1	250	11.8	255	10.5	245	10.2	260	9.2	250	8.9	245	7.2	245	6.9	240	7.2	235	6.9
20	185	5.2	185	5.9	180	6.2	180	6.9	185	8.5	175	6.9	175	7.9	175	9.8	175	11.5	175	13.1	170	13.1	170	13.1
			١	"					3		-73		-73	, ,	"/"		,,,		,,,	ľ	•		l '	ľ
21	320	3.6	305	7.2	310	9.2	300	7.5	280	8.9	280	8.5	275	6.2	260	8.2	240	10.2	235	9.8	235	12.8	235	10.5
22	245	10.2	250	11.1	255	11.8	250	12.5	255	13.1	265	9.8	275	12.1	280	11.1	280	9.8	270	7.9	260	7.9	245	7.5
23	185	4.6	175	6.6	170	8.5	170	7.9	225	9.8	255	12.5		11.8	275	10.2	275	11.5	255	10.2	255	9.5	245	10.5
24	235	8.2	235	8.2	230	6.6	235	7.5	220	7.9	230	8.5	225	6.9	220	5.9	230	7.2	220	8.9	220	9.8	225	9.8
25	230	5.9	225	6.6	225	7.2		13.8	230	15.1	230	12.5	_	12.1	225	10.5	225	12.1	230	13.4	225	13.4	225	11.1
						'	- 55	ا		١	١	١		i	ا ا				•		_	`	Ĭ	
26	190	3.6	200	4.9	185	5.2	185	4.9	220	6.6	250	9.2	240	8.2	235	9.5	230	6.2	210	4.9	195	4.3	180	5.9
27	170	6.2	180	5.6	175	6.9	165	7.9	155	8.5	150	9.8		11.8	145	9.8	100	5.6	60	3.0	50	1.6	290	3.9
28	290	11.8	300	10.8	300	11.1	305	11.8	300	10.8	310	12.1	310	10.2	300	10.2	305	8.9	290	9.8	285	9.2	285	10.8
29	180	5.2	180	5.9	180	6.9	175	7.9	170	8.2	170	10.5	175	10.2	170	10.8	170	10.2	175	10.2	170	8.2	185	5.9
30	180	10.2	220	7.2	225	5.2	220	7.2	215	7.2	225	6.6	225	5.2	225	5.6	230	6.2	220	5.6	220	6.6	230	6.6
				_				·	-				ľ	ا	ľ		•					-		
31	245	4.6	270	3.6	265	3.6	260	4.6	285	3.3		1.3	270	2.0	260	3.6	270	3.6	275	3.0	290	3.3	_	0.3
76													<u> </u>		l									
Mean		6.0		6.3	_	6.6		6.9		7.0		6.8	_	6.6		6.5		6.4		6.2		6.4	_	6.4
<u>-</u>				<u> </u>	l	1								1		<u> </u>		1		<u> </u>)	<u> </u>	<u>'</u>
G.M.T.			_		_					ı	_				١.	_		_ i	_			_	3.7	
G.M.1.	I	•	2	٠. ا	3	-	4	.	5	i- [6	. [7	•	1 8	3.		9.	ľ	ю.	l ^r	I.	I N	oon.
				1		1		1							<u> </u>		<u> </u>		<u> </u>					

Averages for periods of sixty minutes centered at the exact hours, Greenwich Mean Time.

M.S.L. $+ h_a$ (height of anemograph above ground) = 12 metres + 14 metres.

September, 1923.

ı	3.	1	4.	I	5.]	:6.	r	7-	I	8.	1	9.	2	o.	2	1.	2	2.	2	3∙	2	4.	Mean	Day.
325 280 170 270 245	m/s. 6·2 3·3 7·9 4·6 6·2	325 280 170 265 240	m/s. 5·6 3·9 7·5 6·6 5·6	310 280 170 260 250	m/s. 5·2 4·3 7·9 6·6 5·9	305 280 175 260 250	m/s. 5·6 3·9 7·2 6·9 5·2	310 260 175 255 250	m/s. 4·9 3·3 7·5 6·6 5·2	310 250 180 250 250	m/s. 4·6 2·3 5·6 6·6 4·6	310 230 180 245 250	m/s. 3·3 2·0 4·6 6·6 4·6	310 210 210 245 255	m/s. 2·6 3·3 4·9 5·6 3·9	90 220 245 265	m/s. 0·7 2·3 3·6 4·3 3·9	185 200 245 265	m/s. 0·7 2·0 3·3 4·3 3·6	185 310 245 260	m/s. 0·7 2·6 3·6 4·9 3·6	180 325 245 260	ms/. o·3 3·3 4·9 6·6 3·9	m/s. 3·7 2·0 5·4 5·1 5·7	1 2 3 4 5
180 330 175 170 335	5·6 7·2 6·9 4·6 4·9	190 325 175 205 320	5·9 6·2 6·6 3·6 5·9	210 340 175 305 320	5·2 4·9 7·2 5·2 5·6	220 355 175 320 320	4·9 3·9 6·2 4·6 5·6	215 340 175 330 320	3·6 5·9 6·6 3·0 6·6	210 340 170 35 325	2·0 5·2 7·9 2·3 5·6	195 340 175 — 325	2·6 2·0 4·9 0·7 1·6	200 — 175 —	3·6 1·3 4·3 1·0	210 — 175 20 —	3·3 0·3 4·9 3·3 0·7	220 40 175 30	5·2 1·6 3·6 1·6 0·7	215 — 175 20 —	5·2 0·3 3·9 2·6 0·7	225 40 180 25	5·9 1·6 4·9 2·0 1·3	4·4 4·7 4·3 3·9 2·9	6 7 8 9 10
215 240 190 290 330	6·9 4·9 6·9 5·6 6·2	220 230 185 280 315	6·6 4·6 6·2 6·2 8·9	215 225 240 290 335	5·9 5·6 8·9 5·9 8·2	220 225 255 295 320	6·6 5·6 9·2 5·6 9·5	225 225 265 295 320	6·2 4·9 6·2 5·2 8·9	220 220 260 310 320	5·6 3·9 8·5 5·9 7·5	215 210 265 305 305	5·2 3·3 7·2 6·2 6·9	230 200 265 310 315	6·6 3·9 8·2 5·9 6·2	230 200 265 310 320	5·6 3·3 6·9 6·6 4·6	225 200 270 300 315	5·6 3·9 6·2 7·2 5·2	225 190 260 300 345	5·2 4·3 6·9 7·5 6·2	225 190 260 310 300	5·2 3·9 6·2 6·2 4·9	4·2 5·1 7·2 5·8 7·5	11 12 13 14 15
270 285 255 265	3·3 1·3 9·8 10·2 5·9	270 280 280 260 260	3.0 4.6 10.2 8.9 5.9	260 255 290 260 240	3·6 5·2 9·5 9·5 4·3	240 260 290 260 200	3·9 4·3 9·2 8·9 4·6	220 260 290 255 180	4·3 2·3 7·5 9·8 5·9	190 290 290 255 185	4·3 3·6 7·5 10·5 7·5	185 195 285 255 240	3·6 3·3 8·2 10·5	190 290 290 260 245	4·3 5·9 6·2 9·8 10·8	190 290 285 265 250	4·6 6·2 7·2 7·2 II·I	180 285 270 280 260	5·6 6·6 9·8	180 285 265 285 270	5·9 5·9 6·2 9·8	175 275 260 285 280	7.5 8.2 6.9 11.5 14.8	4.5 6.7 8.7 8.9 8.8	16 17 18 19 20
255 235 315 150 240	6·9 9·8 10·5 13·4 17·7	255 230 310 150 245	7·2 8·9 9·8 14·1 15·4	255 235 310 155 250	6·9 9·5 9·8 13·1 13·8	245 235 310 150 250	7.9 9.5 8.2 14.4 12.5	240 235 315 200 250	9·2 7·2 8·2 6·6 12·5	240 220 310 205 250	7·2 6·6 7·2 3·6 7·5	240 230 305 185 255	7·2 6·6 4·6 5·9 8·2	240 220 300 190 245	7·2 5·9 3·3 6·2 10·2	235 230 295 185 245	6.6 6.2 1.6 8.2 10.5	235 230 — 195 240	7·5 1·3 7·9 11·1	245 240 145 200 240	7·9 9·5 2·0 8·9 7·9	250 260 100 215 235	Ì	8·5 7·9 8·5 7·9 13·7	21 22 23 24 25
170 170 160 170 160	7.5 9.8 2.6 7.2 3.3	170 170 165 170 165	7·9 10·2 3·0 8·2 4·9	170 170 170 170 165	6·9 9·8 2·3 8·2 6·6	170 170 170 170	7·2 7·9 3·0 6·9 3·9	170 170 160 170 170	6·9 9·5 4·3 6·9 3·9	170 170 165 170 170	7·2 8·5 5·9 3·9 4·9	170 170 165 170 170	7.5 9.2 6.6 2.3 3.6	170 175 165 170 170	7·2 7·5 6·6 3·0 3·6	165 180 165 — 170	8·5 8·9 4·3 1·3 3·6	165 185 165 145 175	8·9 6·9 6·2 7·9 2·6	170 200 160 155 180	8·9 4·9 5·9 8·2 1·6	170 220 165 145	8·5 4·6 6·6 6·9 1·3	6·7 9·0 3·1 5·8 4·9	26 27 28 29 30
_	6.9	_	7.1		7.1		6.8		6.3	_	5.8	_	5.3		5.3	_	5.0		5.4		5.2		6.1	6.2	

October, 1923.

13.	<u> </u>	4.						•			<u> </u>		<u> </u>		1		<u> </u>		<u> </u>		<u> </u>		1 '	U 4
	'			5.	,	6.	,	7.		8.	<u> </u>	19.		.o.		21.		22.	<u>.</u>	23.		24.	Mean	Day.
6.8	1	6.9		7.0		6.8		6.7		6.0		5.7		5.6		5.7		5.7		5.9		6.8	6.4	
_ r·3	255	2.6	250	2.0		1.3	-	0.0	_	1.0	180	3.0	170	2.6	165	3.3	165	3.6	165	4.3	165	4.9	2.8	31
170 6·2 250 8·5 285 10·8 185 6·2 230 .7·5	260 280	11·5 10·2 6·6 8·5	150 245 280 180 230	9·2 9·5 6·6 7·9	230 280 180 230	7·2 9·5 6·9 7·9	230 280 175 235	7·9 7·5 6·9 8·2	270 275 170 235	10·5 6·6 8·2 6·9	350 275 170 240	5·6 5·9 8·9 7·9	320 270 170 240	6·2 4·9 9·8 7·9	295 255 170 240	8·2 2·6 9·8 6·9	275 230 175 245	7·5 3·0 10·8 7·9	260 200 175 250	9·5 3·6 9·5 6·9	280 195 175 250	13·4 4·3 10·2 6·2	7.6 8.8 8.2 7.2	27 28 29 30
235 8·2 225 10·2 220 11·1	225	8·9 10·5 9·8 8·5	235 225 220	6·2 10·5 10·2	250 225 220 140	7.5 10.2 9.2	260 230 195 150	7·9 9·8 7·2	235 235 180 150	4·9 7·9 5·9	210 225 180	5·9 7·5 5·2	225 225 180	6·6 7·2 4·9 6·6	240 230 200	8·5 4·6	235 235 215	7.5	240 190 185	7·9 3·3 6·6	230 180	7·5 4·3 5·6	8·4 8·9	24 25 26
230 9·8 250 10·5	240 255	10.8	240 245	10.5	240 245	8·9	240	11·8 9·2	240 255	9·5 8·5	245 245	10·2 6·9	245 240	10·2 6·6	245 225	10·5 4·3 6·6	240 220 230	11·1 5·6 4·9	240 205 220	11·5 5·9 6·2	245 190 235	5·9 9·5	9·4 9·2 8·1	21 22 23
275 5·2 — 1·3 145 2·6 240 8·9 170 13·1	200 155 235	3·3 3·0 3·9 6·9	275 200 155 230 170	4·3 3·3 4·6 6·9	275 200 160 230 170	3·0 2·3 4·6 5·9	275 200 160 230 170	3·3 1·6 6·6 3·3	270 150 215 180	3·3 6·9 3·3	270 185 155 205 185	3.0 2.0 8.5 3.9 2.6	275 185 165 195 185	2·3 2·3 10·8 4·6 5·2	275 170 165 190 240	2·6 3·0 10·2 3·9 4·6	275 170 165 190 270	3.0 2.6 14.1 4.3 1.6	270 145 165 190 320	3.0 4.3 13.8 4.3 4.9	270 140 185 200 330	3.0 3.9 14.8 5.2 3.6	3·8 2·5 5·5 7·6 8·5	17 18 19 20
185 2·0 285 11·1 330 7·2 335 2·3 240 4·6	285 320 —	2·3 10·8 7·5 0·0 4·6	240 295 325 305 250	3·9 9·8 6·9 2·0 4·6	240 285 325 310 250	3.0 9.8 6.6 3.9 4.9	240 285 340 315 260	3.0 9.8 6.6 3.0 2.6	235 285 320 — 265	2·0 10·2 5·6 0·7 2·6	200 285 330 — 255	2·3 12·5 5·2 0·0 1·6	195 285 330 —	3.0 11.5 5.6 0.7 1.0	195 280 320 — 210	3.6 13.3 5.2 1.3 2.0	195 285 325 —	4·3 12·8 4·9 0·7 0·7	215 290 315 — 215	2·3 9·2 5·9 0·7 2·3	215 290 305 20 255	2·3 10·5 4·6 1·6 4·9	2·9 8·1 7·8 2·4 2·1	12 13 14 15
265 6·2 245 5·9 175 7·2 250 8·9 325 2·0	245 195 250	6·9 6·9 7·5 7·9 3·6	265 250 215 250 270	6·6 5·6 9·2 7·2 5·9	260 250 220 250 255	5·2 6·9 9·8 6·6 5·2	265 255 225 250 240	6·9 6·2 10·2 5·9 7·5	275 255 225 245 240	5·2 3·6 9·2 5·2 7·2	265 260 225 245 240	4·6 3·3 9·8 3·0 8·5	250 260 220 235 245	6·2 2·6 9·2 2·6 7·9	250 295 225 225 250	6·6 3·0 9·8 3·6 5·6	245 295 225 220 240	6·2 3·0 9·2 3·0 8·5	245 295 220 220 280	6·9 5·2 9·2 2·6 6·2	240 310 225 220 250	6·6 4·9 11·1 3·3 7·5	6·4 5·2 6·1 7·2 4·5	6 7 8 9 10
° m/s. 330 5·2 320 5·2 330 12·8 305 2·3 300 5·6	310 320 330 280	m/s. 4·6 4·9 12·5 2·0 5·9	290 320 335 — 310	m/s. 5·2 3·3 11·8 1·3 7·2	265 300 335 — 315	m/s. 3·9 3·3 12·1 1·3 5·2	265 330 340 220 305	m/s. 5·2 1·6 12·1 2·3 6·6	265 300 345 185 310	m/s. 5·2 2·6 11·8 3·0 5·2	255 290 340 180 310	m/s. 5·2 3·3 10·2 3·6 6·2	250 285 345 180 310	m/s. 3·9 3·3 9·5 3·9 4·6	235 255 350 180 290	m/s. 4·9 3·3 9·8 4·3 5·6	235 235 345 175 290	m/s. 5·2 3·3 9·8 4·6 3·3	235 190 350 175 295	m/s. 4·6 3·9 9·5 3·9 4·3	235 175 350 175 275	5·9 4·9	4·8 5·3 12·2 3·7 5·4	1 2 3 4 5
																			_	/	0 1	la	m/s.	

Direction expressed in degrees from North ($E=90^{\circ}$, $S=180^{\circ}$, $W=270^{\circ}$, $N=360^{\circ}$): Speed in metres per second.

365. Cahirciveen (Valencia Observatory):

Ha (height of anemograph above M.S.L.) = Height of ground above

Day.	1		2		3		4		5		(5.	:	7.		8.	٥) .	I	0.	1	ı.	No	on.
1 2 3 4 5	165 285 230 280 250	m/s. 3·6 7·2 11·1 12·1 5·6	160 290 240 280 255	m/s. 3·6 7·5 13·8 12·5 2·6	° 160 290 240 280	m/s. 3·6 7·5 15·1 12·1 1·3	160 290 230 280 255	m/s. 4·9 6·6 13·1 11·1 3·6	° 160 280 230 270	m/s. 4·3 4·3 12·5 11·1 1·3	0 160 255 230 275 225	m/s. 4.6 1.6 12.5 11.5 2.3	° 160 205 235 280	m/s. 5·9 2·6 14·1 9·2 1·0	160 190 235 270 310	m/s. 4·6 3·0 14·4 10·2 2·3	165 190 235 270	m/s. 4·6 3·0 15·7 8·9 1·0	185 180 250 270 300	m/s. 3·9 4·6 14·4 9·2 5·2	185 175 280 260 345	m/s. 4·9 5·9 13·1 10·5 2·3	180 215 270 260 310	m/s. 5·9 5·6 9·2 11·1 2·6
6 7 8 9	10 325 — 340 30	1.6 6.2 0.0 10.8 9.2	285 — 330 70	1·3 7·9 1·3 10·5 4·3	290 310 325 70	1·3 8·5 2·6 10·2 6·6	55 315 310 325 55	1·6 6·9 1·6 11·1 8·2	55 320 315 320 35	2·0 7·2 4·6 13·1 5·6	60 345 320 320 40	2·3 5·2 4·3 I3·1 4·6	30 330 320 340 45	4·9 3·9 4·9 12·1 2·0	30 300 330 350 80	3.6 3.0 3.3 12.5 2.0	25 310 330 345 75	3.0 2.3 4.3 12.1 3.9	30 300 280 350 50	3.9 2.0 4.3 10.5 5.9	15 260 290 10 60	5·2 3·0 4·6 13·1 5·9	10 210 300 10 55	6·2 3·0 4·3 13·1 3·6
11 12 13 14 15	200 300 170	0·0 0·0 8·2 10·5 6·2	 220 295 170	0·3 0·3 10·2 11·1 9·5	130 220 295 175	0·3 1·6 10·5 11·8	140 220 295 180	0·7 1·6 11·5 9·8 11·5	155 220 290 200	1.0 2.0 10.5 11.1 11.8		1·3 0·3 9·8 9·8	215 290 250	0·7 0·3 11·1 10·2 15·4	20 230 220 305 250	2·0 2·6 11·1 8·2 16·7	240 220 300 250	0·7 2·0 10·8 8·9 15·4	210 220 295 235	0·0 2·0 11·1 6·6 19·3	210 220 290 240	0·3 2·0 11·1 8·9 19·7	215 220 280 245	0·7 3·3 10·2 8·9 20·3
16 17 18 19 20	320 240 290 330 10	2·0 15·4 8·5 5·2 4·9	270 250 305 340 5	8·2 17·0 7·9 4·6 7·9	255 250 310 355 340	10·5 15·4 9·2 6·6 7·9	255 265 325 360 350	11·1 15·1 8·9 5·2 8·9	250 290 320 355 350	11·8 13·4 6·6 7·9 5·6	245 275 335 355 340	13·1 11·5 3·3 8·5 7·9	250 295 285 350 330	8·5 8·9 9·5 6·9	275	14·1 10·5 10·5 8·9 7·5	260 265 270 10	11·8 13·1 11·1 6·6 7·5	295	12·8 10·2 13·4 9·2 6·9	235 285 275 345 350	7·5 13·8 9·5 8·5	240 260 285 360 350	13·1 11·1 14·1 7·5 8·9
21 22 23 24 25	360 50 100	1.6 1.3 2.0 0.3 2.6	360 — — — — 100	3.0 1.3 1.3 2.6	15 65 105	2·0 1·3 2·0 1·6 1·3	55 65 — 100	2·3 1·3 5·6 1·3 2·0	75 105 100	1.0 1.0 5.9 2.3 1.6	70 65 80 105 100	2·3 1·6 3·0 2·3 2·3	- 65 -	1·3 1·3 4·9 0·3 1·0	90 65 80 —	1.6 2.0 3.9 0.7 1.3	65 80 —	0·7 1·6 1·6	65 60 —	0.0 1.0 1.0	65 50 — 140	0·7 3·0 2·6 0·0 3·0	335 65 70 — 160	2·6 2·6 4·6 0·3 3·3
26 27 28 29 30	 90 50	1·0 1·3 1·6 2·6 1·0		1·3 1·6 1·3 5·2 2·0	175 30 60 35 115	2·0 2·3 2·3 3·6 2·0	75 30 60 — 115	2·3 2·3 3·9 1·3 2·6	60 30 60 35	2·6 3·3 3·6 2·0 1·3	 30 60 115	0·7 2·3 2·3 0·3 1·6	- 60 -	1.3 1.9 1.3	55 — — — 115	1.6 1.0 1.3 1.0 2.6	55 — — 35 —	2·0 1·0 2·3 1·3	55 75 — — —	2·0 3·9 0·0 1·0	55 120 60 — 150	2·6 3·6 2·0 0·0 4·9	70 95 60 — 160	3.0 3.9 2.3 0.7 5.6
Mean		4.8	_	5.4		5.8	_	5.9	_	5.7	_	5.3		5.3	_	5.6		5.4		5.7		6.2		6.4

366. Cahirciveen (Valencia Observatory): $H_a = 12$ metres +14 metres.

	I. 2.		·																•					
Mean	_	6.4	_	6.9	_	7.0	_	6.4	_	6.4		6.2	-	5.6		5.9	_	6.1		5.9	-	6.1	—	5.9
31	280	1.6		1.0		1.0	280	1.6	265	2.6	_	1.3	230	2.0	230	1.6		1.3	_	1.3	220	1.6	_	1.3
29 30	190	7.2	210	6.2 1.3	140 240	3.0	155 240	2·3	160 245	3·6 7·9	165 250	3·3 7·5	170 255	4·9 9·2	185 265	5·2 7·9	160 280	9.5	270	9.2	280	11.5	290	9.8
27 28	290	0.5	285 330	9·2	350	7.9	280 350	13·1	²⁷⁵ 340	3.9	²⁷⁵ 350	9.2	275 340	1·6 8·9	230 335	9.5	335	10.2	330 160	8·9 8·9	330 155	7.5	330 160	8.9
2 6	270 280	11.8	275	11.1	280 280	12.5	280	11.5	280	11.8	285	9.5	290	6.6	285	5.9	285 190	4.6	280 190	2.0	240 175	2.3	215 175	3·0 6·6
24 25	185 145	3.3	250 165	4.6	250 165	5.9	255 165	5.6	255 165	6.6	265 170	8·9 6·6	270 170	7·9 6·6	260 170	6.2	250 170	4.6	195	5.6	215	8.2	220	8.5
22 23	300 270	9.5	295 275	9.8	290 295	8.5	285 315	9.5	280 315	9.8	290 320	10.5	290 325	8.5	285 330	7·5 9·8	285 330	6·9 10·8	330	14·8 6·2 11·8	325 240	8.2	320 245	7.2
21		1.0	290	4.3	275	5.9	265	6.6	255	6.2	265	6.6	260	6.2	255	6.6	245	7.2	250	8.5	270 275	8·2 10·8	² 75 265	7.5 8.2
19 20	330 15	4·3 6·9	330 20	3.6	320 30	6.6	330 35	3.3	330 20	4·3 3·6	325 10	5·9	320 10	6·2 6·6	350 10	5·6 5·9	340 20	3.9	345 10	6·9	350 25	3.0	345 40	8·5 2·3
17 18	235 280	7.5	230 275	7·5 8·9	240 285	9·5 8·2	240 280	5·2 6·6	240 290	4·9 6·9	240 305	3.9	245 3 10	4·6 5·2	280 310	5·2 4·6	260 305	3.6	250 315	4.3	325 325	3.9	235 330	4.3
16	275	4.6	265	4.9	265	4.6	250	4.3	245	4.9	245	4.3	245	2.3	245	4.6	245	5.9	245	3.6	265	4.6	270	3.6
14 15	165 350	4.3	170 350	4.3	175 350	4.9	185 335	3.0	190 320	4·3 4·3	195 325	4.3	210 325	4·6 1·6	220 330	3.3	225 325	3.3	225 300	5·9 2·6	225 305	5·9 2·6	225 305	3.6
12 13	175 10	8·2 2·0	175 —	8.5	175 —	0.3	175 —	1.3 5.5	175 —	9.5	175 —	9.8	175 —	0.0	175 —	9·5	175 —	0.0	175 —	0.7	175	7.9	175	7.9
11	180	6.2	180	6.9	180	6.6	180	6.6	175	6.2	175	6.9	175	7.5	175	7.2	175	7·9 8·5	175	8·2 8·5	175	8.5	180	8.2
9 10	345 220	3·9	360 225	3.3	355 230	3·6 5·6	340 225	3·6 4·6	335 220	2·0 5·2	335 230	2·3 5·6	320 220	2·3 4·3	230	5.2	230	0·7 4·9	220	6.3	220	0·7 5·9	220	0·7 4·9
7 8	170 285	11.1	170 290	11·1 10·2	175 290	9.5	175 300	7.9	175 320	8.9	180 320	7·5 8·5	200 360	5·2 4·6	220 350	4·3 5·6	215 320	6.6	215 340	5.9	230 340	7.5	225 330	5·2 6·2
6	10	5.6	15	3.9	20	2.0		0.3		1.0		1.3	_	0.3	-	1.3	-	1.3	_	1.0	135	2.3	240	3.0
4 5	250 5	8.2	250 15	10·5 8·2	250 10	10·5 8·5	² 45 20	9.5	240 10	10·2 10·2	240 10	8·9	250 10	10·8 8·5	245 10	8·5 8·5	240 5	9.2	240 10	9.5	230 5	10.8	240 360	9.8 13.1
2 3	280 275	9.8	² 75 285	8·5 9·2	280 295	7.5	290 315	4·9 7·9	245 310	9·5 7·9	250 320	9.5	250 335	5·9 10·8	280 325	9.2	290 335	7.5	295 340	7.5	290 325	7.9	290 310	3.6
1		m/s 0.3) <u> </u>	m/s) <u></u>	m/s	<u> </u>	m/s	<u> </u>	m/s	_	m/s	°	m/s	_	m/s	_	m/s		n/s	300	3.0	295	m/s.

WIND: DIRECTION AND SPEED.

Averages for periods of sixty minutes centered at the exact hours, Greenwich Mean Time.

M.S.L. + ha (height of anemograph above ground) = 12 metres + 14 metres.

November, 1923.

r	3.	I	1 .	1	5.	16	5.	r	7.	1	8.	19) .	20	Э.	2	ı.	22	2.	23	3.	24	4.	Mean	Day.
175 235 275 260 300	m/s. 5·9 8·5 10·8 10·2 4·3	240 235 275 265 310	m/s. 7·5 9·8 13·4 11·1 4·9	300 240 270 265 300	m/s. 6·6 8·9 12·5 10·5 5·9	295 240 275 260 310	m/s. 6·9 8·2 12·5 9·5 7·2	295 240 270 265 330	m/s. 5·2 8·9 11·8 9·2 3·9	290 240 270 265 350	m/s. 7·2 7·5 13·1 6·6 3·9	300 240 280 255 320	m/s. 6·9 8·9 12·1 9·8 5·2	295 240 280 255 355	m/s. 6·9 7·9 12·8 8·5 5·6	290 240 280 270 345	m/s. 6·2 8·5 12·5 5·6 4·6	290 240 275 265 350	m/s. 6·2 9·8 12·8 6·6 3·0	290 240 265 250	m/s. 5·9 8·5 12·5 3·3 1·0	300 230 275 285 25	m/s. 6·6 10·8 13·4 3·3 4·3	m/s. 5·5 6·8 12·8 9·5 3·5	1 2 3 4 5
5 200 300 15 30	4·9 3·3 3·9 8·9 2·6	10 185 300 10	5·6 4·3 4·6 8·2 1·3	10 175 300 10 330	3·9 5·6 4·6 8·9 3·0	340 175 330 10 355	2·3 5·6 3·6 9·2 2·0	345 170 345 25 20	2·0 5·2 5·6 8·5 2·0	315 170 355 30	3·9 5·6 5·9 10·2 1·3	20 175 350 15	1·6 3·3 6·2 13·8 0·3	175 335 25	1·3 3·6 8·2 13·1 0·0	175 350 20	0·7 2·3 8·5 16·1 0·7	95 140 345 25	1.6 6.9 13.8 0.3	135 330 30	1·3 1·6 8·9 12·1 0·3	20 335 25 	2·3 0·0 7·5 9·5 0·0	2·9 4·3 4·6 II·4 3·3	6 7 8 9 10
160 225 220 280 245	3·9 4·3 10·2 8·9 22·6	160 225 220 280 250	3·3 4·9 10·2 9·8 22·0	160 225 230 290 260	2·6 3·0 9·5 6·6 20·0	160 225 240 280 280	1.6 2.6 11.8 9.8 18.4	225 245 245 245 285	1·3 3·0 9·8 7·5 15·1	225 255 255 245 290	0·0 2·3 8·9 7·5 10·8	215 265 260 290	0·7 2·3 10·5 7·5 10·5	195 285 250 285	1.0 3.3 10.8 6.2 10.8	190 320 245 285	0·7 3·6 10·2 3·9 8·9	70 185 305 185 290	1.6 4.9 9.8 3.6 6.9	180 315 185 270	0·7 4·9 11·8 3·9 7·2	185 310 185 250	0·3 5·9 12·5 4·6 9·8	1·1 2·5 10·4 8·3 13 ·7	11 12 13 14 15
235 245 285 350 330	10·8 11·8 11·1 8·5	220 270 280 340 350	10·5 12·5 14·1 9·8 8·9	275	10·8 13·8 11·8 11·5 8·2	205 280 300 350 5	13·4 13·1 10·5 10·5 6·2	220 270 320 350 345	14·4 10·5 8·5 9·8 6·6	225 290 330 350 5	13·1 8·2 7·5 9·8 5·9	225 260 345 360 360	11·5 10·2 5·2 9·2 4·3	255 250 350 360 360	13·8 9·5 3·0 7·5 5·2	250 265 5 5 5	15·1 10·5 3·6 7·2 4·9	240 265 5 10 355	9·5 4·3 7·9 3·9	260 255 355 360 355	14·1 5·6 7·9 3·3	255 205 330 360 360	17·0 9·5 7·2 6·9 2·0	12·0 11·8 8·7 8·2 6·7	16 17 18 19 20
355 60 80 — 165	2·6 3·0 3·9 0·7 4·9	70 70 70 — 165	3.9 3.3 3.9	40 60 60 — 170	2·0 3·9 3·0 0·0 3·9	60 105 — 185	1.0 3.3 2.3 0.0	80 30 — — 200	2·0 3·9 0·7 1·3 3·9	65 40 105 — 200	2·3 2·3 2·3 1·3 3·3	55 — 105 100 200	2·3 0·0 1·6 1·6 3·3	65 — 105 100 195	1.6 0.3 2.0 1.6 3.9	65 — — 100 205	2·3 1·0 0·3 2·0 3·9	 100 205	1.0 0.3 0.7 1.6 4.3	 100 255	3.0 1.9 0.3 1.3	65 — — 100 —	2·0 1·0 0·3 2·0 1·0	1·7 1·9 2·6 1·1 2·8	21 22 23 24 25
300 95 60 30 175	4·6 3·9 3·0 2·6 5·6	75 60 360 185	0·3 3·6 1·6 2·3 5·2	75 55 360 200	0·3 4·3 3·0 2·0 4·9	355 75 50 10	1.6 4.9 1.6 3.0 5.9	30 80 — 20 185	1.6 3.6 0.3 2.3 6.6	80 50 30 190	3·0 3·6 3·0 1·6	80 35 185	1·3 4·3 0·7 3·3 5·9	80 50 — 185	0·7 4·3 2·0 1·0 6·9	30 80 55 — 200	1.6 2.6 3.3 1.3 6.2	30 80 55 80 240	2·0 3·0 2·6 2·3 7·5	30 90 55 — 315	2·0 2·0 1·6 1·0 4·6	30 55 	2·0 1·3 1·6 1·0 0·7	1·7 2·9 1·9 1·9	26 27 28 29 30
	6.7		6.8		6.5		6.4		5.8	_	5.2		5.2		5.4	_	5.3		5.1	_	4.8	_	4.9	5.7	

December, 1923.

•	m/s.	۰ ا	m/s.	1 °	m/s.	0	m/s.		m/s.	0	m/s.	•	m/s.	0	m/s.	1 °	m/s.	1 °	m/s.	°	m/s.	•	m/s.	m/s.	
180	3.6	175	4.6	175	3.9	175	4·3	175 310	4.9	140 310	6·2 5·9	150 305	8·5 8·5	300 300	8·5 7·9	325 300	5.9	280 275	7.2	270 270	9·2 5·9	²⁷⁵ ²⁷⁵	9.8	3·6 8·3	I 2
300	7·5 3·6	290 275	3.3	300 265	2.3	305 230	3.0	200	3.3	180	5.6	170	7.5	165	9.2	170	9.5	170	9.8	220	7.2	245	9.5	7.0	3
240	11.5	240 10	9.5	240 10	9.8	240	8.2	250 360	4·6 9·8	260 360	4·9 8·9	265 10	4·3 6·6	220 5	7.9	120	6.6	360	1.3	45 5	2.6	10	5.6	8·3 8·5	4 5
						ľ		ľ			_	177	8.5		8.9	170	9.2	170	10.2	175	10.8	170	10.8	4.7	6
230	3.6	160 220	5.6	160 220	5.6	170 220	5.9	170 215	6·9 8·9	170 225	7·9 9·5	175 250	13.1		13.4	290	10.2	295	9.8	290	9.8	285	12.1	8.6	7
340	7.9	335 220	7.9	320 250	7.5	340 230	5.2	360 210	3.3	3 ² 5 215	5·2 3·0	315 225	6·9 3·6	325 230	5.2	340 225	4.3	360 225	1.6	320 225	3.0	345 215	3.9	6·4 2·9	8
220	6.2	225	6.2	220	6.6	205	4.9	205	4.9	195	4.6	195	4.9	195	4.9	195	5.2	190	5.6	190	5.6	185	6.6	5.3	10
175	8.9	175	8.9	175	8.5	175	8.2	175	7.5	175	8.2	175	8.2	175	7.9	180	8.5	175	8.2	175	7.5	175	8.2	7.7	11
175	8.5	175	7.9	175	7.5	175 15	6·9 2·0	175 115	7·5 3·0	175 135	5·6 2·3	315 120	7.2	325	1.3	340 130	9.2	10 145	7·5 4·6	75 150	4.9	10 155	4.3	8·2 1·5	12 13
230	6.9	230	7.5	225	7.9	230	8.9	235	9.2	250	9.2	335	5.9	350 280	3.9	350	4·3 5·6	350 260	4·6 5·2	350 275	3·3 4·6	350 275	2.3	5·7 3·8	14 15
320	1.3	295	4.6	290	6.6	290	5.6	285	5.9	280	4.3	280	4.9	200	5.5	270			-				1	1	
270	3.3	265 240	3.6	250 240	3.9	250 240	4·3 3·6	250 240	2.6	240	0·7 3·0	215 240	3.6	230 240	4.9	220 240	3.9	230 265	5·2 3·0	240 265	7.5	240 270	3.9	4.3	16 17
330	5.2	330	4.6	330	4.6	330	4.3	330	2.6	330	3.3	330	3·6 8·9	330	2.3	330	3.3	330 10	7.2	330 15	3.0	330 20	1·6 5·6	4·6 7·2	18
345	9.2	345 50	3.0	345 55	11.5	355 55	2.0	355 45	7.5	355	6·9 0·7	5	0.3	— 10	9·2 0·7	5 65	1.6	-	1.3	-	1.0	_	1.0	3.2	20
270	7.2	270	6.2	270	6.9	275	12.1	285	11.1	295	11.8	305	10.5	315	9.2	315	8.5	325	6.9	305	5.9	295	10.2	7.4	21
260	8·5 8·9	265	6.0	265 320	6.6	260 320	12.5	265	11.8	265	10.8	265	10.8	260 290	9·5 3·9	260 280	9.8	250 270	8·9 4·6	245 260	9.2	255 205	2.6	10·8 7·1	22 23
315 260	10.8	320 280	11.5	290	7.9	310	5·6	310 355	5·6 4·6	305 55	4·9 5·2	290 65	3.3	70	2.6	_	1·3	—	1.3		0.3		10.8	7·3 8·2	24
225	9.8	225	9.8	230	12.8	230	12.5	235	13.8	245	10.2	255	9.5	265	8.2	260	8.9	265	10.2	265	11.8	270	10.9		25
220	6.2	230	8·2 8·5	225 220	8·2 8·5	230 220	9.5	235 220	12·8 10·5	1.5	10.8	260	8·2 10·8	280	8·2	280 240	9·5	280 260	9·2 10·8	²⁷⁵ ²⁷⁵	9.2	280 290	9.5	8·6 7·5	26 27
325	7.9	225 320	6.6	315	6.6	320	4.6	320	2.0	225	0.7	215 —	0.7		1.3	_	0.7		1.3	330	2.0		1.0	7.2	28
160 315	6.2	180 315	3.6	215 305	3.9	230 300	5.2	230 290	3·9 6·9	210 290	3·9 7·5	190 285	3·9 8·2	185 290	4·9 8·2	180 300	5.6	175 290	6·2 8·2	180 280	6·6 7·2	180 280	5.9	4·9 8·1	29 30
210	2.6	225	2.0	235	4.6	240	3.6	240	3.3	250	4.3	265	3.6	265	3.6	265	2.0	265	2.0	265	3.0	265	2.3	2.4	31
							6.8								<u> </u>						5.7		6.1	6.2	
_	6.4		6.5	_	6.7		0.8		6.4		6.0		6.3		6.2		6.0		5.9		3 /				
13	3.	I	\$.	. I	5.	10	5.	17	7.	18	3.	IĢ	9.	20).	2	I.	2:	2.	2	3.	2	4.	Mean	Day.

367. Cahirciveen (Valencia Observatory) : Ha = 17 metres + 13 metres.

1923.

	J:	an.	Feb.		Mar.		April		М	lay	Ju	ne	Ju	ıly	A	ug.	Sept.		Oct.		Nov.		D	ec.
Day.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max: in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust
1 2 3 4 5	m/s. 18 25 25 16 26	h. m. 13 35 21 25 2 20 23 20 13 0	m/s. 25 16 16 17 27	h. m. 18 25 18 50 5 0 23 35 21 45	m/s. 25 27 19 17 16	h. m. 22 45 2 45 12 35 12 55 0 20	7 19 10	h. m. 14 55 16 10 21 5 19 25 15 20	m/s. 10 8 7 13	h. m. 12 45 9 55 0 30 12 45 8 25	m/s. 13 † 14 17 11	h. m. 9 30 † 6 30 8 0 16 40	m/s. 8 13 13 6	h. m. 18 0 16 20 2 35 11 40 17 10	m/s. 14 30 11 21 14	h. m. 23 50 3 55 11 25 15 0 0 10	m/s. 10 6 15 11	h. m. 9 35 13 40 10 10 2 20 2 50	m/s. 12 15 23 13	h. m. 4 50 3 20 4 35 0 40 19 0	13 21 20	h. m. 21 55 23 45 9 25 4 20 18 40	24	h. m 20 0 16 5 12 15 9 35 10 55
6 7 8 9 10	16 18 23 30 23	0 25 23 25 23 5 19 15 3 15	27 43 15 33 19	0 35 4 45 16 0 12 40 6 40	21 22 9 14 21	6 20 1 30 2 40 22 15 11 35	11	20 10 14 55 23 55 11 30 0 50	9 9 10 21 18	17 25 14 55 14 0 15 15 20 10	10 16 21 21 18	3 5 22 45 3 50 17 30 0 40	11 12 15 13	21 50 14 40 12 35 9 50 0 50	† 16 11	† 4 10 10 25 13 15 16 30	13 12 12 11	13 30 0 50 17 40 4 20 16 0	15 12 17 17	8 50 8 10 14 25 1 10 22 0	14 17	17 55 2 35 23 25 21 10 1 10	20 20 19 11	22 10 1 10 6 25 0 5 24 0
11 12 13 14 15	20 5 10 15 9	5 45 22 55 23 50 7 5 15 10	15 13 12 20 21	6 20 22 30 0 5 23 50 4 15	18 21 14 8 12	21 35 10 0 1 45 23 15 12 10	19	0 I0 15 30 15 55 17 30 5 40	22 16 19 21 19	3 45 1 30 19 25 11 30 20 15	12 11 13 9 15	6 50 12 50 6 20 2 10 11 0	12 14	12 45 16 50 10 0 10 50 8 15	13 14 9 9	23 0 13 25 0 55 14 45 12 45	11 11 19 14 17	13 45 0 50 9 45 23 10 10 50	11 19 15 14 8	22 15 21 45 1 10 1 20 23 30	19 19	13 20 24 0 7 15 0 15 14 20	16 18 7 13 9	11 0 5 45 21 35 17 0 20 10
16 17 18 19 20	9 9 9 17 20	16 15 13 10 18 25 22 30 4 50	19 14 26 12 23	10 0 11 30 1 40 0 20 15 25	12 11 11 10 8	7 50 23 55 0 5 9 55 0 10	25 15 17	24 0 20 10 0 0 13 25 22 45	16 19 10 13 12	5 20 2 55 20 50 9 30 3 30	12 9 10 13 11	13 55 2 55 23 0 17.50 12 25	9 10	9 50 17 50 13 25 3 55 22 45	18 17 15 11 22	23 35 1 15 5 15 20 20 21 5	13 25 21 18 21	2 35 6 25 6 45 11 55 22 45	26 28	1 10 22 35 24 0 0 10 17 15	23 22	22 35 1 35 11 0 17 10 4 10	12 13 12 16	22 25 2 50 3 25 15 25 0 40
21 22 23 24 25	10 13 9 10 12	5 0 11 0 9 45 6 35 13 0	20 12 23 13 17	10 40 6 20 17 10 19 30 23 10	9 7 6 19 21	17 25 21 30 14 25 23 0 2 0	14 14	16 40 15 55 13 15 21 35 1 0	13 12 15 14	17 40 10 10 7 50 23 5 18 15	10 9 8 10 10	17 10 6 50 16 0 15 45 14 15	12 16 9	13 45 23 45 2 45 16 5 16 25	22 17 22 18 18	0 15 0 30 6 55 7 5 10 10	20 16 20 27 26	0 45 20 5 2 55 14 5 9 30	17 19 22 22 21	11 50 5 40 13 15 9 25 10 45	9 7 11 4 11	5 35 11 35 4 45 2 45 21 0	16 19 17 15	17 45 6 15 3 45 13 5 17 10
26 27 28 29 30	8 10 11 15 13	14 40 8 20 13 50 13 20 2 10	36 29 22 —	18 40 0 35 21 5 —	25 22 12 16 11	19 15 1 20 4 50 18 10 5 35	9	1 10 23 30 11 0 17 15 6 35	18 11 14 15 16	13 40 1 5 17 0 17 50 0 20	12 10 7 8 8	8 55 17 10 12 10 11 20 17 5	12 15 12 11 17	10 15 5 20 1 30 15 5 15 0	17 23 15 26 17	22 50 11 10 5 45 8 45 5 55	15 19 11 14 18	23 55 14 50 19 35 14 10 11 50	27 20 19 18 20	16 5 6 10 0 55 23 20 0 30	9 8 9 14	12 50 9 55 19 45 2 5 19 35	19 20 25 18	17 10 19 10 2 10 8 35 2 35
31	18	12 25	_	_	14	12 20	_	-	13	18 10	_	-	12	8 30	12	3 0		-	9	8 5	_	_	7	0 10

[†] Defective record.

DISTRIBUTION OF WIND SPEED: EXTREME VELOCITIES AS RECORDED BY THE DINES TUBE ANEMOGRAPH.

368. Cahirciveen (Valencia Observatory) : $H^a = 17 \text{ metres} + 13 \text{ metres}$.

1923.

					ICMPIDI						<u> </u>										
				L		JTION OF	WIND.				EXTREME VELOCITIES.										
N	Month.	•	More than I	10·8 to	17·1 m/s.	5·5 to 11 m/s.	1.6 to 5.4 m/s.	o to	No Record.	H	Iighest Hou	rly Wind	Hi	Highest Gust.							
			Dates of Occurrence.	Duration.	No. of Days.	Duration.	Duration.	Duration.	Duration.	Duration.	Veer from N.	Speed.		Iid. ime.	Speed.	מ	l'ime	·.			
Jan.			_	hr. o	11	hr. 95	hr. 310	hr. 262	hr. 77	hr. o	270	m/s. 16	day.	hour. 19	m/s. 30		h. 19	. m. 15			
Feb.	•••		4	18	17	125	324	160	45	o	170	24	7	5	43	7	4	45			
Mar.	•••	•••		0	11	87	268	292	97	o	260	16	1	23	27	2	2	45			
April	•••	•••		0	12	68	320	258	74	o	110	15	9	9	30	9	11	30			
May	•••	•••	. –	0	6	31	411	264	38	o	350	13	25	18	22	11	16	5			
June	•••	•••		0	3	24	309	329	58	o	200	13	9	17	21	8	3	50			
July	•••	•••		0	I	1	259	405	74	5	250	11	30	15	17	30	15	0			
Aug.	•••	•••	r	3	10	64	383	227	43	24	250	18	2	12	30	2	3	55			
Sept.	•••	•••	1	ı	7	53	391	228	47	0	250	17	25	9	27	24	14	5			
Oct.	•••	•••	_	0	13	67	390	266	21	0	200	16	18	24	28	19	0	10			
Nov.	•••	•••	ı	3	7	65	² 34	283	128	7	270	18	15	14	29	16	22	35			
Dec.	•••			o	11	38	418	233	55	0	240	15	28	2	25	28	2	10			
Year	•••	•••	7	25	109	718	4,017	3,207	757	36	170	24	Feb. 7	5	43	Feb. 7	4	4 5			

MINIMUM TEMPERATURE "ON THE GRASS" DURING THE INTERVAL 18H. TO 9H. G.M.T. Readings in degrees absolute.

369. Cahirciveen (Valencia Observatory).

1923.

Day.	Jan.	Feb.	Mar.	April	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.	a.
I	73.1	83.6	75.9	71.9	80.5	77·9 75·3	79.0	82.7	79·5 76·9	83.3	80.3	77.2
2	82.1	83.4	76.9	72.3	79.7	75.3	84.9	83.7		81.4	77.0	75.5
3	77.9	l †	77.1	74.2	80.9	77:9	85.9	83.5	80.1	80 · 2	83.1	74.9
4	76.5	77:3	72.5	77.9	82.6	81.9	84.8	†	80.7	76∙9	77.2	76·4 74·8
5	79.1	78.5	79.1	76.9	80.3	79.7	85.1	86.3	82.1	80.1	75.7	74.8
6	75.3	78∙0	79.8	74 · 1	80.1	81.9	82.1	84.5	83.9	78.9	72.3	71.5
7 8	81.2	74.1	78.6	76.3	72.3	77.0	84.3	86.9	84.8	83.9	72.8	78.0
8	78.5	72.5	77.0	72.3	75.9	83.1	84.1	84.5	77.2	80.2	77.3	75.9
9 10	77.2	75.0	72.9	78.5	77 · I	84.3	87.5	85.8	83.3	83·o	76.5	73.1
10	75.1	78.9	76.8	74.4	75.8	81.5	83.9	84.8	79.1	82.1	71.7	79.7
II	74.8	75.2	74.9	75.2	76.9	81.5	79.5	8r·o	77.9	80.9	74.8	80.
12	72.2	77.5 81.8	79.1	73.3	74.5	79.1	83 · 1	86.9	85.5	79.9	81.4	81.
13	75.2		75·9 71·7	74·I	72.7	84.3	82.7	87.9	85.1	78.6	82.7	72.0
14	82.0	72.0		76.4	75.9	80.9	83.0	85.1	81.1	75·2 71·9	74.8	73
15	76.9	79.6	75.2	76.9	75.7	84.3	83.5	81.5	79.0	71.9	73.1	74
16	79.1	75.9	73.7	78.7	77.4	†	83.9	81.9	77.3	76.3	73.6	78.
17 18	78⋅1	77·I	73·7 74·8	78.5	76.9	80.9	82.5	85.1	82.0	82.3	74.1	79.
18	72.4	76.7	73·1	80.7	79.3	84∙0	80.0	84 · 1	79.8	78·1	72.6	79.
19	78.9	73·1	74·1	74.1	79·3 80·6	81.3	84.9	84.7	79.5	79.1	75.0	75.
20	77.8	70.9	72.0	80.5	80.6	81.8	87.5	86.3	80.9	78.5	74·I	75.
21	75.2	75.8	72.5	75.3	79.9	82.3	87.6	83.1	83.7	77.7	72.1	71.
22	78.3	73.6	75.9	74.2	82.5	81.5	87:4	83.1	80.0	79·I	67.5	80.
23	74.3	71.3	75.0	74.2	80∙0	85.1	1	81.1	79.9	79.9	70·1	77
24	78.2	76.3	74.6	71.3	73·I	85.1	83.0	81.1	77:3	76·2 78·6	68.1	79·
25	76.9	78.1	79.8	79.9	79.1	85∙0	87.0	80.5	82.1	78.0	00-1	l .
26	80.2	79.2	78.5	77.9	76.7	84.7	84.1	83.6	83.7	75.9	74.3	80.
27 28	80.3	78·1	81.8	74.8	78.0	82.0	84.7	82.0	85.0	77.3	69.0	78
	76.5	76.9	79·I	76.5	76.8	80.6	84.8	81.3	82.9	78.9	69.1	78.
29	81.4		77.5	79.7	74·I	84.0	84.3	80·8 80·1	86·7 82·5	78·5 80·9	70·1 66·9	76·2
30	82.5	_	80.6	83.1	78.5	83.7	84.9	90.1	02.2	00.9	00.9	30.
31	81.9	-	73.9	-	78.0		82.5	79.8		79.5		79.
n	77.7	76.7	76.1	76·1	77.8	82.5	84.1	83.5	8r·3	79·I	73.8	77.

Notes:—(1) The initial 2 of the readings is omitted, i.e., 275 o degrees absolute is written 75 o.

⁽²⁾ The minimum refers to the interval from 18h. the previous day to 9h. on the day to which it is entered.

† No record.

370. Cahirciveen (Valencia Observatory).

				oud All F							Wea	ther.					
Day.	7h	13h	18h	7h	9h	131	151	h 18	3h 21	h 7h	9h		13h	15h	18h	21 h	Remarks.
1 2 3 4 5	St. St. St. St. Cu. St. : A. St.	St. St. St. St. St. Cu. St. Cu. St. Cu.	St. St. Cu.: A. St. St. Cu.: A. Cu. St.: A. St. St. Cu.	10 10 8 8 9	10 10 10 9	10 8 8 9 5	10 7 8 10 5	10 8 7 10 4	9 4 10		•		•	•		 •°	Fair to o \triangle early, o \bigoplus day. c or o all day, occasional \bigoplus ⁰ c or o with p \bigoplus ⁰ day: fair at n : c or o a : o in p : \bigoplus at n : \bigoplus ² early, c to fair day with p \bigoplus .
6 7 8 9	St. Cu. : A. Cu. St. St. Cu. Cu. St.	St. : A. St. St. Cu. St. Cu. : A. Cu. Cu. : St. Cu.	St. St. St. Cu. : A. St. St. St. Cu.	7 10 9 1	9 10 4 7 9	10 10 6 6	10 10 6 7 4	10 10 7 7	10 10	 •° y. p★	• ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °		 •° 	•°	• • • • • • • • • • • • • • • • • • •	•° •° • ···	cp \bullet to fair in $a : \bullet$ in $p : o$ with \bullet at $n : o$ with intermittent \bullet all day. •• early, b to bc $a : b$ to o in $p : \bullet$ at $n : o$ Squally with frequent p \bullet during day, fine squally with frequent p \bullet all day. [n]
11 12 13 14	St. St. Cu. St. St. St. St.	St. Cu. : A. Cu. St. Cu. : A. Cu. St. St. Cu. St. Cu. St.	St. Cu. : A. St. St. Cu. : A. Cu. St. St. Cu. St.	4 9 10 10	6 2 10 10	8 3 10 5 10	9 7 10 8 10	8 4 10 9 10	10 10 8	 • • • ≡ 	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		 • ° ≡ ° • ° ≡ °	p ● = •°=°	 = 	p• •°≡°	p in $a: 0$ to be $p:$ fine at $n:$ Fine \square early, a fine day. O with $p \bullet a: \equiv^0$ and \equiv with \bullet^0 all day. O with \bullet^0 & \equiv^0 early: fair a and $p: c$ at n be to $a: \bullet^0$ & \equiv^0 $p: c$ or oat $n:$
16 17 18 19 20	St. Cu. St. St. St. St. Cu.	St. St. St. Cu. St. St. Cu. : Ci.	St. St. St. Cu. St. St. Cu. : Ci.	- 7 1 10 7	10 9 3 10 6	10 8 10	10 10 9 8 8	10 9 10 3	10	=0 0 == 1 = 0 0	=° •° ≡ 	0		 p•0	···	 • °	[● 0
21 22 23 24 25	St. St. St. St. St.	St. Cu. : Cu. St. Cu. St. St. Cu. St. Cu.	Cu. St. Cu. : A. St. St. Cu. St. Cu. St. Cu.	10 10 2 6 4		10 10 10 8 7	5 7 10 8 7	9 3 6 10	10 10	●°≡ 	 						
26 27 28 29 30	St. St. Cu. St. St. St. St.	St. Cu. St. : A. St. St. : St. Cu. : Cu. St. St.	St. Cu. St. Cu. St. Cu. St. St. St.	10 10	10 10	10	10	10 10 10	10 10	 •°≡'			•	 •°≡°	 •0≡0 •≡0	 •0 ≡0	Overcast and dull all day. Overcast and dull all day. $\bullet^0 \& \equiv^0 \text{ early } \& a : o p \text{ and } n : o \text{ early, } \bullet^0 \& \bullet \text{ in } a : \bullet^0 \& \equiv^0 p \text{ and } n$ $\bullet^0 \text{ early, } o a : \bullet^0 \text{ or } \bullet p : o \equiv^0 n :$
31 Mean Cloud Am'nt	St.	St.	St.	10 7·6			-	-	-	●⁰≡		0 -	•	•		● ⁰ ≡ ⁰	o with ●0 & ≡0 or ● at times all day.

371. Cahirciveen (Valencia Observatory).

February, 1923.

1				ī	1		1		- 1			1	1		1	1
1	St.	St.							10	•0	•	●0≡0	•			o with ● or ●°, all day.
2	St.	St.						10	9		• • • •			. • • •	•••	o with \bullet or \bullet ⁰ , early & a : o p and n :
3	St. Cu. : Cu. St. Cu.	St. Cu. : A. Cu. : A.St. St. Cu. : Ci.	St.: St. Cu.: A. St. St. Cu.	8	7 8	9	10 8	9	8		•••		•••	•••	•••	o or cearly & $a: p \oplus p$ and $n: \oplus p$: op \oplus early, o to bc $a: cp: bcn:$
4	St. Cu.	St. Cu. : Ci. St.		9 10				10 10	7]			• ≡ ⁰	•	•	$c \& o early, o \bullet o r o \bullet^{\circ} all day.$
5	St. Cu.	St.	SI.	10	10	10	10	10	10			•	•="	•		ca dearly, d of d o anday.
6	St. Cu.	St. Cu. : A. St. : A.Cu.	St. Cu.	10	7	7	10	3	1			l l	P▲	•••		\bullet early, cp \bullet to b a : op $\triangle p$: op \triangle to b a
7	Cu.: St.	St. : A. St.	St.: A. St.	10	7 8	10	10		10				^ -	•••	p●²	\bullet early, o or c a: \bullet ϕ : $p \bullet n$:
8	Cu.	St. Cu. : A. Cu.	St. Cu.	2	4	6	10	3	1							$p \bullet \text{ early, bc } a : p \blacktriangle \bullet p : b \text{ to cp} \blacktriangle n :$
9	Cu. : St.	St.			10	10	8	7	7		• • •	•		•••		p igoplus early, o a : o igoplus to c b : bc to o n :
10	St. Cu.	Cu. : A. St.	St. Cu. : Ci. St.	10	7	8	6	7	I	●0	•••		•••	•••	•••	$0 \bullet_0 \text{ early, c } a : \text{cp} \bullet \text{ to bc } p : \text{cp} \bullet \text{ to b } n$
11	St. : A. St.	Cu.	St. Cu.			ı	8	10	10			1	1			$p \bullet \text{ early, b to c day, o} \bullet_0 \text{ to o } n$:
12	St. : St. Cu.	St.	St. Cu.	9 10	3		10		10	• • • •	 p●	•			:::	$p \bullet early & a: \bullet at times p and n:$
13	St. St. Cu.	St.	St.Cu.: A.Cu.: Ci.Cu.		10	10	6	5	10	 •°	=0					\bullet early, $o \equiv 0$ a : o to b p and n :
14		A. Cu.	St. Cu. : A. St.	_	I	3	6	7	5			l l		•••		\square early, b a: b to o p : c or bc n:
15	St.	St. : A. St.	St.: A. Cu.	10		10	10	7 8	ĭ	● ≡ 0	•	•	•			$0 \bullet \equiv^0 a \text{ and } p : p \bullet \text{ to b at } n :$
Ĭ						1			1		•					
16	St. Cu.		St. Cu.: Cu.: A. St.		10	10	10	8	9		•		•	•••	p●	bc early, \bullet a and p : bc to op \bullet n:
17	St.	St.	St. Cu.	10	10		10	10	10		•••	•	≡0	•••	●f	op ● or o ● all day.
18	St. Cu. : Cu.	St.	St. Cu.	9	9	10	8	8	3	•••	•••	p●	•••	•••	=0	
19	Cu. : A. St. Cu. : A. St. : A. Cu.	St. Cu. : A. St. St. Cu. : A. St.	St. Cu. : A. St. St.	4	10		10	10 10	10 8		•••		•••			b to c a : c or o p : \equiv^0 at n : Learly, bc to $o \oplus^0 a$: $o \oplus^0$ to $o \oplus p$: $o \oplus$
20	Cu A. St A. Cu.	St. Cu A. St.	St.	7	10	10	10	10	°	ш	•••		•••		•••	[o 1
21	St. Cu.	Cu. : St. Cu.	St. : St. Cu.	10	7	7	7	8	3					•••		op \bullet early, bctop \blacktriangle T a and p : p \blacktriangle \bullet to b
22	St.	St. Cu. : A. St.	Cu.: St. Cu.	10	10	7 8	10	4	I				p●		 	$o \bullet a : op \bullet to bc p : fine at n :$
23	St.: St. Cu.	St. Cu. : A. St.	St.	8	8		10	10	10						● = 0	bc to op \bullet $a: o \bullet p$ and $n:$
24	St.	Cu.: A. Cu.: Ci. Cu.	Cu.: Ci. St.	9	8	6	5	3	8		•••	\				\bullet early, op \bullet to ca: b to cp and n:
25	St. Cu.	St. Cu.	St.	10	9	10	10	10	10		•••		● 0	•	●0	\bullet early, o to bc $a : o \bullet^{0} p : o \bullet n$:
٠. ا	St.	St. : St. Cu.	St.	10		8									•0	\bullet early, $p \bullet a$ and $p : o \bullet$ at $n :$
26	St. St.	St. : St. Cu.	St. Cu. : Cu.	10	10		10		10	•			•	•	1	
27 28	St. St.	St. Cu. : Ci.Cu. : Ci.St.	St. Cu Cu.	10	10	6	7	7	5 10		•		•••	•••		$0 \bullet a \cdot op \bullet p \cdot oto bc n$. $0 \bullet early, op \bullet to bc a : p \blacktriangle p : o or c n$:
lean		5t.CuCI.CuCI.St.		10	-	-	_	_5_	10						- ···	o carry, op o to be u . p p . o or c n .
loud				8.8	8.0	0	0.0		6						İ	
m'nt				0.0	0.3	0.4	0.9	7.9	0.7]				
1 110		1	<u> </u>		1	'	1		1 1	<u> </u>		<u>' </u>			<u> </u>	<u>.</u>
	7h	13h	18h	7h	oh	13h	15h	18h	21h	7h	9h	13h	15h	18h	21h	
Day.	,	-5-		1′		"	J.,			/-	3	-5	-5-			Remarks.
ا . ر				1-								<u> </u>				1
		Cloud Forms.]			mo					Wea	ther.			
l				Į.	(A	All F	`orm	s).		l						

i																
						Amo					Wea	ther.				
Day.	7 ^h	13h	18h	7h	9h	131	151	181	21h	7h	9h	13h	15h	18h	21 h	Remarks.
1 2 3 4 5	St. Cu. Cu. St. Cu. St. Cu. Cu.	St. : A. St. St. Cu. : Cu. St. Cu. : Cu. St. Cu. : A. Cu.	St. Cu. : Cu. St. Cu. : A. Cu. St. Cu. : A. Cu. St. Cu. Cu. : A. St.	8 7 10 7 2	10 9 8 10 5	10 4 7 10 5	10 5 6 10 5	8 6 6 10 3	7 9 9 10 8	 p ^	 p● 	•	•			c or o a: o ● p: fair at n: p ● early, p ● ▲ all day: op ● to o n: p ● ▲ early, c in a: p ▲ in p: o at n: Fair early, c to o during day. ● early, fair during day.
6 7 8 9	Cu. St. Cu. St. Cu. St. St. Cu.	St. Cu. : Cu. St. Cu. : Cu. : A. Cu. Cu. : A. Cu. : A. St. St. Cu. : Cu. : A. Cu. St. Cu. : Cu. : A. Cu.	St. Cu. St. Cu. St.Cu.: A.Cu.: Ci.Cu. St.: St. Cu.: Cu. St.	10 9 6 10	6 9 8 7 10	3 7 3 5 10	7 7 4 6 10	7 8 3 8 8	6 10 2 2 2	p ● •						● early, fair to op ● or cp ● day. p ● early, c or o all day. o early to bc in p : fine n : Fair or fine day with ∞ in p : o ● early & a : o ● to c p : b at n :
11 12 13 14	St. Cu. : A. St. St. Cu. Cu. St.	St. St. Cu.: Cu. Cu.: A. Cu. Cu.	St. Cu. St. Cu. St. Cu. : A. St. Cu. : Cu. : Cu.	7 10 8 - 10	10 4 - 10	7 3 1	8 3 3 3	10 6 2 7	10 7 - 7 -	 8	=° • ··· ··· ∞	•° 8	• 8	• 8	●°≡° ∞	b early, $o \equiv^0 a : o \oplus p : o \equiv^0 \bigoplus^0 n :$ $o \oplus$ early & $a : c$ in $p : cp \oplus$ to $b n :$ bc to $cp \oplus$ early, fine day. \square early, b to bc day: c at $n :$ o in $a :$ fine in p & at $n : \infty$ all day.
16 17 18 19 20	St. Cu. St. — St. St. Cu.	St. Cu. St. Cu. Cu. St. Cu. St. Cu. : Cu.	St. Cu. St. Cu. ————————————————————————————————————	10 6 - 10 2	9 9 10 10	8 7 5 8 7	9 4 7 10 7	7 1 - 10 8	9 5 - 3 10	≡° ≡° ⊔ ≡°	⊗ ≅° ⊗ ⊗	88888	88888	: 8 8 8 8	: 8 8 8	\equiv^{0} early, $o \infty a$: $c \infty$ to $b c \infty p$: o at n : \equiv^{0} early, o to $c \infty a$: $c \infty$ to $b \infty p$ and n $\equiv^{0} \sqcup$ early, fine with ∞ all day. bc early, c or o with ∞a and p : $b \infty n$ $\equiv^{0} \sqcup$ early, c or o with ∞ day: o o o o :
2I 22 23 24 25	St. Cu. St. Cu. St. St. Cu. : Ci. St. St. Cu.	St. Cu. : A. Cu. St. Cu. Cu. St. Cu. : Ci. Cu. Cu.	St. Cu. : Ci. St. St. Cu. St. Cu. St. Cu. St. Cu. Cu. Cu.	9 10 9 9	8 8 5 9 5	7 7 3 7 5	5 6 3 8 6	7 2 2 7 3	IO - IO	=° =° =°	8 8 8 8 .:.	8 8 8 ::	. 8888	: 88:	 =0 ●0=0	Cloudy with \equiv^0 or ∞ all day. o to be with ∞ a : be ∞ to b p : b n : o \equiv^0 early, be to b with \equiv^0 or ∞ day. $\triangle \equiv^0$ early, c or o with ∞ day, $\bigoplus_0 n$: $\equiv^0 \bigoplus$ early, cp \bigoplus to b a : be to b p : b at n
26 27 28 29 30	St. Cu. St. Cu. : Ci. St. St. A. St. St. Cu. St. Cu.	St. Cu. St. Cu. : A. Cu. St. Cu. : Cu. St. Cu. : A. St. St. Cu. : Cu.	St. Cu. St. Cu. : A. Cu. St. Cu. : A. Cu. St. : A. St. Cu.	9 8 3 10 9	9 10 2 10 10	9 7 3 10 3	8 7 2 10 5	10 7 3 10 2	10 3 10 1	 ≡° •	 ≡° 	 8	 	 •°	● ≡ ⁰	bc early, c or o day, $\bullet \equiv^0$ at n : \bullet early, c or o with $\equiv^0 a : c p : \bullet n :$ \bullet early, fine day, bc early, o or c $a : o \infty p : \bullet n :$ \bullet early, o to b $a : b$ or bc p and $n :$ \bullet [b n]
31 Mean Cloud	St.	St.	St. Cu : Ci.	10		10	8	8	$\frac{3}{5 \cdot 6}$	þ	<u></u>	•			<u></u>	bc with \triangle early, o to $o \bullet a : o \bullet$ to bc p
373.	St. : Ci.	Cu.: Ci. St. Cu.: Cu.	St. St. Cu. : Cu.	7 2	5	4	8 2	10 2	10 2	ננ					=0	April, 1923. \square early, fair day : $o \equiv^0$ at n : \square early, fine day & n :
1		Cu. : Ci.	St.		5 1 10 9 8	4 1 10 8 7							i i		1 1	□ early, fair day: $o \equiv^0$ at n : □ early, fine day & n : o a : ● in p & at n : ● early, c or o all day. p● early & a : c or be p and n :
1 2 3 4	St. : Ci. St. : Ci. St. St. Cu. : A. St. St. Cu. : A. St.	Cu.: Ci. St. Cu.: Cu. St. Cu.: A. St. St. Cu.: A. Cu.	St. St. Cu. : Cu. St. : A. St. St. Cu. : A. Cu.	2 10	10	1 10 8	2 10 7	10	2 10 9 6 10 4 10 7	 		 •	 •	 •	 •≡⁰ 	□ early, fair day: $o \equiv^0$ at n : □ early, fine day & n : o a : \bigoplus in p & at n : \bigoplus early, c or o all day. p \bigoplus early & a : c or b c p and p : [o \bigoplus at p early, p or p or p p p early, p or p p p early, p or p p p early, p or p p p
1 2 3 4 5 6 7 8	St.: Ci. St.: Ci. St. St. Cu.: A. St. St. Cu.: A. St. St. Cu.: A. St. St.: St. Cu. St. Cu.: Cu. St. Cu. St.: A. St.	Cu.: Ci. St. Cu.: Cu. St. Cu.: A. St. St. Cu.: A. Cu. St. Cu.: Cu. St. Cu.: Cu. Cu.: Cu.: Ci. Cu.: A. Cu. Cu.: A. St. St. Cu.: A. St.	St. St. Cu.: Cu. St.: A. St. St. Cu.: A. Cu. St. Cu.: A. Cu. St. Cu.: Cu. St. Cu. St. Cu. St. Cu. St. Cu.	2 10 7 8 3 10 1	1 10 9 8 4 6 1 9 8 10 2 10	1 10 8 7 4 6 2	2 10 7 7 9 7 8 10	2 10 7 7 10 3 9 8	2 10 9 6 10 4 10 7	☐ 	:::::::::::::::::::::::::::::::::::::::		 • p•° 	 • • • • • 		□ early, fair day: $o \equiv^0$ at n : □ early, fine day & n : o a : ● in p & at n : ● early, c or o all day. p● early & a : c or bc p and n : [o ● at n early, b or bc a : b or bc p and n : □ early, op ● to bc a : b or bc p and n : □ early, fine a : b to o p : o ● $0 \equiv^0$ n : ■ early, o or c with ∞ all day.
1 2 3 4 5 6 7 8 9 10 11 12 13	St.: Ci. St.: Ci. St. St. Cu.: A. St. St. Cu.: A. St. St. Cu.: Cu. St. Cu. St. Cu. St.: A. St. St. Cu. St. Cu. St.: A. St. St. Cu. St. Cu. St. Cu. St. Cu.	Cu.: Ci. St. Cu.: Cu. St. Cu.: A. St. St. Cu.: A. Cu. St. Cu.: Cu. St. Cu.: Ci. St. Cu.: Ci. St. Cu.: Ci. Cu.: A. Cu. Cu.: A. St. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: A. St. St. Cu.: A. St. St. Cu.: A. St. St. Cu.: A. St.	St. St. Cu. : Cu. St. : A. St. St. Cu. : A. Cu. St. Cu. : A. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.	2 10 7 8 3 10 1 10 9 9 1	1 10 9 8 4 6 1 9 8 10 2 10	1 10 8 7 4 6 2 10 7 10 8 10	2 10 7 7 7 8 10 7 10 10 10 10 10 10	2 10 7 7 10 3 9 8 10 8 7 9	2 10 9 6 10 4 10 7 10 10] p•° ∞ 	 8 8 1 1		 p ● 0 ∞ ∞ 	 	 • = 0 • • • • •	□ early, fair day: $o \equiv^0$ at n : □ early, fine day & n : o a : ● in p & at n : ● early, c or o all day. p● early & a : c or c
1 2 3 4 5 6 7 8 9 10 11 12 13 114 15 16 17 18 19	St. : Ci. St. : Ci. St. St. Cu. : A. St. St. Cu. : A. St. St. Cu. : Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. St. Cu. St. St. Cu. St. St. Cu. St. : A. St. St. Cu. : A. Cu. Cu. St. : St. Cu. St. : St. Cu.	Cu.: Ci. St. Cu.: Cu. St. Cu.: A. St. St. Cu.: A. Cu. St. Cu.: Cu. St. Cu.: Ci. St. Cu.: A. Cu. Cu.: A. St. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St.: A. St. St. Cu. St.: A. St. St. Cu. St.: A. St. St. Cu. St.: A. St. St. Cu. St.: Cu. St.: Cu. St.: Cu. St.: Cu. St.: Cu. St.: Cu.	St. St. Cu.: Cu. St.: A. St. St. Cu.: A. Cu. St. Cu.: A. Cu. St. Cu.	2 10 7 8 3 10 1 10 9 1 10 8 8 8	1 10 9 8 4 6 1 9 8 10 2 10 10 9	1 10 8 7 4 6 2 10 7 10 10 10 7 10 10 7	2 10 7 7 7 8 10 7 10 10 10 10 10 7 7 8 8 10 7 10 10 10 10 10 10 10 10 10 10 10 10 10	2 10 7 7 10 3 9 8 10 8 7 9 10 10 10 7 8	2 10 9 6 10 4 10 7 10 10 10 7 8 10	□ p•° ∞ ∞ • d p• 		 	 p ● 0 ∞ ∞ p ● 0 ∞ p ● 0 ()	 • • • • • • • • • • • • •	= 0	□ early, fair day: $o \equiv^0$ at n : □ early, fine day & n : o a : • in p & at n : • early, c or o all day. p• early & a : c or bc p and n : [o • at n] p• early, b or bc a : cp• or op• p • early, op• to bc a : b or bc p and n : □ early, fine a : b to o p : o • o • o 0 o 0 o 0 o 0 o 0 o 0 o 0 o 0
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	St.: Ci. St.: Ci. St. St. Cu.: A. St. St. Cu.: A. St. St. Cu.: A. St. St. Cu.: Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. St. Cu. St. St. Cu. St. St. St. Cu. St. St. St. St. St. St. St. St. St. St	Cu.: Ci. St. Cu.: Cu. St. Cu.: A. St. St. Cu.: A. Cu. St. Cu.: Cu. St. Cu.: Ci. St. Cu.: Ci. St. Cu.: Ci. Cu.: A. St. St. Cu.: A. St. St. Cu.: A. St. St. Cu.: A. St. St. Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu. St. Cu. St. Cu.	St. St. Cu.: Cu. St.: A. St. St. Cu.: A. Cu. St. Cu.: A. Cu. St. Cu.	2 10 7 8 3 10 1 10 9 9 1 10 8 8 7 10 10 5 7	1 10 9 8 46 1 9 8 10 2 10 10 7 10 10 7 5 6 10 6 1	1 10 8 7 46 2 10 7 10 10 10 10 7 4 9 5 8 4	2 10 7 7 7 8 10 7 10 10 10 10 10 10 10 10 10 10 10 10 10	2 10 7 7 10 3 9 8 10 8 7 9 10 10 7 8 8 8 9 10 10 10 10 10 10 10 10 10 10 10 10 10	2 10 9 6 10 4 10 7 10 10 7 8 10 10 1 9 1 10 10 9 1	□ 		 	 p ● 0 ∞ ∞ p ● 0 ∞ () ∞ 	 	= 0	□ early, fair day: $o \equiv^0$ at n : □ early, fine day & n : o a : o in p & at n : o early, coro all day. po early & a : cor bc p and n : [o o at n] po early, b or bc a : cpo or opo p early, opo to bc a : b or bc p and n : □ early, fine a : b to o p : o o o p : n : o early, o or c with ∞ all day. ∞ a and p , variable sky: o at n : o early & a : coro p : o, some o n : c to opo early, o o n and n : opo early, o o n and n : c to opo a: o o n : o o o o o o o o o o o o o o o o o o o
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	St.: Ci. St.: Ci. St. St. Cu.: A. St. St. Cu.: A. St. St. Cu.: Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. St. Cu. St. St. Cu. St. St. Cu. St. St. Cu. St. St. St. Cu.: Cu. St. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: A. St. St. St. Cu.: A. St. St.: A. St. St.: A. St. St.: A. St. St.: St. Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu.	Cu.: Ci. St. Cu.: Cu. St. Cu.: A. St. St. Cu.: A. Cu. St. Cu.: Cu. St. Cu.: Ci. St. Cu.: Ci. St. Cu.: Ci. St. Cu.: Ci. St. Cu.: A. St. St. Cu.: Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu.	St. St. Cu.: Cu. St.: A. St. St. Cu.: A. Cu. St. Cu.: A. Cu. St. Cu.: A. St. St. Cu.: A. St.	2 10 7 8 3 10 9 9 1 10 8 8 8 7 10 6 3 9 7 8 5 10 6 10 10 10 10 10 10 10 10 10 10 10 10 10	1 10 9 8 4 6 1 9 8 10 10 7 5 6 10 6 1 8 10 10 10 10 10 10 10 10 10 10 10 10 10	1 10 8 7 4 6 2 10 7 10 8 10 10 10 7 4 7 6 5 10 10 10 10 10 10 10 10 10 10 10 10 10	2 10 7 7 7 8 10 7 10 10 10 10 10 10 10 10 10 10 10 10 10	2 10 7 7 10 3 9 8 10 8 7 9 10 10 7 8 8 9 2 5 10 10 10 10 10 10 10 10 10 10 10 10 10	2 10 9 6 10 4 10 7 10 10 7 8 10 10 1 9 1 10 9 1 10 9 10 10 9 10 10 10 10 10 10 10 10 10 10 10 10 10]				 	= 0	□ early, fair day: $o \equiv^0$ at n : □ early, fine day & n : o a : ● in p & at n : ● early, c or o all day. p● early & a : c or bc p and n : [o ⊕ at n] p● early, b or bc a : cp or op p ● early, fine a : b to o p : o o o o o o o o o o
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Mean cloud	St.: Ci. St.: Ci. St. St. Cu.: A. St. St. Cu.: A. St. St. Cu.: Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. St. Cu. St. St. Cu. St. St. Cu. St. St. Cu. St. St. St. Cu.: Cu. St. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: A. St. St. St. Cu.: A. St. St.: A. St. St.: A. St. St.: A. St. St.: St. Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu.	Cu.: Ci. St. Cu.: Cu. St. Cu.: A. St. St. Cu.: A. Cu. St. Cu.: Cu. St. Cu.: Ci. St. Cu.: Ci. St. Cu.: Ci. St. Cu.: Ci. St. Cu.: A. St. St. Cu.: Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu. St. Cu.: Cu.	St. St. Cu.: Cu. St.: A. St. St. Cu.: A. Cu. St. Cu.: A. Cu. St. Cu.: A. St. St. Cu.: A. St.	2 10 7 8 3 10 9 9 1 10 8 8 7 10 10 5 7 7 10 6 3 9 7 8 10 10 7 7 7 8 10 10 10 10 10 10 10 10 10 10 10 10 10	1 10 9 8 4 6 1 9 8 10 10 7 5 6 10 10 10 7 7 2	1 10 8 7 4 6 2 10 7 10 8 10 10 10 10 10 10 10 10 10 10 10 10 10	2 10 7 7 7 8 8 10 7 10 10 10 10 10 10 10 10 10 10 10 10 10	2 10 7 7 7 10 3 9 8 10 10 10 7 8 8 9 2 5 10 10 10 10 10 10 10 10 10 10 10 10 10	2 10 9 6 10 4 10 7 10 10 10 7 8 10 10 10 10 10 10 10 10 10 10 10 10 10]				 	= 0	□ early, fair day: $o \equiv^0$ at n : □ early, fine day & n : o a : ● in p & at n : ● early, c or o all day. p● early & a : c or bc p and n : [o ⊕ at n] p● early, b or bc a : cp or op p ● early, fine a : b to o p : o o o o o o o o o o

374. Cahirciveen (Valencia Observatory).

Cloud Forms.

Day.

		Cloud Forms.					Amo		t			Wea	ther.			Remarks.
Day.	7h	13h	18h	7h	9h	131	151	18	h 21 h	7h	9h	13h	15h	18h	21h	Remarks.
1 2 3 4 5	St. Cu. : A. St. St. Cu. St. St. St. A. Cu. : A. St. : St.	St. Cu. : Cu. St. Cu. : Cu. St. St. Cu. : Cu. St. Cu. : A. Cu.	St. Cu. : Cu. : A. St. St. Cu. : Cu. St. : A. St. St. Cu. St. Cu.:F.Ci.		8 8 10 10	7 8 10 8 8	5 7 10 10	5 4 10 10	7 10 10	 ≡° •°≡°	 •°≡°	 =0 			≡° ≡° 	Cloudy a : fair p : $o \equiv^0 n$: $b \supseteq early$, c a to fair p : c n : $\equiv^0 early$, o a , p and n : some $\equiv^0 p$ and n : $o \bigoplus^0 \equiv^0 early$, o all day, \bigoplus^0 late a : $\supseteq early$, cloudy, $p \bigoplus$ late a :
6 7 8 9 10	St. St. Cu. St.: St. Cu. St. Cu.: Cu.: A. Cu. St. Cu.: Cu.: Cu.	St. Cu. Cu. St. Cu. St. Cu. : Cu. St. Cu. : Cu.	St. Cu. : A. St. St. Cu. : Cu. St. Cu. : Cu. St. Cu. : Cu.	10 3 10 8 6	3 9 7 8	3 8 8 8	10 1 7 7 10	8 	1 1 6	•°≡° p•	•°	 p•		() •	 •	o
11 12 13 14 15	St. Cu. : Cu. St. St. Cu. St. Cu. : A. St. St. Cu.	St. Cu. : Cu. : A. Cu. St. Cu. St. : A. St. St. Cu. : Cu.	St. Cu. : Cu. St. St. Cu. St. : A. St. St. Cu. : Ci. Cu.	7 10 8 8 7	8 6 7 10 7	7 10 6 10 4	7 10 10 10	7 10 9 10	9 5 8	 p♠ p●° p●	 p● 	 p● 	 •	 p● p●	p●▲ p●	p igoplus early, cloudy with $p igoplus day$, b to opq cp $igoplus early$ & $a: p igoplus p$ and $n:$ $p igoplus early$, o to fair $a:$ bc to $op:$ bc $n:$ $p igoplus a$ and $p:$ cloudy $n:$ b to o with $p igoplus early$ all day.
16 17 18 19 20	St. Cu. : A. Cu. St. Cu. St. : St. Cu. St. : A. St. St. : A. St.	St. Cu. St. Cu. : A. St. St. Cu. St. Cu. : A. Cu. : A.St St. Cu.	St. Cu. : A. St. St. : A. St. St. Cu. St. : A. St. St. Cu.	7 8 7 10	5 8 6 9 10	8 8 7 9	8 8 6 10	8 10 8 10	10 10	 P● 		()			 p●⁰ •	op $lacktriangle$ early, bc to c day, o at n : 'op $lacktriangle$ early, cloudy day, o at n : $[p lacktriangle n$ op $lacktriangle$ to bc early & a : bc () op $lacktriangle$ c op $lacktriangle$ early, o all day, $lacktriangle$ at n : o $lacktriangle$ early, overcast all day.
21 22 23 24 25	St. : A. St. St. St. St. Cu. St.	St. Cu. St. St. Cu. : Cu. St. Cu. : A. St. St. Cu.	St. St. St. Cu. : Cu. St. Cu. : A. St. St. Cu.	9 10 10 8 10	8 10 6 8 10	8 10 3 10 8	10 10 2 10 7	10 5 10 7	10 5 10	 ●°≡° 	 • p•°	•••		• ° · · · · · · · · · · · · · · · · · ·	 •°≡°	o ● early, c in $a : p \bullet \& \bullet p : o at n :$ o ● 0 = 0 or o ● early & $a : op \bullet to o \bullet p $ op ● early, fair to fine day op ● early, c to o day, o ● 0 = 0 n : o ● 0 early, o to c with p ● day : bc n :
26 27 28 29 30	St. Cu. St. Cu. St. Cu. : Ci. St. St. Cu. St. Cu. : Ci. Cu.	St. Cu. Cu. St. Cu. : Cu. Cu. : A. Cu. : A. St. St. Cu. : A. St.	St. Cu. St. Cu. St. Cu. : A. Cu. Cu. : A. Cu. : A. St. St. Cu. : A. St.	8 9 7 4 8	8 9 7 4 3	8 5 3 4 10	5 7 3 2 10	7 3 4 2 10	3 1 2	p● 	 80 	•••		p ● °	8 : :	c to be with $p igoplus day : o at n :$ op $igoplus early, o to be a : cp igoplus to bp : b n :$ b to $c \infty a : b$ or $be p \ and n :$ Fair or fine all day. b to $o \ a : o$ with $\infty p \ and n :$
31 Mean Cloud	A. Cu.	Cu.	Cu.	2 7·8	2 7·5	<u>3</u>	7.2	1-	$\frac{2}{37\cdot 2}$		8		8			Fine with ∞ all day.
375	. Cahirciveen (\	/alencia Observato	ory).	1	1	1	,	1	1							June, 1923.
1 2 3 4 5	St. : A. St. A. Cu. St. St. St.	St. Cu. Cu. : A. Cu. Fr. St. : Ci. St. St. Cu. : Cu. St.	St. Cu.: A. Cu. St. Cu.: A. Cu.: A. St St. Cu.: Cu. St. Cu.: A. St.	9	5 1 6 8 10	8 4 8 7 10	9 7 9 6 10	9 - 8 4 8	6	88 € : :	 8 8 8 	: : ⊕ 8 8	: : ⊕88	8 8	8 8 : : :	Fair $a: 0$ or $c p: fair n: \infty all day.Fine a: fair p \ and n: \infty all day.o \equiv^0 early, bc \infty a: c or op \ and \ n: \oplus p: p \bullet early, o or c \ a: bc \ p \ and \ n: p \bullet early, o or c all day.$
6 7 8 9 10	St. Cu. : A. St. St. St. St. St. St. : St. Cu.	St. Cu. : A. St. St. : A. St. St. : St. Cu. St. St. : St. Cu.	St. Cu. : A. St. St. St. : A. St. St. St. Cu.	10 10	10 8 10 10	10 10 9 10 7	10 8 10 6	10 10 10 6	10 10	 ≡ ⁰ p•0	 ●°≡° ≡°	 • =° 	 ≡°	 ≡ ⁰ ● 	 ≡°	o or c all day, some ∞ a : $p \bigoplus^{0} \text{ early, c or o } a : \text{ op } \bigoplus \equiv^{0} \text{ to o } p : \text{ o at } n$ o with \bigoplus or $\bigoplus^{0} a : \text{ o or c } p \text{ and } n :$ $o \equiv \bigoplus^{0} \text{ early, o with } \equiv^{0} \text{ all day.}$ op $\bigoplus^{0} \text{ early, c or bc all day.}$
11 12 13 14 15	St.: St. Cu. St. St. Cu. St. St. Cu. St. Cu.	St. Cu. : Cu. St. : A. St. St. : St. Cu. St. Cu. : Cu. St.	St. Cu.: A. St. St. St. Cu.: Cu. St. Cu.: A. St. St.	9 10 10 8 10	8 10 10 8 10	4 10 8 4 10	5 10 6 4 10	8 10 7 10	10 8 10	 =0 =0	 ≡° •°≡°		 •°≡° 	 ≡° 	 ●°≡° ≡°	o to be early & a : fair p : o at n : c or o a : o $\equiv^0 \bigoplus^0 p$ and n : o with $\bigoplus^0 \equiv^0 a$: c to be p : c at n : c to be a : b to o p : o $\equiv^0 n$: [c at n] $\equiv^0 \& \equiv \text{early}, \equiv^0 \text{ with } \bigoplus \text{ or } \bigoplus^0 a$: $\bigoplus p$
16 17 18 19 20	St. St. Cu. St. St. Cu. : A. Cu. St. Cu.	St. Cu. Cu.: St. Cu. St. St. Cu. St.Cu.: Ci.Cu.	St.: St. Cu. St.: A. St. St.: A. St. St. Cu. St. Cu.	10 10 10 5 7	9 8 10 6 7	8 8 10 1 7	8 10 8 1 7	9 10 10 1	10	p●° ≡°				 ≡° 	 ≡° ≡° 	$p igodetilde{igodeta}^0$ early, o or c all day. o to bc a : c or o, some $\equiv p$: $o \equiv^0 n$: $\equiv \& \equiv^0$ early, o or c day: \equiv^0 at n : $o \equiv^0$ early, bc or b a : fine p and n : Fine early, cloudy day, o n :
21 22 23 24 25	St. St. St.: St. Cu. St. Cu. St. Cu.	St. St. Cu. St. St.: St. Cu. St. Cu.: A. St.	St. St. Cu. St. : St. Cu. St. Cu. St. Cu. : A. St.	10 10 10	10 9 10 10	10 7 10 10	10 8 10 10	10 9 9 9	10 10	≡° 	●°≡° 	 	•		≡º 	Dull day with $lacktriangle$, $lacktriangle$ $lacktriangle$ $a: p \leftilde$ $p: \equiv^0 n$ \equiv^0 early, dull day. c or o all day. Overcast all day. Overcast all day.
26 27 28 29 30 Mean	St. St.: St. Cu. St. Cu. St.: St. Cu. St.: A. St.	St. St. Cu. : Ci. St. St. Cu. : A. St. Fr.St. : St.Cu. : A.St. St.	St. Cu.: A. Cu.	8 2 10 10	10 8 9 10	10 7 10 9 10	8 7 9 10 10	. 8	10 8 10 2	≡º 	=° 	 =0	 =0		::: ::: :::	o with some $\equiv^0 \& \bigoplus^0 a$: o to b p : o at n o early, cloudy day, o at n : o to b early, c or o day. Overcast all day. o in a : o with $\equiv^0 \& \bigoplus^0 p$: fine n :
Mean Cloud Am'nt				8.8	8.5	8 · 2	8.2	8.	8.7	<u> </u>						
Day.	7h	13h	18h	7h	9ћ	131	151	18	h 21 h	7h	9h	13h	15h	18h	21h	Remarks.

Cloud Amount (All Forms).

Weather.

July, 1923.

,	,															July, 1923.		
F.		Cloud Forms.					Amo					Wea	ther.					
Day.	7h	13h	18h	7h	9h	13h	15h	181	21h	7h	9h	13h	15h	18h	21h	Remarks.		
1 2 3 4 5	St.: St. Cu. St.: A. St. St. St.: St. Cu. St.: A. St.	St. Cu.: A. St. St.: A. St. St. Cu.: A. St. St. Cu.: A. St. St. Cu.: A. Cu.	St.: St. Cu. St.: A. St. St. Cu.: A. St. St. Cu.: A. St. St. Cu.: A. St.	10 10 10 8	10 10 10	10 10 9 10 8	10 10 7 10	10 10 8 8	10 10 8 8 7	 •° 					=0 	bc early, o all day with \equiv^0 at n : o all day, some \bigoplus $\&$ \bigoplus in evening. \bigoplus 0 $\&$ \bigoplus early, o or c day, bc to c n : c or o all day. o with \bigoplus or \bigoplus 0 \equiv 0 a : o \bigoplus 0 \equiv 0 p : cloudy n :		
6 7 8 9	A. Cu. : A. St. St. St. Cu. St. : St. Cu. St. Cu. : Cu.	Cu.: A. Cu. St. St.: A. St. St. Cu. St. Cu.	St. : A. Cu. St. : St. Cu. St. St. Cu. : A. Cu. St. Cu. : Cu.	8 10 8 10 7	7 10 8 7 4	4 10 10 8 3	1 10 10 7 3	3 10 10 4 4	3 10 10 5 2		 •°≡° 	 	∞ •°≡°	∞ •	∞ •°≡°			
11 12 13 14 15	A. Cu. St. St. Cu. St. St.	Cu.: A. Cu. St. Cu.: Cu. St. Cu. St. Cu. St. Cu. St. Cu.	A. Cu.: A. St. St. Cu.: Cu. St. Cu. St. Cu.: A. St. St. Cu.	2 10 1 2 10	2 8 1 1 10	2 6 1 6 10	6 3 - 9 10	5 2 1 10 10	6 2 2 9 10	Q •°≡° •		 =0	 •°			\triangle early, fine a : fair p and n : b to $o \bullet^0 \equiv^0$ early, c or bc a : b p and n : A very fine day. \triangle early, b a : bc to $o p$: o n : o all day, \bullet or $\bullet^0 a$ and p : $\equiv^0 p$: o at n :		
16 17 18 19 20	St. Cu. St. : St. Cu. St. Cu. St. St. St.	St. Cu. : A. St. St. Cu. : Cu. St. Cu. : A. St. St. St.	St. Cu. : A. Cu. St. Cu. : Cu. St. Cu. : A. St. St. St.	8 9 7 10 9	8 7 8 10 10	7 10 10	7 7 8 10	6 8 10 10	8 8 10 10 8	 •		•••	 ≡°	 •°≡°	 •°≡°	o to b early, c or o with $p igoplus^0 a$: o to be $p igoplus early, o or c a: bc or b p: c at n: bc to o a: c or o p: o at n: o all day, igoplus \& \equiv^0 a: o \& \equiv^0 p: igoplus^0 \equiv^0 n: o all day, igoplus^0 \equiv^0 a: \& early p: c at n:$		
2I 22 23 24 25	St. Fr. St.: St. Cu. St. St. St.	St.: St. Cu. St. Cu. St. St. St. St. St.	St. : St. Cu. St. Cu. St. Cu. St. Cu. St. St. Cu.	10 10 10	10 9 10 10 10	10 10 10 10 8	10 10 10 10	10 8 10 8	10 3 10 8	 •° 	 •0 =0 	 = =0 	 =0 	 =0 	• ° ≡ °	o all day, \equiv^0 late $p : \bigoplus^0$ at $n :$ [o $n :$ o all day, $\bigoplus^0 \equiv^0$ early, $p \bigoplus^0 \& \bigoplus^0$ evening o $\bigoplus a : o \bigoplus^0 \equiv^0 \& o \equiv \text{to } o p :$ fair $n :$ b to $o \equiv^0$ early, $o \equiv^0$ all day with \bigoplus^0 at $n :$ o $\bigoplus^0 \equiv^0 \& p \bigoplus$ early, o $a : \text{c or bc } p \text{ and } n :$		
26 27 28 29 30	St. Cu. St. St. St. Cu. St. Cu. St. Cu. St. Cu.	St. Cu. St.: St. Cu. St.: Cu. St.: Cu. St.: A. St.	St. Cu. St. : A. St. St. : Cu. Cu. St. Cu.	10 7 10 10	8 10 6 10	8 10 9	7 10 8 10 7	7 10 5 6 3	10 9 10	•	 •°	 •° p•			•≡° 	Cloudy all day, o at n : oallday, \bullet at times $a: p \bullet or \bullet^0 \equiv^0 p$ and n : c to be with $p \bullet a: fair p: o n:$ op \bullet early, $o \bullet a$ and p with $\bullet^0: o n:$ $p \bullet early, o \bullet to op \bullet a: c to b p: o at n: [p: cp \bullet n:$		
Mean Cloud Am'nt		St. : St. Cu.	St. Cu. : Cu.	$\frac{7}{8 \cdot 5}$	<u>9</u> 8·2	8.2		1	7 7 7 8	P●	p●			•••		b to cp $lacktriangle$ early, op $lacktriangle$ or c a : cp $lacktriangle$ to		
377	. Cahirciveen (\	/alencia Observat	ory).		1	1		1			1	1	1		1	August, 1923.		
1 2 3 4 5	St. Cu. : Cu. St. St. Cu. : A. Cu. St. : St. Cu. : Cu. St. : Cu. : Cu.	St. Cu. : Cu. St. St. Cu. : A. Cu. Cu. : A. Cu. Cu.	St. Cu.: A.St.: A.Cu. St. Cu.: A. Cu. Cu.: A. St. St. Cu. Cu.	4 10 7 8 10	9 10 7 8 9	6 10 4 6 6	7	7 6 7 9 2		•≡° 	 =0 	•			 =0	\triangle early, b to op \blacksquare a : bc or c p : o n : o with \blacksquare $\& \equiv^0 a$: op \blacksquare to bc p : o n : op \blacksquare early, c to b a : fair p : c n : cloudy a : bc to op: o at n : o \blacksquare early, o to bc a : bc or b p : b $\equiv^0 n$:		
6 7 8 9	St. St. St. St.: A. St. St.: A. Cu.	St.: A. St. St. Cu.: A. Cu. St. St. Cu.: Cu. Cu.: A. St.	St. : A. St. A. St.: A. Cu. St. St. Cu.: Cu. A. Cu.	10 10 10 7 6	10 10 10 8 6	10 6 10 7 1	10 8 10 8 3	10 7 10 7 3	10 10 10 9	:: ≡° ::d	● =0 	 =0 		● ● 0 = 0 	● =0 	bc to o early, $o \oplus a : o \text{ to } o \oplus p : o \oplus n :$ $\bullet \circ \equiv \circ \& \oplus \text{ early, o to bc } a : c p : o n :$ $o \equiv \circ \text{ with } p \oplus a : o \oplus \text{ to } o p : o \oplus \& \equiv \circ n :$ $o \oplus \equiv \circ \text{ early, c to b } a : c p : o n :$ $\bullet \text{ early, fine to cloudy day o } n :$		
11 12 13 14 15	A. Cu. : A. St. St. St. St. : St. Cu. : A. Cu. St. Cu. : Ci. Cu.	St.Cu.: Cu.: Ci.Cu.	St. St. Cu. St. Cu.: A. Cu. St.Cu.: A.Cu.: A.St. St. Cu.	7	6 10 10 8 7	8 10 10 7 5	7 10 6 7 5	10 10 4 7 8	10 10 10 9 5	4 •°≡° •	 ●°≡° 	 ●°≡° 	 •°≡° ()	() •°≡° ···	 •°≡°	\triangle early, c or bc a : ctoo \bigcirc ^{0}p : o \bigcirc 0 to o n : o \bigcirc 0 \equiv 0 all day. o \bigcirc \bigcirc early, o \bigcirc \bigcirc a : o to bc p : o at n : \triangle early, cloudy a : c to bc p : o at n : \triangle early, o to bc a : bc () or c () p : fair n :		
16 17 18 19 20	St. : A. St. St. : St. Cu. St. : St. Cu. Cu. : St. Cu. St.	St. Cu. : A. St. St. : St. Cu. St. : St. Cu. St. Cu. St. Cu.		10 8 9 5 10	9 8 8 10	8 8 10 10	7 8 10 10	10 9 10 10	10 10 10	p● 		() p•⁰ 	() 	• p • • ≡ °	p ● °	bc to op \bigoplus early, o () $p : o \bigoplus n$: o \bigoplus early, op \bigoplus to \subseteq a: c to op \bigoplus $p : p \bigoplus^0 n$: op \bigoplus early, o or c a: op \bigoplus^0 to c $p : o$ at n: o to bc early, o a and $p : o \bigoplus^0 \supseteq^0 \& o \bigoplus^0 n$: o $\bigoplus^0 \supseteq^0$ early, o to $\bigoplus^0 \supseteq^0$ a: o, some $\bigoplus^0 p : o n$: [op $\bigoplus^0 p : bc n$:		
21 22 23 24 25	St.: St. Cu. St. Cu.: A. Cu. St. St.: St. Cu. St.: St. Cu. St.: A. St.	St. Cu. : Cu, St. Cu. : Ci. Cu. St. Cu. : A. Cu. St. Cu. St. Cu.	St.: St. Cu. St. Cu.: A. Cu. St. Cu.: A. St. St.Cu.: A.Cu.: A.St. St.: A. Cu.	8 6 10 7 10	7 2 10 9 10	6 3 5 7 10	5 7 5 9	8 3 9 4 5	6 6 8 2 10	 • • •	 P•°		•	p● 		o \bigoplus \bigoplus early, \bigoplus or \bigoplus \bigoplus : be to \bigoplus early, fine \bigoplus : c to \bigoplus be \bigoplus : be to \bigoplus early, o to be \bigoplus : c or \bigoplus and \bigoplus : op \bigoplus early, o to be \bigoplus : be \bigoplus : be early, o with \bigoplus \bigoplus : o \bigoplus to be \bigoplus : be \bigoplus :		
26 27 28 29 30	St. : A. St. St. Cu.	Cu. St. : A. St. St.Cu.: Ci.Cu.: A.Cu. St. Cu. : A. St. St. Cu.	St. Cu. St. Cu.	7 7 5 10 5	9 8 10 4	7 10 6 8 2	9 6 7 6	6 7 7 6 7	7 8 8 1 9	 •	 p• p•°	 p● 	p ● p • · · · · · · · · · · · · · · · · · ·	 p•	 p● 	bc to o with $p \oplus$ all day. c to o with $p \oplus$ all day. cp \oplus to bc early & a : bc p : c n : o \oplus to c a : cp \oplus to bc p : fine n : Mainly b or bc but some cp \oplus p : o n :		
31 Mean Cloud Am'nt	St. : St. Cu.	Cu. : St. Cu.	St. Cu.: A. Cu.	<u>7</u> 8∙o	<u>7</u> 8·4	7.2	5 7·3	6 7·2	5 2 8 · 1							op ● early, bc to cp ● a : bc p : c to bc n :		
Day.	7h	13h	18h	7h	9ћ	13h	15h	181	21 h	7h	9h	13h	15h	18h	21h	Remarks.		
,.	Cloud Forms.						Amo		:		I	Wea	ther.	1	1	С ещалас.		

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		Cloud Forms.		(Clou (Al		Amo orm:					Wea	ther.				
Day.	7h	13h	18h	7h	9h	13h	15h	18h	21 h	7h	9h	13h	15h	18h	21h	Remarks.	
1 2 3 4 5	St. Cu. : A. Cu. Cu. St. : St. Cu. St. : A. St. St. : Fr. St.	Cu. : Ci. Cu. Cu. St. St.Cu.: A.St.: A.Cu. St. : St. Cu.	Cu. Cu. St. St. Cu. : A. Cu. St. : St. Cu.	8	8	5 3 10 7	7	10 5	4 10 10 2 10	 	 () •° 	 () • 	 () •	() () 	() 	\triangle early, bc to cp \bigcirc a : b () p : bc n : \triangle early, bc () to b () day, o at n : \triangle early, o \bigcirc all day, o \bigcirc \bigcirc at n : o \bigcirc \bigcirc early, c day, fine n : Fine early, o or c day & n :	
6 7 8 9 10	St. St. St. : A. Cu. St. St. Cu.	St. St. Cu. : Ci. St. Fr. St. : St. Cu. St. St. Cu. : Cu.	St. St. Cu. : Ci. St. St. Cu. : St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.: Ci.St.	10 1 8 10 1	6	4 8	4 9	4	10 - 10 9 3	•°≡° •°≡° 	● ⁰ ≡ ⁰ p ● ⁰ • ⁰ 	●≡° •°≡°	● ≡° • ° ≡° ()		• ° · · · · · · · · · · · · · · · · · ·	$ \begin{array}{l} \circ \bullet^0 \equiv^0 a : \circ \bullet \equiv^0 \text{ to o } p : \circ \bullet^0 n : \\ \circ \bullet^0 \equiv^0 \text{ early, op} \bullet \text{ to bc } a : \text{ bc } p : \text{ b } n : \\ \bullet \text{ early, fair } a : \circ \text{ or c } p \text{ and } n : \\ \circ \bullet^0 \equiv^0 \text{ early, o} \bullet^0 a \text{ and } p : \circ \text{ at } n : \\ \bullet \text{ early, bc to b } a : \text{ b } () p : \text{ b at } n : \end{array} $	
11 12 13 14 15	St. Cu.: A. Cu. St. St.: A. St. St.: St. Cu. St.: St. Cu.	St. Cu. St.: A. St. St.: A. St. Cu. St. Cu.	St.: St. Cu. St. St.: St. Cu. St. Cu.: Cu. St.: St. Cu.: A. Cu.	10 I 10 I 7			9 8 10 3 9	10	10 10 10 4 1	Q •°≡° ···	 •° 	() 		 p● p●°	• ° · · · · · · · · · · · · · · · · · ·	\triangle early, bc () a : coro p : $o \bullet o n$: $o \bullet to \circ o \bullet o = o a : o or \circ p \text{ and } n$: $o \bullet o \bullet o \bullet o = o a : o or \circ p \text{ and } n$: $o \bullet o \bullet o \bullet o \bullet o a : o \bullet o \bullet o \bullet o \bullet o \bullet o \bullet o \bullet o \bullet o \bullet o$	
16 17 18 19 20	St. Cu. St. St. Cu. St. : Cu. St. Cu. : Ci. St.	Cu.: A. St. St.: A. St. St.: St. Cu. St. Cu.: Cu. St. Cu.: A. St.	St. Cu. : Ci. St. St. : St. Cu. St. Cu. : Cu. St. Cu. : Cu. St. : St. Cu. : A. Cu. St.	10 I 9 10 I	8	8 7	4	9 10 3 7 10	6 9 2 7 10	p ● = 0 p • = 0 	 • • • • • • • • •	 p ● 	 	 p ● p ● 		op $lacktriangle$ early, cor bc a : cor o p : bc n : o $lacktriangle$ a: bc to op $lacktriangle$ p: o at n : op $lacktriangle$ to c a : c to b with p $lacktriangle$ p: b n : c or o with p $lacktriangle$ day, cloudy n : o to bc a : o to o $lacktriangle$ p: o at n :	
21 22 23 24 25	St. Cu. St. Cu. Cu. St.: St. Cu.: A. St. St.: St. Cu.: A. Cu.	St. Cu.: A. Cu. St. Cu.: Cu. St.: A. St. St.: A. St.	St. Cu. : A. Cu. Cu. : A. Cu. : Ci. Cu. Cu. St. : St. Cu. : Cu. St. : St. Cu.	9 9 10 I	7 5 0 1	3 7 0	3 2 10	7 2	10 10 1 10 7	 p● p● 		•	 		• ° · · · · · · · · · · · · · · · · · ·	o $a: o$ to bc $p: o \multimap^o n:$ op \bigoplus early, c or o to b with p \bigoplus day: o $n:$ o \bigoplus early, op \bigoplus to $a: c$ to b $p: b$ $n:$ \bigoplus early, o to o \bigoplus $a: o \bigoplus$ $p: o$ $n:$ bc to op \bigoplus $a: o$ or c to op \bigoplus $p: c$ $n:$	
26 27 28 29 30 Mean	St.: St. Cu.: A. St. St.: St. Cu. St. St.: St. Cu. Ci. St.	St.: A. St. St. St. Cu.: A. Cu. St.: St. Cu.: A. Cu. St.		10 I 9 I	0 I	7 1	10 1	10 10 2	10 10 10 - 10	 =0 	 =0 	• ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °			• ° = ° · · · · · · · · · · · · · · · · ·	o all day: $o igotimes {}^0 n$: o with $igotimes$ or $igotimes {}^0 a$ t times all day. $o \equiv^0 igotimes {}^0$ to $c \ a$: c or $o \ p$ with \equiv^0 : $o igotimes {}^0 a$: op $igotimes$ early, o or $c \ a$: c to $b \ p$: b n : Fine early to o in p : $igotimes {}^0 p$: o at n :	
Cloud Am'nt		_		8 · 2 7	9	7.6	7.3	7:3	7.2								
379.	. Cahirciveen (V	alencia Observato	ory).							I						October, 1923.	
1 2 3 4 5	St. Cu. St. Cu. Cu.: St. St. Cu.: Ci. St.	St. Cu. : Ci. Cu. St.Cu.: Ci.St.: A.Cu. St. Cu. A. Cu. St. Cu.	St. Cu. : A. St. St. Cu. : A. Cu. A. St. : A. Cu.	8 5	8	7 6	7	5	5 10 3 10 2	 p● •°≡°	 •°	 p● 	 p● 			op \bigoplus early, c or bc all day. o \bigoplus early, o or c all day, o $n : \bigoplus$ toh. o \bigoplus early, c or o with $p \bigoplus$ day, b $n :$ b to c $a :$ bc to o $p :$ o $n :$ o \bigoplus early, o \bigoplus to c $a :$ c to cp \bigoplus : [fine $n :$	
6 7 8 9 10	St. Cu. St. St. St. Cu. : A. St. St.	St. Cu. : A. Cu. St. St. St. Cu. : A. Cu. St. : A. St.	St.	10 I 10 I	0 1	0 1 0 1	10	10 10	10 10 10 10	 ∞ 	p ● ° = ° ∞	 ● ≡ 0 	 •° 	•	 ≡ ⁰ • ⁰ ≡ ⁰ 	op \bullet to c a and p : o at n : o \bullet o \equiv o a: o \bullet p: o \equiv o n : o ∞ to o \bullet a: o \bullet to o \equiv o p: o \bullet o \bullet o \bullet o \bullet o \bullet o \bullet o \bullet o \bullet o at o o in p : o \bullet at n :	
11 12 13 14 15	St.: A. St. St. Cu.: A. St. Cu. St. Cu. St. Cu. St. Cu.	St.: A. St. Cu.: St. Cu. Cu.: St. Cu. Cu.: St. Cu.: A. Cu. Cu. St. Cu.: A. Cu.	St.: St. Cu.: A. Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. St. Cu.: A. Cu.	9 8 7	8 7 3 3	3 7	8 6 8 5 6	8 5 6 5 7	9 5 1 1 5	 p• 		≡° 	 0 	 0 0		o to o p	
16 17 18 19 20	St. Cu.: A. St. St. Cu.: St. St.: St. Cu. Cu.: St. St. Cu.: A. St.	St. Cu. St. St.: St. Cu. Cu.: Ci. Cu. St.: St. Cu.	St. : St. Cu. St. St. Cu. : A. St.	10 I 10 I 5	3	0 1 0 1	10 1	10 10	10 10 10 7 10	 =0 0 	 =0 	 ≡° 	 ≡° •° 		●° • ≡°	corop	
21 22 23 24 25	Cu.: A. St. Cu.: A. St. St. Cu. St. Cu.: A. St. St. Cu.	St. Cu. St. Cu. St. Cu. St. Cu. : A. St. St. Cu. : Cu.	St.: St. Cu. St. Cu.: A. Cu. St. Cu.: A. Cu. St. Cu.: A. St. St. Cu.: Cu.	7 10 9 I	7	7 3 8	3	7 4 8	10 10 5 7 10		 A [\$\z	•° P▲		 p● 	 p●	o	
26 27 28 29 30	Cu. Nb. : St. Cu. St. Cu. Cu. : St. Cu. St. St. St. Cu. : Cu. : Ci. Cu.	St. : A. St. St. : St. Cu. St. Cu. St. Cu. St. St. Cu.: A. Cu.	St. Cu.: A. St.	10 I 7 10 I	0 9 0 1	9 1	10 8	6	10 8 7 10 3	p ● =0 •	 •° 	 •	• p•0	• p • ≡ °	 ≡º 	o to b with $p \oplus a : o \oplus p : o \oplus to o n$: $o \oplus to c a : op \oplus p : o or c n$: $o \oplus to c a : op \oplus to b c p : b c to o n$: $o \oplus a \ and \ p : \equiv^0 \text{ in } p \& \text{ at } n : \bigoplus^0 \text{ at times } n$: $o \oplus \text{ early , fair } a : b \text{ to } cp \oplus p \ and \ n$:	
Mean Cloud Am'nt		St. Cu.	St. Cu.: A. St.	9 8·7 7	· 8			8·1	_					•••		cp igoplus early, o or ca: bc to op: on:	
	7h	13h	18ь	7h	9h	3h	15h	18ь	21 h	7h	9h	13h	15h	18h	21h		
Day.		Cloud Forms.			loue (All							Wear	ther.			Remarks.	
	l			<u></u>	(2 = 11			٠,٠									

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}		Cloud Forms.				ud . Il F			:			Wea	ther.			
Day.	7h	13h	18h	7h	9h	13h	15h	18h	21 h	7 ^h	9h	13h	15h	18h	21h	Remarks.
1 2 3 4 5	St. Cu. St. Cu. St. St.; St. Cu. Cu.; St. Cu.	St.: St. Cu.: A. Cu. St. St. Cu.: A. St. Cu. St. Cu.: A. Cu.	St. Cu. St. St.: St. Cu. St.Cu.: A. Cu.: A. St. St. Cu.: A. Cu.	10 10 10 8 8	9 10 10 5 8		10 10 5 7 6	3 10 8 8 8	4 10 8 6 10	 =0 	 p • ° p • ° 	 b⊕₀ 	•	 p• p•	 • ° p•	o to bc $a: o \oplus to b p: bc to op \oplus n:$ bc early, $o \oplus a$ and $p: o \oplus on:$ $o \equiv o$ early, $op \oplus a: cp \oplus to bc p: cp \oplus n:$ $op \oplus to bc day, bc to op \oplus n:$ $op \oplus \Delta to bc a: b() to cp \oplus p: op \oplus n:$
6 7 8 9 10	Cu.: St. St. St. St. St. St. St. Cu. St.	Cu. St.: A. St. St.: St. Cu.: A. St. St. Cu.: Cu. A. Cu.	St. : A. St. St. : A. St. St. Cu. : A. Cu. St. Cu. St. Cu.	4 5 10 10	3 10 10 5 3	3 10 10 5 7	3 10 10 6 9	10 10 3 3 10	10 8 2 1 8	:: p • d	 p● 	() 	() • ···	p● ≡º		op \bigoplus early, b() $a:b()$ to op \bigoplus $p:o \bigoplus$ to c n op \bigoplus early, bc to o $a:o \bigoplus$ $p:\bigoplus$ & $\bigoplus_0 n:$ op \bigoplus a and $p:b$ to op \bigoplus $n:$ bc to cqp \bigoplus $a:b$ ct ob $p:b$ $n:$ b \bigoplus to c $a:c$ or o with \equiv o $p:o$ \equiv o to c n
11 12 13 14 15	St.: St. Cu. St. St. St. St. St. Cu. St. Cu.	St. Cu. St. St. St. Cu. : Cu. St. Cu.	St. St. St. St. Cu. : A. St. St. Cu.	10 10 10 8 2	10	10 10 10 3 4	10 10 10 7 3	10 10 7 5 2	10 10 10 1 4	≡° ≡° •≡° 	 ● 0=0 p●	=0 ●=0 ●=0 	∞ •=0 •0=0 ···	● 0 = 0 ● = 0 	p	$0 \equiv^{0} a : 0 \text{ with } \equiv^{0} \text{ or } \infty \text{ p: } 0 0 0 \equiv^{0} n :$ $0 \oplus^{0} \equiv^{0} a : 0 \oplus^{0} p : 0 \oplus^{0} \equiv^{0} n :$ $0 \oplus \equiv^{0} a : 0 \oplus \equiv^{0} \text{ to } c p : c \text{ to } o p \oplus n :$ $0 \oplus \triangleq^{0} \text{ to } b a : p \triangleq \text{ to } b p : b \text{ to } c p \oplus n :$ $0 \oplus^{2}, bc, cpq \triangleq^{0} a : cp \triangleq^{0} \text{ to } b p : op \text{ to } bc n$
16 17 18 19 20	St. Cu. St. Cu. Cu. St. Cu. St. Cu.	St. Cu. St. Cu. : A. St. Cu. : A. St. St. Cu. St. Cu. St. Cu.	St. St. Cu. : Nb. St. Cu. St. Cu. St. Cu. St. Cu.	8 10 6 6 8	7 8 6 6 5	5 9 8 7 5	7 5 7 4 10	7 7 3 10	10 10 3 2 7	 p●⁰ p●	 P●º	 p● p▲	 P ^	● p▲	• p •	op \bigoplus early, c or bc a : bc to \bigoplus p : o n : c or o with p \bigoplus nearly all day. bc or c with p \bigoplus & p \bigoplus day, b to op \bigoplus n : bc to op \bigoplus a : cp \bigoplus to b p : b to cp \bigoplus n : bc to o all day with p \bigoplus \bigoplus \bigoplus \bigoplus \bigoplus \bigoplus \bigoplus \bigoplus \bigoplus \bigoplus
21 22 23 24 25	Cu. : St. ————————————————————————————————————	St. Cu. : Cu. : A. Cu. Cu. A. Cu. A. Cu. St. Cu. : A. Cu. St. Cu. : A. Cu. St. Cu. : A. Cu.	St. Cu. St. : St. Cu. St. Cu. 	6 - 1 - 9	2 1 1 2 3	3 - 2 3 8	7 - 1 9	5 2 1 - 9	I - -	ננננ:	ננננ:		p ● ° · · · · · · · · · · · · · · · · · ·	() p•	 	cp ⊕ early, fine a : b to cp ⊕ p : b □ n : b □ a : fine p : fine with □ n : b □ early, fine day, b □ at n : b □ a : fine p : fine with □ & \equiv ^{0}n : □ early, bc to op ⊕ all day, op ⊕ n :
26 27 28 29 30	Cu.: A. St. St.: A. St. St. St.	Nb. : St. St. : A. St. St.Cu.: A.Cu.: Ci.Cu. St. Cu. : Cu. A. Cu. St. : St. Cu. : A. St.	St.: St. Cu. St.: A. St. St.: St. Cu.: A. St. St. Cu.: St. Cu. St.	10 4 8 10 -	7 7	4 5	10 10 6 7	7 10 5 1	1 6 8 - 10	: - -	[8 [3	• 8	• 8 	:: 8 ::	≡° ∞ ⊔	o $lacktriangle$ early, o $a: o lacktriangle$ to bc $p: b \equiv^0 n:$ blearly, bc to o $lacktriangle$ at times $p: bc n$ c \equiv^0 learly, c or bc day with ∞ . o $lacktriangle$ early, c to b day, b $llocktriangle$ n: learly, b to o $a: o$ to o $lacktriangle$ $p: o$ at $n: llocktriangle$
Mean Cloud m'nt				6.7	6.6	6.7	7.0	6.3	5.7							
381.	Cahirciveen (V	/alencia Observato	ory).													December, 1923.
1 2 3 4 5	St. St. Cu. : St. St. St.	St. Cu. : A. Cu. Cu. St. Cu. : Cu. St. : A. St. St. Cu.	St. St. Cu. St. : A. St. St. St. Cu.		10 10 8 9	3	9	8	10 2 10 8 1	 p●⁰ 	 p• 	 P ^	 P _	•		o or c a : bc to o
6 7 8 9	St. Cu. St. St. St. St. St.	St. : A. St.	Fr. St. : St. : A. St. St. St. Cu. St. : A. St. St. : A. St. St. : A. St.	1 10 5 8 10	10 10 8	10 10 3 10	10 9 4 10	10 10 5	10 10 2 10 10	 • 0 	 p• 	 ● • 0 ≡ 0 p • 0		 p●° p●°	• 0 p • 0 	b \square early, $ca:op:o \bullet^o n$: o with \bullet or $\bullet^o a$: $ctoop \bullet p$ and n : o to b all day with $p \bullet$ or \triangle : bn : o \bullet^o early, $bctooa:op \bullet p:on:$ o early to $op \bullet a$ and $p:oatn:$
11 12 13 14 15	St. Cu. St. St. St. St. St.	St.: St. Cu. St. St. Cu.: Ci. Cu. St. St. Cu.	St. St. St. St. St. Cu.	8 10 1 10 10	9 10 2 10	8 10 2 10	10 10 2 10 8	10 2 10	10 1 10 10		 • ° 	 ● ⁰ ≡ ⁰	 ● ≡ ⁰ 	 •≡° 	 •≡° 	o or c all day with $lacktriangle$ 0 at p : $o \equiv$ 0 all day with $lacktriangle$ 0 a & $lacktriangle$ p and p : Fine all day, \equiv 0 at p : \equiv 0 early, o all day with $lacktriangle$ late p : A dull day.
16 17 18 19 20	St. St. St. St. St.	St. St. Cu. St. Cu. St. Cu. : A. Cu. St. Cu. : Cu. : Cu. St. Cu. : Cu. St. Cu. : Cu.	St. St. St. St. Cu. : A. St. St. Cu. : Ci. Cu. St. Cu. : Ci. Cu. St. Cu. : Ci. Cu.	10 10 5 5 2	10 9 10 9 7	10 8 7 7 7	7 7 7 7	10 10 6 6 7	10 10 9 8	● 0 ≡ 0 ● 0 ≡ 0 ≡ 0 	●°≡° ●°≡°	•••		 	p ● 0 ● 0 = 0 ∞	$0 \bigoplus_{i=0}^{0} a : 0 p : \text{op} \bigoplus_{i=0}^{n} n :$ $\bigoplus_{i=0}^{0} \text{or } p \bigoplus_{i=0}^{n} a : \text{cloudy } p : \bigoplus_{i=0}^{0} m :$ Some $\equiv_{i=0}^{0} \text{early}, 0 a : c \text{ or } b c p : 0 n :$ bearly, 0 or c to bc $p : c \text{ or } o n :$ bearly, c $a \text{ to } o \infty n :$
21 22 23 24 25	St. St. Cu. St. : St. Cu. St. St. St.	St. St. St. Cu. : Cu. St. St.	St. St. St. St. Cu.: A. St. St.: A. St. St. St.	10 9 5 10 10	10 10 5 10	10 10 7 10	10 9 10	7 10	10 10 10	 ≡° ≡° •°≡°	● 0 = 0 ● 0 = 0 ● 0 = 0		● ≡ ⁰ ● 0 0 0 0	 	=0 00=0 0	o
26 27 28 29 30	St. Cu. : A. St. St. : Cu. St. : Cu. St. : Cu. St. Cu.	St. St. St. Cu. : Cu. St. Cu. : Ci St.	St. St. St. Cu. : A. St. St. St. Cu.	10 10 5 10	10 8 10 9	10 10 7 10 8	10 6 10 8	10 8 10 8	10 10 7 10 4	 ≡° •°	 •• ••	•	• • • • • •	• •°≡°	P●0 ≡0 	
or Mean loud	St.	St.	St.	10 7·9	9.0	8.1	10 8·7	10	8.5		=0	_=0	<u>=</u> 0	<u>● º</u> = º	<u>●≡</u> 0	$o \equiv^0$ all day with $\bigoplus^0 p$ and n :
m'nt	7h	13h	18h	<u> </u>	<u> </u>	1	<u> </u>	<u> </u>	21h	<u> </u> 	gh .	13h	15h	18h	21h	
Day.		Cloud Forms.	1		Clo	ı ud	Amo	l	1		1	1	<u> </u>	<u></u>	<u> </u>	Remarks.

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M.O. 279 (Richmond)

Air Ministry METEOROLOGICAL OFFICE

OBSERVATORIES' YEAR BOOK 1923

Comprising the results obtained from autographic records and eye observations at the observatories at Lerwick, Aberdeen, Eskdalemuir, Cahirciveen (Valencia Observatory), Richmond (Kew Observatory), and Benson.

RICHMOND (KEW OBSERVATORY)

Published by the Authority of the METEOROLOGICAL COMMITTEE



LONDON:

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RICHMOND (KEW OBSERVATORY).

Latitude	on			51° 28′ N. 0° 19′ W. 12h Im.
Heights in Me	tres above	Sea L	evel.	
Barometer				10.4
Raingauge				5.5
Robinson Cup Anemograp	h			25
Dines Tube Anemograph	• •	• •	• •	25
Heights in M	etres abov	e Groun	nd.	
Thermometer Bulbs				3.0
Sunshine Recorder				
Robinson Cun Anemogran				20

INTRODUCTION.

20

Dines Tube Anemograph

SITE.

The Observatory was built in 1769 as the private observatory of King George III. Since 1842 it has been devoted to physics and meteorology. The meteorological records are continuous from 1854. The observatory is in the Old Deer Park, Richmond (Surrey), about 10 miles (16 km.) to the west of the City of London. It lies within a bend of the river Thames, which is distant about 300 metres on the north and west sides of the Observatory, and stands on a low artificial mound whose level is about 1½ metres higher than that of the surrounding park. Kew Gardens, which are extensively wooded, lie to the east-north-east, the nearest point of the Gardens being about 600 metres away. The town of Richmond, to the south-east, is about 1,100 metres distant. On the east side of the Park is the main road from Richmond to Kew. The Old Deer Park is mainly open pasture. Round the Observatory a golf course has been laid out. Another open area partly wooded, Syon Park, lies to the north-north-east across the river. Richmond Park is about 1½ miles (2½ km). to the south-east. For general views of the Observatory building and the exposure lawn, see Figs. 19 and 20. A site plan showing the arrangement of the various instruments is reproduced in Fig. 18.

METEOROLOGY.

The elements dealt with in the following tables are: atmospheric pressure, temperature, humidity, rainfall, sunshine, solar radiation, wind speed and direction, earth temperature, minimum temperature on the grass, level of underground water, and a diary of cloud and weather.

For brief descriptions of most of the instruments from which values of the above elements have been obtained and of the methods of tabulating the records, reference should be made to the General Introduction (pp. II-I8). The following notes supplement, where necessary, the information contained therein.

FIG. 18. SITE PLAN.

[To face page 286.

KEW OBSERVATORY.

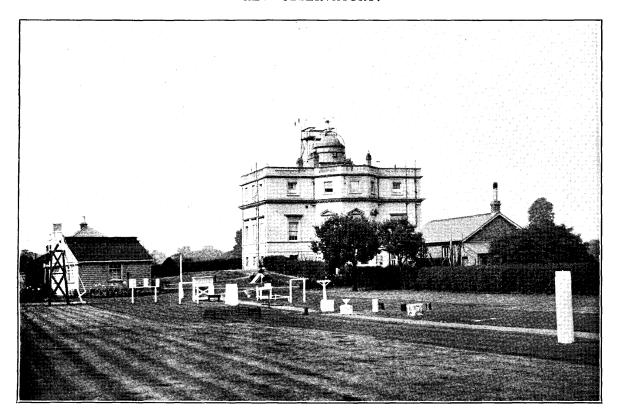


Fig. 19. General View showing Raingauges and Experimental Thermometer Screen on the lawn.

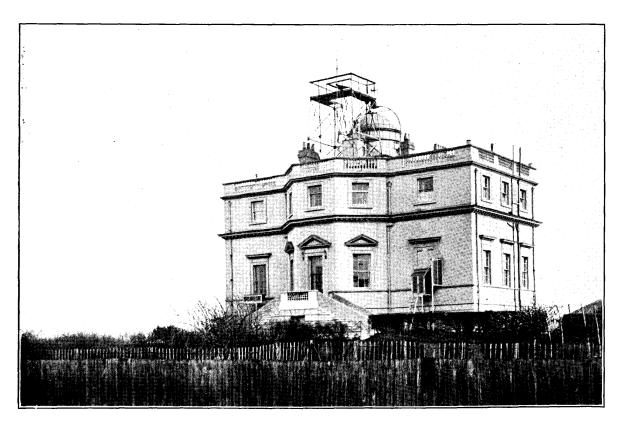


Fig. 20. View from North Showing North Wall Screen.

To face page 287.]

Notes on Instruments.

Pressure.—The barograph is mounted in the magnetograph room (in the basement of the Observatory) where the diurnal variation of temperature is very small. The barograph magnifies barometric changes in the ratio 1.553: 1, i.e. the change of ordinate equivalent to a change of 1 mm. in the height of the barometer is 1.553 mm. "Residual corrections," obtained from the control observations taken daily with the standard Newman barometer (No. 34) at 9h, 15h and 21h, are applied to the hourly The same correction is applied to all the readings on the same photographic sheet, i.e. generally for forty-eight hours. The individual entries published for the hours of the control observations may differ by 2 mb. from those observations. The Newman barometer is compared from time to time with the two large mercury barometers, which were set up in 1855 and 1860 and are still regarded as standards. A zero correction is based on these comparisons. A comparison, made in 1923, confirmed the correction +0.2 mb. (+.006 mercury inch) which has been applied for many years. Comparisons are made on the assumption that the value of the acceleration due to gravity is $g=981 \cdot 199$ cm./sec². This is the value given by pendulum observations. The departure from the value given for the latitude by Helmert's formula is insignificant. On a few occasions when a loss of trace occurred, the missing hourly values were derived from the Dines Float Barograph. cription of this instrument appears on p. 94.) There were twenty-eight hours in the year for which this was necessary.

Temperature and Humidity.—The thermograph is mounted in the West Room on the first floor of the Observatory. The thermometers are exposed in the screen attached to the north wall of the Observatory main building. This screen has single louvres and the bottom is open. There is an additional flat louvred screen which shields the main screen from direct sunshine when the sun is in the West and not The height of the bottom of the bulbs of the recording thermometers above the bottom of the sides of the screen containing them is 30 cm. in summer, 33 cm. in winter. The height of the bulbs above the top of the artificial mound on which the Observatory stands is approximately 3 metres; the height above the lawn where the raingauge is situated is approximately 5 metres. The scale values of the photographic records are not identical for the dry and wet-bulb curves. For the dry-bulb, tube No. 4 was in use and the scale value was I mm.=0.2715a; for the wet-bulb the old Falmouth wet-bulb tube (no number) was in use and the scale value was I mm. = 0.290a.

The control thermometers (dry 173971, wet 173969) which were graduated and mounted by Messrs. Negretti & Zambra in 1915 had been made and filled many years before and were therefore well seasoned. The National Physical Laboratory certificates dated 1915 give corrections to the nearest 0.05° C., the largest being 0.010. The thermometers are tested each January in ice. According to tests made in January 1923, there was no indication of any change of zero.

Control eye-readings of the standard thermometers are taken daily at 9h., 15h. and 21h. Residual corrections obtained from the control observations are applied to the hourly measurements of the curves. The same correction is applied to all the readings on the same photographic sheet, i.e. generally for forty-eight hours. The individual entries published for the hours of the control observations may differ by 0.3a from these observations. The larger departures refer to occasions when temperature is oscillating or changing rapidly.

When failure of the dry-bulb trace occurs recourse is had to the trace from the Callendar platinum-thermometer recorder, the thermometer of which is in the Northwall screen and adjacent to the mercury thermometers. Twenty-six hours had to be thus dealt with during the year. When the wet-bulb trace is missing or defective, the missing values are derived from the dry-bulb trace and the records of a hair hygrograph. The same procedure is always adopted when the wet-bulb reading is below 273a. 179 hours had thus to be dealt with during the year. The loss was

principally due to doubtful behaviour of the wet-bulb thermometer at temperatures near the freezing point of water. Humidity is determined from the dry and wet bulb readings by the table, based on Glaisher's factors, published in the Computer's Handbook.

It may be noted that during 1923, as in previous years, the temperatures published for Kew Observatory in the Daily Weather Report and elsewhere also refer to the North-wall screen. For the daily and weekly reports the readings of maximum and minimum thermometers exposed in that screen are utilised.

Rainfall.—As from January 1921, the standard raingauge for the Observatory has been an 8-inch gauge with the deep "Snowdon" funnel (M.O. 1271). The site is level and protected from wind, principally by hedges about $1\frac{1}{2}m$. high and distant 11 metres to East and 17 metres to West. The readings of this standard gauge are at 7h. and 18h. The hourly readings of the Beckley gauge are adjusted to give totals in agreement with the standard gauge.

Sunshine.—The sunshine recorder is mounted on the south parapet of the roof. The same frame (M.O. 12) has been in use since 1880 and it is believed that the ball has not been changed. The ball is now somewhat yellow.

Solar Radiation.—Observations are made with an Angström pyrheliometer, which measures the intensity of the direct radiation received from the sun by a surface which is normal to the sun's rays. The observations are made within half an hour of noon on all days except Sundays, provided that the sun is visible and not too much obscured by cloud, fog or thick haze. The conditions of the intervening atmosphere are indicated in Tables 440–451 in the column "sky." The amount of radiation is given in milliwatts per square centimetre in the column headed "total." For conversion to the unit more ordinarily employed abroad, the following relation may be used, Imw. per sq. cm. = 0.01435 gramme-calorie per sq. cm. per minute. The vertical component, i.e. the direct radiation received per square centimetre of a horizontal surface, is also given.

The Ångström instruments in use are by Rose, Stockholm. No. 100 was in use from January to April and from October to December; No. 24 from March to September. The ammeter is No. 68956, which was certified at the National Physical Laboratory in 1919. The black strips of Instrument No. 100 were renewed in September 1923. The readings are evaluated according to Ångström's original instructions. To bring the readings into accordance with the scale adopted by the Smithsonian Institution, a correction of 3.5 per cent. is required.*

Wind Speed and Direction.—The Robinson Cup Anemograph from which the results are mainly derived is exposed on the roof of the Observatory (see Fig. 19). This instrument has 9 inch cups; the radius of the circle described by their centres is 24 inches. The horizontal arms are 17.8 mm, wide; their vertical thickness is 4.6 mm, in the middle and 2.5 mm, at the edges. The oblique stays are rectangular in section, the dimensions being 6.3 mm. (facing the wind) and 3.8 mm. (facing upwards). The height of the cups above the lawn is 20 m. There are trees in the neighbourhood reaching greater heights. Those along the river to the West of the Observatory and about 280 m. away average 25 m.

Wind direction is taken from the Beckley vane. Direction is not tabulated when the speed of the wind averages less than 1.6 metres per second. Data missing owing to imperfections of the trace or other causes are replaced by results from the Dines tube anemograph, the head of which is approximately at the same height as the Robinson anemograph cups. The head of the new Dines instrument, set up at the beginning of the year, is of the Mark II pattern, No. 1017. In the vertical tube there are 80 holes in 4 rows of 20. The diameter of each hole is 3 mm. The connecting tubes, 17 metres long, have the internal diameter 12 mm. The recorder is M.O. 1017.†

Earth Temperature.—The thermometers in use were M.O. 5 at 30 cm. and M.O. 10 at 122 cm. The ground in which the tubes for the thermometers are sunk is under grass. The soil is gravel. The site is well exposed. There are, however, three fruit trees about 9 metres to the east and 6 metres high. The bulb of the lower thermometer is 430 cm. above sea level. As will be seen from Table 468, the surface of the underground water did not reach this level during the year, the limit being 319 cm. above sea level in March.

Minimum Temperature on the Grass.—The grass minimum thermometer is set at 18h and read at 9h on the succeeding day, the reading being assigned to the day of reading. The "grass minimum" thermometer in use was M.O. 9.

This thermometer has a spherical bulb, diameter 17 mm. The thermometer is placed with the bulb about 25 mm. above the turf. The exposure is good, there being no obstruction within 76° from the zenith.

Notes on the Meteorological Tables.

Pressure.—The highest and lowest of the mean daily values throughout 1923 were 1037·1 mb. on January 25th and 980·2 mb. on February 27th. pressure for February, 1001.83 mb., was abnormally low, and was nearly 20 mb. lower than the mean pressure for January, which was the month of highest mean pressure. Only one of the last II days of February had a mean pressure exceeding The range in the mean monthly diurnal inequalities in Table 395 varies somewhat irregularly from month to month, the largest range 1.64 mb. in October being more than double the lowest 0.70 mb. in June. As usual, the type of the diurnal variation differs widely in different months, but a double oscillation is easily recognisable in all months except August. The principal maximum appears in the forenoon in 7 months, but in the afternoon in 5, and in the year as a whole the maxima at 10h and 22h are equal. The principal minimum appears at 16h in the diurnal inequality for the year, and it occurs in the afternoon, between 14h and 18h, in all months except December, when it occurs at 6h. The differences between the different months and seasons are most clearly brought out by considering the Fourier coefficients calculated from the diurnal inequalities. The inequality is supposed to be given by the equivalent expressions—

$$a_1 \cos 15t^\circ + b_1 \sin 15t^\circ + a_2 \cos 30t^\circ + b_2 \sin 30t^\circ + \dots$$

 $c_1 \sin (15t^\circ + \alpha_1) + c_2 \sin (30t^\circ + \alpha_2) + \dots$

t being the time elapsed in hours since the first midnight of the day. The curves having being tabulated according to Greenwich time, the values of the Fourier coefficients, as originally calculated, referred to Greenwich time. In Table A, however, the phase angles really refer to local mean time, allowance having been made for the difference between Greenwich and local time. It has not been thought necessary to record here the values of the a and b coefficients, which remain available at the observatory for future use. In addition to the monthly values, of the c and α coefficients, there are values for the year as a whole, and for three seasons each of 4 months. Winter comprises January, February, November, December; summer the months May to August; and equinox the remaining 4 months. Arithmetic means are also given of the 12 monthly values of the c coefficients. In cases such as that of the 12-hour wave, where the variation in the phase angle throughout the year is small, the result from the mean diurnal inequality for the year gives an adequate idea of the real importance of the term. But when the variations of phase are as great as in the case of the 24- and 8-hour waves, the contributions from the different months to the mean diurnal inequality for the year cancel out to such an extent that a very inadequate idea is conveyed. If we formed arithmetic mean values of c_1 from the months composing the three seasons, the mean for equinox would be the largest, and the mean for winter would be 90 per cent. of that for summer. The summer value of c_1 owes its prominence merely to a less variability of phase angle. Great as the variability of phase is in the months of the other seasons, it is much less than it was in 1922. The winter value of c_1 is thrice, and the equinoctial value four times the corresponding value for 1922.

While the 12-hour term phase angle α_2 is much less variable than α_1 , it has a recognisable seasonal variation. As usual, the summer value is the lowest. The winter value of α_2 is unusually high. This is due to the high values of α_2 in November and January, and to the low value of c_2 in February. The equinoctial value of c_2 is a good deal higher than in 1922, but the winter value is lower, and the mean value for the whole year is but little higher than in 1922.

The phase angle α_3 has, as usual, a large comparatively regular annual variation. It is the transition during April and September, between the high values of α_3 in winter and the low values in summer that leads to the very low values of c_3 in these two months and in the equinoctial season. The value of c_3 in the mean diurnal inequality for the year is three times as large as in 1922, but it still gives a very inadequate idea of the real importance of the 8-hour term.

The variations of α_4 are large and of a less regular character than those of α_3 , and they must be regarded as to a considerable extent accidental. The values of c_4 and α_4 for the equinoctial and summer seasons are fairly similar to those of 1922. But the winter value of c_4 is twice as big in 1923 as in 1922, and the summer value of α_4 in 1923 is larger by 120° than that of 1922. The latter fact is not very surprising in view of the cancelling out that occurs between the contributions from the different seasons to the yearly value of c_4 .

Table 396 records the highest and the lowest pressure for each day of the year. The highest pressure of the year, 1038·4 mb., was recorded on January 25th, and the lowest pressure, 976·1 mb., on February 22nd. Thus the range for the year was 62·3 mb. The largest range of pressure experienced in any one month was 45·8 mb. in October, the mean of the 12 monthly ranges being 37·6 mb. The mean daily range for each month is deducible from the values of the mean maximum and the mean minimum in the last line of Table 396. These mean daily ranges vary from 10·89 mb. in December to 4·31 mb. in July. Allowing equal weight to the several months, the daily mean range for the year is 7·28 mb. This is fully 9 times the range of the regular diurnal inequality for the year given in Table 395. This helps to bring out the smallness of the regular changes of barometric pressure as compared with the irregular.

TABLE A.

Diurnal Variation of Barometric Pressure. Fourier Coefficients.

Richmond (Kew Observatory), Longitude o° 10′ W.

Month or	Seaso	on.	c_{1}	α ₁	c_2	α ₂	c _s	α_3	c4	α_4
			mb.	0 /	mb.	•	mb.	0	mb.	•
January			•168	25 49	.287	165.4	•165	344	•069	222
February			.287	93 9	·178	149.9	.075	330	.024	64
March			·247	319 44	•385	152.9	.079	328	•040	11
April	• •	•••	•298	43 49	•393	152.6	·016	153	•051	332
May			•179	57 49	.315	145.3	·084	165	•030	335
June			.076	320 7	•303	135.0	.070	162	.013	50
July			.417	357 39	•326	138.7	•122	152	•005	177
August	• •	••	•573	359 49	.278	144.5	•204	III	.050	333 333 35177 300 351177 222 16.
September			.065	352 40	473	153.6	•019	219	∙060	358
October			·653	112 15	.384	151.9	.143	352	·02I	176
November			.201	81 51	•393	166.6	·180	360	.022	221
December	••	••	.422	173 9	•277	153.8	•240	349	•069	164
Arithmetic I	Mean		•299				•116		·038	
Year				50.70	.333	151.3	.042		∙008	
Winter	• •	•••	•145 •165	50 19 112 41	·329 ·282	160.5	.163	348	•032	189
Equinox	• • •		•170	71 6		152.8	.048	340	.031	352
Summer	• • •	::	.287	4 12	•409 •30 5	140.8	.110	138	.018	321

Note.—Winter comprises the four months, January, February, November, December.

Equinox the months March, April, September, October, and Summer May to August.

Temperature.—The highest and lowest of the mean daily values throughout the year were 299·3a (79°·3 F.) on July 12th, and 270·3a (27°·1 F.) on November 26th. The mean temperature of the representative day of the year was 283·01a (50°·0 F.).

Fourier coefficients were calculated from the inequality data, as in the case of barometric pressure. The amplitudes and phase angles are given in Table B. The small variation in the 24-hour term phase angle is emphasised by the smallness of the excess of the arithmetic mean value of c_1 over the value from the mean diurnal inequality for the year. The 24-hour term is the dominant one, especially in summer. Absolutely considered, the 12-hour term has its largest value in March, and the winter value is only very slightly in excess of the equinoctial. But relative to the 24-hour term, the 12-hour term is much more important in winter than in the other seasons. The annual variation in α_2 is considerably more marked than that in α_1 . The summer and winter 8-hour waves are nearly opposite in phase, and the arithmetic mean value of c_3 is more than double the value obtained for c_3 from the mean diurnal inequality for the year. The excess of the arithmetic mean value is even more pronounced in the case of c_4 . The differences, however, between the values of α_4 for the four equinoctial months are small, with the result that the equinoctial value of c_4 exceeds that of c_3 . In the case of individual months c_3 is usually considerably larger than c_4 , its excess being especially conspicuous in summer.

The highest temperature of the year, $305 \cdot 3a$ ($90^{\circ} \cdot I$ F.), was recorded on July 12th, and the lowest temperature, $267 \cdot 8a$ ($22^{\circ} \cdot 6$ F.), on November 8th. The range of temperature for the year was thus $37 \cdot 5a$ ($67^{\circ} \cdot 5$ F.). The largest range of temperature in any one month was $27 \cdot 0a$ ($48^{\circ} \cdot 6$ F.) in April, the mean of the twelve monthly ranges being $20 \cdot 0a$ ($36^{\circ} \cdot 0$ F.).

The mean daily range for each month is deducible from the values of the mean maximum and the mean minimum. These mean daily ranges vary from 10·0a in July to $5\cdot3a$ in February. Allowing equal weight to the several months, the mean daily range for the year is $7\cdot57a$ ($13^{\circ}\cdot6$ F.). This is only 46 per cent. larger than the range in the mean diurnal inequality for the year.

TABLE B.

Diurnal Variation of Temperature. Fourier Coefficients.

Richmond (Kew Observatory), Longitude o° 19' W.

Month o	r Seaso	on.	c_{1}	α_1	c ₂	α_2	c ₃	α_{3}	C4	α4
	·		a.	· ,	a.	0	a.	0	a.	
January			1.564	220 18	•545	36.6	153	222	•023	69
February			1.336	222 46	.628	32.3	.052	249	.111	161
March			2.331	220 44	• 703	38.5	.065	313	•067	194
April	••		2:877	226 22	.419	50.0	•093	39	·058	214
May			3.192	224 I	·o66	44.3	.270	28	.031	75
June			2.927	224 15	•097	145.3	187	46	•072	343
July			4.024	222 58	115	80·1	.315	30	-088	34
August	• •		4.005	222 55	•198	76.0	•432	21	.043	336
September			3.785	224 40	•620	45.6	.233	29	.167	206
October			1.884	238 5	• 58 5	60.2	.121	296	•129	184
November			1.665	219 35	•663	32.9	171	228	•035	258
December	••		1.107	228 21	•518	32.6	•175	192	•040	11
Arithmetic 1	Mean		2.958	••	0.430		0.189		0.072	••
Year			2.552	224 20	•405	44.6	∙086	15	•023	192
Winter			1.416	222 15	· 588	33.5	•130	217	•018	154
Equinox			2 · 706	226 35	•576	47.9	•096	15	•103	199
Summer			3.537	223 27	102	85·o	•297	29	•049	12

Relative Humidity.—The highest mean daily value of relative humidity was 96.7, a value experienced on January 17th and on November 1st and 25th, and the lowest 56.5 on July 7th. The highest mean daily value of aqueous vapour pressure was 21.6 mb. on July 11th, and the lowest 4.4 mb. on December 20th.

In the diurnal inequalities of relative humidity for the year as a whole, and for most of the individual months, only a single oscillation is visible in the 24 hours, the maximum occurring in the forenoon and the minimum in the early afternoon, but in a few months there seems to be a trace of a secondary minimum in the morning.

Rainfall.—As the irregularity of the figures in Table 412 shows, there is much that must be regarded as accidental in the hourly figures, even for a whole year. The greatest total hourly rainfall, 39.6 mm., occurred between 23h and 24h, but of this 23.5 mm., or 59 per cent., fell on a single day (July 9th), during an intense thunderstorm. In this one hour there fell nearly four times the total rainfall of the month of June. The total amount for the year, 638.2 mm. (25.1 in.), differs little from the normal. October, with a total of 135.4 mm. (5.33 in.), was much the wettest month of the year, and June, with a total of 6.4 mm., (0.25 in.) was much the dryest. The greatest rainfall in any one (Greenwich) day was 29.7 mm. (I.17 in.) on July 10th. But 28.7 mm. fell on the last two hours of July 9th, and during the night July 9th-10th there was a continuous fall of 52·1 mm. (2·05 in.). [This was the great storm which kept London awake all night. At Chelsea Mr. Spencer Russell registered nearly 7,000 lightning flashes in six hours.] Other large daily totals were 23.5 mm. on October 3rd, 21.6 mm. on October 12th, and 19.7 mm. There were 505.0 hours of rainfall in the year, so that the average on March 13th. rate of fall, when rain occurred, was 1.26 mm. per hour. This is very sensibly higher than the rate for 1922. The excess is to be ascribed to the high average rate of fall for July, viz., 3·25 mm. per hour. The average rate of fall for October, 1·79 mm. per hour is also high. On the other hand, the average rate of fall for June was only 0.75 mm. per hour. In February, there were only five days on which no rain was recorded, and in October, only seven. In June, though the total fall was so small, rain was recorded on nine days, or only one day less than in August, which had six times as large a total fall. August 2nd to August 14th (13 days) was free from rain, and so were the 12 days, June 27th to July 8th.

"Snow Lying" was registered at 7 h. on four mornings in December, the 20th, 21st, 22nd, and 27th. On December 22nd, after a prolonged fall of snow which had lasted from 11 h. 15 m. to 22 h. 30 m. on the preceding day, the depth was about an inch. No deeper deposit was recorded during the year.

Sunshine.—August, with a total of 247·0 hours of sunshine, 55 per cent. of the possible, was the sunniest month of the year; while December, with a total of 35·5 hours, 15 per cent. of the possible, was the least sunny. The longest duration of sunshine on any one day was 14·3 hours on June 23rd. The next longest duration, 14·1 hours, occurred on July 11th. On this occasion sunshine was continuous from 7h to 19h, and the same was true of July 13th. On the intermediate day, July 12th, sunshine was continuous from 6h to 18h. These three successive days between them had 40·3 hours of sunshine. Several days had a higher percentage of possible sunshine than June 23rd, the outstanding occasion being August 30th, with a percentage of 91. In the year as a whole there were 70 days in which no sunshine was recorded. Of these, 13 occurred in December, and 11 in each of the two months January and March. In July there was no single day wholly devoid of sunshine, and there were only two sunless days in each of the three months May, August and September.

Solar Radiation.—The highest value of the total radiation was 98.9 mw/cm.² on March 26th, the highest value of the vertical component being 73 mw/cm.² on May 16th.

Wind Speed and Direction.—February 27th, with an average speed of 9·3 metres per second, was the most windy day of the year, November 13th, with an average speed of 9·2 metres per second, being very little behind. At the other end of the scale, January 17th was credited with an average speed of only 0·1 metre per second. No sensible wind was recorded between 8h on the 17th and 4h on the 18th. The next lowest average daily speed was 0·6 metres per second on March 22nd and on November 26th. At low speeds, however, the effects of friction in the Robinson Anemograph are apt to be large and uncertain. The mean hourly speeds varied from 4·19 metres per second in February to 2·94 metres per second in September, the mean of the 12 monthly means being 3·44 metres per second.

On the average of the twelve months, the mean hourly values were as follows, the highest and lowest values being in heavy type:—

Hour	1h	2h	3h	4h	5h	6h	7h	8h	9h	10h	11h	12h	m/s
Velocity	2·80	2·66	2·69	2·64	2·77	2·74	3·13	3·27	3·67	4·07	4·44	4·37	
Hour Velocity	13h 4·63	14h 4·41	15h 4·46	16h 4·02	17h 3·97	18h 3·52	19h 3·37	20h 3·07	3·19	22h 2·95	23h 2·95	24h 2·68	m/s

For the twelve hours ending with 18h the mean velocity was 4.00 metres per second, as against 2.88 metres per second for the remaining twelve hours.

A new Dines anemograph was brought into use at the end of February. This instrument is provided with a larger vane and with a twin-lever direction recorder. The agreement between the Dines records and those of the Robinson anemograph was not so satisfactory as hitherto. A reason for this discrepancy, a defective joint in one of the connecting tubes, was found in May 1924. To allow for this, the estimates of wind speed given by the Dines instrument during 1923 have now been increased by 10 per cent. The "highest gust" of Table 465 refers to the amended figures. The other columns of the Table are, for this year, derived from the Robinson records.

It is to be noted that the corresponding tables in the Weekly and Monthly Weather Reports, 1923, require similar amendment.

Earth Temperature.—In examining the results it should be borne in mind that there is a very sensible diurnal variation of temperature at 30 cm. depth, the amplitude varying with the season; and, moreover, the mean value for the day does not occur at 9h, the hour when the earth thermometers are read. This is no doubt partly accountable for the irregular variation in the difference between corresponding monthly mean values of the air temperature and the temperature at 30cm. depth. The algebraic excess of the temperature at 30 cm. depth over the air temperature varies only from +1.4a in November to -1.7a in January. The diurnal variation of temperature at 122 cm. depth is very small, and the differences between the mean monthly temperatures at that depth and the corresponding air temperatures show a fairly regular progression throughout the year. The algebraic excess of the temperature at 122 cm. depth over the air temperature varies from +5.7a in November to -4.8a in July. The underground temperature is the higher in January and February, and from September to December. In March the two monthly means were identical, and in April very nearly so. In the year as a whole the underground temperature was the higher by 0.2a. At 30 cm. depth the highest and lowest temperatures recorded during the year were 294.5a on July 13th and 275 Ia on December 5th. At 122 cm. depth the highest and lowest temperatures were 288.8a on August 15th and 16th and 278.9a on January 26th, 27th and 29th. The absolute range for the year thus reduces from 37.5a (67°.5 F.) in the screen to 19.4a (34° · 9 F.) at 30 cm. depth, and to 9.9a (17° · 8 F.) at 122 cm. depth.

Grass Minimum Temperature.—The mean of the monthly means is 276·24a (37°·8 F.). The monthly mean fell below the freezing point of water in January, November and December, being only 271·1a in November. In the latter month the grass minimum temperature was below the freezing point of water on no less than 21 days, including the 22nd to the 30th inclusive. The highest mean monthly value, that for July, exceeds the lowest by only 12·9a (23°·2 F.). The grass minimum temperature did not fall to the freezing temperature of water between June 19th and August 30th, but July was the only month with no occurrence of so low a temperature.

Level of Underground Water.—Table 468 gives the mean daily value of the level of underground water and the highest and lowest levels attained during each month. The heights are reckoned from mean sea level. The level actually measured is that of the surface of water in a pipe which passes down through the floor of the basement into the ground immediately under the Observatory. The water level depends partly on the local rainfall, but mostly on the water level in the river Thames. The river close to the Observatory is tidal. The sluices at Richmond Lock, 800 metres south of the Observatory, are drawn up at half-tide and the flow of the tide is then unobstructed up to Teddington. The height of the river depends partly on the rainfall throughout the whole Thames Valley, and partly on the tides. A fortnightly fluctuation owing to the latter cause is sometimes recognisable in the records of the level of underground water.*

The general tendency in water level was upwards until the maximum 319 cm. was attained in March, then downwards to the minimum 173 cm. in September, and then again upwards. The level on December 31st was higher by 49 cm. than it was on January 1st, and the mean level for the year, 229 cm., was 31 cm. above the mean for 1922. In August, however, the mean level was identical with that of 1922, and the mean levels for September and October were slightly lower than in 1922. The position towards the end of the year was presumably largely due to the heavy rainfall of October.

Diary of Cloud and Weather.—As explained in the footnotes, observations are lacking at 15h on Sundays and a few other days. The last line in each monthly table gives the mean amount of cloud for each of the six hours of observation. The following mean data are derived from these:—

Mean Amount	of Cloud	from Six	Observation	Hours.
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Month	Jan.	Feb.	Mar.	Apl.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Cloud	6.8	7.8	8·o	7:3	7:4	8.1	5.9	5.6	5 ·8	7:3	6.5	7:3	7.0

Mean Amount of Cloud for the Year at the Six Observation Hours.

Hour	7h	9h	1 3h	15h	18h	2 1 h
Cloud	6.9	7.4	7.7	7.5	6.7	5.8

We see that June, though it had much the lowest rainfall, was the cloudiest month of the year, being closely followed by March. The least cloudy month was August, which had also the highest percentage of possible bright sunshine. August was closely followed by September and July. For the year as a whole 13h was a slightly more cloudy hour than 15h or 9h.

^{*} Graphs showing the fluctuations of water level during the years 1914 to 1921 were published in the Annual Supplements to the Geophysical Journal.

The use of the symbols \equiv and ∞ in the weather columns of Tables 469–480 is governed as far as daylight observations are concerned by the following conventions which are in accordance with the general practice adopted by the Meteorological Office.*

If the Orange Tree Inn, 1,000 metres S.E. of the Observatory cannot be seen there is fog \equiv . If trees 200 metres away cannot be seen, there is thick fog \equiv ².

If the Orange Tree Inn can be seen but not the chimneys of the Electric Power Station at Chelsea, 10 kilometres away, there is either mist \equiv^0 or haze ∞ , the distinction being made according to the relative humidity at the Observatory. On occasions when the humidity is 80 per cent. or above, the obscurity is attributed to mist; when the humidity is below that limit to haze.

The symbols are used at night to indicate as nearly as may be the same degrees of atmospheric obscurity.

ATMOSPHERIC ELECTRICITY.

The instruments in use throughout the year in connection with atmospheric electricity have been the Kelvin water-dropper and the Benndorf radium collector electrographs, the Kelvin portable electrometer No. 80, the electrostatic voltmeters Nos. 1684 and 1685, a Wilson universal electrometer No. 7960, and two Ebert aspiration instruments, Nos. 3327 and 2965.

The portable electrometer and the electrostatic voltmeters are used for converting the electrogram readings into true potential gradient in the open. The apparatus for the absolute observations consists essentially of a long insulated rod, carrying a lighted fuse at the end, connected to the electrometer or voltmeter. Readings are taken with the fuse at one metre and at two metres above the ground, the grass on which is kept short. The site is in the Observatory garden, as remote as possible from trees or buildings. If no change occurred in the position or environment of the water-dropper—the instrument the curves from which are regularly tabulated—a constant ratio might persist between the potential at the spot where the jet breaks into drops and the corresponding potential observed with the absolute instruments. But the assumption of a constant ratio is unsafe, and the practice is to calculate for each month a factor based on the absolute observations which are taken in the garden on all convenient dry days. Such factors are given in Table 482.

The data appearing in Table 481 include for each month the electrical character figure assigned from consideration of the potential gradient curve for each day. Of the character figures, o simply denotes the absence of negative potential, I implies the existence of negative potential at one or at more times during the day, but with a total duration of less than 3 hours, while 2 implies the existence of negative potential with a total duration exceeding 3 hours. There are few days on which the potential gradient curves do not show numerous short period oscillations, superposed on the regular diurnal variation. In fact the absence of such oscillations can usually be accepted as evidence of imperfect insulation in the electrograph. Thus character o does not connote the absence of irregular oscillations, as it does in the case of magnetic Still it is unusual on days free from negative potential to have the large rapid oscillations which usually accompany negative potential. The duration of negative potential and the amplitudes of the extreme negative voltages are much greater on some days of character 2 than others; and even in the case of character 1 the duration of negative potential may be anything from 1 or 2 minutes to 3 hours. Thus these numerals, and still more the monthly means of the character figures, have no precise physical significance. At the same time, the monthly mean character figure gives a fairly satisfactory idea of the greater or less prevalence of negative potential throughout the month. According to this criterion, February

^{*} The convention as to mist and haze was altered in April 1925.

showed considerably more negative potential than any other month. It contained 9 days of character 2, and only 7 of character 0. In calculating the diurnal inequality for this month use was made of several 24-hour periods which were not Greenwich days. At the other end of the scale was June, with a mean character figure of 0·30, there being 21 days free from negative potential. Taking the year as a whole there were 180 days, or 49 per cent., free from negative potential, while 152 were of character 1, and 33 of character 2. The mean character figure for the year, 0·60, is identical with that for 1922, and the numbers of days of characters 0, 1 and 2 in the two years are nearly identical.

Table 482 gives daily data derived from measurements of the electrograms taken with a mean value scale as in late years. They represent means for 60-minute intervals centered at the exact hours 3h, 9h, 15h, and 21h G.M.T. Blanks indicate that the trace was in some way defective. On some occasions the curve, though existent, is so oscillatory that no satisfactory estimate is possible of the mean value of the ordinate. Such occasions are indicated by the letter z. If there is no doubt as to the sign of the hourly mean value, though a numerical measure is unobtainable, the sign is indicated by a + or a - attached to the z. The symbol z \pm indicates that there were oscillations on both sides of the zero line, and that the sign of the mean value was uncertain. Occasionally a gap in the record from the Kelvin electrograph can be filled by reference to the corresponding Benndorf trace, but such occasions are rare.

The extreme hourly mean values in Table 482 are +1545 v/m at 9h on November 8th, and -995 v/m at 9h on February 21st. But much higher instantaneous values were recorded, and possibly even higher mean hourly values might have been obtained from the occasions when the trace was too oscillatory to be measured.

Of the two sets of mean monthly values at 3h, 9h, 15h and 21h given in Table 482 at the foot of each month's data, the first set (a) represents the arithmetic means of all the positive potentials in the column, the second set (b) represents the algebraic mean derived from all days on which all four hours were represented. The last line gives the mean value for each month as derived from the (a) and the (b) values, respectively.

For reasons explained in last year's Year Book, it is believed that the values (a) may be expected to give very approximately the true monthly mean from all days when negative potentials are excluded, while the values (b) may be expected to give very approximately the true monthly mean when negative potentials are included. But a reservation is necessary in both cases, for the highly oscillatory occasions such as are met with during thunderstorms have been omitted, and this omission may have a sensible effect.

If the monthly means in Tables 482 and 483 be compared, it will be found that the quiet day mean is the highest in nine months out of the twelve. In some of the nine months, especially April and March, its excess over the mean (a)—which always exceeds the mean (b)—is considerable; in others of the months, including February, September and November, the excess is trifling. In one of the remaining three months, December, the quiet day mean and mean (a) are identical. In the other two months, June and August, mean (a) is slightly the larger. For the year as a whole, allowing equal weight to the 12 months, the quiet day mean, the mean (a), and the mean (b) are respectively 318 v/m, 296 v/m, and 276 v/m. The corresponding results for 1922 were respectively 318 v/m, 293 v/m, and 271 v/m, so that here again there is extraordinarily close agreement between the electrical results for the two years.

The diurnal inequalities and the mean monthly and annual values in Table 483 are based on the curves of quiet days selected from those entirely free from negative potential. Other objects aimed at in the selection of the days are freedom from large irregular movements, absence of indications of inferior insulation in the electrograph, and the avoidance, so far as possible, of large non-cyclic changes. The quiet days numbered 10 in each month; but to complete that number in February it was necessary to include several 24-hour periods which did not commence at midnight.

Except in this case the non-cyclic change is given explicitly in Table 483, so that anyone who may desire to reproduce the figures as they were before the non-cyclic correction was applied can easily do so. In calculating the table the non-cyclic correction was invariably applied in the usual way. As already remarked, the mean values of the potential gradient from the selected quiet days are identical for 1923 and 1922, and there is even a close approach to equality between corresponding seasonal values. But the differences between corresponding individual months were mostly substantial and sometimes large. In December the 1923 mean was the larger by 80 v/m; in October and February it exhibited deficiencies of 81 v/m and 80 v/m. Thus the exact agreement of the two yearly means must be regarded as largely accidental.

All the seasonal diurnal inequalities show a well marked double oscillation. This is also conspicuous in the diurnal inequalities of most of the individual months, and is recognisable in all. In summer the morning and afternoon minima are The principal minimum occurs in the early morning in all the other seasons, and in every single month except July, August and September, when it occurs in the early afternoon. The principal maximum occurs in the forenoon except in the months of March, April and October, and the equinoctial season, when it occurs in In September the forenoon and afternoon maxima are equal. phenomena show a substantial difference from those of the previous year, when the principal maximum appeared in the afternoon in 7 individual months and even in the year as a whole. If the inequalities for the year and the seasons are compared with the corresponding inequalities for atmospheric pollution given in Table 485, a remarkably close similarity will be noticed in the hours of occurrence of the principal maximum and minimum. There are, however, substantial differences of The relative prominence of the forenoon minimum in summer, and of the forenoon maximum in the equinoctial season, is much greater in the case of atmospheric pollution than in the case of potential gradient.

Air-earth Current at 15h (Table 481).

To determine the current flowing from air to earth, the conductivity of the atmosphere at one metre above the ground is measured by means of the Wilson universal electrometer.* For calculating the conductivity at 15h, four observations, each giving the leakage from a charged plate in 5 minutes, are averaged. The product of the conductivity so determined and the potential gradient at 15h (as given in Table 482) is taken as the measure of the air-earth current. The conductivity is not observed during rain nor when the potential gradient is negative. Data are available for about half the days of the year 1923.

The conditions under which the air-earth current is measured are maintained as uniform as possible, but they differ from the conditions under which the vertical current passes from the air to the earth in the absence of the apparatus. The presumption is that the results obtained would require to be multiplied by a factor to represent the true air-earth current. The monthly mean of the observed values of the current varied from 1.07 in September to 0.52 in December in terms of the unit 1×10^{-16} ampère per square centimetre. Allowing equal weight to each month, the mean for the year in terms of the above unit is 0.77. Here again, there is very little difference from the corresponding value 0.74 found for 1922.

Ionic Charges at 15h (Table 481).

Table 467 also gives the volume-charges carried by such positive and negative ions (including all of the more mobile type) as are caught by the Ebert apparatus.† The observations extend over some 20 minutes near 15h, being simultaneous with the experiments with the Wilson electrometer.

^{*} Proceedings of the Cambridge Philosophical Society. Vol. 13, p. 184 (1906). † Physikalische Zeitschrift, Vol. 8, No. 8, p. 246 (1907).

Normally, two Ebert instruments are in use, one charged positively, the other negatively, the signs alternating from day to day.

During the first nine months of the year, the days when electric charge measurements were made only for ions of one sign were very few, and it was deemed best to derive the monthly means only from those days when ions of both signs But in the last three months the behaviour of only one of The charge given to it was + and - on the two Ebert instruments was reliable. alternate days. The result was that for a good many days there was a satisfactory result only for the charge of one sign, and to have omitted all these days would have reduced too much the number of days available. It was decided accordingly to utilise all the observations of the last three months in the monthly means. terms of the unit 1×10^{-16} coulomb per cubic centimetre, the mean monthly values of the positive charges varied from 0.83 in August to 0.34 in December; those of the negative charges varied from 0.70 in August to 0.23 in October. For the year, allowing equal weight to the several months, the means are 0.49 for the positive and 0.37 for the negative charges. These values are both a little less than the corresponding values for 1922.

ATMOSPHERIC POLLUTION.

Tables 484 and 485 give results derived from the Owens atmospheric pollution recorder or Air-filter No. 1.* The instrument is situated in the same building as the electrograph, and the level of the air it samples is about $1\frac{1}{2}$ metres above that of the adjacent ground. The weight of the pollution is not obtained directly, but is deduced from shade numbers 0, 1, 2, etc., assigned to the deposit left on filter paper through which a measured volume of air has been drawn. Shade number 1 answers to 0.32 milligrams per cubic metre, according to Mr. J. G. Clark's determinations.†

Table 484 gives mean hourly values derived from all the days of the month for which complete records were obtained. There were 292 such days in the year. The highest and lowest of these hourly values are in heavy type.

Table 485 gives diurnal inequalities derived from the data in Table 484 after the application of non-cyclic corrections. The principal reason for computing the diurnal inequalities was to facilitate comparison with the corresponding diurnal variations in barometric pressure and the potential gradient of atmospheric electricity.

Record was lacking entirely for a few days, and for the greater part of a good many other days, owing to defective behaviour of the apparatus. Of the days of complete record, November 26th was the dirtiest, the mean amount of pollution from the hourly values being 1·3 milligrams per cubic metre. The highest individual measurement on this day, applying to the four successive hours, 15h to 18h, was 2·6 milligrams per cubic metre. A like amount was observed at 10h and 11h on December 5th.

The mean value for the year, 0.305 milligrams per cubic metre, is only about 3/4ths of that for the previous year. Every month of 1923 except June and December showed a decrease as compared with the corresponding month of 1922. The January mean was only half that of the previous January.

The nature of the diurnal variation is most easily recognised in Table 485. A double oscillation is always recognisable, and it is usually well marked; but there is considerable variety in the hours of occurrence of the principal maximum and minimum. In the diurnal inequalities for the year as a whole, for the winter and summer seasons, and for eight individual months, the principal maximum occurs in the forenoon, most commonly at 9h, but at 8h or 7h in the case of three summer months. In the four remaining months and in the equinoctial season the principal

^{*}A description of the instrument is given in the Report of the Advisory Committee for Atmospheric Pollution. 4th Report, 1017-1018 (p. 20).

Pollution. 4th Report, 1917–1918 (p. 20).
† London, M.O. Report of the Advisory Committee for Atmospheric Pollution. 3rd Report, 1916–1917 (p. 20).

maximum occurs in the afternoon. The principal minimum occurs at midnight in July. In every other month and in all the season inequalities it occurs in the early morning, at an earlier hour in summer than in winter.

TERRESTRIAL MAGNETISM.

Absolute observations of declination, dip and horizontal force have been taken usually once a week. The instruments employed have been the Jones unifilar magnetometer with declination magnet K.O.90, collimator magnet K.C.1 and mirror magnet A.N, and the Barrow dip circle No. 33, with $3\frac{1}{2}$ -inch needles. In the absolute observations of horizontal force, deflections were made at three distances, 22.5, 30 and 40 cm., and values were calculated for the distribution constants P and Q from all the observations of the year. The values obtained of late years have been as follows:—

.020		•	Mean Value at 22.5, 30 and 40 cm.
Year.	P.	Q.	of $\log_{10} (r + Pr^2 + Qr^4)$
1919	+1.496	-1525	<u>1</u> .99958
1920	+0.971	—12 80	<u> </u>
1921	+0.272	-1054	<u>1</u> .99930
1922	+1.809	-1642	<u>1</u> ·99966
1923	+2.240	—1787	<u>1</u> ·99977

Values for earlier years will be found in the Report for the year 1920.* It will be seen that numerical increases in P and Q tend to neutralise one another, so that the effect on the value of H (horizontal force) of the fluctuations from year to year in the values of P and Q is less serious than might appear at first sight. A recent investigation tends to show that these fluctuations are more apparent than real, and it was decided—though with some hesitation—to employ mean values for P and Q, derived from the seven years 1917 to 1923. The reason for commencing with 1917 was the fact that an accident calculated to influence the values of P and Q occurred in 1916. The mean value thus obtained for $\log_{10} (1 + Pr^{-2} + Qr^{-4})$ was $\overline{1} \cdot 99955$. The difference between this and the mean value for 1922, which had been employed provisionally in the reductions of the absolute observations taken during 1923, represents a reduction of 2γ in the value of H.

The Adie magnetographs have remained in regular operation during the year. The scale value of the declination magnetograph remained as in previous years 1 mm. = 0.87'. Some special observations on the H magnetograph were made in January with a view to judging of the accuracy of the setting of the magnet. The theoretical position of that magnet is perpendicular to the magnetic meridian. In practice it is obvious that this ideal is seldom attained. The magnetic meridian is not a fixed but a varying direction; its extreme positions in the course of a magnetic storm may differ by more than 2°. It is subject, moreover, to a continuous change in one direction, owing to the secular change of D. The position of the H magnet is readily altered as desired by turning the torsion head. But frequent recourses to this practice is objectionable for several reasons. Fortunately in the case of an H magnet—the ideal position of which represents a maximum in the magnetic couple—a small departure from perpendicularity to the magnetic meridian is immaterial to the degree of accuracy, iy, usually aimed at. Even at the present high rate of the secular change in D, it requires five years for the magnetic meridian to alter 1°. As cos 1°0 is 0.9998, and sin 1° is 0.017, it is really unnecessary, so far as provision for secular change is concerned, to move the torsion head oftener than once in five years, especially if each time it is done the alteration anticipates the future by two or three years. During the building operations in 1913, the magnetograph was for a time in action in the "Experimental House," and before it was restored to the magnetograph room, chalk lines were laid out on the floor, representing the position at the time of the magnetic meridian. By making allowance for the secular change, these lines or lines derived from them

^{*} Hourly Values from Autographic Records, 1920, p. 54.

have served for all operations on the magnetograph since 1913. It was thought well on the present occasion to make sure that the line on the floor supposed to represent the magnetic meridian did really do so. In the presence of the magnetograph magnets, the magnetic moments of which are large, the laying down of an exact magnetic meridian in the magnetograph room is a difficult process. The meridian obtained with the help of the magnetometer Dover 140 was not identical with the line on the floor, but the difference was less than 20'. The position of the deflection bar during scale value determinations, which was always determined by reference to the lines on the floor, would thus appear to have possessed the necessary accuracy. The position of the H magnet itself seemed more in error than was expected from considerations of the secular change, and it was brought into a more correct position by turning the torsion head. Some unintended change seems to have occurred, because a few days later the scale value, which previous to the operations had been I mm. = 5.7γ , was found to be I mm. = 7.1γ . This was altered to I mm. = 6.3γ by altering the distance apart of the bifilar wires, movement of the torsion head in the direction opposite to that of the earlier change being required to bring the magnet perpendicular to the meridian. Determinations made later in the year showed no change of scale value.

The scale value of the vertical force (V) curves varied from 1 mm. = 11.7γ at the beginning of the year to 1 mm. = 10.7γ at the end of the year. The method of determining the scale values was that due to Broun, an auxiliary magnet being used to deflect the D and H magnets at the same distances and under like conditions, and similarly with the D and V magnets. The D, H and V magnets are alike in size and shape, and the deflection distances relatively large, viz., 85 cm. for H and D, and 75 cm. for V and D. The disturbance of the magnetic curves by artificial electric currents has been much as in the previous year. The publication of diurnal inequalities of D and H has thus been continued. As in previous years, a temperature correction of 3.1γ per 1° C. was applied to the readings of the H curves.

Particulars of the magnetic character of individual days on the international scale "o" (quiet), "I" (moderately disturbed) and "2" (highly disturbed), as contributed quarterly to Prof. van Everdingen, at De Bilt, for utilisation in the international lists, appear in Table 490. It also gives the number of days in each month to which the several characters were assigned, and the numerical mean of the character figures treated as if ordinary arithmetical quantities. As there is a wide range in the disturbance to which any one figure is attached, and an uncertain personal element in assigning the figure, the monthly means should be regarded as giving only a general indication of the disturbance prevailing.

While this is the case, the difference between the figures for 1922 and 1923 is so large as to put beyond a doubt the fact that the latter year was decidedly the quieter. Each month of 1923, with the exception of November, showed a smaller mean character figure than the corresponding month of 1922. The mean character figure for 1923 was less than two-thirds of that for 1922, and the number of days of character "2" in 1923 was less than half that for 1922. Judging by the mean character figure and the number of days of character 2, October was the most disturbed and August the quietest month of the year. Fifteen successive days, August 16th—30th, were judged of character 0, and no single day of the month was of character 2.

The following were amongst the most disturbed days of the year: March 24th, 25th; September 26th, 27th; October 15th, 16th. No disturbance, however, was of a very outstanding character.

At Kew Observatory, large disturbance in V is rare, and it never occurs without large disturbance in D and H; thus it is immaterial whether the V curves are considered or not when assigning daily character figures. But on individual occasions disturbance may be much more prominent in H than in D, and conversely. In allotting daily characters in the weekly chronicle prepared for Mining Engineers, D only is under consideration, whereas H is equally considered when assigning

characters for De Bilt. Also the object in view is different in the case of Mining Engineers. In their case the precise period of the day which is disturbed is of importance. Two-hour periods are dealt with, and when character 2 is assigned to a particular day, the periods during which the D curve has that character are particularised. The number of these disturbed periods at different hours of the day during 1923 was as follows:—

Hour	0-2h	2-4h	4-6h	6–8h	8-10h	10–12h	12–14h	14–16h	16–18h	18–20h	20-22h	22-24h
Disturbed occasions	6	6	3	0	0	0	I	3	6	7	7	6

This represents a total for the year of 45 occasions, i.e. 90 hours, considered highly disturbed, as compared with 322 hours in 1922. Of the 90 disturbed hours during 1923, October contributed 32 and September 24. March and May each contributed 12 highly disturbed hours and December 10. The remaining seven months contributed nothing, a very outstanding example of quiet conditions. The twelve hours, 4h–16h, contributed only 16 per cent. of the disturbed hours, as compared with 27 per cent. in the previous year.

The data for Mining Engineers are issued within a few days of the end of the week, so that the characters have to be settled for only a few days at a time, and D only is considered. A few August days, the characters of which had been assigned in the Superintendent's absence, were reconsidered, leading to a slight diminution in the number of o's assigned. Taking the revised figures, the days awarded characters 0, I and 2 numbered, respectively, 262, 92 and II, giving a mean character figure for the year of 0.3I, as compared with 0.65 for 1922.

Prior to 1919 diurnal inequalities were given only for the five international quiet days, and before taking the readings the curves were smoothed by hand. A change of procedure appeared desirable when D inequalities were prepared from all ordinary days (i.e. all days except those of character 2). Accordingly, all the curves are now measured with a mean value scale, the 60-minute intervals employed centering at exact hours G.M.T.

In all the inequalities the non-cyclic change has been allowed for in the usual way, i.e. by assuming it to come in at a uniform rate throughout the day. Particulars as to the size of the non-cyclic changes are given in Table 491. In addition to the results for 1923 there are data for the previous ten years, so far as available, so as to cover a complete sunspot period. Results for D' (the ordinary day declination) were available only from 1918. As usual, the non-cyclic changes in D' and D (i.e. the quiet day declination) vary irregularly from month to month. As is usual on quiet days, the non-cyclic change in H has a decided tendency to be positive, but two months, April and September, had small negative values. The mean value for the year, as a whole, is smaller than in any one of the previous ten years with the exception of 1914.

The diurnal inequalities of declination from ordinary days, i.e. all days except those highly disturbed, are given in Table 486. Of the II days omitted as highly disturbed, 8 occurred in the equinoctial months, 2 in a summer month (May), and I in a winter month (December).

The diurnal inequalities for D and H from the international quiet days are given in Tables 487 and 488. The international quiet days in 1923 had the following dates:—

January	• •	7	8	18	19	27	July	 5	14	15	21	24
February		9	12	13	2Í	23	August	 I	18	21	28	29
March		8	9	10	II	23	September	 7	8	1 6	21	22
April		2	5	17	26	27	October	 2	3	23	24	30
May					22		November	 5	\mathbf{I} O	15	20	25
June	• •	9	IO	17	18	24	December	 2	7	17	21	22

(19889)

The units employed in the inequality tables are 1' in D and 1 γ (1 \times 10-5 C.G.S. In the case of D the minus sign means that the magnet points to the east of its mean position for the day. Inequalities are given for each month of the year, for the year as a whole, and for three seasons defined as in previous years. maximum and minimum hourly values are in heavy type. There is, as usual, a distinct difference in character between the diurnal inequalities of D on quiet and ordinary days; the easterly deviation near midnight is decidedly smaller in the quiet days. difference is especially marked in the winter months. At that season the principal minimum (i.e. the easterly extreme) has a tendency to shift from the morning to the late evening hours. In Table 486 it occurs at 22h or 23h in the four winter months, whereas in Table 487 it occurs in the forenoon in every month of the year. January and December, it is true, the difference between the morning and evening minima on quiet days is very small. The time of the principal maximum is the same in Tables 486 and 487, in ten months out of the twelve; but in November and December, it is at 12h in Table 487, an hour earlier than in Table 486. maximum is at 13h in both Tables in all the other months, with the exception of June and July, when it is at 14h. The tendency in the maximum to be later in summer than in winter is recognisable in the seasonal inequalities.

As regards H, all the seasonal inequalities show a principal minimum at 11h, and this is true of eight individual months. Of the remaining months, two, August and September, have the principal minimum at 10h, and two, January and December, have it shortly after midnight. The principal maximum occurs at 10h or 18h in all the seasonal inequalities, and in eight individual months. Of the remaining months, three, July, August and September, have the principal maximum later in the afternoon, but one, March, has it at 7h. A double daily oscillation with maxima in the forenoon and afternoon is recognisable in most, if not all the months, and is comparatively prominent in all the winter and equinoctial months. In January, February and December, the excess of the afternoon over the morning maximum is not large.

Table 489 is intended to give a general picture of the chief magnetic phenomena of the year, and a survey of the phenomena for 1923 and the previous ten years, thus including an 11-year period. As we have just been discussing the diurnal inequalities, attention is first claimed by the ranges, A.D.'s, and non-cyclic changes. By A.D. (average departure) is meant the arithmetic mean of the 24 hourly departures from the mean of the day. It is a quantity which is less dependent than the range on the accident of how the times of maximum and minimum happen to lie relative to the nearest hour G.M.T. The data under D' relate to the declination from the ordinary days, those under D to the declination from quiet days. It will be noticed that while the D range exceeds the D' range in May and September, the A.D. is decidedly greater for D' than for D in these, as in all the other months of the year. influence of disturbance in increasing the amplitude of the regular diurnal variation is more conspicuous in the A.D. than in the range. Considering the extreme quietness of 1923, it is a little surprising to find the difference between the ordinary and quiet day inequalities so decided as it is. In the case of the mean diurnal inequality for the year, 1923 shows a decided decline in amplitude as compared with 1922 in all the ranges and A.D.'s, and this decline is clearly apparent both in the ranges and the A.D.'s in most individual months of the year. There are, however, exceptions to this, especially in the months of April, September and November. compared with the previous ten years, 1923 has the smallest range and A.D. in the case of D, and only slightly exceeds 1913 in the case of H. The range and A.D. in D in 1923 were only about 57 per cent. of the corresponding quantities in 1917, the year of sunspot maximum. For H, the range in 1923 was 63 per cent. of that for 1917, but in the case of the A.D., the percentage was only 52.

The data in the earlier columns of Table 489 are of interest chiefly in connection with the secular change. The data for D, H, N (north component) and W (west component) are derived from the hourly measurements of the curves of the

international quiet days. The values of I (inclination) are derived from the absolute observations corrected to the mean of the day. The values of V and T (total force) are derived by combining the values of I and H. The mean monthly values of D from quiet days exceeded that from ordinary days on the average by $0' \cdot 04$. The quiet day mean was the larger in seven months and the smaller in four, the two means being identical only in June.

Comparing the yearly means in Table 489, we see that the fall in D from 1922 to 1923 was 11'·5, as compared with 11'·1 in each of the two previous years. It is the largest annual change recorded since magnetic observations started at Kew. The average yearly fall for the ten years, 1913 to 1923, was 10'·0, as compared with an average of only 6'·4 between 1903 and 1913. The mean value found for H is the same as for 1922. The change in this element of late years has been small, but until the last year there has been a steady decline since 1913, amounting in all to 111 γ . Inclination shows a fall of 0'·6 since 1922. The change in this element of late years has been almost insignificant. The highest of the mean monthly values of H exceeds the lowest by only 5γ . This uniformity is due partly to H having been nearly stationary, and partly to the exceptional quietness of the year. After a large magnetic storm H is nearly always considerably depressed, and in a disturbed year this is almost certain to exert a considerable influence on several of the mean monthly values.

Every month shows a fall in D as compared with the previous month. It is this change that is responsible for the slow rise in N, and the large fall in W. Every monthly mean value of W is less than that of the previous month. Since 1913, W has fallen 546γ . The fall, 59γ , since 1922, is thus only a little above the average of late years.

The vertical component and the total force show a decided fall, as in recent previous years. The average annual falls in these elements since 1913 have been respectively 22 γ and 25 γ , thus the falls, 21 γ and 20 γ , since 1922, have differed little from the mean. Instrumental and observational uncertainties enter more into the values of V and T than into those of D and H, and are probably largely responsible for the irregularities apparent in the monthly values of the former elements and in their secular change.

Table 492 gives the mean yearly values of magnetic declination, inclination, horizontal force and vertical force for a number of observatories, the publications of which are received at Kew Observatory. Table 493 includes a few stations for which there were no data for years subsequent to 1920. It also completes gaps in the Pavlovsk, Pola and San Fernando data.

Results for 1923 were not to hand for a considerable number of stations. Judging by the data available, the fall of westerly declination throughout the northwest of Europe varied little from place to place, and was appreciably greater than for the previous year. If we take the eight stations, Eskdalemuir, Stonyhurst, Potsdam, De Bilt, Kew, Greenwich, Valencia and Val Joyeux, we find the mean fall of declination from 1922 to 1923 to be 11'.6, as compared with 11'.0 for 1921 to 1922. In the south-west of Europe the fall during the year 1922 to 1923 was somewhat less, the mean from the three stations, Coimbra, Tortosa and San Fernando, being 9'.5.

Potsdam showed in 1922 to 1923 a small rise of inclination, though somewhat less than in the previous year. The more westerly stations showed a fall, which though small, was on the average greater than in the previous year. The results obtained for the secular change of horizontal force in Western Europe were somewhat conflicting. There was a fall at Eskdalemuir, Potsdam, De Bilt, and San Fernando, but a rise at Stonyhurst, Valencia, Greenwich, Val Joyeux and Tortosa. No change was recorded at Kew. In all, or practically all cases, however, the secular change of horizontal force when algebraically considered was in excess of that for the previous year. At present secular change in inclination and horizontal force is so slow in Western Europe that small instrumental or observational defects might influence even the sign of the result.

SEISMOLOGY.

Table C, shown below, gives a résumé of the results obtained during the year from the Milne seismograph (No. 9) in the basement. The boom points north and south, so the instrument measures tilting in the east-west direction. Observations to determine the sensitiveness made on February 8th, June 29th, September 28th and December 19th, gave results in close agreement, the mean value found for the angle of tilt answering to 1 mm. ordinate on the trace being 0.53". Observations made on the oscillation period on these three occasions gave a mean of 17.3 seconds. In an instrument of this type it is difficult, if not impossible, to discriminate between the different kinds of waves, and there is often considerable uncertainty as to the time of commencement. Thus the information given in Table C is confined to the time of the largest movement and its amplitude. Numerical measurements are not given if the measured amplitude is less than 1 mm. The letters a, b, c denote amplitudes on an increasing scale, a representing an amplitude not exceeding 0.2 mm., b an amplitude of at least 0.2 mm, but less than 0.5 mm, and c an amplitude of at least 0.5 mm, but less than 1.0 mm. The amplitude is partly determined by the approach in the period of the earthquake wave to the natural period of the boom, but a large amplitude is never experienced unless the earthquake has been a really considerable one. The limit of registration, 17 mm., was exceeded on two occasions, viz., February 3rd and September 1st (the great Japanese earthquake), and on September 2nd a movement had an amplitude of 13 mm. The other movements of the year were comparatively small.

TABLE C.—SEISMOLOGICAL DIARY.

Maximum.

Richmond (Kew Observatory).

Maximum.

Maximum.

Times G.M.T.

Maximum.

Maximum.

1923.

Maximum.

	Maxii	num.		Maxin	iuii.		Maxin	ıum.		Maxin	uum.	Ì	Maxii	num.		Maxim	ium.
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Jan. 12 13 21 22 22 27	h. m. 3 I 10 38 4 26 1 38 9 46 8 44	mm. a b b a 4.5	Mar. 1 2 3 4 4 13 14 15 24	h. m. 9 17 17 53 23 6 0 47 8 21 20 40 21 55 5 50 23 23 13 26	mm. b 2.8 a b a c 2.3 I.0 I.9	May 1 4 4 30 30 31	h. m. 11 36 17 13 23 32 18 33 22 26	mm. a 2·7 b b b	July 2 10 13 14	h. m. 3 29 1 32 12 15 0 54	mm. c b 3:7	Sept. 1 1 2 2 2 9 11 14 16 17 21 26 30	h. m. 3 52 8 33 3 39 3 44 3 51 10 23 23 34 22 56 9 19 13 36 17 56 7 39 20 33 9 17 1 33	mm. >17.0‡ c 13.0 4.9 5.3 5.4 c c 3.0 a b b 1.7 b 1.2 3.3	Nov. 2 3 4 5 6 6 9 17 18 19 21 22 25 27 28	h. m. 23 00 17 18 1 30 22 27 18 27 20 17 4 13 3 53 22 28 3 59 14 15 8 21 17 39 4 19 0 47	mm. 1 · 4 1 · 7 b 3 · 9 b c b b l i b a b b b a b b
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Date.	Time.	Amp.	Date.	Time.	Amp.	Date.	Time.	Amp.	Date.	Time.	Amp.	Date.	Time.	Amp.	Date.	Time.	Amp.
Feb. 2 2 3 4 5 15 16 16 19 21 23 24 28	h. m. 1 57 6 1 ? 13 21 23 44 23 32 7 23 10 12 0 32 1 42 7 3 8 22 22 23	mm. c 2·5 >17·0* a b a a b b 5·9	Apr. 5 13 19 23 24 25 29	h. m. 23 7 16 21 4 13 4 10 22 47 20 13 9 56	mm. a 1.6 c 2.4 a a c	June 1 1 2 17 18 19 22	h. m. 18 18 21 14 2 4 18 15 9 48 23 25 7 34	mm. 3.9 c b a b a 2.9	Aug. 1 8 10 11 12 12 14 16 17 19 23 27 29	h. m. 5 29 13 24 2 52 2 6 7 1 10 59 18 4 21 21 2 8 13 41 6 19 12 14	mm. b a b c a b a b a b a b a b a b a b 3.3	Oct. 1 3 7 10 20 23	h. m. 8 56 16 54 4 37 7 23 4 5 16 47	mm. c a 25 5.4 b a	Dec. 5 5 20 27	h. m. 21 11 23 45 15 50 15 34	mm. 3.6 b a b

Limits of registration (17.0 mm.) exceeded from 16h 48m—16h 56m. Disturbance visible till after 22h 00m. Disturbances were recorded between May 5th and May 28th, but time marking arrangements failed. Limits of registration (17.0 mm.) exceeded at 3h 52m.

382. Richmond (Kew Observatory): H_b (height of barometer cistern above M.S.L.) = 10.4 metres.

January, 1923.

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384. Richmond (Kew Observatory): H_b (height of barometer cistern above M.S.L.) = 10.4 metres.

March, 1923.

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	26	023.2	023.0	023	023-1	023.2	023.3	023.3	023.4	023.4	023.4	023.0	022.6	022.2	012.9	012.5	021.2	021 · 1	021.0	021.1	021.4	021.5	021.2	021.0	021.1	022.3
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(Sea le	Rich	mond	Ke mb.	w Ok	oserva	itory)	: H	b = 1	10·4:	metro	es.	mb.	mb.	mb.	mb.	mb.	mb.	mb.] mb.	mb.	mb.	mb.	mb.	Apri	il, 19	23.
(Sea le	Rich	mond mb. o13·5 o18·7	mb. o13·3 o18·9	mb.	mb. 012.9	mb.	mb.	b = 1 mb. o13.9 o20.2	mb. 014·3	mb.	mb.	mb. 015·2 020·8	mb. 015·0	mb. 015·2 020·2	mb. 015·1 020·1	mb. 015·1 019·9	mb. 015·2 019·9	mb. 015·6 020·1	mb. 016·2 020·4	mb. 016·8 020·6	mb. 017·4 020·9	mb. 017·7 021·3	mb. 018·0	Mb. 018-4	mb. o18.8	mb. 015·2 020·2
(Sea le	Rich	mond o13·5 o18·7 o21·0	mb. 013·3 018·9 020·8	mb. 013.2 019.1 020.7	mb. 012·9 019·0	mb. 013.2 019.4 020.6	# H o13.5 o19.7 o20.7	b = 1 mb. 013.9 020.2 020.6	mb. 014·3 020·5	mb. 014.9 020.7	mb. 015·1 021·0 020·3	mb. 015·2 020·8	mb. 015.0 020.6 019.3	mb. 015·2 020·2 018·5	mb. 015·1 020·1 017·9	mb. 015·1 019·9 016·9	mb. 015·2 019·9 016·6	mb. 015·6 020·1 016·3	mb. 016·2 020·4 016·2	mb. 016·8 020·6 016·2	mb. 017·4 020·9 016·3	mb. 017·7 021·3 016·1	mb. 018·0 021·5 015·6	mb. 018·4 021·4 014·9	mb. o18.8 c21.2 o14.4	23. mb. o15·2 020·2 o18·5
(Sea le	Rich	mond o13·5 o18·7 o21·0 o13·8	mb. 013·3 018·9 020·8 013·0	mb. 013·2 019·1 020·7 012·3	mb. 012·9 019·0 020·5	mb. 013·2 019·4 020·6 011·5	mb. o13.5 o19.7 o20.7 o11.5	b = 1 mb. 013.9 020.2 020.6 011.4	mb. 014·3 020·5 020·6 011·1	mb. 014·9 020·7 020·3 010·5	mb. 015·1 021·0 020·3 009·9	mb. 015·2 020·8 019·9 009·2	mb. 015.0 020.6 019.3 008.4	mb. 015·2 020·2 018·5 007·8	mb. 015·1 020·1 017·9	mb. 015·1 019·9 016·9 006·9	mb. 015·2 019·9 016·6 006·4	mb. 015·6 020·1 016·3 005·9	mb. 016·2 020·4 016·2 006·1	mb. 016·8 020·6 016·2 006·1	mb. 017·4 020·9 016·3 005·9	mb. 017·7 021·3 016·1 005·6	mb. 018·0 021·5 015·6 005·2	mb. 018·4 021·4 014·9 c04·8	mb. 018·8 021·2 014·4 c04·6	mb. 015·2 020·2 018·5 cc8·8
(Sea le	Rich 1 2 3 4 5	mond o13·5 o18·7 o21·0 o13·8 oo4·3	mb. 013·3 018·9 020·8 013·0 004·1	mb. 013·2 019·1 020·7 012·3 003·9	mb. 012·9 019·0 020·5 011·7	mb. 013.2 019.4 020.6 011.5	mb. 013.5 019.7 020.7 011.5	b = 1 mb. 013·9 020·2 020·6 011·4 003·8	mb. 014·3 020·5 020·6 011·1 004·0	mb. 014·9 020·7 020·3 010·5 004·2	mb. 015·1 021·0 020·3 009·9 004·6	mb. 015·2 020·8 019·9 009·2	mb. 015·0 020·6 019·3 008·4	mb. 1 015·2 020·2 018·5 007·8	mb. 015·1 020·1 017·9 007·3 004·2	mb. 015·1 019·9 016·9 006·9	mb. 015·2 019·9 016·6 006·4 003·9	mb. 015·6 020·1 016·3 005·9 004·0	mb. 016·2 020·4 016·2 006·1	mb. 016·8 020·6 016·2 006·1 004·6	mb. 017·4 020·9 016·3 005·9 004·6	mb. 017·7 021·3 016·1 005·6 c04·6	mb. 018·0 021·5 015·6 005·2 004·6	mb. 018·4 021·4 014·9 004·8	mb. 018·8 021·2 014·4 004·6 004·5	mb. 015·2 020·2 018·5 cc8·8 co4·2
(Sea le	Rich 1 2 3 4 5	mb. 013·5 018·7 021·0 013·8 004·3	mb. 013·3 018·9 020·8 013·0 004·1	mb. 013·2 019·1 020·7 012·3 003·9	mb. 012·9 019·0 020·5 011·7 003·7	mb. 013·2 019·4 020·6 011·5 003·6	mb. 013·5 019·7 020·7 011·5 003·7	b = 1 mb. 013·9 020·2 020·6 011·4 003·8	mb. 014·3 020·5 020·6 011·1 004·0	mb. 014·9 020·7 020·3 010·5 004·2	mb. 015·1 021·0 020·3 009·9 004·6	mb. 015·2 020·8 019·9 009·2 004·7	mb. 015·0 020·6 019·3 008·4 004·6	mb. 015·2 020·2 018·5 007·8 004·3	mb. 015·1 020·1 017·9 007·3 004·2	mb. 015·1 019·9 016·9 006·9 004·1	mb. 015·2 019·9 016·6 006·4 003·9	mb. 015·6 020·1 016·3 005·9 004·0	mb. 016·2 020·4 016·2 006·1 004·2	mb. 016·8 020·6 016·2 006·1 004·6	mb. 017·4 020·9 016·3 005·9 004·6	mb. 017·7 021·3 016·1 005·6 c04·6	mb. 018·0 021·5 015·6 005·2 004·6 003·6	mb. 018·4 021·4 014·9 004·8 004·6	mb. 018·8 021·2 014·4 004·6 004·5	mb. 015·2 020·2 018·5 cc8·8 co4·2 co4·1
(Sea le	Rich 1 2 3 4 5	mond o13·5 o18·7 o21·0 o13·8 o04·3 o04·4 o03·5	mb. 013·3 018·9 020·8 013·0 004·1	mb. 013·2 019·1 020·7 012·3 003·9 004·1	mb. 012·9 019·0 020·5 011·7 003·7	mb. 013·2 019·4 020·6 011·5 003·6 004·3	mb. 013·5 019·7 020·7 011·5 003·7 004·3	b = 1 mb. o13·9 o20·2 o20·6 o11·4 o03·8 o04·6 o03·2	mb. 014·3 020·5 020·6 011·1 004·0 004·7 003·5	mb. 014·9 020·7 020·3 010·5 004·2 004·6 003·5	mb. 015·1 021·0 020·3 009·9 004·6 003·6	mb. 015·2 020·8 019·9 009·2 004·7	mb. 015·0 020·6 019·3 008·4 004·6	mb. 1 015·2 020·2 018·5 007·8 004·3 004·2 003·6	mb. 015·1 020·1 017·9 007·3 004·2 004·1	mb. 015·1 019·9 016·9 006·9 004·1	mb. 015·2 019·9 016·6 006·4 003·9 003·4 003·3	mb. 015·6 020·1 016·3 005·9 004·0 003·6 003·4	mb. 016·2 020·4 016·2 006·1 004·2 003·5 003·7	mb. 016·8 020·6 016·2 006·1 004·6	mb. 017·4 020·9 016·3 005·9 004·6	mb. 017·7 021·3 016·1 005·6 c04·6	mb. 018·0 021·5·6 005·2 004·6 003·6 004·8	mb. 018·4 021·4 014·9 004·8 004·6	mb. 018·8 021·2 014·4 004·6 004·5	mb. 015·2 020·2 018·5 cc8·8 co4·2 co4·1
(Sea le	Rich 1 2 3 4 5 6 7 8 9	mond o13·5 o18·7 o21·0 o13·8 o04·3 o04·4 o03·5 o04·8 o10·3	mb. 013·3 018·9 020·8 013·0 004·1 004·4 003·2 004·8 010·2	mb. 013·2 019·1 020·7 012·3 003·9 004·1 003·0 004·8 010·2	mb. 012·9 019·0 020·5 011·7 003·7 004·2 0003·0 004·8	mb. 013·2 019·4 020·6 011·5 003·6 004·3 002·9 005·1	mb. 013·5 019·7 020·7 011·5 003·7 004·3 003·0 005·8 010·0	b = 1 mb. 013·9 020·2 020·6 011·4 003·8 004·6 003·2 006·2 0010·0	mb. 014·3 020·5 020·6 011·1 004·0 004·7 003·5 006·8 009·8	metre mb. 014·9 020·7 020·3 010·5 004·2 004·6 003·5 007·3 009·3	mb. 015·1 021·0 020·3 009·9 004·6 003·6 007·5 008·9	mb. 015·2 020·8 019·9 009·2 004·7 004·4 003·8 007·9 008·2	mb. 015·0 020·6 019·3 008·4 004·6 004·4 003·7 008·1	mb. 015·2 020·2 018·5 007·8 004·3 004·2 003·6 008·4 007·4	mb. 015·1 020·1 017·9 007·3 004·2 004·1 003·5 008·5 007·0	mb. 015·1 019·9 016·9 006·9 004·1 003·8 003·4 008·4	mb. 015·2 019·9 016·6 006·4 003·9 003·4 003·3 008·4 006·1	mb. 015·6 020·1 016·3 005·9 004·0 003·6 003·4 008·8 005·7	mb. 016·2 020·4 016·2 006·1 004·2 003·5 003·7 009·1 005·7	mb. 016·8 020·6 016·2 006·1 004·6 003·7 004·1 009·5 005·7	mb. 017·4 020·9 016·3 005·9 004·6 003·8 004·7 009·9	mb. 017·7 021·3 016·1 005·6 004·6 003·7 004·9 010·3 005·9	mb. 018·0 021·5 015·6 005·2 004·6 003·6 004·8 010·4 005·9	Mb. 018·4 021·4 014·9 004·8 004·6 003·6 004·7 010·4 006·0	mb. 018·8 021·2 014·4 004·5 003·6 004·7 010·5 005·8	23. mb. 015·2 020·2 018·5 cc8·8 co4·2 co4·1 co3·7 co7·9
(Sea le	Rich 1 2 3 4 5 6 7 8 9	mond o13·5 o18·7 o21·0 o13·8 o04·3 o04·4 o03·5 o04·8 o10·3	mb. 013·3 018·9 020·8 013·0 004·1 004·4 003·2 004·8 010·2	mb. 013·2 019·1 020·7 012·3 003·9 004·1 003·0 004·8 010·2	mb. 012·9 019·0 020·5 011·7 003·7 004·2 0003·0 004·8	mb. 013·2 019·4 020·6 011·5 003·6 004·3 002·9 005·1	mb. 013·5 019·7 020·7 011·5 003·7 004·3 003·0 005·8 010·0	b = 1 mb. 013·9 020·2 020·6 011·4 003·8 004·6 003·2 006·2 0010·0	mb. 014·3 020·5 020·6 011·1 004·0 004·7 003·5 006·8 009·8	metre mb. 014·9 020·7 020·3 010·5 004·2 004·6 003·5 007·3 009·3	mb. 015·1 021·0 020·3 009·9 004·6 003·6 007·5 008·9	mb. 015·2 020·8 019·9 009·2 004·7 004·4 003·8 007·9 008·2	mb. 015·0 020·6 019·3 008·4 004·6 004·4 003·7 008·1	mb. 015·2 020·2 018·5 007·8 004·3 004·2 003·6 008·4 007·4	mb. 015·1 020·1 017·9 007·3 004·2 004·1 003·5 008·5 007·0	mb. 015·1 019·9 016·9 006·9 004·1 003·8 003·4 008·4	mb. 015·2 019·9 016·6 006·4 003·9 003·4 003·3 008·4 006·1	mb. 015·6 020·1 016·3 005·9 004·0 003·6 003·4 008·8 005·7	mb. 016·2 020·4 016·2 006·1 004·2 003·5 003·7 009·1 005·7	mb. 016·8 020·6 016·2 006·1 004·6 003·7 004·1 009·5 005·7	mb. 017·4 020·9 016·3 005·9 004·6 003·8 004·7 009·9	mb. 017·7 021·3 016·1 005·6 004·6 003·7 004·9 010·3 005·9	mb. 018·0 021·5 015·6 005·2 004·6 003·6 004·8 010·4 005·9	Mb. 018·4 021·4 014·9 004·8 004·6 003·6 004·7 010·4 006·0	mb. 018·8 021·2 014·4 004·5 003·6 004·7 010·5 005·8	mb. 015·2 020·2 018·5 cc8·8 co4·2 co4·1 co3·7 co7·7
(Sea le	Rich 1 2 3 4 5 6 7 8 9 10	mb. 013·5 018·7 021·0 013·8 004·3 004·4 003·5 004·8 010·3 005·7	mb. 013·3 018·9 020·8 013·0 004·1 004·4 003·2 004·8 010·2 005·9	mb. 013·2 019·1 020·7 012·3 003·9 004·1 003·0 004·8 010·2 005·8	mb. 012·9 019·0 020·5 011·7 003·7 004·2 003·0 004·8 010·0 005·8	mb. 013·2 019·4 020·6 011·5 003·6 004·3 002·9 005·1 010·0 006·0	mb. 013·5 019·7 020·7 011·5 003·7 004·3 003·0 005·8 010·0 006·0	mb. 013·9 020·2 020·6 011·4 003·8 004·6 003·2 006·2 010·0 006·1	mb. 014·3 020·5 020·6 011·1 004·0 004·7 003·5 006·8 009·8	mb. 014·9 020·7 020·3 010·5 004·2 004·6 003·5 009·3 000·1	mb. 015·1 021·0 020·3 009·9 004·6 003·6 007·5 008·9 005·9	mb. 015·2 020·8 019·9 009·2 004·7 004·4 003·8 007·9 008·2 005·4	mb. 015·0 020·6 019·3 008·4 004·4 003·7 008·1 007·8 004·7	mb. 015·2 020·2 018·5 007·8 004·3 004·2 003·6 008·4 007·4 004·5	mb. 015·1 020·1 017·9 007·3 004·1 003·5 008·5 007·0 004·3	mb. 015·1 019·9 006·9 004·1 003·8 003·4 008·4 006·4 004·2	mb. 015·2 016·6 006·4 003·9 003·4 003·3 008·4 006·1 003·9	mb. 015·6 020·1 016·3 005·9 004·0 003·6 003·4 008·8 005·7	mb. 016·2 020·4 016·2 006·1 004·2 003·5 003·7 009·1 005·7 003·7	mb. 016·8 020·6 016·2 006·1 004·6 003·7 004·1 009·5 005·7 003·9	mb. 017·4 020·9 016·3 005·9 004·6 003·8 004·7 009·9 005·9 004·3	mb. 017·7 021·3 016·1 005·6 004·6 003·7 004·9 010·3 005·9 004·3	mb. 018·0 021·5 015·6 005·2 004·6 003·6 004·8 010·4 005·9 003·9	mb. 018·4 021·4 014·9 004·8 004·6 003·6 004·7 010·4 006·0 003·3	mb. 018·8 021·2 014·4 004·6 004·5 003·6 005·8 003·5	mb. 015·2 020·2 018·5 008·8 004·2 004·1 003·7 007·7 007·9 004·9
385.	Rich 1 2 3 4 5 6 7 8 9 10 11 12	mond o13·5 o18·7 o21·0 o13·8 o04·3 o04·4 o03·5 o04·8 o10·3 o05·7 o03·9 oo1·0	mb. 013·3 018·9 020·8 013·0 004·1 004·4 003·2 004·8 010·2 005·9 003·9	mb. 013·2 019·1 020·7 012·3 003·9 004·1 003·0 004·8 010·2 005·8	mb. 012·9 019·0 020·5 011·7 004·2 003·0 004·8 010·0 005·8	mb. 013·2 019·4 020·6 001·5 003·6 004·3 002·9 005·1 010·0 006·0 003·7 998·1	mb. o13·5 o19·7 o20·7 o11·5 o03·7 o04·3 o05·8 o10·0 o06·0 o04·0	b = 1 mb. o13·9 o20·2 o20·6 o11·4 oo3·8 oo4·6 oo3·2 oo6·2 ol0·0 oo6·1	mb. 014·3 020·5 020·6 011·1 004·0 004·7 003·5 006·8 009·8 006·1	mb. 014.9 020.7 020.3 010.5 004.2 004.6 003.5 009.3 006.1 004.7 997.3	mb. 015·10 020·3 009·9 004·6 003·6 007·5 008·9 005·9 004·8 996·7	mb. 015·2 020·8 019·9 009·2 004·7 004·4 003·8 007·9 008·2 005·4 004·9	mb. 015.0 020.6 019.3 008.4 004.6 004.4 003.7 008.1 007.8 004.7	mb. 015·2 020·2 018·5 007·8 004·3 004·2 003·6 008·4 007·4 004·5 004·3 994·1	mb. 015·1 020·1 017·9 007·3 004·2 004·1 003·5 007·0 004·3 004·2 993·8	mb. 015·1 019·9 016·9 006·9 004·1 003·8 003·4 006·4 004·2 003·7 993·7	mb. 015·2 019·9 016·6 006·4 003·9 003·4 006·1 003·9 003·5 993·6	mb. 015·6 020·1 016·3 005·9 004·0 003·6 003·4 008·8 005·7 003·3 993·7	mb. o16·2 o20·4 o16·2 co6·1 oo4·2 co3·5 co3·7 co9·1 oo5·7 co3·7 co2·8 994·1	mb. 016·8 020·6 016·2 006·1 004·6 003·7 004·1 009·5 005·7 003·9 003·0 994·8	mb. 017:4 020:9 016:3 005:9 004:6 003:8 004:7 009:9 005:9 004:3	mb. 017.7 021.3 016.1 005.6 004.6 003.7 004.9 010.3 005.9 004.3	mb. 018·0 021·5 015·6 005·2 004·6 003·6 004·8 010·4 005·9 003·9 002·1 995·4	mb. 018·4 021·4 021·4 014·9 014·9 004·6 003·6 004·7 010·4 006·0 003·3	mb. o18.8 o21.2 o14.4 cc4.5 co3.6 cc4.7 o10.5 co5.8 co3.5	mb. 015·2 020·2 018·5 cc8·8 co4·2 co4·1 co3·6 co7·9 co4·9 co3·6 co3·6 co3·6
385.	Rich 1 2 3 4 5 6 7 8 9 10	mond mb. 013·5 018·7 021·0 013·8 004·4 003·5 004·8 005·7 003·9 001·0 995·3	mb. 013·3 018·9 020·8 013·0 004·1 004·4 003·2 004·8 010·2 005·9 003·9 000·5 995·0	w Ok mb. o13·2 o19·1 o20·7 o12·3 oo3·9 oo4·1 oo3·6 o99·1 o99·1	mb. 012·9 019·0 020·5 011·7 003·7 004·2 003·0 005·8 003·5 998·4 994·0	mb. 013·2 019·4 020·6 011·5 003·6 004·3 002·9 005·1 010·0 006·0 003·7 998·1	mb. 013·5 019·7 020·7 011·5 003·7 004·3 005·8 010·0 006·0 004·0 997·7	b = 1 mb. 013·9 020·2 020·6 011·4 003·8 004·6 003·2 006·2 010·0 006·1 004·3 997·6 995·1	mb. 014·3 020·5 020·6 011·1 004·0 004·7 003·5 006·8 009·8 006·1	mb. 6014.9 020.7 020.3 010.5 004.2 004.6 003.5 009.3 006.1 004.7 994.9	mb. 015·1 021·0 020·3 009·9 004·6 007·5 008·9 005·9 004·8 909·9	mb. 015·2 020·8 019·9 009·2 004·7 004·4 003·8 007·9 008·2 005·4 004·9 995·3	mb. 015·0 020·6 019·3 008·4 004·6 004·4 003·7 006·1 007·8 004·7 994·7	mb. 1015 · 2 020 · 2 018 · 5 007 · 8 004 · 2 003 · 6 008 · 4 007 · 4 004 · 5 009 · 8 109 ·	mb. 015·1 020·1 017·9 007·3 004·2 004·1 003·5 007·0 004·3 004·2 993·8	mb. 015·1 019·9 016·9 006·9 004·1 003·8 003·4 006·4 006·4 004·2 003·7 993·7 993·7	mb. 015·2 019·9 016·6 006·4 003·9 003·4 006·1 003·9 003·5 993·6 992·1	mb. 015·6 020·1 016·3 005·9 004·0 003·6 003·4 008·8 005·7 003·3 993·7	mb. 016·2 020·4 016·2 006·2 003·5 003·7 005·7 005·7 002·8 994·1 991·6	mb. 016·8 020·6 016·2 006·1 004·6 003·7 004·1 009·5 005·7 003·9 003·0 994·8	mb. 017.4 020.9 016.3 005.9 004.6 003.8 004.7 009.9 005.9 004.3 003.0 995.5 991.9	mb. 017·7 021·3 016·1 005·6 004·6 004·9 010·3 005·9 004·3 002·5 995·4 992·2	mb. 018·0 021·5 015·6 005·6 004·6 003·6 004·8 010·4 005·9 003·9	mb. 018·4 021·4 014·9 004·8 004·6 003·6 004·7 010·4 006·0 003·3 001·4 095·6 092·7	mb. o18·8 o21·2 o14·4 cc4·6 cc4·5 co3·6 co4·5 co5·8 co3·5 co1·6 sp5·5 sp3·1	mb. 015·2 020·2 018·5 004·2 004·1 003·7 007·9 004·9 003·6 996·3 898·7
385.	Rich 1 2 3 4 5 5 6 7 8 9 10 11 12 13 14	mont mb. 013·5 018·7 021·0 013·8 004·4 003·5 004·8 005·7 003·9 001·0 993·2	mb. o13·3 o18·9 o2o·8 o13·0 o04·1 o04·4 o03·2 o05·9 o03·9 o05·9 o93·2	w Ot mb. o13:2019:1 o20:7 o12:3003:9 o04:1 o10:2 o05:8 o03:6 o999:1 9993:3	mb. 012·9 019·0 020·5 011·7 003·7 004·2 003·0 004·8 010·0 005·8 003·5 998·4 994·0	mb. 013·2 019·4 020·6 011·5 003·6 004·3 002·9 005·1 010·0 006·0 003·7 998·1 994·7	mb. 013·5 019·7 020·7 011·5 003·7 004·3 005·8 010·0 006·0 004·0 997·7 995·0 994·3	b = 1 mb. 013·9 020·2 020·6 011·4 003·8 004·6 003·2 006·2 010·0 004·3 997·6 997·6 995·1 995·1	mb. 014·3 020·5 020·6 011·1 004·0 004·7 003·5 006·8 006·1 004·7 995·7 995·7 995·2	metro mb. 014·9 020·7 020·3 010·5 004·2 004·6 003·5 007·3 006·1 004·7 997·3 997·3 995·4	mb. 015·1 021·0 020·3 009·9 004·6 003·6 007·5 008·9 005·9 004·8 996·7 996·7	mb. 015·22·8 019·9 009·2 004·7 003·8 007·9 008·2 005·4 004·9 995·3 996·0	mb. 015·0 020·6 019·3 008·4 004·6 004·4 003·7 008·1 007·8 004·7 994·7 994·2 995·9	mb. 015·2 020·2 018·5 007·8 004·3 004·2 003·6 008·4 007·4 004·5 004·3 994·1 995·5	mb. 015·1 020·1 017·9 007·3 004·2 004·1 003·5 007·3 004·2 993·8 993·8 993·3	mb. 015·1 019·9 016·9 006·9 004·1 003·8 003·4 006·4 006·4 006·3 009·7 993·7 996·1	mb. 015·2 019·9 016·6 006·4 003·9 003·4 003·3 006·1 003·5 993·6 993·6 999·1	mb. 015.6 020·1 016·3 005·9 004·0 003·6 003·4 008·8 005·7 003·3 993·7 992·0	mb. 016·2 020·4 016·2 006·1 004·2 003·5 003·7 005·7 005·7 002·8 991·6 996·7	mb. 016·8 020·6 016·2 006·1 004·6 003·7 004·1 009·5 005·7 003·0 994·7 997·1	mb. 017·4 020·9 016·3 005·9 004·6 003·8 004·7 005·9 005·9 005·9 005·9 005·9 005·9 005·9 005·9	mb. 017·7 021·3 016·1 005·6 004·6 003·7 004·9 010·3 005·9 004·3 005·9 995·4 995·4	mb. 018·0 021·5 015·6 005·2 004·6 003·6 004·8 010·4 005·9 003·9 002·1 992·4 998·1	Mpr mb. 018·46 021·49 014·9 004·7 010·40 003·6 003·3 001·46 992·7 998·2	mb. 018·8 021·2 014·4 004·5 03·6 004·7 010·5 005·8 003·5 01·6 995·5 993·1 998·2	mb. o15·2 020·2 o18·5 cc8·8 co4·2 co4·1 co3·7 co7·9 co4·9 co3·6 996·3 998·7 995·7
385.	Rich 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	mb. 013·5 018·7 021·0 013·8 004·3 004·4 003·5 004·8 010·3 005·7 003·9 001·0 995·3 993·2 998·2	mb. 013:3 018:9 020:8 013:0 004:1 004:4 003:2 005:9 000:5 995:0 993:2 998:1	mb. 013:2 019:1 020:7 012:3 003:9 004:1 003:0 004:8 010:2 005:8 003:6 999:1 994:4 993:3 998:1	mb. 012·9 019·0 020·5 0011·7 004·2 003·0 004·8 010·0 005·8 003·5 998·4 994·0 993·6	mb. 013·2 019·4 020·6 004·3 005·1 010·0 006·0 003·7 998·1 994·7 993·9	mb. 013·5 019·7 020·7 020·7 004·3 003·0 005·8 010·0 006·0 004·0 997·7 995·0 994·3 998·2	b = 1 mb. 013·9 020·2 020·6 011·4 003·8 004·6 003·2 010·0 006·1 004·3 997·6 995·1 998·3	mb. 014·3 020·5 6 011·1 004·0 004·7 003·5 006·8 009·8 006·1 004·7 995·1 995·2 998·4	metre mb. 014·9 020·7 020·7 020·3 010·5 004·2 004·6 003·5 007·3 009·3 006·1 004·7 997·3 994·9 995·4 998·4	mb. 015·1 021·0 021·0 020·3 000·3 000·3 000·5 000·5 000·5 900·5 900·7 994·8 995·6 998·3	mb. 015:20:08 019:99:009:20 004:7 004:4:9 005:4 004:995:3 994:5 996:0 998:2	mb. 015·0 020·6 019·3 008·4 004·6 004·4 003·7 008·1 007·8 004·7 994·7 994·7 995·9 998·2	mb. 015·2 020·2 018·5 007·8 004·2 003·6 008·4 007·4 004·5 004·3 994·1 993·8 995·5 998·3	mb. 015·1 020·1 017·9 007·3 004·2 004·1 003·5 007·0 004·3 004·2 993·8 993·3 995·9 998·1	mb. 015·1 019·9 016·9 006·9 004·1 003·8 008·4 006·4 004·2 003·7 993·7 992·7 996·1 998·0	mb. 015·2 019·9 016·6 006·4 003·9 003·4 006·1 003·9 003·5 993·6 992·1 996·2 997·8	mb. 015.6 020.1 016.3 005.9 004.0 003.6 003.4 008.8 005.7 003.3 993.7 003.3 993.7 992.0	mb. 016·2 020·4 016·2 006·1 004·2 003·5 003·7 009·1 005·7 002·8 994·1 991·6 996·7 998·2	mb. 016-8 020-6 006-2 006-1 004-6 003-7 004-1 009-5 003-0 094-8 991-7 997-1 998-6	mb. 017·4 020·9 006·3 005·9 004·6 003·8 004·7 005·9 005·9 004·3 003·0 995·5 991·9 997·6 999·1	mb. 017.7 021.3 005.6 004.6 004.9 010.3 005.9 004.3 002.5 995.4 992.2 997.9 999.5	mb. 018·0 021·5 005·2 004·6 003·6 005·9 003·9 002·1 995·4 998·1 999·9	mb. 018·4 021·4 0014·9 014·9 010·4 0003·6 0003·3 001·4 995·6 992·7 998·2 000·3	mb. o18.8 c21.2 o14.4 cc4.5 co3.6 cc4.6 co4.5 co5.8 co3.5 co1.6 c95.5 co1.6 c95.5 co5.8 co2.6 co5.8	mb. 015·2 020·2 018·5 028·8 024·2 024·1 03·7 07·7 07·9 04·9 03·6 996·3 998·7 995·7 998·5
385.	Rich 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	mond o13·5 o18·7 o21·0 o13·8 o04·3 o04·4 o03·5 o04·8 o10·3 o05·7 o03·9 o01·0 995·3 998·2 oo0·6	mb. 013·3 018·9 020·88 013·0 004·1 004·4 003·2 005·9 000·5 993·2 998·1 001·0	mb. 013·2 019·1 020·7 003·9 004·1 004·8 010·2 005·8 003·6 999·1 998·1	mb. 012·9 019·0 020·5 010·7 004·2 003·5 005·8 003·5 998·0 993·6 998·0 001·7	mb. 013·2 019·4 020·6 001·5 003·6 004·3 002·9 908·1 0002 003·7 998·1	mb. 013-5 019-7 020-7 020-7 004-3 003-0 005-8 010-0 006-0 997-7 995-0 994-3 998-2 003-2	b = 1 mb. o13·9 o20·2 o20·6 o11·4 o3·8 o04·6 o3·2 o10·0 o06·1 o04·3 997·6 995·1 998·3 o03·6	mb. 014·3 020·5 020·6 011·1 004·0 004·7 006·8 009·8 006·1 004·7 997·7 995·1 995·2 998·4	metre mb. ol4·9 o2o·7 o2o·3 olo-5 oo4·2 oo4·6 oo3·5 oo7·3 oo9·3 oo6·1 oo4·7 997·3 998·4 oo5·1	mb. 015·11 021·0 021·0 000·9 0	mb. 015·2 020·8 019·9 004·7 004·7 004·7 008·2 005·4 004·9 995·3 996·0 998·2	mb. 015·0 020·6 019·3 008·4 004·4 003·7 008·1 007·8 004·7 994·7 994·7 995·9 998·2 006·6	mb. 1015·2 020·2 018·5 004·3 004·5 004·3 994·1 993·8 995·5 998·3	mb. 015·1 020·1 017·9 007·3 004·1 003·5 007·0 004·3 004·2 993·8 993·9 998·1 007·7	mb. 015·1 019·9 016·9 006·9 004·1 003·8 008·4 006·4 004·2 003·7 993·7 993·7 996·1 998·0 008·2	mb. 015·2 019·9 016·6 006·4 003·9 003·4 006·1 003·9 003·5 993·6 992·1 996·2 997·8	mb. 015·6 020·1 016·3 005·9 004·0 003·4 008·8 005·7 003·3 993·7 992·0 996·4 997·8 009·7	mb. 016·2 020·4 016·2 006·1 004·2 003·5 009·1 005·7 003·7 002·8 994·1 996·7 998·2 010·5	mb. 016·8 020·6 006·1 004·6 003·7 004·1 009·5 005·7 003·9 99·8 99·7 997·1 998·6 011·6	mb. 017·4 020·9 016·3 005·9 004·6 003·8 005·9 006·3 009·9 006·3 006·	mb. 017·7 021·3 016·11 005·6 004·6 003·7 0010·3 005·9 004·3 002·5 995·4 992·2 997·9 999·5	mb. 018·0 021·5 025·6 005·6 004·6 003·6 003·6 005·9 003·9 002·1 995·4 998·1 999·9	mb. 018·4 021·4 014·9 016·4 003·6 003·6 0003·3 0010·4 0995·6 9995·7 998·2 000·3 015·2	mb. 018.8 021.2 014.4 016.6 016.6 016.5 016.6 016.5 016.6 016.6 016.6 016.6 016.6 016.6 016.6 016.6 016.6 016.6 016.6 016.6 016.6 016.6	mb. o15·2 020·2 o18·5 c08·8 c04·1 c03·7 c07·9 c04·9 c03·6 996·3 998·7 995·7 g98·5
385.	Rich 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	mond mb. 013·5 018·7 021·0 013·8 004·4 003·5 004·8 005·7 003·9 005·3 993·2 998·2 000·6 016·0	mb. 013·3 018·9 020·8 013·0 004·1 004·4 003·2 005·9 000·5 9993·2 998·1 001·0 016·3	mb. 013·2 019·1 020·7 012·3 003·9 004·1 003·0 003·0 003·0 999·1 9993·3 998·1 001·4 016·6	mb. 012·9 019·0 020·5 011·7 003·7 004·2 003·0 005·8 005·8 003·5 998·4 993·6 998·0 001·7 001·7	mb. 013·2 019·4 020·6 001·5 003·6 004·3 002·9 005·1 006·0 003·7 998·1 998·1 002-5 017·0	mb. 013·5 019·7 020·7 010·5 003·7 004·3 003·0 006·0 004·0 9997 9994·3 998·2 003-2 018·1	b = 1 mb. o13·9 o20·2 o20·6 o11·4 oo3·8 oo4·6 oo3·2 oo6·1 oo4·3 997·1 995·0 998·3 oo3·6 oo18·2	mb. 014·3 020·5 020·6 011·1 004·0 004·7 003·5 006·8 006·8 006·1 004·7 995·1 995·2 998·4 004·4 018·7	metro mb. 014·9 020·7 020·3 010·5 004·2 004·6 003·5 007·3 009·3 006·1 004·7 997·3 9994 005·1 018·9	mb. 015·11 021·0 020·3 000·9 0004·6 003·6 007·5 008·9 905·9 905·9 998·3 005·8 018·9 005·8	mb. 015·2 020·8 019·9 009·2 004·7 004·4 003·8 008·2 005·4 004·9 995·3 996·0 998·2 006·2	mb. 015·0 020·6 019·3 008·4 004·6 004·4 003·7 006·1 004·7 994·7 994·7 995·9 998·2 006·6 018·8	mb. 1015·2 020·2 020·3 004·2 003·6 004·3 994·8 995·5 998·3 007·2 018·7	mb. 015·1 020·1 017·9 004·2 004·1 003·5 009·5 004·2 993·8 993·8 995·9 998·1 007·7 018·6	mb. 015·1 019·9 016·9 006·9 004·1 003·8 006·4 006·4 004·2 003·7 993·7 996·1 998·0 008·2 018·3	mb. 015·2 019·9 016·6 006·4 003·9 003·4 006·1 003·9 003·5 993·6 993·6 993·6 993·8 008·7	mb. 015.6 020.1 016.3 006.9 0003.6 003.6 003.4 003.7 003.3 993.7 992.7 996.4 997.8	mb. 016·2 020·4 016·2 006·1 004·2 003·5 003·7 005·7 003·7 002·8 994·1 996·7 998·2 010·5	mb. 016·8 020·6 016·2 006·1 004·6 003·7 004·1 009·5 005·7 003·9 003·0 994·8 991·7 997·1 998·6 011·6 018·4	mb. 017·4 020·9 016·3 004·6 003·8 004·7 005·9 005·9 004·3 003·0 995·5 991·1 012·8 018·5	mb. 017·7 021·3 016·1 005·6 004·6 0010·3 005·9 004·3 002·5 995·4 998·9 999·5 013·9 0013·9 0013·9	mb. 018·0 021·5 015·6 005·2 004·6 003·6 004·8 010·4 005·9 003·9 002·1 992·4 998·1 999·9	mb. 018·4 021·4 014·9 004·6 003·6 003·6 004·6 003·3 0010·4 006·0 003·3 001-4 0992·0 003·3 0015·2 0018·1	mb. o18.8 c21.2 o14.4 cc4.6 cc4.6 cc4.5 co3.6 co4.6 co4.7 co5.8 co3.5 co1.6 co5.8 co3.5 co1.6 co5.8 co3.5	mb. o15·2 020·2 o18·5 c08·8 c04·2 c04·1 c03·7 c07·9 c04·9 c03·6 996·3 998·7 995·7 998·5 c07·1 o18·0
(Sea le	Rich 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	mb. 013·5 018·7 021·0 021·0 021·0 021·0 03·9 004·4 003·5 004·8 010·3 005·7 003·9 001·0 995·3 993·2 998·2 006·6 016·0 017·3 005·9	mb. o13·33 o18·9 o18·39 o18·30 o20·8 o13·0 o04·1 o04·4 o03·2 o05·9 o05·9 o05·9 o016·3 o016·3 o016·7 o05·1	mb. 013-2 019-1 002-7 012-3 003-9 004-1 003-0 004-8 010-2 005-8 003-6 999-1 001-4 016-6 016-6 004-9	mb. :012·9 019·0 :020·5 :011·7 :003·7 :004·2 :003·0 :004·8 :010·0 :005·8 :003·5 :004·8 :0093·6 :093·6 :093·6 :093·6 :006·9 :016·1 :004·0	mb. 013·2 019·4 020·6 004·3 002·9 005·1 010·0 006·0 003·7 998·1 002·5 017·9 998·1	mb. 013·5 019·7 011·5 003·7 011·5 003·7 004·3 003·0 005·8 010·0 006·0 004·0 997·7 995·0 994·3 998·2 003·2 018·1 004·1	b = 1 mb. o13·9 o20·2 o20·6 o11·4 oo3·8 oo4·6 oo3·2 oo6·2 oi0·0 oo6·1 oo4·3 997·6 995·1 995·0 998·3 oo3·6 oi4·9 oo4·1	mb. 014·3 020·5 0020·6 011·1 004·0 004·7 003·5 006·8 006·1 004·7 995·1 995·2 998·4 004·4 018·7 004·0 004·0	metre mb. 014·9 020·7 020·3 010·5 004·2 004·6 003·5 007·3 009·3 006·1 004·7 997·3 994·9 995·4 005·1 018·9 0014·3 003·9 0014·3	mb. 015·11 021·0 021·0 020·3 0009 004·6 003·6 007·5 008·9 004·8 996·7 994·8 995·6 998·3 005·8 018·9 014·1 004·1	mb. 015:20:8 009:2 004:7 004:4 003:8 007:9 008:2 005:4 004:9 995:3 996:0 998:2 006:2 019:0 0013:4 003:9	mb. 015·0 020·6 019·3 008·4 004·4 003·7 008·1 007·8 004·7 994·7 994·2 995·9 998·2 006·6 018·8 012·5 004·0	mb. 015·2 020·2 018·5 007·8 004·3 004·2 003·6 008·4 007·4 004·5 004·3 995·5 998·3 007·2 018·8 007·2 018·8 007·8	mb. 015-1 020-1 1 020-1 1 020-1 1 020-1 1 007-3 004-2 004-1 003-5 007-0 004-3 004-2 993-8 995-3 995-9 998-1 007-7 018-6 004-1 0010-8 004-1	mb. 015·1 019·9 016·9 006·9 004·1 003·8 008·4 006·4 004·2 003·7 998·0 008·2 010·1 003·8	mb. 015·2 019·9 016·6 006·4 003·9 003·4 006·1 003·9 003·5 993·6 992·1 996·2 997·8 008·7 018·0 009·5 004·0	mb. 015·6 020·1 016·3 005·9 004·0 003·4 008·8 005·7 003·3 993·7 996·4 997·8 009·7 009·2 009·2	mb. 016·2 020·4 016·2 006·1 004·2 003·5 003·7 005·7 002·8 994·1 996·7 998·2 010·5 018·4 008·9 004·0	mb. 016·8 020·6 000·10·20 000·11·00·10·20 000·11·00·10·20 000 000 000 000 000 000 000 000 000	mb. 017·4 020·9 004·6 003·8 004·7 005·9 005·9 004·3 003·0 995·5 997·1 012·8 008·4 004·9	mb. 017-7-9021-3-3-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	mb. 018·0 021·5 015·6 005·2 004·6 003·6 004·8 010·4 005·9 003·9 002·1 995·4 998·1 999·9 014·7 018·3 007·5 004·9	mb. o18:4 o21:4 co4:6 co4:6 co4:6 co6:0 co	mb. o18.8 c21.2 cc4.6 cc4.5 co3.6 cc4.5 co5.8 co1.6 695.5 695.5 co1.6 co5.0 co5.0 co5.0	mb. o15.2 020.2 o18.5 co8.8 co4.2 co4.1 co3.7 co7.7 co7.9 co4.9 co3.6 g96.3 893.7 g95.7 g98.5 co7.1 o18.0 o12.2 co4.4
385.	Rich 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	mb. 013·5 018·7 021·0 021·0 021·0 021·0 03·9 004·4 003·5 004·8 010·3 005·7 003·9 001·0 995·3 993·2 998·2 006·6 016·0 017·3 005·9	mb. o13·33 o18·9 o18·39 o18·30 o20·8 o13·0 o04·1 o04·4 o03·2 o05·9 o05·9 o05·9 o016·3 o016·3 o016·7 o05·1	mb. 013-2 019-1 002-7 012-3 003-9 004-1 003-0 004-8 010-2 005-8 003-6 999-1 001-4 016-6 016-6 004-9	mb. :012·9 019·0 :020·5 :011·7 :003·7 :004·2 :003·0 :004·8 :010·0 :005·8 :003·5 :004·8 :0093·6 :093·6 :093·6 :093·6 :006·9 :016·1 :004·0	mb. 013·2 019·4 020·6 004·3 002·9 005·1 010·0 006·0 003·7 998·1 002·5 017·9 998·1	mb. 013·5 019·7 011·5 003·7 011·5 003·7 004·3 003·0 005·8 010·0 006·0 004·0 997·7 995·0 994·3 998·2 003·2 018·1 004·1	b = 1 mb. o13·9 o20·2 o20·6 o11·4 oo3·8 oo4·6 oo3·2 oo6·1 oo4·3 997·1 995·0 998·3 oo3·6 oo18·2	mb. 014·3 020·5 0020·6 011·1 004·0 004·7 003·5 006·8 006·1 004·7 995·1 995·2 998·4 004·4 018·7 004·0 004·0	metre mb. 014·9 020·7 020·3 010·5 004·2 004·6 003·5 007·3 009·3 006·1 004·7 997·3 994·9 995·4 005·1 018·9 0014·3 003·9 0014·3	mb. 015·11 021·0 021·0 020·3 0009 004·6 003·6 007·5 008·9 004·8 996·7 994·8 995·6 998·3 005·8 018·9 014·1 004·1	mb. 015:20:8 009:2 004:7 004:4 003:8 007:9 008:2 005:4 004:9 995:3 996:0 998:2 006:2 019:0 0013:4 003:9	mb. 015·0 020·6 019·3 008·4 004·4 003·7 008·1 007·8 004·7 994·7 994·2 995·9 998·2 006·6 018·8 012·5 004·0	mb. 015·2 020·2 018·5 007·8 004·3 004·2 003·6 008·4 007·4 004·5 004·3 995·5 998·3 007·2 018·8 007·2 018·8 007·8	mb. 015-1 020-1 1 020-1 1 020-1 1 020-1 1 007-3 004-2 004-1 003-5 007-0 004-3 004-2 993-8 995-3 995-9 998-1 007-7 018-6 004-1 0010-8 004-1	mb. 015·1 019·9 016·9 006·9 004·1 003·8 008·4 006·4 004·2 003·7 998·0 008·2 010·1 003·8	mb. 015·2 019·9 016·6 006·4 003·9 003·4 006·1 003·9 003·5 993·6 992·1 996·2 997·8 008·7 018·0 009·5 004·0	mb. 015·6 020·1 016·3 005·9 004·0 003·4 008·8 005·7 003·3 993·7 996·4 997·8 009·7 009·2 009·2	mb. 016·2 020·4 016·2 006·1 004·2 003·5 003·7 005·7 002·8 994·1 996·7 998·2 010·5 018·4 008·9 004·0	mb. 016·8 020·6 000·10·20 000·11·00·10·20 000·11·00·10·20 000 000 000 000 000 000 000 000 000	mb. 017·4 020·9 004·6 003·8 004·7 005·9 005·9 004·3 003·0 995·5 997·1 012·8 008·4 004·9	mb. 017-7-9021-3-3-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	mb. 018·0 021·5 015·6 005·2 004·6 003·6 004·8 010·4 005·9 003·9 002·1 995·4 998·1 999·9 014·7 018·3 007·5 004·9	mb. o18:4 o21:4 co4:6 co4:6 co4:6 co6:0 co	mb. o18.8 c21.2 cc4.6 cc4.5 co3.6 cc4.5 co5.8 co1.6 695.5 695.5 co1.6 co5.0 co5.0 co5.0	mb. o15.2 020.2 o18.5 co8.8 co4.2 co4.1 co3.7 co7.7 co7.9 co4.9 co3.6 g96.3 893.7 g95.7 g98.5 co7.1 o18.0 o12.2 co4.4
385.	Rich 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	mont mb. 013·5 018·7 021·0 013·8 004·4 003·5 004·9 001·0 995·3 993·2 998·2 000·6 016·0 017·3 005·9 005·0	mb. 013·3 018·9 020·8 013·0 004·1 004·4 003·2 005·9 000·5 993·2 998·1 001·0 016·3 016·7 005·1 005·0	mb. 013·2 019·1 020·7 012·3 003·9 004·1 003·0 004·8 010·2 005·8 003·6 999·1 999·1 001·4 006·6 016·4 004·9 004·9	mb. 012·9 019·0 020·5 0011·7 004·2 003·0 004·8 010·0 005·8 003·5 998·4 998·0 001·7 016·9 016·1 004·0 004·5	mb. 013·2 019·4 020·6 001·5 003·6 004·3 002·9 998·1 000-5 017·9 998·1 002-5 017·9 015·6 004·1 004·5	mb. 013-5 019-7 020-7 020-7 004-3 003-0 005-8 010-0 006-0 004-0 997-7 994-3 998-2 018-1 015-4 004-1	b = 1 mb. o13·9 o20·2 o20·6 o11·4 o3·8 o04·6 o3·2 o10·0 o06·1 o04·3 997·6 o998·3 o3·6 o18·2 o14·9 o04·1 o04·6	mb. 014·3 020·5 020·6 011·1 004·0 004·7 003·5 006·8 009·8 006·1 004·7 997·7 997·7 995·1 995·2 998·4 004·4 018·7 014·7 004·0 004·6	metre mb. oli4.9 oli4.9 oli6.00 oli6.0	mb. 015·11 021·0 020·3 0004·6 0004·6 0007·5 008·9 005·9 004·8 996·7 9994·8 995·6 0014·1 004·1 004·5	mb. 015·2 020·8 019·9 004·7 004·4 003·8 006·2 005·4 004·9 995·3 996·0 998·2 006·2 0013·4 003·9 006·2 006	mb. 015·0 020·6 019·3 008·4 004·6 004·7 007·8 004·7 994·7 994·7 995·9 998·2 006·6 018·8 012·5 004·1	mb. 1015·2 020·2 018·5 007·3 004·3 994·1 995·5 998·3 007·2 011·8 004·1 003·7	mb. 015·1 020·1 017·9 007·3 004·2 004·1 003·5 008·5 007·0 004·3 004-2 993·8 993·3 995·9 998·1 007·7 018·6 010·8 004·1 003·3	mb. 015·1 019·9 016·9 006·9 004·1 003·8 008·4 004·2 003·7 993·7 998·0 008·2 018·3 010·1 003·8 002·6	mb. 015·2 019·9 016·6 006·4 003·9 003·4 006·1 003·9 003·5 993·6 992·1 996·2 997·8 008·7 018·0 009·5 004·0 002·8	mb. 015.6 020.1 016.3 005.9 004.0 003.6 005.7 003.7 003.3 993.7 992.0 996.4 009.7 018.1 009.2 004.0 003.3	mb. 016·2 020·4 016·2 006·1 004·2 003·5 005·7 003·7 002·8 994·1 991·6 996·7 998·2 010·5 018·4 008·9 004·0 003·5	mb. 016·8 020·6 016·2 006·1 004·6 003·7 003·9 003·0 994·8 991·7 997·1 998·6 011·6 018·4 008·6 004·3 004·0	mb. 017·4 020·9 016·3·9 004·6 003·8 005·9 005·9 005·9 004·3 003·0 995·5 991·9 997·6 999·1 012·8 018·5 008·4 004·4	mb. 017·7 021·3 016·1 016·1 05·6 004·6 003·7 0010·3 005·9 004·3 002·5 995·4 992·2 997·9 999·5 013·9 004·6	mb. 018·0 021·5 015·6 005·2 004·6 003·6 003·6 005·9 003·9 002·1 995·4 998·1 999·9 014·7 018·3 007·5 004·9 005·2	mb. 018·4 021·4 014·9 016·9 003·6 004·6 006·0 003·3 016·4 995·6 992·7 998·2 006·8 005·1	mb. 018.8 021.2 014.4 5 019.6	mb. 015·2 020·2 018·5 004·1 003·7 007·9 004·9 003·6 996·3 998·5 007·1 018·0 012·2 004·4 004·3
385.	Rich 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	mond o13·5 o18·7 o21·0 o13·8 o04·3 o04·3 o05·7 o03·9 o01·0 995·3 998·2 o06·6 o16·0 o17·3 o05·9 o05·9	mb. o13:3 o18:9 o20:8 o13:0 o04:1 o04:4 o03:2 o04:8 o10:2 o05:9 o05:9 o01:0 o16:3 o05:1 o05:0 o04:2 998:5	mb. 013·2 019·1 002·7 012·3 003·9 004·1 003·0 004·8 010·2 005·8 003·6 999·1 001·4 004·9 004·9 003·6 998·7	mb. :012·9 019·0 020·5 001·7 003·7 004·2 003·0 005·8 005	mb. 013·2 019·4 020·6 020·6 020·6 004·3 002·9 005·1 010·0 006·0 003·7 998·1 994·7 998·1 002·5 017·9 998·1 004·5 004·5 003·2 999·6	mb. 013·5 019·7 011·5 003·7 004·3 003·0 006·0 004·0 997·7 995·0 994·3 998·2 003·2 008·1 004·7 003·2 000·2	b = 1 mb. o13·9 o20·2 o20·6 o11·4 oo3·8 oo4·6 oo3·2 oo6·2 ol0·0 oo6·1 oo4·3 997·6 995·1 995·0 998·3 oo3·6 o18·2 ol4·9 oo4·1 oo4·6 oo2·9 oo0·8	mb. 014·3 020·5 020·6 011·1 004·0 020·6 011·1 004·0 004·7 997·7 995·1 995·2 998·4 004·4 0018·7 004·0 004·6 001·3 0004·6 0001·3 0004·6 0004·6 0004·6 0004·6 0004·6 0004·6 0004·6 0004·6 0004·6 0004·6 0004·6 0004·6 0004·6 0004·6 0004·6 0004·6 0004·6 0004·6 0004·6 0004·	metro mb. o14·9 o20·7 o20·3 o10·5 o04·2 o04·6 o03·5 o07·3 o09·3 o06·1 o04·7 997·3 998·4 o05·1 o18·9 o014·3 o014·3 o01·7 o018·8	mb. 015-11 021-0 021-0 020-3 000-9 004-6 003-6 007-5 008-9 005-9 004-8 998-3 005-8 018-9 004-1 004-1 004-1 004-5 001-2 002-1 004-5	mb. 015:20:8 009:20 004:7 004:4 003:8 007:9 008:20 005:4 004:9 998:2 006:20 0013:4 003:9 004:5 000:5	mb. 015·0 020·6 019·3 008·4 004·4 003·7 008·1 007·8 004·7 994·7 994·7 995·9 998·2 006·6 018·8 012·5 004·1 999·6 002·8	mb. 015 · 2 020 · 2 018 · 5 007 · 8 004 · 3 004 · 2 003 · 6 008 · 4 007 · 4 004 · 5 998 · 3 007 · 2 018 · 7 001 · 8 004 · 1 003 · 7	mb. 015-1 020-1 1020-1	mb. 015·1 019·9 006·9 004·1 003·8 003·4 006·4 006·4 004·2 003·7 993·7 998·0 008·2 010·1 003·8 002·6	mb. 015·2 019·9 016·6 006·4 003·9 003·4 003·3 008·4 006·1 003·9 993·6 992·1 996·2 997·8 008·7 0019·5 004·0 002·8	mb. 015-6 020-1 016-3 005-9 004-0 003-6 003-4 005-7 003-7 003-3 993-7 8997-8 009-7 003-3 997-8 009-7 003-3 997-8	mb. 016·2 020·4 016·2 06·1 004·2 003·5 003·7 005·7 002·8 994·1 991·6 996·7 998·2 010·5 018·4 008·9 004·0 003·5	mb. 016-8 020-6 016-2 006-1 004-6 003-7 004-1 009-5 005-7 003-0 994-8 991-7 1998-6 0011-6 004-3 004-0 005-6 004-3 004-0 005-6 004-3 004-0 005-6	mb. 017·4 020·9 004·6 003·8 004·7 009·9 005·9 004·3 003·0 995·5 991·9 999·1 012·8 0108·4 004·9 004·4	mb. 017·70 021·3 0016·1 005·6 004·6 004·9 010·3 005·9 004·3 002·5 995·4 992·2 999·5 0013·9 004·6 007·9 004·6	mb. 018·0 021·5 015·6 005·2 004·6 003·6 004·8 010·4 005·9 003·9 002·1 995·4 998·1 999·9 014·7 007·5 004·9	mb. o18:4 o21:4 co4:8 co4:6 co4:6 co4:7 o10:4 co6:0 co3:6 co1:4 co6:0 co3:6 co1:4 co6:0 co5:0 co	mb. o18.8 o21.2 oc4.6 cc4.5 co3.6 co4.5 co5.8 co3.5 co1.6 695.5 698.2 co6.5 o15.5 co5.6 co6.5 co	mb. o15.2 020.2 o18.5 co8.8 co4.2 co4.1 o3.7 co7.7 co7.9 co4.9 co3.6 996.3 893.7 995.7 998.5 co7.1 o18.0 o12.2 co4.4 co4.3 co0.6 co2.7
385.	Rich 1 2 3 4 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	mb. 013·5 018·7 021·0 013·8 004·3 004·4 003·5 004·8 010·3 005·7 003·9 001·0 995·3 993·2 998·2 000·6 016·0 017·3 005·9 005·0 004·3 998·4 008·1	mb. o13·3 o18·9 o20·8 o13·0 o04·1 o004·4 o005·9 o005·9 o005·9 o005·0 o06·1 o005·0 o004·2 o006·3 o006·1 o006	mb. 013-2 019-1 020-7 020-7 020-7 020-7 003-0 004-1 003-0 004-8 003-0 004-8 003-0 004-8 003-0 004-9 004-9 004-9 004-9 004-9 004-9 004-9 004-9	mb. 012·9 019·0 020·5 0011·7 003·7 004·2 003·0 005·8 005·8 005·8 001·7 016·9 016·1 004·0 004·5 003·4 999·2 008·2	mb. 013·2 019·4 020·6 004·3 005·1 010·0 006·0 003·7 998·1 002·5 017·9 993·9 015·6 004·1 004·5 003·2 003·2	mb. 013·5 019·7 010·7 010·7 003·7 004·3 005·8 010·0 006·0 004·0 997·7 995·0 994·3 998·2 003·2 018·1 004·1 004·1 004·7 003·2 000-2 000-2	b = 1 mb. o13·9 o20·2 o20·6 o11·4 oo3·8 oo4·6 oo3·2 oo6·2 oi0·0 oo6·1 oo4·3 997·6 995·1 995·0 998·3 oo3·6 oi8·9 oo4·6 oo2·9 oo0·8 oo9·5	mb. 014·3 020·5 002·6 001·1 004·0 004·0 004·0 004·0 004·0 004·0 002·6 0001·3 0009·6	metre mb. 014·9 020·7 020·3 010·5 004·2 004·6 003·5 007·3 006·1 004·7 997·3 994·9 995·4 998·4 005·1 018·9 001·7 0001·7 0001·8 0009·7 001·8	mb. 015·1 021·0 021·0 020·3 000·9 004·6 003·6 007·5 008·9 005·9 004·8 996·7 994·8 995·6 998·3 005·8 018·9 1004·1 0004·5 0001·2 0	mb. 015·2020·8 019·20 009·2 004·7 003·8 007·9 908·2 005·4 004·9 995·3 994·5 006·2 019·0 003·9 0004·5 00002·4 010·1	mb. 015·0 020·6 019·3 008·4 004·4 003·7 008·1 007·8 004·7 994·7 994·2 995·9 998·2 006·6 018·8 012·5 004·1 999·6 002·8 010·3	mb. 015·2 020·2 018·5 004·3 004·5 004·3 995·5 998·3 007·2 018·7 001·8 004·1 999·3 004·1 999·3 001·2 010·2 010·2 010·2	mb. 015-1 020-1 1 020-1 1 020-1 1 020-1 1 017-9 007-3 004-2 004-1 003-5 0004-3 004-2 993-8 993-3 995-9 1 007-7 018-6 004-1 003-3 1 003-3 1 010-2 003-2 003-2 003-2 003-2 003-2 003-2 003-2 0003-2 003-2 003-2 003-2 003-2 003-2 003-2 003-2 003-2 003-2 003-2	mb. 015·1 019·9 016·9 006·9 004·1 003·8 008·4 006·4 004·2 003·7 993·7 992·7 998·0 008·2 018·3 000·8 000·8 000·9	mb. 015·2 019·9 016·6 006·4 003·9 003·5 993·6 992·1 096·2 997·8 008·7 018·0 002·8 0998·0 003·7 010·1 0	mb. 015·6 020·1 016·3 005·9 004·0 003·6 003·4 008·8 005·7 003·3 993·7 992·0 996·4 997·8 009·2 004·0 003·3 997·8	mb. 016·2 020·4 016·2 006·1 004·2 003·5 003·7 002·8 994·1 991·6 996·7 998·2 010·5 018·4 000·3 003·5	mb. 016-8 020-6 016-2 006-1 004-6 003-7 004-1 009-5 005-7 003-9 003-0 099-8 099-8 0018-4 008-6 004-3 004-0 005-5 0	mb. 017·4 020·9 004·6 003·8 004·7 0095·9 004·3 003·0 995·5 991·9 997·6 012·8 008·4 004·9 004·4 006·2 011·8	mb. 017-7 021-3 016-1 005-6 004-9 010-3 005-9 004-3 002-5 995-4 992-2 997-9 004-9 004-9 004-9 004-6 998-3 007-1 012-3	mb. 018·0 021·5 015·6 005·2 004·6 003·6 004·8 010·4 005·9 003·9 002·1 995·4 998·1 999·9 014·7 018·3 004·9 005·2 098·4	mb. 018:4 021:4 004:9 004:9 004:9 006:0 003:6 003:6 003:6 003:3 001:4 995:6 992:7 998:2 006:0 005:1	mb. o18.8 c21.2 o14.4 cc4.5 co4.6 cc4.5 co5.8 co3.6 co5.8 co3.6 co5.6 co	23. mb. o15·2 020·2 o18·5 c08·8 c04·2 c04·1 c03·7 c07·7 c07·9 c04·9 c03·6 g96·3 893·7 g95·7 g98·5 c07·1 o18·0 o12·2 c04·3 c00·4 c00·7 o10·1
385.	Rich I 2 3 4 4 5 5 6 7 8 9 10 II 12 13 14 15 16 17 18 19 20 21 22 23 24	mond o13·5 o18·7 o21·0 o13·8 o04·4 o03·5 o04·8 o10·3 o05·7 o03·9 o01·0 995·3 998·2 o00·6 o16·0 o17·3 o05·9 o06·3 o07	mb. 013:3018:9020:88 010:2004:1	mb. 013·2 019·1 020·7 003·9 004·1 000·2 005·8 003·6 999·1 994·4 993·3 998·1 001·4 004·9 004·9 004·9 004·9 004·9	mb. 012·9 019·0 020·5 0011·7 004·2 003·0 004·8 010·0 005·8 003·5 998·4 994·0 998·0 001·7 016·9 016·1 004·5 003·4 999·2 008·2 008·2 008·2 008·2 008·2	mb. 013·2 019·4 020·6 004·3 005·1 010·0 006·0 003·7 998·1 002·5 017·9 005·6 004·1 004·5 003·6 004·5 003·6 004·1 004·5	mb. 013·5 019·7 020·7 020·7 020·7 020·7 03·7 03·7 03·7 095·0 06·0 06·0 06·0 06·0 06·0 07 07 07 07 07 07 07 07 07 07 07 07 07	b = 1 mb. 013·9 020·2 020·6 03·8 004·6 003·2 010·0 006·1 004·3 997·6 995·1 995·0 998·3 003·6 018·2 014·9 004·6 002·9 000·8 009·5 017·5	mb. 014·3 020·5 0011·1 004·0 004·7 003·5 006·8 009·8 006·1 004·7 995·1 995·2 998·4 018·7 004·6 004·6 002·6 001·3 009·6 018·0	metre mb. o14·9 o20·7 o20·3 o10·5 o04·2 o04·6 o07·3 o06·1 o04·7 o997·3 o99·4 o995·4 o05·1 o18·9 o04·4 o05·1 o18·9 o04·7 o01·7 o000000000000000000000000000000000000	mb. 015·1 021·0 021·0 021·0 021·0 03009.9 004·6 003·6 007·5 008·9 005·9 004·1	mb. 015-20-8 019-9 004-7 004-4 003-9 005-4 004-9 995-3 994-5 006-2 003-9 004-5 000-5 000-1 018-2	mb. 015·0 020·6 019·3 008·4 004·6 004·7 008·1 007·8 004·7 994·7 995·9 998·2 006·6 018·8 012·5 004·1 999·6 002·8 010·3 018·0 018·0	mb. 015·2 020·2 018·5 003·6 008·4 007·4 004·5 004·3 995·5 998·3 007·2 018·7 003·7 999·3 003·2 0010·2 017·9 0017·9	mb. 015·1 020·1 017·9 007·3 004·2 004·1 003·5 007·0 004·3 004·2 993·8 993·3 995·9 998·1 007·7 018·6 004·1 003·3 004·1 003·3	mb. 015·1 019·9 016·9 006·9 004·1 003·8 006·4 006·4 004·2 003·7 998·0 008·2 018·3 010·1 003·8 003·6 003·6	mb. 015·2 019·9 016·6 006·4 003·9 003·5 993·6 992·1 996·2 997·8 009·5 00	mb. 015.6 020.1 016.3 005.9 004.0 003.6 003.4 008.8 005.7 003.7 003.3 993.7 003.8 009.7 018.1 009.7 00	mb. 016·2 020·4 016·2 006·1 004·2 003·5 003·7 003·7 002·8 994·1 991·6 996·7 998·2 010·5 018·4 008·9 004·0 003·5 004·0 0010·7 0016·7	mb. 016-8 020-6 016-2 006-1 004-6 003-7 004-1 009-5 005-7 003-9 003-0 0994-8 991-7 998-6 004-3 004-0 098-0 005-4 011-4 016-6 005-4	mb. 017.4 020.9 004.6 003.8 004.7 009.9 005.9 004.3 003.0 995.5 991.9 997.6 012.8 012.8 012.8 004.9 004.9 004.9 006.2 011.8 006.2	mb. 017.7 021.3 016.1 005.6 004.6 004.9 010.3 005.9 004.3 002.5 995.4 992.2 997.9 004.6 998.3 007.1 012.3 016.5	mb. 018·0 021·5 005·2 004·6 003·6 005·9 003·9 002·1 995·4 998·1 999·9 014·7 018·3 007·5 004·9 005·9 005·9 005·9 005·9	mb. 018:4 021:4 004:4 004:4 004:4 006:0 003:6 004:6 003:6 003:3 001:4 995:6 992:7 998:2 008:1 006:0 009:3 007:4 006:0 009:3 007:4 006:0 009:3 007:4 006:0 009:3 007:4 006:0 009:3 007:4 006:0 009:3 007:4 006:0 009:3 007:4 009:3 007:4 009:3 007:4 009:3 007:4	mb. o18.8 c21.2 o14.4 cc4.5 co3.6 cc4.6 cc4.5 co5.8 co3.6 co5.8 co1.6 co5.9 cc0.5 cc0.6 cc0.5 cc0.6 cc0.5 cc0.6 cc0.5 cc0.6 cc0.5 cc0.6 cc	23. mb. 015·2 020·2 018·5 028·8 024·1 03·7 07·7 07·9 04·9 03·6 996·3 993·7 995·7 998·5 007·1 018·0 0012·2 004·4 004·3 000-6 002·7 010·1 016·7
385.	Rich 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	mond mb. o13·5 o21·0 o21·0 o13·8 o4·3 o04·4 o3·5 o4·8 o10·3 o5·7 o3·9 o1·0 998·3 998·4 o8·1 o14·3 o13·5	mb. ol3;3 ol8;9 ol2;0 ol4;1 oo4;4 oo3;2 oo4;8 ol0;2 oo5;9 oo5;9 oo5;9 oo1;0 oo1;0 oo1;0 oo4;2 oo5;0 oo4;2 oo5;0 oo4;2 oo5;0 oo4;2 oo5;0 oo4;2 oo5;0 oo4;2 oo5;0 oo4;2 oo5;0 oo4;2 oo5;0 oo4;2 oo5;0 oo4;2 oo5;0 oo4;2 oo5;0 oo4;2 oo5;0 oo4;2 oo5;0 oo4;2 oo5;0 oo6;0 oo4;2 oo5;0 oo6;0 oo	mb. 013:29 019:1 002:73 003:9 004:1 003:0 004:8 010:2 005:8 003:6 999:1 001:4 004:9 004:9 003:6 998:7 006:6 006:4 004:9 004:9	mb. :012·9 019·0 020·5 011·7 003·5 998·4 994·0 993·6 1004·5 003·5 004·5 003·4 999·2 008·2 016·0 009·0	mb. 013·2 019·4 010·0 03·6 001·5 003·6 004·3 002·9 005·1 010·0 006·0 003·7 998·1 994·7 998·1 002·5 0015·6 004·1 004·5 003·2 999·6 008·3 016·1 007·4	mb. 013·5 019·7 011·5 003·7 004·3 003·0 005·8 010·0 004·0 997·7 995·0 998·2 018·1 004·7 003·2 000·2 000·0 006·1	b = 1 mb. o13·9 o20·2 o20·6 o11·4 oo3·8 oo4·6 oo3·2 oo6·2 ol0·0 oo6·1 oo4·3 997·6 995·1 995·0 998·3 oo3·6 o18·2 o14·9 oo4·1 oo4·6 oo2·9 oo4·1 oo4·6	mb. 014·3 020·5 020·6 011·1 004·0 020·6 011·1 004·0 004·7 997·7 995·1 998·4 004·4 004·6 002·6 001·3 009·6 018·0 002·6 0003·7	metro mb. o14·9 o20·7 o20·3 o10·5 o04·2 o04·6 o03·5 o07·3 o09·3 o06·1 o04·7 997·3 998·4 998·4 o05·1 o04·7 o01·8 o09·7 o118·2 o02·7	mb. 015-11 021-0 021-0 020-3 000-9 004-6 003-6 007-5 008-9 005-9 005-8 998-3 005-8 998-3 005-8 001-1 004-1 0	mb. 015:2020:8 019:99 009:20 004:4 003:8 007:99 008:20 005:4 004:99 998:20 006:20	mb. 015·0 020·6 019·3 008·4 004·6 004·4 003·7 008·1 007·8 004·7 994·7 994·7 994·2 995·9 998·2 006·6 018·8 012·5 004·0 004·1 999·6 002·8 010·3 018·0 000·2	mb. 015 · 2 020 · 2 018 · 5 007 · 8 004 · 3 004 · 2 003 · 6 008 · 4 007 · 4 004 · 5 993 · 8 995 · 5 998 · 3 007 · 2 011 · 8 004 · 1 003 · 7 999 · 3 0010 · 2 017 · 9 999 · 6	mb. 015-1 1020-1	mb. 015·1 019·9 006·9 004·1 003·8 003·4 006·4 006·4 004·2 003·7 993·7 998·1 003·8 002·6 003·5 010·0 0017·3 0998·4	mb. 015-2 019-9 016-6 006-4 003-9 003-4 003-3 008-4 006-1 003-9 993-6 993-6 993-6 997-8 008-7 0018-0 002-8 003-7 010-1 017-0 0998-2	mb. 015-6 020-11 016-3 005-9 004-0 003-6 003-4 005-7 003-7 003-3 993-7 992-0 4997-8 009-7 003-3 997-8 009-7 016-9 097-9 016-9 016-9 097-9 016-9 016-9 097-9 016-9 016-9 097-9 016-9 016-9 097-9 016-9	mb. o16·2 o20·4 o16·2 c06·1 o04·2 c03·5 c03·7 c09·1 o05·7 c03·7 c09·1 o05·7 g98·2 o10·5 o08·9 o04·0 o03·5	mb. 016.8 020.6 016.2 006.1 004.6 003.7 004.1 0095.5 005.7 003.9 003.0 994.8 991.7 998.6 011.6 004.3 004.0 098.0 005.4 011.4 011.6 0997.9	mb. 017:4 020:9 016:3 005:9 004:6 003:8 004:7 005:9 005:9 004:3 003:0 995:5 991:0 999:1 012:8 018:5 008:4 004:9 004:4 998:4 006:2 011:8 016:8 998:4	mb. 017:7 021:3 016:5 5998:1	mb. 018.0 021.5 015.6 005.2 004.6 003.6 004.8 010.4 005.9 003.9 002.1 995.4 998.1 999.9 014.7 007.5 004.9 007.5 0012.5 0016.0 0998.1	mb. o18:4 021:4 021:4 021:4 026:0 03:6 004:7 010:4 006:0 003:3 01:4 995:6 992:7 000:4 006:0 003:3 001:4 998:3 007:9 013:5 015:4 997:9	mb. o18.8 o21.2 c2.4 c2.4 c2.4 c2.4 c3.6 c3.5 c3.5 c3.5 c3.5 c3.5 c3.5 c3.5 c3.5	mb. o15.2 020.2 o18.5 co8.8 co4.2 co4.1 co3.7 co7.7 co7.9 co4.9 co3.6 g96.3 g93.7 g95.7 g98.5 co7.1 o18.0 o12.2 co4.4 co4.3 co0.6 co2.7 co10.1 co16.7 co2.5
385.	Rich 1 2 3 4 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	mond mb. o13·5 o18·7 o21·0 o21·0 o21·0 o21·0 o21·0 o3·9 o01·0 995·3 993·2 998·2 o00·6 o16·0 o17·3 o05·9 o05·0 o04·3 998·4 o08·1 o14·3 o13·5	mb. o13:33 o18:9 o18:9 o20:8 o13:0 o04:1 o04:4 o3:2 o05:9 o05:9 o05:9 o016:3 o016:7 o05:0 o04:2 998:5 o08:0 o014:9 o012:2 998:6	mb. 013-2 019-1 002-7 012-3 003-9 004-1 003-0 004-8 003-0 004-8 003-0 004-8 003-0 004-8 003-0 004-8 003-0 004-8 003-0 004-8 003-0 004-9 004-9 004-9 004-9 004-9 004-9	mb. :012·9 019·0 020·5 011·7 004·2 005·8 010·0 005·5 0	mb. 013·2 019·4 020·6 03·6 004·3 002·9 005·1 010·0 003·7 998·1 002·5 0017·9 998·1 002·5 0017·9 998·1 002·5 0017·9 998·1 002·5 0017·9 998·1 002·5 0017·9 998·1 002·5 0017·9 998·1	mb. 013·5 019·7 011·5 003·7 004·3 003·0 005·8 010·0 006·0 004·0 997·7 995·0 994·3 998·2 003·2 004·1 004·7 003·2 009·0 016·7 006·1	b = 1 mb. o13·9 o20·2 o20·6 o11·4 oo3·8 oo4·6 oo3·2 oo6·2 ol0·0 oo6·1 oo4·3 997·6 995·1 995·0 998·3 oo3·6 o18·2 ol4·9 oo4·6 oo2·9 oo4·1 oo4·6 oo2·9 oo4·9 oo4·9 oo5·8	mb. 014·3 020·5 0020·6 011·1 004·0 004·7 003·5 006·8 009·8 006·1 004·7 997·7 995·1 004·4 018·7 004·6 0018·0 002·6 0018·0 003·7 004·6 0018·0 003·7 0995·1 099	metre mb. 014·9 020·7 020·3 010·5 004·2 004·6 003·5 007·3 009·3 006·1 004·7 997·3 999·9 04·4 001·7 001·8 009·7 0018·2 002·7 0018·2 002·7 099·10/2 0	mb. 015·11 021·0 021·0 020·3 000·9 004·6 003·6 007·5 008·9 005·9 004·8 996·7 9994·8 996·7 994·8 996·7 0014·1 004·1 004·1 004·5 001·2 002·1 010·1	mb. 015:2020:8 9009:2 004:7 004:4 003:8 007:9 908:2 005:4 004:9 995:3 994:5 009:0 000:3 4 003:9 004:5 002:4 010:1 018:2 000:8 995:2	mb. 015.0 020.6 019.3 008.4 004.6 004.4 003.7 008.1 007.8 004.7 994.7 994.2 995.9 998.2 006.6 018.8 012.5 004.0 004.1	mb. 015·2 020·2 018·5 004·3 004·2 003·6 008·4 007·4 004·5 004·3 994·1 993·8 995·5 998·3 007·2 011·8 003·7 999·3 003·2 017·9 0999·6	mb. 015-1 020-1 1 020-1 1 020-1 1 020-1 1 020-1 1 020-1 1 020-1 1 020-1	mb. 015·1 019·9 006·9 004·1 003·8 003·4 006·4 004·2 003·7 993·7 998·0 008·2 018·3 0010·1 003·8 002·6 0998·2 0017·3 0998·4	mb. 015·2 019·9 016·6 006·4 003·9 003·4 006·1 003·9 003·5 993·6 992·1 996·2 997·8 008·7 018·0 009·5 004·0 002·8 098·0 003·7 010·1 017·0 0998·2	mb. 015-6 020-1 016-3 005-9 004-0 003-6 003-4 008-8 005-7 003-7 003-3 993-7 003-3 993-7 009-2 004-0 003-3 009-2 004-0 003-3 0997-8	mb. o16·2 o20·4 o16·2 c06·1 o04·2 c03·5 c03·7 c09·1 o05·7 c03·7 c02·8 994·1 996·7 998·2 o10·5 o18·4 o08·9 o04·0 o03·5 997·9 004·2 o10·7 o16·7 o997·4	mb. 016-8 020-6 6 020-6	mb. 017·4 020·9 004·6 003·8 004·7 0095·9 004·3 003·0 995·5 991·9 999·1 012·8 004·4 006·2 001·8 016·8 0998·4 006·2 001·9 001·9	mb. 017.7 021.3 016-1 005-6 004-6 010-3 005-9 010-3 005-9 004-3 007-9 004-9 004-9 004-6 0988-3 007-1 012-3 016-5 098-1 002-8	mb. 018·0 021·5 015·6 05·2 004·6 003·6 003·9 002·1 995·4 998·1 999·9 014·7 0018·3 007·5 004·9 007·5 0012·5 0016·0 0998·1	mb. o18:4 o21:4 co4:8 co4:6 co3:6 co4:7 o10:4 co6:0 co3:3 co1:4 co6:0 co5:0 co5:1 co6:8 co5:0 co5:1 co6:8 co7:9 co	mb. o18.8 o21.2 oco4.6 cc4.5 co3.6 cc4.5 co3.5 co1.6 695.5 693.1 cc6.5 c	23. mb. o15.2 020.2 o18.5 c08.8 c04.2 c04.1 o03.7 c07.7 c07.9 c04.9 c03.6 g96.3 893.7 g95.7 g98.5 c07.1 o18.0 o12.2 c04.4 c04.3 c00.6 c02.7 c010.1 c016.7 c02.5
385.	Rich 1 2 3 4 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	mond mb. 013·5 018·7 021·0 013·8 004·4 003·5 004·8 010·3 005·7 003·9 001·0 995·3 993·2 998·2 000·6 017·3 005·0 004·3 998·4 010·3 013·5	mb. o13:3 o18:9 o20:8 o20:8 o20:8 o20:8 o20:8 o20:9 o2	mb. 013·2 019·1 020·7 003·9 004·1 000·8 010·2 005·8 003·6 999·1 994·4 016·6 016·4 016·6 016·4 004·9 004·9 004·9 004·9 006·3	mb. 012·9 019·0 020·5 0010·0 004·2 003·0 005·8 010·0 005·8 001·7 016·9 016·1 004·0 004·5 003·4 999·2 008·2 016·0 009·0 995·5 006·9 006·9	mb. 013·2 019·4 020·6 004·3 005·1 010·0 006·0 003·7 998·1 002·5 017·9 998·1 002·5 004·1 004·1 004·5 003·7 999-6 008·3 016·1 007·4	mb. 013·5 019·7 020·7 001·5 003·7 005·8 010·0 006·0 004·0 997·7 995·0 994·3 998·2 003·2 004·1 004·7 003·2 009·0 016·7 006·1	b = 1 mb. 013·9 020·2 020·6 011·4 003·8 004·6 006·1 004·3 997·6 995·1 998·3 003·6 018·2 014·9 004·6 002·9 004·1 004·6 002·9 995·3 009·5 009·5	mb. 014·3 020·5 011·1 004·0 004·7 003·5 006·8 009·8 006·1 004·7 995·1 995·2 998·4 004·4 018·7 004·0 002·6 001·3 009·6 003·7 995·1 009·9	metre mb. o14:9 o20:7 o20:3 o10:5 o04:2 o04:6 o07:3 o09:3 o06:1 o04:7 o997:3 o995:4 o05:1 o18:9 o04:4 o05:1 o18:9 o04:4 o05:1 o18:0 o09:7 o18:2 o002:7 o995:1 o18:2 o002:7 o995:1 o18:2 o002:7 o995:1 o18:2 o002:7 o995:1 o18:2 o002:7 o18:2 o002:7 o995:1 o18:2 o002:7 o995:1 o18:2 o002:7 o995:1 o18:2 o002:7 o995:1 o18:2 o002:7 o995:1 o18:2 o002:7 o995:1 o18:2 o002:7 o995:1 o18:2 o002:7 o995:1 o18:2 o002:7 o995:1 o18:2 o002:7 o995:1 o18:2 o002:7 o002:7 o0	mb. 015·1 021·0 021·0 021·0 000·3 6 000·3 6 000·5 9 005·9 005·8 018·9 005·8 018·1 004·1 004·1 004·1 0001·2	mb. 015·2020·8 019·99 004·5 000·5 4 019·0 000·1 000·1 000·1 000·1 000·1 010·1 018·2 000·8 0995·2 010·9 000·8	mb. 015·0 020·6 019·3 008·4 003·7 008·1 007·8 004·7 994·7 995·9 998·2 006·6 018·8 012·5 004·1 999·6 002·8 010·3 018·0 000·2 994·4 010·8	mb. 015 · 2 020 · 2 018 · 5 03 · 6 004 · 3 094 · 1 093 · 8 003 · 7 001 · 8 003 · 7 001 · 8 001 · 7 001 · 7 0	mb. 015-1 020-1 017-9 007-3 004-2 004-1 003-5 008-5 007-0 004-3 004-2 993-8 993-3 995-9 998-1 007-7 018-6 004-1 003-3 004-2 004-1 007-7 018-6 004-1 003-3 010-2 010-6 0095-7 010-6	mb. 015·1 019·9 016·9 006·9 004·1 003·8 006·4 006·4 004·2 003·7 993·7 992·7 996·1 098·0 003·5 010·0 007·3 998·4 996·9 950·3 30	mb. 015·2 019·9 016·6	mb. 015.6 020.1 016.3 005.9 004.0 003.6 003.4 008.8 005.7 003.7 003.3 993.7 003.8 009.7 018.1 009.7 009.8 00	mb. 016·2 020·4 016·2 003·5 003·7 009·1 005·7 099·1 008·9 008·9 008·9 009·9 009·9 0010·7 0016·7 0997·4	mb. 016-8 020-6 01	mb. 017:4 020:9 004:6 003:8 004:7 009:9 005:9 007:8 012:8 004:9 004:4 004:9 004:4 006:2 001:8 006:2 001:8 006:3 006:3 007:0 007:	mb. 017.7 021.3 005.6 004.9 010.3 005.9 004.3 002.5 995.4 992.2 997.9 999.5 013.9 004.9 004.9 004.9 004.9 004.9 006.1	mb. 018·0 021·5 005·2 004·6 005·2 004·6 005·9 003·9 002·1 995·4 998·1 990·9 004·7 018·3 004·9 005·2 098·4 007·5 016·0 0998·1	mb. 018:4 014:9 021:4 004:9 004:6 003:6 003:6 003:6 003:6 003:3 001:4 995:6 992:7 998:2 018:1 005:0 005:1 998:3 007:9 004:1 006:1	mb. o18.8 c21.2 o14.4 cc4.5 co3.6 cc4.6 cc4.5 co5.8 co3.6 co5.8 co3.6 co5.9 cc0.6 s95.5 s93.1 cc6.5 o17.8 cc6.8 cc6.8 cc6.8 cc6.8 cc6.8 cc6.8 cc6.8 cc6.8 cc6.8 cc6.8 cc6.8 cc	23. mb. 015·2 020·2 018·5 008·8 004·2 004·1 007·7 007·9 004·9 003·6 996·3 893·7 995·7 998·5 007·1 018·0 012·2 004·4 004·3 000·6 002·7 0010·1 016·7 002·5
385.	Rich 1 2 3 4 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	mond mb. o13·5 o21·0 o13·8 o21·0 o13·8 o24·4 o3·5 o4·8 o10·3 o5·7 o3·9 o1·0 o3·5 o3·9 o1·0 o1·3 o5·9 o5·0 o14·3 o13·5 o11·0 o10·2 o1	mb. ol3;3 ol8;9 ol2;0 ol4;1 ol2;0 ol4;4 ol3;2 ol4;8 ol0;2 ol5;9 ol6;0 ol6;3 ol6;7 ol5;0 ol6;3 ol6;7 ol5;0 ol6;3 ol6;7 ol6;0 ol6;3 ol6;7 ol7;0 ol	mb. o13:20:19:10 o19:10 o03:09:10 o03:09 o04:10 o03:00 o04:8 o10:20 o05:8 o03:6 999:1 o01:4 o04:9 o04:9 o03:6 o06:4 o04:9 o06:6 o06:	mb. 012·9 019·0 020·5 011·7 003·7 004·2 003·0 005·8 001·7 006·9 016·1 004·0 004·5 003·4 999·2 006·9 001·0 009·4	mb. 013·2 019·4 002·6 001·5 003·6 004·3 002·9 005·1 010·0 006·0 003·7 998·1 004·5 004·5 003·2 999·6 008·3 016·1 007·4 995·2 007·8 009·3	mb. 013·5 019·7 011·5 003·7 004·3 003·0 005·8 010·0 006·0 004·0 997·7 995·3 998·2 003·2 009·0 016·7 006·1 995·4 008·6	b = 1 mb. o13·9 o20·2 o20·6 o11·4 o03·8 o04·6 o03·2 o06·2 o10·0 o06·1 o04·3 997·6 995·1 995·1 o04·6 o02·9 o04·1 o04·6 o02·9 o04·1 o04·6 o02·9 o04·1 o04·6 o02·9 o00·8 o09·5 o11·8 o09·5	mb. 014·3 3020·5 0020·6 011·1 004·0 004·7 997·7 995·1 998·4 004·4 004·0 002·6 0013·3 009·6 0018·0 003·7 995·1 009·9 000009·2 000009·2 000009·2 000009·2 000009·2 0000000000	metro mb. o14·9 o20·7 o20·3 o10·5 o04·2 o04·6 o03·5 o07·3 o09·3 o06·1 o04·7 997·3 995·4 998·4 o05·1 o01·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o00009·7 o00009·7 o0009·7 o0009·7 o00009·7 o0009·7 o0009·7 o00009·7 o0009·7	mb. 015-11 021-0 020-3 000-9 004-6 003-6 007-5 008-9 005-9 004-8 996-7 9994-8 998-3 005-8 001-2 002-1 004-1	mb. o15:2:020:8 o19:99 o09:2:004:7 o04:4:003:8 o07:9 o08:2:005:4 o04:99 995:3 994:5:09 004:5 o00:5:000:1 o00:5:000	mb. 015.0 020.6 019.3 008.4 004.6 004.7 008.1 007.8 004.7 994.7 994.7 994.9 999.6 006.6 018.8 012.5 004.0 004.1	mb. o15 · 2 o20 · 2 o18 · 5 o07 · 8 o04 · 3 o04 · 2 o03 · 6 o08 · 4 o07 · 4 o04 · 5 g94 · 1 g93 · 8 o04 · 1 o03 · 7 o11 · 8 o04 · 1 o03 · 7 g99 · 6 g99 · 6 g99 · 6 g99 · 6 g99 · 7 g010 · 8 g01	mb. 015-1 1017-19 1017	mb. 015·1 019·9 006·9 004·1 003·8 003·4 006·4 004·2 003·7 993·7 998·0 008·2 0018·3 0010·1 003·8 002·6 009·4 009·9 0009·4	mb. 015-2 019-9 016-6 006-4 003-9 003-4 003-3 008-4 006-1 003-9 003-5 993-6 992-1 997-8 008-7 0018-0 009-5 004-0 009-5 010-1 017-0 0998-2 0997-7 010-1 0017-0 009-5 0009-5	mb. 615-6 6020-11 6016-3 605-9 6003-6 6003-6 6003-7 6020-7	mb. o16·2 o20·4 o16·2 co6·1 o04·2 co3·5 co3·7 co9·1 o05·7 co3·7 co16·1 o04·2 o10·5 o18·4 co8·9 co4·0 co3·5 co10·2 co10·7	mb. 016-8 020-6 016-2 006-1 004-6 003-7 004-1 009-5 005-7 003-9 003-0 994-8 9997-1 998-6 011-6 004-3 004-0 998-0 005-4 011-4 008-6 0010-6 0010-6 0010-9 009-9	mb. 017:4 020:9 004:6 003:8 004:7 009:9 005:9 004:3 003:0 995:5 999:9 999:1 012:8 018:5 008:4 004:9 004:4 998:4 006:2 011:8 011:0 01	mb. o17·77 o21·33 o16·1 c05·6 c04·6 c03·7 o04·9 o10·3 c05·9 c04·3 c02·5 995·4 999·9 o04·9 c04·9	mb. o18 o o21 o o21 o o15 o co5 o co4 o o3 o co4 o o3 o o3 o co5 o o3 o o3 o o3 o o3 o o3 o o3 o o3 o	mb. o18.4 021.4 021.4 021.4 021.4 026.0 03.6 003.6 003.6 003.6 003.6 003.3 001.4 995.6 992.7 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 0016.3 0016	mb. o18.82 c21.24 cc4.65 co3.67 co5.88 co3.55 co1.66 s95.55 s93.1 co6.55 co5.16 co5.10	23. mb. o15.2 020.2 o18.5 co8.8 co4.2 co4.1 co3.7 co7.7 co7.9 co4.9 co3.6 g96.3 g98.7 g98.5 co7.1 o18.0 o18.0 co4.4 co4.3 co6.6 co2.7 co7.9 co6.7 co7.9 co7.9 co7.9 co7.9 co7.9 co7.9 co7.9 co7.9 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.1 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.1 co7.9 co7.9 co7.9 co7.1 co7.9 co7
385.	Rich 1 2 3 4 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	mond mb. o13·5 o21·0 o13·8 o21·0 o13·8 o24·4 o3·5 o4·8 o10·3 o5·7 o3·9 o1·0 o3·5 o3·9 o1·0 o1·3 o5·9 o5·0 o14·3 o13·5 o11·0 o10·2 o1	mb. ol3;3 ol8;9 ol2;0 ol4;1 ol2;0 ol4;4 ol3;2 ol4;8 ol0;2 ol5;9 ol6;0 ol6;3 ol6;7 ol5;0 ol6;3 ol6;7 ol5;0 ol6;3 ol6;7 ol6;0 ol6;3 ol6;7 ol7;0 ol	mb. o13:20:19:10 o19:10 o03:09:10 o03:09 o04:10 o03:00 o04:8 o10:20 o05:8 o03:6 999:1 o01:4 o04:9 o04:9 o03:6 o06:4 o04:9 o06:6 o06:	mb. 012·9 019·0 020·5 011·7 003·7 004·2 003·0 005·8 001·7 006·9 016·1 004·0 004·5 003·4 999·2 006·9 001·0 009·4	mb. 013·2 019·4 002·6 001·5 003·6 004·3 002·9 005·1 010·0 006·0 003·7 998·1 004·5 004·5 003·2 999·6 008·3 016·1 007·4 995·2 007·8	mb. 013·5 019·7 011·5 003·7 004·3 003·0 005·8 010·0 006·0 004·0 997·7 995·3 998·2 003·2 009·0 016·7 006·1 995·4 008·6	b = 1 mb. 013·9 020·2 020·6 011·4 003·8 004·6 006·1 004·3 997·6 995·1 998·3 003·6 018·2 014·9 004·6 002·9 004·1 004·6 002·9 995·3 009·5 009·5	mb. 014·3 3020·5 0020·6 011·1 004·0 004·7 997·7 995·1 998·4 004·4 004·0 002·6 0013·3 009·6 0018·0 003·7 995·1 009·9 000009·2 000009·2 000009·2 000009·2 000009·2 0000000000	metro mb. o14·9 o20·7 o20·3 o10·5 o04·2 o04·6 o03·5 o07·3 o09·3 o06·1 o04·7 997·3 995·4 998·4 o05·1 o01·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o01·8 o09·7 o00009·7 o00009·7 o0009·7 o0009·7 o00009·7 o0009·7 o0009·7 o00009·7 o0009·7	mb. 015-11 021-0 020-3 000-9 004-6 003-6 007-5 008-9 005-9 004-8 996-7 9994-8 998-3 005-8 001-2 002-1 004-1	mb. o15:2:020:8 o19:99 o09:2:004:7 o04:4:003:8 o07:9 o08:2:005:4 o04:99 995:3 994:5:09 004:5 o00:5:000:1 o00:5:000	mb. 015.0 020.6 019.3 008.4 004.6 004.7 008.1 007.8 004.7 994.7 994.7 994.9 999.6 006.6 018.8 012.5 004.0 004.1	mb. o15 · 2 o20 · 2 o18 · 5 o07 · 8 o04 · 3 o04 · 2 o03 · 6 o08 · 4 o07 · 4 o04 · 5 g94 · 1 g93 · 8 o04 · 1 o03 · 7 o11 · 8 o04 · 1 o03 · 7 g99 · 6 g99 · 6 g99 · 6 g99 · 6 g99 · 7 g010 · 8 g01	mb. 015-1 1017-19 1017	mb. 015·1 019·9 006·9 004·1 003·8 003·4 006·4 004·2 003·7 993·7 998·0 008·2 0018·3 0010·1 003·8 002·6 009·4 009·9 0009·4	mb. 015-2 019-9 016-6 006-4 003-9 003-4 003-3 008-4 006-1 003-9 003-5 993-6 992-1 997-8 008-7 0018-0 009-5 004-0 009-5 010-1 017-0 0998-2 0997-7 010-1 0017-0 009-5 0009-5	mb. 615-6 6020-11 6016-3 605-9 6003-6 6003-6 6003-7 6020-7	mb. o16·2 o20·4 o16·2 co6·1 o04·2 co3·5 co3·7 co9·1 o05·7 co3·7 co16·1 o04·2 o10·5 o18·4 co8·9 co4·0 co3·5 co10·2 co10·7	mb. 016-8 020-6 016-2 006-1 004-6 003-7 004-1 009-5 005-7 003-9 003-0 994-8 9997-1 998-6 011-6 004-3 004-0 998-0 005-4 011-4 008-6 0010-6 0010-6 0010-9 009-9	mb. 017:4 020:9 004:6 003:8 004:7 009:9 005:9 004:3 003:0 995:5 999:9 999:1 012:8 018:5 008:4 004:9 004:4 998:4 006:2 011:8 011:0 01	mb. o17·77 o21·33 o16·1 c05·6 c04·6 c03·7 o04·9 o10·3 c05·9 c04·3 c02·5 995·4 999·9 o04·9 c04·9	mb. o18 o o21 o o21 o o15 o co5 o co4 o o3 o co4 o o3 o o3 o co5 o o3 o o3 o o3 o o3 o o3 o o3 o o3 o	mb. o18.4 021.4 021.4 021.4 021.4 026.0 03.6 003.6 003.6 003.6 003.6 003.3 001.4 995.6 992.7 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 018.1 000.3 0015.2 0016.3 0016	mb. o18.82 c21.24 cc4.65 co3.67 co5.88 co3.55 co1.66 s95.55 s93.1 co6.55 co5.16 co5.10	23. mb. o15.2 020.2 o18.5 co8.8 co4.2 co4.1 co3.7 co7.7 co7.9 co4.9 co3.6 g96.3 g98.7 g98.5 co7.1 o18.0 o18.0 co4.4 co4.3 co6.6 co2.7 co7.9 co6.7 co7.9 co7.9 co7.9 co7.9 co7.9 co7.9 co7.9 co7.9 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.1 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.1 co7.9 co7.9 co7.9 co7.1 co7.9 co7
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385.	Rich 1 2 3 4 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mond mb. 013·5 018·7 021·0 013·8 004·3 004·4 003·5 004·8 010·3 005·7 003·9 001·0 995·3 993·2 998·2 000·6 016·0 017·3 005·0 004·3 998·4 008·1 014·3 013·5 997·3 005·0 010·2 010·9	mb. o13·33 o18·9 o13·30 o18·9 o13·0 o04·1 o04·4 o05·9 o05·9 o05·9 o05·9 o06·1 o05·0 o04·2 o05·0 o04·2 o05·0 o04·2 o05·0 o06·1 o05·0 o06·1 o05·0 o06·1	mb. 013-2 019-1 020-7 020-7 003-9 004-1 005-8 003-6 999-1 994-4 993-3 998-7 001-6 016-6 01	mb. 012·9 019·0 020·5 0011·7 003·7 004·2 003·0 004·8 010·0 005·8 003·5 998·4 994·0 993·6 998·0 001·7 016·9 016·1 004·2 008·2 016·0 009·0 009·3 009	mb. 013·2 019·4 020·6 004·3 005·1 010·0 006·0 003·7 998·1 002·5 017·9 993·9 015·6 004·1 004·5 003·2 007·4 995·2 007·8 011·0 009·3 011·1	mb. 013·50 019·70 0013·50 003·70 004·30 005·8 010·00 006·00 004·00 997·7 995·00 994·3 998·2 003·2 018·1 004·1 004·7 006·1 995·4 008·6 011·4 009·3 011·5	b = 1 mb. o13·9 o20·2 o20·6 o11·4 o03·8 o04·6 o03·2 o06·2 o10·0 o06·1 o04·3 997·6 995·1 995·1 o04·6 o02·9 o04·1 o04·6 o02·9 o04·1 o04·6 o02·9 o04·1 o04·6 o02·9 o00·8 o09·5 o11·8 o09·5	mb. 014·3 020·5 0011·1 004·0 004·7 003·5 006·8 009·8 006·1 004·7 997·7 995·1 995·2 998·4 004·4 018·7 004·0 004·6 001·3 009·6 018·0 003·7 995·1 009·9 0012·0 009·9 012·2 012·2	metre mb. ol4:9 o20:7 o20:3 o10:5 o04:2 o04:6 o03:5 o07:3 o09:3 o06:1 o04:7 997:3 994:9 995:4 998:4 o05:1 o18:9 o04:4 o05:1 o18:9 o04:7 o01:8 o09:7 o01:8 o09:7 o01:8 o09:7 o01:8 o09:7 o01:8 o09:7 o01:8 o09:7 o01:8 o09:7 o01:8 o09:7 o01:8 o09:7 o0	mb. 015·1 021·0 021·0 021·0 020·3 000·9 004·6 003·6 007·5 008·9 005·9 004·8 996·7 994·8 995·6 998·3 005·8 018·9 004·1 004·1 004·1 004·1 004·1 0001·2 002·1 010·1 010·1 0001·2 0001·2 0001·3 000	mb. 015-2020-8 9009-2 004-7 004-4 003-8 007-9 908-2 005-4 004-5 000-5 000-5 000-1 018-2 000-8 995-2 019-0 011-5 000-1 018-2 019-0 005-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 019-0 006-5 009-1 018-2 00	mb. 015.0 020.6 019.3 008.4 004.6 004.7 008.1 007.8 004.7 994.7 994.2 995.9 998.2 006.6 018.8 012.5 004.0 004.1 999.6 002.8 010.3 018.0 000.2 010.8 011.4 009.5 013.7 1006	mb. 015·2 020·2 018·5 007·8 004·3 004·5 004·5 004·5 007·2 018·7 001·8 003·7 0099·6 0099·6 0099·6 0010·8 0009·4 0013·9 0010·8 0009·4 0013·9 0010·8 0009·4 0013·9 0010·8 0009·4 0013·9 0010·8 0009·4 0013·9 0010·8 0009·4 0010·8 0009·4 0010·8 0009·4 0010·8 0009·4 0010·8 0009·4 0010·8 0009·4 0010·8 0009·4 0010·8 0009·4 0010·8 0009·4 0010·8 0009·4 0010·8 0009·4 0010·8 0009·4 0010·8 0009·4 0010·8 001	mb. 015-1 020-1 1 020-1 1 020-1 1 020-1 1 017-9 007-3 004-2 004-1 003-5 007-0 004-3 004-2 993-8 995-3 995-9 998-1 007-7 18-66 004-1 003-3 010-2 017-7 9999-0 005-7 010-6 009-3 0113-7 0006 1 0006-1 00	mb. 015·1 019·9 016·9 006·9 006·4 00	mb. 015·2 019·9 016·6 006·4 003·9 003·5 993·6 992·1 0000·5 000000000000000000000000000000	mb. 015-6 020-1 016-3 005-9 004-0 003-6 003-4 008-8 005-7 003-7 003-3 993-7 992-0 996-4 997-8 009-2 004-0 003-3 997-8 003-2 004-0 003-3 997-8 003-9 010-4 009-9 0114-6	mb. 016·2 020·4 016·2 003·5 003·7 009·1 005·7 099·1 0010·5 010·5 010·7 0997·4 0999·5 010·2 0009·8 0010·7 0010·2 0009·8 0010·7	mb. 016-8 020-6 010-2 000-115-3 000-15-3 000-15-3 000-15-8 000-15-3 000-16-8 000-16-9 000-16-	mb. 017:4 020:9 004:6 003:8 004:7 0095:9 004:3 003:0 995:5 997:9 997:1 012:8 008:4 004:9 004:4 006:2 011:8 001:9 001:0 010:7 0	mb. 017-7 021-3 016-1 005-6 004-9 010-3 005-9 004-3 007-9 004-9 004-9 004-6 098-3 007-1 010-9 0010-6 010-6 010-6 010-6	mb. 018·0 021·5 015·6 005·2 004·6 003·6 005·9 003·9 002·1 995·4 998·1 998·1 007·5 0012·5 0016·0 0998·1 0010·9 0010·9 0010·9 0010·9 0010·5	mb. 018:4 021:4 004:9 004:9 006:0 003:6 003:6 003:6 003:6 003:3 001:4 995:6 992:7 998:2 006:0 005:1 998:3 007:9 004:1 011:2 010:6 010:6 010:6	mb. o18.8 c21.2 o14.4 cc4.5 co4.6 cc4.5 co5.8 co3.6 co3.6 co5.8 co3.6 co5.9 co5.9 co5.9 co5.9 co6.1 co5.0 co6.1 co5.0 co6.1 co5.0 co6.1 co5.0 co6.1 co5.0 co6.1 co5.0 co6.1 co	23. mb. o15·2 020·2 o18·5 c08·8 c04·2 c04·1 c03·6 g96·3 g98·5 c07·1 o18·0 o12·2 c04·1 o18·0 o12·2 c04·1 o18·0 o12·2 c04·1 o18·0 o18
Station Tevel.	Rich I 2 3 4 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 1 level)	mond mb. 013·5 018·7 021·0 013·8 004·4 003·5 004·8 010·3 005·7 003·9 001·0 095·3 095·3 005·0 017·3 005·9 005·0 004·3 998·4 010·3 013·5 997·3 005·0 011·0 010·2 010·9 010·9 010·9 010·9 010·9 01008 01008 01008 01008 01008 01008 01008 01008 01008 01008 01008 01008 01008 01008 01008 01008	mb. 013:3 018:9 020:88 013:0 004:1 004:4 005:9 003:2 005:9 000:5 993:2 998:1 001:0 004:2 005:0 004:2 998:5 008:0 014:9 0012:2 0099:1 001:0 005:1 005:0 004:2 005:0 004:2 005:0 004:2 005:0 004:2 005:0 004:2 005:0 005:0 006:0 005:0 006:0	mb. 013·2 019·1 020·7 004·1 020·7 004·8 010·2 005·8 010·2 005·8 003·6 999·1 994·4 016·6 016·4 004·9 003·6 998·7 015·6 010·6 0996·2 006·3 011·0 00997 010·9 01006 068	mb. 012·9 019·0 020·5 0011·0 009·4 011·2 009·4 1006 054 1006 0554 1007 1	mb. 013·2 019·4 020·6 004·3 005·1 010·0 006·0 003·7 998·1 002·5 017·9 908·1 004·5 003·2 007·4 995·2 007·8 011·0 009·3 011·0 009·3 011·0 009·3	mb. 013·5 019·7 020·7 020·7 020·7 020·7 004·3 005·8 010·0 005·8 010·0 004·0 997·7 995·0 994·3 998·2 003·2 018·1 004·7 003·2 000-2 009·0 016·7 006·1 995·4 008·6 011·4 009·3 011·5 1006 -81	b = 1 mb. o13·9 o20·2 o20·6 o11·4 oo3·8 oo4·6 oo3·2 o10·0 oo6·1 oo4·3 997·6 995·1 998·3 oo3·6 oo14·9 oo4·6 oo2·9 oo4·9 oo5 oo7·5 oo4·9 oo9·5 oo1·8 oo9·5 oo1·8 oo9·5 oo1·8 oo9·5 oo1·8 oo9·5 oo1·8 oo9·5 oo1·8 oo9·5 oo1·8 oo9·5 oo1·8 oo9·5 oo1·8 oo9·5 oo1·8 oo9·5 oo1·8 oo9·5 oo1·8 oo9·5 oo1·8 oo9·5 oo1·8 oo9·5 oo1·8	mb. ol4:3 ol4:3 ol20:5 ol20:6	metre mb. o14·9 o20·7 o10·0 o14·9 o20·7 o10·0 o14·9 o20·0 o14·9 o14·0 o14·7 o10·0 o14·0 o14·7 o10·0 o10·0 o1	mb. 015·11 021·0 0	mb. 015-2020-8 019-9 009-2 009-2 009-2 009-2 009-2 005-4 004-9 995-3 994-5 996-0 013-4 003-9 004-5 000-5 000-1 1018-2 000-8 995-2 019-0 019-1 018-2 000-6 019-1 018-2 01	mb. 015·0 020·6 019·3 008·4 004·6 004·7 008·1 007·8 004·7 994·7 994·2 995·9 998·2 006·6 018·8 012·5 004·1 999·6 002·8 010·3 010·3 011·4 009·5 013·7 01006 1 000·2	mb. 015:2 020:2 018:5 03:6	mb. 015·1 020·1 017·9 007·3 004·2 004·1 003·5 007·0 004·3 004·2 993·8 993·3 995·9 998·1 007·7 018·6 003·3 004·2 1003·3 004·1 003·1 004·1 004·1 004·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 0	mb. 015·1 019·9 016·9 006·9 004·1 003·7 993·7 992·7 996·1 998·0 008·2 018·3 010·1 003·8 002·6 017·3 998·4 996·9 010·3 010·9 010·	mb. 015·2 016·6	mb. 015.6 020.1 016.3 005.9 004.0 003.4 008.8 005.7 003.3 993.7 992.0 996.4 997.8 009.7 018.1 009.2 0004.0 0003.3 997.8 009.7 018.1 009.2 010.4 009.9 010.4 009.9 010.4 009.9 010.4 009.9	mb. 016·2 020·4 016·2 003·5 003·5 003·7 003·7 002·8 994·1 991·6 996·7 998·2 010·5 018·4 008·9 004·0 003·5 016·7 0997·4 999·5 010·2 009·8 0010·2 009·8 0010·2 009·8 0010·2 009·8 0010·2 009·8 0010·3	mb. 016-8 020-6 006-1 004-6 003-7 004-1 009-5 005-7 003-9 994-8 991-7 997-1 998-6 011-6 018-4 008-6 011-6 01	mb. o17.4 o20.9 o16.3 o05.9 o04.9 o05.9 o04.4 o04.9 o04.9 o04.9 o06.2 o11.5 o06.2 o11.5 o06.2 o11.5 o06.2	mb. 017.7 021.3 016.1 016.1 016.1 005.6 004.9 010.3 005.9 004.3 002.5 995.4 992.2 997.9 013.9 013.9 014.9 004.9 004.6 1010.9 010.6 016.2 0007 1.18	mb. 018·0 021·5 021·5 005·2 004·6 003·6 005·9 003·9 002·1 995·4 998·1 998·1 007·5 006·0 998·1 0010·9 010·8 011·0 010·9 010·8 011·0 010·9 010·8 010·8 010·9 010·8 010·9 010·8 010·9 010·8 010·9 010·8 010·8 010·9 010·8 0	mb. 018:4 021:4 014:9 021:4 014:9 016:0 003:6 003:6 003:6 003:3 001:4 995:6 992:7 998:2 018:1 006:8 005:0 005:0 015:2 010:6 010:8 01	mb. 018.8 021.2 014.4 016.4 016.4 016.5 016.5 017.8 006.5 017.8 006.5 017.8 006.5 017.1 007.1 007.2	23. mb. o15·2 020·2 o18·5 c08·8 c04·2 c04·1 c03·6 g96·3 g98·7 g95·7 g98·5 c07·1 o18·0 o012·2 c04·4 o04·3 o00-6 o02·7 o016·7 o02·5 o11·0 o09·7 o13·5 c06 ·77 c008
Station Tevel.	Rich I 2 3 4 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 1 level)	mond mb. 013·5 018·7 021·0 013·8 004·4 003·5 004·8 010·3 005·7 003·9 005·0 014·3 005·9 005·0 014·3 005·9 001·0 014·3 013·5	mb. 013:3 018:9 020:88 013:0 004:1 004:4 010:2 005:9 000:5 993:2 998:1 001:0 004:2 005:1 005:0 004:2 998:5 008:0 014:9 0010:0 004:2 005:0 004:2 005:0 004:0 005:1 005:0 004:0 005:1 005:0 004:0 005:1 005:0 004:0 005:1 005:0 004:0 005:1 005:0 004:0 005:1 005:0 004:0 005:1 005:0 004:0 005:0	mb. 013·2 019·1 020·7 004·1 020·7 004·8 010·2 005·8 010·2 005·8 003·6 999·1 994·4 016·6 016·4 004·9 003·6 998·7 015·6 010·6 0996·2 006·3 011·0 00997 010·9 01006 068	mb. 012·9 019·0 020·5 0011·0 009·4 011·2 009·4 011·2 009·4 011·2 006 054	mb. 013·2 019·4 020·6 004·3 005·1 010·0 006·0 003·7 998·1 002·5 017·9 908·1 004·5 003·2 007·4 995·2 007·8 011·0 009·3 011·0 009·3 011·0 009·3	mb. 013·5 019·7 020·7 020·7 020·7 020·7 004·3 005·8 010·0 005·8 010·0 004·0 997·7 995·0 994·3 998·2 003·2 018·1 004·7 003·2 000-2 009·0 016·7 006·1 995·4 008·6 011·4 009·3 011·5 1006 -81	b = 1 mb. 013·9 020·2 020·6 011·4 003·8 004·6 003·2 010·0 995·1 995·0 998·3 003·6 018·2 014·9 004·1 004·6 002·9 004·1 004·6 002·9 004·1 004·6 002·9 004·1 004·6 002·9 004·1 004·6 002·9 004·1 004·6 002·9 004·1 004·6	mb. ol4:3 ol4:3 ol20:5 ol20:6	metre mb. o14·9 o20·7 o10·0 o14·9 o20·7 o10·0 o14·9 o20·0 o14·2 o10·0 o14·2 o10·0 o14·2 o10·0 o14·2 o10·0 o14·3 o1	mb. 015·11 021·0 021·0 0021·0 0021·0 0004·6 003·6 007·5 008·9 005·9 004·8 999·7 994·8 995·6 998·3 005·8 018·9 014·11 004·5 001·2 002·11 108·3 001·7 0011·8 0099·0 013·3 0009·0 013·3 0009·0 013·3 0009·0 0009·0 00000000	mb. 015-2020-8 019-9 009-2 009-2 009-2 009-2 009-2 005-4 004-9 995-3 994-5 996-0 013-4 003-9 004-5 000-5 000-1 1018-2 000-8 995-2 019-0 019-1 018-2 000-6 019-1 018-2 01	mb. 015·0 020·6 019·3 008·4 004·6 004·7 008·1 007·8 004·7 994·7 994·2 995·9 998·2 006·6 018·8 012·5 004·1 999·6 002·8 010·3 010·3 011·4 009·5 013·7 01006 1 000·2	mb. 015:2 020:2 018:5 03:6	mb. 015·1 020·1 017·9 007·3 004·2 004·1 003·5 007·0 004·3 004·2 993·8 993·3 995·9 998·1 007·7 018·6 003·3 004·2 1003·3 004·1 003·1 004·1 004·1 004·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 005·1 0	mb. 015·1 019·9 016·9 006·9 004·1 003·7 993·7 992·7 996·1 998·0 008·2 018·3 010·1 003·8 002·6 017·3 998·4 996·9 010·3 010·9 010·	mb. 015·2 019·9 016·6 006·4 003·9 003·5 993·6 992·1 996·2 997·8 008·7 018·0 009·5 0004·0 002·8 098·0 0010·1 017·0 098·2 0997·7 018·0 009·5 0004·0 002·8 0004·0 0004·0 0004·0 0004·0 0004·0 00000000	mb. 015.6 020.1 016.3 005.9 004.0 003.4 008.8 005.7 003.3 993.7 992.0 996.4 997.8 009.7 018.1 009.2 0004.0 0003.3 997.8 009.7 018.1 009.2 010.4 009.9 010.4 009.9 010.4 009.9 010.4 009.9	mb. 016·2 020·4 016·2 003·5 003·5 003·7 003·7 002·8 994·1 991·6 996·7 998·2 010·5 018·4 008·9 004·0 003·5 016·7 0997·4 999·5 010·2 009·8 0010·2 009·8 0010·2 009·8 0010·2 009·8 0010·2 009·8 0010·3	mb. 016-8 020-6 006-1 004-6 003-7 004-1 009-5 005-7 003-9 003-0 994-8 991-7 997-1 998-6 011-6 018-4 008-6 018-4 008-6 011-6 010-6 01	mb. 017·4 020·9 004·9 005·9 004·4 0995·5 9997·1 012·8 018·5 008·4 004·9 004·4 0998·4 0011·0 010·3 0015·9 0010·3 0015·9 0010·3	mb. 017.7 021.3 016.1 016.1 016.1 005.6 004.9 010.3 005.9 004.3 002.5 995.4 992.2 997.9 013.9 013.9 014.9 004.9 004.6 1010.9 010.6 016.2 0007 1.18	mb. 018·0 021·5 021·5 005·2 004·6 003·6 010·4 005·9 003·9 014·7 018·3 007·5 004·9 0012·5 016·0 0998·1 010·9 010·8 011·0 010·9 010·8 011·0 010·9 010·8 011·0 010·9 010·8 011·0	mb. 018:4 021:4 014:9 021:4 014:9 016:0 003:6 004:6 003:6 003:3 001:4 995:6 992:7 998:2 000:1 998:3 0015:2 018:1 000:1 0	mb. 018.8 021.2 014.4 016.4 016.6 016.5 016.6 016.5 017.8 016.5 017.8 016.5 017.8 016.5 017.8 01	23. mb. 015·2 020·2 018·5 020·2 018·5 020·7 020
Station Tevel.	Rich 1 2 3 4 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 1 level)	mond mb. 013·5 018·7 021·0 013·8 004·4 003·5 004·8 010·3 005·7 003·9 001·0 095·3 095·3 005·0 017·3 005·9 005·0 004·3 998·4 008·1 014·3 013·5 997·3 005·0 011·0 010·2 010·9 010·9 010·9 010·9 01008 01008 01008 01008 01008 01008 01008 01008 01008 01008 01008	mb. 013:3 018:9 020:88 013:0 004:1 004:4 005:9 003:2 005:9 000:5 993:2 998:1 001:0 004:2 005:0 004:2 998:5 008:0 014:9 0012:2 0099:1 001:0 005:1 005:0 004:2 005:0 004:2 005:0 004:2 005:0 004:2 005:0 004:2 005:0 005:0 006:0 005:0 006:0	mb. 013·2 019·1 020·7 004·1 000-7 004·8 010·2 005·8 003·6 999·1 994·4 993·3 998·1 001·4 004·9 004·9 004·9 005·6 010·6 010·6 010·6 010·6 010·6 010·6 010·6 010·6 010·6	mb. 012·9 019·0 020·5 0011·0 009·4 011·2 009·4 1006 054 1006 0554 1007 1	mb. 013·2 019·4 020·6 004·3 005·1 010·0 006·0 003·7 998·1 002·5 017·9 998·1 002·5 017·9 998·1 002·5 017·9 003·7 998·1 004·1 004·5 003·7 999·6 003·7 00	mb. 013·5 019·7 020·7 020·7 020·7 000-3 005·8 010·0 006·0 004·0 997·7 995·0 994·3 998·2 003·2 018·1 004·7 003·2 000-2 000-0 016·7 006·1 995·4 008·6 011·4 009·3 011·5 1006 -81	b = 1 mb. 013·9 020·2 020·6 03·8 004·6 003·2 010·0 995·1 995·0 998·3 003·6 018·2 014·9 004·6 002·9 004·6 002·9 004·6 0017·5 004·9 995·3 009·5 011·8 009·2 011·8 0196 1006	mb. 014·3 020·5 020·6 020·6 020·6 020·6 020·6 020·6 020·6 020·6 020·6 020·6 020·6 030·7 095·1 004·0 00	metro mb. o14·9 o20·7 o20·3 o10·5 o04·2 o04·6 o03·5 o07·3 o09·3 o06·1 o04·7 o997·3 o995·4 o998·4 o05·1 o18·2 o002·7 o08·1 o009 o09 o00 o00	mb. 015-11 021-0 020-3 000-9 004-6 003-6 007-5 008-9 005-9 005-8 03-6 007-5 008-9 005-8 03-6 007-7 009-5 49-10-10-10-10-10-10-10-10-10-10-10-10-10-	mb. o15:2020:8 o19:99 o09:2 o04:7 o04:4 o03:8 o07:9 o08:2 o05:4 o04:9 995:3 994:5 998:2 o06:2 o0013:4 o03:9 o004:5 o005:0 o0013:4 o007:0 o007:	mb. 015·0 020·6 019·3 008·4 004·6 004·7 008·1 007·8 004·7 994·7 994·2 995·9 998·2 006·6 018·8 012·5 004·0 004·1 999·6 002·8 010·3 018·0 000·2 994·4 010·8 011·4 009·5 013·7 0 1006 1 '70 1006 1	mb. o15 · 2 o20 · 2 o18 · 5 o7 · 8 o04 · 3 o04 · 2 o03 · 6 o08 · 4 o07 · 4 o04 · 5 g994 · 1 g998 · 3 o07 · 2 o11 · 8 o04 · 1 o03 · 7 g999 · 6 g999 · 6 g999 · 6 o10 · 8 o09 · 1 o06 · 1 o07 · 0 o77 ·	mb. 015-11 020-11 020-11 020-11 020-11 020-11 020-11 020-11 020-12 020-11 020-12 020-1	mb. 015·1 019·9 006·9 004·1 003·8 003·4 006·4 004·2 003·7 993·7 998·0 008·2 0010·1 003·8 002·6 003·8 0010·1 003·8 002·6 010·1 003·8 0010·1 003·8 0010·1 0010·	mb. 015·2 016·6	mb. 015-6 020-11 016-3 005-9 004-0 003-6 003-7 003-7 003-3 993-7 992-6 997-8 003-3 997-8 003-7 018-1 009-7 910-4 016-9 016-9 016-6 006 018 0007 18 000	mb. o16·2 o20·4 o16·2 c06·1 o04·2 c03·5 c03·7 c09·1 o05·7 c09·1 o05·7 o02·8 994·1 9916·7 998·2 o10·5 o18·4 o08·9 o04·0 o03·5 0997·4 999·5 c010·7 c016·7 c0997·4 c009·8 c010·7 c01	mb. o16-8 o16-8 o16-2 o20-6 o16-2 o06-1 o04-6 c03-7 c04-1 c09-5 c05-7 c03-9 c03-0 c03-0 c03-0 c04-0 c04-1 c098-0 c04-0 c098-0 c04-0 c098-0 c04-0 c06	mb. 017:4 020:9 016:3 005:9 004:6 003:8 004:7 005:9 005:9 004:3 018:5 008:4 004:9 004:4 006:2 011:8 001:9 011:0 010:3 001:9 011:0 00	mb. o17·77 o21·33 o16·1 c05·6 c04·6 c03·7 c04·9 o10·3 c05·9 c04·3 c02·5 g95·4 g99? g99? g99? g99? c04·9 c04·	mb. o18 · o o21 · 5 c05 · 2 c04 · 6 c03 · 6 c04 · 8 o10 · 4 c05 · 9 c02 · 1 c05 · 9 c02 · 1 c05 · 9 c05 · 2 c04 · 6 c04 · 8 c05 · 9 c05 · 2 c06 · 6 c07 · 5 c06 · 6 c07 · 5 c06 · 6 c07 · 5 c06 · 6 c07 · 7 c07 · 7 c0	mb. 018:4 021:4 014:9 021:4 014:9 016:0 003:6 003:6 003:6 003:3 001:4 995:6 992:7 998:2 018:1 006:8 005:0 005:0 015:2 010:6 010:8 01	mb. 018.8 021.2 014.4 016.4 016.4 016.5 016.5 017.8 006.5 017.8 006.5 017.8 006.5 017.1 007.1 007.2	23. mb. o15.2 020.2 o18.5 co8.8 co4.2 co4.1 co3.7 co7.7 co7.9 co4.9 co3.6 g96.3 g93.7 g95.7 g98.5 co7.1 o18.0 o12.2 co4.4 co4.3 co0.6 co2.7 co10.1 co16.7 co2.5 co97.7 co2.5 co6.7 co7.9 co3.6 co7.1 co18.0 co7.1 co18.0 co7.1 co18.0 co7.1 co18.0 co7.1 co18.0 co7.1 co18.0 co7.1 co18.0 co7.1 co18.0 co7.1 co18.0 co7.1 co6.0 co7.7 co7.9 co7.1 co6.0 co7.7 co7.9 co7.7 co7.9 co7.1 co7.7 co7.9 co7.1 co7.7 co7.9 co7.1 co7.7 co7.9 co7.1 co7.7 co7.9 co7.1 co7.7 co7.9 co7.1 co7.7 co7.9 co7.1 co7.7 co7.9 co7.1 co7.7 co7.9 co7.1 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.9 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.7 co7.9 co7.9 co7.7 co7.9 co7.9 co7.7 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7.9 co7.1 co7.9 co7

386. Richmond (Kew Observatory): H_b (height of barometer cistern above M.S.L.) = 10.4 metres.

May, 1923.

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						mb.																			
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2	022.9	022.7	022.8	022.6	022.6	022.9	023.1	023.0	023.1	023.2	022.8	022.5	022.2	022.0	021.5	021.4	021.1	021.3	021.7	022.0	022.2	021.8	021.4	021.4	102
						022.0																			
4	017.4	017.2	017.0	o16·8	016.7	016.7	016.1	015.6	015.2	014.7	014.7	014.3	014.0	014.1	014.0	013.9	013.7	014.0	014.3	014.9	015.1	015.3	015.6	015.6	j (o
5	015.2	015.0	014.8	014.7	014.5	014.3	014.0	013.8	013.2	013.5	012.8	011.8	010.7	009.2	009.0	007.3	006.4	005.2	004.5	004.8	005.5	006-2	007.0	007.5	5 01
	007.8	008.1	008.7	009.3	010.3	011.2	011.9	012.7	013.1	013.8	014.0	014.2	014.3	014.3	013.8	014.3	014.5	014.4	015.2	016.0	016-3	016.4	016-3	016-3	3 01
						016.6																			
8	o18·7	018.7	o18·6	018.0	018.0	017.9	018.0	o18∙o	017.6	017.3	016.8	019.1	015.8	015.3	015.0	014.7	013.2	012.9	012.4	011.0	011.7	011.7	011.8	010.7	7 (0:
9	010.7	010.8	010.6	010.5	010.4	010.6	010.2	010.2	010.2	010.0	009.2	008.6	007.8	007.2	006.4	005.6	005.3	005.4	005.4	005.2	005.6	005.2	005.2	co5·3	3 00
IO	005·I	004.8	005.0	005.3	005.9	006.3	006.4	006.9	007.6	008-4	008.8	008.7	009.1	009.0	008.9	008.7	008.3	007.9	007.3	006.9	006.1	004.7	003.4	C02·0	0
11	999.9	998∙0	996.7	995.9	996.0	995.7	995.1	994.3	993.8	993.2	992.7	992.5	992.6	992.7	992.8	993.5	993·5	994.5	995.1	995.7	996-3	996.7	997.0	997.2	2 91
12	997.2	997.0	997.0	997:3	997.9	998.5	999.0	999.5	000.2	000.5	000.7	001.8	003.1	002.8	003.4	003.8	004.3	co4·2	004.6	CO5.1	005.4	005.4	co5·1	co5.0	P
1 13	004.7	004.3	003.8	003.1	002.7	002.2	001.6	001.4	001.3	001.3	001.2	COI ·2	001.3	001.3	001.0	001.0	001.3	001.5	001.0	002.5	002.6	002.7	co3.c	co3.1	I CO
2 14	003.2	003.3	003.4	oo3∙6	004.0	004.9	005.5	005.9	006.2	006.6	006.8	006.7	006.6	006.6	006.5	006.4	006.3	co6·3	006.6	co6.8	co7.1	007.1	CO7.2	co6.6) c
Level 12	0 06·6	006.3	006.0	005.8	005.6	005.6	005.5	005.4	005.0	004.7	004.6	004.2	004.6	004.1	004.0	003.6	003.2	003.0	003.6	003.2	003.2	003.1	co2·9	CO2·4	c
⊈ 16	002.1	001.7	001.4	001.1	001.1	001.3	001.4	001.7	002.2	002.6	002.6	003.6	003.8	005-1	005.1	005.8	006.4	007:4	co8·o	co8·7	co9·6	010-2	010.6	010.0	c
:≓ 17 ·	011.0	011.0	010.8	010.7	010.0	011.0	011.2	011.4	011.2	011.6	012.1	012.3	012.7	013.0	012.9	013.3	013.7	014.2	015.1	015.9	016.5	017.0	017.3	017.4	l lo:
<u>ig</u> 18	017.5	017.5	017.6	017.8	017.9	018.0	018-3	o18∙6	o18·5	o18·5	o18·6	018.4	018.5	018.3	018.2	018.0	017.8	017.8	017.9	017.9	018.0	017.7	017.6	017.2	2 0
						015.2																			
20	012.0	011.8	011.2	011.3	011.3	011.4	011.2	011.7	011.3	011.1	010.8	010.5	010.1	009.7	009.7	009.6	009.3	009.2	009.3	009.2	009-2	009.0	oc8·8	co8·5	01
21	008.3	008.2	008.3	008.2	008.8	009.3	009.5	009.9	010.3	010.6	010.9	010.0	011.3	011·6	011.7	012.0	012.1	012.2	012.4	012.9	013.3	013.7	013.9	014.3	3 0 1
22	014.2	014.5	014.4	014.4	014.4	014.6	014.8	015.1	015.0	014.9	014.8	014.8	014.8	014.8	014.8	014.8	014.8	014.8	014.2	014.6	014.6	014.4	014.3	014.5	2 (0:
23	014.0	013.7	013.4	013.1	013.1	013.3	013.3	013.2	012.9	012.7	012.7	012.6	013.1	013.2	013.7	014.4	014.9	015.7	010.0	017.2	018.0	018.2	018.8	010.0	0
24	019.4	019.8	020.0	020.4	021.2	021.6	022.0	022.3	022.3	022.3	022.3	022.1	021.8	021.5	021.0	020.7	020.2	020.0	019.8	019.7	019.7	010.1	018.7	018.0	02
25	017.4	016.6	015.6	014.7	013.9	013.2	012.5	011.9	010.9	010.4	009.6	008.7	008.1	008.0	007.4	007.9	007.7	007.8	007.9	008-3	cc8·9	008.8	cc9·0	cc9·1	0:
26	008.9	008.9	008.8	008.9	009.2	009-6	010.1	010-2	010.2	010.1	010.3	010.3	010·3	010.4	010.3	010.3	010-3	010.8	011.0	011.3	011.7	011.9	012.0	012.0	o
27 28	012.0	012.4	012.6	012.7	013.0	013.6	013.4	014.1	014.2	014.4	014.2	014.7	014.8	014.9	014.9	014.9	014.9	012.3	015.4	015.6	015.9	010.0	015.7	015.6	PO:
28	015.2	014.8	014.4	014.2	014.4	014.7	014.8	014.9	014.9	015.3	014.8	014.9	014.9	015.2	015.5	012.4	010.0	010.8	017.7	018.2	018.2	019.5	019.2	019.5	0
29	010.2	019.0	018.4	o18·1	017.9	017.8	017.7	017.6	017.5	017.5	017.1	017.2	017.0	017.1	017.0	010.8	010.8	010.0	017.1	017.3	017.5	017.4	017.6	017.6	(O)
30	017.7	• 17·6	017.5	017.5	017.8	018.1	018.3	018.4	018.4	018-2	018.0	018.0	017.8	017.6	017.6	017.7	017.9	018.1	018.4	019.2	019.9	020.2	020.5	020.8	(0)
31	021.1	021.1	021.1	021.1	021.3	021.4	021.2	021.3	021.5	021.7	021.4	021.1	020.7	020.0	019.1	o18·5	018-1	017.9	018-5	018-8	019·2	019.0	019.1	019.0	02
an	1012	1012	1012	1012	1012	1012	1012	1012	1012			1012	1012	1012			1011	1012							
ation level)	.64			.22										.29		.09						.92			
ean	1013	1013	IOI3	1013	IOI3	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1013	1014	1014	1014	IOI4	10
a level)	.91		.61	.49		.79	.83	.94	.88	•94	·81	.70	.67		.37	.34	.24	.36	.60	.92	.17	.19	.23	•14	1

387. Richmond (Kew Observatory): $H_b = 10.4$ metres.

June, 1923

37.	Kicii	mond	i (178	W UD	serva	itory)	: n	b = 1	.0•4 1	neue	.S.														0, 19	
		mb.	mb.	l mb.	mb.	l mb.	l mb.	mb.	l mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	l n
↑	I	010.0	018.0	018.8	018.0	010.2	010.3	010.5	010.0	020.1	020.3	020.6	020.5	020.5	021.0	021.0	021.2	021.2	021.3	021.6	022.0	023.2	023.7	024.0	024.2	2 (02
ļ	2	024.4	024.5	024.5	024.8	025·T	025.5	025.8	026.0	026.0	lo26·o	lo26∙o	026.0	l026·1	025.9	025.7	025.5	025:3	025.2	025.1	025.1	025.1	025.1	024.8	024.4	4 [02
1	3	024.0	023.3	022.8	022.5	022.2	021.7	021.5	021.1	020:5	020.0	010.4	018.7	017.5	016.6	015.7	014.8	014.0	013.1	012.9	012.7	012.4	012.2	011.9	011.3	30:
1	1	010.6	010.3	010.0	010.1	DIO:3	010.6	OII	OII.7	011.8	013.1	012.8	013.3	013.4	013.2	013.3	013.4	013.4	013.4	013.7	014.1	014.6	014.8	014.6	014.4	ı 10:
-	5	014.5	014.4	014.5	014.6	010 5	014.8	014.8	015.2	015.4	015.7	015.0	015.9	015.0	015.8	015.2	015.4	015.1	014.9	014.7	014.7	014.7	014.3	014.1	014 0	olo
1	J	314 3	014 4	014 3	014 0	014 3	014 0	014	015 2	0134	015 /		015	-13	-5	55	3 4	- 3	' -	' '	' '	١.,	, 5			l
	6	013.9	013.8	013.4	013.6	013.6	013.8	014.4	014.8	015.2	015.6	015.6	015.8	016.3	017.0	017.3	017.7	018∙1	018.4	o18·8	019.0	019.5	019.8	020.0	020.3	30
ļ	7	020.4	lo20·6	1020.8	021.2	021.5	022.0	022.3	022.4	022.5	022.7	lo22·8	022.7	022.5	022.5	022.2	022.1	021.9	021.8	021.8	022.1	022.2	022.1	022.1	021.0	ЭΙC
1	8	021.7	021.6	021.2	021.0	020.0	020:5	020.3	020.3	010.7	010.7	010.8	019.3	018∙6	017.0	017.6	017.6	017.6	017.6	016.7	016.5	016.2	016.2	016.1	015.6	50
İ	9	015:0	014.5	014.2	014.2	014.3	014:3	014.4	014.7	014.8	014.8	015.2	015.2	015.5	015.6	015.6	015.4	015.6	015.9	016.5	016·8	017.3	017.3	017.4	017.2	٥l٥
1	10	017.2	017:0	014.2	014 2	014 2	014 2	014 4	014 /	017.7	017.7	018.2	018.5	018.4	018.1	018.3	οτ <u>8</u> ·5	010.0	010.5	020.1	020.6	021 ·C	021.3	021.6	021.7	7lo
	10	01/2	0170	1010-7	010.3	010-0	010.7	010.9	01/2	01//	01//	010 2	010 5	010 4	010 1	010 3		, -							′	1
	II	021.7	021.6	021.6	021.0	022.3	022.0	023.5	023.8	024.1	024.5	024.6	025.1	025.2	025.5	025.8	026.4	026.8	027.5	028-2	028.9	029.5	030.0	030-5	030.7	70
1	12	030.8	030.8	030.7	030.8	030.7	031.0	030.2	030.4	030.0	020.6	020.1	028.1	027.3	026.7	026.0	025.2	024.8	024.2	023.7	023.4	022∙€	021.6	020.9	020.1	ı 0
e-	13	010.4	018.0	018.2	017.0	017.4	017.1	016.2	016.2	015.0	015.4	015.0	014.7	014.0	013.6	013.6	013.9	014.4	015.3	015.7	016.0	016.5	016.7	016∙8	017.2	20
۶	14	017:3	017.2	017.4	017.9	017 4	0171	010.5	030.0	020.3	020.6	021.0	021.3	021.4	021.3	021.3	021.2	021.0	021.0	021.0	021.1	021.3	021.2	021.1	020.0	lo
۲.	15	020.7	020.5	020.0	017 9	010 2	019 0	019 5	070.0	018.0	017.5	017:0	016.4	015.5	014.0	013.7	013.0	012.1	011.6	011.4	010.0	010.0	010.4	CCQ-7	cc9.8	do
Station Level	-5	,	0203	020.0	019.7	019.7	019.4	019.2	019.0	010.0	01/3	017.0	010 4	015 5	014 9	013 /	3-3			'				- /		1
ဓ္	16	010.0	000.0	000.7	000.7	000.8	0.00	010.6	011.3	012.7	014.3	015.3	015.9	016.3	016.0	016.0	016.9	016.9	017.3	017.7	018.0	018.4	018.5	018·6	018.0	o
Ď		010-1	010.0	010.0	OTO	010.6	010.0	020.4	020.6	020.0	021.1	021.2	021.4	021.5	021.6	021.5	021.3	021.2	021.4	021.7	021.9	022.2	022.1	022.1	022.3	30
$\ddot{\mathbf{s}}$	18	022·T	021.7	021.4	021.2	019 0	020 0	020 4	020 0	020.0	020.8	020.8	020.6	050.3	020.1	0.010	010.7	010.4	010.3	019.4	019.5	3.610	020.0	020.0	019.7	lo
ł	19	010.5	010.3	018.0	018.7	018.0	0211	021 2	078.9	028.1	018.1	018.2	018.2	017:0	018.0	017.7	017.5	017.4	017.3	017.3	017.4	017.5	017.5	017.4	017.4	10
1	20	017:0	017.0	017.0	010-7	010.0	010.1	010.1	010.2	010.1	020.0	020.5	020.9	021.4	021.8	022.3	022.5	022.8	023.0	023.3	023.8	024.1	024.4	024.7	024.6	δlo
		1 , ,	01,0	0170	017.1	017.3	017.0	010.0	010.0	019.3	020.0	020-5	020 9	021 4	021 0	022 3	322 3		5	33	3	•	' '	' '	'	l
	21	024.4	024.4	024.3	024.0	024.1	024:0	022.0	022.4	022.2	023.3	023.3	023.1	022.6	022.5	022.4	022.0	021.9	021.8	021.9	021.9	021.9	021.9	021.9	021.7	70
1	22	021.4	021.2	021.3	020:0	021.1	027.4	023 9	023 4	023.0	023.3	023.4	022.2	022.2	022.4	022·I	022.0	022.3	022.8	022.9	023.1	023.6	023.9	024.2	024.1	ιc
1		024.1	024.2	024.2	024.4	0211	0214	021	021.0	021 9	025.3	022 4	024.5	024.2	024.0	023.6	023.5	023.5	023.5	023.5	023.8	024.1	024.3	024.3	024.2	2 0
1	24	024.1	023.0	023.6	023.4	0224 9	023.0	025.4	025.3	025.3	025 2	024 /	022.5	024 3	024 0	021.4	021.1	020.8	020.8	020.8	021.0	021.4	021.3	021.2	020.0	alo
1	25	020.6	020.1	010.5	010.3	070.7	023 4	023.5	023.7	023.0	023.2	023.0	019.0	022 3	070.0	010.0	018.0	018.6	018.4	018.6	018.7	018.8	018.7	018∙6	018∙€	δlo
	-3	020 0	020 1	019 3	019.2	019.1	019.0	019.1	019.1	019.0	019.0	019.0	019.0	019.0	019.0	019 0	010 9	010 0	1010 4	010	,		,			1
1	26	018.0	017.0	017.8	017.6	017.6	017.6	017.8	017:0	017.7	018.0	018.1	018-4	018.7	018.7	018.0	018.6	018-6	018.8	019.0	019.4	020.0	020.3	020.4	020-6	5 c
1	27	020.7	020.7	020.7	020.5	020.7	020.8	020:0	020.0	020.8	020.8	030:0	020.7	020.5	020.3	010.0	010.6	010.4	019.3	019.7	019.9	020.4	021.0	021.2	021.2	2 0
	28	021.1	020.0	020.0	021.3	021.6	021.7	023.1	020 9	020 0	020 0	020 9	022.1	020 3	023:0	021.8	021.8	021.6	021.5	021.4	021.8	022.2	022.3	022.4	022.4	4lc
	29	022:4	022.4	023.4	0221	022.4	022.7	022.5	022.2	022.1	022.2	022.2	022 3	0221	022 0	021.1	020:0	020.6	020.6	020.6	020.7	020.8	020.9	021.1	020.0	ilo
\downarrow	30	020.6	020.2	020·I	010.8	010.8	020.0	020-1	020.1	010.6	070.3	018.8	018.3	018.1	017.7	017:3	017.2	017.0	016.9	017:1	017.2	017.4	017.5	017.5	017.6	5 0
<u>. </u>			I	ļ	ļ —	\ 	ļ		·	l	<u> </u>	!]]									-1-
an		1019	1019	1019	1019	1019	1019	1019	1020	1019	1020	1020	1020	1019	1019	1019	1019	1019	1019	1019	1019	1019	1020	1020	1019	I
atio	n level)	.86	.69	.52	.51	•56	73	•88	•00	1.99	·08	1:18	.06	.91	·80	-61	.49	·41	45	.56	.73	1 .99	.04	1 .04	1 .90	<u>ય </u>
an		1021	1020	1020	1020	1020	1021	1021	1021	1021	1021	1021	1021	1021	1021	1020	1020	1020	1020	1020	1020	1021	1021	1021	1021	Ţ
a le	vel)	.13	•96	.79	.78	.83	.01	.15					.32				.74	-66	.70	-81	.99	.25	.31	.31	.23	3
~ 14	rr]			<u> </u>						-0					22	24.	٦,
G.M	L. I.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	1 44.	1,1

388. Richmond (Kew Observatory): H_b (height of barometer cistern above M.S.L.) = 10.4 metres.

July, 1923.

388	. Rich	mond	(Ke	w Obs	erva	tory)	: H	(hei	ght o	t bar	omet	er cı	stern	abov	re M.	S.L.)	= 10	0·4 m	ietres	5. 				Ju	ıy, 19	rzs.
I	ay.	ı.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
1		mb. mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.											
	I 2	017.5	017.4	017.2	017·1 018·2	017.3	017.0	017.0	018.0	017.3	017.0	016.3	018.5	018.5	015.3	014.9	014.6	014.4	014.4	014.4	014.6	014.7	014.8	014.8	014.7	018·1
	3	014.6	014.5	014.4	014.4	014.5	014.6	014.8	014.7	014.4	014.6	014.5	014.5	014.4	014.5	014.5	014.5	014'4	014.6	014.7	014.8	015.3	015.4	015.5	5 OI5·6	014.7
	4	015.8	015.8	016.2	016.4	016.7	017.1	017.4	017.6	017.9	018.0	018.1	018.1	018.0	017.8	017.8	017.8	017.7	017.9	018.2	108.0	019.1	020.7	019.7	019.8	017·7 020·3
1	5	019.9		0201	020.3	020 0	02019	021 1	020 9	020 0	020 /	020 4	020 4	020 2	020 1	019 9	019 5	019 3	0194	0190	020 0		,			3
	6	020.7	020.7	020.6	020.8	020.8	020.7	020.7	020.7	020.4	020.1	019.7	019.5	019.3	018.9	018.8	018.7	018.7	018.7	019.1	019.1	019.2	019.3	019.2	019.0	019.8
	7 8	016.0	016.8	016.8	017.9	017.7	017.7	017.7	017.4	017.1	018.0	010.7	010.4	019.0	018.7	018.6	015.4	015.4	018.6	019 1	019.4	020.0	020.5	020.7	020.7	018.6
	9	020.8	020.8	020.5	020.7	020.8	020.9	020.8	020.6	020.4	020.2	019.7	019.1	018∙6	0.810	017:4	017.0	016.7	o16·6	016.7	017.0	017.2	017.2	017.1	017.2	019.9
	10	016.5	015.2	015.1	015.3	014.0	014.0	014.5	014.0	014.7	014.0	014.5	014.1	013.5	013.2	013.2	013.2	013.2	012.9	013.7	015.3	015.4	015.0	015.9	,010.0	014.6
	11	016.8	017.0	017.4	017.9	018.7	019.1	019.5	020.0	020-2	020.6	020.7	020.8	020-9	020.8	020.8	020.5	020.3	020.5	020.8	021.5	022.0	022.0	022.3	021.9	020.0
	12 13	021.7	021.6	021.8	022.0	018.8	022.1	022.0	022.0	018.0	022.0	021.7	021.4	020·9 017·1	020.7	020.4	017.0	019·7	019·6 017·3	019.6	019.9	020.2	018.6	018.7	020.0	021.0
vel	14	018∙1	0.810	017.8	017.8	018.1	018.7	018-2	018.1	017.6	017.9	o18·c	017.8	017.5	017.3	o16·8	016.5	016.4	016.2	016.0	016.1	016.3	016.3	016.2	2 015.9	017.3
Le	15	015.4	015.1	014.4	014.1	013.9	014.0	013.5	013.3	012.8	012.4	012.2	011.6	011.4	011.1	011.3	011.1	010.8	010.7	010.7	010.8	010.8	011.0	011.0	010.0	012.4
Station Level	16	010.1	009.7	009.3	009.0	008.9	009.1	009.2	009.4	009.6	009.7	009.8	010.2	010.4	010.3	010.6	010.8	010.6	010.8	011.0	011.1	011.7	012.3	012.2	012.5	010.3
ati	17	012.4	012.2	012.0	011.9	011.9	012.0	012.0	011.9	011.7	011.6	011.5	011.5	011.6	011.4	011.5	011.5	011.3	011.4	011.6	011.5	011.7	012.0	012.1	012.0	011.8
St	18 19	012.1	012.0	012.0	012.1	012.5	012.0	013.1	013.5	013.9	014.2	018.6	014.7	014.9	019.0	018.8	015.3	015.0 018.2	015.9	018.3	018.3	017.2	019.6	018.8	018.9	014·6 018·7
1	20	019.3	019.6	019.8	019·8	020.2	020.8	021.3	021.6	021.9	021.8	021.9	022.2	022.4	022.4	022.3	022.2	022.0	021.9	022.2	022.7	023.4	023.7	023.7	023.9	021.7
	21	023.8	023.8	023.0	024.0	024.3	024.7	025.4	025.7	025.9	025.7	025.4	025.3	025.1	024.9	024.6	024.4	024.3	024.3	024.4	024.8	025.5	025.7	025.9	025.9	024 9
1	22	025.9	025.8	025.5	025.6	025.9	026.0	026.0	025.9	025.8	025.5	025.2	024.8	024.3	024.0	023.4	022.9	022.5	022.0	021.5	021.5	021.5	021.4	021.2	2020.7	024 1
	23 24																									014.5
	25	012.4	012.2	011.6	011.4	010.8	010.6	010.3	010.4	010.2	010.3	009.5	009.6	009.9	009.4	008.7	008.3	008.3	008.1	008.0	008.1	008.7	009.2	009.5	; 009.7	009.9
	26	000.0	000.7	000.8	000.8	 010:1	010.5	010.7	0.110	011.2	01 I.V	011.6	011.4	011.1	011.0	011.1	0.1.1	011.4	011.4	011.6	011.8	012.6	013.2	013.8	014.2	011.2
	27	014.2	014.3	014.6	014.9	015.2	015.6	016-2	016.3	016.6	016.5	016.4	016.3	o15·8	015.5	015.0	014.6	014.4	014.0	013.8	013.7	013.4	013.1	012.6	012.0	014.8
	28	011.0	010.1	009.5	008.8	008.4	007.7	007.2	006.8	006.1	005.5	004.8	004.4	003.1	002.3	001.9	001.6	001.6	002.1	002.3	002.9	003.6	004.1	004.6	004.7	005.4
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390. Richmond (Kew Observatory): H_b (height of barometer cistern above M.S.L.) = 10.4 metres.

September, 1923.

Day.		ı.	2.	3.	4.	5.	6.	7.	8.	9.	IO.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Me
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1	I	011.9	011.0	011.0	011.0	021.4	022:1	033.0	023.5	024.0	024.0	024.1	024.5	024.8	024.9	024.7	024.8	025.1	025.6	025.9	026.4	026.5	026.8	026.9	027.1	02
	2	019.5	019.9	020.4	020.6	027.8	028:0	028.2	028.4	028.4	028.1	028.0	027.6	027.3	027.0	026.6	026.5	026.4	026.4	026.5	026.6	026.9	026.7	026.4	026.2	02
i	3	027.2	027.5	027.0	027.0	02/0	023:5	023.5	022.0	022.7	022.3	021.8	021.7	021.8	021.8	021.7	022.1	022.6	023.1	023.9	024.7	024.2	025.7	026.1	026	302
	4	025.0	025.3	024.0	024.3	026.7	025 3	026.0	027.0	027.2	026.0	026.6	026.4	025.9	025.3	025.1	025.1	025.1	025.1	025.3	025.6	025.7	026.0	026.3	026.7	102
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	7 8	024 1	024 1	025 9	025.5	026:0	027.6	027.6	027.8	027.7	027.7	027.6	027.6	027.3	026.6	026.0	025.4	025.1	024.9	024.9	024.9	024.9	024.8	024.7	024	302
1	0	020 3	020 4	020 3	021.6	021.2	021.2	021.1	020.0	020.6	020.3	019.9	019.4	o18∙6	018∙1	017.3	017.1	016.9	016.8	010.8	017.1	017.3	017.5	017.4	017.2	201
i	9 10	023.0	076.0	016.7	076.3	016.2	016.3	016.5	016.8	017.0	017.4	017.1	017.0	016.7	016.5	016.5	016.5	016.7	017.2	017.8	018.5	018.7	018.7	018.9	018.0	101
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1	11	018.8	018.7	018.6	018.5	018.6	018.6	018.8	010.0	018.8	018.5	018.3	017.7	016.7	016.0	015.5	014·8 011·5	014.5	014.4	014.6	014.8	014.9	014.0	014.7	014	
<u> </u>	. 12	010 0	010 /	012.8	012.5	012.6	012.7	012.8	012.8	012.8	013.0	012.3	012.2	o11·8	011.7	011.2	011.5	011.6	o11.0	012.2	012.7	012.8	012.7	012.6	012	101
Į.	. 14	014 0	013.3	012.0	011.6	011.4	011.4	011.5	011.5	011.3	010.8	010.1	009.3	008.5	007.8	007.3	006.7	006.4	000.3	000.2	000.8	000.7	000.9	000.4		
Ģ	13	005.7	005:0	004:5	004.3	003.7	003.0	003.0	004.0	003.7	003.4	003.1	002.4	8.100	001.4	000.8	000 7	999.9	999.6	999.6	999.8	999.7	999.4	1999.0	1999.0	100
-1	14	000.7	000.3	000.4	000.7	000.8	000.3	000.6	001.1	001.5	001.7	001.5	001.5	001.6	001.0	002.2	002.7	002.8	003.3	003.9	004.5	005.5	000.1	000.0	1007.	loc
d	15	999 1	999 3	999 4	999 /	999 0					ì	1		1] .		_							۱.,
Station Level	16	007.5	007.0	008.5	000.3	000.0	010.5	011.1	011.8	012.4	012.8	012.9	013.0	013.1	013.4	013.2	013.4	013.9	014.6	015.2	015.8	010.1	010.7	010.9	010.0	101
Ή.	10	00/3	016.6	016.3	015.7	015.4	015.1	014.5	013.6	012.9	012.1	010.8	009.9	008.4	007.1	005.9	004.8	003.4	002.7	002.0	000.5	999.6	998.5	997.0	990-2	100
ta	17 18	004.8	002.8	003:0	003.6	003.2	004.0	004.5	994.8	995.0	995.8	997.4	998.7	999.5	999.8	000.6	000.0	001.2	001.0	002.5	003.5	003.0	004.0	005.2	005.7	199
ကု	70	994.0	006.0	007.3	007.7	008.6	000.3	000.0	010.2	010.6	011.1	011.1	011.1	0.110	010.6	010.3	010.1	0.010	009.7	009.4	009.1	008.2	007.9	co7·4	000.7	TCC
1	19 20	006:0	005.3	004:0	005:0	005:2	005.7	006.2	006.8	007.0	007.1	007.3	007.5	007.4	007.2	007:3	007.6	007.9	008.0	008.4	008.7	008.0	008.2	607.3	005.0	Picc
1		0000	005 2	004 9		-	,			'	,										0	0 .	0-	000.	008.	یا
1	21	004:2	001.1	008.7	007.1	006.4	996.9	997.6	998.4	999.1	999.1	999.3	999.9	000.4	001.7	002.9	003.8	004.8	005.9	007.2	008.0	000.5	000.7	000.7	000	
İ	22	007:0	006.8	000.3	005.3	004.6	004.3	004.1	003.9	003.7	003.2	002.6	002.4	001.7	001.6	001.1	999.9	999:4	998.9	999.0	998.7	990.4	997.0	997.7	997	la
1	23	007.4	007:4	007.2	007.1	997.0	996.9	996.9	996.7	996.4	996.2	995.7	995.4	994.9	994.7	994.2	994·6 009·7	995.3	996.8	997:9	999.1	999.9	000.4	001.2	002.0	و ا
İ	24	99/ 4	004.I	004.8	005.0	006.8	007.4	008.3	009.1	009.5	010.2	010.4	010.5	o1o∙6	010.0	009.9	009.7	009.7	000.1	000.0	008.2	007.2	000.1	004.9	003	
1	24 25	003.4	001.3	000.1	000.6	001.3	002.1	002.7	003.4	003.8	003.9	004·I	004.5	004.9	004.8	005.1	005.3	005.9	006.4	006.9	007.3	007.0	000.0	000.3	000.0	ľ
1	~5	002 4	001 2		1			'					!		i		ا							004.8	004.0	١.
1	26	000.7	010.5	011.2	012.0	013.3	014.5	015.6	016.7	017.3	018∙3	018.9	019.2	020.0	020.5	021.4	021.6	022.0	022.7	023.3	023.9	024.3	024.4	024.0	024	
		025.3	025.2	025.2	025.1	025.3	025.6	025.5	025.8	025.9	026.2	025.8	025.5	025.0	024.6	024.1	024.0	023.8	024.2	024.4	024.4	024.4	024.3	024.2	024	
	28	024.3	024.4	023.8	023.6	023.8	023.8	023.8	024.2	024.3	024.4	024.5	024.6	024.6	024.6	024.8	024.9	025.1	025.8	020.2	020.0	020.0	027.2	027.2	027.2	lo
1	29	027.3	027.6	027.6	027.8	027.9	028.2	028.7	029.2	029.5	029.5	029.4	029.4	029.3	029.3	029.1	029.1	029.3	029.2	029.2	029.3	029.5	029.0	029.3	029 2	100
	30	020.0	028.8	028.6	028.6	028.4	028.2	028.3	028.3	028.6	028.3	028.0	027.7	027.2	026.4	025.6	024.9	024.6	024.4	024.3	024.1	023.5	023.1	0227	022 1	Ľ
<u> </u>					<u> </u>	<u> </u>	<u> </u>	<u> </u>													TOT 5	TOTE	1015	TOTE	1015	10
ean		1014	1014	1014	1014	1014	1014	1014	1015	1015	1015	1015	1015	1014	1014	1014	1014	1014	1014	1014	1015	1015	34	•27	.101	1
	level)																									
ean		TOTS	TOT 5	1015	1015	1015	1015	1016	1016	1016	1016	1016	1016	1016	1015	1015	1015	1015	1015	1010	1010	1010	TOTO	1010	1010	10
ea lev	rel)	.95	.74	.51	•45	.59	.83	.11	.34	.44	.46	.31	.24	.01	·8o	·61	•49	.56	.77	.12	.42	•52	.00	•53	1 40	1_
		95	17																							
																							_	ctobe	40	^

391.	Rich	mond	(Ke	w Ob	serva	tory)	: H) = I	0.4	metre	es.												0	ctobe	r, 19	23.
										- 1	1 1.	Lmb	lmb	l mb	mb	mh	mb	ı mb.	mb.	ı mb.	mb.	mb.	mb.	mb.	mb.	mb.
↑		mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	IIID.	mb.	078.0	018.6	018.4	018:4	018.3	018.4	018.6	018.0	019.3	019.1	019.1	019.3	019.1	019.0	019·2 017·3
- 1	I	021.6	020.6	020.0	019.7	010.3	018.9	010.0	019.2	019.3	019.1	010.9	010.0	010.4	010 4	016.8	016.3	016.1	015.7	015.0	015.9	015.5	015.3	014.8	013.0	017.3
	2	019.2	019.1	018.	018.	018.6	018.5	018.0	018.0	018.5	010.2	010.2	017.9	017.5	0173	007.5	008:5	000.7	000.4	001.2	002.1	002.7	003.6	004.4	004 C	004 - 5
- }	3	013.4	012.6	011.0	010.5	010.1	008.8	007.5	006.2	005.0	003.7	1003.0	000-1	997.0	9971	99/ 3	014.8	075.4	016.1	016.4	017:0	002.7	017.4	017.3	017.3	012
- 1	4	005.8	006.6	007	3 007-8	3 008-3	000.1	010.5	011.0	011.2	012.0	012.5	013.1	013.0	013.9	014 3	014 0	013.0	0101	013.6	013.3	013.4	013.2	013.0	012.6	012.5
}	5	017.1	016.8	016.	016.7	016.7	016.2	010.0	010.0	010.5	010.4	010.1	015.7	015.1	014.5	014 2	014 0	013 9	013	013	3 3	1 1			ł	015.2
	•		1	}		}	ì	1	Ì]	1	l	6				017.6	011.0	012.4	012.8	013.3	013.7	014.0	014.2	014.4	012.1
- [6	012.5	012.0	011.	9011.0	011.0	010.9	011.2	011.3	011.2	011.7	011.0	011.0	011.5	011.4	011.3	011.0	011 9	012.5	012.2	011.5	010.4	000.3	008.3	007.8	012.1
- 1	7	014.5	014.4	014.4	1014.6	015.1	015.1	015.1	015.3	015.6	015.1	014.9	014.0	014.2	014.0	013.0	013.1	012.7	012 5	017.5	010:0	000.5	000.1	007.7	007.1	013.4
}																										
1	9	006.2	005.8	005	005.4	005.3	005.4	005.6	005.9	006.6	006.8	007.7	008.2	008.9	010.0	010.8	012.0	012.7	013.0	015.0	015.5	013 0	008.1	008.8	000.3	009.7
ļ	10	016.8	016.7	016	016.1	016.1	015.5	015.6	015.6	015.3	014.3	013.4	012.7	011.4	010.1	000	008.4	009.1	007.9	1007.0	007.7	00/3	000 1	000 0	009 3	012.2
ļ			[1	i l	t	1	į		1	ļ	1	1		l				070.6	0.70.0	010.4	070.3	ото-т	000.4	8.800	010.5
1	11	009.4	009.4	009.2	2 009 1	010.0	010.0	010.4	011.1	o11.8	012.1	012.1	011.7	011.6	011.2	011.2	010.9	010.0	010.0	010.2	010.4	003.3	003.7	003.0	004.2	010·5 996·1
•	12	008.0	006.0	005	5004.2	1003.2	001.3	999.9	996.2	995.5	993.5	992.8	991.5	989.6	988.3	989.0	990.3	991.1	1991.9	1992.3	992.7	993 2	993 /	993 9	001.2	996·1
	13	004.2	003.5	003	1992.6	992.3	992.0	992.1	992.5	992.8	992.9	993.4	993.6	993.9	994.4	995.3	996.0	996.9	997.8	998.6	999.4	000-2	000.7	001 0	010:0	995·3
(છે	14	001.5	001.6	001.0	002.0	002.2	002.5	002.7	002.7	003.0	003.0	003.2	003.1	003.3	003.7	004.0	004.2	005.4	006.5	007.3	008.2	000.9	009.0	010 1	010 9	004·5
e 🤆	15	011.2	011.0	012	2012.	013.2	013.4	013.0	014.9	015.3	015.5	015.6	015.5	015.1	015.0	014.9	014.9	015.2	015.2	015.2	015.7	010.0	010.0	015.7	015.0	014.5
Station Level	-3	011)	011 9		,		3 7	1	' '	ا ا		-		1			ľ	l		l	l	1 00		l		
ď	76	015.4	015.2	OT 4.0	OT 4.5	30T4.6	074.6	014.7	075.0	015.3	015.2	015.1	015.0	014.9	015.0	014.9	015.2	015.9	016.5	017.0	017.7	018.8	019.1	019.0	019.7	015·9 022·5
5	16	015 4	020.1	020	014	020:0	021.2	021.0	022.3	022.0	023.3	023.8	023.4	023.2	023.1	022.9	023.0	023.2	023.5	023.5	023.7	023.8	023.9	023.9	023.7	022·5 017·9
:≒	17	019.9	0201	020	3020	020 9	021 3	021.2	030.0	020:4	010.8	010.1	0.810	017.0	016.1	015.6	015.1	014.6	014.4	014.0	013.6	013.3	012.8	011.9	011.3	017·9 007·0
ta																										
Ś	19	010.0	1000.0	007.0	-1007	1005.0	005.4	005.3	005.8	005	005 0	007.5	007:2	007:0	006.4	006.0	005.4	004.8	003.8	003.5	002.2	000.8	999.7	998.9	997.8	005.0
	20	000.5	000.2	1005.	/1005.7	1005.0	1005.7	1000.3	000.0	007.4	007-7	00/3	00, 2	00, 0	1000 4	" "	13 4	١ '		"	1	1 1		i '		i
- 1					000				000.6	000.0	000.0	J	000:3	080.6	080.3	080.0	088.0	080.5	990.4	991.7	992.8	993.8	993.8	993.7	993.6	991·7 992·6
1	21	996.7	995.3	1993.	992.2	1991.2	990.3	990.7	1990.0	1990.0	990.9	1990 7	990 2	000.5	007.4	001.3	001.7	002.7	003.5	993.9	994.1	994.4	994.3	1994·3	994.0	992 • 6
ļ	22	993.3	993.0	1992.0	0 992.4	1992.3	992.1	1992.0	1992.2	992.0	992.0	1991.9	991 4	990.3	991 4	991 3	070.1	070:5	070.0	080.6	980·a	981.4	981.3	981.3	981.1	992·6 984·6
i	23	993.8	993.3	992.9	9992.4	1991.6	990 I	1988.8	987.8	9×5.3	984.1	982.5	900.5	979.3	970.7	970.0	084.6	085.0	085.2	085.0	085.3	086·0	986.4	987.0	987.8	984·6 983·7
1																										
-	25	988.2	988.7	989.2	2 989.8	990.5	991.0	991.9	992.9	993.6	994.6	995.4	996.4	997.2	997.0	1999.1	990.0	999-1	999 /	0000	001 1	/		, ''	1	995·6
- 1	-																									
	26	999.8	999.0	997.2	1995	993.2	991.4	991.8	991.6	992.5	994.1	995.7	1990.0	996.7	1997:4	997.9	1990.0	999.5	999.0	999 6	001.6	002.2	002.6	003.5	993.6	996·6 990·5
1	27	994.3	992.8	991.0	989.8	3 988·8	987.9	987.8	988.3	987.9	987.7	1988-2	989.2	989.9	1989.9	990.I	990.3	1990.8	991.1	991.5	991.0	00E.4	006.3	007.1	007.8	990·5 998·3
- 1																										
- [29	008.4	009.5	010.0	010.6	011.2	012.0	012.7	013.6	014.3	014.9	014.9	014.4	014.4	014.2	014.2	014.1	014.3	014.0	014.8	014.0	014.7	014 3	014 1	014.2	013·2 013·2
- 1	30	014.0	013.9	013.7	013.4	013.4	013.1	013.2	013.4	013.6	013.9	013.7	013.3	012.9	012.6	012.4	012.2	012.3	012.0	012.7	012.9	013.2	013.3	013 /	014 2	013.2
]																										
1	31	014.5	015.0	015	015.6	016.0	016.4	017.0	018.2	019.2	019.7	020.2	020.1	020.0	019.9	020.2	020.5	021.0	021.0	020.0	022.2	022.7	022.0	022 9	023 2	019.2
· ·	J-				-[- 						·}	ļ	 -									1007	1007	1007	1006
Mean		1006	1006	1006	1006	1005	1005	1005	1005	1006	1006	1006	1005	1005	1005	1005	1005	1006	1006	1000	1000	1007	1007	1007	1007	1000
	ion level)	·85		1											.54	.50	.77	1 .13	1 .49	1 .80	1 •97	1 .121	.19	1 13	1 0/	~/
	011 10 101)					1007		1007	1007	1007	1007		_	1006	1006	1006	1007	1007	1007	1008	1008	1008	1008	1008	1008	1007
Mean	1\	11.	83						•19					.85	.79	.84	.02	.38	.74	.05	.23	.41	· 4 5	·41	.33	<u>.5</u> 3
(Sea l	evei)			-3						-34	-33			<u> — 3</u>				1	'	<u>-</u>						
					١.	1 -	6	-	8.				1.0			1	16	17.	18.	19.	20.	21.	22.	23.	24.	Mean
G.1	М.Т	I.	2.	3.	1 4.	5.	6.	7.	1 0.	9.	10.	II.	12.	13.	14.	15.	1 10.	1 1/.	10.	1 19.						
No		an nr		e exce	eeds 1	000 m	b. the	leadi	ng fig	ure i	is not	print	ed i.	e. 10	05·6 I	nb. is	writ	ten oc	5.6.	This	rule	does r	ot, h	owev	er, ap	ply to

392. Richmond (Kew Observatory): H_b (height of barometer cistern above M.S.L.) = 10.4 metres.

November, 1923.

	Day.	ı.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
-	<u> </u>	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.			mb.	mb.
	1 2	017.7	017.6	017.1	016.0	017.0	016.0	017:1	1017:5	017.7	017.8	8018.0	017.9	017.7	017.9	018.1	018.4	018.8	019.2	2 019.4	019.5	019.0	olo18·5	017.4	016.6	017.9
	3 4	009.5	000	1009.5	009.	1009.6	000	009.	7010	010.5	010	010	8 900	009.5	009-2	2009.1	009.1	009.3	009.4	1009.4	009.3	009.2	009.1	009.0	008.0	008.8
	5	008.4	008.1	007.5	007-3	3006-8	8 006.2	2006.0	005-8	005.0	004-8	004.0	002.8	001.6	000-6	999.8	999.3	998.7	998.7	998.5	998.1	998-2	997.9	997.9	998-1	002.7
İ	6																									004.4
	7 8	013.8	8013.6	013.1	012.4	012.3	011.9	011.6	011.7	011.2	010.7	1009.6	008.7	007.3	006.1	005.4	004.9	CO4 · 4	003.5	5002.8	001.8	cco.7	000.6	999.9	98.8	CO7.7
	9 10	998.1	997.8	997.0	996.7	7 996·7 8 016·5	7 996·3 5 017·4	996.3 018.6	9 019·6	3 020·8	997.0	997:	997:4	997.8	022.0	022.5	023.3	024.0	024.5	025.2	025.4	025.5	025.9	026.2	026.2	020 · 4
	11	026.1	026.3	026.0	025.6	026.0	025.0	026.4	1026.0	026.8	026.6	026.2	025.0	024.7	023.8	023.6	023.6	024.2	023.0	023.6	023.8	023.0	022.8	022.4	021.8	024.8
-	7.0	020.9	021.1	020.1	019.2	018.6	018.1	018.4	018-3	017.4	016.4	µ015·4	015.1	014.1	013.2	012.3	012.3	011.6	011.4	9·110	8011.5	011.3	010.7	cc9.8	cc9·7	015·2
	13	985.2	983.5	981.8	981.9	982.4	983.1	984.6	987.0	988.6	990-1	991.1	991.6	992.4	993.4	994.7	995.7	996.7	997.9	998.7	999.7	000.5	cco-8	COI ·2	coi	991 5
Const T assistant	15	1	İ	1	1	1	1	1		1		1		1		i	1	i	1	Ì	1	1	1	1	1	. 601.0
4	16 17																									co1·0
0	1 18 1 19	006.5	006.1	005.6	005.1	004.4	003.7	003.4	003.1	003.0	co3·1	¦003∙1	002.9	002.6	002.3	001.9	001.3	COI .4	001.5	001.6	COI	COI ·4	COI ·4	COI ·4	COI .4	co3·0 cco·9
1	20	001.6	001.5	001.4	001.2	000.8	000.2	000.2	000.1	999.8	999.5	999.1	998.6	998.3	997.9	998.0	998.0	998.0	998.1	998.2	998.6	998.8	999.0	559.3	999.7	999.5
	21																									co2·9
	22 23																									010.6
	24 25	021.6	015.7	016.0	016.4	016.7	017.0	017.6	018.4	018.9	019.4	019.7	019.7	019·7 020·6	019.5	010.0	020.0	020.1	020.6	020.8	018.3	021.3	021.4	021.5	021.6	018·c
	26		ĺ					1			ł	İ			Ī		1						1			012.6
	27	010.5	010.5	010.0	009.9	010.0	009.8	009.8	009.9	010.1	010.3	010.1	009.9	008∙8	co8·1	007.8	co7·6	co7.5	co7.6	007.8	co7·4	co7·3	¦cc6∙8	cc6·2	cc6·c	cc8·8
	28 29	998.7	999.0	999.1	999.3	999.5	999.8	000.5	001 .2	002.0	002.6	003.0	003.2	003.3	co3·4	004.0	co4.8	co5·5	co6.5	co7·7	' co8∙5	CC9-2	cc9·8	010.4	011.2	1999∙7 co3∙€
Y	30	011.8	012.8	013.4	014.3	015.0	015.5	016.5	017.4	017.7	018-4	018-5	018.5	018.3	018.0	018.0	018.5	019.0	019.5	019.6	019.4	019.5	019.5	019.3	019.3	017.2
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Mean (Sea	ı level)	1009		.16 1009			1009						1009		1008 ·51						1009					
		1 1-1							37	35		<u> </u>	<u></u>					,	<u> </u>		<u> </u>	<u> </u>		· - T-	. 72	
393	3. Rich	mond	(Kev	w Obs	erva	tory)	: H _b	_ I	0.41	netre	s.												Dec	embe	r, 19	23.
393		mb. I	mb.	mb.	mb. I	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.
393	I 2	mb. 019·0	mb. 018·9	mb. 018·4	mb. 018·2	mb. 017·6 999·0	mb. 017·4 998·0	mb. 017·3 997·1	mb. 017·0 996·0	mb. 016·7 995·8	mb. 016·5 995·8	015·9 995·3	015·4 994·7	014·6 994·5	013·8 994·1	013·3 994·2	012·7 994·2	012·2 994·5	011·6 994·9	010·7 995·0	009·8	CC9·1	mb. co7·8	mb. cc6·7	mb.	mb. 014·3
393	I 2 3 4	mb. 019·0 004·8 996·6	mb. 018·9 003·5 997·3	mb. 018·4 001·8 997·6	mb. 018·2 000·5 997·7	mb. 017·6 999·0 997·7 001·1	mb. 017·4 998·0 997·7	mb. 017·3 997·1 998·2 998·1	mb. 017·0 996·0 998·9	mb. 016·7 995·8 999·6 994·6	mb. 016·5 995·8 000·0 993·3	015·9 995·3 000·3 991·6	015·4 994·7 000·3 989·9	014·6 994·5 000·2 989·4	013·8 994·1 000·5 989·4	013·3 994·2 001·1 989·3	012·7 994·2 001·6 989·2	012·2 994·5 002·4 989·2	011·6 994·9 003·1 989·1	010·7 995·0 003·4 989·2	004·1 989·2	cc9·1 c95·4 co4·8 989·3	mb. co7·8 995·5 co4·6	mb. cc6·7 995·9 co4·6	mb. co5·9 gg6·2 co4·8	mb. 014·3 996·9 cco·5
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393	1 2 3 4 5	mb. 019·0 004·8 996·6 004·4 989·4 005·8	mb. 018·9 003·5 997·3 004·0 989·7	mb. 018·4 001·8 997·6 003·2 989·8	mb. 018·2 000·5 997·7 002·4 989·8	mb. 017·6 999·0 997·7 001·1 990·1	mb. 017·4 998·0 997·7 999·3 990·4	mb. 017·3 997·1 998·2 998·1 990·8	mb. 017·0 996·0 998·9 996·7 991·7	mb. 016·7 995·8 999·6 994·6 992·7	mb. 016·5 995·8 000·0 993·3 993·6	015·9 995·3 000·3 991·6 994·2	015·4 994·7 000·3 989·9 994·3	014·6 994·5 000·2 989·4 994·7	013·8 994·1 000·5 989·4 995·2	013·3 994·2 001·1 989·3 996·1	012·7 994·2 001·6 989·2 997·4	012·2 994·5 002·4 989·2 998·6	011·6 994·9 003·1 989·1 000·0	010·7 995·0 003·4 989·2 000·8	015.8	095.4 095.4 004.8 989.3 002.2	mb. co7·8 995·5 co4·6 989·3 co2·8	mb. cc6·7 995·9 co4·6 989·4 co3·6	mb. co5·9 gg6·2 co4·8 g89·5 co4·8	mb. 014·3 996·9 cco·5 994·1 995·3
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393	1 2 3 4 5 6 7 8	mb. 019·0 004·8 996·6 004·4 989·4 005·8 014·8 994·7	mb. 018·9 003·5 997·3 004·0 989·7 006·4 014·6 994·4	mb. 018·4 001·8 997·6 003·2 989·8 006·8 014·1 994·5	mb. 018·2 000·5 997·7 002·4 989·8 007·5 013·1 994·4	mb. 017·6 999·0 997·7 001·1 990·1 008·6 012·4 994·7 007·1	mb. 017·4 998·0 997·7 999·3 990·4 009·4 011·6 994·9 008·1	mb. 017·3 997·1 998·2 998·1 990·8 010·5 011·1 995·4 008·9	mb. 1 017:0 996:0 998:9 996:7 991:7 011:6 010:8 996:0	mb. 016·7 995·8 999·6 994·6 992·7 012·4 010·1 996·8	mb. 016·5 995·8 000·0 993·3 993·6 013·1 009·8 997·7 012·2	015.9 995.3 000.3 991.6 994.2 013.4 008.9 998.1	015·4 994·7 000·3 989·9 994·3 013·8 008·0 998·2 013·6	014.6 994.5 000.2 989.4 994.7 013.7 006.1 998.3 013.8	013.8 994.1 000.5 989.4 995.2 013.8 005.0 998.3 014.5	013·3 994·2 001·1 989·3 996·1 014·3 004·0 998·8	012·7 994·2 001·6 989·2 997·4 014·7 003·0 999·2 016·7	012·2 994·5 002·4 989·2 998·6 015·3 002·0 999·8 017·6	011.6 994.9 003.1 989.1 000.0 015.7 001.0 000.3 018.2	010·7 995·0 003·4 989·2 000·8 016·0 000·2 000·8 018·9	015.8 999.4 004.1 989.2 01.4 015.8 999.4 019.5	095.4 095.4 004.8 989.3 002.2 015.6 998.6 001.8	mb. co7·8 995·5 co4·6 989·3 co2·8 o15·6 997·5 co2·7 o2o·7	mb. cc6·7 995·9 co4·6 989·4 co3·6 o15·4 996·2 co3·2 o2o·8	mb. co5.9 cc6.2 cc4.8 cc4.8 cc4.8 cc5.3 cc4.8	mb. 014·3 996·9 cco·5 894·1 995·3 cc6·6 998·1 013·1
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PRESSURE AT STATION LEVEL AND AT SEA LEVEL.

ANNUAL MEANS OF HOURLY VALUES.

From readings in millibars at exact hours, Greenwich Mean Time.

Richmond (Kew Observatory): $H_b = 10.4$ metres.

1923.

G.M.T.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
Station Level	mb. 012·70	mb. 012·59	mb. 012·44	mb. 012·36	mb. 012·38	mb. 012·45	mb. 012.60	mb. 012·79	mb. 012·85	mb. 012·91	mb. 012·83	mb. 012·63	mb. 012·40	mb. 012·23	mb. 012·14	mb. 012·13	mb. 012·19	mb. 012·35	mb. 012·57	mb. 012·76	mb. 012·89	mb. 012·93	mb. 012·91	mb. 012·88	mb. 012·58
Sea Level	013.97	013.87	013.71	013.64	013.66	013.72	013.88	014.06	014.11	014.17	014.09	013.89	013.66	013.49	013.39	013.38	013.45	013.61	013.83	014.03	014·16	014-20	014.19	014·16	013.85

PRESSURE AT STATION LEVEL: MONTHLY MEANS AND DIURNAL INEQUALITIES.

The departures from the mean of the day are adjusted for non-cyclic change.

Richmond (Kew Observatory): $H_b = 10.4$ metres.

1923.

1	1	Hour.	G.M.T.		ı		1)		1					Ī .		1	ŀ	1	1		l .			
Month	Mean.		2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.
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	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.
Jan.	1021 52	+0.01	+0.11	+0.06	-0.01	0.0 8	-0.13	-0.01	+0.25	+0.42	+0.48	+0.43	-0.01	-o·37	0 ⋅54	-0.49	-0.40	-0.29	-0.19	+0.09	+0.17	+0.14	+0.15	+0.15	+0.06
Feb.	1001.83	+0.29	+o·23	+0.09	-0.04	−0.0 9	_o.16	-o·18	-0.03	-0.11	0.07	+0.01	o·15	−0 •28	-0.41	0 ∙43	-0.34	-0.23	0.00	+0.21	+0.27	+0.31	+o·38	+0.33	+0.39
Mar.	1016-11	0.06	-0.14	-0.27	-o.31	-0.51	-o·o6	+0.20	+0.44	+o·58	+0.66	+0.57	+0.41	+0.08	-o·19	-o·43	0 ⋅55	-0.49	-0.29	0.0 9	+0.03	+0.07	+0.07	-0·02	-0.01
1	l	١.					١.						l	ار		_			İ			١.			1.
April	1006.77	+0.27	+0.13	-0.04	-0.10	-0.11	+0.07	+0.22	+o.33	+0.31	+0.33	+0.10	-0.07	-0·26	-0.42	-0.61	 -0 ∙70	-0.61	-0.49	-0.10	+0.53	+0.37	+0.42	+0.41	+0.41
May	1012.49	+0.18	+0.01	-0.13	-0.25	-o·15	+0.02	+0.00	+0.10	+0.13	+0.50	+0.07	-0.04	-o·o8	-0.20	-o·37	-0.41	-0.21	-0.39	-0.10	+0.12	+0.40	+0.40	+0.45	+0.35
June	1019.79	+0.04	-0.13	-0.29	-0.30	-o·25	-0.07	+0.08	+0.50	+0.10	+0.58	+0.33	+0.27	+0.13	+0.01	-o·17	-0.29	-0.37	-o·33	-0.22	-0.04	+0.51	+0.27	+0.27	+0.10
Teeles	70706	10.74	0.00	0.05	0.00	10.77	Lovar	10.45	10.54	10.18	10.45	10.00	Lavas		0.00	0.40	0.60	0.57	0.56	0.60	0.22	10.07	LOUTO	10.00	10.06
July	1014.96	+0.14	-0.03	-0.07	0.03	+0.11	+0.31	+0.47	+0.94	10.40	10.45	1-0.33	10.20	0.00	0.22	-0.40	-0.00	0.00	-0.70	0.66	-0.33	+0.01	+0.19	10.20	+0.20
Sont	1013.03	+0.09	+0.14	+0.12	0.48	+0.20	10.44	+0.03	10.04	+0.07	0.40	+0.35	+0.11	-0.07	0.24	-0.52	.057	-0.50	-0.03	-0.00	-1 0.35	-1 0.27	+0.01	10.12	+0.14
Sept.	1014.77	+0.07	_0.10	-0.41	-0.40	-0.30	-0.13	70.14	+0.30	1-0.43	T-0.40	+0.31	T0.23	-0.01	-0.24	-0.44		-0.32	-0.32	0.00	70.20	TO 37	T 0.43	70.34	+0.20
Oct.	1006-27	±0.60	+0.32	-0.01	-0.23	-0.41	-0.65	-0.50	-0.33	-0.18	0.16	-0.13	-0.41	-0.67	0.73	-0.60	-0·5T	-0.15	+0.21	+0.52	+0.60	+0.84	+ 0.91	+0.86	140.78
Nov	1007.94	±0.τ8	+0.18	-0.13	-0.30	-0.30	-0.26	-0.04	+0.31	+0.33	+0.47	+0.27	-0.11	-0.40	-0.70	-0.66	O.5T	-0.26	-0.03	+0.18	+0.33	+0.40	+0.34	+0.28	1.0.21
Dec.	1014.39	-0.01	-0.14	-0.34	-0.52	-0.64	-0.79	-0.65	-0.34	0.00	+0.34	+0.32	+0.16	-0.12	-0.20	-0.10	+0.05	+0.37	+0.52	+0.61	+0.52	+0.45	+0.33	+0.22	+0.21
				- 34					- 34																
Year	1012.49	+0.15	+0.04	-0.12	-0.20	-o·18	-0.11	+0.04	+0.21	+0.27	+0.33	+0.25	+0.05	-o·18	-0.35	-0.45	-0·46	-0.39	-0.24	-0.03	+0.16	+0.29	+0.53	+0.31	+0.27
	"	١. ٢	' '		1			•								10			'			-			1 1

ABSOLUTE EXTREMES OF PRESSURE AT STATION LEVEL FOR EACH DAY.

Maximum and Minimum for the interval oh. to 24h., Greenwich Mean Time.

396	. Ric	hmon	d (Kew	Obse	rvator	y) : H	b = 10	•4 me	etres.	•													1	923.
Month	Ja	ın.	Fe	eb.	М	ar.	A	oril.	M:	ay.	Ju	ne.	Jul	y.	Au	g.	Sej	ot.	Oc	et.	No	ov.	D	ec.
Day.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
1 2 3 4	mb. 014·7 013·7 008·4 020·2	mb. 998·9 002·8 002·7 008·4	mb. 020·9 016·2 016·8 020·8	mb. 015·3 014·2 014·2 013·1	996·8 002·3	990·3	mb. 018·8 021·6 021·3 014·4	018.6	mb. 023·1 023·2 022·3 017·7	021.1	024.4	024.2	015.7	014.3			mb. 018·7 027·1 028·5 026·3	026.2	mb. 022·1 019·3 013·9 017·5	997.0	mb. 023·2 019·6 016·6 010·5	016·5 004·9	mb. 019·3 005·9 004·9	mb. 005·9 994·0 996·2 989·0
5 6 7 8 9	020·1 021·0 020·1 020·4 020·2 010·3	003·8 010·6 011·7 010·2	020·6 012·3 998·4 994·4 006·9 004·6	995·6 985·4 977·5 994·4	007·9 016·5 018·3	018·6 007·5 001·8 006·0 016·5	004·7 004·8 005·0 010·5 010·6	003·6 003·4 002·9 004·7 005·6	015·6 016·4 019·6 019·3 011·0	004·5 007·4 016·0 010·7 005·1	016·0 020·3 022·8 022·0 017·5	014·0 013·4 020·3 015·6 014·0	021·2 020·9 019·0 020·8 021·0	019·3 018·6 015·3 016·5 016·6	022·5 018·4 017·6 019·1 020·1	016·1 016·3 015·0 017·2 016·6	026·5 027·9 024·3	024·0 021·6 024·3 016·7	015.8	010·9 007·8 006·9 005·1	008·9 010·5 014·5 014·0 011·7 026·3	998·1 010·5 998·8 996·1	004·8 016·1 015·3 003·9 021·0 024·0	
11 12 13 14 15	012·4 024·1 027·7 027·4 029·9	012.2	020.8	011·9 016·0 016·4	024·2 024·2 025·7	019·0 016·6 024·1	005·0 001·8 995·5 998·4 000·5	993·6 991·6 993·1	005·5 005·0 007·3	996·9 000·9 003·0	031·1 020·1 021·5	019·9 013·6 017·1	022·2 020·1 018·9	019·5 016·8 015·9	025·9 022·1 021·5	022·0 017·9 016·4	014·5 012·7 006·0	011·4 006·0 998·9	008·8 001·2 010·9	987·7 992·0 001·2	009·8	009·6 987·1	027·1 032·6 033·7	024·0 025·4 026·2 024·3 024·1
16 17 18 19	032.9	029·6 029·7 018·6	008·9 008·9 007·9 999·2 005·8	991·0 992·6	025.8	022·0 023·9 018·6	015·5 019·0 017·8 006·5 005·3	015·5 006·5 003·7	017·4 018·7 017·2	010·7 017·2 011·9	022·4 022·3 019·7	018·9 019·2 017·2	012·5 018·2 019·3	011·2 011·9 018·1	016·5 009·6 013·5	002·7 001·0 009·6	016·9 005·7 011·2	996·2 992·2 005·7	023·7 011·3	019.7	007·2 007·0 006·7 002·0 001·9	997.3	028·I 024·3 024·0 024·0 030·2	022·4 021·1 019·7 020·3 021·2
21 22 23 24 25	029·6 029·1 036·8 035·9 038·4	026·I 027·3 033·2	995.3	976·1 976·3 988·1	016·0 013·7 019·2	013·3 010·7 013·3	005·0 008·1 014·0 018·4 014·5	998·3 008·0 013·9	015·2 019·0 022·4	014·1 012·4 018·0	024·3 025·5 024·2	021·7 020·9 023·4 020·7 018·4	026·1 020·7 014·1	020·7 010·7 010·7	012·9 013·2 010·2	998·5 997·0	008·3 002·0 010·7	997·5 994·2 002·0	994·4 994·0 987·8	990·5 978·2 980·6	005·3 009·1 014·7 021·6 021·8	005·3 008·9 014·7	012.8	001·3 000·4 002·8
26 27 28 29 30	037·4 032·4 026·7 024·7 021·7	032·4 024·9 024·7 015·7 016·2	984.9	979·6 978·7 984·9 —	021.3	015·0 015·8 021·1	004·6 011·3 012·1 011·0 017·1	004·6	019·6 019·5	011·9 014·1 016·8	021·3 022·5 022·8	019.3	016·7 012·0 007·0	012·0 001·5 004·0	003·1 013·4 013·2	001·4 002·7 989 ·2	026·2 027·3 029·6	023.6	995·8 007·8	987·1 993·6 007·8			007·6 024·0 030·2	996·6 994·9 988·3 024·0 012·3
31 Mean	023·I 1025 '35	020·7 1017 ·65	— 1006 '77	997 '49	1019		 1009 ·98	1004	1015			, ,	999·2 1017 ·18	1012	1016	1009				014·2 1002 ·10	1	~	1	021·1 1008 ·98

Readings in degrees absolute at exact hours, Greenwich Mean Time.

397. Richmond (Kew Observatory): North Wall Screen: ht (height of thermometer bulb above the ground) = 3.0 metres.

January, 1923.

								1											. —						
Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20,	21.	22.	23.	24.	M
1 2 3 4 5	79·5 81·0 76·6	80·7 76·6	a. 76·5 80·0 80·5 76·6 71·6	80·0 80·3 76·1	80·1 80·0 75·5	80·I	80·9 79·9 75·4	81·4 79·7 76·2	82·4 80·0 76·8	83·0 80·6	81·5 78·7	82·4 79·2	84·0 82·2 80·2	82·1 80·7	84·2 81·1 80·1	84·I 80·4 79·2	83·6 80·3 78·0	83·8 79·8 77·2	79·1 76·4	80·8 78·4 75·5	81·2 78·1	78·0	81·0 77·5	81·0 76·9 72·8	8 8
6 7 8 9	75·0 82·9 75·5	75·2 82·9 74·9	78·0 76·2 82·5 74·5 76·9	77·3 82·4 75·4	77·6 82·5 76·3	78·3 82·5	78·9 82·5 78·3	79·5 82·6 79·5	80·0 83·0 80·4	80·6 83·6 80·9	80·9 84·0 81·6	81·6 84·0 82·1	82·4 83·6 80·9	83·1 83·9 80·9	83·4 82·5 80·6	83·0 82·6 80·0	83·0 82·0 79·0	83·1 81·0 77·7	83·0 80·0 77·6	83·0 79·0	77·9	77.4	82·9 76·6	82·9 76·0	8
12 13	77·0 73·1 77·6	77.4 72.6 77.9	75·1 77·5 72·6 78·3 75·7	77.6 72.6 78.6	77·3 72·0 78·7	76·8 71·4 79·1	76·1 71·7 79·5	76·0 71·8 79·7	75·5 72·6 80·2	75·8 72·2 81·0	77·1 72·9 82·6	78·3 73·2 83·9	78·8 73·5 83·5	79·2 73·7 83·1	79·1 74·2 83·2	78·3 74·3 83·0	77·4 74·5 82·7	76·6 75·2 81·4	75·6 75·6 80·5	75·6 76·1	74·8 76·6 78·3	74·I 76·9	73·7 77·2	73·5 77·5	7 7 8
16 17 18 19 20	73·4 73·4 76·1	72·I 73·2 75·I	79·0 71·9 73·6 74·6 81·6	73·9 73·6	71·3 74·1 73·3	70·I 74·5 73·6	70·2 74·8 74·2	70·2 75·1 74·6	70·3 75·4 74·6	76·1 75·4	70·6 77·0 76·1	71·0 79·0 78·1	70·9 80·1 78·9	71·1 80·9 78·9	70·9 80·6 79·0	70·9 79·5 79·2	69·9 78·6 79·7	69·8 78·4 80·4	69·5 77·8 80·6	70·7 77·3 81·2	72·2 77·6 81·1	72·6 77·4 81·0	73·0 77·3	76·6	7
21 22 23 24 25	79·6 80·0 73·3	79·3 78·5 73·3	73·7 79·1 77·6 73·6 78·4	78·4 77·0 73·7	77·7 76·2 73·6	77·6 75·3 73·6	77·4 74·6 73·9	77·0 74·0 75·1	76·8 74·2 76·1	77·6 75·4 77·6	81·1 76·6 78·4	82·2 78·1 79·4	82·6 78·6 80·0	83·1 78·7 80·9	83·1 78·6 80·7	82·9 78·1 80·6	82·4 76·8 80·5	81·6 75·1 80·5	81·2 74·1 80·8	80·9 73·7 81·0	80·4 74·1 80·7	80·3 73·6	80·7 73·3	73·I	7
29	79·4 77·5 79·3	77·6 79·1	77·1 79·0 77·4 79·0 81·9	79·0 78·4 79·4	79·0 78·7 79·4	78·7 78·8 79·1	78·7 78·7 79·4	78·7 78·9 79·2	78·9 79·5 80·3	79·5 80·4 81·5	79·7 81·4 82·0	81.9	80·8 82·4 81·8	81·4 82·6 81·7	81·9 82·3 81·9	81·5 82·1 82·1	81·8 81·3	80·9 81·3 82·0	80·3 80·9 82·1	79·8 80·5 82·1	79·0 80·3 82·1	78·2 80·0 82·4	78·3 79·7 82·3	77·8 79·5 82·0	7 8 8
31	82.4	82.5	81.9	81.9	82.2	82.5	82.6	82.7	82.9	83.5	83.8	84.7	84.4	84.8	84.5	84.5	84.9	84.9	84.8	84.4	84.2	84.4	83.8	83.5	8

398. Richmond (Kew Observatory) : North Wall Screen : $h_t = 3 \cdot o$ metres.

February, 1923.

2 84 3 84	4.0	33.6	$\begin{bmatrix} a. \\ 83.9 \end{bmatrix}$	82.0	a.	a.	a.	a.	a.	a.	a.	a.	a.	$\mid a$.	$\mid a$.	$\mid a$.	$\mid a$.	a.	$\mid a$.	$\mid a$.	a.	a.	a.	a.	
2 84 3 84	4.0	33.0	U.) 'Y			Ω 4 ⋅ τ Ι	84.2	84.2	84.5	84.7	85.0	80.0	85.7	85.2	84.0	85.0	85.3	80.0	84.8	84.5	84.0	8	84.0	8	۰
3 184	4.8		82.8	83.0	84.0	84.0	82.0	82:0	84.3	84.6	85.7	85.4	85.5	85.4	85.1	85.2	85.7	85.0	85.0	84.7	84.6	84.5	84.3	84.8	04.5
4 80		84.7	84.6	84.5	84.4	82.8	82.6	82.5	82.5	84:0	84.5	84.5	84.8	84.5	84.0	82.5	82.7	82.2	83.0	81.2	81.1	81.0	87.0	80.0	04.0
	0.0	80.7	80.2	80.4	80.5	80.2	70.6	70.5	70.2	81.0	8T 2	8T·6	82.2	82:0	81.7	81.0	80.6	80.0	78.0	76.6	75.9	75.5	74.2	72:0	03.4
5 72	2.1	71.8	71.4	71.5	71.1	70.6	70.6	71.0	72.8	76.0	78.0	70.6	81.0	81-5	8T·5	80.8	70.4	78.2	77.4	77.0	76.9	76.4	76·T	76.3	79.0
, , , , , , , , , , , , , , , , , , ,	'	,	/- 4	7-3	/	,,,,	, , ,	,	,	,,,,	,,,,,	,,,	0.0	5	01 3	000	794	, 2	// 4	''	,,,,	/ 4	/ -	1,03	13.1
6 76	6.9	77.2	77.0	76.5	76.5	76.8	77:3	77.0	78·o	78.5	78.9	78.2	79.0	78.5	78∙0	78.7	78.4	78.8	78·o	77.9	78.6	79.4	79.3	78.5	77.9
7 178	8·o ′	77:5	77·I	76.4	77·I	78.5	79·I	79.5	80.1	80·0	80·0	80.5	81.5	82.5	82.8	82.9	82.0	82.9	83.1	83.2	83.4	83.6	83.7	84.0	80.7
8 84	4.1 8	83·I	83·I	83·1	82.7	82.6	82.6	82.9	82.8	82.9	83.0	82.7	80.5	80.8	$ 81\cdot8 $	81.6	81.4	80.7	80·1	79.4	78.2	77.6	77.0	78.2	81.5
9 177	7.5	77·0	76.9	77.8	78∙o	77.7	76.7	76.2	76.9	78.4	79.0	80.2	81.5	82.0	82.5	82.4	80.9	79.6	79.2	78.9	79.3	79.9	80·0	80·1	70 · T
10 80	0.2	80∙3	8o·5	80.5	80∙6	8o·6	80∙8	80.3	80∙1	80.4	80.5	80∙6	80∙3	79.9	80.2	80.3	80.5	80∙6	80.7	80.7	80.6	80.6	81.0	81.2	80.5
		87.0	Q+.+	80.6	-0	-0.0	~ 0	70.6	90.6	0	00.0	00	۰	0	0	00.0	0-	00.	00.7	-0.0		(1	
11 81 12 79	1.5	78.6	97.1	77.1	79.7	79.3	79.4	79.0	75.7	01.7	02.2	80.7	02·4 81.6	03.3	03.2	02.2	80.6	80.5	80.1	79.3	78·9 79·2	79.0	129.0	79.6	80.9
13 79	0.0	70.2	70·I	78.7	78.2	78.T	78.T	78·T	78.2	78.7	70.1	70:0	70.2	70.6	70:4	70.5	70.3	70.2	70.2	79.0	78.9	79.1	78.7	78.9	70.0
14 77	7.7	77.6	77.2	77.1	77.T	76.0	77.0	77.2	77.3	77.5	77.5	77.5	77.6	77:0	78.2	78.5	78.4	77.5	77.0	76.5	76.5	76.6	76.5	76.0	70.0
15 76	6.0	75.0	76·I	76.1	76.0	75.3	75.5	75.7	76.0	76·T	76.3	77.I	70.0	80.0	80.5	80:5	70.8	70.5	70.5	70.6	80.0	80.0	80.0	80.4	77.3
-5		,,,	,	,	/ -	/33	133	13 /	, ,	, , ,	1, 3	// -	,,,,,	0	100 5	3	,,,	1,33	193	190			000	4	1779
16 80	80.5	8o·6	80.9	80.4	79.5	78.2	77.6	77.4	78.3	79.5	81.3	82.4	82.4	82.6	82.4	82.0	80.4	79.4	79.5	79.6	80·o	80.5	80.5	80.5	80.3
17 79	79.9	79.9	80.5	79.7	78.9	78.5	78.3	78·0	78.9	80.2	181.5	8.18	81 ∙6	l8 1∙ 4	81.0	81.2	80·8	78.9	78·o	77.2	77.0	77.0	76.7	76.5	70.4
18 170	76·0	75.7	75.3	75.0	75.0	75.0	75.0	75·I	75.5	76.4	77.5	78.5	79·I	79.6	81.0	81.2	81.0	79.9	79.0	78.9	77.9	77.3	76.0	75.8	77.4
19 70	76·I	75·I	74.7	75.3	75.0	75.4	75.8	76∙0	76.5	76.6	76.5	76.6	76.6	76.5	76.1	75.7	75.3	75.2	75.2	75·I	75.2	74.9	74.7	74.6	75.6
20 74	74.7	74.6	74.7	74.7	74.6	74.7	74.6	74.5	74.7	74.8	75.0	75.5	75.2	75.5	75.2	75.1	75.1	75.2	74.8	74.6	74.2	73.9	73.7	73.8	74.7
27			74.6	77.0	77.0	6	-6.0	-6				0	0	_0 -		0									i
21 74 22 75	4.2	74.1	74.6	75.0	75.2	75.0	70.2	70.7	77.5	77.7	79.5	81.3	80.1	70.1	79.2	80.0	79.5	77.7	77.7	76.9	76.7	76.0	75.7	75.6	77·1
23 77	27.5	77.6	77.0	78.0	74.7	73.0	73.5	73.2	75.0	70.4	00.2	28.0	00.0	01.1	87.0	79.1	70.3	79.1	79.2	79.3	78.5	78.2	77.6	77.7	77.4
24 78	8.0	78.0	77.0	70 T	70:1	70.3	77.3	77.2	80.7	77.5	77.5	70.0	79.4	87.0	87.0	80.5	80.8	70.5	70.9	70.0	75·8 80·5	75.3	77.6	77.5	78.0
25 80	30.0	80.0	70.6	70.5	70:0	78.0	78.3	78.4	70.4	80.7	80.6	81.5	82.2	82.6	82.2	80.5	82.0	81.5	80.7	78.2	78.8	70.6	00.4	100.0	80.0
-5		00 0	790	1/9 3	1,90	1,09	/° 3	/° 4	19 4	00 1	100.0	01.5	02 3	02 0	02 2	02.7	03.0	01.3	00.2	70.2	70.0	79.0	79.5	79.9	00.2
2 6 80	0.9	81·1	81.4	81.4	81.1	81·o	80.7	80.9	81.4	82.6	84.2	85.3	85.3	85.0	84.8	84.5	83.4	82.5	81.5	81.1	81.0	80.1	80·a	81.0	82.2
27 80	50·4	79:9	80.2	80.1	79.6	79.5	79.6	8o·o	81.4	82.1	82.4	82.7	83.4	83·I	83.1	83.0	82.3	81.8	81.4	81.0	81.0	81·0	81.0	81.1	81.3
28 81	31·1	81.0	80.9	81.4	81.4	81.3	8o·6	80.4	81.4	82.0	82.6	83·o	83.8	82.9	83.4	82.9	82.1	81.5	79.6	79.5	79.4	79.2	79.6	79.4	81.3
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Mean 78	′8·9	78.8	78.7	78.7	78.4	78.3	78.2	78.2	78.8	79.6	80.3	80·8	81.1	81.2	81.3	81.2	80.7	80.1	79·6	79.1	79.0	78.9	78.9	78.8	79.5
G.M.T	1.	2.	3.	1		6.		8.			7.	Noon	7.2	7.4	7.5	76	T.77			20	21				Moor
S.M	1.		3.	4.	5.	0.	7⋅	0.	9.	10.	11.	TAOOL	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
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10. 11. Noon 13. 14. 15. 16. 17.

399. Richmond (Kew Observatory): North Wall Screen: h_t (height of thermometer bulb above the ground) = 3.0 metres.

March, 1923.

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1 2 3 4 5	77·4 76·7	81·8 76·4 76·9	81·4 76·0 76·7	75·5 76·5	80·0 74·9 76·0	a. 80·0 79·2 74·2 75·6 75·0	79·1 73·9 76·0	79·5 74·2 77·0	80·6 74·3 77·5	81·6 76·1 78·0	82·7 78·8 78·5	81·1	83·7 82·1 80·4	84·2 83·1 79·9	84·2 83·8 81·1	83·8 83·6 81·0	82·7 82·9 80·7	81·9 79·6	80·4 80·5 78·9	79·6 79·0 78·3	77·7 78·3	78·8 76·9 77·8	78·2 76·5 77·4	76·1	81 · 2 78 · 2 78 · 1
6 7 8 9	77:9 78:5 80:1 76:2	77·0 78·4 79·6 76·0	77·7 78·4 79·1 75·9	77·6 78·0 79·5 75·6	77·3 78·5 79·4 75·5	77.6 78.2 78.2 75.3 75.7	77·9 78·0 78·0 75·3	77·8 79·1 78·6 75·6	77·6 80·1 79·0 75·7	80·1 81·5 79·0 75·9	82·0 80·5 79·2 76·4	83·3 81·2 80·0 76·8	83·7 83·0 80·7 77·2	84·0 81·0 80·5 77·3	83·5 81·2 81·0 77·8	82·7 81·6 79·9 78·2	81·9 81·4 79·6 78·4	81.6 80.6 78.8 78.2	81·5 80·1 78·0 78·0	80·4 80·5 77·5 77·6	79·6 81·0 77·2 77·4	79·0 80·8 77·1 77·0	78·6 80·2 76·8 77·0	78·6 80·3 76·6 76·8	79·9 80·1 79·0 76·7
11 12 13 14	76·4 78·6 77·1	74·8 78·6 76·9	74·0 78·8 77·1	73·4 79·0 77·6	73·4 79·0 77·6	76·1 72·5 79·0 77·6 76·5	72·8 79·0 77·6	73·8 78·6 77·8	77·0 78·7 78·0	78·8 78·3 78·9	80·5 78·6 79·5	79·1 79·6	80·8 79·5 79·6	81·0 79·5 79·9	80·8 79·6 78·7	80·3 79·6 79·0	79·4 79·6 78·6	78·7 79·7 78·5	78·5 79·8 78·2	77·9 79·8 77·8	77·6 79·6 77·4	77·6 79·0	77·7 78·5 76·9	78·2 77·7 76·8	77 · 6 77 · 3 79 · 1 78 · 1 77 · 3
16 17 18 19 20	79·0 78·4 78·0	79·I 78·I	79·4 78·0	78·3 77·7 76·0	77·9 77·2 76·6	78·1 78·0 77·0 76·1 73·2	78·2 77·0 76·6	78·6 78·0	79·2 78·7	79·6 79·5 79·4	80·2 80·2	80.7	81·4 81·7 81·5	82·6 81·9 82·3	82·5 81·3 81·7	82·3 81·1	80·6 80·1	80·6 80·1 79·7	80·0 79·6 79·3	79·6 79·2 79·2	79·2 78·9 78·5	79·1 78·5	78·6 78·0	78·4 77·9 76·8	79 · 1
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31	82·o	81.9	81.4	80.9	80.5	80.6	81.1	82.0	83.4	84.0	85.5	87.0	87.0	86.4	86.2	86·o	86.5	84.7	83.6	81.4	81.5	81.4	81.1	81.0	83.
Mean	78.7	78.4	l~0.0	78·I	77.9	77.7	77.8	78·5	79:3	80.3	81.2	82.0	82.6	82.8	82.8	82.6	82.1	81.4	80.7	80.1	79.7	79.3	79.1	79.0	8o·
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400. Rid	81.7 79.2 80.4 78.5 83.4 84.8 82.4 79.0	a. 78.7 79.5 79.6 78.6 81.4 81.5 79.1 80.4 76.2 73.1 82.6 84.4 82.3 78.5	a. 78·7 79·4 79·5 78·4 81·5 79·2 81·4 75·8 81·5 79·2 81·4 82·4 82·6 78·5	a. 78.8 79.5 79.1 78.2 80.9 80.7 79.3 81.3 75.4 73.5 82.4 83.1 78.2	atory) a. 79.0 79.5 79.0 78.1 81.0 80.2 79.4 80.9 75.6 73.6 82.5 88.9 98.77.7	a. 78·7 79·9 79·1 77·6 81·1 80·0 79·3 80·3 75·6	a. 79.6 80.9 79.3 78.3 81.4 79.9 79.6 80.0 76.6 74.5 82.9 85.2 81.0 80.0	a. 80·3 81·2 80·2 80·9 82·5 80·0 80·1 80·2 77·8 76·1 83·7 85·8 82·5 81·4	a. 80·8 82·0 81·7 83·7 83·9 80·1 81·1 79·9 78·1 77·3 84·5 85·4 83·9 82·1	a. 81·9 83·2 83·4 86·0 84·5 80·6 82·5 78·0 79·5 86·4 85·0 84·8 82·0	a. 83.0 84.5 84.9 87.1 85.3 80.6 83.8 80.9 78.0 80.7 86.9 87.0 85.9	a. 84.6 85.4 85.4 88.6 85.6 80.6 84.7 80.4 78.3 82.5 88.0 89.9 86.2 81.7	a. 86·3 86·5 87·0 89·0 86·0 80·8 85·6 81·0 78·0 83·6 89·0 90·8 85·9 84·5	a. 86·2 87·0 87·5 89·7 85·8 81·2 86·6 81·0 77·9 84·5 89·2 88·5 85·8 83·2	85.6 87.3 87.5 89.7 85.1 81.5 86.9 82.5 78.2 84.8 87.1 86.4 85.4 83.3	85·4 86·5 87·8 89·0 85·0 81·0 87·4 81·8 78·3 85·2 87·1 85·9 84·6 83·1	85·1 84·9 86·9 87·4 83·3 80·6 86·0 81·1 78·1 85·3 87·1 85·8 84·0 82·6	84·5 83·8 85·0 85·6 82·6 80·6 85·7 77·6 85·1 86·7 84·9 82·4 82·8	83.8 82.9 83.9 84.4 82.1 80.2 84.9 80.1 76.4 83.7 86.2 84.8 82.0 81.0	83·3 81·9 82·3 83·8 82·2 80·0 83·1 79·5 75·4 83·4 85·7 83·7 82·0 79·5	82·7 81·3 82·3 82·9 82·2 79·8 82·4 79·0 75·4 83·4 84·8 83·1 81·8 79·0	81·5 81·0 81·4 82·1 82·0 79·6 81·6 78·9 75·0 83·8 84·4 83·4 81·5 78·3	a. 80·9 80·5 80·3 82·1 81·9 79·3 81·3 78·6 74·3 83·4 83·4 83·3 80·6 77·3	a. 80·5 80·1 79·4 81·6 81·8 79·3 80·4 78·5 73·9 83·8 83·5 82·9 79·5 76·9	82 · 82 · 83 · 82 · 76 · 85 · 85 · 83 · 80 · 85 · 83 · 80 · 85 · 85 · 85 · 85 · 85 · 85 · 85
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TEMPERATURE.

Readings in degrees absolute at exact hours, Greenwich Mean Time.

401. Richmond (Kew Observatory): North Wall Screen: ht (height of thermometer bulb above the ground) = 3.0 metres.

May, 1923.

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402. Richmond (Kew Observatory): North Wall Screen: ht = 3.0 metres.

June, 1923.

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ı	l٥.	a.	a. 81·3	a. 81·2	a. 81·2	а. 81 о	a. 81 2	a. 81.6	a. 82·2	a. 82·7	a. 83·2	a. 83·8	a. 84·7	$\begin{array}{c} a. \\ 85.8 \end{array}$	a. 85·7	86·4	85·5	84·9	84·8	85.0	84.7	84.1	83.7	82.9	82.7	
2																										
3	70	9.4	77.7	82.2	70·7	77.5	81.6	81.0	81.6	82.2	82.6	83.1	82.7	82.2	83.8	83.7	83.3	83.4	83.1	82.8	82.1	81.7	81.2	80.7	83·4 80·4 84·2	8ž·4
4 5	80	0.0	70.8	70.3	70.2	70.5	70.7	80.6	81.0	81.6	80.7	81.2	82.0	83.7	84.7	86.2	85.9	86.8	87.0	86.2	85.5	84.7	84.6	84.2	84.2	82.8
,																										
6	84	i.I	84.0	84.3	84.1	84.0	84.3	84.2	84.2	83.9	84.7	85.6	86.5	86.6	88.8	80.0	04.1	80.0	80.7	80.1	88·o	86.6	86.2	86.1	83·5 84·7 85·6	86.6
7 8																										
9																									87·4 84·1	87.9
10	3	7.5	87.5	87.4	87.2	87.5	87.9	88.5	88.5	88·o	87.9	87.9	87.5	90.2	91.4	91.9	92.1	91.6	91.1	89.1	87.5	86.4	85.4	84.8	84.1	88.4
II	8:	3.6	83.5	83.0	82.6	83.5	84.1	85.1	86.5	87.4	87.6	87.4	87.5	88.6	89.4	89.5	89.6	89.5	88.6	88·o	86.4	85·o	84.0	83.0	82·0	86∙1
12	3	0.1	80.1	79.9	8o·o	81.1	82.7	84.0	85.5	86.5	87.0	87.8	88·8	89.6	89∙0	88.4	87.8	87.1	85.9	85.5	85.1	85.0	84.5	84.9	85·1	85.0
13	3	5.5	85.6	86∙1	86.3	87.0	87.3	88.1	89.4	90.4	90·I	91.8	92.8	93.1	93.0	93.1	93.1	90.9	89.7	88.1	87.1	86.6	85.5	84.5	85·I 83·6 85·8	86.3
14	3	5·1	84.7	84.2	84.2	83.8	83.8	84.8	85.1	86.2	86.7	87.1	87.8	88.2	87.7	88.4	86.5	87.0	86.7	86.6	86.6	86.4	86.3	86.2	85.8	85.5
15	O	3.0	03.1	02.0	02.0	102.0	03.3	103.7	02.1	100.7	07.0	07.2	0/2	07.0	00.3	00 4	100 3	"	/	1						
16	3	5·I	84.2	83.2	83.1	82.9	83.2	82.6	83·I	83.3	82.0	82.1	83·o	83.9	83.6	84.9	85·o	85.0	85.3	84.7	84.0	83.2	82.9	82.7	82·2 79·8 85·6 83·7 83·9	83.6
17	3	1.8	81.8	81.8	81.3	81.3	81.3	81.8	83.0	83.7	83.9	84.7	85·o	85.7	85.8	86.7	86.9	87.6	86.8	86.6	85.3	83.5	81.7	81.2	79.8	84.6
18	79	3.I	79.2	78.8	79.9	80.2	80.7	81.7	83.3	84.9	86.3	86.1	86.9	88.3	87.6	88.4	87.7	87.8	87.8	86.7	86.1	85.5	84.7	84.1	83.7	86.3
19	8	5.6	85.5	85.3	85.0	85.1	85.5	85.6	86.1	86.7	87.1	87.7	87.0	86.T	86.7	86.5	85.5	85·T	85.0	85·I	84.8	84.1	84.0	83.9	83.9	84.5
20	١٠,	34	ე⊙	030	020	02.0	030	030	039	94 4	103 x	00 1	00 /	-	,	1 3	1 3 3	"	"	-		1			1	[
21	8:	3:5	82.8	82.5	81.8	81.9	82.9	85.0	86∙1	88·o	89·I	89.9	90.3	91.5	91.4	91.0	90.0	89.5	89.4	88.6	88.4	88.0	87.6	87.2	86·5 86·4 90·9 89·2	87.1
22	86	5.4	86∙1	86·I	86.2	86.6	87.7	89.2	90·I	91.2	90.7	91.5	92.5	93.6	93·I	93.4	93.9	92.6	91.7	92.6	91.1	89.6	99.0	07.3	00.4	01.9
23	86	5•1	85.2	84.7	84.2	84.3	86∙1	87.6	89.7	90.5	91.6	93.I	94·I	94.9	95.6	96.8	96.5	90.0	03.3	190.2	95.1	00.6	00 · T	80.6	80.2	01.0
24	193	0.2	89.7	89.2	89.0	89.1	90.0	00.I	90.2	90.7	91.9	91.8	92.7	92.0	92.2 86.1	93.4	85.2	85.0	85.0	84.5	84.0	84.0	83·I	83.4	89·2 83·4	86.5
25																										
26	8:	3.6	83.2	82.5	82.9	83.0	83.5	84.5	85.7	86.8	87.0	87.0	86.7	85.6	85.9	87.1	88.3	88·o	88.1	87· o	86.2	85.2	83.6	83.4	81·9 84·8	85.3
27																										
28	84	4.5	84.0	83.9	84.1	84.3	84.8	85.7	87.5	88.9	89.9	91.1	91.0	92.1	92.0	92.3	92 1	91.6	06.7	05:0	01.5	00.T	80.0	87.4	86.5	80.8
29	8	5·1	84.7	84.2	83.6	83.4	84.1	85.1	86.9	88.6	90.2	91.5	93.1	94.4	95.4	190.0	90.2	90.0	190.7	95.0	90.5	89.6	88.9	88.5	86·5 87·1	88.8
30	lo:	5.2	84.7	84.2	83.2	04.1	04.8	80.0	07.5	89.4	90.5	91.0	92.2	92.1	92.4	92.0	92 2	9- 4		7					<u> </u>	
Mean	. 8.	4.0	83.6	83.3	83.2	83.4	83.9	84.8	85.7	86.6	87.2	87.7	88.2	88.9	88.9	89.3	89.2	88.9	88.5	88·o	87.1	86.3	85.6	85.1	84.5	86.3
G.M.T		I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
			l		<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	1	1	1	1	<u> </u>	-	1	<u> </u>	<u> </u>	<u>. </u>	<u> </u>	<u> </u>	<u>'</u>	<u>'</u>		<u></u>	

103. Richmond (Kew Observatory): North Wall Screen: h_t (height of thermometer bulb above the ground) = $3 \cdot 0$ metres.

July, 1923.

																								ly, 19	
Day.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
1 2 3 4 5	86·1 85·5 88·2	84·8 85·2 87·5	84·2 84·0	83·7 84·5 87·5	83·6 84·6 87·7	84·8 85·1 87·9	86·3 87·0 89·3	a. 86·7 87·9 89·9 89·7 90·8	90·5 90·8	90·1 90·4	90·5 90·2 92·1	91·5 90·6 92·0	93·0 91·2 93·5	93·2 90·7 93·9	92·9 90·8 94·7	92·7 90·3 95·0	92·5 90·7 95·2	92·3 89·9 94·5	94.8	90·2 89·9 92·3	88·9 89·4 90·5	88·8 89·5	87·0 88·6 87·5	86·0 88·5 86·0	88 · 8 88 · 5 90 · 8
6 7 8 9	88·9	91·1 92·4 86·9	92·0 86·2	90·5 91·5 86·7	91·0 91·5 86·9	93·0 91·2 87·9	95·7 90·5 89·4	93·8 98·9 90·6 91·3 91·4	99·5 90·5	00·6 91·4 95·3	93·4 96·3	94·I	02·5 95·7 98·9	03·4 97·4	99·I	03·6 98·7 01·7	03·9 99·4 99·8	02·4 98·7 98·5	97·1	99·0 96·4 94·9	93.2	96·2 92·0 93·2	91.4	94·4 89·5 90·2	93.6
11 12 13 14 15	92.6	93·9 94·5 92·1	92.3	92·9 93·5 91·6	93·4 92·7	94·3 93·9 92·6	95·I	94·8 97·8 97·4 93·2 93·7	99·7 93·7	02·2 01·4 95·1	02·9 02·6 95·8	03·9 96·3	04·3 04·7 97·7	04·5 04·8 99·2	04·9 03·8 99·2	04·7 02·6 98·7	05·1 02·5 98·8	03·9 02·1 99·4	02·3 01·8 98·8	00·1 98·5 97·0	98·6 96·6 95·2	97·6 94·5 94·3	94·0 93·8	95·6 93·4 93·3	98·6 9 5 ·3
16 17 18 19 20	86∙3	87·0 86·6 85·8	86·8 85·1	86·1 86·6 84·2	86.5	87·0 85·2	86·1	92·0 93·5 88·4 88·6 92·1	90·I	90.5	91.5	91·6	91.8	92.8	93·3 89·8	92·6 89·8	92·2 89·6	92·1 89·5	88·5 91·6 89·0	89·4 90·8 88·7	89·5 90·2 88·7	90·4 89·0 89·2 88·7 93·5	87·5 87·6 89·1	88·1 87·4 89·5	89·6 88· 6
21 22 23 24 25	90·5 88·0 89·9	89·6 87·4 89·6	89·0 87·0 88·6	88·5 86·6 87·5	88·5 86·7 87·5	89·5 88·0 87·5	90·4 89·0 88·2	91·0 92·4 89·9 89·2 91·5	92·4 91·0 90·1	93·6 92·0 90·5	94·5 93·0 91·5	95·4 95·1 92·4	95·6 94·7 93·6	96·2 94·5 94·7	96·3 91·9 95·6	97·0 92·1 96·4	97·0 92·0 96·5	96·5 91·5 96·3	96·0 91·5 95·1	90·5 93·6	92·2 90·4 92·I	93·2 90·6 90·5 91·0 88·8	90·5 91·1	90·3 90·1	92·7 90·5 91·6
26 27 28 29 30	84·7 89·1 85·9	89·0 85·6	83·2 89·0 85·2	82·8 88·6 85·0	83·3 88·8 85·1	84·5 89·2 86·1	85·4 90·0 87·1	87·6 86·6 90·1 88·7 89·6	87·8 91·2 90·2	91·6 89·1	89·9 91·0 92·0	90·5 90·3 92·9	91·6 90·6 92·2	92·I 90·5 92·9	92·3 91·7 93·3	91·7 93·2 93·6	91·6 91·9 92·7	91·1 90·8	90·7 90·5 91·4	89·9 89·6 90·7	89·8 87·7 90·7	89.8	89·1 86·9 89·2	89·1 86·5 89·2	89·8 89·7
31	87.9	87.5	87.0	86.7	86.8	87.8	88.2	88.7	90.0	90.6	91.0	91.6	91.1	90.5	90.4	89.1	88.3	87.7	87.6	85.9	85.6	85.7	85.1	84.7	88.2
			100	000	00.0	88.0	80.8	07.7	02.2	03.3	04.2	04.8	95.4	96.0	96.1	95.9	95.9	95.3	94.5	93.0	91.9	91.0	90.2	89.7	92.2
Mean		88.7	<u> </u>		1		<u> </u>		1	[<u> </u>		<u> </u>	1	1	1	<u> </u>	<u> </u>	1	1		<u> </u>		. 10	102
404. Ric	hmoņe a. 84:3	d (Ke	a. 84·2	80rV:	atory)): N a. 85.1	orth a. 86.6	Wall	Scre	en :	ht =	3.0 a.	metr	es.	a.	a. 93.4	a. 93·3	a. 93·5	a. 92·7	a.	<i>a</i> . 90.0	a. 89·3	a. 88·5	st, 19	a. 89·1
404. Ric	a. 84·3 86·8 87·0 85·3 83·5	a. 84.4 87.1 86.6 83.9 83.0	a. 84.2 87.4 86.5 83.2 82.3	a. 83.9 86.9 86.2 83.3 81.6	atory) a. 83.7 86.6 86.2 83.1 81.6	a. 85.1 88.0 86.5 85.0 84.9	orth a. 86.6 89.0 87.5 86.1 87.9	Wall a. 87.8 90.5 88.5 87.6 90.5	Scre a. 89.1 91.6 89.6 89.5 93.2	en: 89.9 92.9 90.0 90.6 94.6	ht = a. 91·1 94·0 91·1 92·5 96·0	3.0 a. 91.5 94.0 92.1 93.0 96.7	metr a. 92.7 94.8 93.3 94.0 97.2	a. 93.2 94.1 93.5 95.9 98.1	a. 93.5 92.5 93.8 96.2 98.3	93·4 92·1 94·0 96·4 97·0	93·3 94·1 93·6 97·3 97·3	93·5 93·6 93·1 95·0 97·0	92·7 92·8 91·9 93·1 96·7	a. 91·1 90·5 90·0 90·9	90·0 89·2 88·6 88·6 90·6	a. 89·3 88·3 87·7 87·0 91·0	a. 88·5 87·7 86·6 85·8 89·5	a. 87.6 87.4 86.3 84.8 88.6	a. 89·1 90·5 89·6 89·5 91·2
404. Ric	a. 84·3 86·8 87·0 85·3 83·5 88·4 88·6 87·4	a. 84.4 87.1 86.6 83.9 83.0 87.9 88.5 88.4	a. 84·2 87·4 86·5 83·2 82·3 87·5 87·0 88·3 87·0	a. 83.9 86.9 86.2 83.3 81.6 86.5 86.4 88.0 85.9	a. 83.7 86.6 86.2 83.1 81.6 86.1 86.0 87.5	a. 85·1 88·0 86·5 85·0 84·9 86·6 87·2 88·5 87·4	orth a. 86.6 89.0 87.5 86.1 87.9 87.0 88.4 89.8	Wall a. 87.8 90.5 88.5 87.6 90.5 88.3	Scre a. 89·1 91·6 89·6 89·5 93·2 90·0 92·1 92·4 93·6	en: 89.9 92.9 90.0 90.6 94.6 91.4 93.3 93.3	ht = 4.0 91.1 94.0 91.1 92.5 96.0 93.1 93.8 94.9 97.4	3.0 a. 91.5 94.0 92.1 93.0 96.7 94.0 94.2 97.0 99.4	metr 92.7 94.8 93.3 94.0 97.2 95.4 95.9 97.9 90.4	a. 93.2 94.1 93.5 95.9 98.1 96.4 96.9 99.2	a. 93.5 92.5 93.8 96.2 98.3 96.5 97.4 90.5 01.7	93.4 92.1 94.0 96.4 97.0 97.1 97.1 00.6 01.0	93·3 94·1 93·6 97·3 97·3 97·2 01·1 00·9	93·5 93·6 93·1 95·0 97·0 97·3 97·8 99·9 00·0	92·7 92·8 91·9 93·1 96·7 95·5 96·4 99·5 98·7	a. 91·1 90·5 90·9 94·1 93·6 94·0 95·7	90.0 89.2 88.6 88.6 90.6 91.8 92.7 93.8 95.2	a. 89·3 88·3 87·7 87·0 91·0 89·8 91·6 91·9	a. 88·5 87·7 86·6 85·8 89·5 89·0 90·1 89·6 92·7	a. 87·6 87·4 86·3 84·8 88·6 88·4 89·3 88·4 91·7	a. 89·1 90·5 89·6 89·5 91·2 91·4 92·2 93·6 94·2
404. Ric 1 2 3 4 5 6 7 8 9	a. 84·3 86·8 87·3 88·4 88·6 88·6 88·6 89·4 90·4	a. 84·4 87·1 86·6 83·9 88·5 88·4 86·9 89·5 88·7 86·3 87·2	a. 84·2 87·4 86·5 83·2 82·3 87·5 87·0 88·3 87·0 89·1 88·5 86·1	83.9 86.9 86.2 83.3 81.6 86.5 86.4 88.0 85.9 88.6 87.9 88.6 87.9 88.6 85.5 86.5	atory) a. 83.7 86.6 86.2 83.1 81.6 86.1 86.0 87.5 85.9 88.0 87.6 86.1	a. 85·1 88·0 86·6 87·2 88·6 87·6 88·6 86·6	orth a. 86.6 89.0 87.5 86.1 87.9 87.0 88.4 89.8 89.3 89.9	Wall a. 87.8 90.5 88.5 87.6 90.5 88.3 90.6 90.5 91.4	Scre a. 89·1 91·6 89·6 89·5 93·2 90·0 92·1 92·4 91·9 92·3 93·1 94·4	en: 89.9 92.9 90.0 90.6 91.4 93.3 93.3 93.3 95.9 93.2 93.3 94.6 96.8	ht = a. 91·1 94·0 91·1 92·5 96·0 93·1 93·8 94·9 95·0 93·7 95·4 98·1	3.0 a. 91.5 94.0 93.0 96.7 94.0 94.2 97.0 99.4 96.1 94.9 96.0 99.6	metr a. 92.7 94.8 93.3 94.0 97.2 95.4 96.5 95.9 90.4 96.5 95.9 90.4	es. a. 93.2 94.1 93.5 95.9 98.1 96.4 96.9 99.2 01.3 96.6 96.0 98.0	a. 93.5 92.5 93.8 96.2 98.3 96.5 97.4 00.5 98.0 96.0 98.6 00.5	93.4 92.1 94.0 96.4 97.0 97.1 90.6 01.0 97.2 96.4 97.6 00.2	93·3 94·1 93·6 97·3 97·0 97·2 01·1 00·9 97·7 96·4 97·0 99·5	93.5 93.6 93.1 95.0 97.0 97.3 97.8 99.9 00.0 97.2 96.0 96.5 99.2	92·7 92·8 91·9 93·1 96·7 95·5 96·4 99·5 98·7 96·1	a. 91·1 90·5 90·0 90·9 94·1 93·6 94·0 95·7 94·1 93·1 93·1 93·1 93·1	90·0 89·2 88·6 88·6 90·6 91·8 92·7 93·8 95·2 93·3 91·6 90·1 94·9	a. 89·3 88·3 87·7 87·0 91·0 89·8 91·6 91·9 92·1 90·0 90·4	a. 88·5 87·7 86·6 85·8 89·5 90·1 89·6 92·7 91·8 88·7 89·5 93·0	a. 87.6 87.4 86.3 84.8 88.6 88.4 89.3 88.4 91.7 90.5 87.0 88.9 92.0 93.2	a. 89·1 90·5 89·6 89·5 91·2 91·4 92·2 93·6 94·2
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405. Richmond (Kew Observatory): North Wall Screen: h_t (height of thermometer bulb above the ground) = 3.0 metres.

September, 1923.

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3	80.1	80.5	79.4	80.0	79.5	79.3	80.5	82.5	84.7	86.3	87.5	87·7 86·6	89·1	89.7	89.7	90.9	90.6	89.8	86.3	85.0	84.1	83.7	82.7	81.8	
4	80.2	80.2	181.7	181.7	81.0	182.7	04.2	05.2	05.2	185.7	80.2	80.0	190.0	187.2	107.3	199.0	100.0	100.4	192.0	105.4	104.9	103.0	83.2	82.9	ľ
5	82.7	81.0	81.6	81.1	81.0	81.7	82.7	83.7	85.7	87.2	88.5	89.6	90.6	91.3	91.8	92.1	91.9	91.1	89.1	87.6	86.5	85.6	84.7	84.1	ľ
6	83.5	83.2	82.1	82.0	82.0	82.6	82.9	83.8	85.0	85.8	87.6	88.7	90.4	91.1	92.6	93.7	94.1	92.9	90.4	88.6	87.5	86.3	85.7	85.1	8
7	84.3	183.8	83.8	84.7	185.7	186.6	87.1	87.6	188.5	8 q ⋅6	91.1	91.4	0.16	92.0	93.9	94.2	94.5	92.6	90.6	88.6	87.6	86.5	85·I	183.6	18
8	82.9	82.0	81.0	80·I	79.5	78.9	80.6	82.5	84.6	87.1	88.7	89.7	91.3	92.1	92.6	92.7	92.6	90.7	88.6	86.7	85.3	83.6	82.2	81.0	18
9	80.6	79.8	79·I	79.0	78.3	78.2	79.6	82.6	185.8	88.4	90.7	92.2	93.6	94.3	94.9	94.2	95·I	93.8	91.5	89.6	88.3	87.0	87.1	87.1	8
10	86.7	85.2	85.6	85.5	85.8	85.7	86∙1	86.8	88.8	90.9	91.5	92.4	93.2	93.9	93.5	93.0	92.6	90.5	89.4	89.4	88.7	88.4	88∙0	87.8	8
11	87.2	86.9	86.6	86.7	86.9	86.7	86.5	87.0	87.5	88.9	90.3	90·9 91·2	92.0	93.5	93.7	93.9	93.9	92.5	90.5	89.3	88.3	87·o	86∙1	85·o	8
12	85.0	84.4	84.0	84.0	83.6	83.4	84.4	85.4	87.0	88.3	89.9	91.2	92.5	93.3	93.6	93.8	92.9	91.9	90.0	88.3	87.5	86.4	85.0	84.5	8
13	84·I	183.2	83.1	83.2	83.3	82.6	83.1	84.5	86·o	88·o	90.3	92.4	94·I	95.0	95.2	94.2	93.2	91.8	90.4	88.6	88.5	87.9	87.6	87.4	18
14	87.4	86.2	86.7	87.1	87.4	88∙o	88.6	89.2	90.0	91.5	92.6	92.8	93.3	93.2	92·I	92.4	91.3	90.8	90·I	88.2	88·o	87.8	87.9	87.3	8
15		1	1	1	1	1 .				1	Į	92·8 88·3	i		1			1	- 1					1	ł
16	80.7	80.2	79.7	79.2	79.0	78.7	79.7	81.2	83.2	84.6	85.6	86·2 88·2 84·6 86·1 86·1	87.2	88·o	88.6	88.3	88∙1	86.4	84.8	83.7	83.2	82.3	81.5	81.2	8
17	80.5	79.2	78.8	79.3	78.9	78.9	80∙3	83.2	85.6	86.9	87.8	88.2	88∙9	89.2	89∙1	88.8	88.6	86.2	84.6	83∙6	82.5	82.4	83.2	83·o	8.
18	82.7	82.2	83.8	84.5	83.6	83.5	83.6	84.3	85∙0	85.2	84.4	84.6	86∙1	87∙1	86.6	87.3	87.4	85.8	84.8	84.0	83.3	82.6	81.9	81.3	8.
19	80∙8	80.9	80.5	8o·o	79.8	79.7	80∙8	82.5	84·o	85.1	86∙1	86∙1	87.1	87.2	87.4	85.6	85.4	85·0	84.7	84.7	84.8	84.6	84.7	84.5	8
20	84.6	84.5	84.3	83.3	82.6	81.8	81.9	82.6	83.7	85·o	85.5	86.1	36.1	86.6	86.8	86.3	86∙1	85.3	85∙0	84.6	84.3	84.1	84.1	83.5	8.
21	82.7	82.1	82.1	82.3	83.1	83.9	84.1	85.5	86.6	87.2	88.1	88·0 88·1 87·5 87·1 88·5	37.9	88.4	87.4	86.9	86.6	85.6	84.2	83.0	82.1	81.6	81.4	80.2	8,
22	82.0	83.2	83.8	84.1	84.6	84.6	85.1	86∙1	87∙1	87.0	87∙0	88∙1 [8	38.3	85.6	86.2	85.5	85.1	84.8	84.6	84.6	84.5	84∙1	83.5	83.2	8
23	82.6	82.6	81.8	81.1	8o·8	79.5	31.3	33.3	84.7	84.7	86∙3	87.5	38∙ı	88.5	87.9	86∙6	85∙1	84.2	84∙1	83.8	83∙1	82.6	81.8	82.1	83
24	8.18	81.7	81.4	81.3	81.1	80.2	30·9 8	32.3	84.5	85.6	86.6	87.1	38∙ı	88.7	88.6	88∙3	86.8	85.6	84.9	84.8	84.8	84.7	85·o	85.6	84
25	85.7	85.5	84.6	85.1	84.6	84.1	35·o 8	36.2	87.4	88∙1	87.7	88.5	88∙1	88.6	88.2	88.2	87.6	86.7	35.8	86.2	86∙1	85.9	85.7	85.7	86
26	85.6	85.6	85.9	85.5	85.2	84.7	35.5	36.2	88·1	88.8	89.3	90.4	0.6	90.6	90.1	89.6	89.4	88.7	38.2	87.4	86.9	86.6	86 ∙ o ∣	85.5	87
27	84.8	84.6	83.5	83.5	82.3	83·I	33.9 8	35.1	87·I	87.8	89.9	90.5	0.10	91.9	92·I	91.5	90.6	89.3 8	38.6 18	87.6	86.7	86·ı l	85.2	84.7	8
28	84.5	84.0	83.3	83.7	83.9	83.5	34·I 8	35.8	87.4	88.8	90.6	91.5	2.5	92.9	92.0	92·I	92.0	91.6) I·I	90·8 i	90.7	90·I	89.6	88∙9	88
29	88.5	88.2	88.4	88.4	88 ⋅ 1	88·1	38.4	38.6	89.9	90.8	92·I	93.4	14.3	94.8	95·I	95·I	94.5	93.3	92.9	92.7	92.2	92.2	92·I	91.9	91
30	91.6	91.5	91.4	91·1	91·0	90.9	01.1	8.10	92.5	93∙1	93.2	93.7	4.9	95.1	95.5	95.9	95.3	92.9	39.9	88.6	87.7	86.9	85.8	85.6	91
an	83.8	83.4	83.2	33.1	82.9	82.8	33.7	34.9	36.4	87.5	88.6	89.3	00.1	90.5	90.6	90.6	90·I	89.0	37.7	86.7	86·o	85.4	84.9	84.4	86

406. Richmond (Kew Observatory) : North Wall Screen : $h_t = 3 \cdot o$ metres.

October, 1923.

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1 2 3 4 5		85.6	185·T	184.8	184.8	184.0	82.2	182.0	18⊿ ∙ т	184.8	86∙т	186.7	187.0	187.4	187.2	187·T	187.2	187·T	186.5	18a · T	183.7	83.7	183.5	183.1	182.7	a. 87·0 85·2 80·7 81·7 79·7
6 7 8 9 10		85.9	87.5	87.7	88.1	88.3	83.7	83.7	84.5	85·7 89·8	90.2	87·0	90.5	87·3	89.8	87.2	87·1	86.5	86.3	85.9	85.7	85.6	86·0 84·6	86.0	82·0 85·9 86·7 84·5 85·4	84·2 84·4 86·0 87·9 86·8
11 12 13 14 15		78·7 76·4	78.0	77.3	75.7	75·5	73·6	76·6 74·6	77.6	79·2 77·8	79.8	82·7 82·0	83.3	81.6	81.5	82.2	82·2 84·0	82.8	81.0	79·2 79·9	78·3 78·9	77·9 78·7	77·I	77·6	83·3 79·9 78·7 76·7 77·2	79·2 79·0
16 17 18 19 20		91.0	01.7	01.7	01.0	91.0	82.0	82.1	82.2	83.2	83.6	84.7	80.0	85·7	80.1	86.5	85.0	84.8	84.2	84.2	84.1	84.0	84.1	84.4	04.7	
21 22 23 24 25																									81·7 81·3 82·8 81·0	
26 27 28 29 30		80·6 84·1 84·0 81·0 85·5	81·6 85·1 84·1 80·3 85·6	82·5 86·1 83·7 80·1 85·5	83·9 85·7 83·7 79·4 85·4	84·7 85·7 83·8 79·3 85·1	84.6 86.2 83.9 79.5 85.2	81·7 86·1 83·8 80·1 85·2	81·8 84·7 84·0 81·5 85·5	82·7 84·2 84·9 82·7 85·6	83·8 85·1 85·1 83·7 85·9	84·7 87·1 86·5 85·2 86·1	85·2 85·6 86·7 85·8 86·5	85·3 86·1 87·1 86·5 87·0	86·8 86·4 86·7 86·6 87·0	86·9 86·7 86·5 86·3	86·2 86·1 86·2 85·7 87·1	85·2 85·5 85·1 85·1 86·7	84·4 85·4 84·3 84·8 86·5	83·5 85·1 84·3 84·9 86·5	83·4 85·2 83·6 84·7 86·2	84·3 85·6 83·0 85·0 85·8	84·6 85·1 82·6 85·2 85·7	84·9 85·1 81·7 85·2 84·6	84·7 84·7 81·2 85·5 84·2	84·0 85·5 84·5 83·4 85·9
31				l	l	 -			<u> </u>		i														77.1	
Mean		82.6	82.5	82.4	82.4	82.3	82.3	82.5	82.9	83.8	84.8	85.6	86·o	86.0	85.9	85.8	85.4	84.8	84.2	83.7	83.2	83.1	82.8	82.6	82.4	83.7
G.M.T.	•••	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean

407. Richmond (Kew Observatory): North Wall Screen: ht (height of thermometer bulb above the ground) = 3.0 metres.

November, 1923.

Day.		I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mear
I 2		78∙1	78.3	78.8	79·I	78.4	77.6	77.5	77.2	77.3	78.7	80·0	a. 81·2 81·3 86·8	82.7	83.3	83.6	83·I	82.0	80.7	79.9	79.7	79.2	79.2	80·1	80·8	80·1 79·8
3 4 5		8o·6	82·7 80·2 77·8	79.7	79.3	79·2 78·2	79.4	79.0	79.6	80.5	81.3	82.1	82·9 81·8	83.2	83.7	83.3	82.3	81.4	80.7	80.2	79.8	79.2	79.0	79.0	78.7	8o·6
6 7 8 9 10		73·9 70·2 77·1	73·5 70·0 77·1	73·9 70·0 76·9	73·5 69·0 76·9	73·0 68·9 75·9	72·9 67·9 74·9	72·8 67·9 74·1	72·8 68·4 74·1	73·6 69·0 73·9	74·9 69·9 75·2	76·0 73·0 75·8	80·3 77·5 75·1 76·2 81·6	78·6 78·4 76·4	78·6 80·2 76·7	79·0 80·1 76·5	78·1 79·3 76·6	77·1 78·5	75·1 77·7 77·5	74·7 78·2 77·9	74·3 78·1 77·5	73·8 78·5 78·1	72·1 78·0 78·5	70·7 77·6 78·4	70·1 77·2 78·5	74·7 74·1 76·6
11 12 13 14		71·6 79·6 82·0	71·5 80·1 83·4	71·0 80·0 83·4	70·5 80·1 83·2	70·6 81·0 82·5	70·8 81·5 82·0	70·5 81·8 81·6	70·5 82·4 80·5	71·2 83·2 80·1	73·7 84·1 80·3	76·8 84·5 80·7	79·9 79·1 84·6 81·1 80·6	81·0 85·0 81·1	81·5 85·4 81·1	81·8 85·0 80·5	80·5 84·5 70·6	79·7 84·5 78·6	79·4 84·2 77·8	79·1 83·7 77·1	79·0 83·5 76·6	79·1 83·1 76·3	79·5 83·0 76·1	79·6 83·0 76·0	79·6 82·8 76·0	76·0 82·9 80·1
16 17 18 19 20		79·3 75·1	80·0 74·5 74·8	80·0 74·I 75·I	80·8 73·9 75·7	81·4 73·6 75·6	77·5 74·3 76·0	77·8 74·4 76·2	77·7 74·1 76·2	78·5 74·2 76·5	79·4 75·6 77·7	78·6 75·6 79·0	81·2 79·8 77·4 79·6 76·7	80·1 79·1 80·1	80·4 79·5 80·1	80·3 79·2 80·2	79·5 78·4 79·3	78·6 77·8 77·9	78·1 77·6 77·1	77·2 76·7 76·1	76·6 76·0 75·7	75·5 75·3	76·6 74·7 74·7	76·6 74·6 74·0	76·1 74·7 73·7	78·7 75·9 76·8
21 22 23 24 25		74·9 73·1 75·0	74·9 72·7 74·9	75·2 72·6 74·6	75·1 72·2 74·5	75·2 71·8 74·2	75.4 72.2 73.9	75·5 72·8 73·4	75·6 73·3 72·6	75·7 73·7 72·6	76·I 74·I 72·6	76·8 74·2 72·6	77·1 77·1 75·1 72·6 71·5	77·2 75·8 73·0	77·4 77·1 73·4	77·6 76·2 73·6	77·2 75·5 73·2	77·0 75·2 73·2	76·7 75·7 73·1	76·1 73·1	75·7 75·5 73·1	74·8 75·2 73·1	74·3 75·1	73·8 75·2 72·7	73.4 75.0 72.6	75·0 74·4 73·4
26 27 28 29 30		70·I 74·I 74·3	70·2 73·9	70·0 74·0	69·I 74·2	68·6 74·7	68·4 75·3	68·4 75·7	69·0 75·6	69·5 75·8	75·8 74·8	75·9	70·6 71·2 75·8 75·3 75·7	71·5 75·7 75·4	71·3 75·6 75·1	73·4 75·4 75·4	73·6 74·9 74·9	73·6 74·1 74·8	72·8 74·1 75·3	72·5 73·8 75·6	72·6 74·I 75·5	72·7 74·I 75·4	73·I 74·I 75·3	73·0 74·2 75·2	73·7 74·2 74·8	71·1 74·8 74·9
Mean	•••	75.9	75.9	75.7	75.6	75.2	75.3	75.2	75.4	75.9	76.7	77:5	78.2	78·9	79.1	79.0	78.5	78.1	77.5	77.1	76.7	76.5	76.2	76·o	75.8	76.8

408. Richmond (Kew Observatory): North Wall Screen: ht = 3.0 metres.

December, 1923.

G.M.T.	•••	Ι.	2.	3.	4.	5.	6.	7.	8.	9.	10.		Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
Mean	•••		·	\ 		76.3		76.5		76.6		.				78.9					77.1		76.9		76.7	
31			i	1	Į.	1	ł	l		1	1	1	75.2			t .	Į.	Į.	1	1	1	i	78.5	78.9	78.9	76·1
29 30		75·1 75·5	74·6 76·4	74·3	73·9	73·4 77·5	73·o	72·5 77·9	72·4 78·5	72·6 79·0	73.5	73·8 79·7	74·8 80·1	75·9 77·6	76·0	76·5 77·3	76·1	75·6 76·8	75·6 76·7	75·9 76·5	75·8 76·5	75·9 76·5		75·7 76·0	75·7 76·0	74·8 77·3
27 28		74·1 82·0	74·1 82·6	74·1 82·7	74·3 82·5	74·3 82·2	74·5 82·2	74·9 82·7	75·0	76·I	77·6 78·0	77·9 78·0	78·0 78·5	78·7 78·9	79·5 78·9	78·9	79.9	79·5 78·4	79·5	77.5	77:5	77.2	76.5	76·o	75.5	79.2
26		81.9	81.5	81.3	81.5	81.1	80.9	80.5	8o·6	81.0	77.7	77:3	76.7	76.6	76.6	76.3	76.2	76·I	76.0	75.7	75.6	74.9	73·9 80·1		73·5 81·2	78·0
24 25		75·6 72·6						77°1	70·I	77.0	77·1 70·4	77·5 71·8	77·6 73·0		75.2	75.3	75.4	75.3	75.6	75.8	77.1	77.6		80·6	81.6	
23		80.2	79.5	78.9		79.3	78.4	80·I	79.4	78.6	78.4	79.0	79.3	79.5	79.6	79.5	78.6	78·1 78·5	78·I	77.8	77.0	76.8	76·5 74·1	75.9	76·0	78·6 76·5
2I 22			72·5 73·6		71.7	71·8 73·7	72.2	73.7	73.9	74.2	74.7	75.0	74·1 81·1	74·2	73.7	73·8 83·0	73.7	73·5 82·9	73.5	73.6	73.6	73·7 82·4	73·6 82·1	73·6 81·0	73·5 80·5	73·4 78·7
19 20		77·0	77.4	77.5	77·4 74·4	74.6	77.1	77·5 74·4	74.3	75·3	77·5 75·4	77·8 75·5	78·1 75·4	78·1 75·7	77.8	77·4 74·7	77·0 73·8	74·2 73·7	73.3	72.6	72.2	71.9	71.7		71.7	
17 18		80.9	81.1	81.4	80.8	81.9	81.4	80.7	80.7	80.9	81.9	82.3	82.1	82.1	81.7	81.4	81.1	80.8	80.2	80.0	179.0	78·7 73·3	70.1	77.7	77.2	80·7 76·2
16		73.7	74.6	75.3	75.5	75.8	76.8	77.1	77·I	77.5	78.5	80.4	81·2 81·9	81.3	81.7	81.8	81.7	81.5	80·6	80·1	79·4 81·4	79·I	79·5		79·8 80·7	78·6 81·0
14 15		79·1 80·5	78·5 80·1	77·3 79·6	76·6 79·9	76·5 78·8	78.1	77.8	73·8 77·3	76·9	73·I	73·4 78·9	74·7 79·0	75·9 79·4	77.9	78·7 79·5	79.1	78·o	77.0	76.0		75.5			74.0	
12 13		79 5	80·1 79·5	79.3	79·I	79.1	79.3	78.8	78.6	78.6	79.3	80.6	81.1	81.9	82.1	81.6	81.5	80·7 77·8	80.2	80·1	79.6	79.7	79.6	79.6	79.2	79·9 76·9
11		80.4	80.2	80.1	80.0	80.0	80·o	80.0	80.0	80.2	80.8	80.7	81·2 81·6	81.4	81.2	81.6	81.4	80·8	80.8	80.0	80.8	80·6	80·5 79·7	80·4 70·6	80·4 70·6	80·6 80·5
10 10		70·1		69.8	75.3	71.8	74.4	72.8	72.6	73.7 74.1	75·6	77.0	76·2 78·8	79.2	79.8	80·0	8 0 ∙0	74·6 80·1	79.9						8 o ∙4	
7 8			72·3 81·9 76·6	82.1	81.6	71.7	81.4	81.5	81.2	80.6	80.7	81.2	81.1	81.2	81.0	8o·6	80.0	78.6	77.9	77:3		78.5		78.5	78·I	80·2 74·7
6			76.6	76.5	76.4	76.1	76·o	76.1	76.2	76.5	76.6	76.7	77:3	77·1 78·6	77.8	77·6 79·0			74·6 79·1		71·2 79·5			71·9 80·1		75·5 76·1
4 5				72.0		74·1 74·2	75·0 74·0		76·6 75·1	77·1	77·5 76·2		78·1 78·0	78·2		79·7 78·5	79·1	77·8 76·0	77·6 74·5	75.0	75.6	75.7	75.9	76.1	76.6	
3		73.0	73.2	78·9 72·8	79·I	72.3		72.4	72.7	72.5	73.5		76.2		78·o	77:9	80·0 77·0	75.3	74.2			72.6	72.7	72.3	72.4	74·0 76·3
I				a. 69·8	1.	a. 70·3	a. 70·7	a. 71·9		a. 74.5	a. 76·1	a. 78∙1	$\frac{a}{78.6}$	a. 79·6	a. 79·6	a. 79:3	a. 78·5	a. 78·4	78.6	79.0	79.5	79.5	79.3	79.3	78.6	75·9 78·3
					1 -	T =)					1 0		1 0		a.	a.	1 a.	a.	a.	a.	a.	a.

TEMPERATURE: ANNUAL MEANS OF HOURLY VALUES.

From readings in degrees absolute at exact hours, Greenwich Mean Time.

409. Richmond (Kew Observatory): North Wall Screen: $h_t = 3.0$ metres.

1923.

I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
a. 81·27	a. 81 ·∞	a. 80·81	a. 80∙67	80·61	a. 80·77	a. 81·25	a. 81·92	$a.82 \cdot 77$	<i>a</i> . 83⋅60	a. 84·40	a. 85·04	a. 85·53	a. 85·77	 85 · 83	a. 85·62	a. 85·25	a. 84·69	<i>a</i> . 83∙98	a. 83·22	a. 82·71	a. 82·24	а. 81 · 84	a. 81 · 52	<i>a</i> . 83∙01

TEMPERATURE: MONTHLY MEANS AND DIURNAL INEQUALITIES.

The departures from the mean of the day are adjusted for non-cyclic change.

410. Richmond (Kew Observatory): North Wall Screen: $h_t = 3 \cdot o$ metres.

1923.

i	1	Hour.	G.M.T.	.1	ı	i i	<u> </u>	1	1	1			1												
Month.	Mean.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.
L CD.	2/9 50	-003	1-07/	a. -1·14 -0·84 -1·66	1-0.40	-1.10	1-1-21	1-1.20	1 - 1 - 30	1-0.0V	1-0.07	10.77	1 1 T · 2 2	T . DD	L T . 77 4	1 T .QT	L T.72	1 1 7.78	1 1 0.601	1 0.74	0.00	A T		1 ~	0
April May	281·67 283·81	-2·06 -2·42	-2·44 -2·76	$ \begin{array}{r} -2.52 \\ -3.02 \\ -2.99 \end{array} $	-2·58 - 3·19	-2·70	-2.55 -2.62	-1·87	-0·96	-0.08 +0.17	+0.81	+1.57	+2·25	+2·97	+ 3·08 ±2·88	+3·02 +3·14	+2·96	+2.47	+1.80	+0·94	+0.07	-o·36	-o·8 ₄	-1.30	-1.77
16.	777 13	~ ~ ~ ~	ı <i>ɔ~ɔ</i>	-3·91 -3·65 -3·24	1 4 00	A OT	1 3 04	1-2 39	I T.T.	1 + 0 2 3	-1.22	+2.10	1+2.90	2 · T 5	+3.00	1-1-X-MX	Ⅰ	しよっ・クり	1_L_2.2T	土 つ・つつ	10.70		T.08	T - 92 -	0.45
1 101.	~	0 90	1-090	-1·48 -1·09 -0·80	1-21	T. 32	11-54	— 1 ·D1	I — I · 40	IO•85I	O · TO	-L0.71	1 T . 4 E	12.10	9.36	112.28	1 1 T - 70	1 1 7.30	1 0.80	1 1 0.281	10.04	~ ~ ~ 0	.		1 a 0al
Year	282.98	−1. 73	-2.01	-2.19	-2.33	-2· 4 0	-2.23	-1.76	1.10	-0.24	+0.20	+1.38	+2.02	+2.51	+2.75	+2.81	+2.60	+2.23	+1.67	+o·96	+0.30	-o.31	-o·77	-1.17	— I ·49

ABSOLUTE EXTREMES OF TEMPERATURE FOR EACH DAY.

Maximum and Minimum for the interval oh. to 24h., Greenwich Mean Time.

411. Richmond (Kew Observatory): North Wall Screen: $h_t = 3.0$ metres.

1923.

Month	Ja	n.	Fe	b.	Ma	ar.	Ap	ril	Ma	ay	Ju	ne	Ju	ly	At	ıg.	Ser	pt.	Oc	t.	No	ov.	De	ec.
Day.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.
1 2 3 4 5	a. 79·1 84·4 82·4 80·8 81·0	a. 73°4 79°1 76°9 72°1 71°1	a. 85·5 85·8 85·0 82·4 81·6	a. 83·4 83·8 80·8 72·9 70·2	a. 84·2 84·5 84·2 81·2 82·5	a. 79.3 77.5 73.0 75.5 73.5	a. 86·8 87·8 88·1 89·9 86·4	a. 78·5 79·3 78·7 77·4 80·6	a. 90·8 93·3 96·4 98·0 98·5	a. 81·6 79·7 83·9 82·4 84·2	a. 86·6 84·4 93·3 84·0 87·1	a. 81·0 81·1 76·0 80·4 78·7	a. 91·5 93·7 91·5 96·2 02·1	a. 85·5 83·5 83·6 86·0 83·6	a. 93·7 95·4 94·1 97·5 98·5	a. 83·6 86·5 86·1 82·5 81·0	a. 89·9 89·5 91·1 88·7 92·2	a. 78·8 80·1 79·2 80·0 80·8	a. 88·1 87·7 83·3 85·2 83·1	a. 84·7 82·6 78·3 77·9 74·7	a. 82·7 83·7 87·3 83·8 83·2	a. 76·3 77·0 80·8 78·7 77·5	a. 79·7 81·8 78·1 81·1 78·6	a. 69·6 71·7 71·5 72·0 73·6
6 7 8 9 10	79·1 83·5 84·1 82·1 80·5	74·1 74·5 76·0 74·4 76·0	79·5 84·0 84·2 82·5 81·5	76·3 76·3 76·2 75·0 79·9	84·1 83·4 81·4 78·4 80·1	77·0 77·6 76·5 75·2 75·6	81·5 87·4 82·6 78·5 85·5	79·2 79·1 78·4 73·9 72·9	94·0 90·2 89·8 89·3 84·7	85·7 84·5 82·6 79·1 77·4	87·7 90·3 90·1 90·6 92·3	82·6 82·9 82·5 85·4 84·1	03·2 04·3 99·7 02·1 01·2	88·8 90·3 89·4 85·8 90·0	97·6 98·8 01·2 02·4 98·0	85·9 85·8 87·4 85·5 87·9	94·4 94·6 93·0 95·4 94·1	80·5 83·5 78·7 78·1 85·1	87·6 87·6 87·6 91·1 89·5	81·7 80·5 83·6 84·5 84·4	80·7 79·1 80·6 78·6 81·7	74·1 70·1 67·8 73·6 76·8	77·8 80·5 82·2 78·1 80·5	70·9 71·5 77·0 71·1 69·3
11 12 13 14 15	79·3 79·5 77·5 84·0 79·8	73·4 73·4 71·4 76·3 75·0	83·5 81·7 79·6 78·6 80·6	78·8 74·4 77·9 76·0 75·0	79·3 81·2 80·0 80·0 78·3	75·6 72·2 77·7 76·7 76·2	89·4 90·9 86·5 84·5 85·6	82·3 82·9 79·5 76·9 75·9	84·8 82·6 84·8 86·1 85·5	77·2 74·7 77·3 77·9 77·8	89·7 89·9 93·3 89·3 87·8	81·9 79·1 85·1 83·6 82·5	04 4 05 3 05 0 99 8 98 5	89·9 92·1 93·0 91·5 89·9	96·7 98·7 00·6 98·8 93·4	86·9 84·4 85·8 90·4 84·6	94·0 93·9 95·6 93·4 88·9	85·0 83·1 82·5 86·1 81·2	86·1 87·6 85·4 84·0 84·8	83·3 79·9 78·7 76·0 73·6	80·7 81·9 85·5 83·6 83·0	70·6 70·1 79·4 75·7 72·9	81·7 82·1 82·3 79·8 80·5	79·9 79·5 78·2 72·7 73·9
16 17 18 19 20	81·2 74·2 81·0 81·4 81·8	74·2 69·4 73·1 73·1 74·4	82·9 82·0 81·4 76·7 75·6	77·2 76·5 74·9 74·4 73·6	80·9 82·6 82·3 82·3 83·3	77·9 77·7 76·8 76·0 73·1	85·0 83·5 84·4 83·2 85·6	78·8 77·9 78·4 78·6 77·8	82·9 84·6 83·8 86·2 88·3	76·6 76·6 77·8 78·1 81·8	85·4 88·0 88·8 88·6 86·7	82·0 79·8 78·5 83·7 82·7	96·0 93·4 93·4 93·0 00·5	88·9 86·0 86·3 84·1 89·5	92·4 91·9 91·6 92·6 93·7	82·0 86·3 85·7 84·4 86·5	88·7 89·6 87·4 87·8 87·2	78·6 78·3 81·2 79·6 81·6	85·6 86·1 86·9 90·9 86·6	76·2 81·2 78·9 81·6 81·5	82·2 81·5 79·5 80·3 77·6	76·7 76·1 73·1 73·6 71·2	81·9 83·0 82·5 78·3 75·8	73·6 78·6 77·2 72·9 71·5
21 22 23 24 25	78·6 83·3 81·3 81·0 83·5	72·1 76·5 73·0 73·0 76·4	81·4 81·3 81·5 81·4 83·3	73·8 73·1 75·1 77·4 77·6	85·2 82·4 81·0 86·0 87·9	76·0 76·0 76·8 77·5 77·2	84·3 86·1 82·9 84·0 84·8	76·5 76·9 73·6 76·2 75·4	88·2 90·7 88·2 88·2 87·2	81·7 80·7 79·6 76·4 77·8	91·6 94·2 97·0 93·8 89·6	81·5 85·9 84·1 88·9 83·0	99·4 97·2 95·6 97·1 93·7	88·1 88·1 86·5 86·5 87·4	94·1 93·0 92·1 91·1 90·7	85·9 85·1 82·2 84·7 82·6	88·8 88·6 88·6 89·2 89·2	80·2 80·1 79·1 80·1 84·0	87·7 86·2 87·1 87·1 87·1	81·0 80·8 81·2 79·7 80·8	78·3 77·6 77·1 75·1 73·0	74·9 73·4 71·8 72·2 69·5	75·1 83·4 80·5 78·6 81·6	71·5 73·5 75·8 73·4 69·7
26 27 28 29 30	80·6 81·9 82·8 82·5 85·3	77·0 77·8 77·3 78·9 80·8	85·6 83·5 84·1 —	79·9 79·3 79·0 —	90·3 92·9 87·6 86·1 86·6	79·8 77·9 81·7 79·5 78·7	86·4 85·6 86·6 86·8 88·4	78·5 76·5 77·5 79·8 83·0	86·3 85·4 86·5 83·2 88·9	77·3 79·1 80·2 80·0 79·8	89·0 92·2 92·8 97·1 92·9	81·9 80·6 83·8 83·2 82·9	92·6 93·0 93·4 93·7 94·5	85·3 82·3 86·5 84·7 87·9	94·4 90·5 90·5 88·6 89·8	86·7 84·5 83·6 82·3 82·0	90·7 92·5 92·9 95·2 95·9	84·7 81·9 83·1 88·0 85·5	87·2 87·2 87·2 86·8 87·1	80·4 83·9 81·2 79·2 84·2	72·I 73·7 75·6 77·I	68·5 68·3 73·7 74·2 71·5	82·0 81·2 82·8 76·5 80·3	73·5 73·5 75·5 72·0 75·5
31 Mean	85·0 81·4	75·0	82.0	<u>76·7</u>	87·5 83·5	80·5 76·9			85·2 88·1	80·1 79·7	90.1	82.3	91.7	8 ₄ · ₇	90·7 94·6	78·9	91.4	81.6	86·5 86·8	76·6 80·4	 79·8	73.7	79·0 80·2	74.4

Richmond (Kew Observatory): North Wall Screen: ht (height of thermometer bulbs above the ground) = 3.0 metres.

2. Richmon	iu (ik	, w			- • • •																				lanuar	y, 1923.
Day.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.
1 2 3 4 5	% 88 95 87 93 99	% 88 94 87 95 94	% 87 90 92 92 97	% 87 93 89 97 99	% 93 97 86 95 96	% 91 94 86 99 99	% 95 96 86 97 97	% 95 99 87 95 96	% 96 96 86 91 96	% 96 95 84 91 95	% 93 91 79 85 94	% 91 90 73 85 89	% 88 89 73 79 81	% 85 90 75 73 78	% 85 90 79 77 79	% 87 91 81 83 87	% 88 92 83 85 91	% 90 92 87 91 93	% 91 92 90 93	% 90 91 91 91 94	% 92 84 89 99	% 93 87 93 91 89	% 95 89 94 99 86	% 95 89 93 95 79	% 90·6 92·0 85·3 90·4 91·6	mb. 7·1 10·4 8·6 7·2 7·3
6 7 8 9	83 97 92 95 83	80 97 85 95 82	79 95 88 99 79	77 95 91 97 79	77 97 91 95 81	80 95 91 93 84	87 94 92 94 84	85 94 92 86 79	87 94 89 86 78	80 95 87 92 75	78 97 87 92 77	75 97 87 79 73	71 96 93 71 68	69 96 89 67 69	75 95 86 64 68	83 93 80 69 75	87 95 75 73 76	89 95 75 83 7 ⁶	89 95 81 84 82	93 93 85 80 87	93 96 88 82 86	97 96 92 81 85	96 95 92 79 83	99 93 93 83 84	83·3 95·3 87·5 84·3 78·8	6·5 9·8 9·8 7·5 6·7
11 12 13 14	83 85 95 91 83	85 82 93 89 83	89 82 95 94 87	89 83 95 95 88	88 83 97 97 89	93 88 99 95 88	95 90 99 94 77	93 87 99 95 77	93 91 97 97 77	85 89 99 96 77	79 83 97 91 79	75 80 95 84 78	75 76 96 84 76	71 76 96 86 74	70 77 96 85 76	73 80 96 83 77	75 83 98 73 79	79 87 97 69 78	78 90 93 65 81	79 89 90 67 84	79 88 91 73 84	81 93 89 83 88	83 95 89 83 89	87 96 89 83 88	82·3 85·3 95·1 85·6 81·4	6·3 6·7 6·1 8·7 6·8
16 17 18 19 20	91 91 94 93 92	93 97 94 97 92	93 91 94 99 93	91 96 94 97 80	94 96 93 99 74	91 99 93 97 74	94 99 95 99 72	94 99 91 100 71	95 99 95 99 70	89 99 97 99 71	84 96 99 97 76	75 99 91 89 69	75 99 83 86 72	75 99 76 86 66	75 99 73 87 57	74 99 80 90 56	74 99 85 90 60	73 99 85 86 59	75 99 88 86 63	73 96 89 84 61	79 94 89 86 63	84 95 88 92 64	88 91 88 93 67	89 91 91 96 65	84·0 96·7 89·4 92·7 70·9	7·9 5·2 7·1 7·8 6·3
21 22 23 24 25	65 90 67 79 93	65 93 75 81 93	67 91 77 81 91	65 94 78 83 91	63 95 83 83 89	68 95 83 85 90	71 95 83 87 93	71 97 80 87 95	73 95 80 87 93	75 95 73 87 89	76 84 69 87 85	73 77 62 86 83	74 73 56 85 80	74 70 55 85 77	77 70 57 85 72	79 69 60 87 75	77 72 67 89 69	84 78 75 87 71	84 81 79 86 71	88 79 83 84 76	87 79 77 86 83	89 81 79 85 85	93 78 79 91 89	91 77 77 93 88	75·7 84·0 73·1 85·3 84·3	5·5 8·5 5·6 7·2 8·2
26 27 28 29 30	89 79 97 87 93	88 81 97 90 92	89 83 95 93 93	91 78 94 93 97	88 79 91 93 97	84 83 91 93 96	86 87 93 91 93	8 6 89 91 94 93	87 90 91 90 92	85 89 86 85 92	85 89 80 85 87	80 82 79 87 82	80 79 75 89 82	77 78 76 92 77	75 75 76 89 81	73 78 78 89 83	71 80 76 88 86	75 84 76 87 87	73 86 80 85 90	79 87 79 85 89	76 91 79 89 89	81 94 80 88 89	80 93 81 89 92	80 94 85 92 93	81·7 84·2 84·6 89·2 89·3	7·7 8·2 8·6 9·4 10·9
31	92	87	87	87	89	91	91	91	91	90	89	83	86	74	77	84	82	85	8o	82	81	73	79	83	85.0	10.8
Mean	88.4	88.5	89.1	89 · 1	89.3	89.9	90 · 5	89.9	89·7	88 · 3	86.1	82.2	8o·3					83·0			<u> </u>		87·7 mb.		85·8 mb.	7.8
Pressure* 413. Richm	7·3	7·3				7.3					8·1 n: l			8·1	!	ļ		7.8	7.7	7.5	7.5			Fe	bruar	y, 1923
1 2 3 4 5	% 86 91 85 93 99	`		% 87 93 83 93 99		% 87 93 84 94 99	% 87 93 86 94 99		% 87 91 80 89	% 85 91 84 75 97	% 87 87 75 72 97	% 87 85 71 71 83	% 87 85 68 64 75	% 88 87 71 63 75	% 92 89 68 63 74	% 89 85 71 63 80	% 83 85 76 73 82	% 83 85 79 74 87	% 84 85 79 79 88	% 84 88 84 92 87	% 84 89 92 90 87	% 87 89 92 93 90	% 89 87 92 99	% 91 85 93 93 91	% 86·5 89·2 81·0 83·3 90·4	mb. 11·7 12·1 10·2 8·1 6·7
6 7 8 9	91 97 87 99 83	88 93 93 97 85	85 92 93 95 85	87 93 92 95 85	85 97 91 99 84	85 94 91 97 83	81 90 92 95 80	83 86 89 99 87	77 85 88 95 89	75 87 88 95 86	77 93 88 94 86	75 94 97 91 86	75 93 85 84 89	75 88 86 81 93	76 88 82 78 94	76 87 85 76 91	79 96 86 80 92	81 93 89 79 89	85 92 91 78 86	88 95 90 81 89	93 92 97 81 91	93 90 95 79 89	93 89 95 79 92	94 86 95 83 87	83·2 91·4 90·0 88·2 87·5	7·1 9·5 9·9 8·3 9·0
11 12 13 14 15	87 91 95 88 100	84 93 97 89 100	79 95 97 93 100	85 99 94 93 100	85 99 97 93 10 0	87 95 97 95 100	87 99 97 100 100	89 99 95 97 100	87 99 95 95 100	84 100 90 95 100	78 99 87 99 97	78 89 90 99	76 76 85 99 89	72 71 82 99 86	71 75 86 97 85	74 78 85 99 86	78 80 85 97 86	81 82 85 100 89	85 83 89 100 90	87 91 87 100 90	87 91 87 99 86	90 91 87 100 91	90 94 91 99 93	91 94 85 100 91	82·9 90·1 90·4 96·6 94·2	8·7 8·2 8·3 8·0 8·1
16 17 18 19 20	93 89 90 99 91	95 93 90 100 91	93 92 91 100 89	94 89 95 100 88	93 89 100 100 89	97 91 100 100 89	97 91 100 100 87	99 93 99 100 81	95 87 100 99 82	93 82 97 97 81	84 75 95 87 77	76 72 95 83 77	76 73 99 87 81	78 75 94 86 78	81 81 91 85 79	83 81 91 89 77	89 83 86 89 82	93 89 85 89 79	90 88 89 89 81	91 91 90 89 83	85 88 94 88 81	84 89 95 93 81	85 89 99 97 83	91 86 97 97 85	89·0 85·8 94·0 93·5 83·3	9·1 8·2 7·8 6·8 5·7
21 22 23 24 25	87 88 89 97 93	91 91 89 94 93	89 95 89 97 97	91 93 88 94 97	97 96 89 95 99	97 96 91 91 95	93 99 89 91 97	97 95 88 91 100	92 91 87 90 97	94 85 84 85 99	87 80 82 86 96	83 75 80 87 92	82 78 75 91 88	89 75 69 91 86	85 82 67 87 82	76 85 65 94 79	78 88 73 91 76	88 90 83 91 73	87 86 87 91 80	87 81 91 92 88	88 79 91 90 89	89 83 97 90 91	89 88 99 90 94	89 89 95 94 95	88·5 87·0 84·7 91·3 90·6	7·1 7·2 7·4 9·1 9·2
26 27 28	95 77 83	96 81 79	91 82 81	89 79 77	91 81 73	93 80 73	96 79 72	96 76 78	96 71 75	99 69 70	91 70 67	73 71 74	65 68 69	64 69 81	63 70 75	65 68 69	66 71 78	70 74 75 84·1	79 78 87	71 83 90	70 80 87 87.7	83 81 89	70 81 87	72 79 81 89·6	81·5 75·6 77·9	9·3 8·3 8·5
Mean Vapour	<u> </u>		91·4 mb.	mb.	mb.	1	<u> </u>		89·8	i	85·5	83·3	80·8	1	1	i	1	mb.	mb.	mb	. mb	mb.	mb.	mb.	mb.	<u> </u>
Pressure*	8.4			8.3	8.2				8.3		8.7		8.7					8.5	8.4	8.3	8.2	8.2	8.3	8.3	8.4‡	<u> </u>
Hour G.M.T.	1.	2.	3.	4.	5.	6.	7,	8.	9.	IO.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	

^{*} Computed from the mean temperatures and mean relative humidities.

[†] Mean of the column.

414. Richmond (Kew Observatory): North Wall Screen: ht (height of thermometer bulbs above the ground) = 3.0 metres.

	`				•,																				Marc	h, 1923.
Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
1 2 3 4 5	% 86 79 92 91 93	% 81 76 99 88 100	% 83 72 99 89 99	% 82 76 97 89 97	% 81 74 99 91 99	% 80 81 97 93 99	97 93 100	% 72 81 99 92 100	% 71 75 97 89 97	% 69 69 97 89 87	% 66 64 89 87 80	% 64 60 78 85 81	% 61 59 70 79 78	% 59 60 64 77 73	% 56 59 61 75 73	% 57 63 55 76 83	% 68 67 60 76 83	% 73 81 67 82 85	% 81 81 75 86 89	% 86 83 86 88 93	% 91 86 89 85 91	93 89 93 88 93	% 96 89 93 88 95	% 93 92 91 95 97	% 75·8 75·0 85·2 86·2 90·2	mb. 8·3 8·1 7·5 7·5 8·0
6 7 8 9	99 93 85 93 82	99 93 86 89 7 9	97 93 93 83 79	99 94 90 84 80	100 91 90 77 84	99 94 95 79 90	99 94 94 77 90	99 90 93 77 93	97 85 91 79 93	95 81 94 81 92	84 93 91 83 91	73 85 83 87 89	73 72 75 85 83	71 96 75 88 79	69 92 65 87 81	78 91 80 84 73	87 84 83 80 76	91 87 85 79 75	92 93 85 81 82	83 89 87 85 83	86 83 85 85 82	91 85 87 86 85	93 91 89 82 85	93 86 92 83 81	89·5 89·1 86·3 83·3	8·9 9·0 8·0 6·5 7·0
11 12 13 14 15	83 84 91 92 83	81 89 93 93 86	81 96 95 95 86	81 93 94 91 90	85 93 99 91 90	89 97 99 91 92	87 91 99 91 92	85 93 97 88 95	85 85 97 91 92	83 75 94 87 91	77 69 91 86 89	75 65 89 79 85	71 64 86 67 89	68 64 87 66 85	66 63 89 72 85	66 66 85 69 85	70 69 91 72 91	74 71 90 65 92	75 71 90 69 94	77 80 89 73 94	80 87 85 77 93	79 89 87 81 93	81 88 81 91	82 91 91 83 88	78·3 80·5 91·5 81·4 89·5	6·6 6·6 8·6 7·1 7·3
16 17 18 19 20	94 86 85 85 99	93 89 88 89 99	93 86 87 89 97	93 88 88 89 97	93 93 89 91 95	95 93 89 91 97	93 94 89 91 99	91 91 85 85 100	89 89 82 83 97	89 85 78 79 97	84 82 74 77 95	79 79 68 68 68 91	81 76 63 65 86	82 71 64 64 79	82 69 60 64 72	86 71 62 68 73	86 75 66 74 68	86 72 67 77 72	89 76 73 76 81	86 80 77 82 85	85 82 79 83 85	86 83 83 85 89	87 84 87 89 86	87 85 87 91 91	87·9 82·5 77·9 80·5 88·7	8·2 8·1 7·3 7·4 7·9
21 22 23 24 25	93 100 100 93 90	91 100 100 91 97	93 99 100 93 94	91 100 100 91 97	95 100 100 93 94	91 99 100 91 95	94 100 99 95 100	95 99 100 94 94	91 94 100 86 88	86 95 99 79 85	86 90 99 81 85	81 87 95 76 81	75 85 86 66 80	71 83 93 64 80	68 82 85 63 77	77 82 81 64 75	83 85 91 63 72	84 86 91 73 69	87 89 91 78 81	93 91 91 86 93	97 93 91 87 91	95 91 97 96	97 93 99 96	99 99 93 93 96	88·2 92·9 94·7 83·2 87·7	9·2 8·6 9·0 8·7 10·7
26 27 28 29 30	99 96 89 84 99	100 100 89 84 95	99 100 91 87 97	100 100 90 85 97	99 90 87	100 100 92 87 100	100 99 89 87 94	93 85 85 92	99 80 75 80 82	95 72 70 75 76	81 64 62 77 67	73 55 62 80 61	73 53 61 76 57	73 53 61 73 56	78 53 61 73 63	73 49 65 78 57	77 50 69 82 59	78 56 79 88 59	83 62 84 85 65	89 69 83 93 70	99 73 82 95 77	100 88 83 95 73	99 91 82 95 70	99 90 84 94 74	90·3 77·1 78·4 84·2 76·9	12·2 11·5 10·3 9·8 9·2
31	71	72	77	81	86	85	84	79	72	73	67	62	61	64	65	67	63	71	75	80	85	85	89	86	74.7	9.2
Mean	90.0	90·6	91.0	91.1	91.7	92.9	92.5	91.0	87.5	84 · 4	81 · o	76.7	72·8	72.3	71 · 2	72.2	74.6	77.6	81 · 3	84.7	86•1	88.7	89·6	89.9	84.2	8.5
Vapour Pressure*	mb. 8·2		mb. 8•1				mb. 8·o	mb. 8·2	mb. 8·3	mb. 8·5	mb. 8·7			mb. 8·7					mb. 8·5	mb. 8∙6	mb. 8·4	mb. 8·5	mb. 8·5	mb. 8·4	mb. 8·4‡	
415. Richmo	ond (Kew	/ Ob:	serva	atory	') : 1	Nort.	h W	all S	cree	n : h	nt = 3	·o n	netre	s.										Apr	il, 1923.
1 2 3 4 5	% 91 95 95 95 95	% 94 97 97 97 77	% 97 95 94 97 77	% 95 94 95 97 75	% 97 95 93 95 72	% 97 94 91 95 72	% 97 93 94 94 70	% 94 92 89 81 69	% 92 88 83 68 69	% 87 87 83 76 52 65	% 85 79 71 46 63	% 77 74 67 42 62	% 63 63 65 44 58	% 65 59 56 41 53	% 71 55 53 41 51	% 7° 58 54 5° 57	% 73 63 53 55 72	% 77 69 53 65 76	% 77 78 59 68 76	% 77 82 71 72 74	% 82 86 68 76 72	% 85 89 80 81 75	% 91 92 87 84 75	% 91 93 93 84 76	% 84·3 81·9 76·5 71·9 69·5	mb. 9.7 9.7 9.2 9.0 8.5
6 7 8 9	82 85 94 66 93	84 87 93 73 93	81 89 84 77 93	85 89 79 76 93	87 87 77 75 95	85 90 77 73 93	86 91 79 68 91	85 91 75 59 89	82 87 68 58 78	77 81 67 49 63	79 77 64 56 57	79 69 67 54 55	77 66 68 56 52	73 59 68 59 53	73 53 63 56 57	73 53 57 57 60	78 63 58 60 63	77 65 57 65 64	80 72 61 72 74	80 80 66 79 86	81 83 66 82 89	82 89 64 88 83	83 92 65 91 86	83 95 63 93 77	80·4 78·6 70·7 67·8 76·9	8·3 9·2 7·3 5·4 7·6
11 12 13 14 15	82 88 92 86 93	92 93 95 86 99	93 93 93 86 95	95 96 91 88 92	96 93 93 89 99	96 92 92 85 97	95 88 89 80 90	95 83 86 75 83	90 82 75 69 76	82 88 68 69 70	80 80 64 68 61	75 68 65 67 62	72 69 60 61 60	74 79 61 76 63	89 87 65 65 69	88 89 67 71 70	92 88 71 73 70	82 88 82 66 88	83 87 89 73 84	79 91 87 81 84	78 92 83 82 87	72 92 84 87 85	80 88 81 93 91	85 88 85 97 93	85.0 86.7 80.0 77.8 81.8	12·3 9·9 8·1 8·8
16 17 18 19 20	95 77 82 77 82	94 77 78 78 78 89	93 74 76 77 93	99 75 79 76 91	97 74 75 77 94	92 73 72 75 89	91 67 69 73 86	88 68 67 74 83	86 66 65 70 81	76 63 67 71 79	71 59 68 74 83	73 60 65 75 76	71 57 62 76 69	73 59 59 73 68	70 57 59 70 65	67 59 60 69 64	69 64 59 73 60	70 69 64 74 62	76 71 68 76 58	84 76 71 78 59	80 74 75 79 67	74 76 77 77 77	79 79 76 76 76 78	76 79 77 79 80	81·4 68·8 69·6 74·8 76·3	9·1 7·1 7·3 7·9 8·2
21 22 23 24 25	81 75 82 76 84	87 74 84 81 84	83 76 88 83 83	79 78 89 85 82	78 81 91 83 85	75 80 89 79 77	73 78 83 72 82	71 79 76 61 85	66 72 60 58 83	63 64 59 53 83	59 57 57 49 86	57 54 59 44 87	57 49 56 45 91	55 47 57 43 89	54 49 54 43 87	57 47 57 43 90	62 47 57 42 90	69 51 58 45 89	76 57 57 54 89	79 61 62 69 82	80 69 65 75 88	79 71 75 75 87	75 77 81 77 89	77 85 77 78 91	70·5 65·6 69·9 63·0 85·7	7·2 7·5 6·5 6·1 9·5
26 27 28 29 30	89 81 88 86 89	91 87 91 84 88	92 84 93 84 87	93 88 94 83 87	93 88 93 87 89	95 85 91 92 89	92 79 85 91 83	85 74 80 89 81	79 67 64 85 82	77 61 55 83 82	71 57 51 78 82	68 54 46 81 78	81 52 46 70 79	76 48 52 69 73	76 46 62 72 73	73 47 73 73 72	60 44 66 75 75	65 53 71 73 77	73 62 63 77 82	83 61 75 86 85	72 67 74 89 83	71 73 78 90 82	79 81 83 90 82	81 87 86 90 83	80·0 67·6 73·4 82·3 81·9	9·2 7·3 8·1 10·4 11·8
Mean	85.3	87.5	8 ₇ ·0	87.3	87 · 6	86 • 1	83.6	80 · 2	75·o	70.4	67.7	65.2	63·2	62 · 7	62.8	64.2							82.7		76·o	8 · 6†
Vapour Pressure*	mb. 8·3	mb. 8·2		mb. 8·2		mb. 8·1	mb. 8·3		mb. 8·4	mb. 8·3	mb. 8·4	mb. 8·4	mb. 8·6			mb. 8·7		mb. 8·7		mb. 8·7		mb. 8·5	mb. 8·5	mb. 8·4	mb. 8·4‡	
Hour G.M.T.	ī.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	_

 $^{\ ^{\}bullet}$ Computed from the mean temperature and mean relative humidity.

416. Richmond (Kew Observatory): North Wall Screen: ht (height of thermometer bulbs above the ground) = $3 \cdot 0$ metres.

	•																								Ma	y, 1923.
Day.	ı.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.
1 2 3 4 5	% 83 95 97 91 86	% 83 96 97 95 89	% 84 99 93 95 92	% .84 .99 .95 .97 .96	% 85 97 96 96 95	% 89 95 97 96 95	% 85 92 93 84 84	% 79 87 89 74 78	% 74 74 80 64 74	% 72 73 74 57 77	% 71 69 67 54 70	% 69 64 62 49 61	% 71 62 58 47 53	% 73 59 55 47 47	% 70 56 47 49 49	% 66 57 50 49 53	% 66 57 52 53 46	% 65 59 49 53 46	% 73 61 56 57 47	% 75 77 69 69 57	% 80 79 77 75 64	% 87 82 79 79 69	% 92 85 88 82 78	% 93 89 92 85 82	% 77·7 77·7 75·5 70·8 70·4	mb. 11·9 12·6 14·2 14·5 14·6
6 7 8 9	87 75 83 65 81	89 76 83 65 81	91 80 88 70 81	91 78 87 72 83	87 82 86 73 84	88 80 82 71 81	82 75 79 69 76	82 69 79 66 77	76 67 75 61 81	65 63 67 59 81	55 61 60 59 79	53 60 57 55 68	50 60 54 53 65	52 60 51 54 58	49 58 51 53 48	45 59 54 51 48	47 63 54 57 41	51 66 53 59 43	54 67 52 63 49	61 69 55 69 56	65 69 57 74 66	69 73 52 73 70	75 81 60 79 68	72 85 66 85 79	68·4 69·5 66·4 64·4 68·6	12·2 11·0 9·8 8·6 7·2
11 12 13 14 15	83 85 89 85 77	83 84 87 87 78	85 82 88 91 79	86 87 91 91 81	85 87 93 93 82	79 84 95 90 79	75 77 94 83 76	67 72 88 73 75	58 63 82 68 73	59 60 76 61 65	56 56 70 56 75	55 74 53 51 67	55 84 51 49 87	49 68 52 45 78	60 64 48 48 81	63 81 50 46 81	53 78 51 42 80	64 60 53 47 70	80 61 53 52 81	68 64 64 65 85	65 77 69 68 87	78 76 70 74 89	79 81 83 73 91	81 85 81 76 94	69·4 74·5 72·2 67·4 79·3	7·5 6·9 7·5 7·6 8·7
16 17 18 19 20	91 81 77 86 81	93 81 77 86 81	91 83 80 88 81	93 85 80 88 82	92 85 77 87 82	89 84 77 83 81	85 85 73 78 75	80 77 63 75 74	80 62 57 76 70	71 60 60 74 61	57 61 57 72 63	76 52 56 68 65	58 55 57 63 65	83 56 55 68 59	59 47 57 66 67	58 50 59 68 69	58 52 57 67 70	62 56 62 68 74	64 51 68 68 73	71 59 71 70 76	76 64 75 75 78	76 67 77 78 84	81 70 82 81 87	82 76 83 83 89	76·3 66·7 68·1 75·7 74·3	7·3 6·8 7·2 9·2 9·9
21 22 23 24 25	91 91 88 94 90	92 92 89 97 93	91 91 89 99 86	90 88 87 99 86	90 87 85 95 85	87 86 84 88 87	83 87 81 83 86	79 89 74 70 84	73 87 71 63 78	69 80 73 62 75	64 71 88 58 62	61 63 77 54 56	61 65 89 52 52	62 59 83 50 59	57 56 93 51	53 57 92 53 62	55 57 92 51 65	55 61 91 51 64	61 66 91 55 68	67 74 92 65 72	70 78 91 79 69	76 85 89 82 71	83 91 90 85 78	87 89 90 87 83	73·3 77·0 86·2 71·8 73·5	10·5 11·2 11·2 8·3 8·5
26 27 28 29 30	85 86 89 95 100	90 87 93 94 100	91 84 95 95 97	92 90 95 95 99	90 90 95 99 95	88 91 95 99	86 81 89 96 99	76 77 92 88 96	63 68 89 92 93	63 64 95 95 86	57 62 79 93 77	52 64 78 92 74	55 64 74 91 65	53 57 82 91 62	53 58 82 88 62	54 63 83 92 72	57 67 64 89 75	59 70 65 89 68	61 80 89 93 75	65 79 95 92 75	67 81 93 95 77	75 84 92 97 77	78 86 92 97 81	81 87 93 97 85	70·5 75·7 86·9 93·4 83·1	8·2 8·5 10·3 10·5
31	84	85	89	86	87	86	86	83	8o	79	77	75	73	70	67	67	65	70	72	75	78	77	83	83	78.3	9.0
Mean	86·2	87.2	88·o	88.8	88.5	87.3	83 · 1	7 ⁸ ·5	73 · 3	70.2	66•3	63.3	62 · 5	1		<u> </u>	1							84.5	74.3	9.7
Vapour Pressure.*	mb. 9·4	l	mb. 9·3	mb.	mb. 9·2	mb. 9°4	mb. 9·6	mb. 9·6	9·5	mb. 9·5	mb. 9.5		mb. 9·6	mb. 9.5		mb. 9·6			mb. 9·4		mb. 9·5		mb. 9.5	9.5	mb. 9·5‡	
417. Richm	ond	(Kev	v Ob	Berva	atory):1	Nort.	h W	all S	cree	n : h		·o m	etre												, 1923.
1 2 3 4 5	% 83 88 95 80 80	% 85 88 97 89 80	% 86 88 95 85 83	% 86 89 97 84 85	% 91 91 95 81 82	% 92 89 93 77 83	% 88 88 89 72 80	% 83 84 82 74 77	% 85 83 77 68 74	% 81 87 73 62 76	% 81 82 62 58 76	% 78 77 49 61 73	% 76 78 53 60 67	% 77 77 49 59 66	% 72 75 45 58 58	% 76 73 51 59 57	% 78 74 55 60 54	% 79 72 53 64 53	% 79 75 63 66 59	% 82 75 68 70 65	% 83 76 72 69 71	% 82 76 73 72 71	% 85 77 74 77 70	% 87 85 78 77 81	% 82·2 81·2 72·5 70·1 71·6	mb. 10·3 9·7 10·3 8·2 8·7
6 7 8 9 10	87 87 85 83 88	90 89 86 83 88	85 88 87 87 89	82 87 92 87 89	83 89 88 89 88	78 87 86 88 85	77 84 84 87 82	76 78 71 86 79	85 71 65 85 83	81 67 64 82 84	77 65 62 84 84	69 67 60 84 81	68 65 57 83 60	83 63 59 83 47	82 63 57 82 47	87 65 63 80 47	87 67 65 79 46	92 65 68 80 48	92 69 70 80 57	93 72 71 83 61	93 79 74 83 65	93 78 78 87 67	93 79 79 86 74	86 83 82 87 77	84·0 75·3 73·1 84·0 71·7	11·1 11·6 11·1 14·1 12·5
11 12 13 14 15	81 80 94 66 71	81 89 93 69 70	86 87 93 67 75	87 86 93 70 76	86 85 89 74 75	81 78 91 77 68	75 73 85 75 72	59 70 79 72 71	58 65 74 68 66	60 60 77 61 62	58 57 67 63 66	63 54 53 60 63	55 50 51 59 65	48 54 50 60 80	47 55 46 55 86	47 60 47 56 87	48 61 55 55 88	52 69 56 55 87	53 77 56 59 89	57 81 61 63 91	63 87 59 61 91	70 93 61 63 93	71 93 63 67 94	79 93 67 73 81	65·2 72·9 69·7 64·4 77·6	9·8 10·2 12·5 9·7 11·2
16 17 18 19 20	81 75 93 87 72	71 78 91 87 76	72 81 97 88 78	72 83 90 90 80	75 78 91 93 82	75 76 91 92 82	87 70 85 94 79	83 61 79 93 78	78 59 74 93 76	83 59 69 92 73	81 57 68 79 71	69 58 63 75 59	68 55 60 68 59	66 55 65 62 60	63 53 59 59 57	61 51 68 59 59	59 47 65 59 63	60 51 70 55 65	65 53 72 59 64	67 68 75 62 68	69 75 79 63 76	73 81 86 66 73	71 87 87 66 76	74 91 88 70 75	71·9 66·4 77·7 75·8 70·7	9·2 8·5 10·6 11·5 9·5
21 22 23 24 25	77 90 82 70 69	81 91 87 69 72	82 93 87 75 76	85 91 87 73 75	84 88 90 73 76	79 82 82 67 74	73 78 80 66 69	69 76 70 67 71	65 70 69 65 70	65 73 67 57 69	63 67 61 55 74	63 61 57 52 69	60 57 54 55 77	59 59 51 56 82	58 58 48 49 81	66 54 51 53 85	71 59 51 56 87	72 58 49 61 82	78 57 49 63 86	81 61 55 62 89	83 67 66 65 84	86 70 67 65 96	87 76 67 67 92	89 80 66 68 93	73·7 71·7 66·7 62·8 78·5	11·8 13·7 13·9 12·9
26 27 28 29 30	90 93 90 88 92	91 96 89 85 95	95 95 90 86 97	93 96 91 87 95	92 99 90 88 91	88 93 90 86 84	86 90 90 85 77	80 86 71 78 69	75 79 61 70 64	73 73 56 66 61	73 75 52 63 56	76 77 51 58 56	87 68 49 51 56	83 62 49 49 53	77 62 52 47 56	72 63 55 44 59	73 67 58 45 61	73 53 62 44 64	78 51 62 57 65	80 55 66 71 66	85 68 73 75 69	92 76 79 80 72	92 82 81 89 74	97 85 90 90 79	83·3 77·1 70·6 70·1 71·5	11·7 12·0 12·4 13·2 12·7
	83.2	84.5	85.8	85 · 9	85.9	83 · 1	80.7	75.7	72.5	70.4	67.9	ļ	ı		l	1	1	1	1		ı		l		73.5	11.2
Mean		<u> </u>			ι															. 1			,			-
Vapour	mb.	mb.	mb. 10·7	mb. 10·6	mb. 10·8	mb. 10•7	mb. 11·2	mb.	mb. 11·3	mb. 11•2	mb. 11·3	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb 11⋅4	mb.	mb.	mb.	mb.	mb. 11·1‡	

Computed from the mean temperatures and mean relative humidities.

[†] Mean of the column.

418. Richmond (Kew Observatory): North Wall Screen: ht (height of thermometer bulbs above the ground) = 3.0 metres.

July, 1923.

																									Ju	ly, 1923
Day.	I,	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.
1 2 3 4 5	% 81 77 88 86 86 88	% 81 82 90 88 90	% 81 85 92 87 95	% 86 86 91 82 97	% 80 87 92 79 93	% 77 84 92 79 88	% 75 78 87 70 79	% 67 65 75 70 68	% 59 62 67 64 59	% 56 59 71 63 61	% 57 55 70 58 55	% 61 53 67 57 54	% 59 53 65 55 49	% 57 52 69 51 45	% 53 54 70 50 43	% 53 55 74 51 42	% 52 58 72 48 41	% 55 61 75 53 47	% 58 65 75 50 51	% 61 70 75 60 57	% 63 76 79 65 62	% 66 77 80 71 65	% 70 83 82 78 67	% 74 86 84 87 70	% 66·0 69·0 78·5 66·7 65·6	mb. 11·1 12·3 13·7 13·5 15·4
6 7 8 9	74 78 73 79 94	78 80 77 89 97	81 79 79 89 97	83 80 80 88 94	82 79 80 89 97	79 71 80 84 90	73 57 81 79 89	68 47 79 69 91	63 45 76 57 88	55 43 70 54 69	50 39 64 47 64	46 37 63 43 65	45 38 57 39 60	43 37 50 39 56	42 37 45 35 49	41 42 45 33 53	42 45 39 41 60	45 54 41 41 62	49 54 44 45 74	58 53 49 65 90	64 66 68 75 89	67 65 70 74 96	70 59 74 87 93	73 68 79 97 93	61·3 56·5 64·9 63·7 79·7	16·9 17·6 15·9 15·4 20·2
11 12 13 14	91 86 61 86 81	94 91 59 87 81	95 90 62 83 86	95 93 64 87 88	99 96 67 82 89	91 88 67 81 93	87 83 64 80 80	77 77 56 77 76	72 58 49 72 68	70 47 47 67 65	63 47 43 68 61	62 47 47 66 61	58 46 39 61 58	48 44 40 56 57	47 42 40 56 62	44 45 52 61 65	49 43 53 62 69	47 46 54 60 66	50 43 55 64 73	58 49 69 73 83	77 55 71 78 79	79 56 80 79 87	82 59 79 81 84	83 59 81 79 82	71·8 62·6 57·8 72·8 74·3	21·6 21·4 18·9 19·5 17·9
16 17 18 19	84 70 90 79 90	89 74 92 83 88	89 80 91 85 89	90 83 92 90 90	90 83 89 89 90	90 79 85 83 88	90 75 84 79 87	83 67 78 68 79	88 64 69 60 72	72 57 61 59 69	57 57 47 53 67	53 57 51 55 60	48 63 49 57 55	46 57 49 73 51	44 67 44 71 51	43 83 46 79 48	43 76 47 73 48	44 77 50 79 46	50 83 55 85 47	53 79 60 89 57	60 79 62 90 63	59 79 67 91 69	61 92 73 90 75	67 87 75 88 81	66·7 73·3 67·2 76·7 69·3	15.0 13.6 12.6 13.5 17.2
21 22 23 24 25	83 81 82 90 75	85 87 85 89 78	87 88 87 77 77	88 89 86 73 82	84 92 85 78 85	84 88 82 77 84	80 83 76 72 83	75 76 73 69 79	69 70 70 57 77	67 69 66 55 77	63 63 64 55 64	57 63 60 53 64	56 59 59 50 82	53 56 59 47 88	49 53 80 48 88	49 53 75 42 87	49 53 75 42 88	47 55 77 43 82	51 55 80 47 74	59 61 89 52 77	66 61 91 70 78	72 69 90 75 80	77 74 89 75 83	80 81 90 75 86	68·o 69·9 77·7 63·3 79·7	16·2 15·9 15·5 13·4 16·1
26 27 28 29 30	88 73 82 90 84	88 77 84 94 94	90 82 87 93 92	89 83 89 95 91	88 83 88 94 90	80 77 86 89 84	70 76 81 87 79	59 68 83 79 70	56 59 77 71 65	55 53 72 67 63	51 52 80 62 59	47 50 87 58 54	47 57 84 59 53	46 49 84 59 51	45 48 76 61 67	45 52 64 54 69	44 59 70 56 66	43 56 63 59 67	45 61 65 60 70	51 67 73 67 73	55 67 80 72 79	60 69 84 77 83	64 78 86 79 90	69 80 89 80 89	61·8 65·5 79·5 73·6 74·0	10·8 11·3 15·1 13·9 14·4
31	91	89	89	91	88	85	8o _.	76	72	67	65	60	63	75	79	83	89	91	83	88	90	86	82	82	81 · 1	13.9
Mean	82.4	85.2	85.9	86 · 9	86.7	83.4	78.8	72.4	66.3	62 · 1	58 · 1	56.7	55.6	54 · 4	54.7	55 · 7	56.5	57·6	6o·o	66.6	71.9	74.9	77:9	8o·5	69.6	15.5
Vapour Pressure.*	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	
				-				-								1-J TI		J 1	5 5	3 1						·
419. Richm																0/	0/	0/	0/	0/ 1	0/ 1	0/	0/			t, 1923 mb.
1 2 3 4 5	% 91 88 78 83 92	% 90 87 81 82 93	% 91 88 79 91 96	% 91 92 81 91	% 93 93 81 92 97	% 88 89 80 84 77	% 83 81 75 82 72	% 73 70 69 80 67	% 68 60 62 73 58	% 63 57 59 65 55	% 59 49 50 57 49	% 52 49 43 50 46	% 53 49 40 51 44	% 46 53 43 45 41	% 43 63 41 45 42	% 45 68 39 43 39	% 48 58 41 45 41	% 42 53 43 51 42	% 49 57 45 55 47	% 61 66 54 59 59	% 73 72 59 73 72	% 76 75 66 84 69	% 79 79 74 89 77	% 84 79 77 91 82	68·3 69·9 60·9 68·9 65·0	12·4 13·8 11·4 12·8
6 7 8 9	85 83 87	87 83	87 88	90 95	91 94	88 91 85	86 86	77 75	72 67	62 61	55 59	53	43 50	39 48	39 45	43 48	42	41 46	50 52	59 61	64 66	76 71 69	77 79	82 82	66·2 68·0	13·9 15·0
10	93 89	87 89 90	87 94 92	88 94 92	89 95 92	86 90	83 75 83	78 66 78	70 55 71	65 48 61	65 43 55	55 58 39 49	56 44 49	53 43 47	47 44 43	47 47 44	47 42 49 45	43 59 46	41 62 52	59 71 58	65 72 61	75 65	82 81 63	87 85 69	67·9 67·1 66·3	16·3 16·7 15·3
10 11 12 13 14 15	93	87 89	94	94	95	86	75	66	55	48	65 43	58 39	56 44	53 43	47 44	47 47	42 49	43 59	41 62	71	72	75	81	87 85	67·9 67·1	16·3 16·7
11 12 13	93 89 69 92 65 88	87 89 90 72 93 76 92	94 92 72 93 80 92	94 92 73 94 85 90	95 92 74 93 85 90	86 90 74 88 86 85	75 83 64 75 76 83	53 59 67	55 71 51 54 58 69	48 61 48 49 53 58	65 43 55 47 48 51 56	58 39 49 43 48 53 61	56 44 49 41 45 53 55	53 43 47 41 43 55 58	47 44 43 41 42 53 56	47 47 44 39 43 51 55	42 49 45 41 44 54 55	43 59 46 44 43 58 57	41 62 52 46 49 61 62	53 57 69 76	72 61 59 64 73 81	75 65 66 62 77 85	81 63 79 65 82 81	87 85 69 83 66 85 83	67·9 67·1 66·3 56·9 63·3 66·5 72·7	16·3 16·7 15·3 12·4 13·5 16·5 18·8
11 12 13 14 15 16 17 18	93 89 69 92 65 88 83 77 73 87 79	87 89 90 72 93 76 92 77 81 73 87 85	94 92 72 93 80 92 82 85 74 87 87	94 92 73 94 85 90 84 85 72 87 88	95 92 74 93 85 90 84 86 72 87 90	86 90 74 88 86 85 90 83 73 84	75 83 64 75 76 83 93 82 73 84 83	53 59 67 77 88 70 66 79 77	55 71 51 54 58 69 88 61 59 72 69	48 61 48 49 53 58 80 53 59 65 65	65 43 55 47 48 51 56 70 50 76 57 61	58 39 49 43 48 53 61 57 48 84 59 61	56 44 49 41 45 53 55 57 45 78 85 60	53 43 47 41 43 55 58 45 45 75 79 54	47 44 43 41 42 53 56 47 47 78 77 58	47 47 44 39 43 51 55 44 47 76 71 55	42 49 45 41 44 54 55 36 46 86 61 58	43 59 46 44 43 58 57 43 45 66 65 62	41 62 52 46 49 61 62 51 55 64 64 66	58 53 57 69 76 55 73 72 68	72 61 59 64 73 81 57 60 75 76 72	75 65 66 62 77 85 63 61 78 78 76	81 63 79 65 82 81 69 67 79 76 80	87 85 69 83 66 85 83 77 72 87 77 84	67.9 67.1 66.3 56.9 63.3 66.5 72.7 67.6 62.9 73.4 75.9 71.7	16·3 16·7 15·3 12·4 13·5 16·5 18·8 12·8 10·4 13·2 13·4 12·8
11 12 13 14 15 16 17 18 19 20 21 22 23 24	93 89 69 92 65 88 83 77 73 87 79 85 88 77 89	87 89 90 72 93 76 92 77 81 73 85 86 86 79 81 93	94 92 72 93 80 92 82 85 74 87 86 85 82 83 92	94 92 73 94 85 90 84 85 72 87 88 86 87 81 84 94	95 92 74 93 85 90 84 86 72 87 90 88 84 86 94	86 90 74 88 86 85 90 83 73 84 85 87 83 79 89	75 83 64 75 76 83 93 82 73 84 83 86 82 75 80 91	53 59 67 77 88 70 66 79 77 82 80 68 73 89	55 71 51 54 58 69 88 61 59 72 69 84 64 63 64 94	48 61 48 49 53 58 80 53 59 65 65 79 61 60 57 87	65 43 55 47 48 51 56 70 50 76 57 61 78 59 53 54 77	58 39 49 43 48 53 61 57 48 84 59 61 79 63 53 57 69	56 44 49 41 45 53 55 57 45 78 85 60 79 67 54 58 82	53 43 47 41 43 55 58 45 75 79 54 78 67 45 59 85	47 44 43 41 42 53 56 47 47 78 77 58 73 70 43 74 81	47 47 44 39 43 51 55 44 47 76 71 55 72 67 49 80 74	42 49 45 41 54 55 36 46 86 61 58 78 49 51 84 72	43 59 46 44 43 58 57 43 45 66 65 62 78 48 51 88 75	41 62 52 46 49 61 62 51 55 64 66 81 56 49 93 80	71 58 53 57 69 76 55 73 72 68 82 63 59 94 78	72 61 59 64 73 81 57 60 75 76 72 84 69 64 91 78	75 65 66 62 77 85 63 61 78 78 76 83 69 88 74	81 63 79 65 82 81 69 67 79 76 80 85 77 70 93 82	87 85 69 83 66 85 83 77 72 87 77 84 86 78 75 93 87	67.9 67.1 66.3 56.9 63.3 66.5 72.7 67.6 62.9 73.4 75.9 71.1 63.7 77.7 84.1	16·3 16·7 15·3 12·4 13·5 16·5 18·8 12·8 10·4 13·2 13·4 12·8 15·4 14·4 11·0 12·6 14·3 12·3 10·7 12·3 10·7 12·3 10·4
11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	93 89 69 92 655 88 83 77 73 85 88 77 80 93 85 82 89 87 82	87 89 90 72 93 76 92 77 81 73 85 86 79 81 79 90 87 85	94 92 72 93 80 92 82 85 74 87 86 85 82 83 92 81 79 87 87	94 92 73 94 85 90 84 85 72 87 88 86 87 81 84 94 83 84 93 88 89	95 92 74 93 88 90 84 86 72 87 90 88 86 94 87 91 93 93	86 90 74 88 86 85 90 83 73 84 85 87 83 79 94 87 91 92 78 87	75 83 64 75 76 83 93 82 73 84 83 86 82 75 80 91 84 90 85 79 83	66 78 53 59 67 77 88 70 66 77 82 80 80 73 89 76 71 89	55 71 51 54 58 69 88 61 59 72 69 84 64 63 64 73 82 64 67 95	48 61 48 49 53 58 80 53 59 65 65 79 61 60 57 68 70 62 67 96	65 43 55 47 48 51 56 70 50 76 57 61 78 59 53 54 77 61 66 57 59 91	58 39 49 43 48 53 61 57 48 84 59 61 79 63 57 69 59 67 55 52 86	56 44 49 41 45 53 55 57 45 86 60 79 67 54 58 57 63 69 48 91	53 43 47 41 43 55 58 45 75 79 47 45 78 67 74 59 65 71 46 99	47 44 43 41 42 53 56 47 47 78 77 58 73 70 43 74 63 65 69 91	47 47 44 39 43 51 55 44 47 76 71 55 72 67 49 80 74 65 59 64 51 51 51 51 51 51 51 51 51 51 51 51 51	42 49 45 41 44 54 55 36 61 58 78 49 51 84 70 54 59 59	43 59 46 44 43 58 57 43 45 66 65 62 78 48 57 73 59 73 56 87	41 62 52 46 49 61 62 51 55 64 64 68 73 71 76 61 82	71 58 53 57 69 76 55 55 73 72 68 82 63 59 94 77 78 77 79 81 65 89	72 61 59 64 73 81 57 60 75 76 72 84 69 64 91 78 76 80 71 83	75 65 66 77 85 63 61 78 78 78 76 83 69 88 74 80 85 76	81 63 79 65 82 81 69 67 79 76 80 85 77 70 93 82 86 85 79 76 76 76 76 77 70 76 76 76 76 76 76 76 76 76 76 76 76 76	87 85 69 83 66 85 83 77 72 87 77 77 77 84 86 78 78 78 87 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 88 87 87	67.9 67.1 66.3 56.9 63.3 66.5 72.7 67.6 62.9 73.4 75.9 71.7 81.8 71.1 63.7 77.7 77.7 84.1 74.3 76.1 77.0 68.0 86.9	16·3 16·7 15·3 12·4 13·5 16·5 18·8 10·4 13·2 13·4 13·2 13·4 14·4 11·6 14·3 12·0 14·7 12·3 10·7 12·4 8·9
11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	93 89 69 92 655 88 83 77 73 79 85 88 87 89 87 82 65 89 87 86 65	87 89 90 72 93 76 92 77 81 73 85 86 79 81 93 81 79 90 87 85 63 86	94 92 72 93 80 92 82 85 74 87 86 85 82 83 92 87 63 87	94 92 73 94 85 90 84 85 72 87 88 86 87 81 84 94 93 88 89 68	95 92 74 93 85 90 84 86 72 87 90 88 84 80 86 94 91 73 91 73	86 90 74 88 86 85 90 83 73 84 85 87 83 79 94 87 73 93	75 83 64 75 76 83 93 82 73 84 83 86 82 75 80 91 84 90 85 79 83 70 83	66 78 53 59 67 77 88 70 66 79 77 82 80 68 73 89 76 71 89 61	55 71 51 54 58 69 88 61 59 72 69 84 64 63 64 67 95 58	48 61 48 49 53 58 80 53 59 65 65 65 79 61 60 70 62 67 96 53 64	65 43 55 47 48 51 56 70 50 76 57 61 78 59 53 54 77 61 66 57 59 91 51 60	58 39 49 43 48 53 61 57 48 84 59 61 79 63 57 69 59 67 55 52 86 50 50 50 50 50 50 50 50 50 50	56 44 49 41 45 53 55 57 45 85 60 67 54 58 57 63 64 48 51 51 50	53 43 47 41 43 55 58 45 75 79 44 45 59 65 71 46 46 46 54	47 44 43 41 42 53 56 47 47 78 73 70 43 74 81 63 65 69 49 49 45	47 47 44 39 43 51 55 44 47 76 72 67 49 80 74 65 59 64 51 93 48 58	42 49 45 41 44 55 36 61 58 78 49 51 84 72 69 58 70 48 61	43 59 46 44 43 58 57 43 45 66 65 62 78 48 57 73 59 73 56 87 56 66	41 62 52 46 49 61 62 51 55 64 64 68 73 71 76 61 82 59	71 58 53 57 69 76 55 55 73 72 68 82 63 59 94 78 75 75 79 81 65 86 66	72 61 59 64 73 81 57 60 75 76 72 84 69 64 91 78 76 80 80 80 71 83 73 83 73 84 86 86 86 86 86 86 86 86 86 86 86 86 86	75 65 66 62 77 85 63 61 78 78 78 78 83 69 69 88 88 76 77 78 85 77 77 78 85 78 77 77 77 77 77 77 77 77 77 77 77 77	81 63 79 65 82 81 69 76 80 85 77 70 93 86 85 77 76 76 79 93 89 76 76 77 79 76 77 70 77 70 70 70 70 70 70 70 70 70 70	87 85 69 83 66 85 83 77 72 87 77 77 84 86 78 79 87 87 87 87 87 87 87 87 87 87 87 87 87	67.9 67.1 66.3 56.9 63.3 66.5 72.7 67.6 62.9 73.4 75.9 71.1 63.7 77.7 77.7 77.7 84.1 74.3 76.1 77.0 68.0 86.9 61.3	16·3 16·7 15·3 12·4 13·5 16·5 18·8 12·8 10·4 13·2 13·4 11·0 12·6 14·3 12·0 14·7 12·3 10·7 12·4 8·9
11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Mean	93 89 69 92 65 88 83 77 73 85 88 77 78 80 93 85 82 85 87 85 86 87 88 87 88 88 88 88 88 88 88	87 89 90 72 93 76 92 77 81 73 85 86 86 86 87 99 81 99 87 85 63 86 83 99	94 92 72 93 80 92 85 74 87 86 85 83 92 87 87 63 87 85·5 mb.	94 92 73 94 85 90 84 85 72 87 88 86 87 81 84 93 84 93 84 93 86 89 68	95 92 74 93 85 90 84 86 72 87 90 88 84 80 86 94 87 91 93 91 93 91 93 91 93 91 93 91 93 91 91 91 91 91 91 91 91 91 91 91 91 91	86 90 74 88 88 86 85 90 83 73 84 85 87 83 79 94 87 78 87 73 88 87 73 88 87 87 88 87 88 87 88 88 87 88 88	75 83 64 75 76 83 93 82 73 84 83 86 82 75 80 91 84 90 85 79 83 70 86 81 · o 81	66 78 53 59 67 77 88 70 66 79 77 82 80 68 73 89 76 71 89 76 77 74·1	55 71 51 54 58 69 88 61 59 72 69 84 64 63 64 94 73 82 64 67 95 58 69 68 22 69 68 69 69 69 69 69 69 69 69 69 69 69 69 69	48 61 48 49 53 58 80 53 59 65 79 61 60 57 87 68 70 62 62 67 96 53 62 62 62 62 62 97 98 98 98 98 98 98 98 98 98 98 98 98 98	65 43 55 47 48 51 56 70 50 76 78 59 53 54 77 61 66 57 59 91 51 60 58·8	58 39 49 43 48 53 61 57 48 84 59 61 79 63 57 69 59 67 55 52 86 50 50 50 50 50 50 50 50 50 50	56 44 49 41 45 53 55 77 45 78 85 60 79 67 54 58 82 57 63 69 48 91 57 50 57 60 79	53 43 47 41 43 55 58 45 75 79 45 78 67 45 59 85 59 65 71 46 90 46 54 54 54 54	47 44 43 41 42 53 56 47 47 78 73 70 43 74 81 63 65 69 49 91 45 51 55·7 78 78	47 47 44 39 43 51 55 44 47 76 71 55 72 67 49 80 74 65 59 64 51 93 48 55 65 66 66 66 66 66 66 66 66 66 66 66	42 49 45 41 44 54 53 36 46 86 61 58 78 49 51 84 72 69 54 91 48 61 55 61 61 61 61 61 61 61 61 61 61 61 61 61	43 59 46 44 43 58 57 43 45 66 65 62 78 48 75 73 56 87 73 56 66 87 56 66 66 78 78 78 78 78 78 78 78 78 78 78 78 78	41 62 52 46 49 61 62 51 55 64 64 66 81 73 80 73 77 60 73 70 60 73 75 75 75 77 76 77 77 77 77 77 77 77 77 77 77 77	71 58 53 57 69 76 55 55 73 72 68 82 63 59 94 78 75 79 81 65 83 67 77	72 61 59 64 73 81 57 60 75 76 72 84 69 64 91 78 76 80 80 71 83 73 81 74 75 76 80 77 78 78 78 78 78 78 78 78 78 78 78 78	75 65 66 62 77 85 63 61 78 78 76 83 69 88 74 80 85 77 78 87 74 89 74 89 89 89 89 89 89 89 89 89 89 89 89 89	81 63 79 65 82 81 69 67 79 78 80 85 77 70 93 82 86 85 79 76 76 79 93 87 87 89 80 78 78 78 78 78 78 78 78 78 78 78 78 78	87 85 69 83 66 85 83 77 72 87 77 77 84 86 78 87 85 88 88 88 88 81 81 61 81 81 81 81 81 81 81 81 81 81 81 81 81	67.9 67.1 66.3 56.9 63.3 66.5 72.7 67.6 62.9 73.4 75.9 71.1 63.7 77.7 84.1 74.3 76.1 77.0 68.0 86.9 61.3 74.8	16·3 16·7 15·3 12·4 13·5 16·5 18·8 12·8 10·4 13·2 13·4 12·8 15·4 14·4 11·0 12·6 14·3 12·0 14·7 12·3 10·7 12·3 10·7 12·3 10·7 12·3 10·7 12·3 10·7 12·3 10·7 12·3 10·7 12·7 12·3 10·7 12·7

[•] Computed from the mean temperature and mean relative humidity.

420. Richmond (Kew Observatory): North Wall Screen: ht (height of thermometer bulbs above the ground) = 3.0 metres.

September, 1923.

																								Seb) tem be	r, 1923.
Day.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean.	Vapour Pressure.*
1 2 3 4 5	% 91 87 99 97 87	% 95 87 92 93 91	% 95 89 99 89 91	% 97 89 93 91 93	% 99 91 97 95 92	% 99 91 97 92 91	% 93 85 93 86 88	% 88 77 85 83 89	% 83 64 75 91 85	% 72 56 66 93 71	% 72 53 61 93 63	% 77 55 55 94 59	% 63 53 53 93 57	% 51 56 50 94 57	% 50 51 50 96 54	% 51 50 48 89 55	% 55 53 47 79 57	% 60 59 53 80 62	% 71 66 71 73 72	% 74 77 75 73 79	% 77 86 82 75 83	% 77 86 85 82 87	% 80 93 88 84 90	% 83 89 92 88 92	% 77·4 72·5 75·2 87·7 76·8	mb. 10·4 10·0 10·2 12·1 11·7
6 7 8 9	92 91 82 96 92	93 92 85 97 100	96 96 92 99 96	99 97 93 100 95	97 97 94 99 96	99 94 95 97 97	97 93 93 95 95	96 91 88 89 91	92 87 81 86 82	89 83 64 79 71	82 76 61 72 70	76 75 53 65	67 73 53 60 58	66 75 52 57 58	62 64 51 52 57	63 61 51 60 59	61 58 51 55 55	56 63 59 60 66	68 68 69 71 71	76 70 80 81 69	79 69 84 86 82	83 68 95 94 80	87 72 91 93 83	88 79 96 93 85	81·9 79·0 75·2 80·7 78·2	13.0 13.8 11.0 12.8 14.2
11 12 13 14 15	82 79 97 81 91	92 78 99 88 91	93 82 97 88 88	92 82 100 89 87	89 85 97 89 88	92 86 100 90 91	89 83 100 88 90	83 82 95 83 83	80 75 91 80 77	80 68 85 71 72	73 65 77 68 68	69 63 68 63 62	64 59 60 60 68	53 57 55 59 79	49 56 57 66 81	48 55 57 67 83	49 57 57 69 87	55 61 65 73 83	70 72 70 78 90	77 80 81 93 90	79 83 82 91 88	83 89 80 93 92	78 95 82 93 93	80 96 81 91 93	75·1 74·2 80·8 79·4 83·9	13·6 12·4 13·9 14·8 11·9
16 17 18 19 20	93 94 93 92 87	93 99 92 93 87	95 99 89 93 87	95 97 91 94 83	95 97 93 95 80	95 95 90 93 78	94 97 91 91 77	92 82 85 83 73	83 72 75 72 68	64 63 74 65 60	54 85 61 56	59 53 78 64 55	55 50 68 65 58	52 52 64 63 57	48 47 65 65 58	53 55 64 80 61	57 55 63 82 62	63 67 70 85 67	76 78 76 91 69	81 84 81 91 72	82 86 81 89 76	87 89 83 88 76	89 92 88 87 75	91 93 91 87 85	77·2 77·0 80·5 82·1 71 2	9·6 10·0 10·8 10·6 9·5
21 22 23 24 25	92 89 95 84 88	95 88 92 88 89	96 93 93 89 93	97 95 93 91 93	95 92 96 92 89	95 85 99 95 89	93 85 96 96 86	85 82 86 91 81	77 82 83 81 74	74 85 88 73 66	70 84 76 65 70	71 73 69 64 62	73 67 66 60 69	55 85 62 55 63	61 79 66 55 64	61 82 69 59 65	64 83 82 67 65	65 83 83 73 70	67 89 78 79 75	71 92 79 81 72	77 85 81 87 68	81 89 81 92 74	84 91 84 93 77	91 95 82 89 81	78·6 85·5 83·7 79·0 76·1	10·8 12·0 10·8 10·7 11·7
26 27 28 29 30	85 96 91 94 94	95 93 94 94	85 95 96 92 93	85 95 95 91 95	82 97 91 93 95	81 95 92 93 94	80 97 92 93 94	87 92 82 95 89	81 84 76 90 83	79 80 74 87 75	76 72 72 80 72	67 67 71 77 74	66 67 72 74 72	67 59 73 74 69	71 61 82 75 71	73 63 84 73 67	75 69 80 80 66	80 76 82 87 73	81 78 85 88 87	85 82 85 89 92	91 87 85 93 93	91 90 89 93 95	94 92 90 91 93	95 93 92 92 96	80·7 82·6 84·4 87·0 84·3	13·2 13·4 14·7 18·2 18·0
Mean	90.4	91.7	92·6	92.9	92 · 9	92.7	91.0	86•3	80.3	74.2	70 · 2	66.6	64 • 1	62.3	62 · 1	63·5	64.8	69•3	75.9	80.4	82.9	85.7	87.4	89.3	79.6	12.3
Vapour. Pressure*	mb. 11·6	mb. 11•5	mb. 11•5	mb. 11•4	mb. 11·2	mb. 11·2	mb. 11·6	mb. 11•9	mb. 12·2	mb. 12•1	mb. 12·3	mb. 12·3	mb. 12•4	mb. 12·3	mb. 12·4	mb. 12·6	mb. 12·6	mb. 12·4	mb. 12·6	mb. 12·5	mb. 12·3	mb. 12·3	mb. 12·0	mb. 11•9	mb. 12·0‡	
421. Richm	ond	/Kay	v Oh	sarv	atory	n) :]	Nort	h W	all S	cree	en: l	ht = 3	·o m	etre	s.									(Octobe	r, 1923.
721. 110	1 %	%	1 %	1 %	%	% 96	%	1 %	%	%	%	%	%	%	% 91	% %	% 89	% 89	% 90	% 92	% 91	% 93	% 93	% 89	93.6	mb. 14·8
1 2 3 4 5	97 86 79 78 85	97 91 79 79 89	99 92 81 79 91	99 93 84 79 93	92 89 77 95	93 91 76 97	99 89 92 77 97	95 86 86 78 91	97 80 82 74 85	94 72 79 67 85	90 73 81 62 72	90 75 87 57 67	94 72 86 59 66	90 79 87 57 67	80 91 56 66	81 91 57 72	82 95 60 76	89 91 64 78	93 91 65 79	92 89 71 79	87 85 74 83	79 80 79 84	81 79 83 85	82 79 85 89	84·3 85·6 70·4 82·0	11·9 9·0 7·9 8·0
6 7 8 9	91 95 97 94 82	93 97 96 91 83	96 97 96 92 84	97 96 99 90 84	97 99 99 89 83	96 96 99 89 83	96 97 97 85 84	96 95 95 83 84	89 91 83 86 86	83 85 74 79 81	76 76 71 74 82	64 67 67 67 85	59 73 67 53 90	63 76 57 53 93	60 79 63 54 90	67 77 73 58 87	69 73 79 65 92	77 77 76 73 89	85 83 83 76 92	87 83 87 79 93	89 92 93 78 87	92 96 91 80 79	95 97 93 80 80	95 97 94 82 91	83·7 87·2 84·6 77·3 85·8	11·1 11·6 12·6 13·0 13·4
11 12 13 14 15	93 96 86 93 97	92 96 87 94 97	93 96 86 97 97	95 96 86 97 97	93 99 82 97 97	93 97 80 97 97	91 97 78 93 97	92 99 78 93 97	88 97 75 89 89	85 95 68 84 83	85 92 67 76 76	85 88 66 68 67	83 91 63 75 65	82 92 58 71 63	87 92 63 74 59	88 89 68 75 64	88 89 73 76 71	89 88 80 83 80	91 89 84 89 83	91 89 87 94 91	90 85 87 94 89	90 83 91 92 91	92 89 93 93 93	96 89 94 97 93	89·5 92·3 78·2 87·1 84·8	12·2 11·9 8·6 8·2 10·2
16 17 18 19 20	99 95 93 88 93	99 97 93 89 96	95 99 95 87 95	97 99 100 86 96	94 97 99 87 96	95 96 99 82 95	93 97 93 80 93	87 95 89 81 96	8 ₄ 90 8 ₄ 79 91	78 74 87 79 82	74 73 89 80 75	67 70 80 83 69	67 73 70 89 65	67 77 71 93 64	73 79 71 91 67	73 81 71 93 72	75 82 76 93 78	79 83 77 89 83	83 85 80 90 83	87 87 82 93 82	91 90 86 97 83	93 91 91 92 83	93 92 91 91 87	95 91 89 92 91	84·9 87·3 85·7 87·6 84·0	9·3 11·2 11·3 13·7 10·7
21 22 23 24 25	90 82 85 85 81	88 82 87 87 82	83 85 87 92 82	81 86 87 92 83	80 89 89 93 80	84 86 86 95 80	79 85 86 91 77	87 79 92 85 74	8 ₃ 7 ₅ 9 ₂ 8 ₀ 7 ₄	81 67 94 73 68	79 67 93 67 59	75 62 93 63 60	8 ₁ 6 ₂ 8 ₉ 5 ₉ 5 ₉	87 86 84 61 61	89 82 85 67 64	82 79 82 70 71	74	76	85 83 80 83 80	83 85 81 82 81	85 83 81 85 87	86 81 84 85 91	84 84 87 87 89	82 85 89 83 87	83·4 79·9 86·5 79·9 75·5	11·6 9·4 11·1 9·9 9·7
26 27 28 29 30	87 89 81 91 79	85 82 82 93 78	88 78 84 93 81	84 87 87 97 84	81 89 87 97 88	84 85 86 97 88	91 87 87 94 88	92 91 86 88 85	92 92 84 83 85	78 84 81 77 85	70 79 67 76 83	68 83 68 76 83	76 76 66 69 79	65 71 73 65 80	66 65 70 65 82	71 69 69 70 80	69 74 76	81 78	83 68 81 79 84	85 69 82 81 88	85 78	77 76 86 76 93		81 77 93 74 97	79·9 78·1 80·0 81·7 84·7	10·4 11·2 10·7 10·3 12·5
31 Mean	97 89·2	96 89·6	96	99 91 · 8	96	97 90·8	96 89·9	99 88 · 8	96 85·7	86 80·3	-	73	66 72 · 8	67	63		-		97 83·	99 8 85.		_	-	100	88.9	10.8
Vapour	mb.	mb.	mb.	 mb.	mb.	mb.	mb.	mb.	mb.	mb	. mb	 . mb.	mb	 mb.	 mb	. mb	. mb	. mb	.(mb	. mb	 - mb	. mb	. mb	o. mb.	. mb.	<u> </u>
Pressure*	10.6	10.6	10.6	10.7	10.6	10.6	10.6	10.8	11.1	11.0	11.0	10.9	10.	10.8	10.0	10.	7 10.	7 10.	7 10.	7 10.	6 10.6	6 10.	5 10 ·	4 10·5	10.7	Į
Hour G.M.T	Ι.	2.	3.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean	

^{*} Computed from the mean temperature and mean relative humidity.

[†] Mean of the column.

422. Richmond (Kew Observatory): North Wall Screen: ht (height of thermometer bulbs above the ground) = 3.0 metres.

1 2 3 4 5 0 7 8 9 10 11 10 10 10	vapour Pressure. mb. 9.8 0 9.8
1 100 100 100 100 100 100 100 100 100 1	
6 03 01 80 03 01 93 93 95 93 91 82 68 67 71 73 78 79 84 92 86 89 91 93 87 8	11·3 3·5 7·6 8·7
7	7·3 5·9 5·9 7·2 5·9 7·2 6·8
11	6·3 7·0 9·9 7·5 7·5 7·5
17	7·2 7·8 7·1 6·4 6·5 6·6 6·1
21	6.8 6.5 6.5 5.6 5.8 5.7 5.1
27 99 99 99 95 91 95 91 91	6.5 4.8 3.4 4.9 7.9 6.1 6.6 6.4 5.9
mean 83.0 83.9 89.7 95.1 30 3 95.1 69 9 60 0 60 1 63 9 7 9 7 9 7 9 7 9 7 9 7 9 7 9 7 9 7 9	5.8 7.01
Vapour mb.	nb. 5·9‡
423. Richmond (Kew Observatory): North Wall Screen: ht = 3.0 metres.	mber, 1923.
% % % % % % % % % %	mb.
2	5·7 8·1 2·8 6·1 1·7 7·1 4·5 7·1
7	6·9 3·5 7·1 8·8 6·7 5·9 7·1
11	10.0 9.6 5.8 7.9 7.0 7.0
16 90 93 93 93 94 91 91 92 93 93 93 94 91 91 92 93 93 93 93 93 94 94 94 94 95 94 95 94 95 94 95	5·9 5·7 9·3 8·0 5·5 3·4 4·4
22 06 09 07 09 06 06 09 09 05 05 86 81 83 81 78 79 79 80 79 81 85 86 85 8	5·3 8·1 6·8 6·8 6·7 5·8
24 84 83 87 90 90 83 83 87 92 93 92 94 97 94 91 89 79 74 75 76 77 81 85 83 8	·8 7·4
24	7·8 7·1 8·2 6·2 7·9
24 84 83 87 90 90 83 83 87 92 93 92 94 97 94 91 89 79 74 75 76 77 81 85 85 83 85 85 87 95 91 91 91 91 85 77 76 76 76 79 82 89 96 92 95 94 97 95 88 85 87 95 91 91 91 91 93 91 90 86 85 86 86 85 89 87 93 93 93 95 97 97 97 97 97 97 97 97 97 97 97 97 97	7·8 7·1 8·2 6·2 7·9 3·8 7·1
24 84 83 87 90 90 83 83 87 92 93 92 94 97 94 91 89 79 74 75 76 77 81 85 85 83 85 85 85 85 87 95 91 91 91 91 85 77 76 76 76 79 82 89 96 92 95 94 97 95 88 85 87 89 96 92 95 94 97 95 88 85 87 95 91 91 91 91 91 93 91 90 86 85 86 86 85 89 87 93 93 93 95 96 82 89 96 85 87 96 96 82 89 96 87 97 97 97 97 97 97 97 97 97 97 97 97 97	7·8 7·1 8·2 6·2 7·9 7·6 7·3
24 84 83 87 90 90 88 83 87 92 93 92 94 97 94 91 89 79 74 75 76 77 81 85 85 83 82 89 89 89 89 89 89 89 87 93 87 95 91 91 91 85 77 76 76 76 79 82 89 89 96 92 95 94 97 95 88 82 89 96 92 95 94 97 95 88 82 89 96 92 95 94 97 95 88 82 89 96 92 95 94 97 95 88 82 89 96 92 95 94 97 95 88 82 89 96 92 95 94 97 95 88 82 89 96 92 95 94 97 95 88 82 89 96 92 95 94 97 95 88 82 89 87 93 93 93 95 96 96 96 96 96 96 96 96 96 96 96 96 96	7·8 7·1 8·2 6·2 7·9 3·8 7·1

^{*} Computed from the mean temperature and mean relative humidity.

[†] Mean of the column.

RELATIVE HUMIDITY AND VAPOUR PRESSURE: ANNUAL MEANS OF HOURLY VALUES.

From the monthly means, for exact hours, Greenwich Mean Time.

424. Richmond (Kew Observatory): North Wall Screen: $h_t = 3 \cdot 0$ metres.

1923.

G.M.T.	I.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	Mean
Relative Humidity	% 87·3	% 88·3	% 88·9	% 89·3	89.6	% 88·7	% 86·9	% 84·1	% 80·5	% 77·0	% 73·9	% 71·1	% 69·2	% 68·3	68·0	% 69·3	% 70·8	% 72·8	% 75·7	% 79·0	% 81·1	% 83·1	% 85·0	% 86·3	% 79·8
Vapour Pressure in millibars		mb. 9·4		mb. 9·3		mb. 9.4	mb. 9°5	mb. 9·5		mb. 9·8		mb. 9∙9						mb. 10•0			mb. 9·7		mb. 9·6		

RELATIVE HUMIDITY: MONTHLY MEANS AND DIURNAL INEQUALITIES.

The departures from the mean of the day are adjusted for non-cyclic change.

Richmond (Kew Observatory): North Wall Screen: $h_t = 3.0$ metres.

1923.

Month.	Mean.	Hour 1.	G.M.T. 2.	3.	4.	5.	6.	7-	8.	9.	10.	II.	Noon.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.
Jan. Feb. Mar.	87.4	+ 3.4	+ 3·8	+ 3.9	十 3.7	l + 4·5l	+ 4.5	+ 4.4	+ 4.6	+ 2.4	+ 0.7	- 1.9	% - 3.6 - 4.1 - 7.6	- 6.6	− 7·0	- 7.2	7·I	- 5.0	- 3.3	- I·5	+ 0.5	十 0.3	+ 1.9	+ 2.7	+ 2.2
April May June	74.3	+11.9	+12.9	+13.7	+14.5	+14.2	+13.0	+ 8.8	+ 4.2	- I.O	— 4·I	— 8·o	- 10·8 - 11·0	-11.8	-13·I	-14.8	-12.8	-13.6	-12.9	— 8·5	— 3·3	+ 0.5	+ 3.4	+ 7.7	+10.2
July Aug. Sept.	70.2	+13.1	+13.8	+15.3	+16.7	+17.6	+15.0	+10.8	+ 3.9	- 2.0	一 7·3	-11.4	-12·9 -13·7 -12·9	-13.2	14 ⋅8	14.6	-14.7	-14.7	-13.5	- 9.6	— 2·6	+ 1.6	+ 4.5	+ 8.3	+11.3
Oct. Nov. Dec.	85.8	+ 2.7	+ 3.0	+ 3.5	+ 3.9	+ 4.3	+ 4.6	+ 4.3	+ 4.1	+ 2.8	+ 0.3	- I·9	- 10·4 - 4·9 - 2·7	— 7·9	 9 ⋅3	-8.9	-6.1	-3.3	- o·6	+ 0.4	+ 1.2	+ 1.2	+ 1.5	+ 2.6	+ 2.4
Year	79.8	+ 7.5	+8.5	+ 9.1	+ 9.5	+ 9.8	+ 8.9	+ 7.1	+ 4.3	+ 0.8	- 2.7	- 5.8	- 8·6	-10.5	-11.5	−11 ·8	-10.4	– 9·0	– 6∙9	- 4.0	- 0.7	+ 1.3	+ 3.3	+ 5.2	+ 6.5

RAINFALL: ANNUAL TOTALS OF HOURLY VALUES.

Amounts, in millimetres; durations, in hours for periods of sixty minutes, between the exact hours, Greenwich Mean Time.

426. Richmond (Kew Observatory): H_r (height of receiving surface above M.S.L.) = H_r (height of station above M.S.L.) + h_r (height of receiving surface above ground) = 5.5 metres + 0.53 metres. 1923.

		 													·											
G. M.T.		o to I.	I to 2.	2 to 3.	3 to 4.	4 to 5.	5 to 6.	6 to 7.	7 to 8.	8 to 9.	9 to 10.	to to	11 to Noon	Noon to 13.	13 to 14.	14 to 15.	15 to 16.	16 to 17.	17 to 18.	18 to 19.	19 to 20.	20 to 21.	2I to 22.	22 to 23.	23 to 24.	o to 24.
Amount	•••	 mm. 23·2	mm. 30·6		mm. 30·2	mm. 18·5			mm. 21·1					mm. 32·I		mm. 36·6				1	mm. 36·9	1	mm. 23·3	mm. 32·4	mm. 39·6	mm. 638·2
Duration		 hr. 22·2	hr. 25.7	hr. 24.7	hr. 23·5	hr. 22·I	hr. 16·6	hr. 16·5	hr. 17·1	hr. 20·3	hr. 18·0	hr. 18·2	hr. 19·5	hr. 18·6	hr. 21·6	hr. 24·4	hr. 20·6	hr. 19·0	hr. 19·3	hr. 22·6	hr. 24·4	hr. 21·6	hr. 22·1	hr. 24.0	hr. 22.4	hr. 505∙0

427. Richmond (Kew Observatory).

NOTES ON RAINFALL.

1923.

The driest period of the year occurred in June and the beginning of July. No precipitation at all was recorded from June 27th to July 8th (12 days). There was no day with as much as a millimetre from May 30th to June 11th (13 days) and again from June 20th to July 8th (19 days). From May 30th to July 8th (40 days) the total fall was only 6.4 mm. The drought was broken by the great storm on the night July 9th—10th.

There was another dry period at the beginning of August; no precipitation being recorded from the 2nd to the 14th (13 days).

Wet Periods.

The most persistent wet weather was in February. Rain fell on every day from February 6th to March 1st, with two exceptions, the 15th and the 20th. In October and again in December there were runs of 11 days with precipitation on each.

Rainfall Duration.

There were 52 calendar days on which the duration of rainfall was registered as 0·1 to 1·0 hour, 41 days with 1·1 to 2·0 hours, 71 days with 2·1 to 6·0 hours, 17 days with 6·1 to 12.0 hours, 2 days with more than 12 hours. The days with the greatest duration were March 13th, when the duration was 15.1 hours, the amount 19.7 mm. and December 30th, when 12.1 hours produced 8.5 mm.

Continuous Falls.

On March 13th it rained continuously for 11.8 hours, producing 18 mm. On December 21st it snowed continuously from 11h. 15m. to 22h. 30m. The water equivalent was only 5 mm.

Heavy Falls in Short Periods.

In the great thunderstorm of July 9th to 10th, 5mm. fell in 12 minutes, 10 mm. in 24 minutes, 25 mm. in 1h. 24m. and 52 mm. in 6 hours. The only other instances of falls of 5 mm. in an hour or less were on October 19th (5 mm. in 30 min., 10 mm. in 90 min.) and October 26th (5 mm. in 36 min.).

Richmond (Kew Observatory): H_r (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + h_r (height 428. January, 1923. of receiving surface above ground) = 5.5 metres + 0.53 metres.

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Richmond (Kaw Observatory) . He

February, 1923.

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430. Richmond (Kew Observatory): H_r (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + h_r (height of receiving surface above ground) = 5.5 metres + 0.53 metres. March, 1923.

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21	•••				.3	•2	1.0	•1	•••	•••	•••				•••										2.5	1.2
22	•••		•••	• • • • • • • • • • • • • • • • • • • •							• 5	•5	•2	•6											2.6	5.5
24	•••						:::									•••	•••	•••					•••			
26	•2	.3	1.1	1.1	.3	•4					•••											1.2	 1·6		3·4 3·0	4·3 2·0
27 28				٠											]										3·5	0.4
29 30										•••														•••		•••
31	•••	•••							•••				<u></u>					<u> </u>								
Sum.	0.4	0.8	2.1	3.8	3.2	5.4	4.9	2.1	3.1	1.2	1.8	0.9	0.2	3.3	2.2	1.3	3.2	1.1	1.0	0.9	0.9	2.8	4.3			49.5
Total Dura-	hr. 0·8	hr.	hr. 2·0	hr. 2•4	hr. 2·1	hr. 3·7	hr. 2·4	hr.	hr. 2·2	hr. 1•8	hr. 3·1	hr. 2·0	hr. 1•6	hr. 2·0	hr. 1·9	hr. 1·4	hr. 3·1	hr. 1.6	hr. 1·1	hr. 1·6	hr. 2·2	hr. 3·5	hr. 2·5	hr. 2·0	hr. 49·5	
i DOH.			1	1		l .	1	1	ı	F		·		<u>'</u>												
431.	Ric	hmo	nd (K	! ew 0	bserva	atory	): H	r = 5	·5 m	etres	+ o.	53 m	etres.							·				Apr	il, 19	23.
431.	Ric	hmoi	nd (K	ew O	mm.	atory	mm.	mm.	<del></del>	etres	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.		mm.	br.
ļ								mm.	mm. 	<del>,</del>	mm. 	mm.	mm. 	mm. 								1	1			hr.
431.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.										mm. 	mm. 	hr. 
431. 1 2 3 4 5	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm. 	mm.	mm.	mm.	mm.				···		···	···			mm.	mm.	hr. 
431. 1 2 3 4 5 6 7	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.				···		···	  		···	mm.  	mm.   o·4	hr I·3
431. 1 2 3 4 5 6	mm.   	mm.	mm.	mm.	mm	mm.	mm.	mm.	mm.	mm.	mm	mm.	mm.	mm.		::		···		···				mm.	mm 0·4	hr 1·3 3·1
431. I 2 3 4 5 6 7 8	mm.	mm.	mm.	mm	mm	mm.	mm	mm.   	mm.	mm.	mm.	mm.	mm.	mm.				···			1.1 		   	mm.	mm 0·4 1·0	hr 1·3 3·1
431. 1 2 3 4 5 6 7 8 9	mm.	mm.	mm.	mm.	mm	mm.	mm	mm.	mm.	mm.	mm	mm.	mm.	mm.	      2.0	     	     	···		     1.6	     I.I			mm	mm 0·4 1·0 3·6 6·1 7·5	hr i·3 3·1 3·3
431. 1 2 3 4 5 6 7 8 9 10 11	mm	mm	mm	mm	mm.	mm.	mm.	mm	mm	mm.	mm.	mm.	mm	mm	     2.0	     	     	     	    	     1.6	      1.1		        	mm	mm 0·4 1·0 3·6 6·1	hr 1·3 3·1 3·3 5·5 5·6
431. I 2 3 4 5 5 6 7 8 9 10 II 12 13	mm	mm	mm	mm	mm	mm.	mm.	mm	mm.	mm.	mm	mm.	mm	mm	     2.0 .1	     			       	     1.6	      		      	mm	mm 3.6 6.1 7.5 3.5 1.9	hr 3·1 3·3 5·5 6·6 3·1 0·4
431. I 2 3 4 5 6 7 8 8 9 10 11 12 13 14 15 16 17	mm	mm	mm	mm	mm	mm	mm	mm.	mm.	mm.	mm.	mm.	mm.	mm	     2.0 .1 	··· ··· ··· ··· ··· ··· ··· ··· ··· ··				     1.6	      		       	mm	mm 0.4 I.0 3.6 6.1 7.5 3.5 I.9 0.8	hr 1·3 3·1 3·3 5·5 5·6 3·1 0·4 1·1
431. I 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	mm	mm	mm	mm	mm	mm.	mm.	mm	mm.	mm.	mm.	mm.	mm.	mm	     2.0 	      				1.6 2.0	      		       	mm	mm 3.6 6.1 7.5 3.5 1.9 0.8	hr 1·3 3·1 3·3 5·5 6 3·1 0·4 1·1
431. I 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	mm	mm	mm	mm	mm	mm	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm	     2.0  	··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··				    1.6  2.0 	      	···· ··· ··· ··· ··· ··· ··· ··· ··· ·	       	mm	mm   o · 4   I · 0     3 · 6   6 · 1   7 · 5   3 · 5   1 · 9   o · 8	hr 1·3 3·1 3·3 5·5 5·6 3·1 0·4 1·1
431.  I 2 3 4 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	mm	mm	mm	mm	mm	mm.	mm.	mm	mm.	mm	mm.	mm.	mm.	mm	     2.0  	      				1.6 2.0		··· ··· ··· ··· ··· ··· ··· ··· ··· ··	       	mm	mm 3.6 6.1 7.5 3.5 1.9 0.8	hr 3·1 3·3 5·5 6 3·1 0·4 1·1
431.  I 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	mm	mm	mm	mm	mm	mm.	mm	mm.	mm.	mm.	mm.	mm.	mm	mm	2·0 ··· ··· ··· ··· ··· ··· ··· ··· ···	··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··				    I·6		··· ··· ··· ··· ··· ··· ··· ··· ··· ··	       	mm	mm 0.4 1.0 3.6 6.1 7.5 3.5 1.9 0.8	hr 3·3
431.  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	mm	mm	mm	mm	mm	mm.	mm	mm	mm.	mm	mm.	mm.	mm	mm	        	··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··		         		1.6	    I·I   	··· ··· ··· ··· ··· ··· ··· ··· ··· ··	       	mm	mm 3.6 6.1 7.5 3.5 1.9 0.8	hr 3·3 3·1 3·3 5·5 6·6 3·1 0·4 1·1
431.  I 2 3 4 5 6 7 8 9 10 II 12 I3 14 I5 16 17 18 19 20 21 22 23 24 25 26 27	mm	mm	mm	mm	mm	mm.	mm	mm.	mm.	mm	mm.	mm.	mm	mm		··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··				1.6 2.0		···· ··· ··· ··· ··· ··· ··· ··· ··· ·	         	mm	mm 0.4 1.0 3.6 6.1 7.5 3.5 1.9 0.8 0.1 0.2 5.0	hr 1·3 3·1 3·3 5·5 5·6 3·1 0·4 1·1 0·1 0·1 0·7 7·4
431.  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	mm	mm	mm	mm	mm	mm	mm	mm	mm.	mm	mm.	mm.	mm	mm		··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··						···· ··· ··· ··· ··· ··· ··· ··· ··· ·	         	mm	mm 3.6 6.1 7.5 3.5 1.9 0.8	hr 3·3 3·1 3·3 5·5 6 3·1 0·4 1·1
431. I 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mm	mm	mm	mm	mm 2.3	mm	mm	mm	mm	mm	mm.	mm.	mm	mm	2.0 ··· ··· ··· ··· ··· ··· ··· ··· ··· ·	··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··						··· ··· ··· ··· ··· ··· ··· ··· ··· ··		mm	mm 3.6 6.1 7.5 3.5 1.9 0.8 0.1 1.9 7.6 0.1 1.9 0.1	hr 3·3
431.  1 2 3 4 5 5 6 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum.	mm	mm	mm	mm	mm 2·3	mm	mm	mm	mm	mm	mm.	mm.	mm	mm	         					1.6 2.0		···· ··· ··· ··· ··· ··· ··· ··· ··· ·		mm	mm 3.6 6.1 7.5 3.5 1.9 0.8 0.1 1.9 7.6 0.1 1.9 0.1	hr 3·1 3·3 5·5 6 3·1 0·4 1·1 0·1 0·9 7·4 8·9 0·1 4·3 0·2
431. I 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 30	mm	mm	mm	mm	mm 2.3	mm	mm	mm	mm	mm	mm		mm	mm										mm	mm 3.6 6.1 7.5 3.5 1.9 0.8	hr 1·3 3·1 3·3 5·5 6 3·1 0·4 1·1 0·1 4·3 0·2 45·3

432. Richmond (Kew Observatory): Hr (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + hr (height of receiving surface above ground) = 5.5 metres + 0.53 metres.

May, 1923.

							01 16	ceivi	ng su	Hace	abov	c gro	und	— o .	) met	162 4	- 0.53	) IIICC	105.						ay, 19	
Day.	0-1	I-2	2-3	3-4	4-5	5–6	6-7	7-8	8-9	9–10	10-11	11-12	12–13	13–14	14-15	15–16	16–17	17~18	18–19	19-20	20-21	21-22	22-23	23-24	0-24	Dura- tion.
	l		l			-					mm		mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	0-24 hr.
1	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.														
2						• • • • • • • • • • • • • • • • • • • •		•••						•••	•••			•••			•••	<b></b>	.1		0·I 2·6	0.3
3		•••		2.3	.3	•••		•••				:::					:::			:::					2.0	1.1
4 5	:::		:::	:::			:::						:::												0.1	0.1
			İ							}		1	1		}								}		l	
6	•••		:::				:::						:::	:::	:::			:::							0.4	1.1
8	:::														•••	٠		· · · ·			··· '					
9							•••							•••	•••	•••							:::	7	0.7	0·6 0·7
10										""					• • • • • • • • • • • • • • • • • • • •	•••		'''	'''		'''			1	<u> </u>	
11	.9	•1	•2	.3		•••	•••	•••							·2		···		1.0		•••		•••	•••	3.6	2.4
12	:::	:::			1.2				:::			1.0				1.5				:::					2.7	2.8
13 14																		•••								
15				•••	•••			•••	.3		.1	•••	1.2	1.6	•6	•3	•••	•••	.3	.9	. •2	.3	.1		5.8	3.9
16	<b> </b>	<b> </b>					l		•4			·r		.5	•2		٠ı								1.3	1.2
17						•••	· 1	•••			• 2	•••		•••	•••	•••	•••	•••	•••		•••	•••	•••	•••	0.3	0.2
18				:::	:::			•••			:::							•••								:::
19 20								•••										•••				•••				
																							• • •			
21 22		:::				:::	•1		:::														•2		1.6	1.7
23							•••	•••		•••	.9	·ı	3.7	•4	4.2	1.6	•2	.1	•2	•6	.5	•••		•••	12.5	7.0
24 25	•••									•••			:::							•••	•••	•••			0.2	0.8
25	•••		'''			•	-																			
26	•••	•••		•••	···	··· (·7)	•••		•••	•••			•••				:::					• • • • •	•••	•••	o·8	I.0
27 28			· I							1.6	•4						•••		1.1	3.3	1.3	·I	.3	•3	8.8	7.1
29	1.2	1.4	1.2	.3	.1	•••		•••	•••	.7	• 2	.3	•4	•2	.1	.5	·I	•••					· I	•••	7.4	9.9
30	•••	•••		•••	•••					•••	•••	•••		•••	•••		•••									
31				•••				•••	•••	•••	•••		•••	•••	•••	•••	•••	•••	•••	•••	•••	•••		•••		
Sum.	2 · I	1.8	1.6	3.8	1.7	1.0	0.3	o·8	0.6	2.4	1.8	1.5	6.1	2.8	5.7	3.6	0.5	0.8	2.9	4.8	1.7	1.5	1.4	1.1	52.3	44.7
Total	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	
	- 1			,	- 1											3·1	1.7	0.8	1.9	2.6	1.8	1.2	3.3	2.0	44.7	1
Dura-	2.0	2.1	1.4	2.2	1.8	1.4	1.3	0.7	0.6	1.7	1.9	1.1	2.4	3.0	2.2	3 -	- /			2 0	. 0		00	20	77 /	
tion.	2.0	2.1	1.4	2.2	1.8	1.4	1.5	0.4	0.0	1.7	1.9	1-1	2.4	3.0	2.2	3 -	- /		- 9	2 0		1 2	0.0		<u> </u>	_
						itory)								3.0	2.2	3 2	- /		- 9			1 2			10, 19	23.
tion.		hmon	d (Ke	w Ob	serva		: Hr	= 5	5 me					mm.	mm.		1	mm.	mm.		mm.	mm.	mm.		ne, 19:	hr.
433.	Rick	hmon	d (Ke	mm.	mm.	mm.	: Hr	= 5 · mm.	5 me	etres -	+ 0 · ;	53 me mm.	tres.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	Jur mm.	mm.	hr.
433.	Ric	hmon	d (Ke	w Ob	mm.	ntory)	: Hr	= 5°	5 me	tres -	+ o·:	53 me	tres.	mm.		mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	Jur	mm.   	hr. 
433.	Rick	hmon	d (Ke	mm.	mm.	mm.	: Hr	= 5 · mm.	5 me	mm.	+ 0 · ;	53 me mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm. 	mm.	Jur mm. 	mm	hr.   o·5
433.  I 2 3	Ricl	hmon mm.	d (Ke	mm.	mm.	mm. 	: Hr	= 5: mm. 	5 me	mm.	+ o·:	53 me mm. 	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm. 	mm.	Jur mm. 	mm.   	hr. 
433. I 2 3 4	Ricl	hmon mm.  	mm	mm.	mm	mm.  	: Hr	= 5 · mm	5 me	mm.	+ o·:	53 me mm.  	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm. 	mm	Jur mm. 	mm  o·2 	hr.   o·5 
433.  1 2 3 4 5 6 7	Ricl	mm.	mm	mm	mm.	mm	: Hr	= 5°	*5 me	mm	+ o·:	53 me mm.  	mm.	mm.	mm.	mm.	mm	mm.	mm	mm	mm.	mm	mm	Jur mm	mm	hr.   o·5
1 2 3 4 5 6 7 8	Ricl	mm.	mm	mm	mm.	mm	: Hr	= 5· mm 	*5 me	mm.	+ 0 · ;	53 me mm. 	mm.	mm.	mm.	mm.	mm	mm.	mm.	mm.	mm.	mm	mm	Jur mm. 	mm o·2 o·1	hr.   o·5 
433.  1 2 3 4 5 6 7	mm	mm	mm	mm	mm.	mm	: Hr	= 5· mm.   	mm.	mm.	+ o · ;	53 me	mm.	mm	mm	mm.	mm.	mm.	mm.	mm.	mm. [	mm.	mm	Jur mm	mm o·2 o·1	hr o·5 o·1
433. 1 2 3 4 5 6 7 8 9 10	Ricl mm	hmon mm.	d (Ke	mm	mm.	mm	: Hr	= 5· mm.   	mm.	mm.	+ o · ;	53 me mm 	mm.	mm	mm	mm.	mm.	mm.	mm.	mm.	mm. [	mm	mm	Jur mm	o·1	hr o·5 o·1
433. 1 2 3 4 5 6 7 8 9	Ricl	mm	mm	mm.	mm.	mm	: Hr	= 5· mm	mm	mm	+ o · : mm	53 me mm	mm	mm.	mm	mm.	mm.	mm.	mm	mm.	mm.	mm	mm	Jur mm	mm	hr o·5 o·1
1 2 3 4 5 6 7 8 9 10 11 12 13	Ricl mm	mm	d (Ke	mm.	mm	mm	: Hr	= 5· mm.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         .	5 me mm.	mm	+ o ·	53 me mm	mm	mm.	mm	mm.	mm.	mm.	mm	mm.	mm.	mm	mm	Jur mm	o·1	hr
1 2 3 4 5 6 7 8 9 10 11 12 13 14	Ricl mm	hmon mm	mm	mm	mm	mm	: Hr	= 5·mm.	5 me mm	mm.	+ o · : mm	53 me mm	mm	mm.	mm.	mm.	mm	mm	mm	mm.	mm.	mm	mm	Jur mm	o·1	hr o·5 o·1 i·5
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	Ricl mm	hmon mm	d (Ke	mm	mm	mm	: Hr	= 5· mm	mm	mm	+ o · :	53 me	mm	mm	mm	mm.	mm	mm.	mm.	mm	mm.	mm	mm	Jur mm	o·1	hr
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	Ricl mm	hmon mm	d (Kemm.)	mm	mm	mm	: Hr	= 5· mm.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         .	mm	mm	+ o · :	53 me mm	mm	mm.	mm	mm.	mm.	mm.	mm.	mm.	mm	mm	mm	Jur mm	o·1	hr o·5
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	Ricl mm	mm	d (Kemm	mm	mm	mm	: Hr	= 5· mm	*5 me  mm	mm	+ o · · · · · · · · · · · · · · · · · ·	53 me mm	mm	mm	mm	mm.	mm	mm.	mm.	mm.	mm.	mm	mm	Jur mm	o·1	hr o·5
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	Ricl mm	mm	d (Kemm		mm	mm	: Hr	= 5· mm		mm	mm	53 me mm	mm	mm	mm	mm	mm	mm.	mm.	mm.	mm	mm	mm	Jur mm	o·1	hr o·5 o·1 i.5 2·5
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	Ricl mm	hmon mm	d (Kemm.)	mm	mm	mm	: Hr	= 5· mm	*5 me  mm	mm	+ o · · · · · · · · · · · · · · · · · ·	53 me mm	mm	mm	mm	mm.	mm	mm.	mm.	mm.	mm	mm	mm	Jur mm	mm	hr o·5
1 2 3 4 5 5 6 7 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	Ricl mm	hmon mm	d (Kemm.)	mm	mm	mm	: Hr mm	= 5· mm	5 me	mm	+ o·:	53 me mm	mm	mm	mm	mm.	mm	mm.	mm	mm.	mm	mm	mm	Jur mm	o·1	hr o·5 o·1 i.5 2·5 o·5 i.2
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	Ricl mm	hmon mm	d (Kemm	mm	mm	mm	: Hr mm	= 5· mm		mm	mm	53 me mm	etres. mm	mm	mm	mm.	mm	mm.	mm	mm.	mm	mm	mm	Jur mm	o·1 2·5	hr o·5 2·5
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	Ricl mm	hmon mm	d (Kemm.)	mm	mm	mm	: Hr mm	= 5· mm		mm	mm	53 me mm	etres. mm	mm	mm	mm	mm	mm.	mm	mm.	mm.	mm	mm	Jur mm	o·1	hr o·5 2·5
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	Ricl mm	hmon mm	d (Kemm	mm	mm	mm	: Hr mm	= 5· mm		mm	mm	53 me mm	mm	mm	mm	mm.	mm	mm.	mm	mm.	mm	mm	mm	Jur mm	o·1 2·5	hr
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	Ricl mm	mm	d (Kemm	mm	mm	mm	: Hr mm	= 5· mm		mm	mm	53 me mm	mm	mm	mm	mm	mm	mm.	mm	mm.	mm	mm	mm	Jur mm	o·1	hr
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	Ricl mm	hmon mm	d (Kemm	mm	mm	mm	: Hr mm	= 5· mm.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         .		mm		53 me mm	mm	mm	mm	mm	mm	mm.	mm	mm.	mm	mm	mm	Jur mm	o·1 2·5	hr
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	Ricl mm	hmon mm	d (Kemm	mm	mm	mm	: Hr mm	== 5· mm		mm	mm	53 me mm	mm	mm	mm	mm	mm	mm.	mm	mm.	mm	mm	mm	Jur mm	o·1	hr
1 2 3 4 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	Ricl mm	mm	d (Kemm	mm	mm	mm	: Hr mm	= 5· mm	5 me mm	mm	+ o·:	53 me mm	etres. mm	mm	mm	mm	mm	mm.	mm	mm.	mm	mm	mm	Jur mm	ne, 19: mm o·2 o·1 i·2 o·4 i·2 o·4 o·3	hr o·5 o·1 i·5 o·5 i·2 i·7 o·7
1 2 3 4 4 5 6 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	Ricl mm	hmon mm	d (Kemm	mm	mm	mm	: Hr mm	= 5· mm	5 me mm	mm	+ o · : mmm	53 me mm	etres. mm	mm	mm	mm	mm	mm.	mm	mm.	mm	mm	mm	Jur mm	o·1	hr
tion.  433.  1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum.	Ricl mm	hmon mm	d (Kemm.	mm	mm	mm	: Hr mm	= 5· mm		etres - mm		53 me mm	mm	mm	mm	mm	mm	mm.	mm	mm.	mm	mm	mm	Jur mm	ne, 19:  mm 2.5	hr o·5 o·1 i·5 o·5 i·2 i·7 o·7
tion.  433.  1 2 3 4 5 5 6 7 8 8 9 10 11 11 12 11 13 11 14 11 15 16 11 17 18 119 20 21 22 23 24 25 26 27 28 29 30 Sum.  Total Dura-	Ricl mm	hmon mm	d (Kemm	mm	mm	mm	: Hr mm	= 5· mm	5 me mm	mm	+ o·:	53 me mm	mm	mm	mm	mm	mm	mm.	mm	mm.	mm	mm	mm	Jur mm	0·1	hr o·5 o·1 i·5 o·5 i·2 i·7 o·7
tion.   433.   1   2   3   4   5   5   6   6   7   8   9   10   11   12   13   14   15   16   17   18   19   20   21   22   23   24   25   26   27   28   29   30   Sum.   Total	Ricl mm	hmon  mm	d (Kemm	mm	mm	mm	: Hr mm	= 5· mm	5 me mm	mm	mm	53 me mm	mm	mm	mm	mm	mm	mm	mm	mm.	mm	mm	mm	Jur mm	o·1  1·2  2·5  o·4 1·2  o·4 0·3  i·  f·4 hr.  hr.	hr o·5 o·1 i·5 o·5 i·2 i·7 o·7

434. Richmond (Kew Observatory): Hr (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) + hr (height of receiving surface above ground) = 5.5 metres + 0.53 metres.

July, 1923.

									8 54-	<u> acc</u>	10010	0-0-				res +	- 55								iy, 19	
Day.	0-I	1-2	2-3	3-4	4-5	5–6	6-7	7-8	8-9	9–10	10–11	11-12	12–13	13-14	14–15	1516	16-17	17–18	18–19	19–20	20–21	21-22	22-23	23-24	0-24	Dura tion 0-2.
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	hr.
1	•••	•••		•••			• • • • • • • • • • • • • • • • • • • •			•••	•••		•••	•••				•••			…					
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9		:::	:::		:::	:::	:::											•••	•••				5.2	23.2	28.7	1.5
10	4.1	6.5	6∙1	6.5	•2	<b></b>		1.6	1.7	•••				•••		•••	•••	•••	2.1	.1	.8		•••	•••	29.7	6.2
II		<b></b>				<b> </b>		<b></b>																		
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15											• • • •	•••		•••	•••		•••	•••	•••	•••		.1	•••	•••	0.1	0.2
16	l <b>.</b>		<b></b>	<b></b>					.3	.5		<b></b>													0.8	0.
17														•••		⋅8	•••	•••	• 4	:::				:::	0.3	0.8
18								:::		:::	:::			•4						•2				•••	1.0	1
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21			l		l		l	l	<b> </b>						<b> </b>											
22															1.1	···		•••		···					 1·6	2.
23 24					:::	:::												•••								<b> </b>
25									•••	•••			1 · 1	.7	• 5	1.3	• 1	•••	•••				•••		3.6	2.
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27									•••								•••	•••	···					1 :::	3.0	1
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30		1.0	•2								•••	\ ··· '	•••	•••		•6	•••	•••				1.4	1.9	1.3	6.4	3.
<b>3</b> 1						<b></b>									•2	.9	1.1	1.3	2.0	•2					5.7	4.
Sum.	4.4	7.5	6.3	6.8	0.2			1.6	2.0	0.2	0.1	1.1	1.4	1.1	3.4	3.6	1.2	1.3	4.2	0.6	1.1	1.5	7.9	2 <b>4</b> ·8	82.9	25.
Total	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	
Dura-	1.2	1.7	1.6	1.3	0.2			0.2	0.2	0.3	0.1	1.2	0∙8	1.4	1.6	2.6	1.0	1.0	1.5	o·8	1.8	1.2	1.4	1.6	25.5	
tion.	<u> </u>		·	-	!	<u> </u>	1	<u> </u>				!!					·····	· · · · · ·			·	<u> </u>				
435.	Ric	hmor	id (K	ow Ol	bserva	atory)	: H	r = 5	·5 m	etres	+ 0.	53 me	etres.											Augu	st, 19	23.
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	hr.
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7 8	•••		1		i	1	1	1	• • • • • • • • • • • • • • • • • • • •	•••				•••	•••	•••	ì	l		[					:::	
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10 11 12 13 14 15 16 17 18 19 20 21 22 23 24								   2.0	       4.5	1-1		     	     3.4 	     		     			       	     					    2·3  2·6 6·8 	
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10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25								   2.0	        4.5	1-1		      	    3.4  			    		       	       	       2·1				     	   2.3  2.6 6.8   6.9 7.0 o.1	      6. 2.
10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25								2.0	         	   		      	       	     					      	      					    2·3  2·6 6·8    6·9 7·0 o·1 4·1 	
10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29								   2.0	       4.5	     		      				         	         	         	       				      		    2.3  2.6 6.8    6.9 7.0 0.1 4.1  9.5	
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10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Sum.								   2-0		     		        	    3.4     			         			         		···			     	   2·3  2·6 6·8   6·9 7·0 o·1 4·1  9·5	
10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30								  2.0  		   		      					         		      						   2·3  2·6 6·8   6·9 7·0 o·1 4·1  9·5 	

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### RAINFALL.

Amounts, in millimetres, for periods of sixty minutes, between the exact hours, Greenwich Mean Time.

436. Richmond (Kew Observatory):  $H_r$  (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) +  $h_r$  (height of receiving surface above ground) = 5.5 metres + 0.53 metres. September, 1923.

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Day	. 0-1	I-2	2-3	3-4	4-5	5-6	6-7	7-8	8-9	9–10	10-11	11-1:	2 12-1	3 13-14	14-15	15–16	16-17	17–18	18-19	19–20	20-21	21-22	22-23	3 23-2	4 0-2.	tion
	- mm	mm	- mm	$-\frac{1}{mm}$	mm	_ <u>mm</u>		mm.		mm.	mm.	mm.		<u>mm.</u>	- mm	mm.		- mm	mm.	mm		mm.	mm.	$-{mm}$		0-24 hr.
I	11111		·   · · · · · ·								•3	1.3			mm.		mm.	mm.		mm.	mm.				1.6	
2		•••																								
3			•••						T.7	1.0		1						•••			•••	•••		•••	1 :::	2.5
4 5	:::			:::	:::	:::		:::	1.7	1		1.3	:::			:::		:::	:::	:::	:::			:::	4.5	3.2
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15				***			•••	•••		•••	•••	•••		•2	.4	•5	.1	.1	•••	***		•••	•••		1.3	2.2
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23			2						.4	.7						7	.7	3		1		2		•••	3.1	3.3
24		•••					•••		'								'					1.2	I O	•••	2.5	2.1
25	.5	• 5	•4	•4	•••		•••		•••		•••		.7	•••	•••		•••	•••		•••	•••	••• [		•••	2.2	3.3
26																								•••	<b> </b>	
27																								•••		
28			•••	•••	•••		•••	•••	•••	•••	•••		•••			•••	•••	•••		•••	***	•••		•••		
30	:::																***							•••	:	•••
	<b> </b>													-						-					<u> </u>	
Sum.	3.6	1.1	2.2	2.3	0.9				2.1	1.8	1.0	2.8	0.7	1.1	I · I	1.9	0.0	0.7	1.0	5.2	0.7	1.4	1.4	o·8	35.0	27.9
Total	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	
Dura-	1.8	2.0	2.4	1.6	1.3						1	1.7	0.3	0.9			0.7	1	1.3	1		1.4	1.3		27.9	
tion.																			<u>.                                     </u>							L
437.	Ric	hmon	d /Ka	w Oh	sarva	tory)	: H.	5.	s mei	tres J	- 0.5	2 me	tres										O	ctoh	er 19	23
437.							: Hr	<del></del>						T				T							er, 19	
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.   1	mm.	mm.	mm.	mm.				1	- 1	1			l	mm.	mm.	mm.	hr.
437.								<del></del>						mm.	mm.   1	mm.	mm.	mm.	mm.    1·2	mm.   1	mm.   1	mm.				hr. 1·4 2·2
1	mm.	mm.	mm. 	mm.	mm.	mm.	mm.	mm.	mm.   1	mm. 1	mm.	mm.	mm.					•••				•••	mm.	mm. 	mm. 0·7	hr.
I 2 3 4	mm.	mm.	mm.  .2 	mm.	mm.	mm.	mm.	mm.	mm.   1	mm. 1	mm.   1	mm.  I·2	mm. • I  3• I	 (3·7)	 (3·7)	·2  (3·7)	3.7)	(3 · 7)	 1·2 ·4 	 I·I ·2 	• 2		mm.	mm.	mm.  0·7  2·7  23·5	hr. 1 · 4 2 · 2 8 · 3
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1 2 3 4 5 6	mm.	mm.	mm.  .2 	mm.	mm.	mm.	mm.	mm.	mm.   1	mm. 1	mm.   1	mm.  I·2	mm. • I  3• I	 (3·7)	 (3·7)	·2  (3·7)	3.7)	(3 · 7)	 1·2 ·4 	 I·I ·2 			mm.	mm.	mm. 0·7 2·7 23·5 1·5	hr. 1 · 4 2 · 2 8 · 3 2 · 7
1 2 3 4 5 6 7	mm	mm.	mm	mm.	mm.	mm.	mm.   1	mm.	mm.   1	mm. 1	mm.   1	mm.	mm. • I  3• I 	.3 (3·7) 	(3 · 7)	·2 (3·7) ···	 (3·7) 	(3 · 7)	 I·2 ·4 	 I·I ·2 			mm	mm	mm. 0·7 2·7 23·5 1·5 9·2	hr. 1 · 4 2 · 2 8 · 3 2 · 7 3 · 9
1 2 3 4 5 6 7 8	mm	mm.	mm	mm.	mm.	mm.	mm.   1	mm.	mm.   1	mm. 1	mm.   1	mm.  I·2 	mm. • I  3• I 	.3 (3·7) 	(3·7) (3·7) 	·2 (3·7) ···	 (3·7)  	(3·7)	··· 1 · 2 · · · · · · · · · · · · · · ·	 I·I ·2 			mm.	mm 1.3	mm. 0·7 2·7 23·5 1·5 9·2 6·2	hr. 1 · 4 2 · 2 8 · 3 2 · 7 3 · 9 4 · 8
1 2 3 4 5 6 7	mm	mm	mm	mm	mm.	mm.	mm.	mm.	mm.   1	mm. 1	mm. 1	mm.	mm: 3.1	.3 (3·7) 	(3·7) ( (	·2 (3·7) 	 (3·7) 	 (3·7) 	 I·2 ·4 	 I·I ·2 	 ·2   2·9 ·5	  2.9 2.0	mm 2·1 2·5	mm	mm. 0·7 2·7 23·5 1·5 9·2	hr. 1 · 4 2 · 2 8 · 3 2 · 7 3 · 9
1 2 3 4 5 6 7 8 9 10	mm	mm	mm ·2 ·1	mm	mm	mm	mm.   1	mm.	mm. 1	mm. 1	mm. 1	mm I·2	mm1 3.1	(3 · 7)	(3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7) (3·7)	(3.7) (	 (3·7) (  	(3·7)	 1·2 ·4   	 I·I ·2   	    2.9 .5	   2·9 2·0	mm	mm	mm. 0·7 2·7 23·5 1·5 9·2 6·2 2·5 1·0	hr. 1·4 2·2 8·3 2·7 3·9 4·8 1·4 2·3
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Richmond (Kew Observatory):  $H_r$  (height of receiving surface above M.S.L.) = H (height of station above M.S.L.) +  $h_r$  (height 438. of receiving surface above ground) = 5.5 metres + 0.53 metres. November, 1923.

Amounts, in millimetres, for periods of sixty minutes, between the exact hours, Greenwich Mean Time.

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Day.	0-1	1-2	2-3	3-4	45	5-6	6-7	7-8	89	9-10	10-11	11–12	12-13	13-14	14-15	15–16	16-17	17–18	18–19	19-20	20-21	21-22	22–23	23-24	0-24	
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Sum.	0.7	1.3	2.4	2.2		3.6	0.4	0.1		0.8	1.5	1.2	0.6	3.1			0.9	1.2	3.6	3.0	1.4	3.1	4.3	1.9	37.3	28.9
Total	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	
Dura-	0.0	1.9	1.7	2.0	•••	o.6	0.3			0.6	1.0	1.7	1.1	0.3			0.9	1.9	3.0	2.3	2.5	2.5	2.0		28.9	
tion.		1	1	١ .		1		1 1							<u>'</u>		· · · · ·					<u> </u>	<u></u>	<del>'</del>	<u>.                                    </u>	-
400	<b>D</b> :		. 1 /1/			_4	. TT			. L													Dag	ram ha	ar 19	73
439.			<u>`</u> _						·5 m						mm	mm I	mm l	mm I	mm J	mm l	mm	mm		mm.		
439.	mm.	hmor	mm.	mm.		atory)	mm.	r = 5	mm.	mm.	+ o·		mm.	mm.	mm. 	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	hr.
I 2	mm. 	mm.	mm.	mm. 	mm. 	mm.	mm. 	mm. 	mm.	mm. 	mm. 	mm. 	mm.	mm. 					1				mm.	mm.	mm.	hr.
1 2 3 4	mm.	mm.	mm.	mm.	mm.	mm.	mm. • 1 • 1	mm.  .9 	mm.  .2  .4	mm.  .8  I·o	mm.  	mm.	mm.	mm.		···	 	·2  					mm.	mm.  	mm. 0·2 2·4 0·1 1·9	hr. 0·1 3·5  2·2
I 2	mm. 	mm.	mm.	mm. 	mm.	mm.	mm. • · · · · · · · · · · · · · · · · · · ·	mm.  .9	mm.  .2	mm.  .8	mm.  	mm. 	mm.	mm. 		•••		·2 		•••			mm.	mm.	mm. 0·2 2·4 0·1	hr. 0·1 3·5
1 2 3 4 5	mm.	mm.	mm.	mm3	mm.	mm.	mm11	mm91	mm2	mm8 I.0	mm.	mm.	mm.	mm.		···	 	·2  					mm.	mm.  	mm. 0·2 2·4 0·1 1·9	hr. 0·1 3·5  2·2
1 2 3 4 5 6 7 8	mm.	mm.	mm.	mm.  .3 	mm.	mm.	mm11	mm91	mm24	mm.  .8  I·o	mm.  .1	mm.	mm.	mm		···	 	·2	  	 			mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5	hr. 0·1 3·5 2·2 0·1 3·2 1·3
1 2 3 4 5	mm.	mm.	mm.	mm	mm.	mm.	mm11	mm91	mm24	mm8 1.0	mm.	mm.	mm.	mm.		  	  	·2	 				mm.	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2	hr. 0·1 3·5 2·2 0·1 3·2
1 2 3 4 5 6 7 8 9	mm.	mm.	mm	mm ·3	mm.	mm.	mm11	mm9	mm ·2 ·4	mm ·8 I·0 ·1 ·1 ·	mm	mm.	mm	mm		    	   	·2	  	   I·I			mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5	hr. 0·1 3·5 2·2 0·1 3·2 1·3
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1 2 3 4 5 5 6 7 8 9 10 11 12 13	mm	mm	mm,	mm · · · · · · · · · · · · · · · ·	mm.	mm.	mm11	mm9	mm ·2 ·4	mm8 I · o	mm	mm.	mm	mm		     	   	·2	  	    	     		mm.	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5 0·1	hr. 0·1 3·5 2·2 0·1 3·2 1·3 0·4
1 2 3 4 5 6 7 8 9 10 11 12	mm	mm	mm	mm	mm.	mm	mm11	mm	mm24	mm	mm	mm.	mm	mm		      	    	·2		     	     		mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5 0·1 0·3 0·3	hr. 0·1 3·5 2·2 0·1 3·2 1·3 0·4 0·7 0·6
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16	mm	mm.	mm	mm3	mm.	mm	mm1	mm	mm ·2 · ·4 · · · · · · · ·	mm8 I·o	mm	mm	mm	mm		··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··		·2	   	     			mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5 0·1 0·3 0·3	hr. 0·1 3·5 2·2 0·1 3·2 1·3 0·4 0·7 0·6
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	mm	mm.	mm	mm	mm.	mm.	mm11	mm	mm ·2 ·4 ·	mm	mm	mm	mm	mm		     	    	·2 ··· ··· ··· ··· ··· ··· ··· ··· ···		    			mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5 0·1 0·3 0·3	hr. 0·1 3·5 2·2 0·1 3·2 1·3 0·4 0·7 0·6
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	mm	mm.	mm	mm		mm.	mm11	mm9	mm ·2 ·4 · · · · · · ·	mm	mm	mm	mm.	mm		   	      	·2		    	      		mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5 0·1 0·3 0·3	hr. o·1 3·5 2·2 o·1 3·2 I·3 o·4 o·7 o·6
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	mm	mm	mm.	mm		mm.	mm11	mm	mm ·2 ·4 ·	mm8 I·o	mm	mm.	mm	mm		   	     	·2	   	    	      		mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5 0·1 0·3 0·3 2·4	hr. o·1 3·5 2·2 o·1 3·2 I·3 o·4 o·7 o·6 o·7
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	mm	mm.	mm	mm		mm.	mm11	mm	mm ·2 ·4 · ·	mm	mm	mm	mm.	mm		   	      	·2		    	      		mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5 0·1 0·3 0·3 2·4	hr. 0·1 3·5 2·2 0·1 3·2 1·3 0·4 0·7 0·6 0·7 11·2 2·3
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	mm	mm.	mm	mm		mm.	mm1	mm9	mm ·2 ·4 · ·	mm	mm	mm	mm	mm				·2	    	      	         		mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5 0·1 0·3 0·3 2·4	hr. o·1 3·5 2·2 o·1 3·2 I·3 o·4 o·7 o·6 o·7 iii·2 2·3 o·1
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	mm	mm.	mm	mm	mm.	mm.	mm1	mm	mm ·2 ·4 ·	mm8 I·o	mm	mm	mm.	mm				·2		       	         		mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5 0·1 0·3 0·3 2·4 5·0 1·7 0·1	hr. 0·1 3·5 2·2 0·1 3·2 1·3 0·4 0·7 0·6 0·7 11·2 2·3
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	mm	mm.	mm	mm	mm.	mm.	mm	mm	mm ·2 ·4	mm	mm	mm	mm	mm				·2		        			mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5 0·1 0·3 0·3 2·4 5·0 1·7 0·1 1·9 10·2 3·1	hr. o·1 3·5 2·2 o·1 3·2 1·3 o·4 o·7 o·6 o·7 11·2 2·3 o·1 3·8 5·1 3·1
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 2i 22 23 24 25 26 27	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm				·2		         	         		mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5 0·1 0·3 0·3 2·4 5·0 1·7 0·1 1·9 10·2	hr. o·1 3·5 2·2 o·1 3·2 1·3 o·4 o·7 o·6 o·7 11·2 2·3 o·1 3·8 5·1
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm				·2					mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5 0·1 0·3 0·3 2·4 5·0 1·7 0·1 1·9 10·2 3·1 6·0 0·6	hr. o·1 3·5 2·2 o·1 3·2 1·3 o·4 o·7 o·6 o·7 11·2 2·3 o·1 3·1 6·8 2·8 1·1
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	mm	mm	mm	mm	mm	mm	mm	mm	mm ·2 ·4	mm	mm	mm	mm	mm				·2					mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·3 0·1 0·3 0·3 2·4 5·0 1·7 0·1 1·9 10·2 3·1 6·0 1·9 0·6 8·5	hr. o·1 3·5 2·2 o·1 o·4 o·7 o·6 o·7 o·7 11·2 2·3 o·1 3·8 5·1 3·1 6·8 2·8 1·1 12·1
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm				·2					mm	mm	mm.  0·2  2·4  0·1  1·9  0·3  0·3    2·4   5·0  1·7  1·9  10·2  3·1  6·0  8·5  1·7	hr. o·1 3·5 2·2 o·1 3·2 1·3 o·4 o·7 o·6 o·7 il·2 2·3 o·1 3·8 5·1 3·1 6·8 2·8 1·1 12·1 3·9
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm				·2					mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 0·3 0·3 0·3 0·3 0·1 0·1 1·7 1·9 10·2 3·1 6·0 1·9 10·2 1·7 52·2	hr. o·1 3·5 2·2 o·1 o·4 o·7 o·6 o·7 o·7 11·2 2·3 o·1 3·8 5·1 3·1 6·8 2·8 1·1 12·1
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Sum. Total.	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm8 I·o	mm	mm	mm	mm				·2					mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·5 0·1 0·3 0·3 2·4 5·0 1·7 0·1 1·9 0·6 8·5 1·7	hr. o·1 3·5 2·2 o·1 3·2 1·3 o·4 o·7 o·6 o·7 il·2 2·3 o·1 3·8 5·1 3·1 6·8 2·8 1·1 12·1 3·9
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Sum.	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm				·2		        3.3			mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 3·2 0·3 0·1 2·4 5·0 1·7 0·1 1·9 10·2 3·1 6·0 1·9 0·6 8·5 1·7 52·2 hr.	hr. o·1 3·5 2·2 o·1 3·2 1·3 o·4 o·7 o·6 o·7 il·2 2·3 o·1 3·8 5·1 3·1 6·8 2·8 1·1 12·1 3·9
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 Sum.  Total. Dura-	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm8 I·o	mm	mm	mm	mm				·2					mm	mm	mm. 0·2 2·4 0·1 1·9 0·1 0·3 0·3 0·3 0·3 0·1 1·7 0·1 1·9 10·2 3·1 6·0 1·7 52·2 hr. 65·1	hr.  0·1  3·5   2·2  0·1   3·2  1·3   0·4  0·7  0·6    0·7   11·2  2·3  0·1  3·8  5·1  3·1  6·8  2·8  1·1  12·1  3·9  65·1

# DURATION OF BRIGHT SUNSHINE.

For periods of sixty minutes, between the exact hours, of Local Apparent Time.

440. Richmond (Kew Observatory):  $h_s$  (Height of recorder above ground) =  $13 \cdot 3$  metres.

January, 1923.

440.	Ric	hmor	nd (K	ew O	bserv	atory/	<b>y</b> ) : r	ls (H	eigni	OI IC	corde	er ab	ove §	groun	$a_j =$	13.3	, mei	ics.			`	Junuu y	, 1923.
Days.	3 to	4 to	5 to	6 to		8 to	9 to	10 to	II to	Noon	13 to				17 to	18 to	19 to	20 to		Per cent.	Angströ	adiation, m Pyrhel	iometer.
	4.	5.	6.	7.	8.	9.	IO.	II.	Noon	to 13.	14.	15.	16.	17.	18.	19.	20.	21.	for Day.	of Possible.	Sky.	Total.	Vertical.
ī	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr. •8	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr. 3·1	% 39 	Mist	mw/cm ² 31·8	mw/cm ²   8 
3 4	=				<u> </u>		··· ··2	1·0 '4	··9 ·7		··· ·5 ·2 ·1	·1		=	_	_	=		3·5 2·9 ·1	44 37 1	Clear	33.2	 9 
6	_	_	_	_	=	·1	7	I.0	I.0	1.0	I.O	1·o	···	_	_	_	_	_	5.9	74 	Clear	55 9	15
8 9 10					=				··· ·1 ·7	·	 •5 	 I·0 ·2			=			=	1.0 1.0	20 12	 Clear	 52·9	  15
11 12	_	=	_	=	-		·8 ·5	1.0	I.0 I.0	I.O I.O	'4 1·0	1.0			_	_	_	_	5·5	63 67 	Clear	55·4 	16 
13 14 15	=	=	=	_					··· ··2 ···			··· ·2 ···			_ _	_	_	=	o∙6 	7 			•••
16 17 18	=	_	_	_						  .8	 				_		_	_	 1·9	  23	 Mist	 22·0	  7
19	=	=	_	_	:::			·		 4	·ī ·7	··8			_	_	_	_	0·I 2·0	1 24	•••	•••	
2I 22 23	=	_				•••	·6 	1.0 1.0	I.0 I.0	 ¹7 1∙0	I.0 I.0	I.0 I.0	 .5		_	_	_	=	0·8 4·7 <b>6·7</b>	9 55 <b>78</b>	 Clear	 53·7	 17
24 25	_	_	=	=		•2	••5					•••	•••		_		_	_	1.0	11	•••	•••	
26 27 28											···				_	_	_	=	0·I		•••	•••	•••
29 30 31	  -	_	_	_				·4 	·4						_	_	_		o·8	9 · 10			
Sum.	_				0.0	0.5	5.0	8.3	9.4	8.4	8.2	7.8	0.7	0.0					48.3				
	<b> </b> -				0.00				0.30										1.56	19			
Mean	<u> </u>			<u> </u>	0.00	0.02	0 10	0 27	0 00	0 2/1	0 20	0 25	0 02	0 00									<u> </u>
441.	Ricl	hmon	d (K	ew O	bserv	atory	(): h		13.3	metr							<del></del>			. o/ I	Fo	bruary,	
I	hr.	hr.	hr. —	hr.	hr.	hr.	hr.	hr. 	hr.	hr.	hr. 	hr.	hr.	hr.	hr.	hr.	hr. —	hr. —	hr.	% 		•••	<b>mw</b> /cm ²
2	_		_	_						 •9	···	•••			_	_	_	_	 2·9	 32	Clear	 51·4	19
3 4 5	_	-	_	_		·5 ···	·6	I.0 I.0	I.0 I.0	·6	·8 ·9	.7 .8	.4 •1		_	_	_		6·3 5·0	<b>68</b> 54	Clear	57·o	22
6 7 8	=	=	=	=		·8 	·7 	··ı		·6 		•1	•••		_	_	=	_	0.1 5.0	31 1	•••	•••	
8 9 10	=	=	_	=				··· ·4 ···	 .9	 1·0	 •9	 1·0	··· ··7 ···					_	4·9 	52 	Mist	42·8 	17 
11 12	_	_	_	_		·9	1.0	·8 ·7	·2 ·3	·4 	··9	·6 	·7 ···	·2 	_	-	111	_	5.7 1.0	59 10 2	•••	•••	
13 14 15	=		=	=						 :4	·1	•••			_		_	_	 0·5	 5		•••	
16 17 18	<u></u>	=	=	<u></u>	···	 1.0	1·0 ·9	1·0 ·8	···	··· ·4	 ·8	···	 •1 •4		_	_			2·3 5·5 0·4	23 55 4	Clear	 70·3	31 
19	_		-													_	_	_	•••		•••	•••	•••
20		-			'''																		
20 21 22 23					···		1.0	·3 ·8 ···	·3 ·4	·	  .8	 3	·4  ·9			=		_	1·3 2·5 2·8	13 24 27		•••	•••
2I 22	_	_			·		1·0	·3 ·8	·3 ·4			•••					_		2.5	24	•••	•••	
21 22 23 24 25 26 27					···	 ·2   	 I.0	·3 ·8 ··· ··· ··· ···	·3 ·4 ··· ··· ·8 ···	··· ·· ·· ·· ·· ·· ··	 .8  	 I·o 	···· ··9 ···· ··2	···					2·5 2·8  0·3 2·0 0·2	24 27  3 19 2	•••	•••	 
21 22 23 24 25 26 27 28					   	2	 I·o   	·3 ·8 ··· ··· ··3 ··· ··· ··· ··· ···	·3 ·4 ··· ··· ·8 ···	··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	 ·8   ·2  ·1	 I·o   	922						2·5 2·8  0·3 2·0	24 27  3	  Clear	  68·1	   34
21 22 23 24 25 26 27 28 Sum.	-			0.0	     7		 I·o     7	·3 ·8 ··· ··· ··3 ··· ·2 <b>8·2</b>	·3 ·4 ··· ··· ·8 ··· ··· 6·9	··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	 .8   .2  .1	 1·0    .9	 ·9  ·2  ·2 4·I	··· ··· ··· ··· ··· ··· ··· ···	···· ··· ··· ···				2·5 2·8  0·3 2·0 0·2 4·1	24 27  3 19 2 38	Clear	68·1	34 
21 22 23 24 25 26 27 28					     7		 I·o     7	3 .8   .3  .2 8.2 0.29	·3 ·4 ··· ··· ·8 ··· ··· 6·9	··· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ·· ··	 .8  .2  .1 5.9	 1·0   .9 5·9	 ·9  ·2  ·2 4·1	0.3 0.01	0.00				2·5 2·8  0·3 2·0 0·2 4·1 50·9	24 27  3 19 2 38	 Clear 	68·1	34 

# DURATION OF BRIGHT SUNSHINE.

For periods of sixty minutes, between the exact hours, of Local Apparent Time.

442. Richmond (Kew Observatory): hs (Height of recorder above ground) = 13.3 metres.

March. 1923.

442.	Rich	mon	d (K	ew Ol	bserv	atory	'): h	s (He	eight	of re	corde	r abo	ve g	roun	d) =	13.3	met	res.				March,	1923.
Day.	3 to	4 to	5 to	6 to	7 to	8 to										18 to			Total	Per cent.	Ra Ångströr	adiation, n Pyrhelio	ometer.
Day.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	to 13.	14.	i5.	16.	17.	18.	19.	20.	21.	for Day.	of Possible.	Sky.	Total.	Vertical.
	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	%		mw/cm ² .	
I	—	<u> </u>	_	•••	···8	I.0	1.0	1·0		·4 ·9	·6 ·4	·5	·5 ·4			_	_	_	2·0 6·7	19 61			
3		=	_	:::			.3	1.0	1.0	1.0	1.0	I .O	1.0	.3		-	-	-	6.6	61	Haze	71.6	37
4									·5			1.0					_	_	5.0	45			
5													1		ı		1	- 1	.2	2		ı	
6 7	=			:::	:::					••5	:::			:::	-::		_	_	.8	7			
8	<b> </b> —		_							•2	•6	•6					_	_	1.4	12			
9 10		_				:::	:::							:::		_	-	-					•••
				j												_	_	_	]				
11 12								1.0		···						-		-	4.0	35	•••		•••
13	-	-	—										:::	:::		_	_	_	-:::				•••
14 15		=	_														-						•••
16	<u> </u>	l						l l	l		·					_ [	_	_					•••
17		_	_							٠ı	1.0	1.0	1.0	.3			_	=1	3.4	29 36			•••
18						••2	···	.4 .8	·9 ·5	.6 1.0	·6 ·6	.7 .1				= $ $	=	_	4·3 3·2	27			
19 20	=	] —	—														- ]	-			•••	•••	•••
21	_		_					.3	.9	1.0	.4	.4				_		-	3.0	25			
22	—	-									}		:::		:::		=	_		- ::: l	•••		•••
23 24	_	_	:::	:::				1.0		1.0	1.0	1.0	1.0	-8			_	-	8.5	69	Haze	54.3	35
25	—				.3	·4	·1		·ı			.4	.2	.6	.5		_	_	2.6	21	•••		•••
26	_	_						.2	-4				.3	·1	·2		-	_	1·2 6·6	10 53	 Clear	98.9	 65
27 28	_				·9 ·4	·4 ·9	·6 ·9	·8   1·0	·9	·8 ·8		I.0 I	1.0			:::	_	_	6.9	55			
29							·3 ·8	•6	٠ĭ	٠6	.5	.3			•••				2·I	17 20	•••	:::	
30			•••		.7	1.0	.0	···	•••	•••				•••	•••								
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Sum.			0.0	0.2	3.2	5.9	6.3	9.3	9.1	10-4	8.1	8.4	7.4	3.8	o·6	0.0	-	—	72.7				
Mean			0.00	0.01	0.10	0.19	0.30	0.30	0.29	0.34	0.26	0.27	0.24	0.13	0.02	0.00			2.35	20			<u> </u>
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2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarria							1.0 2 1.0 2 2 2 3 2 3 3 1.0 1.0 1.0 1.0 1.0 0.33	.3 I.0 .4 I.0	.9 I 0 I 0 2 I 0 2 I 0 3 7 7 7 7 7 8 9 3 I 0 2 I 10 13 3 0 44	.7 1.0 3 1.0 2.8 1.1 3.9 9.9 99.8 55 4.1 1.7 1.0 7.6 1.0 13.5 0.45	.4 1.0 .3 1.0	1·0 ·5 1·0 · 1·0 · 3 9 · · 2 · · · 9 · · 1·0 · 1·0 · 9 · · 9 · 0·32	I · · · · · · · · · · · · · · · · ·	3 -4 -5					2·3 6·4 2·1 9·5 0·3 1·3 9·9 2·7 0·3 0·4 1·2 5·6 8·5 6·7 0·2 6·7 2·4 7·0 12·1 4·7 9·7 9·9 0·6 0·3 118·8 3·96 Total	50 16 73 2 10 74 20 2 3 9 41 62 49 1 48 21 17 50 8 28 85 32 67 68 4 2 29 Per cent	Clear A. st Haze Clear	63·I 74·9	 58  42  42  48  58
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Sum. Mean	3to	    					1.0 2 1.0 2 2 2 3 2 3 3 1.0 1.0 1.0 1.0 1.0 0.33	3 1.0 .4 1.0	.9 I.0 I.0 2 I.0 2 I.0 3 7 7 7 7 8 9 3 I.0 2 I.0 13.3 I.0 II.to	.7 1.0 .3 1.02 .81 .1 .3 .9 .9 .9 .85 .4 .1 .7 1.07 .6 1.0 .4 13.5 0.45	.4 1.0 .3 1.0	1·0 5 1·0 1·0 3 9 2 77 9 6 1·0 1·0 9 6 9 7 0·32	1·0 ·2 1·0 ·2 1·0 · · · · · · · · · ·	3 -4 -5					2·3 6·4 2·1 9·5 0·3 1·3 9·9 2·7 0·3 0·4 1·2 5·6 8·5 6·7 0·2 6·7 2·9 2·4 7·0 12·1 4·7 9·7 9·9 0·6 0·3 118·8 3·96 Total	50 16 73 2 10 74 20 2 3 9 41 62 49 1 48 21 17 50 8 28 85 32 67 68 4 2 — 29  Per cent of	Clear A. st Haze Clear	84·2 84·2 57·8 63·1 74·9 Total.	58
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarrian Summarria							1.0 2 1.0 2 2 3 2 3 3 1.0 1.0 1.0 1.0 1.0 1.0 0.33	3 1.0 .4 1.0	.9 I 0 I 0 2 I 0 2 I 0 3 7 7 7 7 7 8 9 3 I 0 2 I 10 13 3 0 44	.7 1.0 .3 1.02 .81 .1 .3 .9 .9 .9 .85 .4 .1 .7 1.07 .6 1.0 .4 13.5 0.45	.4 1.0 .3 1.0	1·0 ·5 1·0 · 1·0 · 3 9 · · 2 · · · 9 · · 1·0 · 1·0 · 9 · · 9 · 0·32	I · · · · · · · · · · · · · · · · ·	3 -4 -5			        		2·3 6·4 2·1 9·5 0·3 1·3 9·9 2·7 0·3 0·4 1·2 5·6 8·5 6·7 0·2 6·7 2·9 2·4 7·0 12·1 4·7 9·9 0·6 0·3 118·8 3·96 Total for	50 16 73 2 10 74 20 2 3 9 41 62 49 1 48 21 17 50 8 28 85 32 67 68 4 2 — 29  Per cent of	Clear A. st Haze Clear	84·2 84·2 57·8 63·1 74·9	58

### DURATION OF BRIGHT SUNSHINE.

444	D:-L		1/1/			_		_	-										irent T	Cime.		May	1003
444.	Rich	mon	d (K	ew O	bserv	atory	<u>(): h</u>	s (He	eight I	of re	corde	er abo	ove g	roun	$\frac{\mathrm{d}}{\mathrm{l}} =$	13.3	met	res.				may, Radiation	1923.
Day.	3 to	4 to		6 to		8 to	9 to	10 to	II to	Noon	13 to	14 to							Total for	Per cent. of	Ångströ	m Pyrheli	ometer.
	4.	5.	6.	7.	8.	9.	10.	II.	Noon	to 13.	14.	15.	16.	17.	18.	19.	20.	21.		Possible.	Sky.	Total.	Vertical
ı	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr. •6	hr. •9	hr.	hr.	hr.	hr. 3·9	% 26		mw/cm²	mw/cm²
2	-			•4	1.0	1.0	•8	.3	·6 ·6	···	··9	I.0	1.0	·8 ·8	.3	•2		_	9·0 8·3	61 56	Clear	72.4	 59
3 4	-			1.0	1.0	1.0	1.0 .3	1.0	1.0	.7 1.0	1.0	•7	.7	.9	•9	·9			12.2	82	Clear	76.0	62
5	-			1.0	.8			.4	•5	.5	.3	.2	·I	-8	.9	•2	•••	_	5.7	38	•••		•••
6	_				8	1.0	1.0	.9	.8	1·0 5	.0	.8						_	7·3	48 41			
8 9	=			1.0			·.				·1							_	5.6	37	•••		:::
10	-	***		.6					•5	.3	.7	•6	•5	1.0	1.0	.5		_	5.7	37			
11			1.0	1.0	1.0	1.0	.5	·4 ·7	·8 ·4	·8 ·4	·8 ·4	·5 ·7	·4 ·3 ·8	.3	·6 ·9	1.0		_	9·9	59 64	. Clear	78.8	65
13 14	_				:::		.4	·9 ·4	·9	·9	·8 ·9	·7 ·9	·8 ·8	1.0	·8 ·7	·8	 I·	_	7·4 7·7	48 50		:::	•••
15	-		.1	•6	•5	•5	.9	'4	•6	·4	•••	•••	•••	•••	•••	•••	•••	-	4.0	26	•••		•••
16 17	_		I.O		·1		·7	1.0 .7	.4 1.0	·9	·7 ·7	·8	1.0	·5 ·8	·6 ·5	·5 ·4	·2 ·2		8·8 9·2	56 59	Clear Clear	86·3 78·8	73 67
18 19	=	•2	•2			1.0	3	·2	.3	·I	·í							_	3·3 0·4	2I 3		· · · ·	
20	-			.1				.2			٠1							_	0.4	3			•••
2 I 22	_								.2		 ·6	ı.o	·3 ·8	.3	·5	٠1		_	1·4 3·8	9			
23	=	:::						•2	·2		•••			·4 ···				_	0.3	24 2	•••		
24 25	_			1.0	1.0	.I I.0	.I I.0	1.0	·6	1·0	·1	·3 ·8	·7 ·3	·1 ·2	·6	·6		_	4.2	76 28			:::
26	_		.3	1.0	1.0	.6	-8	7	.7	•4	•2	.7	.9	1.0	1.0	•2		_	9.5	59	Clear	74.0	64
27 28	=					8		•••				·8 ···	•••			•••	•••	-	3.1	19 8	•••		
29 30	:::							•2			I.0	 '7	 •5	···	••2				 4·6	 28	 Haze	45.1	 39
31												٠ı		٠ı					0.2	I	•••		
Sum.	0.0	0.3	4.7	9.4	11.4	12.0	12.0	12.1	13.8	14.1	13.8	13.5	13.3	11.6		8.5	0.7	0.0	164.8		_		
Mean	0.00	0.01			0.37			0.39								0.27	0.02	0.00	5.32	34			
445.	Rich	ımon						ıs =												•		June,	1923.
	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	%			mw/cm²
2		•••	•••								•••	•••	•••			•••					•••		
3 4			·2 ·1	·9 ·7	.3	1.0	.I I.O	.3	.I I.0	.1 1.0	.3 1.0	•3	•2				•••	•••	8·4 2·9	52 18			
5		•••	•••	•••					•••	•2	•6	•8	•2	1.0	.7	•••	•••	•••	3.2	21	•••		
6 7 8		•••	•••	•••	••2	·.I		•1	·5	·2	•••	•2							o·8	5 4	•••		
8 9							··I			·6									2.1	13			
10		•••	•••	•••	·2			•••		•6	1.0	1.0	1.0	1.0	1.0	1.0	•4		7.2	44		•••	
11 12		·4 ·6	·9	I.0 I.0	1.0	·6	·2 ·3	•2	·2 ·5	·2 ·2	·8		1.0	·9	1.0	1.0		•••	10·7 5·3	65 32			
13						•2		.6	·7 ·3	·8	.I I.O	1.0	1.0	1.0	.3	·5 ·3			5·3 7·8 5·0	47 30			
15						·ī													0.1	I			
16 17			•••		I.O		 ·6			·1				·1	·4 ·4				0·6 6·9	4 42			
18			•••	···				•••	·3 ·2	·5 ·4 ·1	•••		·7 ···		·4 ···			•••	0.6	4 10	Ci.	45.3	40
19 20		•••	•••	•••	•••						·1 ·2	·3 ·2	•2						1.4	8	•••		
21			•5	1.0	.7	.9		·1		.1						 ·8			3.3	20	 Clear	71.1	63
22 23			.0	1.0	1·0	I.0	1.0	1.0	1.0	1.0	·2 1·0	1.0	·5	.4 1.0	·2 ·8	1.0	.7		5·3 14·3	32 <b>86</b>	Clear	74.1	65
24 25					·6 		1.0		.3	 I	•••		 .I			•••		•••	0·1	. 26 I			
26						<b></b>	·						1.0	.9	.7	•2			2.8	17		•••	
27 28					·7	·4 ·3	.i		···		·6 ·2			·1		•••			2.0	12 18	-:		
29 30			 ∙6	.8 1.0	1·0 ·7	1.0	1.0	1.0	1.0	·9			·8 	·8 ···	1.0	1.0	·1 ·2		5·5	72 33	Haze 	43.5	38
Sum.	0.0	1.0	4.6		10.3	9.5	8.1	8.3	8.3	8.5	8.4	8.2	8.9	9.2	7.8	6.3	2.0	0.0	118.2		_		_
Mean	0.00	0.03	0.15	0.29	0.34	0.32	0.27	0.28	0.28	0.28	0.28	0.27	0.30	0.31	0.26	0.31	0.07	0.00	3.94	24			
Hour	3 to	4 to	5 to	6 to	7 to	8 to	9 to	10 to	11 to	Noon	13 to	14 to	15 to	16 to	17 to	18 to	19 to	20 to	Total for	Per cent. of	Sky.	Total.	Vertical.
L.A.T.	4.	5.	6.	7.	8.	9.	10.	11.	Noon	to 13.	14.	15.	16.	17.	18.	19.	20.	21.	Day.	Possible.	Ångströ	Radiation öm Pyrhel	i, liometer.

For periods of sixty minutes, between the exact hours, of Local Apparent Time.

446. Richmond (Kew Observatory): hs (Height of recorder above ground) = 13.3 metres.

July, 1923.

	{		È-		1	<u> </u>		<u>`</u> _	Ī	1										Per cent.		Radiation, om Pyrhel	iometer.
Day.	3 to	4 to	5 to 6.	6 to	7 to 8.	8 to	9 to	IO to	Noon		13 to	14 to	15 to 16.	16 to	17 to 18.	18 to	19 to 20.	20 to 21.	for Day.	of Possible.	Sky.	Total.	Vertical.
	hr.	hr.	   hr.	hr.	hr.	   hr.	   hr.	hr.	hr.	hr.	   hr.	   hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	   %		<u> </u>	mw/c m²
I 2	:::				1.0	.3	.4			···		I.0			·1			•••	3·7 5·6	22 34	•••		
3 4	:::			·	1.0	·1		·			1.0		1.0	1.0	1.0	I.O			0·4 8·4	2 51	•••	•••	:::
5			.3	1.0	-8	•4	.1	1.0	1.0	1.0	1.0	1.0	1.0	-8	1.0	1.0	.1		11.5	70	Clear	68.9	60
6			.6	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	I·0	1.0	1.0 .8	1.0			13·6 9·8	83 60	Haze	50.7	44
8	:::					1.0	1.0	·8	'4 1.0	.9	1.0	1.0	·5 ·8	·8	.9	•6	•6		7.9	48 69	 Haze	71.8	63
10		:::	1.0	1.0	1.0		1.8	.6	.5	.9	•6	1.4	1.8		:::	:::			4.6	28		/	
11			.7	.9	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	•5		14.1	86 80	Haze Haze	59·5 57·3	52 50
12				.9	1.0	I.0 I.0	I.0 I.0	1	I.0 I.0	I.0 I.0	I.O I.O	I.0 I.0	1.0	1.0	1.0	1.0			13.0	81	Haze	60.6	53
14 15			··6				.8	.5	I.0	1 0	··6	·1	.3 I	'4 ·1	·4 ·3	1.0	 I		2·7 8·4	17 52			
16		<b></b>			.5		.5	.9	-8	1.0	1.0	1.0	.9	.9	.3	.3	.4		8.5	53	Clear	73.9	64
17	_		1.0		.9	·6 ·8	.8	.1	···		···				••2			_	1·2 6·4	7 40			
19 20	_	·4		1.0	I·0	1.0	1.0	1.0		ı.o		1.0		ı	1.0	I.0	··6	_	4·9 11·7	31 73	 Clear	76.6	 66
21					.9	.7	1.0	1.0	1.0	.9	1.0	1.0	1.0	-8	1.0	1.0	.4	_	11.7	74	Clear	71.3	61
22		•••		•2	.6		•2	.9	·4 ·9	·4 ·3	·8	1.0	1.0	1.0	1.0	·6		_	7·4 5·7	47 36	 Clear	72.7	62
23 24	<b>—</b>	••5	.7	.9	1.0	.9	.9	.9	1.0	1.0	1.0	1.0	1.0	I.0	•9	·8 ·5	.2	_	14·0 0·8	<b>89</b> 5	Clear	74.8	64
25	_	•••		T.O.				.2	···	···	1.0		1.0		···	.6	·1	_	12.4	79	Clear	78.2	66
26 27 28	_	·2 ·3	I.0	·6	.0	1.0	.8	•9		.3	.5	.i						_	5.7	37	•••	·	• • • •
28 29	_	•••	···		1.0		··· ·7 ·8		·			·3 ·2	·8	·4 ·3				_	2·1	13 32	•••		
30	_	•••	•2	-8	.9	·6	.8	8.	·4	.2	•1	•••	•••			•••		_	4.8	31			
31		•2	·8 ——	.5	.3													_	1.8	12		ļ	
Sum.	0.0	1.9	10.6		19.9	17.6	<u> </u>	16.8	15.8			17.9		15.4	14.2	13.0	4.6		232.2				
Mean.	0.00								0.21			o·58	o·56	0.50	0.46	0.42	0.15	0.00	7:49	47		August,	1002
447.		hr.	d (K	hr.	DSGrv hr.	hr.	$\frac{1}{1}$ hr.	$\frac{ds}{ds} = \frac{1}{2}$	13·3:	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	%			mw/cm ²
I	hr.	٠1	1,0	.9	1.0	1.0	1.0	1.0	٠9	.9	.9	1.0	1.0	1.0	1.0	·9 ·8	·I	_	13·7 7·2	% 89 47			
3	_	•••	·1	1.0	1.0	1.0	·6	1.0	.7 1.0	'4 I·0 I·0	.3 1.0	I.0 I.0	I.0 I.0	I.0	1.0	1.0	•2	_	12.9	84 82	Clear	74.4	62
4 5	_		1.0	1.0	1.0	1.0	1.0	1.0	.7 1.0	-8	•9	•6	•6	.8	.7	••5		-	11.9	78	•••		
6	_		.2	.7	1.0	1.0	1.0	1.0	1.0	.9	1.0	.9	•3 •8	1.0	•8	·ı			10.0	72 70	 Clear	 56·4	 46
7 8				.4 1.0	1.0	1.0	1.0	1.0	I.0 I.0	1.0 .0	·6	I.O I.O	1.0	1.0	1.0	1.0		_	13·1	70 87	Clear	68.0	56 62
9 10	_		·6 ·3	1.0	1.0	1.0	I.0 I.0	I.0 I.0	·8	.0 I.0	·5	.6 1.0	·6	·6 ·6	·6	··6		_	10.1	73 68	Clear 	70.4	
11	_		٠ı	.9	-8	1.0	1.0	1.0	.9	.7	•4	·ı	٠5	1.0	1.0	٠7			10.1	68	•••		
12 13		•••	·7	I.0	1.0	I.O I.O	I.0	1.0	I.0 I.0	.6 1.0	1·0 •4	·9	·5	··9	.3	·6 ·5		_	9.6	84 65		:::	
14	_	•••		·5		·.ı	1.0	8	I.O I.	·8 ·9	·2 ·9	·4 ·9	·3	I.0 I.	.2 1.0			=	5·4 7·5	37 51	•••		
16	_			.6	1.0	1.0	.2	.1	.3	.7	.8	.3	•2	-8				_	6.0	41	•••		
17	_	•••			·I	·4 ·6							·2 ·6	·3 ·7		 '7		_	1·4 4·6	10 32	•••		
19	_	•••			1.0													_	3·8 	26 	•••		
												•2			1.0	-8		_	6.1	43			
2I 22	=	•••		I.0	.9	1.0	1.0	⋅8	1.0	1.0	1.0	1.0	1.0	1.0	1.0	.7		_	12·4 4·7	87 33	•••		
23 24	_			•••				9						·6			_	=	2.2	16 19			
25	_	_	•5	1.0	1.0			•2	'''		•••							_	2.7				
26 27 28	_	_	•2			1.0	1.0	1.0	7	·6 ·7 ·8	·3	1.0	·9 ·8	·6	·9		_	_	5·5	40 65 62			
29	_	_		 I.O	1.0						 I.0	·8 ···					_	_ ,	8.5		•••		
30	_	_	•6	1.0	1.0	1.0	1.0	1.0	.9	1.0	1.0	1.0	1.0	.9	.9	•2		_	12.5	91	Cloar	72.4	54
31		i	·.I	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	·6					_ <del>-</del> _		8.7	64	Clear	73.4	54
Sum.		0.1			21.5	22.4	21.2	20.9			17.0	17.2	15.7	17.6	16.5	10.8	0.3		247.0				
Mean.	<u> </u>	0.00	0.29	0.62	0.69	0.72	0.68	0.67	0.59	0.62	o·55	0.56	0.51	0.57	0.53	0.35	0.01		7·97	55	<u> </u>	Total	Vertical
Hour	3 to	4 to	5 to	6 to	7 to	8 to	9 to	10 to	11 to	Noon	13 to	14 to	15 to	16 to	17 to	18 to	19 to	20 to	Total for	Per cent. of	I	Total.	Vertical
L.A.T.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	to 13.	14.	15.	16.	17.	18.	19.	20.	21.	Day.	Possible.	Ångströ	Radiation, m Py <del>r</del> heli	ometer.

DURATION OF BRIGHT SUNSHINE.
For periods of sixty minutes, between the exact hours, of Local Apparent Time.

448.	Rich	ımon	d (K	8 <b>w</b> 0		-		-	-										.,,,,,		Sej	otember,	1923.
																-0.4-			Total	Per cent.		Radiation n Pyrheli	
Day.	3 to	4 to	5 to 6.	6 to	7 to 8.	8 to 9.	9 to	IO to		Noon to 13.		14 to 15.	15 to 16.	16 to 17.	18.	19.	20.	21.	for	of Possible.	Sky.	Total.	Vertical.
	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr. 1.0	hr.	hr.   ∙8	hr. '7	hr.	hr.	hr.	hr.	hr.	hr. 8·3	% 61		mw/cm².	mw/cm³.
3	=	=		.0	I.O I.O	1.0 1.0	I.0 I.0	.9	.3	·8	·2 ·6	·8	·7		••5		=	_	7·1 8·6 0·1	53 64 1	Clear	66·o	48
4 5	-	_						I.O	1.0	1.0	1.0	1.0	1.0	1.0	1.0		_	_	8.1	61	Clear	63.3	45
6 7	_	_							·.ı	·9	1.0	1.0	1.0	1·0 ·7	·9 ·5		_	_	5·9	45 24	Haze	58.9	42 
8 9	=	=			·4 1·0	·9	I.0 I.0	1.0	.9 1.0	I.0 I.0	·9	.ð	1·0 '4	.9 1.0	·8 ·4		_	_	9.3	78 72	Cloud  Haze	38·6  48·0	27
10	-	_			•••	.9	⋅8	.9	.9	·6 ·9	·8	·8	1.0	·4 1·0	···		_	_	6·2	48 53	naze	40 0	33
11 12 13						1.0	1.0	1.0 1.0	1.0	1.0	1.0	1.0	1.0		·9		_	_	10·4 5·2	81 41	Haze	64.5	44
14	=	=			1.0	·2 I·0	·8	·8 ·9	·9 ·5	·8 ·2		·6 					_	_	4·7 5·1	37 40	Clear Clear	66·8 66·8	45 45
16	-	-		.3	1.0	I.0 I.0	1.0	1.0	I.O	1.0	·9	·8	·9	·5	·6 ·5		_	_	10·0 11·0	79 <b>88</b>	 Clear	 80·8	53
17 18 19	_	_			.3	I.0 I.0	·8	·4 ·5	.1		.9		·5	·6	·6		_	_	6·0	48 35	CiSt.	50.9	33
20	-	-		8.	1.0	1.0	1.0	.9	•9	•4		•5	٠ı		•••				6.6	54	Clear	77.1	49
2I 22	_	=			·5 	·5	·2 	·2 	·1		·5 ···	·8 ···		·8 ···			_	_	4·6 	38	•••	•••	
23 24	_	=		·4 	·2 I·0 I·0	·2 ·9 I·0	·2 1·0 ·9	·5 ·8 ·6	·6 ·5 ·6	·8 ·7 ·2	·9 ·8 ·6	·7 ·4 ·2	·5 ·7 ·2	.1 .1		-	_		5·1 6·9 5·6	42 57 47	•••		
25 26				•2	.4	.9	•2	•2								_		_	1.9	16		<u></u>	
27 28	_	=	_		 '4	·7 ·9	1.0	·7 ·9	·5 ·6	·7 ·6		·5 ···	·6				_	_	5·1	43 37	Ci.·St. …	28.9	17
29 30	_	_			•••							···	···	I.O	···	_			2.6	22	•••	•••	•••
Sum.		_	0.3	5.6	12.7	18·o	18 6	18.1	15.4	16.3	16.5	16.6	14.4	12.3	8.7	0.0			173.4				
Mean.		_	0.01				0.62		0.21			0.55	0.48	0.41	0.29	0.00	<u> </u>		5.78	46			4000
449.	Rich	hr.	d (K)	bw O	hr.	atory hr.	): h	$s = \frac{1}{hr}$	13·3 hr.	metr	es.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	%		October,   mw/cm².	1923.   mw/cm².
1 2	=	_	_		ı.o	ı.o	I.O	··8				•••			•••	_	_	_	3.9	 34	•••	•••	
3 4		_	=			٠		··8 ·6	··· ·9 ·2		••5	··· ·1	 .8	I.O	··· ·2	_			0.0. 2.0	52 8	•••		
. 6			_			   	·1	.1	•5	···		1.0		•4		_	_	_	3.3	29	•••		
7 8	_	_	_		·1	···	1.0	.4 •1	·4 		 •5	·1	·i			_	_	_	1·1	10 26	 Ci	 68·1	
9 10	=	_	_	•••	•••					·8 ···	·6 					_	=		2.9	26 			37
11			_												•••	_	_	_	0·1	 I	•••		
13	=	_	_		·5 ·7	.9 1.0	I.0 I.0	ı.o .8	·7 ·7	·6	·6 ·5	·7 ·2	·4 ·6	.1 .3		_	_	_	6·8	63 57 <b>87</b>	 Class		
15	_				.7	1.0	1.0	1.0	1.0	.9	1.0	.9	·9	.9		_	_	_	9.3	<b>8</b> 7 40	Clear	71.1	36
16 17 18			=		··· ·4 ···	'4 1·0	·3	·6 ·2	I·0	·9 	 I·	·2 	·7 			_		_	1.9	18	•••		
19	_	_	_			·2 ·2			1.0		 ·8	 ·6	·			_	_	_	0·2 5·2	2 50	Ci.	 61·2	29
21			_										.3	.2		_	_	_	0·5 5·9	5 57	•••		
22 23	_ 	_	_			·7 ···	·8 	1.0 1.0	 .9	 1.0	·3 ···	 .8	.2 .1	·5 ···					0.1	57 1 67	Clear	78·8	36
24 25	=	_	_			·5 ·9	.9	.9	•5	.3	.3	.9	.6	•2	_		_	-	5.8	57	•••	<b>,</b>	
26 27 28			_	_	• • • •	•••	·7 ···	1.0	·8 ·2		.2	·9 ·5	.3 1.0	·2	_	_		_	1.1 2.1	51 11	•••	•••	
29	<u> </u>	_	_	_		 .5	·3 ·4	1·o •5	.7 .5	·7 ·3	·1	·3 ·2		···	_			_	3.1 3.3	33 32 	•••		
30 31	_	_	_	_		·	···	1.0	···	1.0				···	_		_	_	6.1	63	Ci.·St.	48.3	20
Sum.				0.0	4.5	9.6				10.1	8.3	8.7	8.5	4.5	0.3				92.5				_
Mean.			_	0.00		0.31	0.37	0.45	0.41	0.33	0.27	o·28	0.27	0.15	0.01				2.98	28			
Hour	3 to	4 to	5 to	6 to	7 to	8 to	9 to	10 to	11 to	Noon	13 to	14 to	15 to	16 to	17 to	18 to	19 to	<b>20 t</b> o	for	Per cent.	Sky.	Total.	Vertical.
L.A.T.	4.	5.	6.	7.	8.	9.	10.	II.	Noon	to 13.	14.	i5.	16.	17.	18.	19.	20.	21.	Day.	Possible.	Ångströ	Radiation m Pyrhel	iometer.

DURATION OF BRIGHT SUNSHINE.

For periods of sixty minutes, between the exact hours, of Local Apparent Time.

The column	450.	Rich	mon	d (K	ew O	bserv	<i>r</i> atory	1003 1): h	ıs (He	eight	of re	corde	er ab	ove g	roun	d) =	13.3	met	res.		viiic.	No	vember,	1923.
Right   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Start   Star																				Total	Per cent	R Ångströr	adiation, n Pyrhelio	ometer.
The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The color   The					1											17 to 18.				for	of		<u> </u>	
\$\$   \$\frac{1}{3} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		hr.	hr.	   hr.	   hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.	hr.			%	}	mw/cm²	mw/cm ²
3			_	_		1	1	1										_						1 1
3	3	l	_	_				I								_		i 1	_					
9		1	_	_	-	1	1	1	i	1	1					-	-		_	0.2	2	•••	•••	
Section   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Control   Cont	1	_		_	1		1		1				1	1	1 1	-		_	_					1 1
18		_	_	=	—	i	1	1	ı	1 1		1.0	i					-		2.8	30	Mist	39.6	15
14		ı		_	1	1	1	1							i 1		_	_						
14	11	_					1.0	1.0	1.0	1.0	1.0	1.0	•4				_		_					
14	1		_	_		ł	1	į.		- 1				1		_	!!!	_	_	0.4	_		,	
160	14		_	_	_		-8	1	1	}	. 1				1	- 1		- 1						1 1
18												-	-			_	_	_	_	3.7	42	Clear	74.4	25
10	17		_	_		i		1.0	·ı	.7	•3	-8	.9	٠1		_	_		_	4.5	52		•••	1
21			_	_		ı	1		-8	.9	-8	•9	•9					-		5:8	67	•••		!!
## 1	20	-	_	-				•••	.6	'7	•2					_	_							
## 1	I		_		=				1					1	1	=	=	_		[	[	•••	•••	
25	23		_	_	1	1	l .		l :	1 1		- 1			- 1	_	_	_	_	'	i			1
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Sum.			_	_		ı	1		1		i i	1				_		_	_				1	i i
\$\frac{3}{90}\$			_	_	=	I							•••			_		_	_				l .	1 1
Mean,		_	_	_	1	1	1		ŧ								_	_	-				27.7	8
## A\$1.   Richmond   Kow Observatory   She = 13   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She   She	Sum.	_			_	0.1	4.3	6.1	8.9	12.7	12.2	13.8	10.6	4.3	0.1	_	_	_		73·1				
State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   Stat	Mean.	_	_		-	0.00	0.14	0.20	0.30	0.42	0.41	0.46	0.35	0.14	0.00					2.44	28			
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Annual Total. 0·0 3·2 30·9 64·1 94·3 114·8 125·9 143·3 141·4 142·9 136·8 130·3 105·7 82·2 64·7 39·3 7·6 0·0 1427·4 — — — — — — — — — — — — — — — — — — —	Í																							
Total. 0 · 0   3 · 2   30 · 9   64 · 1   94 · 3   114 · 8   125 · 9   143 · 3   141 · 4   142 · 9   136 · 8   130 · 3   105 · 7   82 · 2   64 · 7   39 · 3   7 · 6   0 · 0   1427 · 4	Annual	<u> </u>			<u>'                                    </u>	1	<u> </u>																	
Mean.   0 · 00   0 · 01   0 · 08   0 · 18   0 · 26   0 · 31   0 · 34   0 · 39   0 · 39   0 · 39   0 · 37   0 · 36   0 · 29   0 · 23   0 · 18   0 · 11   0 · 02   0 · 00   3 · 91   32   -   -   -   -   -   -   -   -   -	Total.	0.0	3.5	30.9	64·I	94.3	114.8	125.9	143.3	141.4	142-9	136.8	130.3	105.7	82.2	64.7	39.3	7.6	0.0	1427 · 4				
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Hour 3 to 4 to 5 to 6 to 7 to 8 to 9 to 10 to 11 to Noon 13 to 14 to 15 to 16 to 17 to 18 to 19 to 20 to for Of L.A.T. 4. 5. 6. 7. 8. 9. 10. 11. Noon to 13. 14. 15. 16. 17. 18. 19. 20. 21. Day. Possible. Radiation,		Ī																		Total	Per cent.	Sky.	Total.	Vertical.
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# WIND: DIRECTION AND SPEED.

Direction expressed in degrees from North ( $E=90^{\circ}$ ,  $S=180^{\circ}$ ,  $W=270^{\circ}$ ,  $N=360^{\circ}$ ): Speed in metres per second.

# 452. Richmond (Kew Observatory):

 $H_a$  (height of cups of anemograph above M.S.L.) = Height of ground above

Day.	]		2	.	3	3.	4	.	5	j.	6	).	7		8	3.	9		10	o.	ı	ι.	No	on.
1 2 3 4 5	340 205 230 250	m/s 3·0 3·6 7·5 1·6 0·0	340 200 235 250	m/s. 2·6 4·9 7·5 1·6 0·0	195 230 250	m/s. 0·7 7·9 5·9 1·6 0·3	340 195 225 —	m/s. 1·6 6·9 6·9 1·3 0·7	195 235 250	m/s. 1·3 6·9 6·9 1·6 0·0	340 200 240 250	m/s. 2·0 5·6 5·6 2·0 0·3	200 240 250	m/s. 1·3 5·2 5·9 2·0 0·7	205 240 250 250	m/s. 1·3 4·6 5·2 1·6 2·6	340 205 235 250 230	m/s. 1·6 4·6 6·6 2·0 2·3	330 220 230 245 190	m/s. 1·6 7·5 6·2 2·0 3·6	270 220 240 265 185	m/s. 2·6 8·9 6·9 2·0 4·9	265 225 250 — 190	m/s. 1·6 7·9 6·2 1·3 6·6
6 7 8 9 10	305 — 260 330 245	5.6 1.0 5.9 1.6 6.2	315 260 260 265 245	5·2 1·6 5·6 2·6 5·9	315 260 250 240 240	6·2 2·6 4·9 1·6 7·2	310 255 250 240 245	5·2 3·3 3·6 3·0 6·6	310 235 250 235 245	4·6 3·6 5·2 4·3 6·9	315 220 255 220 240	3.0 5.6 3.9 4.9 6.6	315 205 245 215 235	1·6 6·6 4·9 7·2 7·2	315 215 245 205 240	2·3 7·2 3·9 7·2 7·2	215 245 210 235	1·3 7·2 4·3 8·9 7·5	315 220 230 215 230	2·0 6·6 4·9 7·5 7·5	315 235 240 240 240	2·3 5·2 5·2 8·2 8·9	315 235 240 265 250	3·0 3·9 6·6 6·6
11 12 13 14 15	265 290 — 235 285	3.6 3.6 1.0 3.3	265 315 — 235 255	2·6 4·3 1·0 2·3 3·6	265 330 — 235 255	3.0 3.9 1.0 3.6 2.6	265 345  235 255	3·3 3·3 3·3 3·3	270 360 — 240 255	2·6 3·6 1·3 3·0 3·3	270 360 360 245 255	2·6 3·9 1·6 3·6 1·6	270 360 — 245 265	2·3 3·9 1·3 3·6 3·3	270 360 — 245 275	1.6 2.6 0.7 3.6 3.0	270 — — 245 285	2·3 1·3 0·7 3·6 4·3	270 — — 240 280	3.3 3.3 1.0 3.3	280 360 315 255 280	4·3 2·0 1·6 3·3 3·3	290 360 315 260 285	4·3 3·9 2·3 4·9 3·0
16 17 18 19 20	250 — — — 245	2·0 1·0 0·0 1·3 5·6	250 — — — — 255	2·0 0·0 0·0 1·3 5·2	270 — — 360 290	2·0 0·3 0·0 1·6 4·6	285 — — 320 310	3·0 0·7 0·0 2·3 3·9	305 — — 305 315	1.6 0.3 1.3 2.3 4.9	310 — — 300 320	3.6 0.3 1.9 0.3	310  50 300 305	2·0 0·7 1·6 2·0 4·9	310 — 270 320	2·0 0·0 0·7 2·3 4·6	315 — — 240 300	2·0 0·0 1·3 2·3 5·6	10 — 45 240 310	1.6 0.0 1.6 3.0 4.6	15 — 330 240 320	2·6 0·0 2·0 2·6 6·2	15 — 330 240 310	2·6 0·0 2·3 3·6 8·2
21 22 23 24 25	335 270 5 250	3·9 2·6 5·6 3·3 1·0	340 275 15 250	3.6 2.3 2.0 2.3 1.3	345 275 360 250	3·0 2·3 2·3 3·3 1·3	345 275 360 250	2·0 1·6 1·6 3·3 1·3	345 275 360 250 240	2·0 1·6 2·0 2·3 1·6	275 360 250	1·3 2·0 1·6 2·6 1·0	325 275 360 250	2·0 2·3 2·0 3·0 1·0	275 360 250	0·7 2·0 2·0 3·3 1·3	280 275 — 245 —	2·3 2·0 1·0 3·3 1·0	280 270 360 235	3·3 2·6 1·6 3·9 1·3	280 275 360 235 240	2·6 3·3 2·3 3·3 2·0	285 285 360 240 240	3·0 5·2 2·6 3·3 2·0
26 27 28 29 30	270 275 265 270 280	2·0 2·3 2·0 1·6 3·0	275 265 260 280	1·3 2·0 2·3 2·3 3·0	270 275 265 260 280	1.6 1.6 2.0 3.3 3.0	270 — 265 260 280	1.6 1.3 2.3 3.3 2.0	270 275 265 260 280	2·0 2·0 1·6 3·3 2·6	270 275 — 260 280	2·0 2·0 0·7 3·0 2·0	270 275 265 260 280	2·0 2·0 1·6 3·0 3·0	270 275 265 260 280	1.6 1.6 2.0 3.0 1.6	270 275 265 250 280	1.6 1.6 1.6 3.9 2.0	270 275 265 250 280	2·3 1·6 2·0 4·6 2·0	270 280 265 250 280	1.6 2.6 3.0 3.9 2.6	270 280 275 260 290	2·3 3·0 2·6 3·6 3·3
Mean	265 —	3.3	²⁷⁵	3.6	270	3.9	270 —	2.9	²⁷⁵	3·9 2·9	265 —	<b>2⋅8</b>	260 —	3.1	260 —	3.0	260 —	2.9	250	3.3	260 —	3.7	270	3.8

# 453. Richmond (Kew Observatory): $H_a = 5$ metres + 20 metres.

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I	240	6.6	245	6.6	250	8.5	245	8.2	250	7:5	245	6.6	245	7.9	245	6.6	240	7:5	240	6.6	240	7.5	235	6.2
2	235	8.5	230	7.5	235	7.2	230	6.6	240	6.9	235	6.6	235	6.6	235	5.9	235	5.6	235	6.6	235	5.6	240	4.9
3	245	6.6	245	5.6	245	4.9	250	4.3	245	4.9	250	3.0	250	3.3	250	3.9	250	3.6	230	4.9	245	5.9	245	5.2
4	240	3.9	240	3.0	240	2.6	_	1.3	<u>-</u>	1.3	240	2.0	240	2.0	240	2.0	245	2.3	315	4.6	345	4.9	340	4.6
5	<u> </u>	0.3		0.3		0.0	l —	0.0		0.0	<u> </u>	0.3	i —	0.0	<u> </u>	0.3		1.0	220	2.6	195	3.6	195	4.9
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6	180	2.6	180	4.3	185	3.0	185	3.6	185	6.9	180	4.6	180	5.6	165	3.9	175	5.9	185	8.9	185	8.2	180	8.5
7	210	3.0	210	2.6	210	2.0	205	2.6	190	3.9	185	5.2	175	5.2	165	6.9	165	8.2	170	8.9	170	9.2	180	8.5
8	180	8.9	175	7.5	165	8.5	170	10.2	175	10.2	170	8.9	170	10.2	180	8.5	175	8.5	175	7.2	185	7.2	195	4.6
9	245	1.6	245	1.6	_	1.3		1.3		1.0		0.7		0.3		0.7		1.0		1.3	245	1.6		1.3
10	160	3.6	160	3.0	160	3.6	160	3.0	150	4.6	155	4.3	160	4.3	155	3.9	155	5.6	155	6.2	155	6.2	160	7.5
	180	6.6	200	7.0	200	1.6	100	4	705	5.0	TOC	2.6	TOC	3.0	210	3.2	200	4.6	200	5.2	205	5.9	215	
11	215	2.0	215	7.2	200 215	4·6 2·0	190 215	1.6	195	5·2	190	3.6	190	3.9	210	3.3	200	0.7		0.0	203	0.3		4·3
13	215	1.0	215	1.0	215	1.3	215	1.0		1.0		0.7		0.3		0.7		1.0	55	2.0	45	2.3	50	2.3
14	130	5.2	130	3.6	130	4.3	130	3.3	130	3.9	130	3.6	130	3.6	130	3.6	130	3.9	115	4.3	115	4.3	115	3.0
15	-30	0.7		1.0		1.0	130	1.3		1.0	-50	1.3	-30	1.0		1.3	115	4.3	110	2.6	110	3.3	110	2.0
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16	155	3.0	165	4.3	205	3.3	215	2.3	240	3.0	250	2.0	250	2.3	250	2.0	250	2.3	250	3.0	250	3.3	240	3.6
17	185	4.9	170	4.3	220	4.9	250	3.9	250	2.6	250	2.3	250	3.3	250	2.3	250	2.6	260	3.0	28o	4.3	275	4.3
18	125	5.6	125	5.9	125	5.2	120	6.9	120	7.5	120	6.6	120	6.9	115	7.9	120	7.5	110	5.9	115	5.9	115	4.3
19		1.0		0.7	_	1.0	265	2.0	265	2.0		1.0		0.3		0.7	265	1.6	300	2.0	310	3.9	320	2.6
20	5	4.9	5	4.6	15	4.3	15	3.9	20	4.3	25	4.3	25	4.3	30	4.9	35	4.6	50	4.3	50	3.3	50	2.3
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21	105	3.6	105	4.3	105	4.3	105	4.3	115	4.3	115	3.6	120	5.2	125	4.6	155	5.6	160	4.9	180	4.9	210	3.6
22	245	3.0	245	2.6	² 45	2.6		1.3	245	2.0	-	1.3		0.3	_	1.3		1.3	225	2.3	215	3.3	185	4.3
23	230	6.6	240	6.2	245	5.9	245	5.2	250	4.9	265	5.6	285	5.9	290	5.9	290	5.6	290	5.2	290	4.9	290	4.3
24	185	2.0	185	2.3	185	2.6	180	2.6	135	3.9	125	3.9	115	5.6	115	4.6	115	4.6	125	5.6	130	5.6	130	4.6
25		1.3		1.0		0.3	<b>—</b>	1.0		0.7	_	0.7	I —	0.3		0.3		0.7	-	1.0		0.3	195	2.0
26			l						-6-		-60	- 6		<b>.</b>		r.6	160	5.2	165	٠.۵	205	8.2	225	70.0
26	215	2.6	210	2.6	195	4.3	190	4·6 8·2	160	5·9 8·2	160	5.6	155	5.9	155 210	5·6 7·9	215	9.5	195	5·9	200	11.8	235	10.5
27 28	210	10.2	205	8.9	210	9.2	215	6.9	205	8.2	205	7.2	210	9.2	240	6.9	240	6.6	240	7.2	230	5.9	225	6.6
20	240	7.5	250	6.6	250	7.2	255	0.9	265	0.2	255	7.2	250	7.2	240	0.9	-40					3 9		
Mean	_	4.2		4.0		3.9		3.8		4.5		3.7		4.0		3⋅8		4.3		4.8	_	5.1	_	4.7
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G.M.T.	1		] 4	2.	ļ ,	3.	4	١.		<b>5</b> . أ	l 6	<b>5.</b> .	1 :	7.		3.	9	9.	1	o.	1	ı.	No	on.
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Averages for periods of sixty minutes, centered at the exact hours, Greenwich Mean Time.

M.S.L. + ha (height of an emograph above ground) = 5 metres + 20 metres.

January, 1923.

I	3.	1	4.	1	5.	1	6.	ı	7.	1	8.	,	19.	1 2	20.	2	21.	2	22.	2	:3.	2	4.	Mean	D <b>a</b> y.
215 245 310 190	m/s. 1·0 8·5 6·2 3·0 7·5	265 215 245 320 190	m/s. 1·6 8·5 5·6 2·3 8·2	265 220 250 — 190	m/s. 2·3 9·2 5·2 1·0 6·9	265 220 250 — 180	m/s. 2·0 8·9 3·0 1·0 8·2	265 215 250 — 185	m/s. 1·6 8·2 3·9 1·3 8·2	255 250 — 180	m/s. 1·0 8·2 3·9 0·7 8·2	265 270 250 — 180	m/s. 1·6 3·6 3·3 1·3 7·2	265 225 250 210	m/s. 1·6 4·6 2·6 0·7 5·2	265 230 250 — 280	m/s. 2·0 8·2 2·3 1·3 4·6	215 220 250 — 285	m/s. 3.0 6.9 2.3 1.0 3.0	205 220 250  295	m/s. 3·6 7·9 2·0 1·0 4·3	205 225 250 — 305	m/s. 3·3 7·9 2·0 0·3 5·2	m/s. 1·9 6·8 5·1 1·5 4·0	1 2 3 4 5
300 235 255 270 255	3·9 2·3 3·3 7·5 7·2	300 245 285 265 255	3·9 2·6 3·6 4·9 8·2	295 260 330 265 260	3·3 2·3 3·6 5·9 6·9	290 260 330 255 260	1.6 2.6 2.3 5.6 5.2	285 260 330 250 265	2·0 3·0 3·6 5·2 4·6	260 260 330 250 265	2·0 2·3 2·6 4·6 3·6	260 260 330 225 260	2·3 3·0 1·6 5·6 3·9	260 265 330 240 255	2·6 3·0 2·3 5·2 3·6	260 260 330 245 255	2·3 4·6 1·6 6·2 3·0	260 255 330 240 255	1.6 3.0 2.6 6.6 3.0	260 255 330 240 260	1.6 3.9 2.0 6.6 3.6	255  240 260	1·3 3·6 0·7 6·2 3·3	3·0 3·7 3·6 5·5 5·9	6 7 8 9 10
290 360 — 270 290	4.6 3.6 1.3 5.6 3.9	295 360 — 265 295	4·3 3·9 1·3 4·6	300 360 255 270 290	4.6 3.0 1.6 3.9 4.3	300 5  280 285	3·6 1·6 1·0 3·9 3·9	300 5 255 315 285	2·3 1·6 1·6 3·6 3·3	295 255 335 285	3·0 1·3 2·0 3·0 3·0	290  255 350 285	3.0 1.3 2.3 3.3 2.6	290 5 255 345 285	3·0 2·0 3·0 2·0 2·0	285  245 345 250	3·3 1·3 3·9 1·6 3·0	5 235 315 250	3·3 1·6 3·9 2·0 3·3	235 285 250	3.0 0.7 3.6 2.3 3.0	235 285 250	0·3 4·3 2·3 2·6	3·2 2·5 1·8 3·3 3·2	12 13 14 15
335 245 325	2·3 0·0 3·0 4·3 7·2	350 235 330	2·0 0·0 3·0 3·9 8·2	360 225 350	2·6 0·0 3·0 4·6 8·5	15 — 235 350	3·3 0·0 1·3 4·3 7·9	20 — 360 240 350	3.9 0.0 2.3 4.3 5.9	20 — 360 240 345	3.6 0.0 1.6 4.9 5.9	45 360 250 340	3·3 0·0 2·3 6·2 5·2	50 — 360 265 340	2:3 0:0 2:3 8:5 3:9	50 360 260 340	0·0 3·0 6·6 3·6	360 250 340	0.0 3.3 5.9 3.0	360 245 340	0·0 2·0 4·6 4·9	250 335	0·0 0·7 4·6 3·0	0·1 1·7 3·6 5·5	17 18 19 20
285 290 345 245 255	2·6 6·2 3·0 2·0	285 295 330 245 260	2·0 4·9 2·0 3·3 2·3	285 260 330 240 270	2·3 4·3 2·0 3·9 2·3	265 	2·6 4·3 1·0 3·6 2·3	245 280 330 240 285	3.0 4.6 3.0 3.0	245 275 — 240 290	3·0 3·3 1·0 2·3 3·0	245 260 330 240 270	2·6 3·9 1·6 2·3 2·0	260 320 240 270	1·3 3·6 1·6 2·3 1·6	245 265 250 240 270	2·3 4·6 3·3 2·6 2·0	245 270 250 240	1.6 4.3 2.0 2.0 1.3	280 250 240 270	1·3 5·2 2·3 2·0 1·6	250 305 250 240 270	4.6 2.3 1.6 2.3	2·4 3·4 2·1 2·9 1·7	22 23 24 25 26
270 275 280 265 300	2·0 3·0 3·3 4·6 2·6	270 285 285 275 290	2·0 3·3 3·0 4·6 3·0	270 280 290 280 290	2·0 3·6 3·0 4·6 2·6	270 280 290 275 290	1.6 2.6 3.0 4.6 2.0	270 285 290 270 290	2·0 2·6 2·6 4·9 1·6	285 290 260	1·3 2·0 2·0 4·6 1·3	275 285 290 265 275	1.6 2.0 2.3 4.6 2.6	285 290 270 265	1·3 2·3 2·6 4·6 2·6	275 285 290 270 265	1·6 3·3 3·9 3·0	275 285 285 280 265	2·0 3·6 4·3 2·3 5·9	275 280 285 280 265	1.6 2.6 2.6 4.3 3.3	275 265 285 280 265	2·3 2·6 2·6 2·3	2·2 2·4 3·8 2·5	27 28 29 30
250	4.0	260	3.9	260	3.9	255 —	3.3	245 —	3.3	²⁵⁵	3.0	260.	3.0	240	2.9	240	3.2	245 —	3.0		3.1		2.8	3.2	

# February, 1923.

10	m/s.	۰	m/s.	·	m/s.	٥	m/s.	٥	m/s.	°	m/s.	c	m/s.	۰	m/s.	۰	m/s.	°	m/s.	0	m/s.	°	m/s.	m/s.	
235	7.9	235	7:2	240	6.6	235	6.9	240	6.6	240	6.6	235	8.2	235	7.5	235	7.9	235	7.5	235	8.2	235	7.9	7.3	I
245	5.6	245	4.9	235	4.6	235	5.9	230	6.2	240	4.9	235	5.9	230	5.6	240	6.2	240	6.2	245	6.2	235	4.9	6.1	2
240	5.2	240	4.3	250	4.6	250	3.6	250	3.0	245	3.0	240	3.3	240	3.6	240	3.0	240	3.3	240	3.3	240	3.0	4.2	3
335	4.3	350	4.6	360	3.6	350	3.0	340	1.6		1.3		1.0		0.3	-0-	0.3	180	1.0	180	3.3	180	3.0	2.4	4
210	5.9	205	6.9	210	5.9	200	4.3	195	4.6	195	3.3	190	3.6	190	3.3	185	4.3	100	3.0	100	3.3	100	3 0	~ /	3
-0-		-0-		180	8	185	8.5	180	7.9	170	6.9	175	8.2	180	6.2	185	6.2	200	4.9	210	3.0	210	2.6	6.0	6
185	7.9	185	7·9 8·9	185	8.5	195	6.2	190	4.3	190	6.2	190	6.9	190	6.2	190	7.9	190	7.9	190	7.5	185	7.9	6.3	7
305	5.6	190	1.3	310	3.9	245	2.3	245	2.6	245	2.0	245	2.6	245	1.6	245	2.0		1.3	245	1.6	_	1.0	5.5	8
245	2.3	245	2.0	245	2.0	245	2.0	245	1.6	245	2.0	195	3.0	180	2.3	175	2.6	165	3.3	160	3.9	160	3.6	1.8	9
165	6.6	160	5.2	165	4.9	165	3.3	165	3.3	155	4.3	155	4.9	155	4.9	155	4.3	155	3.9	175	5.2	175	4.9	4.6	10
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230	4.9	215	5.6	215	5.6	225	3.9	215	3.0	215	3.6	215	3.9	215	3.0	215	2.6	215	2.6	215	2.6	215	2·6 1·6	4·3 1·4	11
220	2.0	220	2.6	220	2.0	<u> </u>	1.0		1.3	220	1.6	220	1.6	_	1.3	_	1.3	220	1.6	180	2.0	145	3.6	2.4	13
65	2.3	7º	2.6	85	3.3	100	2.0	110	3.3	115	3.6	115	4.9	120	3.6	120	4·6 1·0	125	4·6 0·7	125	5·9 0·3	125	0.3	2.5	14
115	2.0		1.3	T20	0.7		0.3		0.7	-	1.0	115	1.6	115	1.6	T = =	3.3	155	3.0	155	2.6	155	3.6	2.5	15
110	2.6	115	3.6	130	4.3	140	3.6	145	3.9	150	3.6	155	4.3	155	3.3	155	3 3	255	3 0	-33		-33	,	- 3	
240	3.3	225	4.3	225	3.0	225	2.3	225	2.0	225	2.0	225	2.6	225	2.6	210	2.6	190	3.9	180	4.6	185	4.9	3.0	16
295	3.9	275	3.6	270	1.6	280	1.6	60	3.0	90	6.9	105	5.9	105	7.2	100	8.2	105	6.2	115	7.2	125	5.9	4.3	17
100	3.3	-	1.3	<u> </u>	1.0	90	1.6	335	3.0	335	2.0	335	2.3	270	2.3	265	1.6	l —	0.7		1.0		1.0	4.3	18
320	3.6	320	3.6	330	3.6	340	3.9	340	3.6	345	3.3	340	3.3	355	3.3	360	3.9	10	5.9	15	5.9	_ 5	5.6	2.7	19
50	3.6	50	3.0	50	3.0	50	2.0	50	2.0	85	2.3	95	3.0	105	3.0	105	4.6	105	3.6	105	4.6	105	3.6	3.7	20
		-0-		250	2.0	260	2.0					l .					2.2	245	2.6	245	2.3	245	2.0	3.7	21
260	3.9	285	2.0	270 150	3·9 5·6	260 145	3.9	275 125	3.0	270	3.0	245	3.3	245 185	6.2	245 185	3.3	245 185	6.9	180	7.5	205	7.2	4.1	22
155 290	3·3 5·6	150 290	4.9	290	3.6	290	1.6		0.0	140	1.0	185	5.3	285	1.6	105	1.0		1.3	195	2.0	185	<b>1</b> ·6	3.9	23
130	4.9	135	4.3	135	3.6	135	3.3	135	3.3	135	3.0	130	3.9	115	2.6	115	2.3	115	1.6		1.0	115	2.0	3.2	24
210	3.3	215	2.6	235	3.0	240	2.3	240	2.3	240	2.0	245	1.6		1.3	245	2.0	235	3.6	230	2.6	230	1.6	1.6	25
	"	~	ļ	"				•		, ,-		-43	- "	1	- 3	13		] "							
240	9.5	235	9.2	220	11.1	215	11.1	220	10.2	215	9.8	220	9.2	225	9.8	215	9.8	230	8.5	220	10.2	215	10.8	7.6	26
200	11.8	195	10.3	200	11.2	205	10.2	210	9.2	210	9.2	215	7.9	210	8.5	210	7.9	215	7.9	215	6.9	215	6.9	9.3	27 28
215	6.2	215	5.9	230	6.6	250	5.2	225	4.6	240	4.3	260	3.0	235	3.0	235	2.6	235	3.3	240	4.9	250	4.3	5.8	
	5.0		4.6		4.6		4.0		3.9		2.0		4.2		2.0		4.1		4.0		4.2		3.9	4.2	
_	5.0		"		"		"		39		3.9		4.2		3.9		4.1		4 5		7 ~			<u>'</u> _	
	<u> </u>				·		i									i –		<del>i</del>		Ī		i			_
13	.	I	<b>4</b> .	1	5.	I	6.	I	7.	1	8.	1	9.	2	о.	2	I.	2	2.	2	23.	2	4.	Mean	Day.
										l		1		)		1		]		<u> </u>		<u> </u>		<u> </u>	<u> </u>

Direction expressed in degrees from North ( $E=90^{\circ}$ ,  $S=180^{\circ}$ ,  $W=270^{\circ}$ ,  $N=360^{\circ}$ ): Speed in metres per second.

454. Richmond (Kew Observatory):

 $H_a$  (height of cups of anemograph above M.S.L.) = Height of ground above

Day.	1		2		3		4		5		6		7		8	•	9		10	о.	I	ı.	No	oon.
1 2 3 4 5	245 240 — —	m/s. 4·6 6·6 1·3 1·3 0·3	240 255 — —	m/s. 4·6 6·6 0·7 1·3 0·3	235 250 — 260	m/s. 4·6 6·6 0·3 1·6 0·3	235 245 — 275	m/s. 3·9 5·2 0·3 2·6 0·3	235 240 — 285	m/s. 5·6 5·2 0·0 1·6	235 230 — —	m/s. 5·2 4·9 0·3 1·0	230 230 — 295 —	m/s. 5·9 4·6 0·0 1·6 0·0	245 225 — 335	m/s. 6·2 4·9 0·7 3·9 0·3	250 225 — 340	m/s. 6·6 6·2 1·0 3·9 1·3	250 230 — 340 360	m/s. 6·2 8·2 0·7 3·3 3·6	255 235 205 350 210	m/s. 6·9 8·5 1·6 4·3 5·6	255 235 215 350 185	m/s. 6·9 7·9 2·0 3·6 4·6
6 7 8 9 10	225 230 340 5 20	2·0 3·9 5·6 5·9 3·6	230 335 10 25	1·3 3·0 3·9 6·6 3·3	225 230 340 15 25	2·6 2·3 4·6 7·5 2·6	225 230 340 15 25	2·3 3·6 3·6 5·2 3·3	225 230 340 15 25	2·0 3·6 4·9 5·2 2·6	225 230 350 10 25	1.6 3.3 4.6 4.6 4.6	225 230 350 10 25	2·6 3·6 4·9 3·6 2·6	220 230 350 10 25	2·3 3·3 3·9 2·6 2·0	235 350 10 25	1·3 5·2 4·3 3·9 2·6	195 240 350 5 25	2·0 4·6 4·3 3·3 1·6	200 245 355 5 25	6·2 4·3 5·2 4·3 1·6	205 245 360 5 25	7·9 3·9 4·9 4·3 1·6
11 12 13 14 15	75 — 165 25 25	3·3 0·3 4·9 2·0 5·2	75 — 165 — 15	2·6 0·3 3·0 1·3 5·6	75 — 165 25 15	2·3 0·7 3·0 1·6 6·2	165 25 15	1·3 0·7 2·0 2·3 5·9	75 — 165 25 15	2·3 0·3 2·6 2·3 6·2		1·3 0·7 1·6 5·2	65 — 110 25 15	2·6 1·0 3·0 2·3 5·9	50 60 25 20	2·6 0·7 3·0 2·3 5·9	50 60 40 25 20	2·6 2·6 3·3 2·3 6·2	50 145 360 25 25	2·3 3·3 4·3 3·3 6·9	50 185 360 35 35	2·3 5·9 4·3 4·6 7·9	50 185 360 60 35	2·6 5·2 4·9 6·2 7·9
16 17 18 19 20	55 50 60 50 70	3·3 3·3 4·9 5·2 1·6	55 50 60 50 70	3·3 3·9 5·6 3·6 2·0	55 50 60 50 70	4.6 4.6 6.2 3.3 2.0	55 50 55 50 70	4·3 3·9 4·6 3·9 2·0	55 45 55 50 70	3·6 3·3 4·6 3·9 1·6	55 45 55 50 70	3·9 3·3 3·6 2·6 1·6	55 45 55 50 70	3·3 3·9 4·6 3·3 2·0	55 45 45 50 70	3·6 4·3 4·6 4·6 1·6	55 45 60 60 70	3·6 4·9 8·2 7·9 1·6	55 50 65 70	5·6 6·2 7·5 7·2 1·3	55 60 65 70	4·9 7·5 9·5 7·2 0·0	60 60 60 70	5·9 6·6 9·2 7·5 1·0
21 22 23 24 25	200 — — — —	2·3 1·3 1·0 1·3 0·7	345	1.0 0.3 1.0	265 — 50 —	2·0 0·3 2·3 1·3 0·7	50 320	1.0 0.3 2.3 1.6 1.3		1·0 0·3 2·0 2·0 1·3	270 — 50 —	2·3 0·3 2·3 1·3	280 	1.6 0.3 2.3 0.7 1.3		1·3 0·7 2·0 1·3 0·3	280 — 50 320 —	1.9 1.6 1.3 1.6	280  50 310 190	2·3 0·7 1·6 2·0 3·0	325 — 50 235 185	3·3 1·0 2·0 2·0 4·6	360 50 215 195	2·6 0·7 2·3 2·6 3·3
26 27 28 29 30	— 190 195 185	0·7 1·0 3·6 2·6 2·0	 190 195 185	0·3 0·7 2·6 2·3 2·3	— 190 195 185	0.3 3.3 3.0 1.0	— 190 195 —	0·3 1·0 3·6 3·6	— 195 195 —	0·0 1·0 4·3 3·0 1·3	— 195 195 —	0·3 0·3 2·3 3·0 1·3	 195 195 	0·7 1·0 3·6 3·3 1·3	160 220 195 145	0·0 1·6 4·6 3·6 2·3	160 215 200 105	0·3 2·3 4·9 4·3 2·6	165 235 205 105	0·7 3·0 4·3 3·6 2·6	260 180 215 195 150	2·3 4·6 5·6 4·9 3·6	200 170 205 210 145	2·3 6·6 5·6 3·9 3·3
Mean	- 100	2.8	100	2.5	100	2.7	100	2.3	100	2.0		2·3	105	2.0	_	2.7		3.3	7º —	3.9	75 —	3.3	145 —	3·o 4·5

# 455. Richmond (Kew Observatory): $H_a = 5$ metres + 20 metres.

	0	m/s.	0	m/s.	0	m/s.	, °	m/s.		m/s.	0	m/s.	l °	m/s.		m/s.	·	m/s.	ō	m/s.	0	m/s.	l °	m/s.
1 2 3 4 5	  85 85	0·7 1·0 0·7 2·0 4·3	— — — 85	0·3 0·3 0·7 3·0	  85 85	1·0 0·7 0·3 2·0 2·3	7º - 85 85	1.0 2.0 1.0 1.6 2.3	7º - - 85	1·3 2·0 1·0 1·3 1·6	7º  85 85	0·3 1·6 0·7 2·0 3·3	70 80 — 85	0·3 2·3 1·6 0·7 3·0	70 80 — 85	1.0 2.6 2.0 1.3 3.9	70 80 85 85	0.7 2.6 1.6 1.6 5.2	65 35 105 80	0.0 3.0 2.0 4.9 5.2	 65 360 100 80	1·3 3·9 2·6 5·2 5·2	60 360 110 90	0·7 5·6 1·6 5·2 4·9
6 7 8 9 10	55 75 65 65	3·0 3·9 2·3 3·3 0·7	55 75 65 65 —	2·3 2·6 3·0 1·6 0·0	55 75 65 60	4·6 3·0 5·2 2·6 1·3	55 75 60 45	5·9 2·0 7·5 3·0 0·7	55 75 65 45 40	6·9 1·6 9·2 3·0 2·3	60 	6·2 1·3 8·5 3·6 2·6	60 	5·2 0·7 10·5 4·9 4·3	50 60 40 55	5·9 1·3 11·1 6·9 4·6	60 75 55 45 60	8·2 1·6 11·5 9·2 4·9	70  55 50 80	6·9 1·3 11·8 10·8 6·6	7º 	6·9 1·3 11·1 8·9 7·9	70 65 60 55 90	5.6 2.0 11.5 6.6 7.5
11 12 13 14 15	145 135 200 200	4·6 3·0 3·9 3·3 1·0	145 — 195 195 —	3·6 3·6 3·6 0·7	— 60 190 200 —	1.0 2.0 3.3 3.6 1.3	60 195 200 180	1·3 2·3 5·2 3·0 2·0	65 230 205 —	0·3 2·0 3·6 3·9 1·3	70 210 205	1·3 3·6 3·9 1·3	70 190 210 180	0·0 2·6 3·9 1·6	200 210 160	0·0 1·0 6·6 5·6 4·3	— 70 195 205 160	0·3 2·0 6·9 6·6 3·9	 205 190 160	1.0 0.0 6.9 7.2 5.2	 185 205 165	0·3 0·7 7·9 6·9 5·9	100 185 205 165	0·3 2·6 7·5 6·2 5·6
16 17 18 19 20	130 40 80 95 70	1.6 3.6 2.6 3.9 2.3	45 80 95 35	1·3 3·6 2·3 3·6 3·6	120 45 80 95 30	2·3 3·9 3·0 2·6 3·6	105 45 80 90 35	2·3 3·6 2·3 4·3 3·3	35 80 90 35	1·3 3·3 3·9 3·3 4·3	35 80 80 35	1.6 3.6 3.6 4.3 3.3	80 35 80 85 35	2·6 3·9 5·6 4·9 3·6	65 35 80 85 35	2·0 2·6 5·2 5·2 3·3	65 35 85 85 30	3·9 2·3 4·3 5·2 4·3	70 35 90 90 35	4.6 2.6 2.3 5.9 5.2	65 35 100 95 35	6·9 2·0 3·3 6·2 4·3	70 40 95 95 45	6·2 3·0 3·6 5·6 3·9
21 22 23 24 25	25 35 15 25 190	6·6 4·3 2·3 4·3 2·0	25 35 15 25 190	6·2 4·9 1·6 3·6 2·6	25 30 15 25 190	6·2 5·6 1·6 2·3 2·6	25 30 — 25 190	7·2 4·9 0·7 2·6 3·3	30 30  20 190	7.5 5.6 1.0 2.0 4.9	30 25 15 20 190	6.6 5.6 1.6 2.6 6.2	25 25 — 20 195	6·9 5·9 1·3 8·5	40 30 10 5 200	8·2 5·2 2·3 4·6 8·5	25 35 360 355 200	8.5 6.6 4.3 4.3 9.8	25 35 350 5 205	7.5 8.2 3.6 3.3 10.8	30 35 350 345 205	7·9 8·2 3·9 3·3 10·5	30 35 345 345 205	8·2 8·2 2·3 3·6 10·2
26 27 28 29 30	220 260 — 225 220	5·2 3·0 0·7 3·6 3·6	225 260 — 230 220	3.0 2.0 0.3 3.9 4.3	225 260 — 220 225	3·3 2·3 0·7 3·9 3·6	215 260 — 215 230	3.0 2.0 1.3 3.6 4.9	215 260 — 225 230	3·9 2·0 1·3 3·6 4·6	215 260 — 220 230	3·6 2·3 1·3 5·2 4·9	210 270 30 210 230	4·6 3·6 2·3 4·3 5·6	210 280 20 220 240	5·2 2·6 2·0 3·9 5·6	215 290 270 220 230	6·2 3·0 2·6 3·3 5·6	215 315 260 235 225	6·6 3·0 3·6 5·9	215 325 265 240 225	6·9 3·3 3·9 3·0 5·2	215 310 260 240 225	9·5 2·6 4·3 3·0 5·9
Mean	-	2.9	-	2.5	_	2.7		3.0	_	3.1	_	3.3		3.7	_	4.1	_	4.7	_	5.0	_	5.2	-	1.5
G.M.T.	1		2		3	<b>.</b>	4	ļ.	5	j.	$\epsilon$		7		8	3.	ç	).	10	D.	ī	I.	No	on

WIND: DIRECTION AND SPEED.

Averages for periods of sixty minutes, centered at the exact hours, Greenwich Mean Time.

 $M.S.L. + h_a$  (height of anemograph above ground) = 5 metres + 20 metres.

March, 1923.

r	3.	12	<b>1</b> .	15	5.	1(	5.	I	7.	18	8.	1	9.	20	э.	2	ı.	2:	2.	2	3.	24	1.	Mean	Day.
255 230 255 355 190	m/s. 6·6 7·2 3·0 4·6 5·2	250 215 260 360 215	m/s. 5·2 6·9 3·3 3·6 5·2	245 215 250 360 225	m/s. 5·9 7·5 3·6 3·9 4·9	230 205 260 360 230	m/s. 5·2 8·5 3·0 3·0 5·2	210 200 260 360 220	m/s. 5·9 7·5 2·3 2·6 4·9	200 205 — 360 225	m/s. 3·6 4·6 1·0 2·3 3·6	185 205 — — 225	m/s. 4·6 4·9 1·0 0·7 2·6	180 205 — — 225	m/s. 5·6 5·2 0·7 0·3 2·6	0 170 205 — — 225	m/s. 6·6 3·6 0·7 1·0 3·0	170 205 — — 225	m/s. 6·2 3·3 0·3 1·3 2·3	° 175 205 — — 225	m/s. 5·9 1·6 0·3 0·7 1·6	190 205 —	m/s. 5·9 1·6 1·3 0·3 1·3	m/s. 5·6 5·8 1·2 2·3 2·5	1 2 3 4 5
200 250 360 5	7.5 4.9 6.6 3.9	200 270 360 5	7.5 2.6 5.9 3.6 1.3	195 270 360 5 25	8·2 3·6 7·2 3·3 1·6	195 270 360 5 65	5·6 4·6 5·2 3·3 3·6	195 275 360 10 75	4·9 3·9 6·9 3·0 4·6	195 275 5 20 75	3·9 3·0 5·9 3·6	200 280 10 20 75	3·9 2·3 7·2 3·3 2·0	230 280 10 20 75	3·3 2·6 4·9 3·6 1·6	230 295 10 20 75	3·9 4·9 7·2 3·3 1·6	230 310 10 20 75	2·6 5·2 5·9 3·3 2·0	230 315 5 20 75	3.6 4.3 5.6 3.9 3.9	230 330 5 20 75	3·0 4·9 5·9 2·3 2·3	3·8 3·8 5·4 4·1 2·5	6 7 8 9 10
50 180 360 60 35	3·0 6·2 5·2 6·6 7·5	50 185 360 55 35	3.0 4.9 4.6 6.9 7.9	50 175 5 50 45	3.0 6.6 3.9 5.9 8.5	50 180 20 40 50	3·3 5·2 3·9 5·6 7·9	50 180 25 40 50	2·6 5·9 3·3 5·9 7·2	50 180 25 40 50	3·0 5·2 3·3 5·6 5·6	45 180 25 30 55	2·3 4·3 3·9 5·6 6·6	180 25 35 55	1.0 4.3 3.0 5.2 4.9	45 170 25 35 55	1.6 3.9 3.0 5.2 4.9	45 165 25 35 55	2·0 3·3 2·0 4·9 3·3	45 165 25 35 55	1·6 3·3 2·0 5·2 3·6	45 165 25 35 55	2·0 4·3 2·0 5·2 3·0	2·4 3·3 3·4 4·1 6·1	11 12 13 14 15
60 60 65 70	6·2 7·9 11·1 8·2 1·3	55 65 60 70 75	5·9 9·2 8·9 6·6 1·6	50 70 60 70 75	6·2 8·9 9·8 7·2 3·3	45 70 60 75 75	6·6 7·2 9·5 7·2 3·3	50 70 70 75 75	6·6 7·2 8·5 6·9 4·9	50 65 65 70 75	6·2 6·9 4·6 3·6	50 60 55 70 —	6·2 5·6 7·2 5·9 1·3	50 60 50 70	5·6 4·3 5·9 4·6 1·3	50 60 50 70 70	5·2 3·9 5·9 3·0 2·0	50 60 50 70 70	3·0 4·3 4·6 3·0 1·6	50 60 50 70 70	3.6 3.9 2.3 2.3	50 60 50 — 165	2·6 3·9 4·3 1·3 2·0	4·7 5·3 <b>6·6</b> 5·1 1·9	16 17 18 19 20
50 205 200	3·6 3·6 3·0 3·0	20  50 215 200	3·3 0·3 3·0 2·6 2·3	45 	3·3 0·3 3·0 2·0 2·6	45 50 210 250	2·3 1·0 2·3 2·3 3·3	45 50 50 215 265	2·3 1·6 2·0 2·3 2·6	 30 185	0·7 0·3 1·6 2·6 0·7	345 175	0·0 0·3 2·0 2·0 1·3		0·7 0·0 1·3 0·7 1·0		0.3 1.3 1.3		0.3 0.3 0.3		0·7 0·7 1·0 0·7 0·7	1	1·0 0·3 1·0 1·3	1.7 1.7 1.7	21 22 23 24 25
160 170 195 215 150	2·3 6·6 6·9 3·0 4·3	160 170 195 190 145	2·0 5·9 7·2 3·9 3·3	 155 190 180 140	1·3 6·2 7·5 5·6 3·3	160 155 190 200 140	2·0 6·2 6·6 5·9 3·0	175 185 215 135	0·7 5·9 5·6 2·6 3·3	175 185 — 125	0·3 2·6 4·6 1·3 3·0	175 180 — 125	0·3 3·3 3·0 1·0 2·6	— 175 180 — 125	0·3 2·3 3·6 1·0 2·0	180 185 230	0·7 3·0 3·6 1·6	190 195 230 125	0·7 3·6 3·3 2·0 2·0	200 195 230 100	3·0 3·0 2·6 3·3	195 195 200 100	0·7 3·9 3·0 2·6 1·6	0·9 3·1 4·4 3·1 2·5	26 27 28 29 30
170	3·3 5·0	200	4.6		3·6 4·9	225 —	2·3 4·7		4.4		3.3	_	3.3		2.7	225	2.9	<u>-</u>	2.6	<u>-</u>	2.6		2.5	3.3	31

# April, 1923.

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60 55 105 60	m/s. 1·3 6·9 3·3 6·2 6·2	75 80 130	m/s. 1·0 5·9 3·6 5·2 5·9	135 85 80 135 60	m/s.   2·0 6·6 4·6 5·2 6·2	35 80 75 100 60	m/s.   2·3   6·2   3·9   5·2   5·2	40 80 85 85 60	m/s.   4·3 5·9 4·9 5·9 4·6	60 80 85 85 60	m/s. 4·3 5·6 4·3 3·9 4·9	70 80 85 85 60	m/s.   4.9 5.9 3.0 3.9 3.9	70 80 85 85 60	m/s.   4·3 4·3 1·6 4·3 3·3	70 80 85 85 60	m/s.   2·6   4·3   2·3   4·9   3·0	9 70 80 85 85 60	m/s. 3·3 3·3 2·0 4·6 2·3	70 80 85 85 60	m/s.   2·6 2·0 1·6 5·6 2·6	°   85 60	m/s. 1·3 1·3 5·2 3·0	m/s. 1·8 3·6 2·2 3·6 4·0	1 2 3 4 5
65 65 50 110	5·9 1·3 11·1 6·6 8·2	65 135 65 45 100	6·2 1·6 10·8 6·2 7·9	65 110 65 40 110	6·6 2·0 11·1 5·9 8·2	65 110 60 35 110	5·2 2·3 10·8 5·2 5·2	65 110 60 45 105	4·6 2·3 11·8 4·9 5·2	65 110 60 35 105	3.6 3.6 10.5 3.3 4.3	65 105 60 20 100	3.6 4.3 8.2 3.3 4.3	65 100 55 20 100	4.6 2.6 7.5 1.6 3.0	75 100 50 —	5.6 3.6 5.6 0.3 3.6	75 100 55 — 105	5·6 3·0 4·6 1·0 5·6	75 100 65 — 115	4·3 2·3 6·2 1·0 6·9	75 85 65 — 115	2·6 2·0 4·9 0·3 4·6	5·3 2·2 <b>8·5</b> 4·4 4·5	6 7 8 9 10
165 185 195 160	0·3 2·3 8·2 6·2 6·9	215 180 205 165	1·0 3·3 7·2 4·9 6·2	210 180 175 165	0·3 4·9 7·9 7·5 6·9	230 180 195 140	0·3 3·3 7·5 3·9 4·6	120 235 180 180 135	1.6 3.9 6.6 5.2 5.9	90 245 175 180 170	2·6 3·0 5·6 5·2 3·0	230 185 180 135	1.0 3.9 4.6 2.3 4.6	90 235 195 180 130	2·6 3·0 3·9 1·6 3·6	90 225 195 180 130	3·3 2·3 4·6 2·0 3·6	90 225 200 — 130	3·0 4·3 5·2 1·3 2·6	90 210 210 —	2·0 4·9 4·9 I·0	85 210 210 — 130	3·3 3·3 0·3 1·6	1.5 2.7 5.5 4.2 3.5	11 12 13 14 15
65 30 95 95 40	7·2 3·6 4·9 4·9 5·2	65 30 95 100 45	7·9 3·6 5·2 5·2 6·2	75 45 100 85 50	7·2 4·6 4·9 4·6 7·5	70 60 110 80 45	5·9 3·6 5·2 4·3 7·9	55 60 105 75 50	5·6 5·2 4·3 4·9 6·6	85 60 90 75 50	4·3 3·3 4·9 3·9 7·5	85 65 80 75 40	4·9 3·9 6·9 4·3 6·9	95 80 80 75 30	4·6 3·6 6·6 4·6 7·5	95 80 90 75 30	4·9 2·3 4·9 4·9 7·2	55 80 100 75 35	4·3 3·0 4·6 4·3 5·9	50 80 90 70 30	4.6 1.6 5.6 3.0 5.6	45 80 90 70 30	3·9 1·6 3·9 2·6 5·2	4·2 3·3 4·3 4·5 5·1	16 17 18 19 20
25 50 340 340 205	7·2 10·2 2·3 2·3 9·8	25 45 355 340 205	6·9 9·2 2·3 2·6 9·2	25 30 350 320 210	7·9 9·2 1·6 2·0 9·5	35 — 315 215	7.5 7.5 1.3 1.6 8.2	15 35 — — 215	7.5 8.5 1.0 1.3 7.9	10 30 — — 220	6·6 6·6 1·3 0·7 7·5	5 20 345 — 230	5·9 6·6 2·0 0·0 5·9	10 20 335 225 230	4·6 5·2 1·6 2·6 6·2	15 10 — 190 220	3·9 5·2 1·3 3·0 5·9	15 15 — 190 220	2·3 4·9 1·0 3·0 6·9	20 15 360 190 215	4·3 4·3 3·6 3·0 6·2	35 15 15 190 210	3·3 5·2 2·0 5·6	6·5 6·4 2·1 2·7 7·0	21 22 23 24 25
230 315 260 240 225	7·2 2·6 3·3 3·0 6·6	275 305 250 235 215	6·9 1·6 5·2 3·3 5·9	290 345 285 225 230	4.6 2.3 5.2 3.9 7.5	260  240 225 225	3·3 1·3 3·9 3·0 7·2	285 30 220 225 225	6·2 1·6 3·9 2·3 7·2	260 — 240 225 220	3·3 1·0 2·3 2·3 7·2	275 — 270 225 220	1.6 1.0 3.3 2.0 6.2	275 30 255 225 215	1.6 2.0 2.3 3.0 5.2	260 30 235 225 220	3·0 2·0 3·3 2·6 5·9	245 30 225 225 215	3·3 2·0 3·3 5·6	235 — 225 210 220	2·6 1·3 3·6 4·3 6·6	245 30 225 215 220	3·0 1·6 3·0 3·3 4·9	4.5 2.2 2.8 3.4 5.6	26 27 28 29 30
-	5.4	- 5:3 -		5.6	-	4.8	_	2.1		4.3	_	4.1	-	3.8	-	3.4	-	3.4	_	3.6	_	3.0	4.1		
13	3.	14		15		16		17		18		19	).	20		21		22	2.	23	3.	24		Mean	Day.

Direction expressed in degrees from North ( $E=90^\circ$ ,  $S=180^\circ$ ,  $W=270^\circ$ ,  $N=360^\circ$ ): Speed in metres per second.

# 456. Richmond (Kew Observatory):

 $H_a$  (height of cups of anemograph above M.S.L.) = Height of ground above

Day.	1	τ.		2.		3.	4	į.	5	5.	6	5.	7	,.		3.	(	Э.	I	о.	1	ı.	No	on.
1 2 3 4 5	240 220 — —	m/s. 4·9 1·6 0·3 0·7	235 — — — —	m/s. 4·9 0·7 0·7 0·3 1·0	° 235 — — —	m/s. 5·2 0·7 1·3 0·3 0·0	235 — — —	m/s. 4·9 o·3 i·3 o·3	230 — — —	m/s. 4·3 0·0 1·0 0·3 0·0	230 — — —	m/s. 4·3 1·0 0·7 0·0 0·3	215 — — — —	m/s. 5·6 1·3 1·0 0·0	° 220 — — — — — —	m/s. 6·6 1·0 1·3 0·3 1·3	230 — 190 190	m/s. 5·6 1·0 1·6 1·6 1·3	225 — 190 190 230	m/s. 7·2 1·0 1·6 6·2 1·6	220 230 190 205	m/s. 6·6 2·0 2·0 6·2 1·3	225 245 190 205 185	m/s. 5·9 1·6 2·3 6·9 1·6
6 7 8 9	230 — — — — 325	1.6 1.3 1.0 2.6	230 — — 25 325	1.6 1.3 1.0		1·3 1·3 0·7 3·6 3·0	230 — — 5 310	1.6 0.7 0.7 2.0 3.0		1·3 0·7 0·7 1·6 3·0	235 — 95 5 310	2·0 1·3 1·6 1·6 3·0	250 340 — 360 310	3·0 3·3 1·3 2·6 3·6	280 15 95 345 310	3.0 3.6 1.6 2.0 4.6	265 15 95 — 315	3·0 3·0 1·6 1·3 5·2	250 15 85 — 320	3·3 3·3 3·0 1·0 5·9	270 5 55 250 320	3.0 4.6 3.9 2.6 5.6	285 5 60 260 325	2·3 4·3 4·3 2·6 5·6
11 12 13 14 15	230 265 240 250 205	8·5 2·3 2·6 4·3 4·6	230 265 240 260 195	8·5 2·3 3·3 2·6 6·2	240 275 240 260 210	6·2 1·6 3·3 3·3 5·9	255 	4·9 1·3 3·3 3·0 5·2	260 — 255 260 210	4·3 1·3 3·0 5·6	260 280 260 260 210	4·6 2·3 2·0 3·0 5·6	255 300 260 270 205	5·6 3·6 2·3 3·6 6·9	265 285 260 290 215	6·6 4·3 2·0 3·6 7·9	275 295 250 290 215	7·2 5·6 3·0 4·6 7·5	265 300 270 285 220	7·2 4·3 4·3 4·6 8·5	270 290 260 270 215	7·9 5·6 4·6 4·6 8·2	275 280 270 265 205	7·9 4·6 5·9 4·3 9·5
16 17 18 19 20	240 245 270 — 280	3·6 3·3 2·3 1·0 1·6	240 245 270 — 280	2·3 2·6 2·0 1·0 1·6	240 245 270 — 280	2·6 2·6 1·3 2·3	240 245 270 — 280	2·0 2·0 2·3 1·3 2·3	240 250 270 — 280	2·3 3·0 3·0 1·3 2·6	240 255 270 — 265	2·3 2·6 3·0 1·3 3·3	255 275 275 275 285 250	3.6 3.6 3.3 2.6 4.3	280 285 295 285 260	4·9 4·6 3·9 2·3 3·6	285 295 315 280 250	3·9 4·9 3·0 3·9	275 305 305 260 245	5·9 5·9 4·6 3·3 5·2	285 305 295 260 235	7·2 4·9 3·3 4·3 5·9	260 285 290 265 245	5.6 5.6 3.6 3.6 5.6
21 22 23 24 25	255 300 255 55 225	3·9 1·6 3·6 3·6 2·0	265 — 260 55 225	3·3 1·3 3·0 2·3 3·0	265 300 260 55 225	3·3 1·6 3·3 2·6 2·3	265 300 255 55 225	2·6 2·3 4·3 2·6 2·3	265 285 255 55 225	3·0 2·6 3·6 2·0 2·6	270 260 260 55 245	2·6 3·0 3·0 3·6	285 260 265 55 250	3.6 3.0 4.6 3.6 4.6	295 245 265 70 250	3·9 3·6 4·6 3·9 4·3	285 240 270 65 255	4·6 3·6 4·6 3·6 4·3	295 250 265 70 295	3·9 4·3 4·6 2·6 3·0	295 275 280 70 290	4·9 3·3 4·3 3·0 4·3	280 275 265 40 285	4·9 4·3 5·6 2·3 3·9
26 27 28 29 30	40 40 40 130	0·7 1·0 1·6 3·0 2·0	7º - 40 130	1·3 1·6 1·3 2·6 2·0	 60  40 110	1·3 2·6 1·0 2·3 1·6	50  40 	0·7 2·6 0·7 3·3 0·7	50 — 35 —	1·3 3·0 1·0 2·3 1·3	50 — 35 110	0·7 3·0 0·7 2·0 2·0	50 40 35	0·7 4·3 3·3 1·3	340 50 40 40 110	1·6 4·3 3·9 4·9 3·0	10 60 40 45 110	1.6 4.6 4.3 4.9 3.0	5 60 35 40 105	2·6 3·9 2·6 4·3 2·3	5 45 25 45 85	2·0 4·3 3·6 5·6 3·3	345 55 25 50 95	2·0 3·3 4·3 5·9 5·2
31	80	4.6	75	6.9	75	4.3	75	4.6	75	4.6	70	3.9	65	4.3	70	4.6	65	3.9	65	4.3	65	4.6	70	4.6
Mean	-	2.5		2.2		2.4	_	2.2	_	2.3	-	2.4	_	3.1		3.6		3.7		4.1		4.4		4.2

# 457. Richmond (Kew Observatory): $H_a = 5$ metres + 20 metres.

								<del>. , .</del>			0	/		l === /a . 1		m/s	0	m/s.	0	m/s.	•	m/s.	٥	m/s.
	°	m/s.	0	m/s.	۱	m/s.		m/s.		m/s.		m/s.	70	m/s.	70	m/s.	70	4.3	75	3.6	75	3.6	75	2.6
I	70	4.3	70	4.3	70	3.5	70	3.0	70	3.3	70	3.6	70	4.3	70	2.0	55	2.6	50	3.0	50	4.3	45	4.9
2	55	3.6	55	2.0	55	2.6	55	2.6	55	3.0	55	3.0	55 —	3.3	55	1.3	33	1.3	<u> </u>	1.3	J.	1.3	330	i.6
3	_	0.3		0.7		0.3		0.7		1.0		0.7			30	6.2	30	6.6	20	6.6	20	6.6	15	6.6
4	345	3.0	350	3.6	360	3.6	360	3.0	5	4.3	30	6.2	35	7.2	30	0.3	30	1.3	30	2.0		1.3		1.3
5		1.0		1.3	-	0.7	_	0.3	_	0.7	-	0.7		1.3		0 3		1 3	30		1	٦		
	l		Ī					0.0	220	2.0	225	4.6	225	4.6	330	4.9	325	3.9	310	3.9	315	4.3	320	5.2
6	300	2.3	300	2.3	310	3.9	320	3.9	320	3.9	325 320	4·6 2·0	335 320	1.6	320	2.3	325	2.0	335	1.6	335	1.6	330	1.6
7	_	0.7	_	1.0		0.7		1.3	350	2.3	260		255	3.9	255	6.6	260	7.5	260	7.5	250	8.2	245	8.2
8	260	2.0	260	2.6	260	3.9	255	3.6	255	4.3		3·3		7.5	235	6.9	240	7.9	240	6.6	240	6.9	245	6.6
9	245	6.9	245	7.9	250	7.2	245	6.9	245	5.9	245		240 250	5.9	245	8.2	245	6.2	245	6.2	250	5.6	260	5.6
10	240	5.6	240	5.6	245	5.9	235	6.2	235	0.2	240	5.9	250	39	243	~ ~	~43	~ ~	-43	-	-3-	,		Ŭ
				0.0	070	2.2	270	2.0	270	3.3	285	3.6	295	4.9	310	4.9	305	4.9	310	5.6	315	5.6	315	3.9
11	270	3.3	270	3.9	270	3.3	270	3.0	270	1.0	205	1.0	305	2.0	285	2.0	295	3.9	305	4.6	300	4.3	295	4.6
12	_	1.3		1.3	280	1.3	280	1.3	280	4.6	280	3.9	285	4.6	290	6.2	300	5.6	300	4.9	315	5.6	320	5.9
13	280	2.6	280	2.3	1	2.6				4.6	345	4.3	350	4.6	345	3.6	340	4.3	350	4.3	340	3.3	340	3.6
14	335	3.6	340	4.9	335	4.3	335	4·3	340 320	2.3	320	2.0	320	2.3	310	1.6	290	2.6	270	3.3	265	3.3	265	4.3
15	330	1.6	325	2.6	320	1.6	320	1.0	320	2 3	320	~ 0	320	~ 3	520		-,-		'		ľ			
		2.0	200	4.6	205	2.0	295	4.3	295	4.3	300	4.6	315	5.2	330	5.6	360	5.9	350	5.2	345	4.9	345	5.6
16	300	3.0	300	4.6	305	3.9	295	1.3	355	2.3	350	2.0	350	3.3	345	4.6	335	4.6	355	4.9	340	3.6	330	4.3
17	_	1.0	_	0.7		0.0	_	0.7	333	1.3	350	0.3	350	1.0	J73	i.0	_	i.3	_	i.3	325	1.6	270	2.0
18		0.3		0.3				2.3	230	2.6	230	2.3	230	3.0	230	2.3	230	1.6	245	2.6	295	3.6	310	3.9
19	250	2.0	250	2.0	250	2.3	250	2.6	305	2.6	305	2.3	305	2.6	330	4.3	340	3.6	350	5.6	355	5.6	345	6.2
20	305	3.6	305	3.6	305	2.6	305	2 0	303	~ 0	303	~ 3	202	- ×	33-		~ '	"	00	-				
_	1		205	1.6		1.0		1.3	305	1.6	290	2.0	265	3.3	265	3.3	295	3.6	285	2.6	290	3.6	295	3.3
21	-6-	1.3	305	i	l	2.0	245	2.6	245	2.3	245	3.3	290	4.3	290	3.9	300	4.3	305	4.9	295	4.9	305	4.9
22	260	2.3	255	1.3	245 295	2.6	260	2.0	260	2.0	260	2.3	265	2.3	295	3.6	305	3.6	290	2.3	295	2.0	295	2.3
23	305	1.6		1.0	293	0.7	200	1.0	325	1.6	320	2.6	330	4.6	330	4.3	325	4.3	315	4.6	310	4.3	320	3.3
24		1.3		1.6	310	1.6	310	2.0	310	2.0	310	1.6	310	3.6	315	3.9	310	3.3	305	4.6	335	3.9	345	3.9
25	310	1.6	310	1.0	310	1.0	310	20	3.0	~ ~	310	- 0	J			,	ľ							
26	l	7.2	l	0.2		0.3	l	0.7	_	1.0		0.7	_	0.3	_	1.0	l —	1.3		0.7	<u> </u>	1.3	10	2.0
26	-	1.3	I	0.3	l	0.7		0.7		0.0		1.0	10	2.0	10	2.6	10	2.6	350	3.3	250	2.6	250	2.3
27	-	1.3				1.3	l	0.7		1.0		0.7	l —	0.7	340	2.3	360	2.0	360	2.3	20	3.0	10	2.3
1		1.3		1.3	l	1.0	l	1.0	300	1.6		1.3	_	1.0	l —	0.7		1.3		1.3	305	1.6	-	1.3
29	-	0.7		0.7	_			0.7	300	1.0	60	1.6	345	2.0	345	2.6	325	2.0	285	2.6	265	3.6	295	4.3
30		0.3		0.7		0.7		J /	<b></b>		<u> </u>				<u> </u>						l		<del></del>	
Mean	_	2.2	_	2.3		2.2		2.7	_	2.6	-	2.7	-	3.3	_	3.6	_	3.7		3.8	_	3.9		3.9
	!	1	<u> </u>	1	<u> </u>	<u>'</u>	<u> </u>	1	<u> </u>	<u>!</u>		<u> </u>	<u>'                                     </u>		<u>'</u>	<u>'</u>	i	<u>'</u>	i				\ \r	
G.M.T.	<b>\</b>	I		2.	3	3.	4	ş.	!	5.	(	5.		7.		8.	1	9.	] 1	to.	]	ĮI.	INC	on.
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# WIND: DIRECTION AND SPEED.

Averages for periods of sixty minutes, centered at the exact hours, Greenwich Mean Time.

M.S.L. + ha (height of anemograph above ground) = 5 metres + 20 metres.

May, 1923.

13	3.	ı	4.	r	5.	ı	6.	ı	7.	1	8.	19	9.	2	о.	2	ı.	2	2.	2	3.	2	4.	Mean	Day.
225 275 190 215	m/s. 5·6 2·0 2·6 7·2	215 280 185 225	m/s. 5·6 2·6 4·6 5·9	215 270 195 225	m/s. 6·2 2·3 5·2 5·9	215 — 190 220	m/s. 5·9 1·3 4·9 4·9	205 270 190 210	m/s. 4·3 2·0 4·9 5·6	215 — 195 210	m/s. 3·9 1·3 4·3 4·6	220  195 215	m/s. 3·0 1·0 2·6 3·9	220 — 200 220	m/s. 2·6 1·0 1·6 3·0	220 	m/s. 2·0 0·3 2·0 2·6	230 - 225 225	m/s. 1·3 2·0 1·0 2·0	- - - - - 245	m/s. o·7 o·3 1·3 2·6	- - - - 255	m/s. 1·0 0·3 0·7 1·3 1·6	m/s. 4·6 1·2 2·1 3·0 2·2	1 2 3 4 5
290 5 60 235 325	3·3 1·6 3·6 4·3 3·3 5·2	270 360 65 245 345	3·3 2·0 4·3 4·3 3·0 4·9	265 360 75 280 330	1.6 4.9 3.6 5.2	215 250 10 85 225 320	1.6 4.3 3.9 3.6 4.6	150 — 35 90 260 285	5·6 1·3 3·9 5·2 3·6 5·2	255 95 75 300 280	4·6 1·6 4·3 4·3 3·9 3·6	255 90 75 305 285	5·6 1·6 5·2 3·6 2·3 3·0	255 90 75 305 270	4·9 2·3 4·3 2·0 1·6 3·9	255 95 75 320 260	5·2 2·0 3·3 2·6 3·9 4·6	95 75 345 250	3·3 1·0 5·6 2·0 1·6 5·2	95   235	1·3 3·0 1·0 1·3 6·9	95 40 345 230	1·3 2·3 2·6 2·3 8·2	1·9 3·2 2·5 2·4 4·4	6 7 8 9
295 250 275 265 230	7·9 5·6 5·9 4·6 7·5	290 260 280 265 220	7·2 2·3 5·2 4·6 7·5	295 265 270 255 215	7·9 3·0 5·9 5·6 6·6	295 305 285 255 215	7·2 2·3 5·2 5·6 5·6	295 295 285 260 210	7·9 4·3 5·2 5·2 5·9	300 260 270 260 225	4·9 6·2 6·6 4·9 5·6	290 265 265 250 265	2·3 5·2 5·2 3·9 5·6	295 270 260 220 235	3·6 3·9 4·9 5·6 3·3	285 245 250 220 220	3.6 3.6 4.3 4.3 3.6	265 240 245 220 245	3·3 3·0 5·6 4·9 2·3	265 240 255 210 240	2·0 3·3 4·3 5·6 2·0	265 240 250 215 240	1.6 3.0 4.3 4.6 2.6	5·9 3·5 4·2 4·3 5·9	11 12 13 14 15
290 275 285 265 245	6·2 5·6 3·0 4·3 6·2	310 310 295 265 240	6·6 4·6 3·3 2·6 6·6	285 285 300 270 250	7.5 5.6 3.0 3.9 7.2	295 265 300 265 255	6·2 4·9 1·6 3·3 5·2	295 275 300 260 250	5·2 5·6 2·0 2·3 6·9	285 270 305 265 245	5·2 3·6 1·6 1·6 4·9	260 285  280 250	3.6 3.9 1.3 2.0 6.9	260 290 — 280 245	3·3 2·3 0·7 3·0 5·6	295 290 — 280 240	2·3 2·3 1·0 2·3 5·9	285 275 — — 245	2·3 1·3 1·3 5·9	260 270 — 280 245	2·6 2·3 1·0 1·6 5·6	245 270 — 280 245	3·3 2·0 0·7 2·3 4·9	4·2 3·8 2·5 2·3 4·7	16 17 18 19 20
285 265 315 30 295	4·6 3·9 2·3 2·3 4·3	310 280 325 — 305	3·6 5·9 1·6 1·3 4·6	310 270 10 5 305	3·6 4·9 1·6 2·0 5·2	305 265 20 345 340	4·3 4·9 4·3 1·6 5·2	305 265 35 — 345	3.6 4.9 5.2 1.3 2.0	300 270 40 315 300	2·6 4·6 5·6 1·6	300 270 55 280 285	2·0 4·3 4·6 2·0 2·3	265 55 275	1·3 3·6 3·9 2·6 1·3	300 240 55 215 295	3·0 3·9 3·9 3·0 2·0	300 245 55 220 300	2·3 3·6 3·0 2·6 2·0	300 255 55 220	2·3 3·3 3·0 2·6 I·0	300 255 55 225	1·6 3·0 2·6 3·0 0·7	3·4 3·5 3·8 2·5 3·1	21 22 23 24 25
350 40 35 45 100	3·3 4·3 5·6 6·9 5·2	360 30 30 50 80	3·3 3·6 4·3 5·9 3·6	360 35 25 55 80	3·9 4·6 3·0 6·2 5·9	15 35 60 55 105	4·9 4·6 3·9 4·9 6·2	30 30 120 45 115	4.6 5.6 5.2 5.9 5.9	35 40 125 45 100	3.6 4.6 3.9 4.6 6.6	35 40 70 45 85	3·0 4·3 4·6 6·6	65 40 65 50 80	3·0 3·6 2·0 3·9 5·9	70 40 40 50 75	1.6 3.6 4.3 3.0 5.6	70 40 40 50 80	1.6 1.6 4.3 1.6 4.6	70 40 40 — 85	1.6 1.6 2.6 0.3 5.9	 40  85	0·7 1·3 2·0 1·0 4·3	3·4 3·1 3·9 3·8	26 27 28 29 30
70	4.6	65	4.3	65	5·2 4·6	7º 	5·2 4·3	7º —	4.6	65	5·2 4·I	8 ₅	3.7	85	3.2	75	3.3	70	2.9	70	2.5	7º —	4·3 2·4	3.4	31

# June, 1923.

	Ť		1								8.							1		1		1		l	Day.
_ 4	4.3 - 4.		4·I	_	4.0		4.0		3.8	-	3.4		2.9		2.5		2.4	_	2.4		2.4		2.1	3.1	
240 3 355 2 325 2	2.3	10 240 310 325 285	3.0 2.6 2.3 2.0 3.0	10 285 290 325 270	3·3 1·6 2·0 2·0 2·6	10 230 295 325 310	3.0 2.6 2.3 2.0 3.0	10 230 295 325 315	3.0 2.0 2.6 2.0 3.3	10 285 — 325 315	2·3 2·6 0·7 2·3 2·0	10 300 10 315	1·6 3·0 0·7 2·6 1·6	300  60 310	1·3 3·0 1·0 2·0 2·3	300  60 305	1.0 3.3 1.0 1.0	 300  	0·7 2·3 0·7 0·7 1·3		0·7 0·3 1·0		0·7 0·7 0·3 0·3	1·4 2·0 1·5 1·4 2·0	26 27 28 29 30
305 5 265 3 335 4	5·6   3 3·9   2	280 320 290 300 360	3·0 4·6 3·3 3·0 3·6	290 325 285 295 360	3.6 3.6 4.3 3.6 3.6	270 320 315 310 360	3·9 4·6 3·6 3·3 1·6	270 325 310 330	3·0 5·6 3·3 3·0	265 315 320 330 360	3.9 3.3 3.0 3.0	260 305 330 330 360	1.6 2.0 1.6 3.0 2.0	260 305 — 330 360	2·0 1·6 1·3 3·9 2·0	330 330 360	1·3 1·6 2·6 2·0	260 305 330 310 360	1.6 1.6 1.6 2.0 2.0	260 — 330 305 —	2·6 1·6 3·0 1·3	260 305 330 310	2·0 2·0 1·3 1·6 0·3	2·5 3·3 2·5 2·9 2·5	21 22 23 24 25
340 4 225 2 300 4	1·9 2·3 1·6	335 350 240 310	3·6 3·9 2·0 5·2 5·6	320 335 245 305 345	3·9 3·6 2·6 4·9 5·2	320 350 245 310 355	3·9 4·6 2·3 4·9 4·9	320 350 250 300 360	3·3 3·3 2·6 4·6 3·9	320 345 250 305 360	2·6 3·0 2·0 4·3 3·6	320 — 250 305 360	2·0 1·3 1·6 3·9 1·6	250 305	1.0 0.7 1.6 3.6 1.3	- - 305 -	1.3 0.3 1.0 3.3	— — 305 —	1·3 0·3 1·0 3·3	355 — 250 305 —	2·0 0·3 1·6 4·3 1·0	355 — 250 305 305	1.6 0.0 1.6 3.3 2.0	3·7 2·5 <b>1·4</b> 3·3 3·4	16 17 18 19 20
290   4 305   5 325   3	1·9 3·6	345 295 305 340 240	6·6 5·9 7·5 2·6 3·3	345 285 320 325 230	4·6 5·6 7·5 3·3 3·6	355 285 340 315 220	5·2 5·2 6·9 3·3 3·9	360 285 360 310 220	5·2 6·6 6·2 3·3 3·0	360 290 350 325 220	4·9 5·2 6·2 3·3 2·3	355 290 340 — 220	3·3 4·6 7·2 1·3 1·6	355 275 330 330 220	2·0 3·9 4·6 1·6 1·6	355 270 330 330 220	2·0 3·3 4·6 2·6 1·6	270 330 330 220	1·3 3·0 5·9 3·0 2·6	270 340 330 230	0·7 3·3 5·9 2·3 3·3	275 335 — 300	1·3 3·6 4·3 1·3 3·0	3·9 3·4 5·1 3·4 2·6	11 12 13 14 15
320   2 245   9 245   7	9·8   2 7·5   2	35 285 245 240 290	2·3 3·3 9·5 6·6 7·9	270 245 235 290	1·0 2·6 9·8 6·9 8·2	245 255 235 290	0·3 3·9 8·2 6·9 7·2	250 260 235 295	0·3 3·9 7·5 6·2 6·9	250 260 230 300	0·7 3·6 6·9 6·2 6·2	260 255 240 305	0·7 3·6 7·9 5·9 5·2	260 250 240 290	0·3 2·3 6·2 6·2 5·2	255 245 240 285	0·7 3·0 7·5 5·9 4·9	250 245 240 280	1·0 3·3 5·6 6·9 5·2	255 245 240 275	1.0 2.6 6.9 7.2 4.3	10 260 245 245 270	1·6 3·0 5·6 6·9 3·6	2·6 2·3 6·3 <b>6·8</b> 6·1	6 7 8 9 10
75 2 50 4 275 2 20 5	1.3	55 270 15	m/s.   1·3 3·9 3·6 5·2 1·6	70 50 280 20 355	m/s.   2·6   3·3   3·0   5·9   2·3	55 50 305 20 350	m/s. 4·6 3·9 3·0 5·2 2·0	55 50 330 10 350	m/s. 3·9 3·6 3·9 4·3 2·0	55 50 320 20	m/s. 3·6 3·9 3·9 1·0	55 50 340 20	m/s. 2·6 2·6 5·2 3·6 1·3	55 50 340 20 350	m/s. 2·3 3·3 4·3 2·6 1·6	55 55 335 25 300	m/s. 3·3 2·0 3·3 2·3 2·0	55 55 340 25 285	m/s. 3·6 2·3 3·6 1·6 2·0	55 55 350 — 280	11/s. 2·6 1·6 3·6 1·0 2·0	55 — 350 — 295	m/s. 2·6 0·3 3·3 1·0 3·3	m/s. 3·3 3·0 2·2 4·5 <b>1·4</b>	1 2 3 4 5

Direction expressed in degrees from North ( $E=90^{\circ}$ ,  $S=180^{\circ}$ ,  $W=270^{\circ}$ , N=360): Speed in metres per second.

458. Richmond (Kew Observatory):

Ha (height of cups of anemograph above M.S.L.) = Height of ground above

Day.		Ι.		2.		3.		4.		5.		6.		7.		8.		9.	I	о.	1	Ι.	No	oon.
1 2 3 4 5	° — — — 225 —	m/s. 1·3 0·3 1·3 2·6 1·0	225	m/s. 1·0 0·7 1·3 2·6 0·7	305 — — 225 —	m/s. 2·0 0·7 1·0 3·0 0·0	305 — 205 220	m/s.   1·6   1·0   1·6   3·3   0·3	305  205 220	m/s. 2·0 0·7 3·0 4·3 0·3	205 215	m/s. 0·7 1·0 2·6 3·9 0·3	° — 205 210 —	m/s. 1·3 1·0 2·3 4·9 0·0	305 	m/s. 2·0 1·0 3·0 4·6 1·0	310 255 210 215 110	m/s.   3·3   2·3   4·3   4·9   1·6	325 250 205 215	m/s. 3·6 2·6 4·6 4·3 1·3	310 255 205 220 135	m/s. 4·3 2·3 4·3 4·6 2·3	335 260 205 215 160	m/s. 3·3 2·0 5·6 3·9 2·6
6 7 8 9	90 85 215 250 45	3·3 2·3 1·6 1·6 3·9	90 85 215 — 60	2·6 1·6 1·6 0·7 3·0	90 85 215 — 75	2·6 2·0 1·6 1·0 1·6	90 85 — — 90	2·3 2·6 1·3 1·3 2·0	90 85 215 — 75	3·3 1·6 2·3 0·3 3·3	90 85 215 — 50	3·9 2·3 2·6 0·3 4·9	90 85 230 — 50	4·3 2·6 3·3 1·3 2·6	90 120 240 — 50	4·3 3·0 3·9 0·7 2·0	90 130 265 — 45	4·9 3·3 4·6 1·0 1·6	80 140 260 — 40	5·9 3·9 3·9 0·7 3·6	85 145 260 180 20	6·2 3·9 3·6 1·6 3·0	90 160 255 185 25	6.6 4.3 3.3 2.0 3.0
11 12 13 14 15	85 - 210	0·7 0·3 2·3 0·7 1·6	 85 	0·3 0·7 2·6 0·3 1·0	 85  210	0·0 0·7 1·6 1·3 2·0	 85 	0·7 0·3 2·0 1·0	85  210	0·3 0·3 1·6 1·0 2·0	 85  210	0·3 0·3 1·6 0·7 1·6	85 - 210	0·7 0·3 1·6 1·3 2·3	85  210	1.0 0.3 2.3 1.3 2.6	 175 80 220 235	1·3 2·0 3·3 2·3 2·3	 125 90 225 240	1·3 2·6 5·6 2·6 2·3	125 110 85 245 215	1·6 3·3 4·9 1·6 4·9	180 100 105 — 230	2·0 3·0 4·3 0·3 4·9
16 17 18 19 20	225 270 255 — 210	5·6 2·0 2·3 1·0 2·3	225 270 260 — 210	3.6 1.6 1.3 3.0	225 270 260 — 210	2·6 1·6 2·6 1·3 2·6	225 255 260 270 210	3·3 2·6 1·6 1·6 3·6	225 250 260 — 210	3·9 3·0 2·0 1·0 3·0	225 235 260 270 210	3·9 3·0 2·6 1·6 2:6	225 220 260 270 230	3·9 3·3 2·6 1·6 3·6	230 235 260 255 235	4·3 3·9 3·0 2·3 3·6	225 240 260 220 230	3·3 4·9 3·3 3·6 5·2	245 235 245 210 235	5·2 4·6 3·3 4·9	260 235 255 215 250	5·9 4·6 3·9 4·3 5·6	255 230 265 230 245	5·9 3·6 3·3 4·3 5·6
21 22 23 24 25	245 260 240 230 200	2·6 1·6 2·3 2·0 2·6	245 260 240 255 200	3·0 1·6 2·0 2·6 2·0	245 260 240 290 200	3·6 2·3 2·6 1·6 3·3	245 260 230 295 200	3.0 3.3 1.6 2.3	260 260 220 — 200	3·0 2·6 3·6 1·0 3·9	250 255 215 — 200	3·6 4·6 1·0 3·3	255 235 210 295 205	3·3 3·3 5·9 2·3 4·3	255 215 215 295 235	3·3 5·6 3·3 4·3	255 220 210 300 240	3·3 3·6 5·9 3·0 5·2	235 240 215 275 240	3.6 3.3 6.2 3.6 3.3	240 260 220 265 225	4·3 3·3 6·6 3·0 6·6	245 235 230 265 240	3·9 3·9 6·6 3·0 4·3
26 27 28 29 30	225 260 195 245 205	3.0 2.6 4.9 2.3 3.0	225 — 195 245 205	2·3 1·3 4·6 2·0 3·6	225 260 190 245 210	3.0 2.0 4.3 2.3 3.6	225 — 190 245 220	2·6 1·3 3·3 2·0 3·9	225 260 190 245 225	2·6 1·6 4·6 2·6 4·3	225 260 190 240 230	3·9 2·0 4·9 2·3 4·6	240 260 185 240 230	4·3 2·3 5·6 3·3 4·6	250 265 190 235 245	5·9 2·6 5·9 3·0 4·9	250 295 185 230 245	5.6 3.0 5.9 3.3 5.6	260 280 190 215 235	5·6 3·3 6·2 4·6 6·9	260 250 185 210 240	6·6 3·3 6·6 4·3 5·2	260 250 185 220 245	5·9 3·0 6·2 4·3 5·2
Mean	205	2.3	205 —	4·9 2·0	210	4·3	215	4·6 2·I	210	4·9 2·4	215	2.6		2.9	225	3.1	215 —	3.7	215	4.0	210	5·9 4·3	205	4.0

#### 459. Richmond (Kew Observatory): $H_a = 5$ metres $\pm 20$ metres.

459. K	1CHIH	ma (i	VAM (	UDSOF	vator	<b>y</b> ): 1	a =	5 me	tres -	+ 20	metr	es.												
	ı °	m/s.	۰	m/s.	۰	m/s.	٥	m/s.	٥	m/s.	٥	m/s.	٥	m/s.	ı °	m/s.	·	m/s.	°	m/s.	٥	m/s.	°	m/s.
I	250	5.2	250	4.3	250	3.3	250	2.3	240	3.3	240	3.0	240	5.2	250	5.2	245	5.2	250	5.2	245	5.6	250	6.6
2	225	1.6	225	2.0		1.3	225	2.6	220	2.6	180	2.6	170	3.9	170	4.6	160	6.6	160	7.2	175	8.9	180	8.9
3	215	5.6	215	6.2	220	5.6	220	5.2	220	4.6	225	4.6	225	5.9	235	6.6	240	6.9	240	2.0	235 200	7.2	250	7.9
5		0.0	_	0.3		0.3	_	0.7		0.7	240 180	2.0	240	2.3	135	2.3	155	1.3	235 160	5.2	160	5.9	165	4.9
,	]			ر	Ì	0 3	1	" /	Ì		100			1	-33	7 3	-33	4.3	100	] ] [	100	1 3 9	100	4 9
6	180	2.0	<u> </u>	1.0	180	1.6	l —	1.3	_	1.3	180	1.6	180	2.0	245	2.0	260	2.0	250	3.0	245	2.3	240	2.6
7	1 —	1.0	_	1.3		1.0		0.7	_	0.7	_	0.3		1.3	245	2.6	210	3.3	220	4.3	230	$5 \cdot 4$	220	5.1
8	205	1.6	205	1.6	205	2.0		1.0	205	1.6		1.3	205	2.0	220	2.3	210	2.6	200	2.3	215	3.0	195	3.0
9 10	260	0.3	260	2.0	<u>260</u>	0.3	260	0.3	<u></u> 260	0.0		1.0	_	1.3		1.3	230	2.3	215 260	3.6	220 230	3.9	230 230	3.6
	200	1	100	- 0	200	1 0	200	2 0	200	1 0		1 0		1 3		- 3		+ 3	200	- 0	230		~30	1 0
11	355	2.0	_	1.3		1.3	355	1.6	355	1.6	355	2.0	355	2.3	360	2.6	10	2.0	355	2.0	320	2.0	345	2.0
12	l —	0.3	_	0.3		1.3	_	0.3		0.7	—	0.7	-	1.0	50	1.6	120	2.6	125	3.0	130	2.6	130	2.6
13	155	1.6		0.7		I.0	<u> </u>	0.7	-	0.3	-	1.0	155	1.6	160	3.0	205	2.6	210	4.3	210	4.9	215	4.9
14 15	210	2.0	270	3.6	340	0.0	330	0.3	320	0.3	325	2.6	3 ² 5	3.3	325	3.3	330	3.6	335	0·7 4·6	340	5.9	260 330	4.9
1.5	210	2 0	2,0	3 0	340	4.6	330	3.3	320	3.0	323	20	323	3 3	323	3 3	330	3 °	333	4 ~	340	39	330	49
16		1.0	_	1.0	320	1.6	'	1.0	-	1.3	275	2.0	250	2.0	270	3.6	280	3.6	270	3.9	280	3.6	285	3.9
17	260	2.0	260	1.6	260	2.0	260	2.0	235	3.9	215	5.2	205	5.9	205	6.9	215	8.5	215	7.5	205	6.6	205	7.2
18	225	3.6	225	3.9	225	3.6	225	3.3	225	3.9	225	3.9	225	3.9	230	5.2	245	4.6	250	5.6	250	5.6	240	6.6
19 20	270	2.3	270	1.6	270	2.0	270	1.6		0.7	220	1.0	265	2.0	225	3.3	250 220	2.3	245 210	3.3	240 210	3·6 4·9	250	2.6
20	255	2.6	255	2.0	250	3.0	240	2.6	235	3.0	230	3.0	230	3.0	225	3.3	220	2 3	210	4.3	210	49	210	3.9
21	200	4.6	200	5.6	200	5.2	200	4.6	190	4.3	190	3.6	190	3.9	185	4.9	200	8.2	200	9.2	205	9.2	200	8.5
22	225	3.6	215	4.6	210	4.9	215	4.3	215	5.6	215	5.2	225	5.9	230	5.6	230	6.2	235	6.6	230	8.2	235	7.5
23	240	3.0	240	2.6	240	2.6	240	1.6		1.0	240	1.6	230	3.6	215	5.2	210	6.6	195	7.2	195	7.9	185	6.9
24	165	4.6	180	3.6	195	3.6	200	2.0	200	1.6	_	0.7	_	0.7	_	0.3		0.7	255	0.0	210	1.3		1.3
25	275	2.6	275	2.3	310	2.6	_	1.3	_	1.3	330	1.6	320	2.3		1.3	300	2.0	255	2.3	210	3.3	205	3.9
26	190	5.2	195	5.9	190	6.2	185	6.9	190	6.2	190	4.9	195	5.9	195	5.6	205	6.2	210	7.2	210	6.2	210	4.9
27	195	3.0	195	3.0	195	2.3	195	2.3	195	2.3	195	2.3	210	3.6	230	4.3	235	4.6	235	5.2	230	5.2	235	4.9
28	220	4.3	230	3.9	220	3.9	230	4.6	240	4.6	240	4.3	230	4.9	230	6.2	235	6.9	230	6.2	² 45	6.6	240	6.9
29	240	2.0	_	1.0		0.7	-	0.3		0.3	_	1.3		1.0	230	2.0	180	1.6	130	2.6	120	4.3	155	6.6
30	265	9.5	260	8.2	250	7.5	240	6.2	240	6.6	235	6.6	240	7.5	250	7.9	240	8.2	250	9.5	235	8.5	240	8.2
31	230	2.3	230	2.0		1.3		0.7		0.7	230	1.6	230	2.3	230	3.3	225	3.6	220	4.3	215	15 4.9 2		4.3
	- <u>-</u> -							<u> </u>																
Mean	-	2.7	_	2.6		2.5		2.2		2.3		2.4		3.0		3.4	_	4.0	_	4.2	_	4.9		4.8
G.M.T.		I.	2	2.	:	3.	•	4.		5.		5.		7.	8	8.	,	9.	1	о.	1	ı.	No	on.

Averages for periods of sixty minutes, centered at the exact hours, Greenwich Mean Time.

M.S.L.  $+ h_a$  (height of an emograph above ground) = 5 metres + 20 metres.

July, 1923.

13	j.	I.	4.	I	5.	10	6.	I	7.	I	8.	1	9.	2	0.	2	ı.	2	2.	2	3.	2.	4.	Mean	Day.
325 235 210 225 190	m/s. 3·9 2·6 5·2 4·6 3·0	300 220 215 235 160	m/s. 3·0 3·0 4·3 3·9 2·3	285 225 215 230 155	m/s. 3·0 3·3 4·6 5·2 2·6	295 220 215 220 180	m/s. 3·0 3·3 4·6 4·9	315 210 215 220 175	m/s. 2·3 3·9 4·9 4·6 2·6	315 200 225 220 100	m/s. 2·0 3·6 3·6 3·9 5·2	200 225 215 95	m/s. 1·3 3·9 3·6 3·9 5·9	200 225 210 95	m/s. 1·3 3·0 3·6 2·0 4·9	315 200 225 210 90	m/s. 2·0 2·6 3·6 1·6 4·6	315 205 225 —	m/s. 1·6 2·6 2·3 1·0 4·9	205 225 —	m/s. 1·0 2·3 3·0 1·0 4·3	- - 225 - 90	m/s. 0·3 1·3 2·3 0·7 4·3	m/s. 2·I 2·I 3·3 3·5 2·3	1 2 3 4 5
85   170   235   165   25	6·9 3·9 3·3 2·3 3·6	80 165 235 150 35	7·5 4·6 3·0 2·6 3·0	80 170 220 155 75	7·5 3·9 2·6 3·0 5·2	85 180 230 145 75	7.5 3.3 2.3 3.6 3.3	90 185 245 140 75	6·9 4·6 2·6 3·0 3·0	85 185 255 130 80	6·9 3·9 3·0 3·3 2·3	90 195 270 90 185	6·6 3·6 1·6 5·2 2·0	90 215 — 85	4·6 3·6 1·3 5·2 1·0	85 215 250 85	5·6 2·0 2·0 5·2 1·0	85 215 250 85 185	4·3 2·3 1·6 4·3 1·6	85 215 250 160	3·6 2·3 1·6 2·6 0·7	85 215 250 70	3·0 1·6 2·0 3·3 1·0	5·I 3·I 2·5 2·3 2·6	6 7 8 9
85 135 250 220	1·3 3·3 4·6 2·0 5·6	190 100 160 220 225	1.6 4.3 5.2 2.0 5.9	190 95 165 205 240	1.6 3.6 6.9 3.0 6.2	85 170 210 245	1·3 3·6 5·6 2·0 5·6	190 85 180 — 260	1.6 3.6 4.3 1.3 4.6	85 180 — 230	1·3 3·3 3·6 1·0 4·9	- 85 185 - 230	1·3 3·6 3·3 1·0 4·9	 85 190  235	1.0 3.0 1.6 1.3 3.9	85 190 210 230	0·7 3·0 2·3 2·3 5·2	85 - - 225	1·3 2·6 0·7 1·0 4·6	- 85 - - 225	0·7 3·3 1·3 1·0 3·6	85 — — 225	0·7 3·3 1·3 1·3 3·9	1.0 2.2 3.1 1.4 3.6	11 12 13 14 15
260 250 255 240 250	5·9 3·6 3·6 5·2 5·2	265 200 260 235 255	4.6 6.9 3.6 3.6 4.6	265 200 265 230 250	5·6 4·9 3·6 4·6 4·3	260 215 270 225 250	4·3 3·6 3·6 4·9 3·6	275 215 270 220 235	4·3 3·3 3·0 2·0 3·9	265 225 270 210 235	3·3 3·6 2·0 3·6 3·3	270 240 — 205 240	2·3 2·3 1·0 3·9 3·0	270 215 — 205 240	2·6 3·3 1·3 3·6 2·6	270 215 270 205 240	1.6 4.3 2.6 2.6 3.0	270 230 270 210 240	3.0 3.9 1.6 3.0 2.3	270 255 270 210 240	2·0 2·0 2·3 2·6 2·3	270 220 — 210 245	2·0 3·0 1·3 2·3 2·0	3·9 3·5 2·6 2·9 3·6	16 17 18 19 20
245 235 240 255 245	3·0 4·6 5·2 3·0 3·6	235 245 240 240 245	3·9 4·3 5·2 2·6 3·3	255 250 235 255 210	3·9 4·6 4·3 3·0 4·3	250 240 220 255 205	3·0 3·9 5·6 3·9 4·3	255 240 235 255 210	3·9 4·6 4·9 3·0 4·3	255 225 235 255 215	3·3 3·6 3·6 3·6	260 225 215 240 225	3·6 3·9 3·3 3·9	260 230 215 240 215	2·0 3·0 3·0 2·3 3·6	260 230 215 210 215	2·3 3·3 2·6 3·3 3·9	260 230 220 200 225	2·6 3·6 2·6 2·3 2·6	260 235 220 200 225	2·6 3·9 2·6 3·6 2·3	260 240 230 200 225	2·0 2·6 2·3 2·3 2·3	3·2 3·3 4·2 2·7 3·7	21 22 23 24 25
265 260 180 225 220	6·6 3·0 7·9 4·3 5·6	270 230 200 220 205	6.6 3.6 7.5 4.9 7.2	275 235 210 220 205	6·6 3·0 6·6 5·6 5·2	280 240 205 230 205	6·9 2·6 7·5 5·2 6·6	275 225 210 240 205	6·9 3·9 6·9 4·9 7·9	270 230 230 240 205	6·2 3·6 5·2 4·6 7·2	275 225 240 245 195	4·9 3·6 4·3 3·0 6·6	265 225 245 — 200	3·6 2·3 3·3 1·0 7·5	255 210 245 215 195	3·9 3·3 4·3 5·9	260 210 245 210 200	3·6 3·6 3·0 4·9 6·2	260 205 245 210 200	2·6 4·3 2·6 4·9 5·6	260 200 245 205 200	2·3 3·6 2·3 3·9 5·2	4·6 2·9 5·2 3·6 <b>5·5</b>	26 27 28 29 30
195	5·2 4·3	185	4.3	185	4·9 <b>4·4</b>	175 —	3·6 4·1	185 —	3·6 4·0	180	3.8	225	4·9 3·5	240	3.0	230	3.1	225	2.9	- 225	2.7	²³⁵	2.4	3.2	31

#### Aurust 1993

This is a contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the co																								Augu	st, 19	23.
245   5.9   240   6.02   240   5.02   240   5.02   250   4.06   245   4.90   240   2.02   230   2.02   231   2.02   232   2.05   2.02   5.02   2.02   5.02   2.02   5.02   2.02   5.02   2.02   5.02   2.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02   5.02	, 0	m/s.	٥	m/s.	0	m/s.	٥	m/s.	0	m/s.	٥	m/s.	°	m/s.	0	m/s.	0	m/s.	· ·	m/s.	o	l m/s.	1 °	l m/s.	m/s.	· · ·
185   8-2   180   9-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   8-5   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190   190	245	5.9	240	6.2	240	5.2	240	5.9	250		245		240		230		225		225							1
210   2-3   210   2-3   210   2-0   200   2-3   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   175   3-9   3-9   3-9   3-9   3-9   3-9   3-9   3-9   3-9   3-9   3-9   3-9   3-9   3-9	185		180			8.5	190	8.2		8.5	215	7.2	215	6.9	210	7.5	210	6.2	210	5.6	220	5.6	215	5.2	5.7	2
160   4·9   155   5·6   165   5·2   170   4·9   170   4·9   170   4·6   180   2·3     1·0   180   2·0     1·0     1·0       1·0       1·0       1·0       1·0         1·0           1·0           1·0           1·0           1·0           1·0           1·0           1·0           1·0         1·0         1·0           1·0             1·0	240	8.5	250	l .	245		245			6.9		5.9		4.3		2.6	240	3.3	240	2.6	240	2.3	240	2.0	5.6	3
255 3.0 255 3.0 265 3.6 .260 3.0 265 3.3 255 2.3 265 1.6 — 1.0 — 1.0 — 0.7 — 1.0 — 1.0 — 1.0 2.0 216 4.7 230 4.7 230 4.7 225 3.9 225 3.3 215 3.6 225 3.3 215 3.6 225 3.9 225 3.9 225 3.3 215 3.6 225 3.9 225 3.9 225 3.3 215 3.6 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3.9 225 3	1						1								180	1.6	<u> </u>	0.7		0.0		0.7		0.0	1.7	4
275   4-7   276   4-7   276   4-7   276   4-7   276   4-7   275   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   3-9   225   225   225   225   225   225   225   225   225	160	4.9	155	5.6	165	5.2	170	4.9	170	4.9	170	4.6	180	2.3		1.3	_	1.0	180	2.0		1.0	-	1.3	2.7	5
100   3 \cdot 0   180   3 \cdot 0   180   3 \cdot 3   180   3 \cdot 3   180   3 \cdot 3   175   3 \cdot 3 \cdot 5   2 \cdot 0   2 \cdot 5   3 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot 5   2 \cdot	255	3.0	255	3.0									-					,	_	0.7		1	_	1.0	2.0	6
250 3-9 240 3-9 250 4-3 245 3-3 255 2-6 225 2-0 295 2-0 295 2-0 295 1-6 295 3-6 245 3-6 255 3-6 260 2-6 2-4 1-8 1-8 1-8 1-8 1-8 1-8 1-8 1-8 1-8 1-8	1					i .					_		-						•		_		205			7
			1				1																			8
315 2 0 — 1 1 3 310 2 0 315 2 0 330 2 3 335 2 3 10 2 0 — 1 3 10 1 6 — 1 3 — 0 3 — 0 3 1 8 18 135 3 0 120 2 9 135 3 3 135 3 9 145 3 9 160 3 6 165 2 3 160 2 0 155 1 6 155 1 6 — 1 0 — 1 1 0 2 0 2 0 2 0 2 0 2 0 2 0 2 0 0 2 0 0 2 0 0 2 0 0 2 0 0 2 0 0 2 0 0 0 0 0 0 0 0 0 0 1 1 3 0 0 1 6 0 0 0 1 3 0 0 1 8 18 135 3 0 1 120 2 9 135 3 3 135 3 0 145 3 9 160 3 6 165 2 3 160 2 0 155 1 6 155 1 6 — 1 0 — 1 1 0 2 0 2 0 2 0 2 0 2 0 0 2 0 0 0 0 0	1 -									1	. ~															9
153   3 \cdot 0   120   2 \cdot 0   135   3 \cdot 3 \cdot 125   3 \cdot 0   4 \cdot 3 \cdot 4 \cdot 4 \cdot 6   245   4 \cdot 9   255   4 \cdot 3 \cdot 265   3 \cdot 3 \cdot 265   3 \cdot 3 \cdot 260   2 \cdot 3 \cdot 260   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 3 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20   2 \cdot 20		1.3	205	2.0	270	2.0	255	2.0	205	2.0	295	2.0	295	2.0	_	1.0	295	1.0	295	2.0	345	2.0	355	1.0	1.8	10
220 5·2 250 4·9 250 4·3 240 4·6 245 4·9 250 5·4 3 260 2·0 260 2·0			—					1																		11
220   2·0   -     1·3   260   2·0   260   2·0   310   5·2   315   5·6   310   4·9   310   5·2   315   5·6   320   3·0   320   3·0   320   3·0   320   3·0   320   2·3   -   1·3   3·8   3·8   2.0   3·5   3.0   3.0   320   3·0   320   3·0   320   2·3   -   1·3   3·8   3·8   2.0   3·8   2.0   3·9   2.0   3·9   2.0   3·9   2.0   3·0   2.0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·0   2·				_																		1				12
325			250										205		205			- 1			_		_			13
270  3·9  270  4·3  270  3·0  285  2·6  265  3·3  260  2·6  265  1·6  265  2·6  — 1·3  265  2·0  265  1·6  265  2·3  2·5  205  8·2  210  8·5  215  7·2  210  7·2  220  4·6  240  4·9  240  5·6  240  3·9  230  4·9  230  4·9  225  3·9  5·3  260  3·3  260  3·3  290  3·6  275  4·3  290  4·9  275  2·6  270  2·6  270  1·6  270  2·0  270  2·0  270  2·0  270  2·6  270  2·6  3·7  245  2·6  265  3·3  260  3·6  270  3·3  260  2·6  260  4·6  200  4·6  200  4·6  200  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265  2·3  265	1 -		210		1	I .		1	1				220		220						240	3 I				14
205 8-2 210 8-5 225 7-2 210 7-2 220 4.6 240 4.9 240 5.6 240 3.9 230 4.9 230 4.9 225 3.9 5.3 260 3.3 260 3.6 275 4.3 290 4.9 275 2.6 270 2.6 270 1.6 270 2.0 2.0 270 2.0 270 2.6 270 2.6 3.7 245 2.45 2.6 265 3.3 260 3.6 270 3.3 260 2.6 265 1.0 265 1.0 2.6 2.7 1.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2	323	4 9	310	5 2	313	3.0	310	4.9	310	5.2	313	3.0	320	3.0	320	3.0	320	3.0	320	2.3	_	1.3		1.0	3.0	15
260 3·3 260 3·3 260 3·6 275 4·3 290 4·9 275 2·6 270 2·6 270 2·6 270 2·6 270 2·6 270 2·6 270 2·6 270 2·6 270 2·6 3·7 245 2·6 265 3·3 3 260 3·6 270 3·3 260 2·6 265 1·6 265 2·0 265 2·3 265 2·3 265 2·3 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 2·0 265 3·0 2/0 2·0 2/0 2/0 2/0 2/0 2/0 2/0 2/0 2/0 2/0 2/	270		270	4.3	270	3.0	285	2.6	265	3.3	260	2.6	265	1.6	265	2.6	_	1.3	265	2.0	265	1.6	265	2.3	2.5	16
200 3.3 200 3.3 200 3.6 275 4.3 200 4.9 275 2.6 270 2.6 270 2.6 270 2.0 270 2.0 270 2.0 270 2.6 270 2.6 3.7 245 2.0 265 2.0 265 2.0 265 2.0 265 2.0 265 2.0 265 2.0 265 2.0 265 2.0 265 2.0 2.3 265 2.0 265 2.0 265 2.0 2.3 265 2.0 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 265 2.0 2.3 2.3 265 2.0 2.3 2.3 265 2.0 2.3 2.3 265 2.0 2.3 2.3 2.0 2.0 2.3 2.3 2.0 2.0 2.3 2.0 2.0 2.3 2.0 2.0 2.3 2.0 2.0 2.3 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0		1					210	7.2	220	4.6	240	4.9	240	5.6	240	3.9	230	4.3	230	4.9	230	4.9	225	3.9	5.3	17
220																1				2.0		2.6	270	2.6	3.7	18
205 8·5 200 8·9 200 8·5 210 5·6 245 5·6 245 5·6 245 5·6 245 5·9 240 250 3·6 250 2·6 250 2·6 245 3·3 230 4·3 225 3·6 5·6 235 7·5 240 7·5 235 8·2 235 8·5 230 7·2 245 5·9 240 5·9 240 4·3 240 3·6 275 2·0 275 1·6 252 200 4·3 200 4·3 200 4·9 200 5·2 205 5·9 190 5·2 190 5·2 190 4·3 190 5·6 195 5·2 190 4·3 190 5·6 195 5·2 190 4·3 190 5·6 195 5·2 190 4·3 190 5·6 195 5·2 190 4·3 190 5·6 195 5·2 190 4·3 190 5·6 195 5·9 240 5·9 245 5·9 245 5·2 245 5·9 240 4·3 240 2·6 240 2·6 240 2·6 240 3·0 5·6 100 4·9 100 200 200 200 200 200 200 200 200 200									1	1			_		265				265		265	2.0	265		2.3	19
235	220	4.3	210	4.0	200	2.2	200	3.9	200	4.6	200	4.6	200	2.3	205	2.6	205	3.6	200	3.3	200	3.9	200	3.9	3.2	20
235	205	8.5	200	8.9	200	8.5	210	5.6	245	5.6	245	4.0	250	3.6	250	2.6	250	2.6	245	3.3	230	4.3	225	3.6	5.6	21
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	235			7.5	235	8.2	235	8.5								l .	-						-			22
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	185	6.9	185	7.2	180		175	3.6																		23
215   4·3   200   4·3   200   4·9   200   5·2   205   5·9   190   5·2   190   5·2   190   4·3   190   5·6   195   5·2   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190   4·3   190	205			ı		1	_ ~		265												275		275			24
260   5.6   265   4.6   220   5.6   200   3.9   230   3.6   200   3.3   210   4.9   210   5.2   210   4.9   210   5.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   4.6   4.9   210   5.9   220   2.6   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   4.9   2.0   2.0   2.0   4.9   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0   2.0	215	4.3	200	4.3	200	4.9	200	5.3	205	5.9	190	5.3	190	5.3	190	4.3	190	5.6	195	5.3	190	4.3	190	4.3	3.2	25
260       5·6       265       4·6       220       5·6       200       3·9       230       3·6       200       3·3       210       4·9       210       5·2       210       4·9       205       5·9       210       5·9       220       4·6       4·2         245       7·2       235       7·9       245       8·5       245       7·2       240       5·9       245       5·2       245       4·6       240       2·3       240       2·0       240       2·6       —       1·3       5·1         150       4·9       125       6·2       130       6·9       135       7·5       150       8·5       180       9·2       180       8·5       175       8·2       200       9·8       225       8·5       250       10·2       265       9·2       4·9         240       8·5       240       8·9       245       7·9       240       6·6       235       5·6       220       4·9       230       4·3       235       2·3       230       3·0       —       1·0       230       2·3       230       1·6       6·5         210       5·2       205       5·6       215<						I			200	7.5	195	6.9	200	4.3	195	4.9	195	5.2	195	3.9	195	4.6	195	2.6	5.5	26
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1				1	5.6	1						1													27
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$										5.9				4.6	240		240	2.0	240	2.3	240					28
240     8·5     240     8·9     245     7·9     240     0·6     235     5·6     220     4·9     230     4·3     235     2·3     230     3·0     —     1·0     230     2·3     230     1·6     6·5       210     5·2     205     5·6     215     4·9     220     3·3     225     2·6     205     4·3     195     3·0     —     1·3     —     1·0     195     1·6     2·8       —     4·8     —     4·9     —     5·0     —     4·6     —     4·2     —     3·5     —     3·0     —     2·8     —     2·8     —     2·5     3·5	1 -				-						•			8.5		8.2		9.8	225	8.5	250	10.2				29
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	240	8.5	240	8.9	245	7.9	240	0.0	235	5.6	220	4.9	230		235	2.3	230	3.0		1.0	230	2.3	230	1.6	6.5	30
12 14 15 16 17 -0 1	210	5.2	205	5.6	215	4.9	220	3.3	225	2.6	205	4.3	195	3.0		1.3		1.3		1.3	_	1.0	195	1.6	2.8	31
13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. Mean	_	4.8	_	4.9	_	5.0		4.6	_	4.2	_	4.3		3.2	_	3.0	_	3.0	_	2.8	_	2.8	_	2.5	3.2	
	. 1	3.	I	4.	I	5.	1	6.	,	7.		· 18.		<u>'</u>	<u> </u>	20	<u> </u>	) )T	<del> </del>	22	<u> </u>	22	,	24	Mean	Dav
	l						<u> </u>			·	<u> </u>			- J·			<b> </b>					-J.		7.		

Directions expressed in degrees from North ( $E=90^{\circ}, S=180^{\circ}, W=270^{\circ}, N=360^{\circ}$ ): Speed in metres per second.

# 460. Richmond (Kew Observatory):

 $(H_{\alpha} \text{ height of cups of anemograph above M.S.L.}) = \text{Height of ground above}$ 

Day.	1		2	2.	3	3.	4	<b>ļ</b> .		5.	6	j.	7	7.	8	3.	g	).	1	ю.	1	ı.	No	on.
I	-	m/s.	195	m/s. 2·0	195	m/s.	-	m/s.	° 265	m/s. 1·3 2·3	°  265	m/s. 1·3 2·3	° 265	m/s. 1·3 2·3	195 265	m/s. 1·6 3·0	200 265	m/s. 2·0 3·9	230 260	m/s. 3·0 4·3	240 290	m/s. 3·9 3·9	215 290	m/s. 3·0 3·0
3 4	265 — —	2·3 0·3 1·0	265 — — —	2·6 1·0 1·0	265  240 305	2·6 0·7 1·6 1·6	265 — —	2·3 0·3 1·3	240 305	2.0	240 300	0·7 1·6 1·6	225	3·6 1·3	205	1.0	195 290	3.6	285 195 240	2·0 5·9 3·9	290 200 240	2·0 5·2 4·9	200 245	1·3 4·6 4·6
5 6 7	 230	1.9	260	2.3	 230	1.3	 230	0.3	230	1.0	260 230	2·0 2·6	260 230	2·0 2·6 0·7	260 230	1·6 2·3 0·3	260 230	2·0 3·6 0·0	 235 	1.0 1.0	265 240	2·0 3·6 1·0	240 265	1·6 3·6 1·3
8 9 10	=	0.0	=	0.0		0.0	_ 	0.3		0.7	=	0·0 0·0	=	0.0	_	0.3	_	0.4	140 —	1.6	160 235	2·0 1·6	210 290	4.3
11 12 13 14 15	230 — 230 255	1·0 3·6 0·3 2·0 2·3	230 — 220 255	0·0 2·6 0·7 2·6 2·0	230 — 210 255	0·3 3·3 0·3 2·6 1·6	230 — 205 —	1·3 4·3 0·3 2·6 1·3	225 — 190 255	1.0 3.3 0.3 1.6	225 — 185 —	3.3 0.3 3.3	225 — 180 255	0·7 3·3 0·3 1·6	230  180 255	0·3 4·9 0·3 4·3 2·3	225 — 170 255	0·7 5·6 1·0 6·6 2·0	230 — 175 255	1·3 5·6 1·0 6·6 2·3	255 230 — 170 250	2·3 5·2 1·3 6·9 2·3	235 220 215 175 245	2·0 4·9 1·6 6·9 2·0
16 17 18 19	200 — — 220 220	2·3 1·0 1·0 2·6 4·6	200 — 175 220 220	2·0 1·3 2·3 3·3 5·2	 175 220 225	1·3 1·0 3·3 3·3 4·9	200 — 195 220 240	2·0 1·3 4·6 2·3 4·3	200 250 200 220 245	1.6 1.6 3.6 2.6 3.6	250 200 220 245	1·3 1·6 3·6 2·3 3·6	200 250 200 220 245	2·3 2·0 4·6 3·9 3·6	200 220 210 220 250	2·3 3·0 4·6 2·6 4·6	210 175 220 230 250	3·6 5·6 5·6 4·6 6·6	230 175 235 230 265	4·3 6·9 5·6 3·9 5·6	240 175 240 230 265	4·3 9·2 5·6 5·6 6·6	230 175 245 225 255	4·3 7·5 4·6 5·9 6·6
21 22 23 24 25	215 260 210 240 160	3·3 3·0 3·5 3·6 6·2	200 230 210 240 170	3·0 3·3 3·0 3·3 8·2	180 230 210 240 170	1.6 2.6 3.6 2.6 7.9	225 210 240 185	1:0 4:3 2:3 2:3 5:9	180 220 210 — 200	2·0 3·0 1·6 1·3 5·9	225 215 — — — 195	3·0 5·2 0·7 1·3 4·9	230 210 210 240 195	3·3 5·9 2·6 2·3 6·2	240 210 205 240 195	4·3 5·6 3·0 2·6 7·5	245 215 195 240 210	5·9 5·6 4·9 3·3 7·9	250 215 185 245 215	6·6 4·6 5·6 3·3 7·9	240 215 195 230 215	6·2 3·9 6·6 3·9 7·9	245 230 195 215 210	6·9 4·6 7·9 3·9 8·5
26 27 28 29 30	215 250 200 225	6·2 1·6 1·6 2·3 1·3	215 — — 225 —	4·3 1·3 1·6 1·3	220 — — 225 —	4·3 1·3 0·7 1·6 1·0	225 — — —	4·3 1·3 1·3 1·0	225 — 200 —	5·2 1·6 1·3 1·0	235 240 200 —	4·3 2·0 2·3 1·0 1·3	235 — 200 — 225	3·9 1·3 2·6 1·0 1·6	230 235 200 225	4.3 1.6 3.9 2.0 1.0	230 225 205 225 225	5·2 3·9 4·6 2·0 2·0	240 210 215 225 225	3·9 3·6 5·2 2·0 2·0	240 190 210 225 225	4·9 5·6 4·3 2·0 3·0	265 195 220 225 225	4·6 4·6 4·3 2·0 2·3
Mean	_	2.1		2.2		2.1		2.0		1.9	_	2.0		2.4	_	2.7		3.2	_	3.8	_	4.3		4.3

# 461. Richmond (Kew Observatory): $H_a = 5$ metres + 20 metres.

1	0 m/s 240 2 · 6 235 4 · 6 235 4 · 6 330 2 · 3 260 3 · 9 225 4 · 9 270 4 · 3 240 7 · 9 205 4 · 3 185 9 · 5 240 6 · 2 255 3 · 6 240 5 · 2 255 3 · 6 240 5 · 2 255 3 · 6 240 8 · 9	6 240 2:3 6 225 3:3 70 125 4:3 70 275 2:6 79 275 4:9 79 275 4:9 79 275 4:3 79 240 3:3 70 4:3 70 240 3:3 70 3:9 71 3 235 3:3 72 235 5:6 72 245 3:0 72 245 3:0 72 245 3:0 72 245 3:0 72 245 3:0 72 245 3:0 73 3:9 74 3:0 75 25 3:0 76 25 3:0 77 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:0 78 3:
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	235 4.6 190 3.0 345 10.5 330 2.3 260 3.9 225 4.9 270 4.3 240 7.9 205 4.3 235 3.3 185 9.5 240 6.2 255 3.0 240 5.2 255 3.6 240 5.2 255 3.6 240 8.9	.6    225    3.3 .0    125    4.3 .5    350    9.2 .3    275    2.6 .9    275    4.9 .9    230    5.2 .3    270    4.3 .9    240    8.2 .3    205    3.9 .3    235    3.3 .5    190    9.5 .6    245    3.0 .6    250    3.0 .9    250    3.9 .9    250    3.9 .9    250    3.9 .9    250    6.6
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	190 3.0 345 10.5 330 2.3 260 3.9 270 4.3 240 7.9 205 4.3 235 3.3 185 9.5 240 6.2 255 3.0 260 2.6 240 5.2 255 3.9 250 3.9 250 3.9 250 3.9 250 3.9 260 3.9 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 4.3 270 5.2 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270 2.6 270	.0
3	345 10.5 330 2.3 260 3.9 270 4.3 240 7.9 205 4.3 185 9.5 240 6.2 255 3.0 260 2.6 240 5.2 255 3.9 250 8.9	.5 350 9.2 .3 275 2.6 .9 275 4.9 .9 230 5.2 .3 270 4.3 .9 240 8.2 .3 205 3.9 .3 235 3.3 .5 190 9.5 .2 235 5.6 .0 245 3.0 .6 250 3.0 .2 245 4.6 .6 250 3.9 .9 150 3.9 .9 205 6.6
4       330       7.5       325       6.6       330       6.9       330       6.2       330       7.9       330       6.0       335       0.9       340       6.2       345       1.6         6       240       2.3       235       3.3       230       2.3       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       230       2.6       220       220       250       2.6       230       2.6       230       2.6       225       3.0       240       2.6       240       3.0       240       2.6       230       6.6 </th <th>330 2.3 260 3.9 225 4.9 270 4.3 240 7.9 205 4.3 185 9.5 240 6.2 255 3.0 260 2.6 240 5.2 255 3.9 255 3.9 260 8.9</th> <th>275 2.6 275 4.9 230 5.2 23 270 4.3 29 240 8.2 23 255 3.9 23 255 5.6 245 3.0 245 3.0 245 3.0 245 3.0 245 3.0 25 3.9</th>	330 2.3 260 3.9 225 4.9 270 4.3 240 7.9 205 4.3 185 9.5 240 6.2 255 3.0 260 2.6 240 5.2 255 3.9 255 3.9 260 8.9	275 2.6 275 4.9 230 5.2 23 270 4.3 29 240 8.2 23 255 3.9 23 255 5.6 245 3.0 245 3.0 245 3.0 245 3.0 245 3.0 25 3.9
5   350   2·6   350   1·6   —   0·7   —   1·3   —   1·3   —   1·0   —   1·0   —   1·3   —   1·3   343   1·0   6   240   2·3   235   3·3   230   2·3   230   2·6   230   2·6   230   2·6   230   2·3   250   2·0   250   2·0   250   3·3   7   250   1·6   250   1·6   250   2·0   250   2·3   250   2·3   250   2·3   250   2·0   250   2·0   250   3·0   225   4·9   8   205   2·3   215   2·3   220   2·0   220   1·6   —   1·0   —   1·3   220   2·6   225   3·0   245   3·9   260   4·9   9   210   6·2   220   6·2   220   4·9   220   5·2   225   5·6   215   4·9   225   5·6   230   6·6   230   6·6   230   6·6   240   2·0   10   225   3·3   225   2·6   225   3·6   215   4·3   205   3·9   205   4·3   205   3·3   205   3·0   205   3·0   205   4·9    11   270   3·6   260   3·6   250   3·0   250   2·3   250   3·0   250   3·6   240   3·0   240   2·3   240   2·6   240   3·0   12   —   1·3   —   0·7   —   1·0   —   1·3   225   1·6   —   1·3   225   1·6   165   2·6   120   3·9   180   8·9   13   235   3·0   230   3·6   220   4·3   215   5·2   205   6·9   205   5·2   215   5·2   220   6·6   225   5·9   230   6·2   14   255   2·0   255   1·6   255   2·0   255   2·0   —   1·3   255   1·6   255   2·6   255   3·0   15   —   1·3   270   1·6   —   1·3   —   1·3   250   2·0   2·0   2·3   240   3·0   240   2·3   240   2·3   16   240   1·6   240   1·6   240   2·0   240   1·6   240   2·0   240   2·3   240   3·0   240   2·3   240   4·3   17   250   1·6   250   2·0   —   1·3   —   1·0   —   1·0   —   1·3   250   2·0   2·0   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   250   2·3   2	260 3.9 225 4.9 270 4.3 240 7.9 205 4.3 235 3.3 185 9.5 240 2.5 260 2.6 240 5.2 255 3.6 255 3.6 250 8.9	9 275 4·9 9 230 5·2 3 270 4·3 9 240 3·9 13 205 3·9 13 235 3·3 15 29 9·5 16 250 3·0 16 250 3·0 17 250 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18 3·9 18
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$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	225   4.9 270   4.3 240   7.9 205   4.3 235   3.3 185   9.5 240   6.2 255   3.0 260   2.6 240   5.2 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9 255   3.9	.9         230         5.2           .3         270         4.3           .9         240         8.2           .3         205         3.9           .3         235         3.3           .5         190         9.5           .2         235         5.6           .6         250         3.0           .6         250         3.0           .9         150         3.9           .9         205         6.6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	270 4·3 240 7·9 205 4·3 235 3·3 185 9·5 240 6·2 255 3·0 260 2·6 240 5·2 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255 3·9 255	3 270 4.3 .9 240 8.2 .3 205 3.9 .3 235 3.3 .5 190 9.5 .2 235 5.6 .6 250 3.0 .2 245 3.0 .6 250 3.0 .2 245 3.0 .6 250 3.0 .7 2 245 4.6 .7 2 25 3.9 .8 3.9 .9 150 3.9 .9 205 6.6
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		Noon
G.M.T. 1. 2. 3. 4. 5. 6. 7. 8. 9. 10.	11.	Noon.

Averages for periods of sixty minutes, centered at the exact hours, Greenwich Mean Time.

M.S.L.  $+ h_a$  (height of anemograph above ground) = 5 metres + 20 metres.

September, 1923.

	3.	I	4.	I	5.	I	6.	I	7-	ı	8.	1	9.	20	0.	2	1.	2	2.	2	3.	2	4.	Mean	Day.
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# October, 1923.

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225	1.6	-	1.0	-	1·3		1.0	_	1.0		0.3	_	0.0	_	0.0	_	0.3	_	0.3		0.0		0.3	1.0	31
180 205 200	8·2 7·5 7·5 7·9 6·9	225 180 210 200 195	8·5 8·5 5·6 7·2 7·9	225 180 215 200 190	7·2 9·5 3·6 7·2 6·9	210 175 225 200 195	5·9 7·9 3·6 6·9 7·9	205 180 240 185 195	6·6 8·9 2·6 5·9 6·6	200 180 240 180 190	5·6 7·9 2·6 5·6 6·6	200 175 225 180 185	3·6 8·5 3·9 6·6 6·2	185 180 220 185 190	4·3 8·5 3·6 6·2 5·2	175 180 220 185 190	6·2 9·8 3·6 6·2 5·6	180 180 220 185 190	6·6 7·2 3·3 6·6 4·9	170 180 220 190 220	8·5 8·2 2·6 7·9 1·6	160 175 220 190	6·9 4·6 3·3 6·9	6·7 <b>8·2</b> 4·4 5·2 6·2	26 27 28 29 30
215 195 220	5·2 7·5 9·2 8·2 7·2	200 235 195 215 220	6·2 7·5 7·2 7·5 7·5	210 220 210 195 220	5·2 5·9 6·9 8·2 8·2	205 225 210 200 225	6·2 4·9 6·9 6·6 4·6	215 225 210 205 215	8·2 5·6 7·2 4·6 6·6	230 225 220 205 210	4·3 3·6 5·2 5·2 5·6	230 225 220 200 220	4·9 4·9 5·2 4·6 6·2	230 220 220 200 200 220	4·3 4·3 5·6 4·9 4·9	225 220 220 200 215	4.9 5.2 5.9 6.2 4.3	220 220 220 200 210	4·9 5·6 4·6 4·9 3·0	215 220 215 200 210	5·2 5·6 4·9 5·2 2·6	215 215 215 205 210	4·9 5·2 3·0 6·2 2·6	6·3 5·9 5·5 6·1	21 22 23 24 25
250 2 145 6 240 4	4·6 2·6 6·6 4·3 4·3	255 225 160 255 215	4.6 3.0 5.2 2.6 3.9	255 230 165 235 200	3·3 2·3 5·2 3·3 5·6	250 230 160 235 185	3·3 2·0 3·9 2·0 3·6	250 230 160 — 185	2·6 1·6 4·3 1·0 3·6	250 230 160 — 185	2·0 2·3 3·0 1·3 3·6	250 230 160 235 185	2·6 1·6 3·0 1·6 3·6	250 — 160 245 185	2·3 0·3 3·0 1·6 3·3	250 — 160 — 185	2·0 0·3 3·0 0·7 3·6	250 — 160 — 185	2·3 0·7 3·0 0·7 2·3	250 — 160 — 185	2·0 1·0 2·6 1·0 3·9	250 — 160 — 185	2·3 1·0 3·6 0·0 3·6	2·8 2·0 3·0 4·0 2·5	16 17 18 19 20
180   8 260   5 275   2	3·6 8·9 5·9 2·3 3·6	225 185 260 275 235	3.0 8.9 6.2 3.6 3.0	225 290 260 260 235	3·0 4·6 5·2 2·6 2·6	225 290 255 265 240	2·6 2·6 3·6 3·3 2·0	225 295 255 270	2·6 2·6 2·6 1·3	255 —	1·3 1·3 2·6 1·3 1·0	225 280 255 — 240	1.6 1.6 2.0 1.3 1.6	225 270 255 —	1·6 2·3 2·0 1·0 1·3	255 255 —	1·3 2·0 1·3 1·3	 255  	0·7 2·0 1·3 0·7 1·0	255 255 255 —	1·0 2·3 2·3 1·0 1·6	240 255 —	0·7 2·6 2·3 1·0 1·0	2·6 3·5 4·3 2·0 1·6	11 12 13 14 15
220   5 265   2 265   2	3·9 5·2 4·6 7·2 3·9	255 215 265 260 200	3·9 3·6 3·9 6·6 5·2	245 220 265 250 210	4·3 3·9 2·3 5·2 7·2	255 220 — 240 210	3·9 4·3 1·3 4·9 6·2	250 215 265 235 215	3·6 4·3 2·0 5·6 7·9	250 215 240 235 210	2·0 4·3 2·3 4·6 6·2	250 205 240 235 210	2·6 5·2 2·6 3·3 7·5	250 210 230 235 215	2·0 6·2 2·6 3·6 6·6	250 205 215 235 225	2·3 4·6 3·9 4·3 6·9	250 205 200 230 240	1·6 3·6 4·6 3·6 6·9	250 205 195 230 265	1.6 3.9 5.9 4.3 5.2	250 205 195 230 270	1.6 3.3 5.9 3.6 4.3	2·8 3·6 3·1 5·5 4·9	6 7 8 9 10
235   2 225   2 80   3 350   8	m/s. 2·6 4·3 7·5 8·9 3·0	235 225 45 350 265	m/s. 2·3 3·9 7·5 7·9 2·6	235 235 25 340 240	m/s. 2·6 3·6 6·9 8·2 3·0	250 235 10 345 240	m/s. 3·3 2·6 6·6 6·6 2·3	250 235 360 340 240	m/s. 2·6 2·6 3·9 5·9 2·0	250 235 350 345 240	m/s.   2·0 2·0 4·6 3·3 1·6	325 335 345 240	m/s.   1·0 2·6 4·6 3·6 1·6	340 335 345 240	m/s. 1·3 2·3 5·2 2·6 2·0	250 340 325 345 240	m/s. 2·0 1·6 6·6 2·0 2·0	325 350 240	m/s. 1 · 3 · 3 · 5 · 9 · 1 · 6 · 2 · 0	340 330 — 240	m/s. 1·0 1·6 6·2 1·3 1·6	255 340 325 350	m/s. 2·0 1·6 6·2 1·6 1·3	1.8 2.6 3.8 6.2 1.8	m/s. 1 2 3 4 5

Direction expressed in degrees from North ( $E=90^{\circ}$ ,  $S=180^{\circ}$ ,  $W=270^{\circ}$ ,  $N=360^{\circ}$ ): Speed in metres per second.

### 462. Richmond (Kew Observatory):

 $H_a$  (height of cups of anemograph above M.S.L.) = Height of ground above

Day.	1		2		3	3.	4		5	j.	6		7		8	3.	ç	).	10	о.	1	I.	No	on.
	1 5 1	m/s.	0	m/s.	•	m/s.	1 0	m/s.	0	m/s.	<del>'                                    </del>	m/s.	0	m/s.	0	m/s.	·	m/s.	ì	m/s.	ı°	m/s.	°	m/s.
ı		0.3	l	0.0	l	0.3	l	0.0		0.0		0.3	l	0.3		1.0		0.7		0.7		1.0	<b>-</b>	1.3
2		1.3	225	1.6	225	2.0	l —	1.3	225	1.6		1.3		0.7		0.3		1.0	l —	0.3		1.1	230	2.2
3	205	5.7	200	7.0	200	7.9	195	7.9	205	6.8	215	6.5	215	6.5	220	7.0	225	7.0	210	6.8	210	7.3	215	7.3
4	225	3.9	225	3.9	220	4.6	220	4.9	215	4.6	215	4.3	215	4.9	220	5.6	225	5.6	230	7.2	230	6.6	235	6.9
5	220	3.3	220	2.6	220	3.3	220	2.3	220	3.0	220	2.6	220	2.6	220	2.0	220	2.6	215	2.0	215	2.3	215	2.3
6	250	2.0	250	1.6	250	2.0	250	1.6		1.3		0.7	_	1.0		1.0		1.0	-	1.0	_	1.3	270	2.3
7	290	2.0	290	2.3	_	1.3	290	2.0	_	1.3	290	1.6	290	1.6		1.3	290	2.0	295	2.0	265	3.6	265	3.6
8		0.3		0.0		0.3	l —	0.0		0.7	l —	0.3	_	0.3	_	0.3		0.3	_	0.3		0.7	_	1.0
9	-	0.3		0.7	i	0.3	265	2.0	265	2.3	265	2.3	265	2.6	265	2.3		1.0	_	1.3	— T.	7:5	20	8.2
10	10	5.6	15	6.2	15	5.9	10	4.6	. 10	5.2	5	4.9	360	5.6	5	5.6	10	6.9	15	5.9	15	7.3	20	" -
11	5	4.3	5	3.6	5	3.6	5	3.9	5	2.6	5	1.6	5	2.0	5	2.0	5	1.6	360	2.0	360	3.6	360	3.0
12		1.3	360	1.6		1.0		1.0	_	0.3	_	1.0		1.0		0.3	-	1.0	_	1.0	360	2.0	290	3.3
13	190	4.3	190	5.6	190	4.3	190	5.2	190	7.9	190	7.2	190	10.2	185	8.9	190	10.8	190	9.5		10.8	195	6.0
14	170	11.5	175	10.8	180	11.5	210	5.9	210	5.6	220	4.6	255	5.9	270	4.9	260	4.9	260	5.6	265 165	7·9 10·8	265 175	11.8
15	230	2.0	230	1.6	230	2.0		1.0	-	1.3	_	1.3	190	3.0	170	3.0	165	5.2	160	10.2	105	10.0	1/3	11 0
16	230	8.5	240	6.9	235	7.2	240	6.2	235	4.9	235	3.3	235	3.0	220	3.0	210	3.9	205	3.9	215	5.2	215	6.9
17	185	6.2	185	6.2	180	7.2	185	8.9	190	7.5	155	5.9	235	4.3	210	4.9	210	5.6	220	7.5	225	7.5	225	7.2
1 <b>8</b>	220	3.6	220	2.6	220	2.3		1.0	220	2.0	220	2.0		1.0		1.3	_	1.3	225	3.0	225	3.0	240 285	3.6
19	235	2.6	235	2.3	235	3.3	240	4.3	240	3.6	240	3.6	245	3.9	245	3.9	250	3.3	250 260	4.3	270 275	4·9	275	3.3
20	290	2.0		1.3	_	1.3	290	1.6	290	1.6	255	2.0	250	2.0	250	2.6	250	1.6	200	2.0	2/3	3 0	2/3	3, 3
21	_	1.3	_	1.0	305	2.0	305	2.0	325	3.0	325	2.6	325	1.6	325	1.6	325	2.6	330	3.6	330	3.0	355	3.3
22		1.3	355	1.6	_	1.0	355	1.6	-	1.3	355	2.0	355	2.0		1.3	355	1.6	355	2.0	355	3.0	355	3.0
23	355	2.3	_	0.7	355	1.6	355	2.0	355	2.3	355	2.0	-	1.3	355	1.6	355	2.3	355	2.6	355	2.0	360	1.9
24	360	2.0	36o	2.3	360	1.6	360	1.6	_	1.3	_	1.3		1.3	360	2.0	360	2·0 I·0	360 360	2.3	360	1.3	300	1.0
25		0.7		1.3		0.7	_	1.3	-	1.0	_	1.3	_	1.3		1.0		1.0	300	1.0		1 3		
26		0.3		0.3		0.3		0.0	_	0.7		0.3		1.0	_	1.0	-	1.0	-	0.3	-	0.3	-	0.0
27		1.0		0.7	_	0.3		1.0		0.3		0.7		0.0	_	0.3		0.7		0.0		0.0		1.0
28	85	6.2	85	5.9	85	6.6	80	5.6	75	5.6	70	5.9	65	5.9	65	4.6	60	5.9	55	5·6 2·6	55	4.9	50 35	4·3
29		0.3		0.7	_	0.7	_	1.0		1.0		0.7		0.3	20	1.0	30 20	1.6	35	1.3	35 10	1.6	10	1.6
30	20	3.6	20	2.3		1.3		1.3	20	1.6	20	1.6	20	1.6	20	2.0							<u> </u>	
Mean		3.0	_	2.8		2.9		2.8	_	2.7	-	2.5	_	2.6	-	2.6	-	2.9		3.3	-	3.7	-	3.9

# 463. Richmond (Kew Observatory): $H_a = 5$ metres + 20 metres.

																						<del>. , ,</del>		
	0	m/s.	0	m/s.	0	m/s.	٥	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	0	m/s.	°	m/s.	-0-	m/s.	180	m/s. 4:6
I		1.0		0.7		0.0		0.7	_	1.0		1.3	_	1.3	180	2.0	180	2.6	180	3.0	180	4.9	170	3.0
2	170	7.9	170	8.5	175	7.9	175	9.2	175	9.5	180	8.2	180	8.2	175	7.5	175	5·9 1·3	170	5·2	170	3.3		1.3
3		0.7		1.0		1.3		1.3	-	1.3	180	1.0	180	4.6	180	3.6	165	5.2	165	7.9	170	8.2	175	7.2
4		1.3	_	0.7		0.3	235	2.0	195	3.0	100	3.6	100	1.3		0.7		1.3		1.3	250	1.6	250	3.0
5		1.0		0.7		0.3	_	0.7	_	1.0		1.3		1 3		,		- 3						ĺ
6	٠,	2.2	10	4.3	10	5.2	10	4.6	10	3.6	10	3.3	10	3.3	10	3.6	10	3.3	360	4.9	360	3.3	360	3.3
7	15	3.3		1.0	_	0.3		0.7		0.3		0.7		1.0	360	1.6	360	1.3	90	2.6	175	3.3	175	4.9
8	190	7.5	200	6.6	200	5.9	210	5.6	210	6.9	210	6.2	210	5.6	220	4.3	220	2.6	230	2.6	230	3.6	230	2.0
9	270	2.0	270	2.3	270	1.6		1.3	275	1.6	275	2.0	315	4.3	320	2.6	320	2.6		1.3	320	1.6	320	1.6
IÓ	l	0.3	<u> </u>	0.3		0.3		0.3	_	0.7		1.0		1.0	320	1.6		1.3	320	2.0	255	2.3	235	3.6
					ĺ							7.6		T. 2	225	1.6		1.3	230	2.3	230	3.3	230	2.0
11	235	2.0	l —	1.3		1.3	235	1.6	235	2.0	235	1.0	230	1.3	235 230	1.6	230	2.3	230	1.6	230	2.0	230	2.3
12		1.0	_	0.7	230	1.6	230	2.0	_	1.3	230	2.3	230	1.6		1.3	230	1.6	225	1.6	225	3.0	225	2.3
13	230	1.6	_	1.0	350	2.3	350	1.6	350	2.0	230	1.0	350	2.0	350	1.6	350	2.0		1.3	260	1.6	l — i	1.0
14 15	245	3.6	245	2.3	245	1.6	270	3.0	310	4.9	315	4.3	315	3.6	315	3.3	315	2.6	310	3.6	310	4.3	310	3.9
13	243	ا ،	~43	~ 3	-43		-, -	"	۱	' -	١٠٠		` `										262	6
16	315	2.0	315	2.0	315	2:3	315	2.0	315	2.0	315	2.6	315	2.6	285	3.6	240	3.6	240	5.2	255	4.9	260	4.6
17	265	2.3	265	2.3	265	2.0		1.3	265	3.0	265	2.3	265	3.0	265	1.6	265	2.6	240 285	3.9	240 285	4·6 7·5	245 300	3.9
18	225	4.3	225	3.6	225	3.6	225	3.6	225	3.9	225	3.6	225	2.6	225 280	2.0	230 290	3.0	310	5·9 3·6	315	5.2	315	4.3
19	285	3.0	285	3.6	285	3.9	285	3.3	275	3.3	275	3.3	275	3.6		3.3	345	5.6	345	9.2	350	7.2	345	6.9
20	320	5.5	325	5.9	330	7.2	335	6.2	335	6.2	340	5.6	340	5.6	345	39	343	ر ر	343	-	33-	<b>'</b> -	313	1
		5.0	27.5	4.0	27.5	2.0	315	2.6	315	3.0	315	2.3	315	3.0	315	2.6	315	3.0	315	3.0	315	4.3	315	3.3
21	315	5.2	315	1.0	315	3.0	315	1.6	323	1.3	315	2.6	315	2.3	245	3.6	235	2.6	240	3.6	240	3.9	265	5.2
1	300	3.0	300	2.6	300	2.3	300	2.6	300	1.6	300	3.3	300	7.9	310	7.5	310	7.9	300	7.2	305	9.8	310	8.2
23	285	3.9	275	3.3	275	3.3	255	3.0	255	2.6	255	3.3	255	3.6	260	4.6	260	3.0	240	3.3	240	2.6	240	2.3
25		0.3	7,3	0.7	1	0.7	] =	0.3	350	1.6	<u> </u>	1.0	350	1.6		1.3	-	1.0		1.0	_	1.0	350	1.6
			l				1								265		270	4.2	360	4.6	345	3.9	350	4.9
26	235	3.9	235	3.3	235	3.9	270	5.9	285	5.9	280	4.6	260	5.2	265	1.6	270 355	4.3	350	3.3	350	1.6	355	0.3
27	355	2.3	355	2.6	355	2.0		1.0	_	1.0		0.3	355	1.6	355 345	9.2	350	8.9	345	6.9	345	6.9	335	6.6
28	210	5.2	210	5.6	210	3.0	210	2.6	210	2.3	240	3.0	295	1.3	345	1.6	345	1.6	350	2.0		1.3	==	1.3
29	345	2.3	345	1.6	250	2.6	350	1.3		1.0		1.0	350	1.6	343	1.3	J73	1.3	=	1.3	_	1.3	355	2.3
30		1.0	350	2.0	350	2.0	330	1.0		1.0		1	333								l			1
31	60	3.0	60	3.3	60	2.6	60	2.3	60	2.6	60	2.6	l —	1.3	60	1.6	<u> </u>	1.0	l —	0.7	70	1.6	70	2.0
		ļ	<b> </b> -		<b> </b> -			<u>-</u> -			<b> </b> -			0.7		2.7		3.0		3.5		3.7		3.2
Mean	-	2.7		2.6		2.4	-	2.5	_	2.7	-	2.6	_	3.1	_	3.1		3 0		3 3	<u> </u>	" /	<u> </u>	
	<del>                                     </del>	<u></u>	<del> </del>	<u> </u>	<del>                                     </del>	·	i	·	<u> </u>	<u> </u>	i	<u>.                                    </u>	Ī		Ī,	8.	1	`	) ,	o.	١,	1.	No	on.
G.M.T.		τ.	2	2.	3	3.	4	ļ.		5.	6	5.	1 7	7•	۱ '	э.	\ `	9.	i '	٠.	1 -		<b></b>	
1	1		<u> </u>		1		<u> </u>		<u> </u>		<u> </u>		<u></u>		<u> </u>		<u>-</u>							

Averages for periods of sixty minutes, centered at the exact hours, Greenwich Mean Time.

M.S.L.  $+ h_a$  (height of anemograph above ground) = 5 metres + 20 metres.

November, 1923.

1	3.	1	4.	ı	5.	I	6.	1	7.	I	8.	]	9.	2	ю.	2	21.	2	2.	2	3.	2	24.	Mean	Day.
225 250 220 240 215	m/s. 2·0 2·2 8·2 7·9 2·0	225 250 210 230 215	m/s. 2·0 2·5 7·2 6·9 1·6	265 210 235 200	m/s. 1·3 2·5 6·9 6·9 2·3	270 215 230 165	m/s. 1·0 2·2 7·2 5·2 3·0	260 215 215 215 165	m/s.   1·3   1·8   6·9   4·3   3·0	225 260 230 210	m/s. 1.6 1.8 6.9 4.6 1.3	260 235 210 225	m/s. 0·7 2·2 5·6 5·2 2·0	250 240 215	m/s. 1·0 2·5 5·9 4·9 0·7	240 235 215	m/s. 1·0 2·2 4·9 3·6 0·7	240 245 220	m/s. 1·0 2·9 5·2 3·3 1·0	230 235 220 250	m/s. 1·0 3·6 3·3 4·6 1·6	210 230 220 250	m/s. 1·3 4·7 4·3 3·3 1·6	m/s. 0·9 1·8 6·5 5·2 2·2	1 2 3 4 5 5
290 260 210 — 20	3·3 3·6 3·3 1·0 8·2	290 270 180 — 20	2·3 3·0 4·6 0·7 7·2	290 280 175 — 25	3·0 3·3 4·6 0·3 7·2	290 270 175 265 15	2·0 2·0 2·6 2·0 6·6	290 — 175 5 15	1.6 1.0 2.3 3.6 6.6	 175 10 10	0·7 1·3 2·3 3·9 5·2	175 15 15	0·7 1·0 3·3 5·6 5·9	 175 65 15	1·0 1·3 2·3 8·5 5·2	 175 50 15	0·3 1·0 2·0 5·2 4·9	195 45 15	1·3 0·0 2·3 4·3 4·6	265 40 15	1·3 0·0 1·6 4·9 4·6	290 — — 30 15	1.6 0.0 0.7 4.6 4.9	1·5 1·8 1·5 2·5 6·0	6 7 8 9 10
360 200 195 255 190	3·6 5·6 12·1 7·5 11·1	360 190 195 260 210	2·3 4·3 10·2 5·9 7·5	360 190 190 265 205	2·3 3·6 10·8 5·2 8·2	190 190 275 205	1·3 2·6 9·8 3·3 8·2	 190 190 270 200	1.0 3.6 10.5 3.3 8.2	190 190 270 200	1·0 3·3 10·2 2·6 8·2	190 185 255 205	0·7 2·3 11·8 3·0 9·2	190 185 235 205	0·7 2·6 10·5 3·0 9·5	230	1.0 3.6 10.8 2.6 10.8	190 180 230 215	1.0 4.3 9.8 3.9 9.8	190 180 230 230	0·7 4·3 II·I 2·0 IO·2	190 180 — 235	0·0 2·6 II·I I·3 9·8	2·2 2·3 <b>9·2</b> 5·6 6·7	11 12 13 14 15
220 235 250 285 280	6·2 8·2 4·6 5·9 2·6	230 245 250 285 285	5·2 7·2 5·6 4·3 3·3	230 250 230 285 290	4·3 5·6 4·3 3·9 2·3	220 230 220 290	5·9 4·3 3·3 3·0 1·3	210 220 220 290	4·9 4·3 3·3 2·6 I·0	210 220 235 290	4·9 4·6 4·6 2·0 0·7	205 220 235 290	3·6 4·6 3·3 2·3 0·7	200 220 235 290	4.9 4.6 2.3 2.0 0.7	200 215 235 290	4.9 5.2 2.6 1.6 1.0	195 220 235 290 280	5·2 3·9 2·6 1·6 1·6	190 220 235 290 300	4.6 4.6 2.6 2.0 1.6	195 220 235 290 305	4·6 4·3 2·6 2·0 2·0	5·2 5·9 2·9 3·3 1·8	16 17 18 19 20
355 355 355 360 —	3·0 2·3 2·0 1·3	355 355 360 360	2·6 2·3 3·0 1·6 1·3	355 355 360 360	1·6 1·6 2·6 1·6 1·3	355 355 360 360 —	1.0 1.6 1.6	360 —	1·0 1·3 2·0 1·0 1·0	355 360 —	1·3 1·6 2·0 1·0	355 355 360 ———————————————————————————————————	2·0 2·0 2·0 I·0 I·0	355 360 —	0·7 2·0 2·6 1·0 0·7		1·3 1·6 0·7 0·7	355   	1·6 1·3 1·0 0·7	355 355 360 —	2·0 2·0 3·3 1·0 0·3	355 355 — —	2·0 1·6 1·0 0·3	2.0 1.8 2.0 1.5 1.0	21 22 23 24 25
50 35	0·3 1·3 4·6 3·9 1·0		0·0 1·0 3·9 3·6 0·7	90 50 25	0·0 3·6 4·3 4·3	90 30 20	0·3 3·3 3·6 0·7	360 90 30 20	1·6 4·3 2·0 3·6 0·7	90 30 20	1.0 4.6 1.6 2.6 1.3	90  20 	0·7 4·3 1·3 3·0 1·0	90 - 20 -	0·7 4·6 1·3 3·0 1·3	85  20 	1.0 5.6 0.7 3.6 1.3	85 - 20 180	1.0 5.6 1.0 3.3 1.6	85 - 20 -	0·7 4·6 0·7 3·9 1·3	85 - 20 -	1.3 3.6 1.3	0.6 2.1 3.9 2.3 1.5	26 27 28 29 30
	4.4		3.8	_	3.7	_	3.2		3.1		3.0	_	3.1		3.1		2.9		2.9		3.0		2.8	3.1	

#### December, 1923.

185	m/s. 5.6	190	m/s.	190	m/s.	190	m/s.	185	m/s.	185	m/s.	° 180	m/s. 6·6	18o	m/s.   6·2	° 180	m/s.   7.5	175	m/s. 8·2	175	m/s.     8·9	175	m/s.	m/s.   4 · I	1
180 235 195 335	3·6 2·0 4·9 3·0	235 235 220 20	3·0 1·6 4·6 2·6	235 235 240 20	3·0 2·0 3·9 3·0	235 — 245 20	1·6 0·7 2·0 2·3	235 — 245 20	1·6 0·7 1·6 4·3	245 15	1·0 1·0 2·3 2·6	245 15	1·0 0·7 1·6 3·0	   	0·7 1·0 1·0 2·6	245 15	3.3 1.9 1.3	235 — 15	3.6 1.3 1.0	245 15	0·7 1·3 1·6	   15	0·7 1·3 4·3	4.5 1.2 3.1 2.1	2 3 4 5
360 175 230 320 235	4·3 5·9 2·6 2·0 3·6	360 175 230 320 235	2·3 5·9 1·6 2·3 2·3	175  320 235	1·3 6·9 1·0 2·3 2·3		1.0 7.2 1.0 0.3 2.6	180 — — 235	1·0 7·9 0·7 0·7 2·3	 180   235	0·3 8·2 0·0 0·3 2·6		0·3 8·5 0·7 1·0 2·6	180 — — 235	0·3 8·2 1·0 1·0	- 180 - - 235	0·7 9·2 1·3 1·0 3·0	180 — — 235	1·0 8·5 1·3 1·6	185 230 — 235	0·0 8·5 2·3 0·3 2·3	185 255 — 235	0·3 6·9 2·0 0·7 2·3	2·5 4·5 3·2 1·6 1·8	6 7 8 9 10
230 230 225 —	2·6 2·6 2·6 0·7 4·9	230 230 230 260 315	1.6 2.0 3.0 2.6 4.9	230 — 240 260 315	1.6 1.3 2.6 3.3 3.6	230 260 260 315	1·3 2·3 3·6 3·0 3·0	230 305 260 315	1·0 2·3 3·6 3·6 2·0	230 335 245	1.0 2.0 5.2 4.3 1.0	230 — 350 240 315	2·0 1·0 3·3 4·9 1·6	230  350 240 315	2·6 1·3 2·6 4·6 1·6	230 — 350 225 315	1.6 1.3 3.6 4.6 2.3	350 225 315	1.9 1.3 1.3	 350 235 315	0·7 1·3 3·3 4·3 1·6	350 235 315	0·7 1·6 3·3 1·6	1.7 1.6 2.4 2.6 3.0	11 12 13 14 15
250 245 290 310 335	3·9 4·3 5·9 4·9 5·9	250 245 275 315 335	3·3 3·3 4·6 5·2 5·6	265 245 275 315 335	4·3 3·9 3·9 3·9 5·6	275 245 280 325 335	3·6 3·3 3·3 4·3 5·2	265 245 290 345 330	5·6 3·6 3·6 2·6 4·6	260 250 290 355 330	5·6 4·3 3·3 3·6 4·3	260 255 290 345 315	3·3 3·6 3·6 4·3 4·6	265 240 300 340 310	3·9 3·3 3·9 4·6 4·6	260 235 290 340 315	4·6 3·9 3·6 4·9 4·9	265 230 285 330 315	4·6 3·6 3·3 4·3 4·9	265 230 285 325 315	3·6 4·3 5·2 4·9	265 230 285 3 ² 5 3 ¹ 5	2·3 4·3 3·6 5·9 4·3	3·5 3·2 4·0 4·0 5·7	16 17 18 19 20
315 285 310 240 350	1.6 7.5 8.5 3.3 2.0	310 285 305 240 350	1.6 6.6 6.9 2.6 2.6	285 305 245 350	1·3 5·9 7·2 3·6 2·3	290 295 245 350	1·0 5·2 7·2 3·0 3·3	280 295 325 350	1·0 6·2 6·9 5·9	275 295 330 350	0·7 4·9 6·2 6·6 4·3		0·7 5·6 5·6 6·6 5·2	265 285 350 175	0·3 5·2 5·2 4·9 6·9	265 290 350 185	0·7 5·2 5·6 3·9 8·2	270 290 350 200	0·7 4·3 3·6 3·3 5·6	305 290 350 220	1.0 4.9 3.3 2.0 4.9	305 290 — 235	0·7 4·3 3·6 1·3 3·9	2·2 3·9 5·6 3·6 2·6	21 22 23 24 25
350 350 340 350 60	4·3 0·7 5·9 2·0 4·9	355 350 335 — 60	3·3 2·0 6·2 1·3 4·3	355 350 340 — 60	3·3 2·0 5·6 1·0 5·2	355 350 345 — 60	2·3 1·6 3·3 1·0 5·9	350 345 60	1·3 2·3 3·9 1·0 4·6	355 350 345 350 60	2·3 2·6 3·9 2·0 4·3	355 330 345 350 60	2·0 3·9 3·0 2·3 3·6	355 235 345 — 60	2·0 3·9 2·0 1·3 2·3	355 220 345 — 60	2·3 3·6 3·3 1·3 2·6		1·3 3·9 1·3 1·3	355 210 345 — 60	1.6 5.2 2.3 0.7 2.0	355 210 345 — 60	2·0 4·3 2·3 0·7 1·6	3·5 2·3 4·6 1·4 2·6	26 27 28 29 30
70	2.0	70	2.0	70	2.6	195	3.0	200	2.3	200	2.3	200	2.3	200	2.0	200	2.0	200	2.0	200	2.3	200	1.6	2 · I	31
_	3.8	_	3.2		3.4	_	3.0		3.1		3.3	-	3.2	_	3.0	-	3.3		2.9	-	3.0		2.7	3.1	
1	3.	I.4	ļ. <u> </u>	15	5.	16	5.	17	,.	18	3.	19	9.	2	о.	2	ī.	2	2.	2	3.	2	4.	Mean	Day.

464. Richmond (Kew Observatory):  $H_a = 5$  metres + 20 metres.

1923.

	04. N		110 (170		ooi vat	JI <b>y</b> ) .	110 —	5 met	105	20 1116													132	
	Ja	ın.	Fe	eb.	М	ar.	Ap	ril.	М	ay.	Ju	ne.	Ju	ıly.	A	ug.	Se	pt.	O	ct.	N	o <b>v</b> .	De	ec.
Day.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.	Max. in a Gust.	Time of Gust.
1 2 3 4 5	m/s.	h. m. * * *	m/s. * * * *	h m	m/s. 14 16 7 8 12	h. m. 10 15 <b>10 25</b> 15 30 7 35 15 25	m/s. 7 10 8 12 9	h. m. 19 5 14 25 16 50 13 5 13 35	m/s. 13 5 10 13 12	h m 1 50 14 15 15 10 13 15 19 20	m/s. 8 7 11 13 6	h. m. 7 15 11 10 18 45 6 35 23 45	m/s. 7 7 10 10	h. m. 9 35 17 15 15 10 15 45 19 25		h. m. 13 35 15 45 13 35 17 30 13 40	m/s. 10 8 5 9	h. m. 16 40 9 20 11 10 10 5 14 35	m/s. 7 9 13 20 6	h. m. 15 35 10 10 22 20 10 10 14 25	m/s. 4 7 15 16 6	h. m. 24 0 24 0 19 55 10 35 0 25	m/s. 14 15 3 13	h. m. 23 30 4 30 13 25 10 55 22 0
6 7 8 9 10		* * * *	* * * *	* * *	14 11 13 12 8	13 45 9 45 18 20 2 0 17 55	12 7 20 19 15	8 55 20 50 12 55 9 45 14 25	6 8 7 10 12	11 5 22 0 16 5 21 10 23 55	11 7 <b>16</b> 14 15	11 40 15 40 <b>14 35</b> 1 15 17 0	12 9 9 10 11	17 55 12 0 9 30 22 50 18 40	7 11 7 8 5	14 40 11 50 13 0 14 50 14 30	4 7 4 9 7	6 20 10 55 14 45 13 55 17 5	10 11 11 15 15	15 35 11 0 23 50 11 35 21 25	4 7 8 18 14	13 5 11 50 14 40 19 45 12 5 12 35	9 15 14 5 6	3 0 21 0 1 25 7 10 12 15
11 12 13 14 15	•	* .	* * *	* * *	6 11 8 13 15	13 20 12 30 0 10 14 50 15 55	9 10 14 18 11	I 15 I4 40 II 15 IO 40 I2 25	24 15 13 12 21	14 40 11 35 15 30 11 20 10 15	11 13 14 9 14	10 55 17 5 15 0 7 35 23 30	4 7 10 5 12	11 55 14 45 14 25 15 0 14 45	5 9 10 5 10	16 35 13 35 11 50 12 55 11 50	9 9 7 12 10	16 5 10 40 21 35 14 40 13 40	9 16 13 11 6	1 5 11 45 7 45 14 0 13 55	6 8 <b>22</b> 19 21	0 10 13 15 <b>15 10</b> 3 40 21 15	4 4 10 8 8	11 30 11 35 18 0 19 20 14 0
16 17 18 19 20		*	*	*	11 14 16 13 8	17 0 15 20 <b>13 5</b> 9 10 23 40	11 7 10 10	13 0 17 35 19 15 10 55 20 15	23 17 8 8	13 35 12 35 9 55 15 15 14 20	13 9 6 .9 12	8 35 12 50 15 10 13 55 11 55	12 12 8 10 10	10 45 18 25 0 35 12 50 10 0	9 16 19 7 8	13 45 14 15 12 15 14 0 14 25	10 14 13 13	13 25 11 50 14 25 11 35 14 35	10 9 11 15 9	14 0 10 0 13 45 8 5 11 50	21 18 12 9 7	0 10 5 40 14 5 13 30 11 35	11 8 13 10 14	17 10 11 20 11 10 23 45 9 55
21 22 23 24 25		*	* * * 10 6	* * * 11 35 14 40	7 3 6 7 7	14 40 17 25 13 0 17 45 10 25	16 18 8 9 20	8 25 13 10 23 55 0 35 11 5	10 11 12 7 11	10 20 13 45 11 35 20 35 15 5	8 10 8 9 8	16 35 12 30 16 35 9 50 10 35	8 9 12 8	14 0 15 15 11 30 18 45 10 50	18 15 14 10	11 35 16 0 12 40 0 50 17 5	14 10 <b>18</b> 10 17	11 45 13 40 13 10 <b>14 15</b> 15 40 22 5	} 17 21 15 16 18	6 10 13 45 12 45 14 20 13 10	7 5 6 3 4	11 20 12 30 14 10 2 50 6 55	13 17 11 13	1 5 13 20 11 35 18 45 20 5
26 27 28 29 30	*	•	24 22 16 —	2I 35 0 45 5 20 —	5 11 13 12 7	11 50 11 30 13 20 15 15 23 5	23 6 11 9 14	12 25 10 0 14 45 6 5 14 35	8 8 10 12 12	17 5 17 30 16 15 12 10 16 0	6 6 6 5 7	13 50 12 45 10 50 19 15 12 50	15 8 15 11 15	16 40 16 50 17 25 16 25 19 10	13 14 17 21 21	17 10 12 5 15 10 23 0 2 10	11 10 8 4 5	9 20 15 25 9 15 9 30 13 55	22 18 14 16 15	6 45 5 40 10 40 13 55 13 55	2 10 11 7 6	17 10 21 35 6 30 15 30 0 45	12 9 16 4 9	4 20 22 30 9 10 0 40 16 20
31	•	•	-	-	8	13 55	_		10	16 5	_	-	12	18 55	10	14 15	_	_	3	10 5	_	-	5	1 40

#### DISTRIBUTION OF WIND SPEED: EXTREME VELOCITIES.

465. R	lichn	nond (Kew Ob	servatory	): Ha =	= 5 metre	s + 20 n	netres.								19	23.
				DISTR	IBUTION	OF WIN	D.					EXTREME V	ELOCITIES.			
Month.	•	More than 1	7·1 m/s.	10·8 to	17·1 m/s.	5.5 to 10.7 m/s.	1.6 to 5.4 m/s.	Less than 1.6 m/s.	No Record	Н	ighest Hou	rly Wind	High	est Gust.		
		Dates of Occurrence.	Duration.	No. of Days.	Duration.	Duration.	Duration.	Duration.	Duration	Veer from N.	Speed.	Mid. Time.	Speed.	Da	ate.	
Jan.*			hr. o	o	hr. o	hr. 100	hr. 534	hr. 110	hr. o	° 220	m/s. 9·2	day. hou		d.	h.	m.
Feb.*	•••	_	o	2	8	194	368	102	0	195	12.1	27 1	•	•		
Mar		_	0	I	1	136	438	169	0	65	11.1	18 1		2	10	25
April	•••	_	0	3	, 12	173	440	95	0	55 60	11.8		7 23	26	12	25
May		_	0	o	0	113	517	114	o	205 245 }	9.2		2 24	11	14	40
June	•••	_	0	0	0	79	478	163	o	245 } 180 }	9∙8	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		8	14	35
July	•••	_	0	0	0	75	562	107	0	205	7.9		7 15	26	16	40
Aug	•••	_	0	0	0	135	472	137	0	250	10.2	29 2	3 21	{29 30	23 2	
Sept	•••	_	0	0	0	90	446	184	0	175 345 \	9.2	1 - '	1 18	23	14	
Oct	•••		0	o	0	216	417	111	0	170	10.2		3 22	26	6	45
Nov	•••	-	0	3	16	1 10	365	229	0	195	12.1	13 1	3 22	13	15	10
Dec	•••		0	0	0	99	458	187	0	305	9.8	23 I	1 17	23	11	35
Year	•••	_	0	9	37	1,520	5,495	1,708	0	195	12.1	Feb. 27	0 24	Маугг	T.A.	40
				<del></del>	3/	1,,,20	3,495	1,,50		195∫		Nov. 13	3	1.23911		

^{*}The Dines Tube Anemograph was out of action from Jan. 1st to Feb. 24th.
"Distribution of Wind" and "Highest Hourly Wind" refer (for this year) to the Robinson Cup Anemograph.
"Highest Gust" refers to the Dines Tube Anemograph. See p. 293.

Richmond (Kew Observatory). 466.

Readings, in degrees absolute, at 9h., Greenwich Mean Time.

1923. Tan. Feb. March April May June July Sept. Oct. Nov. Dec. Day. 30 cm 122 cm 30 cm 122 cm 30 cm 122 cm 30 cm 122 cm 30 cm 122 cm 30 cm | 122 cm | 30 cm | 122 cm | 30 cm | 122 cm | 30 cm | 122 cm | 30 cm | 122 cm | 30 cm | 122 cm | 30 cm | 122 cm a a a a  $\boldsymbol{a}$ a a. 79·8 80·0 85·4 85·6 88.3 83.9 83.8 88.8 86.3 88∙0 86·1 82.7 82.0 81.0 82.1 89.1 87.7 84.4 80·0 84.2 79.9 79.2 79.5 75.2 80·1 89·7 89·8 88.3 84·4 84·3 75·8 75·9 75·2 82.2 82.2 86.6 80.7 81.1 84.4 83.8 88.7 87.4 87.4 86.2 79.9 79.2 80·1 77·1 78·2 79.7 86.3 79·8 79·9 80·0 82.3 88.3 86.4 86.3 81.1 79.4 79.0 82.4 81.2 83.9 83.8 88.6 85.6 87.4 82.2 3 80.1 85·7 85·8 86.3 79.8 80.5 79.7 78.6 82.0 81.3 86.2 82.6 85.5 83.8 88·4 88·8 89.5 88.3 86.2 87.3 84.6 82.3 80.0 79.8 81.4 87·o 82.7 84.6 88.2 87.2 83.3 86.3 85.6 79.8 76.4 79.0 79.9 78.4 80 • т 82.5 83.8 90.0 81.3 86·o 90·**3** 90·8 88.2 86.2 6 78.3 78.5 82.3 87·3 88·1 85·o 83.8 86·1 79.8 80·1 81.1 84.1 75·3 75·3 76·6 79.7 81.7 87·1 87·1 79·8 78·5 76.2 79.7 78.0 79.9 78.7 80·1 81.5 83.2 84.9 83.9 91.0 86·o 88.2 86.9 84.0 86.0 84.1 79.5 83·5 83·6 88.2 86.7 79·3 78·9 87.6 78.0 8r · 5 85.4 84.7 85.9 83.9 79.7 79.9 79.1 80.0 82.0 83.9 91.2 86.3 01.2 79.5 80.0 81.6 88.3 8<u>5</u>·8 86.9 85.7 91.6 86.3 87.0 85.4 76.6 79·0 78·5 80.0 81.1 84.0 86.3 79.7 91.0 79.4 83.8 88.5 77.2 79.7 78·8 80.0 81.6 86∙0 86.1 84.2 91.6 86.6 87.4 87.1 85.4 85.7 78.4 83.3 75.6 79.9 92.5 79.7 79:5 78·o 85.7 78.2 76.5 79·0 78·6 80 - т 86.2 88.4 88·o 85.6 80.8 81.6 84.9 83.9 84.2 86.0 87.0 83·1 II 79.7 80 · т 92.2 02.4 76.2 87·0 87·1 81.5 84.0 83.9 85.9 84.2 91.6 85·7 85·8 83.0 79.6 88.5 85.2 80.0 80.0 82.2 87.0 87.9 76.3 77·7 78·4 77·5 78·1 12 94.0 77.3 79.4 87·7 88·4 83·5 83·6 75·8 79·9 80·0 81·5 81·6 79.6 78.6 82.7 84·0 86.5 84.3 94·5 94·0 87.2 91.5 88.6 84.4 79.9 77·7 77·8 13 79.4 79·8 78·6 84·4 84·6 . 78·5 78.4 83.4 76.0 82.5 83.8 87·0 87.6 92.2 88.6 87.1 85.8 82.6 14 79.4 79.9 79.5 88.5 15 76.3 79.4 78.4 79.9 78.0 79.8 81.7 81.5 84.0 83.8 86.7 93.8 87.9 91.9 88.8 87.1 82.2 85.6 82.4 79.6 77.4 86·4 85·8  $82 \cdot 3 \\ 82 \cdot 3$ 85.4 78·5 78·5 16 79.2 77·9 78·4 79.8 83·I 88·o 88.8 86.8 82.0 93.2 79.6 79.8 81·7 81·8 83·7 83·6 88.1 88.7 86.1 82·5 82·8 76.2 78.9 80.0 81.6 8**3**·1 84.6 92.5 90∙0 87·1 85.2 17 18 79.2 77.0 79.6 88.7 87·1 87·0 83.4 85·5 86·3  $88 \!\cdot\! 3$ 85.2 75.4 79.1 78.8 79.9 78.2 79.8 81.6 84.7 91.4 89.6 86·o 77.9 82.0 77.8 79.7 79.8 88.5 78·o 75·5 76·7 78.2 83·3 83·8 88.7 85·5 85·6 83.6 84.7 80.1 84.9 84.9 82.1 10 79.2 79.9 81.5 82.0 91.3 77:4 76:8 77·5 76·8 77.6 79.8 84.7 88.6 86.9 78·o 81.5 81.9 83.4 86.2 88.4 89.4 84.2 85·o 82·0 20 79.2 91.1 79.9 79.7 79 · 1 88.5 81·4 81·6 88.3 21 79.8 78.4 79.8 81.8 84.2 83.5 86.0 84.8 92.2 89.8 85.5 86.8 84.3 85·o 76.6 81.7 83.6 88.5 85·1 85·0 75·9 76·5 79.8 79.8 86.9 88.2 86.7 83.9 76.6 75·4 76·6 81.8 84·5 85·2 84.8 92.6 85.1 81.4 22 79.2 77.0 78.9 80.0 79.7 88.5 79.8 87.4 88.7 84.9 76·4 76·0 81.3 79.1 79.0 81.2 81.8 85·0 92.0 86.4 83.1 77·4 77·5 78·1 79.7 23 79.4 81·5 81·8 88.4 86.4 79.8 89.0 88.6 88.3 84.8 81.2 75.5 79.0 79.7 84.4 91.7 83.0 76.1 24 79.0 79.3 79.8 80·0 84.6 25 81.8 83.5 89∙0 85.0 88.6 88.2 88.2 85.3 86.4 83.0 84.8 76.0 81.2 92.0 75.7 79.3 78.9 88.5 26 76.4 78.7 81.9 81.8 84.3 83.8 87.8 85.2 88.6 88·1 86.2 82.7 84.8 81.0 79.6 80.7 80.0 90.9 75·7 75·4 75.6 79.2 88·6 88·6 85·5 85·8 83.7 27 28 76.9 78.9 79.0 79·7 79·8 81.3 80.2 81.9 81.9 84.9 87.0 85.2 90.1 88.5 88∙1 86·1 83.1 84.7 80·8 79.2 75·9 77·0 82.4 83·7 83·7 83·8 87·5 87·6 85.3 90.5 83·2 82·8 84·5 84·6 80.7 79.0 82.5 80.2 81.9 84.7 88·o 88·o 86.2 77.0 79.4 79.1 77·6 78·2 88.5 76·5 75·8 82.5 88.0 78.9 80.3 83.0 82.0 85.3 90.0 86.9 86·1 75.2 80.4 88.6 86.9 85.3 88.5 88.2 86·1 83·1 84.4 75.6 80.7 83.5 82.0 84.1 87.9 80.2 30 79.0 82.3 90.4 79.1 88.5 82.2 84.8 83.7 86.5 87.8 83.7 31 79.2 79.0 90.0 76.4 79·1 83.4 84.5 88.4 78.7 79.8 80.0 81.9 81.6 84.8 86.3 87.4 8a.8 86.4 86.9 84.1 85.4 78.2 82.5 76.3 Mean 76.7 79.5 79.4 79:3 01.2

The initial 2 or 3 of the readings is omitted; i.e., 275.0 degrees absolute is written 75.0.

#### MINIMUM TEMPERATURE "ON THE GRASS" **DURING** THE INTERVAL 18H. TO 9H. G.M.T.

Readings, in degrees absolute.

#### HEIGHT IN CM. ABOVE M.S.L. OF SURFACE OF UNDERGROUND WATER.

Daily Means and Extremes for Months.

1923.

Nov.

cm.

213 213

213

211

209

206

206

206

205

208

213

215

215 216

218

210

220 221

221

22I

221

221

222

222

220

218

215

Dec.

cm.

217 216

214

213

212

213 215

216

22I

236

239

239

237

235 232

228

226

225 223

223

225 227

230

239 244

226

Oct.

cm.

175 176

177

177

175

177

184

189

195

199

201

201

199

199

200

201

202

205

206

208

210

191

46	7. R	tichm			Obse	_					19	923.		468	3. R		-		Obse				.12 0 7607	
Day.	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.		Day.	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	0
	a. 69·5	a. 82·2	a. 75.7	a. 71·4	a. 83·4	a. 80·5	a. 82·1	a. 81 ·o	a. 74·1	a. 79.9	a. 72.6	a. 64·3		1	cm.	cm.	cm. 282	cm. 286	cm. 263	cm.	cm.	cm. 204	cm. 186	-
2	72.1	83.0	76.0	74·I	74.8	81.0	76.9	81.7	76.9	78.8	74.8	76.9		2	198	217	284	285	262	237	216	203	186	1
3	77.2	81.4			79.0	70.9	78.8	83.7	74.0	74.7	74.5	67.1		3	202	217	287	284	261	241	217	202	185	:
4	70.7	75.6			77·I	80.6	85.0	76·o	73.5	78.6	75.3	66.1	1	4	207	216	295	284	262	244	217	201	184	1
5	68.8	67.9	69.1	75.8	79.2	73.2	78.3	74.2	76.0	69∙1	73.6	68.4		5	211	217	308	285	264	244	214	200	183	1
6	70.0	71.8	71.2	78.9	81.0	81.9	85.5	81.0	76.0	78.2	70.1	73.7		6	215	219	316	288	266	242	213	199	183	1 :
7	69.1	70.1	74.5	78.2	80.8	78.8	85.6	80.5	79.5	76.4	67.3	68.8		7	220	221	318	291	265	239	211	198	181	1
8	81.7	81.6	77.0		81.2		88.6	83.4	72.9	78.1	66.2	78.1		8	224	221	317	290	263	236	210	197	180	1
9	69.9	70.6	74·I	70.0	78.7	84.6	78.9	80.0	73.5	83.7	71.1	69.7	i	9	229	221	317	287	262	233	208	195	179	1
10	73.6	74.3	75.0	66.9	75.0	85.7	89.6	84.7	79.5	81.5	74.5	65.2		IO	233	223	316	284	259	230	208	194	179	. 1
II	69.2	76.2	70.0	80.8	77.0	79.4	86.0	81.5	82.2	82.6	68.5	78.8		rı	236	228	313	281	257	226	208	193	179	]
12	72.2	69.2	66.6	80.9	70.8	72.8	88.2	78.6	79.8	82.0	68.2	78.0		12	239	231	309	278	253	224	207	192	179	)
13	67.2	76.2	76.4	77.6	74.2	83.6	87.9	80.1	77.2	75.2	76.8	74.1		13	240	235	307	277	249	222	207	193	179	]
14	74.3	76.2	73.2	73.6	75.3	83.2	87.0	85.4	84.0	70.4	77.8	70.2	ł	14	242	238	309	279	247	220	207	193	180	1
15	70.7	74.9	75.8	71.1	77.7	80.1	86.2	86.8	80.8	68· <b>4</b>	67.2	73·1	ĺ	15	243	243	313	281	244	219	208	193	180	]
16	73.1	71.4	76.8	73.4	72.6	80.4	88.1	75.4	73.2	70.1	72.5	68.8		16	244	247	315	283	242	219	211	193	180	ı
17	66.4	72.8	76.0	77.4	73.0	79.6	80.8	83.9	71.2	77.6	74.6	74.2		17	244	252	316	285	240	221	213	193	180	1
18	69.2	74.5	74.4	74.0	71.8	72.7	83.8	85.8	74.2	73.3	69.0	76·1		18	242	256	317	287	238	225	215	193	180	2
19	70·1	69.5	73.3	76.8	72.7	82.7	78.8	81.2	76.8	84.7	70.8	73·I	i	19	241	260	317	289	237	227	216	191	179	2
20	75.9	74.3	69.9	77.3	80.8	81.8	87.3	84.5	78.8	80.7	66.8	69∙0	1	20	240	263	315	290	238	226	215	191	178	Ι
21	67.2	72.5	77.1	75·o	82.6	77.7	85.6	87.5	81.5	81.8	73.0	67.6		21	238	267	312	291	239	224	213	190	177	3
22	71.1	67.8	72.4	79.0	75.3	83.3	85.8	82.0	74.1	78·o	70.6	72.9		22	238	271	310	290	239	222	211	189	177	I
23	68.9		73.5	67.2	82.8	, , , ,	83.3	76.2	74.0	78.0	66.4	72.5		23	237	273	309	285	237	220	210	188	176	2
24	66.8	69.2	73·I	71.2	74·I	85.8	81.0	83.3	74.9	75.0	70.9	72.0		24	235	274	307	284	236	218	208	187	175	2
25	70.4	76.2	71.2	70.6	73.7	83.1	86.2	77:4	81.9	78.8	70.9	63.9	İ	25	234	276	304	281	235	217	206	186	175	2
26	70.0	71.2	77.4	79.6	70.1	79.4	81.9	86·o	82.4	76·I	68.9	73.9		26	232	279	301	277	233	215	205	186	174	2
27	76.9	77.2	74.1	70.8	77.3	75.8	76.4	81.3	75.9	79.6	68.7	73.0	l	27	230	281	299	272	231	214	204	188	174	2
28	73.2	78⋅1	8i·8	71.4	79.6	78·1	87·o	81.8	77.2	81.1	70.4	77.1		28	228	281	296	269	230	213	203	189	174	2
29	76.9	-	79.5	76.9	79.7	77·I	81.8	79.0	85.8	74·I	72.8	66∙1		29	225	-	292	267	229	212	203	189	173	2
30	78.4	-	74.6	80.8	78.3	77.2	85.9	80.5	89.4	82.9	69.1	73·I		30	223	_	289	265	229	211	204	189	174	2
31	79:4	_	76.8	_	80.3	_	84.3	72.2	_	79.8		73.8		31	221	-	287	_	231	_	205	187		2
Mean	71.9	74.3	74.0	74.7	77.1	79.6	84.0	81.2	77.7	77.7	71.1	71.6		Mean	229	245	306	283	246	226	210	193	179	1
	1	1	1	1 ' '	1	1		l	1	1	1	1	l	1 1		1	1 -	1 -	1 -	1	ı	ı	, ,	

The initial 2 or 3 of the readings is omitted; i.e., 2750 degrees

absolute is written 75 o.

Note.—The minimum refers to the interval from 18h. the previous day to 9 h. on the day to which it is entered.

Extremes for the months:—Jan., 244, 194; Feb., 282, 216; Mar., 319, 281; Apr., 292, 265; May, 266, 228; June, 245, 211; July, 218, 202; Aug., 205, 185; Sep., 187, 173; Oct., 212, 174; Nov., 222, 205; Dec., 246, 211.

		Cloud Forms.	,			oud A					İ		Wea	ther.			
Day.	7h	13h	18h	7 ^h	9h	131	a 15	h I E	8h 21	Ih	7 ^h	9h	13h	15h	18h	21h	Remarks.
1 2 3 4 5	A. St. Nb. St. Cu. St. Cu. Ci. St. : St.	Ci. Nb. A.Cu.:St.Cu.:Fr.Cu. St. Cu.	Ci. St. Nb. A. Cu.: St.: Fr. Cu. Nb.	2 10 1 9 4	10 1 8	5 0	7	0 10 7 7 (1 0	7 7 0 0	9 10 7 0	d ₀ ≡ ₀ 	□ d ₀ ≡° ≡°	≡° d₀ ≡° ≡°	=° d ₀ =° =° =° =° =° =° =° =° =° =° =° =° =°	<b>■° ■° ■ • • • • • • • • • •</b>	d	
6 7 8 9	A. St. : Nb. A. St. : St. Cu. A. St. : St. Cu. A. St. : Nb.	A. St.: Nb.: Fr.Nb. A. St.: Nb.: Fr.Nb. St. Cu.: Nb. St. Cu.: Fr. Nb.	)	1 10 10 9 0	10 10	10 10	10 10	- IO	0 IC	1 10 0 1 5	 =0  	□ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □	∞ ≡° d₀  g	∞ •° ···	<b>□</b> ≡° ≡°	: : p: [	bmx to bz. $\bigcirc$ 4h. to 10h.: omr to om $a$ : om $p$ : om to odm $a$ : or $\bigcirc$ m to b $p$ : cm to 0 $a$ : b $p$ : $\bigcirc$ 10h. 20m. to 11h. 15m., b to og $a$ : o to bm $p$ : $\bigcirc$ $\bigcirc$ q 12h. 5m.—20m.
11 12 13 14 15	A. St. A.St.:St.Cu.:Nb. St. St. A. St.: St. Cu.	Fr. Cu. ————————————————————————————————————		<1 10 10 10 8	7 10 10	0 10 8	10	1 O	0 IC	7 0 10 0 3	≡° ≡° ≡° ≡°	≡ ≡° ≡° ≡°	8 = 8 = 8	8 8 11 8	8 ≡° 	 ≡° ≡° 	$\square$ , bxf to bz $a$ : bz to cz $p$ : om to bm $a$ : bz to bmx $p$ : $\square$ $n$ :  V, ofx $a$ : ofx to omw $p$ : omw to cm $a$ : cm to b $p$ : bmx to om $a$ : oz to b $p$ :
16 17 18 19 20	A. St. : St. Cu. St. St. St. St. St. Cu.	A. St.: Fr. Cu. St. Fr. Cu. A. St.: St. Cu. St. Cu.: Fr. Nb.	St.	10 10 10 10	10	10 1	3 5	0 10 3 8 5 10	0 10 8 10	0 10 10 10	 =2 = = =	g ≡² • ≡ ∞°	∞ ≡² ≡° ≡° 	80 ≡2 80 ≡0 	8 ≡² ●° ≡° 	=0 =2 =0 	om to oz $a$ : oz to bm $p$ :
21 22 23 24 25	A. St. A. Cu.: St. Cu. St. A. Cu.: St. Cu. A. Cu.: St. Cu.	A. St. : St. Cu. A. Cu. : Det. Cu. Ci. St. Cu. St. Cu.	St. St. — St. Cu. St. Cu.	<1 7 1 8 7	3 0 10	10	0 0 10	2 10 0 0 0 10	0 8 0 0	10 8 0 10 0	prr יוינ	≡° ≡ ≡° ≡°	≡° ⊗ ≡° ≡° ≡°	 :: 8 € 8	≡° .:. 8 ≡°	≡°  ≡° ≡° ≡°	
26 27 28 29 30	St. St.Cu.:Nb.:Fr.Nb. St. Cu. A. St. St. Cu.	St.: St. Cu. St.: St. Cu. A. Cu.: St. Cu. A. St.: Nb. St. Cu.	St.: St. Cu. St.: St. Cu. Nb.: St.	10 10 10 7 10	10 10 8	10 10	10	0 10 - 10	0 2	2 10 10	<b>≡</b> ⁰ <b>d d ≡</b> ⁰	=° d = ° = °	≡° ≡° • •	≡° ≡°  ≡°	≡° ≡° ≡° ≡°	≡° ≡° ≡°	om, om a & p: bm n: om. om to cm a: om p: ● 11h. 3om15h. om to cm a: om p;
Mean Cloud Am'nt		St. Cu.: Fr. Nb.	St.: St. Cu.: Fr. Cu.	1-	-	-	*		5.35		=0	d	=0	=0	=0		om to omd a: om to bc p:
470.	. Richmond (Ke	w Obs.).							~-			***********					February, 1923.
1 2 3 4 5 5	A.St.:St.Cu.:Nb. A. St. : Nb. A. St. : St. Cu. A. Cu. : St. Cu. St.	St. Cu. St. Cu. : Fr. Nb. Ci. : A. St. Cu. Cu. : Fr. Cu.	St. Cu. St. Cu. Ci. : A. St. A. Cu. : St. Cu.	10 10 9 3 10	10 9 2	10 5 3	9	9 5 - 3	5 6	10 10 6 0	 ●°  =²	_ p	.:. 8	d₀ ≡°  ∞	8 p ≡ 8	pr p.:	• In.: o $a$ : o to od $p$ : omr to o $a$ : omr to om $p$ : o to be $a$ : be to o $p$ : $\equiv$ 9h. & 18h. $\implies$ : bm to bem: $\implies$ $n$ : $\equiv$ till 9h. 3om., of to bez $a$ : bez to bm $p$ :
6 7 8	St. Cu. St. Cu. A.St.:Nb.:Fr.Nb.	Ci. Cu. : St. Cu. A. St. : Nb. A. St. : Fr. Nb.	St. Cu. : St. Nb. : Fr. Nb. : St.Cu A. St. : St. Cu.	8 8 10	10	10	9	9 10	3 0	10 8 0	<b>d</b> <b>≡</b> °	& ≡° •	8	∞  ≡º	≡ ● ≡°	 ≡º	b early: cm to or $a$ : oz to orm $p$ :  b early: cm to omr $a$ : omr to c $p$ :  one in. 1om13h. 3om., Line q 12h. 3om.:  [om $p$ : bm $n$ :
9	St. Cu. <b>A</b> .St.:St.Cu.:Fr.Nb.	Cu. Nb.	St. Cu. St. Cu.	3					3 2	4 5	≡⁰	d	■0	∞ •	≡ ₀	≡° ≡°	$\equiv$ till 10h. 15m., bz to om later. om to omr: $\bullet$ a & $p$ :
11 12 13 14 15	Ci.St.:Cu.Nb.:St.Cu. Fr. Cu. St. Nb. St.	Ci.A.Cu.:Cu.Nb.:Cu. A. St.: St. Cu. St. Nb. Ci.Cu.:Ci.:Fr.Cu.:St.	St. · St.	10 10	1 10 9 10	10 10 10	0 IO 10 IO	0 IC	0 IC	3 10 10 10	 ⊒° • ≡²		<b>d d d d d d d d d d</b>	=° = = = =°	=0 =0 =0 =2 =0	<b>d</b> ■ ■ ■ ■ ■	● 0 7h. 50 m. & 12h. 10m., bc to cm $a$ : cm to $\equiv$ till 11h., bfx to om $a$ : om $p$ : [bm $p$ : $\oplus$ oh6h., $\equiv$ 13 h.: om to ofg $\equiv$ after 9h., omr to ofr $a$ : ofg to of $p$ : $\equiv$ till 12h. 30m.: cm to om $p$ :
16 17 18 19 20	St. Cu. Fr. Cu. Nb. St. A. St. : Cu. Nb.	Fr. Cu. : St. : St. Cu. Cu. A.St.:St.Cu.:Fr.Nb. A. St. : Nb. St.	St. Cu. St. Cu. Nb. : Cu. Nb. Nb. : St. St.	2 1 10 10 10	1 10 10	7 10 10	8   8	8 - 8 0 10	0 10 8 1	9 10 1 10 10	$ \begin{array}{c} \equiv^{0} \\ \equiv^{0} \\ \downarrow^{0} \\ \downarrow^{0} \\ \equiv^{0} \end{array} $	≡° ≡° •° ≡°	≡° ≡ ≡° ∞	=°  •° 8	≡° ≡° ≡° ≡°	≡° ≡°  ≡°	bm to om $a$ : om to bm $p$ : $\bigcirc$ $n$ : $\bigcirc$ 2h. 3om.: om to bm $a$ : c to om $p$ : omr to om $a$ : $\equiv$ 13h., omp to bcm $p$ : $\equiv$ $\bigcirc$ 7h1oh. 3om., of to omr $a$ : or to om $p$ : om to omg $a$ $\bigcirc$ $p$ :
21 22 23 24 25	A. St. : Nb. A. St. A. St. : Nb. A.St.:Nb.:Fr.Nb. St.	A.St.:Nb.:Cu.Nb. A. St.: St. Cu. St. Cu. St. A.St.:Nb.:Fr.Nb.	St.	10 10 10 10	8 10 10	10 8 10	10 2 10	0 10 2 0 0 10	0 0 0 0	<1 8 0 10 7	• ] <u> </u>	<b>●</b> °	IX ●         ≡0            d₀         ≡0	≡° •°  ≡°	≡0 ●0 ≡0 ≡0 ≡0	=° •° ≡ =°	omr $a: \mathbb{R}$ 12h. 15m45m.: omr to om $p:$ $\square$ , bmx to omr ₀ $a:$ omr $p:$ $\square$ $n:$ $\square$ early: omr to $c$ $a:$ $c$ to $b$ $p:$ $\square$ $n:$ $\square$ early: $\square$ 1h. 10m3h.: om to omd $\square$ p ⁰ 7h. 30m8h., $\square$ after 9h., of to om $a:$
26 27 23	A. St. : Nb. Ci.:Ci.Cu.:A.St.:Nb. Ci. : Fr. Cu.	Fr. Cu. A. St.: Fr. Nb. Ci. Cu.: Cu.: St. Cu.	Fr. Cu. : Nb. St. Cu. St.Cu.:Cu.Nb.:Fr.Nb	5	10	10	10		0 10	4 10 5	d ₀	•	 ••• 	• 0	 •0	 ≡°	om to bcm $p$ :  to bcq $a$ : bcq to orq, we (gusts) $p$ : $\coprod$ 21h.  (gusts) 9h. 30m13h. 10m.: bc to oqr $a$ : oq to b $a$ : omp to bc $p$ : [oq to oqr $p$ :
Mean Cloud Am'nt				7.4	8.4	8.5	j 8·:	5 7	.66.	. 5							
Day.	7Ь	Cloud Forms.	18h	7 ^h	Clo	oud All F	Amo	noun		1h	7 ^h	9h	13h Wea	15h ather.	18h	21h	Remarks.
				_			——			_							

471. Richmond (Kew Obs.).

March, 1923.

471.	Richmond (Ker	W UUS.).							_							March, 1923.
Down		Cloud Forms.				d An l For						Wea	ther.			
Day.	7h	13h	18h	7h	)h	13h	5h	18h	2 I h	7 ^h	9ћ	13h	15h	18h	21h	Remarks.
1 2 3 4 5	A. St. : Nb. : St. Cu.  ———————————————————————————————————	St. Cu. Cu. Det. Cu.: Fr. Cu. Cu. A. St.: St. Cu.	A. St. A. Cu.: St. Cu. Ci.St.:A.St.:Fr.Cu. Ci.A.St.: A.Cu.: St. Cu. Fr. Cu.: St. Cu.	3 I	I 0	4 2 7	3 -	8 9 3 5 8	10 3 2 3 8	prr:	:: dd ==	.:. 8 8 E	.: 8 8 •°	<b>≡</b> ° 8 8 <b>≡</b> ° <b>≡</b> °	⊸dd iii d	cm to op $a$ : cm to omr $p$ : $\oplus$ 15h. b to bc $a$ : bc to o $p$ : $\bigcirc$ $n$ : $\equiv$ $\sqcup$ till 10h. 30m., bfx to bz $a$ : bz $p$ : $\sqcup$ , bmx to om $a$ : bm to cm $p$ : $\equiv$ , of to om $a$ : omr 0 to cm $p$ :
6 7 8 9	St. Ci. St.: St. Cu. A.Cu.: A.St.: Nb.: Fr.Nb. St.: St. Cu. A.St.:Fr.Nb.:Nb.	A. St.: St. Cu. A. St.: St. Cu. Cu.: St. Cu. A. St. · Nb. St.	Nb. Nb.:Fr.Nb.:St.Cu. St. Cu. A. St. : Nb. St. Cu.	5 8 10 1	7 0	10 I 10 I	0	10	0 10 10 10	<b>4</b> ≡° ≡° ≡°	<b>d</b> : <b>e</b> 8 <b>e e</b>	<b>≡</b> ° 8 8 <b>0 0 ≡</b>		=0 =0 =0 =0 =0	  d₀ ≡⁰	$\equiv \text{till 9h. 3om., of to om } a: \text{o to orm } p: \\ \text{b to orm } a: \text{orm to om } p: \\ \text{T 15h. 45m.} \\ \text{om to omr } a: \text{om to oz } p: \\ \text{om to or}_0 \\ \text{m : } X^0 \\ \text{1oh.} \\ \bullet \\ \text{p 6h. : om to odf } a: \text{of to om } p: \\ \blacksquare \\ n: \\ \end{array}$
11 12 13 14	A. Cu.: St. Cu. Ci. Nb. St. Cu. A.St.:Nb.:Fr.Nb.	A.St.:Cu.:Fr.Cu. St. Cu. Nb. St. Nb. Nb.	St. Cu. A. St. Nb. Fr.Nb.:St.Cu.:St. Nb.	5 10 1 10 1	6 0	9 10 I 10 I	8 0 0	10 10 10	10 10 10 10	≡° ■° ≡°	≡° • • • • • • • • • • • • • • • • • • •	≡°  ⊗ ≡°	 8 ≡°	≡° :: 8 •°	≡° • • • • • • • • • • • • • • • • • • •	bm to om $a : \text{om } p : \equiv \text{about IIh.}$ $\equiv \sqcup : \text{bcfx to o } a : \text{c to o } p : \blacksquare n :$ $\equiv : \text{omr to omrg : om } n :$ om to oz : o $n :$ $\blacksquare^0 a \otimes p : \text{orm to om}$
16 17 18 19 20	St.: Fr. St. St. Fr. Cu. St. Cu. St.	St. Cu. St. Cu. Ci. St. : Cu. Ci.St.:St.:St.Cu. St. Cu.	St.: Fr. St. Fr. Cu.: St. Cu. Ci.St.:A.Cu.:Cu. St.: St. Cu. St.: Cu.	10 I 3 I 9	o o 5	8 4 8	4 8	5 8 10	10 0 3 10 10	iii	≡° ≡° ≡° ≡°	<b>≡</b> ° 8 <b>≡</b>	<b>88</b>	1	≡° ::: ≡° ≡	om om to cm $a$ : cm to bcm $p$ : bmw to om $a$ : bcmq to cm bm to omw $a$ : cz to oz $p$ : ofx to of $a$ : oz $p$ : of to $n$ :
21 22 23 24 25	St. Cu. : Nb. St. : St. Cu. St. Fr. Cu. A. Cu. : St.	A. Cu. A. St. Nb. Cu. A.St.:St.Cu.:St.	A.Cu.:St.:Fr.St. St. Cu. A. St. : Cu. Nb. Cu. : St. Cu. Ci.:A.Cu.:Cu.	10 I 10 I	0	10 1			0 10 10 0 7	⊕dddd	md●dd	8 8 =0	8 8 8	<b>■</b> • • • • • • • • • • • • • • • • • • •	:d	● 5h. 15m7h.: om to bz $a & p : \equiv n$ : $\equiv \text{ till 11h., of w to om}$ • 8h. 10m12h. 30m. & 13h14h.: of rg $a$ : bruw to bz [om $p$ : $\equiv \text{ till 9h., bw to om } a$ : om to bcm $p$ : [to bz $p$ :
26 27 28 29 30	St. Ci.: St. Cu. A.Cu.:A.St.:St.Cu. A. Cu.: St. Cu. A.Cu.:St.:St.Cu.	St. : St. Cu. Ci. : Fr. Cu. Cu. A. Cu. : Cu. A.St.:Cu.:Fr.Cu.	Ci.: St. Cu. Ci.: St. Cu. St. Cu. St. Cu. A.Cu.:Cu.Nb.:St. Ci.Cu.:A.Cu.:St.Cu.	4 9 9 I	8 6 0	8 7 7	o 7 6 0	8	0 10 10 4 10	<b>≡</b> d ::: <b>≘</b>	<b>■</b> 8 :: : <b>®</b>	≡° y  ∞	у  Т	∞ y d₀  ∞	d ::: ° ≡ °	$ \begin{array}{l} \bullet \text{ early : } \equiv \text{ till 9h., of to om } a : \text{or}_0 \text{m} \\ \equiv \text{ bw to cy } a : \text{c to b } p : \oplus \text{ 13h.} \\ \bullet \text{ 3h. : o to bc : } \bullet \text{ d 18h.} \\ \bullet \text{ p 5h. : op to cz } a : \text{ or T to cm } p : \bullet p : \\ \text{cmw to oz } a : \text{ oz to cz } p : \end{aligned} $
31 Mean Cloud	A.St.:St.Cu.:St.	A.Cu.:Cu.Nb.:Fr.Cu.	Ci.:Ci.Cu.:Fr.Cu.	10 I 7·78	o 1	- -	• •6	8 8 · 1	3 6·9	<u>=</u> ⁰				•••		$\triangle$ , om to oz $a$ : oz to bc $p$ :
Am'nt										<del></del>		L				A!! 4000
472.	Richmond (Ke	w Obs.).		1 1				1			1			I	I	April, 1923.
1 2 3 4 5	A.St.:St.:Fr.St. A. St. A. St. : St. A. Cu. Ci.:Ci.St.:A.Cu.:A.St	Cu. St. — A. St. A. St. . A. St. : St. Cu.	A. Cu. : St. Cu. Ci. St. A. Cu. Ci.Cu.:A.Cu.:A.St. Nb.	10 1	ο l	0	- 0 7 I	8 2 8	10 10 2 0 10	ddddd	8 III P P P	8 8 8 8 8 8	8 8 8 8 8	<b>■</b> 8 8 8 <b>● •</b>	d₀ ≡° d₀	omw to cz $a$ : cz to om $p$ : $\equiv$ 15h. omw to bz $a$ : bz to bcz $p$ : $\oplus$ 16h. omw to cz $a$ : cz to bz $p$ : $\equiv n$ : $\equiv$ , bf to b $a$ : b to cz $p$ : $\triangle$ , bcm to oz $a$ : oz to omr ₀ $p$ : $\bullet$ $n$ :
6 7 8 9	A. St.: Nb. St. A.Cu.:Cu.:Fr.Cu. Cu.: Fr. Cu. A.Cu.:St.:St.Cu.	A.St.:Nb.:St.Cu. St.:St.Cu.:Cu.:Fr.Cu. Cu.: Fr. Cu. A.Cu.:Cu.Nb.:St.Cu. A. St.: St. Cu.	A.St.:Nb.:Fr.Nb. Fr. Nb.:St.:St.Cu. Ci. St. Fr. Cu. : St. Cu. St. Cu. : St.	4	4	8 4 10 I	8 - o	10 10 2 9	10 0 0 2 10	<b>p</b> 8 : <b>p</b> •	d  ≅°	≡⁰ ∞  ∞ y	8 8 8 8	≡° ∞  ≡°	=°	omr to om $a$ : om to oz $p$ : $\equiv$ 9h. 3om11h., omw to of $a$ : cz to oz $p$ : bcq to bq [b $n$ : bm to oz $a$ : oz $p$ : $\clubsuit$ ° 12h. 25m. & 13h. 15m. $\frown$ , om to oz: $\bullet$ $n$ : $\lceil \equiv$ 18h., $\lceil \le 23h24h$ .
11 12 13 14	St.: Nb. Ci.:Ci.St.:St.Cu. Ci.:Ci.Cu.:St.Cu. Ci. St.	A.Cu.:A.St.:St.Cu.:Cu. St. Cu. Ci.St.:St.Cu.:Cu. Nb.: Fr. Cu.	Ci.:Ci.St.:A.Cu.:Nb. Nb.: St. Cu. A.St.:Nb.:Fr.Nb. Ci.St.:Fr.Cu.:Nb.	5 6 1	7 5	9 I 8 I 8	7	4 10 10 7	5 8 8 0	=° =° :d	=° d₀ 	& 	•° ···	■ • ° • ° ···	=° =°	<ul> <li>oh. 4om3h.: om to cz a: or to bc p:</li> <li>ih. ● ih3h.: bem to or a: o to omr p:</li> <li>4h5h.: o to bc a: c to or p:</li> <li>b to cu a: cu to cp: ● p ioh. 4om. &amp; [13h. 2om.: bw n;</li> <li>oh. 4om.: bw to o a: orm to bc p:</li> </ul>
15 16 17 18 19 20	Ci.: Cu.  A.St.:St.:Fr.St. St. Cu. St. Cu. A.St.:A.Cu.:St. St.	Ci.:Ci.St.:Cu.:Fr.Cu.  St. Cu. : St.	A.St.:Nb.:Cu.Nb.  A. Cu.: St. Cu. St. Cu. A. Cu.: St. Cu. St. Cu. St. Cu.	10 I 9 10 I 10 I	7 0	10 I 4 5	0 0 8	8 6 8 10 7	10 9 1 0	≡° ≡° ≡° ≡°	■ 8 8 8 <b>■</b>	8 8 8	8 8 8 8	88888	:: ⊜ :: 8 ::	$ \Omega $ , om to o $a$ : oz to cz $p & n$ : o to bcz $a$ : bz to bcz $p$ : om to bcz $a$ : oz to cz $p$ : b $n$ : om to oz: $0^0$ roh. 3om.: b $n$ : om to cz $a$ : oz to bcz $p$ : b $n$ :
21 22 23 24 25	A.Cu.:St.Cu.:Fr.Cu. A. St.: Nb. Cu. A. Cu.: A. St. A.St.:Nb.:Fr.Nb.	A. Cu.: St. Cu. Ci.:Ci.St.:Fr.Cu.:St.Cu. A. Cu.: Cu. Cu. Nb.	St.Cu. Ci.:Ci.Cu.:Ci.St.:St. St. Cu. Cu. Nb.	10 I 9 2	8	9 9 I		10 1	9 10 9 0	 p <b>6</b> ° ∞ •	p ●° ∞		  	 & 	:: d	b to o a: o to c p: ● 6h. 3om. & 1oh.: om to omq a: om to □, b to o a: o p: [bcq p: ● p 3h. 2om.: bc to b ● 6h. 15m8h. 1om., (gust) 11h. 5m.: [om to orq a & p:
26 27 28 29 30	Nb. — A. Cu. : Cu. A. St. : Nb. St. Cu.	A. St. : Cu. Cu. Cu. A. Cu. : Cu. : St. A. St. : St. Cu.	A. St.: Nb. Ci.:Ci.St.:St.:St.Cu. St. Cu.: Cu. Nb. St. Cu. St. Cu.	0 5 10	10 3 <1 0	5	0 6 8 -	6 8 8 9	0 8 2 5 10	• d d • [®]	 8 •	  	• 	8 	.:. d	<ul> <li>oh7h. 3om., Line q</li></ul>
Mean Cloud Am'nt				7.3	9	7.5	†	7.8	5.2							
Day.	7h	13h	18h	7h	!					7 ^h	9h	13h	15h	18h	21h	Remarks.
		Cloud Forms.	· ·			ud A ll Fo						We:	ather.			

#### 473. Richmond (Kew Obs.).

473	3. Richmond (Ke	ow Obs.).														May, 1923.
Dans		Cloud Forms.				ud A						Wea	ather.			
Day	7h	13h	18h	7h	9h	13h	15h	18h	21 h	7h	9ћ	13h	15h	18h	21h	Remarks.
1 2 3 4 5	St. Cu.: F. St. Ci. St.: A. Cu. St. Cu.: St. ————————————————————————————————————	St. Cu. Ci. Cu. : Cu. A. Cu. Ci. Ci.St.:A.St.:St.:St.Co.	Cu. Ci.: Ci. Cu.: A.Cu.: A.St. Ci.: St. Cu. Ci.: Ci. St.: A. Cu. u A.Cu.: A.St.: Fr.Cu: St. Cu.	9	10 5 9 1	10 7 3 3	7 1 8 7		3 10 <1 2 2	bþ⊪b:	p 8 III 8 :	.8 : 8 :			d : d : :	o to bc $a$ : o to b $p$ : $\triangle$ , bm to cz $a$ : cz to b $p$ : $\blacksquare$ 22h. orm to b $a$ : b to c $p$ : $\triangle$ , bm to bc $\triangle$ , b to om $a$ : om to c $p$ : $\blacksquare$ 14h. & 16h.
6 7 8 9	A.St. : Nb. : St.Cu. A. Cu. : St. Cu. A. St. : Ci. : Cu. St. Cu.	Ci. : Cu. Ci. St. : Cu. A.St.:St.:St.Cu. A. Cu. : St. Cu. Cu. Nb.	A.St.:A.Cu.:Cu. A.St.:Fr.Cu.:Nb. St. A.Cu.:St.Cu.:Fr.Nb. Ci.: Cu.		5 6 9 10		10	10	7 10 10 7 2	dd iii iii d	<b>d</b> 8 <b>m</b> 8 <b>m</b>	8 8 ::	 «»	 80 		$\triangle$ , om to b $a$ : b to o $p$ : $\triangle$ , oz to bcz $a$ : c to $\bullet$ $p$ : $\bullet$ 22h23h. om to oz. bcm to o: $\bullet$ 17h17h. 35m., $\bullet$ 21h. & bc to o, $\bullet$ $\blacktriangle$ 12h. 10m., $\bullet$ 12h. 50m.: $\bullet$ $n$ :
11	Ci.Cu.:Ci.St.:St.Cu. Cu.	Ci. Cu. : Nb. Nb. : Cu. Nb.	Ci.:Cu.Nb.:St.Cu. Ci.:Ci.St.:Cu.:Cu.Nb	4 1	8 7	5 9	7 8	6 4	5 2	þ:		P ●	<b>P</b> ●			[& 17h. 45m., ● ▲ 18h. 30m. otobc: ● q 14h. 35m., → (gusts) ● p 15h.
13 14 15	St. A. Cu.: St. Cu. Ci.St.:Ci.:St.Cu.:Fr.Cu.	Cu. Ci. Cu. Nb.	Ci.St.:Cu.:Cu.Nb. Ci.:A.Cu.:Fr.Cu. Nb.: St. Cu.	9 9 6	9 6 10	5 6 10	- 7 10	5 8 9	7 4 3	::   	≡° 		  •°			$\bigcirc$ 3h5h.15m.: o to b a: bc to c p: $\bigcirc$ p $\bigcirc$ , b to o: $\bigcirc$ 18h. [22h. 3om. bc to o a:o p:frequent showers: $\square$ (gusts) a: $\square$ (gust) 13h. 5om.
16 17 18 19 20	Ci.St.:A.Cu.: Fr.Cu.:St.Cu A.St.:Nb.:Fr.Nb. St. Cu. St. Cu. A.Cu.:St.:St.Cu.	Fa.Ci.:Cu.Nb.:Fr.Cu Cu. Nb. : Cu. St. Cu. St. Cu. A.St.:Fr.Cu.St.Cu.	. A.Cu.:Nb.:Cu.Nb.:St.Cu. Cu. Nb.: St. Cu. St.: St. Cu. St. Cu.	9 8 10	10	10	10	10	1 7 10 10	<b>d</b> •° ≡° 	d			8	 ≡° ≡° 	btoo: T12h.48m., $\spadesuit$ p 12h. 35m., Line q. btoo: $\spadesuit$ p 10h. 35m., $-45$ m., $\spadesuit$ p 0 15h.20. c to o. om to o: $\spadesuit$ d ₀ 9 h. o: $\spadesuit$ p ₀ 20h. 15m. $\blacktriangleleft$ 21h. 30m.
21 22 23 24 25	A. St. : St. Cu. A. St. : Nb. A.St.:St.Cu.:Fr.Nb. A.St.:Nb.:Fr.Nb.	A. Cu. : St. Cu. St. Cu. A. St. : Nb. Cu. A. Cu. : St. Cu.	A. Cu.: St. Cu. St. Cu. A.St.:Nb.:Fr.Nb. Cu. A. Cu.: St. Cu.	10 1 10 1	0	8 10 6	10 1	10	7 10 10 <1 3	=° =° =°	 ≡⁰  ∞	•	•	•	80 ≡0 	ow to cz. om a: bc to omo p: ▲ ● p 10h.35m. & 13h.35m.: o to or a: bm to bc a: bc to cp: [o to orm p: ● 5h.45m6h.5m.: om to or a: o to bcp:
26 27 28 29 30	Ci. St.: A. Cu. Ci.:Ci.St.:Fr.Cu.:St.Cu. A.St.:Nb.:St.Cu. Nb.: Fr. Nb. St.	St. Cu. : Cu. A. St. : St. Cu. Cu.:St.Cu.:Fr.Cu. Nb. Cu.	A. Cu. A.Cu.:St.Cu.:Cu. A.St.:St.Cu.:St. Nb. A.Cu.:St.Cu.:Fr.Cu.	10 1 10 1	O	8 1	[O]	6 1 10 1	8 10 10 10 10 10 10 10 10 10 10 10 10 10	<b>d</b> ≡° ≡° ≡°	∞ =0 0 0 0 =0	& & .:. ●° &	& & &	8  ⊕° ≡°	80 ●00 ●00 ■00	
Mean Cloud Am'nt	St. : Fr. St.	St. Cu.		10 7·5	-	-	* -	7.0		<u>=</u> 0	=0				=0	om a: om to cz p:
474	<u>'</u>	w Obs.).					<u>-</u> -	!-			1			•		June, 1923.
1 2 3 4 5	St.: St. Cu. A.St.:Nb.:St.Cu. Ci.: Ci. St. Cu.: Cu. Nb. A.St.:St.:St.Cu.	A. St. : St. : St. Cu. St. Cu. St. Cu. A St. : Cu.	A.St.:St.:St.Cu. Fr. Cu. : St. Cu.	10 I 5 8	0  1 0   9  1	10 I	0 I 0 I	0 1	0	≝° b: d:d	0 ∞ 	8 8 8 8	8 8	& & & 	≡° ⊗  ≡°	om to oz. $\bullet$ d ₀ 6h. 45m. : om to oz. bw to bcm $a$ : bz to o $p$ : $\bullet$ 0h. 5omrh. 3om. : c to o $a$ : o $p$ : $\bullet$ , om to omd $a$ : oz to c $p$ :
6 7 8 9 10	A.St.:St.Cu.:Nb. A.St.:St.:Fr.St.:Cu.Nb. Ci.St.:A.Cu.:St.:St.Cu St.: St. Cu. Ci.St.:A.Cu.:St.:St.Cu.St.	A.St.:Cu.Nb.:St.Cu. St. Cu. A. Cu.: St. Cu. St.: St. Cu. Ci.St.:Ci.Cu.:Cu.	A.Cu.:A.St.:St.Cu.:Cu. A. St.: Fr. Nb.	9 10 I 10 I	8 1 0 1	10 I	0 I 8 I 0 I	0 1	3	 ≅° •°	≡°  	p ● ⁰	p ●°  q 	d ₀	<b>a</b>	or ₀ to om $a:$ o to odm $p: \equiv n:$ or ₀ m to c $a:$ o $p:$ bmw $n:$ $\bigcirc$ , o $a:$ cq to o $p:$ $\bigcirc$ p ₀ 17h. 25m. o $a \stackrel{\circ}{\sim} p:$ o to bc $a:$ bc to b $p:$
11 12 13 14 15	Ci. Cu. Ci. Cu.: St. Cu. A. Cu.: St. Cu. A.St.:A.Cu.:St.Cu.	Ci.St.;St.Cu.;Cu. Ci.St.;A.Cu.;Det.Cu. Ci. St. : Det. Cu. A. Cu. : St. Cu. A. St. : St. Cu.	A. Cu. : Cu.	4 10 10	9   1 0 8	10   I 9   9	0   I 7 7	4 < 1 7 1 4 1 0 1	0	dd‱ : :			  		 ■  ≡°	$\triangle$ , be to 0 $a$ : 0 to b $p$ : $\bigoplus$ 13h. $\bigcirc$ , b to 0 $a$ : 0 $p$ : $\bigoplus$ 21h22h. 30m. om to c $a$ : 0 to be $p$ : 0 to c $a$ : 0 to be $p$ : 0 $a & p$ : $\bigoplus$ 13h. 45m16h. 15m.
16 17 18 19 20	A.St.:St.Cu.:Nb. A. Cu.: St. Cu. A. St.: St. Nb. A. St.: St. Cu.	A.Cu.:A.St.:St.Cu.:Nb. St.Cu.:Cu.:Cu.:Nb. Ci. St.: Cu. St. Cu. A. Cu.: St. Cu.	St. Cu.	3 1	5 0 1 0 1	7 10 10	0	9   1	9	d <b>d = = =</b>	d₀  o⁰ d p •⁰		<u></u>	•••	=° =° =°	o $a:$ o to c $p:$ b to c $a:$ bc to o $p:$ o to c $a:$ o $p:$
21 22 23 24 25	Oi.Cu.:Ci.St.:St.Cu. Ci.Cu.:Ci.:St.Cu. Ci. Cu. A. Cu. St. Cu.	A St.Cu.:St.Cu.:Cu.Nb. A. Cu.: St. Cu. Cu. A.Cu.:St.Cu.;Cu. A. St.: Nb.	A. St. : St. Cu. Ci. : St. Cu. Ci. Cu. : Cu. A. St. : St. Cu. A.St.:Cu.Nb.:St.	8 10 1 2 7 3	2	9 .	8   8 4   3 -   10	8   3   10	3 7 0	 <b>.</b> ≡°	œ 	  	  —	●°   ≡°	≡° ≡°  ≡°	bm to bz & cż $a$ : o to op & om $p & n$ : o to cy $a$ : cy to bm $p & n$ : bwz to b $a$ : bcy $p$ : by to c $n$ : bc to c, bc to c & oy $a$ : oy to o $p & n$ : o: $lacktriangledown$ 15h15h. 3om., $lacktriangledown$ 02th22h.: om $n$ :
26 27 28 29 30	St. Cu. : Nb. Ci. St.	A. St.: Nb. A.Cu.:A.St.Cu.:St.Cu A.Cu.:A.St.:St.Cu. Cu. A.St.:St.Cu.:Det.Cu.	A. St. : St. Cu.	9   8 10   2 1   0	2 1	0 10	9 10	0   10 9   10 2   1	2 إ	の マミ マミ マミ マミ	:: ■ 8 8 ::	•°		:: 8 8 ::	=° d=° =°	om to odm $a$ : odm to be $p$ : c to bmw $n$ : bmw to om $a$ : 0 & oy to be $p$ : be to b $n$ : omw to bz to oy $a$ : ozw $p$ : ozw to bzw $n$ : bwmz to bezy $a$ : bmw $n$ : bfw to bezw:be to oy $a$ : op ₀ to o $p$ : o to be $n$ :
Mean Cloud Am'nt			7	7.8	98	·6 8	5 8	3 7	. 8							
Do	7 h	13h	18h	7h 9					I h	7h	9ћ	13h	15h	18h	21h	Remarks.
Day.		Cloud Forms.		С		d An l Fo						Wea	ther.			пешагаз.

475. Richmond (Kew Obs.).

July, 1923.

475.	. Richmond (Ke	w Obs.).														July, 1923.
		Cloud Forms.					Amo					Wea	ather.			Bernades
Day.	7h	13h	18h	7h	9h	13h	151	181	21 h	7h	9h	13h	15h	18h	21h	Remarks.
1 2 3 4 5	St. Cu. Ci.Cu.:A.Cu.:St.Cu. A. Cu.: St.: Fr. St. A. Cu.: St. Cu. Ci.:Ci.Cu.:Ci.St.	A. St. : St. Cu. A.Cu.:A.St.:St.Cu. A. St. : St. Cu. A. Cu. : Cu. Cu.	St. Cu. : Cu. A. Cu. : St. Cu. St. : St. Cu. Fr. Cu. St. Cu.	10 7 9 8 3	8 4 10 10	10 10 10 4 3	- 10 10 4 0	7 8 10 <1 2	10 4 10 1	9:               			— •• •• ···	   	  	o to bc & o c to bcz to oy $a$ : cy $p$ : bc $n$ : omfw to o $a$ : or to o $p$ : o $n$ : o to bc $a$ : bc to b $p$ : bm to c $a$ : b to bz $p$ :
6 7 8 9	A. Cu. : St. Cu. St. : St. Cu. Ci. A.Cu.:St.Cu.:Cu.Nb.	A. Cu. Ci. : Cu. Ci. : Cu. Ci. : Ci. St.	Ci.Cu.:Ci.:A.Cu.:St.Cu. Cu. Ci. Cu. : A. Cu. A. St. : Cu. Nb.	0 7 10 1 7	9 10 <1 9	0 6 7 7 7	0 6 - 1 4	0 6 3 4 10	0 9 1 9 5	: 8 : <b>d</b> 🖺	  ⊗ ≡⁰	 0 		 ()  T	 =°	bz to b cz to bc a: bc to o p: o a: o to b (): p: bw to ba: b to om p: \( \frac{2}{2} \) zh.45m4h.30m. \( \frac{7}{1} \) 15m8h.15m. & 18h.30m19h. \( \hrac{1}{8} \) [18h. 35m.
11 12 13 14 15	A. Cu. : A. St. A. St.:St.:St.Cu. A. Cu. : Cu.	Fr. Cu.  A. Cu. : St. Cu. Cu. : Cu. Nb.	Cu. Ci. : Ci. St. : A. Cu. Ci. St. A. Cu. : Cu. Nb. Ci.:Ci.Cu.:Cu. Cu.Nb.	2 0 2 10 3	1 0 1 10 7	0 0 0 7 8	0 0 8 -	5 0 3 7	2 1 0 2 10	แฝ ៵ ๖๎๔	8 8 8 8	 80 	 	 	d8 :d =	bm to b bwm to bz $a$ : b to bcz $p$ : bz to b od to c $a$ : c to b $p$ : bw to c $a$ : o to bc $p$ : d 21h. 45m.
16 17 18 19 20	A.St.:Nb.:St.Cu. St. Cu. A. Cu. : Cu. Ci. : Ci. St. A. St. : St. : Fr. St.	Cu. A.St.:St.Cu.:Nb. A.Cu.:St.Cu.:Cu. A. St.: Fr. Nb. Fr. Cu.	St. Cu.: Ma. Cu. A. Cu.: Cu. A. St.: Nb.	10 9 5 4 10	10 8 6 2 6	6 10 8 10 1	5 10 9 10 0	8 10 7 10 0	4 10 9 10 0	: b: :					•••	om to omp $a$ : be to c o to c $a$ : o to op $p$ : op to be $a$ : cytooy $p$ : [to b & or $a$ : omd $p$ : • 12h.30m13h., 13h.30m14h.20m.:bcwz o to c & be $a$ : b to by $p$ : b $n$ :
21 22 23	St. Cu. St. Cu. : Cu. Ci.:Ci.Cu.:A.Cu.:St.Cu.	Cu. St. Cu. Ci.St.:A.St.:Fr.Cu.	Cu. Ci.: Ci. haze St.: St. Cu.	9 8 8	8 10 5	5 9 10	4 - 10	ŀ	3 2 10		 	 	<del></del>			b to c & o a : bcy to b $p$ : b $n$ : c to o a : c to bcy & by $p$ : b $n$ : $\bullet$ 14h.5m., $\bullet$ 14h.15m15h., 19h.45m [21h.5m., d 19h.30m.: bm to bc & cy $a$ : by to b $p$ :
24 25	Ci.St.: Ci.Cu.: A.St.: Cu. A.St.:Nb.:St.Cu.	Ci. : Cu. Nb.	Ci. : Cu. Ci. : St. Cu. : Nb.	3 10	5 10	7 10	5 10	3 9	1 2	=⁰ `	•••				•••	o to omd & orm $a$ : odm to o $p$ : o to b $n$ :
26 27 28 29 30	Ci. : Cu. Ci. : Al. Cu. A.St.:Fr.Nb.:St.Cu. A. Cu. : Fr. Cu. Ci.St.:A.Cu.:Fr.Cu.:Cu	Cu.: St. Cu. A. Cu.: Cu. Nb.: St. Cu.: St. A.St.:St.Cu.:Cu.Nb. A.Cu.:A.St.:Fr.Cu.	Ci. St. : Cu. A.St.:St.Cu.:Fr.St. A.Cu.:St.Cu.:Nb. A. St. : St. Cu. St. Cu. : Nb.	2 4 10 2 7	5 2 10 4 9	7 8 10 10		3 10 9 10	1 9 2 10 10	 G≡₀			 			b to bc & c $a$ : b to bc $p$ : b $n$ : bcwz to cy $a$ : od ₀ to cy & o $p$ : o $n$ : op to o, od ₀ & or $a$ : cur to o $p$ : $n$ 19h. 3om.: b to bc & o $a$ : cy to o $p$ : c to or & c $n$ : [b $n$ : c to o $a$ : oy, op to od $p$ : or $n$ :
31 Mean	Ci.;Al.Cu.;Cu.;Fr.Cu.	A.St.:Nb.:St.Cu.	Nb.	7	10	10	10	10,	3							$\frac{c to \circ a : or to op  p : or to b  n :}{}$
Cloud Am'nt	,			6.0	6.4	6.5	5.7	5.8	4.8							·
476.	Richmond (Ke	w Obs.).					1	1					<del></del>			August, 1923.
1 2 3 4 5	A. Cu. A.Cu.:Fr.Cu.:St.Cu. Ci.Cu.:Ci.St.:Cu A. Cu.	Cu. Ci.Cu.:Ci.St.:A.Cu.:A.St. Cu. Cu. Ci. : Ci. St.	A. Cu. : Cu. Ci. St. : Cu.  Ci. : Ci. St. : A. Cu. Ci. : Ci. Cu. : St. Cu.	2 8 3 0 1	3 2 5 0 3	5 8 5 5 4	5 10 2 3	I 2 <i 7</i 	0	: : : d 🖺	•••		 			or to c & b a: bcy () p: b () y to c n: c to bc & b a: c () y-op ₀ p: c-bc-b n: b to bcy & by () a: bc to b () p: b n: bw to b, bcy to c a & p: bc to bw n: bzw to b & bc a: bcy to cy p: b n:
6 7 8 9	Ci. St. A. Cu: A. St. Ci. : Ci. St. 	Ci. St. Ci. St. : Cu. Ci. Cu. 	Ci. Cu. : A. Cu. Ci. : Ci. St. : Cu.  Cu. Nb.	1 5 3 0	2 3 4 0	8 8 7 0	8 6 5 5	7 3 0 7	3 1 8		•••					bwm to bz, bc to oy $a : cy()$ to bc $p : b n :$ bcwm to b, c to bc() $a : bc()$ to b $p :$ bwm to bc $a : cy$ to bcy $p : by$ to $b n :$ bmw to by $a : bcy$ to cu $p : cu$ to bc $n : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b : bcy b :$
10	A. Cu. : Cu. : St.	Ci. Cu.	Ci. Cu. Ci.	7 2	3	7	9	5	4	⁰≡⊅						b. bc to bm $a$ : ov to bcy $p$ : $\oplus$ 13h. b $n$ :
11 12 13 14 15	A. Cu. : Det. Cu. Ci. St. : Ci. Cu.  A. Cu. : A. St. A. St. : Nb.	Ci. : A. St. : A. Cu. Cu. Cu. : St. Cu. St. Cu. : Cu. Cu.	Ci. St. Cu. : Fr. Cu. Ci. Cu. : Cu.	3 0 6 10	4 1 6 10	3 8 7 5	8 8	3 7 2 0	2	=: d=° =°	•••					bfw to bzw, bcy to by $a$ : by to $bp$ : bzw to $b$ , b to cy $a$ : cy to $bp$ : $bn$ : bcmw to bcz, oz $a$ : czy to $bp$ : o to $bn$ :  • 5h.3om., opm to omr, odm to bcy $a$ : bcy [to $bp$ :
16 17 18 19 20	Ci.: A. St. A.Cu.:St.Cu.:St.Nb. St.Cu.:Nb.:Fr.Nb. Ci.Cu.:A.Cu.:St. A.St.:St.Cu.:Nb.	Ci.St.:Ci.Cu.:Cu. A.St.:St.:Cu.Nb. A.St.:Fr.Nb.:Fr.Cu. St.Cu.:Cu.:Cu.Nb. St. Cu.	A. Cu. : Nb. : Cu. A. St. : St. Cu.	7 10 10 6 10	9 10 8 9 10	8 10 9 9	8 10 9 - 10	10 4 8 10 10	10 6 1 10 9	d ₀ ≡ 0	⊕ : : : <b>⊕</b>	 •° 	 • -	•••	•••	cmw to 0, 0 to cy $a$ : cy to oy $p$ : 0 $n$ : 0 $a$ : 0 to bc $p$ :  0 16h.25m5om.  0 to c $a$ : 0 to c $p$ :  12h.15m5om.  2 bc to 0 $a$ : 0 to c $p$ :  13h.55m.  2 p: 0 m to 0 $a$ : 0 $p$ :
21 22 23 24 25	A.St.:Fr.St.:St,Cu. A. Cu. : Cu. Ci. : St. Cu. Ci. : S . Cu. : St. Ci. : Ci. St.	St. Cu. Cu. St. Cu. Cu. Nb. : Nb. A.Cu.:Cu.:St.Cu.	Cu. Ci. Cu. A. St.: Nb. A.Cu.:A.St.:Cu.Nb.:Nb. St. Cu.	10 2 2 7 1	8 7 8 9	10 4 10 10	10	1 10 9 10	1 0 10 2 10	=dd™d	  •	q  0 !\sq	 •° •°	 •° 	•	ouq to c $a$ : oqd to b $p$ : bw to c $a$ : bc to b $p$ : bmw to o() $a$ : o() to or $p$ : $\spadesuit p \& n$ : bm to otlr, $\spadesuit a \& p$ : $\upalpha a \& p$ : $\upalpha 12h.40m13h.$ bmw to oz $a$ : o $p$ : $\spadesuit^0 n$ :
26 27 28 29	A.St.:St.Cu.:Fr.Nb. A.Cu.:St.Cu.:Cu.:Fr.Cu Fr. Cu. A.St.:Nb.:Fr.Nb.	Ci.Cu.:Ci.St.:St.Cu.:CuNb Cu. Nb. Ci. Cu.: St. Cu.	St. Cu. : Nb. : Cu. Nb. : Cu. Nb. Ci. Cu. : A. Cu. : Cu. Ci. : Nb. : Cu. : Nb. Fr. Cu.	4 <1	9 6 6 10 1	9 9 8 10 2	- 5 8 10 6	3 8 4 9 2	0 8 38 0	: d ; 🕞 a	  •° q	 p ●  • q	 d	 p ● 	: : : <b>-</b> d	o $a:$ o to b $p:$ $\bigcirc$ ° 5h.30m., 8h.10m. & 10h. bc to o () $a:$ op to bc $p:$ $Tp$ $\bigcirc$ 2 $\triangle$ 16h. 15m. b to o $a:$ c to bc $p:$ orm to om: T 15h.45m (gusts) 18h. & 23h. (gusts) oh.35m2h.10m.: bq to bc
31	•••	Ci. Cu.	A.Cu.:St.Cu.:Fr.Nb.	0	3	7	9	7	<u>1</u>	_ <b>=</b> 0					Д	btoca:otocp:●° 16h.3om.,●p 17h.15m.
Mean Cloud Am'nt				4.2	5·6	7.2	7.5	5.3	3 · 7						1	
	7h	13h	18h	7h	9h	13h	15h	181	2 I h	7 ^h	9h	13h	15h	18h	21h	Remarks.
Day.		Cloud Forms.					Amo					Wea	ther.			Rem <b>ai as</b> .
	I			1						<del></del>						

356 <b>477.</b>	, Richmond (Ke	w Obs.).	DIA	1R)	<i>(</i> (	)F	CL	.Οι	JD	AND	WEA	THER	<b>ί.</b>			September, 1923.
		Cloud Forms.				oud All F						Wea	ather.			
Day.	7 ^h	13h	18h	7h	T ·	T	ī	Ť	3h 21h	7h	9h	13h	15h	18h	21h	Remarks.
1 2 3 4 5	Ci.Cu.:Ci.St.:A.Cu.  A. Cu.  A. St.: Fr. Nb.  A. St.: St.: Fr. St.	Cu.: Cu. Nb. A.Cu.: St.Cu.: Cu. Cu. Nb. Ci.: Ci. haze	Ci.: A. Cu.: Cu. Nb. St. Cu.: Fr. Nb. Ci.: Cu. Ci.:Ci.St.:St.:Fr.St. Ci.	0	5 <1 0 10	5 9 4 10 7	6 - 6 10 1	6 7	2 0 I	ııı i bb⊪	<b>#</b> d <b>6</b> : <b>6</b>	  •°	   d 	  =0	:: b: b::	bw to op $a$ : bc to cp $p$ : bw to o $a$ : o to bc $p$ : bw $n$ : $\Rightarrow$ , bwm to o $a$ : o to cm $p$ : bw to orm $a$ : or to cm $p$ : b to om $n$ : om to c $a$ : c to b $p$ :
6 7 8 9	St. Nb.  Cu. : St. Cu.	Cu. A. St. : St. : St. Cu. Cu. Cu.	St. Cu. Ci. A. Cu. : Cu. Fr. Cu. : St.	10 10 0 0	10 10 0 3 4	3 10 0 4 5	0 6 1 - 7	0 6 < 2 8	8 0 <1	≡ d ₀ d ≡ d	iii : iii : d	  	8 - 8	8 : 8	d  ≡° 	bw to ofw & b $a$ : b $p$ & $n$ : omd ₀ to o $a$ : o to bc $p$ : $\equiv$ , bfw to bz $a$ : bz to b $p$ : bm to bfw $n$ : $\equiv$ , bfw to bc $a$ : bc to b $p$ : bw to om $a$ : bw to om $a$ : bc to cz $p$ : o to om $n$ :
11 12 13 14	A. St. : St. St. Cu. St. A. St. : St. : Fr. St. Fr. Cu.	Cu. Ci. A. Cu. Ci.: St.: Fr. Cu. A. St.: Nb.	Ci. : Cu. Ci. : Ci. St. A. Cu. : Cu. A. Cu. : St. : Fr. Cu. A. St. : Nb. : St. Cu.	10 9 10 10 <1	5 6 8 3	5 4 6 7 10	1 4 8 9 4	1 5 3 9 6	0 10 10	<b>=</b> ° d :: : <b>=</b> °	≡°  	  				omw to bc $a$ : bc to b $p$ : b to o $n$ : ow to bc $a$ : bc $p$ : b to ofw $n$ : ofw to bc $a$ : bc to c $p$ : o $n$ : o to c $a & p$ : bm to o $a$ : or o to bc $p$ : bw $n$ :
16 17 18 19	 Ci. A. St. : St. Cu. 	Cu. Ci.: Fr. Cu. Ci.: Cu. A. St.: St. Cu.	Cu.: St. Cu. Ci.: A. St. Ci. Cu. A. Cu.: Nb.	0 1 9 0	6 2 0	3 6 10	- 5 9 10	4 2 1 10	1 1 9	dd :d	d : : :	 	 	  d ₀	d d : :	bw to b $a$ : b to bc $p$ : bwm $n$ : bwm to b $a$ : b to bc $p$ :
20 21 22 23 24 25	St. Cu.  A.Cu.:St.Cu.:Fr.Cu. Ci.Cu.:A.Cu.:St.Cu. Ci. : Nb. : St. Cu. St. Cu. Cu.	St. Cu.  Nb.: St. Cu.  A.St.: Nb.: St.Cu.  Ci.:Ci.St.:Cu.:Cu.Nb.  A. Cu.: Cu.  Ci.: A. Cu.	A. St. : St. Cu.  Cu. : Fr. Cu. A. St. : Nb. : Cu. A. St. : St. Cu. A. St. : St. Cu. St. Cu. : Nb.	3 7 5 <1	10 10 5 5	10 10 7 9	8 9 10 - 8 4	10 10 9 10 10	<1 10 6 10	 ≡°  u ≡°	 d₀   ≡⁰ 		  q	   q	 =0   q	○ oh. 3ohi. — 1h. 15hi.,
26 27 28 29 30 Mean	Ci.: Cu.: St. Cu. A. St.: St. A.St.:A.Cu.:St.Cu. St. St. Cu.	St. Cu. A. St. : St. Cu. Ci. : St. Cu. St. Cu. Cu. : St. Cu.	St.: St. Cu. Ci. St.: A. St. A.Cu.:St.Cu.:Fr.Cu. St. Cu. A. St.	3 10 7 10 10	4 4 3 10 10	10 9	10 9 10 10 -	9 10 10 10	8 10 0 0	d înd dd .	: d : n d			≡°  ≡° 	=0  =0 =0	bw to o $a$ : o to om $p$ : om $n$ : omw to bc $a$ : o $p$ : c to bcw $n$ : bcw to o $a$ : o $p$ : omw to o $a$ : o to omw $p$ : omw to o $a$ : o to b $p$ : bw to ofw $n$ :
Cloud Am'nt				5.4	5.3	6.9	6.6	5.5	8 4.6	<u> </u>						2.4 1. 4000
478.	. Richmond (Ke	w Obs.).		1	Γ	T	1	T	1	1	<u> </u>	1	<del></del>			October, 1923.  [23h. 45m. : ofw to odm
1 2 3	St. Ci. : St. Cu. A. St. : St. Cu.	Nb. Ci.St.: St.Cu.: Nb. Nb.	St. : Nb. St. Nb.	10	5	10	10	10		≡ ≡° ≡°	<b>≡</b> ° <b>●</b> °	0	 •	<b>≡º</b> 	<b>■</b> ⁰	12h. 55m14h., 14h. 55m15h. 5m., 2h2h. 10m., 18h. 25m20h. 5m., [20h. 50m. : bm to or 10h. 50m19h. 50m. : om to orm : on :
4 5	Cu.: Nb.: Fr. Nb. Ci.: St.: St. Cu.	St. Cu. A. St. : St. Cu.	St. Cu. St. : St. Cu. ;	8 8	8	9	6 9	3	8		=0	g œ	 ∞	 ≡º		o $a:$ "(gust) Ioh. Iom. : bc to b $p:$ $\equiv^0 \sqcup$ , bc to oz $a:$ oz to c $p:$
6 7 8 9 10	St.: Fr. St. A. Cu.: St. Cu.  A.St.:St.Cu.:Fr.Nb. St.: St. Cu.	St. Cu. A.St.: St.Cu.: Cu. Ci. St.: Cu. Ci.Cu.:A.Cu.:St.Cu. Nb.	A. St. : St. Cu. A.St. : St. : St.Cu. St. St. Cu. Nb.	1	10 10 5 10	10 10 4 7 10	6 - 9 7 10	10	10	;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;		 ≡°  •°	   ≡ ⁰	8	 • ° • ° 	
11 12 13 14	A.Cu.: St.: St.Cu. Nb. A.St.: A.Cu.: Nb.: Fr.Cu. Cu. 	A.St.: St.Cu.: Nb. Nb. Fr. Cu. Cu. Nb. Cu.	A. St.: St. Cu. A.Cu.: Nb.: St.Cu. Fr. Cu. St.: St. Cu. A. St.: Cu.: St.	10 10 8 1	10 10 2 2 0	10 10 8 5 4	10 6 - 4	8 8 3	I	 P₀ ● ≡⁰	 ≡° ≡°	•	• • · · · · · · · · · · · · · · · · · ·	≡° ≡° ≡°	⊪ :ddd	• early: or to o $a$ : o to or ₀ m $p$ : • 4h.3om15h.3om.: omr $a$ : omr to be $p$ : cp ₀ to b $a$ : c to be $p$ : $\triangle n$ : $\square$ , bx to orhp $a$ : bc to bm $p$ : $\bullet \triangle p$ $\square \equiv 0$ : bm to bc  [12h.3om45m.
19	A. Cu.: St. Cu.: St. Fr. Cu.: St. Cu. A.St.:A.Cu.:Ma.Cu:St.Cu Ci.Cu.: St.Cu.: Fr.Cu.	A.St.: Nb.: St.Cu.	St. Cu. St. Cu.: St. A. St.: St. Cu. St.	8 2 10 8	9 8 10 10	9	6 10 10 10	10 10	10	≡° ≡° ∴ ≡°	≡° ≡° •° 	  •°	:: 8 ●	<b>■</b> ° 8 <b>■</b> °	≡° ≡° ≡° ∷	
20 21	A. St. Nb.	Ci.:Ci.St.:Cu.:Fr.Cu. A.St.:Nb.:St.Cu.	Ci. St. : St. Cu.  A. Cu. : Nb.	10	10	10	_	9		1	≡0	•	<del></del>	•	 =°	orq to o $a$ : o to orm $p$ : b to oq $a$ : oqr to bc $p$ : $\bullet$ ² 13h. 40m.,
22 23 24	Ci.: Ci.Cu.: St.Cu.  A.Cu.: St.: Fr.St. Ci.St.: St.: St.Cu.	Fr. Cu. : St. Cu.  A. St. : Fr. Nb.  Cu.  St. Cu. : Cu. Nb.	Fr. Cu. St. Cu. St. Cu. Nb.: St. Cu.	10 9 1	5 10 <1 1		5 10 4	3	OI	 ≡°		•		 ≡º ●	= :d ::	ou to or $a$ : orq to $b \not p$ : $(0 \text{ gust}) 13h.45^{\text{m}}$ ou to or $a$ : orq to $b \not p$ : $(0 \text{ gust}) 23h. 30\text{m}$ . $(0 \text{ p}) 6h. \& 7h. 5 \text{ m}$ , omp to $b a$ : be to $b \not p$ b to orp $a$ : be to or $a$ : $(0 \text{ gust}) 6h$ .
25 26	Fr. St.  Nb. A.St.: Nb.: St.Cu.	Ci.: St. Cu.: Nb. A.Cu.:A.St.:St.Cu.	Cu. A. Cu. : Cu.	10	9	9	5 4 7	0 2	2	•				≡° 		18h. 10m20m. [6h.45m., orm to be 2 ▲ 6h. 40m., ● 6h7h.20m., ↓ (gust, ● 3h9h. & 11h.15m40m., oqr to 0 a
27 28 29 30	A.St.: St.Cu.: St. Ci.: St. Cu. St. Cu.	Ci.: Cu.: Cu.Nb. St. Cu. St. Cu.	Ci.St.: Cu.: Cu.Nb. St. St. Cu.	8 7	7 7 10	7 9	9	8 10	9	Б	≡° ≡°		— 	≡° 	 ≡º	[o to b $p$ ] c to bcm $a$ : c to bc $p$ : $\bullet$ p 11h. 10m. $\bullet$ , c to o: $\bullet$ p ₀ 11h. 40m. o: $\bullet$ 22h. 20m24h.
31 Mean	St. · St. Cu.	Cu.		9	2	3	4			=0	<u></u>			=0	=_	$\bullet$ oh3h.4om.; om to b $a$ : b to bcm $p$ : $\equiv 1$
Cloud Am'nt				7.3	7.3	8.5	7:7	77.	1 5⋅6							
Day.	7 h	13h	18ь	7h	9h	131	15	ь 18	3h 211	7h	9h	13h	15h	18h	21h	Remarks.
		Cloud Forms.				oud . All F						Wea	ather.			
	<u> </u>									<del></del>						

		Cloud Forms.					Amo					Wea	ther.			
Day.	7h	13h	18h	7h	9h	131	151	18	3h 21 h	7h	9h	13h	15h	18h	21h	Remarks.
1 2 3 4 5	A. St. : St. : St. Cu. St. St. Cu.  St. Cu.	St. A. Cu. St. Cu. Cu. : Fr. Cu. A. St. : St. Cu.	St. St. Cu. St. Cu.  St. Nb.	0 10 10	10 10 0 0	10 <1 10 4 10		10 0 9 0 10	0	≡ ≡ : d	= = :::	8 : : : 8	<b>≡</b> ° 8 .:.	≡° ≡°  •	≡° ≡°  ≡°	[cf & om $\equiv$ till 14h.: $\bullet$ 9h.25m12h.1om.: ofw to $\equiv$ till 10h., ofw $a$ : bz to bm $p$ : bmw $n$ : bmw to 0 $a$ : 0 to od $p$ : b $n$ : b to bey $a$ : bcy $p$ : b to bw $n$ : bw to om: $\bullet$ 17h. 55m19h. 50m.
6 7 8 9 10	Ci. : St.  St. St. St. Cu.	Ci.: Cu. Cu.  St. St. Cu.	 A. Cu. : St. Cu. St. 	7 o 10 1 3	6 0 10 10	4 4 0 5 8	7 6 8 10 5	0 0 3 10 0	10 10			8 8 : 🖺 8	8 8 8 8 8	≡° ≡° ≡° ≡	≡° ≡ • ≡° 	om to bef $a$ : bef to bm $p$ : bmx $n$ : $\square$ , bmx to bez $a & p$ : bfx $n$ : $[                                   $
11 12 13 14 15	St. Cu. St. A. Cu. : St. Cu. A. St. : St. Cu. St. Cu.	Ci. Ci. A. St. Fr. Cu. A. St. : Nb.	St. A. St. Nb.: St.  Fr. Cu.	<1 10 7 10 <1	0 7 10 0	1 9 10 2 10	8 10 2 6	8 5 10 0	0 0	]	⊒ :: ::°	∞ ≡°  ≡°	 =0  	≡° ≡° •° ····	≡ ≡° •° ···	□, bz $a$ : bz to cmx $p$ : $\equiv n$ : $V \equiv \text{early}$ : ofx to cfx $a$ : om to bcm $p$ :  czm to oq $a$ : oq to oqd 0 p $\longrightarrow$ (gusts) $p \in n$ : $\bullet$ oh4h.: or to b $a$ : b $p \in n$ : $[\bullet n$ : $\bullet$ , b to ormq $a$ : Line $[\bullet n]$ (gusts) $[\bullet n]$ (gusts) $[\bullet n]$
16 17 18 19 20	St. Cu. : St. St. : St. Cu. : A. St. : St. Cu. A. Cu. : St. Cu. St. Cu.	A. Cu. : Cu. Fr. Cu. Cu. Ci. : St. Cu. A. Cu. : St. Cu.	Ci. Ci.St.:St.Cu.:Nb.  St. Cu.	1 10 10 5 1	10 6 0 6	4 3 <1 9 8	1 4 - 8 6	0 1 8 0 8	6 0	: 🖺 🗓 🕽 🕽	בבנ:	 8 8 ≡°	 ⊗ ≡⁰	 =0 =0 =0	:d ]	b to o $a$ : b to bc $p$ :  • 5h.2om6h., or to b $a$ : b to bc $p$ :  • $p_0$ 17h.45m.  • $p_0$ bm to oz $p_0$ : oz to bm $p_0$ : bmx $p_0$ :  • $p_0$ to bm $p_0$ : bmx $p_0$ :
21 22 23 24 25	St.: St. Cu. St. St. Cu. St. Cu. St. Cu. St. Cu.	Ci. St. Cu. St.: Nb. A. Cu. St. St.	Ci. St. A. Cu. : St. Cu. St. Cu. St. St. St.	10 9 10	10 10 10 10	9 10 9 10	6 10 4 10	6 10 10	4 10 10	≡° ≡° ⊒° ≡°	<b>■° ■ ■ ■ ■ ■ ■ ■</b>	=0 ●0 =0 =0 =	≡ ⁰ ≡ ⁰ ≡ ⁰ −	≡° ≡° ≡° ≡°	≡° □ = ° ≡ = =	om $a$ : om to bcm $p$ : $\oplus$ 15h. $\bigcup$ 18h. $\bigcup$ n: $\oplus$ 3h. $\neg$ 4h.: om to omd $a$ : omd to bcm $p$ : $\bigcup$ , om $a$ : om to bcm $p$ : om $a & p$ : $\bigoplus$ $p$ : $\bigcap$ $p$ : of $p$ :
26 27 28 29 30	St. St. St. : Fr: St. St. Cu. St.	St. St. St.: Fr. St. St. Cu. 	St.  Nb. St. Cu. 	10 10 10	10 10	0 10 10	8 10	10 10 0	10 10	= = = 0 = 0 = 0	≡ ≡ ≡° ≡°	= = =0 =0 =0	≡ ≡ ≡° ≡	≡ ≡° ≡° ≡	≡ ≡° ::: ⊔	□: ofxg 13h. □ ofx a: ofx to bmx p: om n: om ● * 16h21h. 30m. omd₀ 12h. □, omx to bm: bm to bfx p: □ n:
Mean Cloud Am'nt				7.1	7.5	6.7	7.2	5.	2 5.4							
480.	Richmond (Ke	w Obs.).														December, 1923.
1 2 3 4. 5	A.Cu.:A.St.:St.Cu. A. St. : Nb. St. A. St. : Cu. Nb. St. Cu.	A.Cu.:St.:Fr.St. Ci. St.: Cu. St. Cu.: Nb. A. Cu.: St.	A. St. St. Cu.  A. Cu. St.	10			0 9	1	0	] 🍧 🖩 🗨 ]	]	≡° ≡° ≡° ≡°	≡° 8	P ₀ ≡ ⁰ ≡ ≡ ⁰	 = = =0 =0	[& 18h.] $\bullet$ , bmx to om $a$ : om to bcm $p$ : $\bullet$ 17h.15m. $\bullet$ early: or to bcm $a$ : bcm to bm $p$ : $\equiv \sqcup n$ : $\equiv \sqcup$ , bfx to bm $a \Leftrightarrow p$ : $\bullet$ early: orm to om $a$ : om to bm $p$ : $\bullet$ 15h. $\sqcup$ , om to of $a \Leftrightarrow p$ :
6 7 8 9	St. St. Å. St. : St. Cu. St. Cu. A. St.	Fr. Cu. A. St. A. St. Ci. St. A. St.	St. St.: Fr. St.  St.	10 10 9 1	10 9 0	2 10 10 3 10		10 0 0 10	10 10	<b>⊪</b> :: ] ]	<u>  </u>	≡ ⁰ ≡ ⁰ ≡ ⁰ ≡ ⁰	≡° •° ≡° ≡°	≡ ●° ≡° :	≡ • 0 ≡ 0 ≡ 0 ≡ 0	om to bm $a$ : bm to of $p$ : $\square \equiv n$ : $\square$ , of to om $a$ : om to omr $p \otimes n$ : $\square$ early: o to om $a$ : om to bm $p$ : $\equiv$ 19h. $\square$ , bmx to bm $a \otimes p$ : bfx $n$ : $\square$ , bmx to om $a$ : om to odm $p$ :
11 12 13 14 15	Nb. A. St.: St. Cu. St.: St. Cu. Ci.: Ci. St.: St. St. Cu.	St. St.: St. Cu. Ci.St.:A.St.:St.Cu. Ci. Ci.: Ci. Cu.	St. St.: St. Cu. St. Nb. A. St.: Fr. St.	10 10 9 3 6	10 8 10 4	10 10 10 8 6	7 10 10 10	10 10 10 7 0	10	≡°d₀ ≡° d₀ <b>J</b>	≡° ≡° ⊒° 1	$ \begin{array}{c}                                     $	8 = 0 = 0 = 0	≡° d₀ ≡° ≡° ≡°	≡° ≡° ∷ ≡°	• 0 7h., omr ₀ to om $a$ : om to cm $p$ : $d_{0}$ $n$ : • 0 early: omr ₀ to om $a$ : om $p$ $& n$ : omd to om $a$ : omr ₀ to om $p$ :  • 1 bmx to of $a$ : cf to om $p$ : b to bcz $a$ : bcz to bm $p$ : 1 1 1
16 17 18 19 20	St. Cu. St. Cu. Ci. Cu. : St. Cu. St. : St. Cu. St.	Ci,St. : A.Cu. : St.Cu. St. Cu. St. Cu. St. Cu. St. Cu. St. Cu.	St. Cu. St. : St. Cu. St. Cu. Fr. Cu. : St. Cu. Fr. Cu.	2 9	3 10 1 6	5 10 9 10 9	- 10 8 9 0	1 10 10 6 0	5 1 0	≡° ≡° ∷·	≡° ≡° ∷ ≡°	≡° 8 8	= 8 8	≡° ≡° ≡° ∞		bmx to cm $a$ : bcm to omr ₀ $p$ : omd ₀ to cm $a$ : om to cm $p$ : b to o $a$ : o to cm $p$ : b to om $n$ : om to bcm $a$ : oz to bcm $p$ : $\bigstar$ 16h16h.55m $\bigstar$ $p_0$ 5h. 3om. $\textcircled{\Xi}$ : b to o $a$ : oz to bz $p$ :
21 22 23 24 25	St. Cu. Nb. St. Cu. : Fr. Cu. A. St. : Nb. St.	Nb. St. Cu.: Nb. Fr. Cu. Nb. St. Cu.: St.	Nb. St. Nb. A. St. : St. Cu. A. Cu. : A. St. Nb.	10 3	2	10 1 10 9	-	10 10 2 4 10	IO	≡° ≡ .:. •° ≡°	≡° ≡ ∷ ≡	* =° =° =°	<b>*</b> ≡° ≡°	 ≅ ₀ <b>*</b>	*°  ≡° •°	b to oms $a$ : oms to ofs $p$ : $\equiv$ after $\cong$ : of to om $a \in p$ : b to bm $a$ : bm to b $p$ : b to or ₀ m $a$ : om to bc $p$ : bm to of $a$ : or ₀ $p$ : om $n$ :
26 27 28 29 30	St. Cu. St. : St. Cu. Nb.  St.	St. Cu.: Nb. St. Ci.St.:St.Cu.:Nb. Ci. Cu.: A. Cu. St.	St. Cu.: Nb. St. St. High St. Cu. Nb.	10 0	10 10 6	10 10 10 6 10	9	10 10 10 10	10 10	$ \begin{array}{c}                                     $	=0 =0 =0 ==	≡° ≡° ≡° ≡°	≡° ≡° ≡°	≡ ⁰ ≡ ⁰ ≡ ≡ ⁰	≡0 ≡0 ≡0 ≡0	om to omd ₀ $a:$ om $p:$ $n:$ [omr $n:$ $E:$ early: omrs to om $a:$ om $p:$ om to ompq to omr ₀ $a:$ om to omr $p:$ om to bm $n:$ bf to om $a:$ bc to om $p:$ $n:$ omr to om & ofr $a:$ ofr to omr $p:$ om $n:$
Mean Cloud Am'nt	St.	Nb.	St. Nb.	-			1	-	10 9 6·4	_ <u>=</u> 0	_≡⁰	<u>=</u> 0	=	=	=_	om $a$ : omd $p$ : $\bullet$ $n$ :
Ī	7h	13h	18h	7h	9h	13h	15h	18	h21h	7h	9 <b>h</b>	13h	15h	18h	21h	Domesto
Day.		Cloud Forms.	. (				Amo		t		•	Wea	ther.	<u> </u>	-	Remarks.

OF AIR-EARTH CURRENT.

48	1. I	Richm	ond (I	Kew C	bser	vatory	<u>).                                    </u>																1	923.
		JAN	VUARY.			FEB	RUARY				ARCH.				PRIL.		<u> </u>		MAY.				UNE.	
DAY	Char- acter.			harge per	Char		- 00	Charge pe × 10 ¹⁶ .	Char acter	Air- Earth Curren		harge per × 1016.	Char- acter		1 00 1	harge per × 1016.	Char- acter.		۱ ۵۵ ۱	harge per × 1016.	Char- acter	Air- Earth Current	۱ ۵۵ ۱	harge pe < 1016.
	acter.	× 1016	L/	<u> </u>	acter	× 1010	L)	<u> </u>	acter	× 1016		<u> </u>	lacter	× 1016	+.	<u> 1</u>	1	$\times$ 10 ¹⁶ .	+.	1		× 1016	1 +.	<u> </u>
		Amp/ cm ³ .	Cou	lomb.		Amp/ cm ² .	Cou	lomb.		Amp/ cm ² .	1	lomb.	İ	cm ² .	Coul	lomb.	ļ	Amp/ cm ³ .	1	lomb.		Amp/ cm ³ .	Coul	lomb.
I 2	I	0.47	0.74	0.27	0			:::	1	0.86	0.94	0.45	0				0	1.00	0.37	0.38	0	o·74 		
3	I	0.69	0.21	0.25	0				I				0	0.00	0.29	0.27	0	I·27	0.94	0.45	I	1.02	0.52	0.23
5	2				0	0.23	0.32	0.27	1				1				1				1	1.41	0.20	0.08
6	0				I	1.27	0.25	0.34	I	0.42	0.32	0.10	I	0.49	0.47	0.31	0 I	 0·94	 o∙58	0.37	0	 o·66	0.06	0.45
8	I				2 2	0.47	0.29	0.54	I	o·88	0.45	0.34	1	 o·86		0.27	0	o·88	0.41	0.27	0	0.67	0.63	0.80
10	0	1.05	0.44	0.18	0 2	0.40	0.25	0.12	I	0.70	0.72	0.53	0	1.10	0.35	0.51	I	0.29	0.31	0.14	ő	•••		
11	I	0.62	0.39	0.34	I				0		•••		2				2		•••		0	o·88	0.31	0.45
12	0	0.79	0.36	0.14	I	0.32	0·27 0·83	0.21	2	0.75	•••		2 I	o·87	o·76	0.45	2 I				0	0·30 0·59	0.41	1.04
14	0	)   0·58	0.43	0.29	0	0.77	0.29	0.00	0	0·75 0·45	0.41 0.41	0.39	I				1 2	o·39	0.34	0.25	0	0.42	•••	
16	1	0.48	0.51	0.23	1	0.30	0.52	0.39	0	0.31	0.49	0.43	0	0.46	0.33	0.41	1				1			
17	0	1.63	0.37	0.43	I 2				0				0	0.81	0·29 0·35	0.29	I O	0.30			I O	 0·45	 0·12	0.09
19	ı	0.43			1	0·60 0·81	0.53	0.36	0 I	0·78 0·23	0·37 0·67	0·34 0·59	0	0·76 1·07	0.14	0.12	0				0	0.50	 0·49	0.34
20	I				°	_	}	0.55		-	•		0				0		•••		0	0.94	0.86	0.57
21	0	o·46	0.25	0.31	2 2	0.69	0.21	0.49	0	0·44 0·46	0.32	o·54 o·37	1				1	o·56	o· 58	o·35	0	1.18	0.21	0.14
23 24	0	0.40	o·79 	0.21	1 2	o·77	0.31	0.06	0		•••		O	0.28	0.32	0.28	0	0.91	o·51	0.18	0	•••		•••
25	0	0.60	0.31	0.21	1		•••		0	•••	•••		2	•••	•••	•••	I	•••	0.65	0.98	0		•••	•••
26 27	0	0.99	0.29	0.38	I 2				I 2	1.95	 0·92	 0·43	2 0	 0·54	 o∙36	 0·25	O I		•••		I 0	o·83 o·23	 0·12	0·13
28 29	0 I					1.52	o·47 	o· 18	1 2	1.17	o·70 o·38	o·68 o·27	I				2 . I	0.65	0.41	0.34	0	o·57 o·83	0.20	0.25
30	o	0.23	0.16	0.10					0				I		•••		0	0.65	0.31	0.11	٥		•••	•••
31	0	0.99	0.45	o·35				•••	I							•••	0	1 · 14	0.27	0.11		•••		
Mean	0.52	0.73	0.43	0.31	1.07	0.72	0.40	0.32	o·87	0.77	0.55	0.43	o·67	o·8o	0.39	0.30	0.71	0.78	0.47	0.31	0.30	0.74	0.44	0.36
No.of Days	31	17	15	15	28	14	13	13	31	15	15	15	30	14	13	13	31	15	13	13	30	18	14	14
used.	• 1						1			}								I						
					<u>'</u>								<u>'</u>			<u> </u>	!				''		ZVORD.	
DAV			JLY.				GUST.	arge per		Air-	EMBER.	harge per			OBER.	narge per	G.		EMBER.	harge per	G:		EMBER.	arge pe
DAY.	Char-acter.	Air- Earth Current	Ionic Ch		Char- acter.	Air- Earth Current	Ionic Ch	narge per	Char- acter.		Ionic Cl		Char- acter.	Air- Earth	Ionic Ch	narge per	Char- acter.	Air- Earth	Ionic Cl		Char- acter.		Ionic Cl	narge per
DAY.		Air- Earth Current × 1018.	Ionic Ch	1	Char- acter.	Air- Earth Current × 10 ¹⁸ .	Ionic Ch	I –.	Char- acter.	Air- Earth Current	Ionic Cl	1		Air- Earth Current	Ionic Ch		Char- acter.	Air- Earth Current	Ionic Cl cc. × +.	. 10	Char- acter.	Air- Earth Current	Ionic Cl	1014.
	acter.	Air- Earth Current × 10 ¹⁸ . Amp/ cm ² .	Ionic Ch cc. × +. Could	omb.	acter.	Air- Earth Current × 10 ¹⁶ . Amp/ cm ³ .	Ionic Ch cc. × +. Could	omb.	acter.	Air- Earth Current × 10 ¹⁶ . Amp/ cm ² .	Ionic Cl cc. × +. Could	omb.	acter.	Air- Earth Current × 10 ¹⁶ . Amp/ cm ³ .	Ionic Ch cc. × +. Could	omb.	acter.	Air- Earth Current × 10 ¹⁶ . Amp/ cm ² .	Ionic Cl cc. × +. Could	omb.	acter.	Air- Earth Current × 101°. Amp/ cm².	Ionic Ch cc. × +. Could	omb.
	O O	Air- Earth Current × 1015. Amp/ cm ² . 	Could	omb.	I O I	Air- Earth Current × 10 ¹⁸ .	Ionic Ch cc. × +. Could I·2I 	omb. 0·68	I O I	Air- Earth Current × 10 ¹⁶ . Amp/ cm ² .  0·72	Ionic Cl cc. × +. Could 	omb.	I I 2	Air- Earth Current × 10 ¹⁶ . Amp/ cm ² . 	Ionic Ch cc. × +. Could	omb.	I O O	Air- Earth Current × 10 ¹⁸ . Amp/ cm ² .  0.62	Ionic Cl cc. × +. Could  0·32	omb.	O I I	Air-Earth Current × 10 ¹⁶ . Amp/ cm ² . 	Could	omb.
I 2	o o	Air- Earth Current × 10 ¹⁵ . Amp/ cm ³ . 	Ionic Ch cc. × +. Could	omb.	I O	Air- Earth Current × 10 ¹⁶ . Amp/ cm ³ . I·13	Ionic Ch cc. × +. Could I·2I	omb.	I O	Air- Earth Current × 10 ¹⁶ . Amp/ cm ³ .	Ionic Cl cc. × +. Could	omb.	acter.	Air- Earth Current × 10 ¹⁶ . Amp/ cm ³ .	Ionic Ch cc. × +. Could	omb.	acter.	Air- Earth Current × 10 ¹⁶ . Amp/ cm ³ . 	Ionic Cl cc. × +. Could 	omb.	o I	Air- Earth Current × 101s. Amp/ cm ³ .	Ionic Ch cc. × +. Could	omb.
1 2 3 4	o o o	Air- Earth Current × 1011. Amp/ cm ² .  0·70  I·I7	Could 0.34 0.68	omb.  o·68	I O I O O	Air- Earth Current × 10 ¹⁸ . Amp/ cm ³ . I·13  O·44	Ionic Ch cc. x +. Could I·2I  O·74	omb. 0·68  1·17	I O I I O O	Air-Earth Current × 10 ¹⁴ .  Amp/cm ³ 0·72 0·77	Ionic Cl cc. x +. Could  0·54  0·49	omb	I I 2 O O	Air- Earth Current × 10 ¹⁸ . Amp/ cm ² .  I·32	Could	omb.	I O O I	Air-Earth Current × 10 ¹⁶ .  Amp/cm ³ 0.62 1.28	Ionic Cl   cc. x   +.     Could     o·32     o·31   o·40	omb. o· 10 ··· o· 27 o· 06	O I I 2 I I	Air-Earth Current × 10 ¹⁸ . Amp/cm ² o·69 o·34	Could 0.45 0.31	omb.  o·18   o·53
1 2 3 4 5	0 0 0 0	Air- Earth Current × 1015. Amp/ cm2.  0.70  I.17 I.14	Ionic Ch cc. × +. Could  o·34  o·68 o·70	omb.  o·68 o·16	I O I O	Air- Earth Current × 101s.  Amp/ cm².  1 · 13  0 · 44  0 · 58 1 · 29	Ionic Ct cc. x +. Could I·2I  0·74 	omb.  0.68 1.17 0.90 0.45	I O I I O O O O O	Air- Earth Current × 10 ¹⁶ .  Amp/ cm ³ .  0·72	Could 0·54 0·49	omb.	I I I 2 O O	Air- Earth Current × 1014.  Amp/ cm² I · 32 0 · 59	Could 0.23 0.43	omb o. 16 o. 10	I O O I I I I	Air- Earth Current × 1016.  Amp/ cm².  0.62 1.28 0.92 0.84 0.15	Ionic Cl   cc. ×   +.     Could     o· 32     o· 31   o· 40   o· 35 	omb.  o·10   o·27  o·06  o·22  o·21	O I I 2 I I I O	Air- Earth Current × 10 ¹⁴ . Amp/ cm ² .  0·69  0·34 I·24	Could 0.45 0.31	0·18
1 2 3 4 5 6 7	0 0 0 0 0 0 0 I	Air- Earth Current × 1018. Amp/ cm ³ .  1 · 17 1 · 14 1 · 62 	Ionic Ch cc. × +. Could  0·34  0·68 0·70	omb.  o·68 o·16	I O I O O O	Air-Earth Current × 101s. Amp/cm ³ . I·I3  O·44 	Ionic Ct cc. x +. Could I·2I  O·74 	omb. 0.68  1.17  0.90	I O I I O O O	Air-Earth Current × 1014.  Amp/cm² 0·72 0·77 0·88 0·96	Could 0.54 0.49 0.26 0.43	omb	I I 2 O O I	Air- Earth Current × 1014.  Amp/ cm3 I · 32	Could 0·23	omb o.16	I O O I	Air- Earth Current × 101°. Amp/ cm³.  0.62  I.28	Ionic Cl cc. × +. Could  0·32  0·31	omb.  o·10   o·27  o·06  o·22	o I I 2 I I I I I	Air- Earth Current × 1014. Amp/ cm2.  0.69  0.34	Could 0.45 0.31	0·18
1 2 3 4 5 6 7 8	0 0 0 0 0 0 I 0 I	Air- Earth Current × 1015.1  Amp/ cm².  0.70  1.17 1.14  1.62 0.70	Could 0·34 0·68 0·70 0·39 0·65	omb.  o·68 o·16 o·40 	1 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Air-Earth Current × 101s Amp/cm³ 0 · 44 0 · 58 1 · 29 0 · 89	Ionic Ct cc. x +. Could I·2I  O·74  o·92 o·90 o·51	omb. 0·68  1·17  0·90 0·45 0·20	I O I I O O O O O O	Air- Earth Current × 10 ¹⁶ .] Amp/ cm ² 0·72  0·77 0·88 0·96 	Could  0·54 0·49 0·26 0·43 0·41	omb.   0·41  0·39  0·38   0·22	I I 2 O O I I I O O	Air-Earth Current × 1014.  Amp/cm²	Could 0.23 0.43	omb o.16 o.10 o.43	I O O I I I O O O O O O O O O O O O O O	Air-Earth Current × 1018  Amp/cm³ 0.62 1.28 0.92 0.84 0.15 0.37	Ionic Cl   cc. x   +.     Could       0·32       0·31     0·40   0·35       0·12	omb.   0.10   0.27   0.06   0.22   0.21	o i i i o i o o o o o o o o o o o o o o	Air-Earth Current × 10 ¹³ .  Amp/cm ³ .  0·69  0·34  1·24  0·33  0·55	Could C: X + X + X + X + X + X + X + X + X + X	0·53
1 2 3 4 5 6 7 8 9 10	0 0 0 0 0 0 1 0 1 2	Air-Earth Current x 101s.  Amp/cm³ 0·70 1·17 1·14 1·62 0·70 1·19 0·98 0·94	Onic Chec. × +. Could 0·34 0·68 0·70 0·39 0·65 0·35 0·83 0·43	omb.  o·68 o·16 o·40  o·37 o·27	1 0 1 0 0 0 0 0 0 0 0 0	Air-Earth Current × 101s.  Amp/cm3.  1 · 13  0 · 44   0 · 58 1 · 29 0 · 89 0 · 91	Could 1.21 0.74 0.92 0.51 0.52	omb. 0·68  1·17  0·90 0·45 0·20	I O I I O O O O O O O	Air-Earth Current × 101s. Amp/cm² 0·72 0·77 0·88 0·96 1·26	Could 0·54 0·49 0·41	omb.   o·41  o·39  o·38   o·22	I I 2 O O I I I O O	Air-Earth Current × 101s. Amp/cm³ I · 32 0 · 59 0 · 67	Could  Could  0.23   0.43  0.47	omb o·16 o·10 o·43	I O O O O O O O O	Air-Earth Current × 1018.  Amp/cm3 0.62 1.28 0.92 0.84 0.15 0.37 0.37	Onic CI cc. × +.  Could  0·32  0·31  0·40  0·35  0·12	omb.  o·10   o·27  o·06  o·22  o·21   o·12	o I I 2 I I O I O O O O	Air-Earth Current × 10 ³⁴ .  Amp/cm³.   0·69  0·34  I·24  0·33  0·55  0·58	O·31 O·29	0·18 0·53
1 2 3 4 5 6 7 8 9 10 11 12 13 14	0 0 0 0 0 1 0 1 2 0 0 0 0 0 0 0 0	Air-Earth Current x 101s.  Amp/cm³ 0·70 1·17 1·14 1·62 0·70 1·19 0·98 0·94 0·87	Onic Chec. × +. Could 0·34 0·68 0·70 0·39 0·65 0·35 0·83 0·43 1·03	omb o·68 o·16 o·40 o·37 o·27 o·55 o·22 o·80	1 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Air-Earth Current × 1018.  Amp/cm².  1 · 13  0 · 44  0 · 58 1 · 29 0 · 89 0 · 91  0 · 76 0 · 37	Ionic Ct cc. x +- Could 1·21  0·74  0·92 0·90 0·51 0·52	omb. 0·68  1·17  0·90 0·45 0·20 	I O O O O O O	Air-Earth Current × 101s.  Amp/cm² 0·72 0·77 0·88 0·96 1·26 0·79 0·43 1·17 1·92	Could	omb o·41 o·39 o·38 o·22 o·21 o·41	1 1 2 0 0 0 1 1 1 0 0 2	Air-Earth Current × 10 ¹⁸ .  Amp/cm² I · 32 0 · 59 0 · 67	Could	omb o·16 o·10 o·43	I O O I I I O O O O O O O O O O O O O O	Air-Earth Current × 1018  Amp/cm1 0.62 1.28 0.92 0.84 0.15 0.37	Onic Cl cc. × +. Could  0·32  0·31 0·40 0·35 	omb.   0.10   0.27   0.06   0.22   0.21     0.12	o i i i o o o o	Air-Earth Current × 10 ¹³ .  Amp/cm ³ .  0·69  0·34  1·24  0·33  0·55  0·58	O·45 O·31 O·29	0·53
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15	O O O O I O O O O O O O O O O O O O O O	Air-Earth Current × 1011. Amp/cm² 0.70 1.17 1.14 1.62 0.70 1.19 0.98 0.94 0.87	Onic Chec. ×	omb o·68 o·16 o·40 o·37 o·27 o·55 o·22 o·80	1 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Air-Earth Current × 101s.  Amp/cmi.  1·13 0·44 0·58 1·29 0·89 0·91 0·76 0·37 0·59	Could 1.21 0.74 0.92 0.90 0.51 0.52 0.55 0.40 0.37	0.00mb. 0.68 1.17 0.90 0.45 0.20 0.52 0.22	1 0 1 1 0 0 0 0 0 0 0 0 0 0 1 1	Air-Earth Current × 1011.  Amp/cm1 0·72 0·77 0·88 0·96 1·26 0·79 0·43 1·17 1·92	Could	omb o·41 o·39 o·38 o·22 o·21 o·41 o·16 o·49	1 1 2 0 0 1 1 1 0 0 2 0 1	Air-Earth Current × 10 ¹⁸ .  Amp/cm ² .   I · 32   0 · 59  0 · 67   0 · 40	Could	omb o·16 o·10 o·43	1 0 0 0 1 1 1 1 0 0 0 0 0 0 1 1	Air-Earth Current × 1018.  Amp/cm3 0.62 1.28 0.92 0.84 0.15 0.37 0.37 0.52	Onic CC cc. × +.  Could  0·32  0·31  0·40  0·35  0·12  0·55	omb.  o·10   o·27  o·06  o·22  o·21   o·12   o·86	o I I 2 I I O I O O O O O O	Air-Earth Current × 10 ³⁴ .  Amp/cm³.   0·69  0·34  I·24  0·33  0·55  0·58  0·26	O·45 O·31 O·29 O·27	o·18 ··· o·53 ··· o·39 ··· ···
1 2 3 4 4 5 5 6 7 7 8 9 10 11 12 13 14 15 16 17	O O O O I O O O O O O I I I I I I	Air-Earth Current x 101s  Amp/cm³  0·70  1·17  1·14  1·62  0·70  1·19  0·98  0·94  0·87  0·35  0·64	Onic Chec. ×	onb o·68 o·16 o·40 o·37 o·27 o·55 o·22 o·80 o·54	I O I O O O O O O I I O I I	Air-Earth Current x 1011.  Amp/cm1.  1 · 13  0 · 44  0 · 58  1 · 29  0 · 89  0 · 91   0 · 76  0 · 37  0 · 59  0 · 94	Could 1.21 0.74 0.92 0.90 0.51 0.52 0.37 0.94	omb.  o-68  1·17  o-90  o-45  o-20  o-52  o-22  o-76	I	Air-Earth Current × 1014.  Amp/cm² 0·72 0·77 0·88 0·96 1·26 0·79 0·43 1·17 1·92	Could	omb o·41 o·39 o·38 o·22 o·21 o·41 o·16 o·49	I	Air-Earth Current × 10 ¹⁴ .  Amp/ cm ² .   1·32   0·59  0·67   0·40  0·74  0·44	Could	omb o·16 o·10 o·43	I	Air-Earth Current × 1018.  Amp/cm1 0.62 1.28 0.92 0.84 0.15 0.37 0.37 0.52	Onic Cl cc. × +.  Could 0·32 0·31 0·40 0·35 0·12 0·55	omb.  o·10  ···  o·27  o·06  o·22  o·21  ···  o·12  ···  o·86  ···	0 1 1 2 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0	Air-Earth Current × 10 ³⁴ .  Amp/cm³.   0·69  0·34  I·24  0·33  0·555  0·58  0·26	O·45 O·31 O·29 O·27	omb.  o·18   o·53   o·39    o·31
1 2 3 4 5 5 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19	0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	Air-Earth Current × 1011. Amp/cm1  0·70  1·17  1·14  1·62  0·70  1·19  0·98  0·94  0·87   0·35  0·64	Could  Could  0 · 34   0 · 68  0 · 70  0 · 39   0 · 65  0 · 35  0 · 83  0 · 43  1 · 03   0 · 41  0 · 62	omb o·68 o·16 o·40 o·37 o·27 o·55 o·22 o·80 o·54	I	Air-Earth Current × 1018.  Amp/cm².  1 · 13 0 · 44 0 · 58 1 · 29 0 · 89 0 · 91 0 · 76 0 · 37 0 · 59 0 · 94	Ionic Ct cc. x +.  Could 1.21 0.74 0.92 0.90 0.51 0.52 0.555 0.40 0.37	0.00mb. 0.68 1.17 0.90 0.45 0.20 0.52 0.76	1 0 1 1 0 0 0 0 0 0 0 0 1 1 1 0 0 0 1 1 1 1	Air-Earth Current X 1011.  Amp/cm1 0·72 0·77 0·88 0·96 1·26 0·79 0·43 1·17 1·92 2·72 0·93	Could  Could  0·54   0·49  0·26  0·43   0·41  0·41  0·47  0·63    0·50  0·76	omb.   o·41  o·39  o·38   o·22  o·21  o·41  o·16  o·49   o·57  o·72	I	Air-Earth Current × 10 ¹⁸ .  Amp/cm² 1·32 0·59 0·67 0·40 0·74 0·44	Could Ct. X +. Could Ct. X +. Could Ct. X +. Could Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X Ct. X	omb o·16 o·10 o·43 o·25 o·12	I	Air-Earth Current × 1018.  Amp/cm1 0.62 1.28 0.92 0.84 0.15 0.37 0.52 0.79	Onic Cl cc. × +. Could  0·32  0·31 0·40 0·35  0·12 	omb.  o·10  ···  o·27  o·06  o·22  o·21  ···  o·12  ···  o·86  ···  ···	O I I I I I I I I I I I I I I I I I I I	Air-Earth Current × 10 ¹⁴ .  Amp/cm ² .  0·69  0·34  I·24  0·33  0·55  0·58  0·26	O·45 O·31 O·29 O·27	omb.  o·18   o·53   o·39   o·31   o·18
1 2 3 4 4 5 6 7 7 8 9 10 11 12 13 14 15 16 17 18 19 20	O O O O I I O O O O O O O O O O O O O O	Air-Earth Current X 1018.1 Amp/cm² 0·70 1·17 1·14 1·62 0·70 1·19 0·98 0·94 0·87 0·35 0·64 1·09	Onic Checc. × +. Could 0.34 0.68 0.70 0.39 0.65 0.35 0.83 0.43 1.03 0.41 0.62 0.54	omb o.68 o.16 o.40 o.37 o.27 o.55 o.22 o.80 o.54 o.33	I O O O O O O O O I I I O O O	Air-Earth Current X 1011.  Amp/cm1.  1 · 13  0 · 44   0 · 58  1 · 29  0 · 89  0 · 91   0 · 76  0 · 37  0 · 59  0 · 94	Onic Check	omb.    0.68   0.68   1.17     0.90   0.45   0.20     0.52     0.22   0.76	I	Air-Earth Current × 1011.  Amp/cm1.   0.72   0.77  0.88  0.96   1.26  0.79  0.43  1.17  1.92   2.72  0.93  0.38	Could  0·54 0·49 0·26 0·43 0·41 0·41 0·47 0·63 0·50 0·76 0·67	omb.   o·41  o·39  o·38   o·22  o·21  o·41  o·16  o·49   o·57  o·72  o·55	I	Air-Earth Current × 1015.  Amp/cm² I · 32 0 · 59 0 · 67 0 · 40 0 · 74 0 · 44	Could Ct. X +. Could Ct. X +. Could Ct. X +. Could Ct. X +. Could Ct. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +.	omb o·16 o·10 o·43 o·25 o·12 o·20	I	Air-Earth Current × 1018  Amp/cm³  1 · 28  0 · 92  0 · 84  0 · 15  0 · 37   0 · 52   0 · 79   0 · 42  0 · 71	Onic Cl cc. × +. Could  0·32  0·31 0·40 0·35  0·12  0·55  0·55 	omb.  o·10  ···  o·27  o·06  o·22  o·21  ···  o·12  ···  o·86  ···  o·21  o·68	0 1 1 2 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 1 1 0 0 0 1	Air-Earth Current × 10 ¹⁸ .  Amp/cm ¹ .  0·69  0·34  1·24  0·33  0·55  0·58  0·26  0·49  0·41  0·60	O·45 O·31 O·29 O·27 O·35 O·38	0·18 0·53 0·39 0·18 0·39 0·38 0·18
1 2 3 3 4 4 5 5 6 7 7 8 8 9 10 11 12 13 114 15 16 17 18 19 20 21 22	O O O O O O O O O O O O O O O O O O O	Air-Earth Current × 1011. Amp/cm1  0·70  1·17  1·14  1·62  0·70  1·19  0·98  0·94  0·87   0·35  0·64	Could  Could  0 · 34   0 · 68  0 · 70  0 · 39   0 · 65  0 · 35  0 · 83  0 · 43  1 · 03   0 · 41  0 · 62	omb o·68 o·16 o·40 o·37 o·27 o·55 o·22 o·80 o·54	I	Air-Earth Current X 1018.  Amp/cm².  I · 13  0· 44  0· 58 I · 29 0· 89 0· 91  0· 76 0· 37 0· 59 0· 94  0· 93	Ionic Ct   cc. x	0.00mb. 0.68 1.17 0.90 0.45 0.20 0.52 0.76 0.52 1.29	1 0 1 1 0 0 0 0 0 0 0 0 1 1 1 0 0 0 1 1 1 1 1 1 1 1	Air-Earth Current X 1014.  Amp/cm² 0·72 0·77 0·88 0·96 1·26 0·79 0·43 1·17 1·92 2·72 0·93 0·38	Onic Cl cc. x +. Could O · 54 O · 49 O · 26 O · 43 O · 41 O · 41 O · 41 O · 63 O · 50 O · 76 O · 67	omb o·41 o·39 o·38 o·22 o·21 o·16 o·49 o·57 o·72 o·55	I	Air-Earth Current × 10 ¹⁴ . Amp/cm ³ 1·32  0·59 0·67  0·40  0·74 0·44 0·74	Could Ct. X +. Could Ct. X +. Could Ct. X +. Could Ct. X +. Could Ct. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +.	omb.       o.16     o.16     o.10   o.43             o.25   o.12   o.20	O O O I I I O O O O I I I I O O O I I I I I O O O I I I I I O O O I I I I I O O O I I I I I O O O I I I I I I O O O I I I I I I O O O O I I I I I I O O O O I I I I I I O O O O I I I I I I O O O O I I I I I I O O O O I I I I I I I O O O O I I I I I I I I I I I I I I I I I I I I	Air-Earth Current No. 1018  Amp/cm²  0·62  1·28  0·92  0·84  0·15  0·37  0·52  0·79  0·42  0·71  0·73  0·52	Onic Cl Ccc. ×	omb.   o·10   o·27  o·06  o·22  o·21   o·12   o·86   o·21  o·68  o·25	O 1 1 2 1 1 1 O 0 O O O O O O O I I O O O I I I O O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I O I I I O I I O I I I O I I I O I I O I I I O I I O I I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I O I I I O I I O I I O I I O I I O I I O I I O I I O I I I O I I O I I I O I I O I I I O I I O I I O I I I O I I O I I I O I I O I I I O I I O I I I O I I O I I I O I I O I I I O I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I I O I I I O I I I O I I I O I I I I O I I I O I I I O I I I O I I I I O I I I O I I I O I I I O I I I O I I I O I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I O I I I I I O I I I I I O I I I I I O I I I I I O I I I I I O I I I I I I I I I I I I I I I I I I I I	Air-Earth Current × 10 ¹⁸ .  Amp/cm².   0·69  0·34  1·24  0·33  0·55  0·26  0·49  0·41  0·60  0·52	O·45 O·31 O·29 O·35 O·38 O·25	0·18 0·53 0·39 0·18 0·39 0·31 0·18 0·38 0·06 0·32
1 2 3 4 4 5 6 7 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	O O O O O I I O O O O O I I I I O O O O	Air-Earth Current X 1011. Amp/cm1  Amp/cm2  1 · 17 1 · 14  1 · 62 0 · 70 1 · 19  0 · 98 0 · 94 0 · 87 0 · 35 0 · 64 1 · 09	Onic Ch cc. × +. Could  0·34  0·68 0·70 0·39  0·65 0·35 0·43 1·03  0·62  0·54	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	I	Air-Earth Current × 101s.  Amp/cmi.  1 · 13 0 · 44 0 · 58 1 · 29 0 · 89 0 · 91 0 · 76 0 · 37 0 · 59 0 · 94 0 · 93	Ionic Ct	0.52 0.52 0.52 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76	I	Air-Earth Current X 1011.  Amp/cm1 0·72 0·77 0·88 0·96 1·26 0·79 0·43 1·17 1·92 2·72 0·93 0·38 1·48	Could  Could  0·54   0·49  0·26  0·43   0·41  0·41  0·47  0·63    0·50  0·76  0·67	omb.   o·41  o·39  o·38   o·22  o·21  o·41  o·16  o·49   o·57  o·72  o·55   o·51	I	Air-Earth Current × 1015.  Amp/cm² I · 32 0 · 59 0 · 67 0 · 40 0 · 74 0 · 44 0 · 74 0 · 67	O·47 O·36 O·23 O·47 O·36 O·23 O·63	omb o·16 o·10 o·43 o·25 o·12 o·20	I	Air-Earth Current × 1018.  Amp/cm1 0·62 1·28 0·92 0·84 0·15 0·37 0·37 0·52 0·79 0·42 0·71 0·73 0·52 0·54	Onic Cl cc. × +.  Coule 0·32 0·31 0·40 0·35 0·12 0·55 0·76 0·25 0·25	omb.  o·10  o·27  o·06  o·22  o·21   o·12   o·86   o·25  o·39	O 1 1 2 1 1 1 0 0 0 0 0 0 0 0 0 1 1 0 0 0 0	Air-Earth Current × 10 ¹¹ .  Amp/cm ¹ .  0·69  0·34  1·24  0·33  0·55  0·58  0·26  0·49  0·41  0·60  0·52  0·71	O·45 O·45 O·29 O·27 O·35 O·38 O·25	0·18 0·53 0·39 0·31 0·38 0·38 0·38 0·36 0·32
1 2 3 4 4 5 5 6 7 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	O O O O O O O O O O O O O O O O O O O	Air-Earth Current X 1018.  Amp/cm1 0.70 1.17 1.14 1.62 0.70 1.19 0.98 0.94 0.87 0.35 0.64 1.09 0.72	Onic Chec. X	0.54  0.54  0.33 0.55 0.22 0.80  0.33	I O O O O O O O O O O O O O O O O O O O	Air-Earth Current X 1018.  Amp/cm1.  I · 13 0· 44 0· 58 I · 29 0· 89 0· 91 0· 76 0· 37 0· 59 0· 94 0· 93	Could 1 · 21 0 · 74 0 · 92 0 · 90 0 · 51 0 · 52 0 · 55 0 · 40 0 · 37 0 · 94 0 · 23 1 · 62	0.00mb. 0.68 1.17 0.90 0.45 0.20 0.52 0.76 0.52 1.29	I	Air-Earth Current X 1018.  Amp/cm1 0·72 0·77 0·88 0·96 1·26 0·79 0·43 1·17 1·92 2·72 0·93 0·38 1·48 1·48	Onic Cl cc. x +. Could O·54 O·49 O·26 O·43 O·41 O·41 O·41 O·63 O·50 O·76 O·67	omb o·41 o·39 o·38 o·22 o·21 o·41 o·16 o·49 o·57 o·72 o·55 o·51	I	Air-Earth Current × 10 ¹⁴ . Amp/cm ³ 1·32  0·59 0·67  0·40 0·74 0·44 0·74 0·67 1·36	O·43 O·47 O·36 O·23 O·63	omb o·16 o·10 o·43 o·25 o·12 o·20 o·56	O O O O O O O O O O O O O O O O O O O	Air-Earth Current No. 1018.  Amp/cm² 0·62 1·28 0·92 0·84 0·15 0·37 0·52 0·42 0·71 0·73 0·52 0·54	Onic Cl Ccc. ×	omb.  o·10  o·27  o·06  o·22  o·21   o·12   o·86   o·25   o·39	O 1 1 2 1 1 1 0 0 1 1 0 0 0 0 0 0 1 1 1 1	Air-Earth Current × 10 ¹⁴ ,     0·69     0·34   1·24     0·33   0·55   0·56     0·49   0·41   0·60   0·52     0·71	O·29 O·35 O·38 O·25	0·18 0·53 0·31 0·18 0·38 0·06 0·32 0·29
1 2 3 4 4 5 6 7 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	O O O O O I I O O O O O I I I I O O O O	Air-Earth Current X 1018.1 Amp/cm² 0·70 1·17 1·14 1·62 0·70 1·19 0·98 0·94 0·87 0·35 0·64 1·09 1·09	Onic Chec. X +. Could 0.34 0.68 0.70 0.39 0.65 0.35 0.83 0.43 1.03 0.41 0.62 0.54 0.66	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	I	Air-Earth Current × 101s.  Amp/cmi.  1 · 13 0 · 44 0 · 58 1 · 29 0 · 89 0 · 91 0 · 76 0 · 37 0 · 59 0 · 94 0 · 93	Ionic Ct	0.52 0.52 0.52 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76	I	Air-Earth Current X 1011.  Amp/cm1 0·72 0·77 0·88 0·96 1·26 0·79 0·43 1·17 1·92 2·72 0·93 0·38 1·48	Could  Could  0·54   0·49  0·26  0·43   0·41  0·41  0·47  0·63    0·50  0·76  0·67	omb.   o·41  o·39  o·38   o·22  o·21  o·41  o·16  o·49   o·57  o·72  o·55   o·51	I	Air-Earth Current × 1015.  Amp/cm² I · 32 0 · 59 0 · 67 0 · 40 0 · 74 0 · 44 0 · 74 0 · 67	O·47 O·36 O·23 O·47 O·36 O·23 O·63	omb.   o·16   o·10  o·43    o·25  o·12   o·56  o·12	I	Air-Earth Current × 1018.  Amp/cm1 0·62 1·28 0·92 0·84 0·15 0·37 0·37 0·52 0·79 0·42 0·71 0·73 0·52 0·54 0·29 0·39	Onic Cl cc. × +.  Coule 0·32 0·31 0·40 0·35 0·12 0·55 0·76 0·25 0·25 0·70	omb.  o·10  o·27  o·06  o·22  o·21   o·12   o·86   o·39   o·59	O	Air-Earth Current × 10 ¹¹ .  Amp/cm ¹ .  0·69  0·34  1·24  0·33  0·55  0·58  0·26  0·49  0·41  0·60  0·52  0·71  0·20	O·45 O·45 O·29 O·27 O·35 O·38 O·25 O·31 O·35 O·38 O·25	0·18 0·53 0·39 0·31 0·18 0·38 0·32 0·29 0·29 0·29
1 2 3 4 4 5 6 7 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	O O O O O I I O O O O O I I I I I O O O O O O O O O O O O O O O O O O O O	Air-Earth Current × 1018.  Amp/cm1 0·70 1·17 1·14 1·62 0·70 1·19 0·98 0·94 0·87 0·35 0·64 1·09 1·09 0·72 0·51	Onic Chec. X +. Could 0·34 0·68 0·70 0·39 0·65 0·35 0·83 0·43 1·03 0·41 0·62 0·54 0·66 0·83	0.55 0.22 0.80 0.16 0.40  0.37 0.27 0.55 0.22 0.80  0.54  0.61	I	Air-Earth Current × 1018.  Amp/cm².  1 · 13 0 · 44 0 · 58 1 · 29 0 · 89 0 · 91 0 · 76 0 · 37 0 · 59 0 · 94 0 · 93	Ionic Ct   cc. x	0.00mb. 0.68 1.17 0.90 0.45 0.20 0.52 0.76 0.52 1.29	1 0 1 1 0 0 0 0 0 0 0 0 0 1 1 1 1 1 1 1	Air-Earth Current X 1011.  Amp/cm1 0·72 0·77 0·88 0·96 1·26 0·79 0·43 1·17 1·92 2·72 0·93 0·38 1·48 0·85	Could  Could  0·54  0·49  0·26  0·43   0·41  0·41  0·47  0·63   0·50  0·76  0·67    0·77	omb.   o·41  o·39  o·38   o·22  o·21  o·41  o·16  o·49   o·57  o·72  o·55   o·51   o·40	I	Air-Earth Current X 1014.  Amp/cm² I · 32 0 · 59 0 · 67 0 · 40 0 · 74 0 · 44 0 · 74 0 · 67 I · 36 I · 26 I · 31	O·163  O·163  O·163  O·163  O·163	omb.   o·16   o·10  o·43    o·25  o·12  o·20    o·56  o·12   o·23	I	Air-Earth Current No. 1018.  Amp/cm² I · 28 0 · 92 0 · 84 0 · 15 0 · 37 0 · 52 0 · 79 0 · 42 0 · 71 0 · 73 0 · 52 0 · 74 0 · 73 0 · 52 0 · 74 0 · 74 0 · 74 0 · 74 0 · 74 0 · 74 0 · 74	Onic Cl Ccc. ×  Could Ccc. ×  +.  Could Ccc. ×   O · 32   O · 31  O · 40  O · 35   O · 12   O · 55   O · 76  O · 25   O · 25   O · 70   O · 70   O · 70   O · 70	omb.  o·10  o·27  o·06  o·22  o·21   o·12   o·86   o·25   o·59   o·10	O 1 1 1 2 1 1 1 0 0 0 0 0 0 0 0 1 1 1 1 1	Air-Earth Current × 10 ¹⁴ ,     0·69     0·34   1·24     0·33   0·55   0·58     0·49   0·41   0·60   0·52     0·71       0·20   0·32	O·45 O·29 O·35 O·38 O·25 O·31 O·45 O·35 O·38 O·25 O·37	0·18 0·53 0·39 0·18 0·38 0·38 0·36 0·32 0·29 0·25
1 2 3 4 4 5 6 7 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	O O O O O I I I I O O O I I I I I O O O I I I I I I O O O I I I I I I O O O I I I I I I O O O I I I I I I I O O O I I I I I I I O O O I I I I I I I O O O I I I I I I I I I I I I I I I I I I I I	Air-Earth Current X 1018.1 Amp/cm² 0·70 1·17 1·14 1·62 0·70 1·19 0·98 0·94 0·87 0·35 0·64 1·09 0·72 0·51	Onic Chec. X +. Could 0.34 0.68 0.70 0.39 0.65 0.35 0.83 0.43 1.03 0.41 0.62 0.54 0.66 0.83 0.57	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	I O O O O O O O O I I I O O O O I I I 2 O O O O	Air-Earth Current × 101s.  Amp/cmi.  1 · 13 0 · 44 0 · 58 1 · 29 0 · 89 0 · 91 0 · 76 0 · 37 0 · 59 0 · 94 0 · 93	Ionic Check	0.52 0.76 0.52 1.22 0.76 0.52 0.68 0.68 0.76 0.68 0.76 0.76 0.76	I	Air-Earth Current X 1011.  Amp/cm1.   0.77  0.88  0.96   1.26  0.79  0.43  1.17  1.92   2.72  0.93  0.38   1.48   0.85  0.82	Could  Could  0·54   0·49  0·41  0·41  0·41  0·63    0·50  0·76  0·67   0·67	omb.   o·41  o·39  o·38   o·22  o·21  o·41  o·16  o·49   o·57  o·72  o·55   o·51   o·40  o·45	I	Air-Earth Current × 10 ¹⁴ . Amp/cm ² 1·32  0·59 0·67  0·40 0·74 0·44 0·74 0·67 1·36 1·26	O· 43 O· 47 O· 36 O· 23 O· 63 O· 56	omb.   o·16   o·10  o·43    o·25  o·12  o·20   o·56  o·12    o·56	I	Air-Earth Current (1014).  Amp/cm1 1·28 0·62 0·84 0·15 0·37 0·52 0·79 0·42 0·71 0·73 0·52 0·54 0·29 0·39 0.17	Onic Cl cc. × +.  Could 0·32 0·31 0·40 0·35 0·12 0·55 0·76 0·25 0·25 0·70 0·61	omb.     0.10     0.27   0.06   0.22   0.21     0.12     0.86     0.25     0.39     0.59	O	Air-Earth Current × 1011.  Amp/cm1.  0.69 0.34  1.24 0.33  0.55 0.58 0.26 0.49 0.41 0.60 0.52 0.71 0.20 0.32	O·45 O·29 O·35 O·38 O·25 O·31 O·45	0·18 0·53 0·39 0·31 0·18 0·32 0·29 0·25
1 2 3 4 4 5 5 6 7 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 27 28 29	O O O O O O O O O O O O O O O O O O O	Air-Earth Current X 1011. Amp/cm1  Amp/cm2  1 · 17  1 · 14  1 · 62   0 · 70  1 · 19  0 · 98  0 · 94  0 · 87   1 · 09   1 · 09   1 · 09   1 · 09	Onic Check	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	I O O O O O O O O O O O O O O O O O O O	Air-Earth Current X 1018.  Amp/cm².  I · 13  0 · 44  0 · 58 I · 29 0 · 89 0 · 91  0 · 76 0 · 37 0 · 59  0 · 94	Onic Ct cc. x +. Could 1.21 O.74 O.92 O.90 O.51 O.55 O.40 O.37 O.94	omb.  o-68  1·17  o-90  o-45  o-20  o-52  o-76   o-52  1·29  o-84	I	Air-Earth Current X 1014.  Amp/cm² 0·72 0·77 0·88 0·96 1·26 0·79 0·43 1·17 1·92 2·72 0·93 0·38 1·48 0·85 0·82	Could		I	Air-Earth Current x 10 ¹⁴ . Amp/cm ² 1·32  0·59 0·67  0·40 0·74 0·44 0·74  1·26  1·26  1·31 0·42	O·163  O·163  O·163  O·163  O·163		I	Air-Earth Current × 1014.  Amp/cm² 1 · 28 0 · 92 0 · 84 0 · 15 0 · 37 0 · 52 0 · 79 0 · 79 0 · 73 0 · 52 0 · 71 0 · 73 0 · 52 0 · 71 0 · 73 0 · 52 0 · 74 0 · 73 0 · 52 0 · 74 0 · 29 0 · 39 0 · 17 0 · 46 0 · 39	Onic Cl Ccc. ×  Could Ccc. ×	omb.  o·10  o·27  o·06  o·22  o·21   o·12   o·86   o·25   o·59   o·10	O 1 1 1 2 1 1 1 0 0 0 0 0 0 0 0 0 1 1 1 1	Air-Earth Current × 10 ¹⁴ ,     0·69     0·34   1·24     0·55   0·55     0·49   0·41   0·60   0·52       0·71       0·20   0·32	O:29 O:27 O:35 O:38 O:25 O:31 O:45 O:35 O:38 O:25	0·18 0·53 0·39 0·18 0·38 0·06 0·32 0·29 0·25 0·25
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	octer.  occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording to the content occording toc	Air-Earth Current X 1018.  Amp/cm1 0.70 1.17 1.14 1.62 0.70 1.19 0.98 0.94 0.87 0.64 1.09 0.72 0.72 0.751 0.51	Onic Check	0.55 0.22 0.80 0.10 0.37 0.27 0.55 0.22 0.80  0.54  0.61	I	Air-Earth Current X 1011.   Amp/cm².   I · 13   0 · 44     0 · 58   I · 29   0 · 89   0 · 91     0 · 76   0 · 37   0 · 59   0 · 94                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           .	Ionic Ct   cc. x	0.52 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.52 0.76 0.59	1	Air-Earth Current X 1018.  Amp/cm1 0·72 0·77 0·88 0·96 1·26 0·79 0·43 1·17 1·92 2·72 0·93 0·38 1·48 0·85 0·82	Could		I	Air-Earth Current x 10 ¹⁴ . Amp/cm ² 1·32  0·59 0·67  0·40 0·74 0·44 0·74  1·26  1·26  1·31 0·42	Could Ct. X +. Could Ct. X +. Could Ct. X +. Could Ct. X +. Could Ct. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. Co. X +. 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#### Mean Values for periods of sixty minutes, centered at the exact hours, Greenwich Mean Time.

#### 482. Richmond (Kew Observatory).

1923.

Day.	1	January. I	Factor 2.81.		1	February.	Factor 2.88	j.	J	March. F	actor 2.70.	<del></del>
Day.	3h.	9h.	15h.	21h.	3h.	9h.	15h.	21h.	3h.	9h.	15h.	21h.
I 2	520	605	630	760	85	215 185	60 200	145 100	80 110	230	310	-325
3	85 210	265 505	140 350	405 705	70 85	405	360	405	650	4 ⁰ 5 445	285 285	605 445
4	450	845	535	350	245	430	275	290	430	285	350	335
5	970	730	140	-76 <b>o</b>	575	780	315	430	245	475	110	445
6	225	815	450	745	230	420	345	130	365	285	230	430
7 8	490	155	505	310	345	375	290	175	215	310	-40	255
	85	395	155	760	-185	0	375	735	135	270	335	255
9	620	240	365	480	575	315	315	575	175	295	700	565
10	155	395	310	520	175	<b>-390</b>	-300	<b>-60</b>	350	620	605	660
11	225	630	335	420	100	375	160	505	295	605	380	595
12	170	645	560	605	260	690	375	85	540	745	190	95
13	435	785	645	620	<b>-60</b>	575	735	245	-110	<del>-475</del>	-335	755
14	155	225	365	590	30	45	505	635	700	835	620	715
15	225	380	420	550	260	100	460	215	135	445	500	460
16	210	505	505	730	-15	735	260	620	230	595	515	605
17 18	450	1220	1250	815	145	650	315	420	310	365	700	620
	590	195	605	660	130	-535	460	290	230	390	420	445
19	480	775	505	110	490	175	260	275	350	580	675	650
20	-240	280	325	350	130	575	820	490	515	540	595	160
21	255	395	505	365	200	995	575	605	65	160	730	350
22	225	660	295	310	260	720	-175	215	365	515	365	245
23	155	630	365	465	-6o	230	375	835	325	110	-390	205
24	365	490 620	405	450 480	15	-230	245		150	325	230 160	420
25	435	020	350	400	]		275	545	390	310	100	325
26	325	465	435	550	130	-185	275	300	55	160	190	335
27 28	280	395	325	420	115	345	230	-45	460	285	215	-95
	265	395	310	365	70	345	375	720	80	255	215	270
29	155	335	140	195	ì		1	}	120	215	-55	405
30	210	435	225	240					175	515	175	430
31	110	170	265	335					365	245	190	365
$\operatorname{Means} \left\{ egin{array}{l} (a) \\ (b) \end{array} \right.$	318	503	411	488	205	395	355	399	287	394	380	430
	300	503	411	448	169	253	317	359	274	366	305	388
Mean for day	(a)	430	(b)	415	(a)	339	(b)	275	(a)	373	(b)	333

#### Richmond (Kew Observatory).

1923.

Day.		April. F	actor 2.93.			May. Fac	tor 2·49.		1	June. I	actor 2.53.	
	3h.	9h.	15h.	21h.	3h.	9h.	15h.	21h.	3h.	9h.	15h.	21h.
ı	205	190	295	395	85	235	185	360	125	455	355	380
2	145	295	395	410	285	310	210	160	100	380	255	445
3	145	410	425	630	85	425	200	385	365	190	100	215
4	350	760	220	660	375	500	185	235	75	255	190	280
5	440	720	925	320	275	360	150	225	175	480	200	200
6	-130	320	600	525	125	150	125	110	100	115	315	280
7	280	320	265	540 485	100	300	300	210	140	265	150	290
7 8	90	350	395	485	100	400	500	510	175	125	115	150
9	440	585	660	615	100	310	125	275		125	65	115
10	410	600	395	z-	185	85	175	235	50 65	25	75	150
11	45	310	-115	760	<b>—</b> 150	210	$z\pm$	185	90	165	150	115
12	45	<b>-90</b>	<b>-440</b>	350	250	175	$z\pm$	275.	200	215	90	z+
13	175	250	175	410	-135	260	125	210	100	100	125	125
14	235	350	335	745	100	225	125	225	75	165	140	125
15	525	265	250	365	75	200	z-	z±	125	190	-605	265
16	295	280	645	615	275	210	225	350	150	140	100	125
17 18	175	555	760	395	200	225	185	275	50	140	115	115
	250	555	250	500	150	185	210	200	150	280	125	200
19	145	585	585	525	200	135	60	185	125	90	150	100
20	295	615	585	485	100	150	60	175	115	280	215	200
21	295	395	365	220	85	125	85	175	150	265	150	165
22	205	190	205	250	175	175	135	250	165	200	175	165
23	235	425	205	160	75	160	/ z±	385	175	265	125	125
24	60	310	115	105	535	575	200	200	115	125	100	125
25	160	60	60	-15	² 35	135	_	160	125	150	190	230
26	-15	175	-45	250	185	300	150	585	50	165	115	125
27 28	205	205	220	365	185	275	135	260	115	100	90	90
	190	235	190	205	125	<b>-60</b>	435	-250	90	355	115	75
29	90	130	175	335	50	300	300	225	125	265	140	230
30	105	90	160	250	135	150	475	360	75	175	115	150
31					125	435	435	310				
$s\begin{cases} (a) \\ (b) \end{cases}$	222	363	365	424	172	256	212	266	125	208	150	185
~ (b)	195	340	306	409	162	259	212	248	123	208	126	185
an for day	(a)		(b)	313	(a)		(6)	220	(a)		(6)	161

Note.—The Potential Gradient is reckoned as positive if the potential increases upwards. For indeterminate potential gradient the following notation is used: z +, Indeterminate, positive value; z-, Indeterminate, negative value; z±, Indeterminate in magnitude and sign.

(a) Mean from all positive readings.

(b) Mean from all complete days using both positive and negative readings.

#### Mean Values for periods of sixty minutes centered at the exact hours, Greenwich Mean Time.

482. Richmond (Kew Observatory). 1923.

Day		July. Fa	ctor 2·58.		1	August. I	actor 2.51.			September.	Factor 2.5	6.
Day.	3h.	9h.	15h.	21h.	3h.	9h.	15h.	21h.	3h.	9h.	15h.	21h.
I	90	140	130	105	. 190	225	125	175	220	345	140	230
2	75	285	105	220	115	225	165	165	155	220	140	165
3	155	195	75	195	125	175	65	165	140	345	115	255
3	170	115	140	260	150	265	125	115	130	-100		230
5	195	385	140	490	400	225	115	225	115	90	155 180	75
6	230	425	400	140	140	200	90	115			245	230
		4 ² 5 2 ⁸ 5	400 180	440 180	125	225	90	190	255	165	190	255
7 8	205			1	190	250	125	200	140	320	155	255
	170	105	115	170				100	190	320	140	360
9	170	310	155	310	225	250	90					230
10	$z\pm$	$z\pm$	465	385	75	300	90	150	155	410	255	230
II	335	285	155	195 465	140	450	115	150	75	245	155	295
12	245	425	260	465	115	165	90	225	180	205	155	280
13	310	720	105	285	65	290	100	100	220	295	180	165
14	230	180	115	260	115	315	115	90	100	165	180	155
15	105	115	65	105	90	240	165	175	155	305	-40	460
16	40	115	105	170	240	300	115	90	280	360	155	485
	270	220	155	245	125	140	75	190	370	320	165	410
17 18	115	270	130	105	100	200	z—	300	100	295	565	510
19	140	205	130	130	165	190	100	125	205	345	220	295
20	155	155	170	180	65	65	140	50	z-	245	165	305
27	TOT	155	115	130	_	175	200	275	-205	255	245	640
21	105 180	155		130	140	190	0	190	220	205	190	140
22		155	130		100	165	50	-25	230	270	245	255
23	115	170	0	105	100					360	205	
24	40	230	130	205		z±	z-	240	115		165	155
25	90	105	50	180	115	375	190	225	15	245	103	155
26	195	220	170	205	65	100	150	200	100	245	165	255
27	170	270	*	180	150	215	$z\pm$	225	245	280	180	320
27 28	25	205	130	155	115	215	125	315	255	305	75	165
29	115	195	105	90	140	140	415	115	155	100	140	75
<b>3</b> 0	40	180	50	-155	100	250			115	130	130	205
31	105	205	105	295			165	465				
				218	138	225	124	184	172	264	186	267
$\operatorname{ans} \left\{ egin{array}{l} (a) \\ (b) \end{array} \right.$	157 150	234 233	142 131	201	140	227	124	152	160	257	176	274
lean for day.		188		179		168	/1	) 160	(a)	222	(b)	217

#### Dishmond /Kow Observatory

1923.

uninona (12	ew Observ	atoi <b>y</b> /•							·			192
Day.		October.	Factor 2·67.		]	November.	Factor 2.7	I.		December.	Factor 2 · 4	Ι.
Day.	3h.	9h.	15h.	21h.	3h.	9h.	15h.	21h.	3h.	9h.	15h.	21h
I	375	200	55	280	175	245	285	255	580	640	335	290
2	95	265	145	135	475	595	270	435	50	85	375	195
3	255	280	z	215	120	110	95	190	360	-	460	375
4	175	215	265	480	135	215	175	285	495	-325	<b>—180</b>	675
5	375	520	320	495	135	300	325	120	480	255	665	590
6	160	225	215	320	255	380	340	325	315	530	640	325
7	200	215	135	-295	300	530	365	300	1460	990	50	-50
7 8	105	305 80	255	280	245	1545	350	230	155	605	410	300
9	25	80	200	360	25	540	595	445	-	385	605	26
10	120	265	95	55	405	445	570	530	315	700	580	44.
11	95	415	215	265	215	595	460	245	410	445	470	480
12	105	-ro5	-15	440	920	745	310	120	215	360	565	48
13	105	215	185			165	285	55	460	480	335	480
14	320	520	o ·	535 385	-55	285	310	595	520	215	625	410
15	345	585	215	440	350	540	215	205	240	625	410	49.
16	335	400	335	360	135	435	310	490	410	375	360	33. 38.
17	135	335	295	265	95	340	285	490	255 180	375	240	
18	320	65	335	280	365	650	270	460		460	290	35
19	55	8o	-55	265	190	395	340	435	170 180	420	325	43.
20	105	320	295	145	245	490	445	445	180	410	385	420
21	_	_	-120	320	245	80	490	475	420	665	470	46
22	65	240	495	425	350	555	475	635	530	110	195	25. 38.
23	160	240	25	385	530	705	760	585	240	255	255 480	38.
24	105	280	305	415	445	595	555	515	195	<b>-420</b>	480	55.
25	145	265	320	505	540	675	1165	1490	530	530	400	60
26	105	200	320	255		1190	610	935	135	135	410	43.
	15	200	280	240	1465	1085	730	720	120	470	420	37.
27 28	105	200	240	335	270	595	475	475	85	155	410	33.
29	135	335	360	320	350	800	585	435	360	460	565	625
30	120	145	175	200	380	515	745	490	275	335	290	135
31	105	375	280	175	1				. 10	315	360	420
((a)	162	276	235	319	347	545	440	447	338	433	425 381	392
$as \begin{cases} (a) \\ (b) \end{cases}$	159	262	217	302	333	535	439	443	337	361		363
an for day.		248		235	(a) 44		(b) 4		(a)	397	(b)	361

(a) Mean from all positive readings.
(b) Mean from all complete days, using both positive and negative readings.
The Potential Gradient is reckoned as positive if the potential increases upwards. For indeterminate potential gradient the following notation is used: z +, Indeterminate, positive value; z - Indeterminate, negative value; z ± Indeterminate in magnitude and sign.
* No trace—gas cut off temporarily.

The departures from the mean of the day are adjusted for non-cyclic change.

SELECTED QUIET DAYS.

#### 483. Richmond (Kew Observatory).

1923.

	*		•		_	• •																				
Month and Season.	Hour.	G.M.T	3	4	5	6	7	8	9	10	11	Noon	13	14	15	16	17	18	19	20	21	22	23	Midt.	Non- cyclic change	Mean values.
Jan. Feb. Mar. April May June July Aug. Sept. Oct. Nov. Dec.	v/m - 78 - 92 - 38 - 63 - 63 - 8 - 37 - 32 - 4 - 45 - 71	-134 - 87 - 113 - 66 - 14 - 46 - 41 - 22 - 60 - 128	-102 -118 - <b>185</b> - 43 - 45 - 34 - 42 - 25 - 88	-133 -152 -157 - 40 - 25 - 26 - 43 - 96	- 104 - 106 - 163 - 31 - 23 - 19 + 5 - 46 - 86 - 133	- 84 - 79	$\begin{array}{c} + 55 \\ + 78 \\ + 113 \\ + 56 \\ - 63 \end{array}$	+105 + 35 - 15 + 82 + 56 + 85 +132 + 84 + 73	+ 73 + 15 + 70 + 50 + 77 + 98 + 48 + 30 + <b>90</b>	+ 50 + 44 + 59 + 12 + 29 + 47 + 36 + 17 + 33	+ 28 + 3 - 17 - 9 + 80	+ 70 + 27 + 64 - 8 + 7 - 20 - 17 - 44 - 38 + 77	+ 45 - 8 + 25 - 34 - 43 - 27 - 56 - 46 + 67	+ 14 - 35 - 16 - 58 - 45 - <b>62</b> - 37 + 23	- 42 + 18 - 1 + 54 - 26 - 11 - <b>60</b> - 43 - 58 - 28	- I + 37 + 24 + 82 - 47 - 15 - 59 - 48 - 34 + 3 + 65	- 19 - 42 - 46 - 23 + 42	+ 56 + 149 + 41 - 9 - 13 - 32 + 14 + 97 + 47	+ 23 - 3 + 6 - 8 + 63 + 118 + 47	+ 77 + 96 + 68 + 14 + 29 - 1 + <b>84</b> + 111 + 31	+ 38 + 87 + 70 + 51 + 11 + 44 - 4 + 52 + 87 + 7	+ 10 + 2 + 49 + 32 + 21 - 11 + 25 + 4 + 29 + 74		50 — 56 — 100 + 7 — 33 — 46 — 19 — 29 — 14	+ 63  - 27 - 10 - 21 - 15 + 6 - 20 - 9 + 1 - 27	v/m 468 341 428 404 249 164 235 165 227 288 450 397
Year	<b>–</b> 51	<b>–</b> 75	- 87	<b> 88</b>	- 72	- 32	+ 18	+ 65	+ 72	+ 52	+ 31	+ 19	- 7	- 22	<b>— 12</b>	+ 4	+ 15	+ 41	+ 51	+ 54	+ 38	+ 20	- 4	- 29		318
Winter	- 81	-113	-115	120	-100	- 49	+ 5	+ 78	+100	+ 88	+ 73	+ 65	+ 28	- 2	+ 8	+ 34	+ 34	+ 46	+ 53	+ 42	+ 15	+ 3	<b>–</b> 31	- 60		414
Eqnx.	<b>– 3</b> 8	- 70	-104	-112	-100	— <b>7</b> 8	— <b>3</b> 0	+ 27	+ 41	+ 38	+ 7	+ 3	- 21	<b>—</b> 25	_ 8	+ 19	+ 40	+ 79	+ 96	+ 92	+ 74	+ 46	+ 27	- 4		337
Sumr.	- 35	<b>42</b>	- 41	- 33	- 17	+ 30	+ 78	+ 89	+ 74	+ 31	+ 13	<b>– 10</b>	- 27	- 39	- 35	<b>- 42</b>	- 28	- 3	+ 5	+ 28	+ 26	+ 10	- 8	- 23		203

 $AIR\ \ POLLUTION:\ \ HOURLY\ \ MEANS\ \ FOR\ \ EACH\ \ MONTH\ \ (milligrams\ \ per\ \ cubic\ \ metre).$ 

COMPLETE DAYS ONLY.

#### 484. Richmond (Kew Observatory).

1923.

Month and Season.	Hour.	G.M.T	3	4	5	6	7	8	9	10	11	Noon	13	14	15	16	17	18	19	20	21	22	23	Midt.	Mean	No. of days used.
Jan. Feb. Mar. April May June July Aug. Sept. Oct. Nov. Dec.	mg/m³ ·112 ·240 ·339 ·134 ·166 ·253 ·192 ·237 ·170 ·173 ·282 ·304	mg/m³ ·112 ·186 ·259 ·173 ·144 ·227 ·192 ·208 ·186 ·198 ·282 ·285	mg/m³ · 070 · 186 · 246 · 160 · 176 · 227 · 256 · 195 · 150 · 147 · 243 · 285	mg/m³ · 054 · 214 · 259 · 186 · 166 · 240 · 278 · 182 · 150 · 173 · 218 · 253	mg/m³ · 054 · 214 · 246 · 186 · 186 · 285 · 234 · 182 · 202 · 122 · 218 · 253	mg/m³ · 125 · 266 · 259 · 221 · 259 · 320 · 288 · 307 · 285 · 198 · 230 · 253	mg/m³ ·237 ·320 ·352 ·307 ·339 ·333 ·320 ·362 ·320 ·272 ·333 ·304	mg/m³ · 278 · 387 · 422 · 333 · 371 · 333 · 342 · 307 · 355 · 320 · 397 · 438	mg/m³ · 333 · 506 · 486 · 368 · 362 · 342 · 320 · 307 · 371 · 320 · 448 · 605	mg/m³ · 333 · 454 · 474 · 333 · 339 · 307 · 278 · 307 · 371 · 320 · 474 · 538	mg/m³ · 307 · 438 · 413 · 333 · 352 · 320 · 256 · 278 · 304 · 320 · 461 · 490	mg/m³ - 320 - 400 - 422 - 307 - 301 - 333 - 256 - 291 - 304 - 320 - 410 - 438	mg/m³ · 307 · 400 · 352 · 272 · 278 · 307 · 246 · 278 · 285 · 320 · 410 · 403	mg/m³ · 291 · 374 · 339 · 307 · 301 · 298 · 256 · 237 · 269 · 320 · 384 · 387	mg/m³ · 291 · 387 · 352 · 307 · 288 · 262 · 202 · 237 · 269 · 294 · 448 · 371	mg/m³ · 320 · 387 · 330 · 307 · 288 · 285 · 202 · 237 · 285 · 320 · 448 · 371	mg/m³ · 333 · 413 · 352 · 333 · 288 · 307 · 202 · 278 · 285 · 320 · 538 · 422	mg/m³ · 320 · 438 · 394 · 346 · 310 · 320 · 214 · 278 · 320 · 346 · 538 · 454	mg/m³ ·349 ·413 ·381 ·368 ·320 ·333 ·182 ·307 ·336 ·512 ·506	mg/m³ ·333 ·413 ·464 ·432 ·320 ·333 ·214 ·307 ·355 ·320 ·525 ·506	mg/m³ · 320 · 387 · 454 · 381 · 320 · 333 · 246 · 307 · 336 · 320 · 486 · 506	mg/m³ · 320 · 400 · 422 · 320 · 259 · 307 · 234 · 237 · 304 · 422 · 470	mg/m³ · 266 · 266 · 403 · 259 · 218 · 298 · 214 · 237 · 253 · 221 · 371 · 387	mg/m³ ·125 ·240 ·394 ·208 ·186 ·240 ·182 ·224 ·218 ·198 ·320 ·336	mg/m³ ·246 ·348 ·367 ·287 ·272 ·298 ·242 ·264 ·278 ·271 ·391 ·399	23 24 31 26 31 28 30 23 19 13 25
Year	-217	•204	·195	•198	•199	•251	.317	•357	∙397	.377	•356	•342	•321	.314	.309	.315	.339	·356	•363	•377	•366	•332	·283	.239	•305	292
Winter	.235	.216	•196	·185	·185	•219	•299	•375	· <b>4</b> 73	·450	.424	•392	·380	•359	.374	.381	-426	•437	•445	•444	•425	.403	•323	.255	•346	91
Eqnx. Spring Autm. Sumr.	·237 ·171 ·212	·216 ·192 · <b>193</b>	·203 ·149 ·213	·223 ·161	·216 ·162 ·222	·240 ·241 ·293	·329 ·296 ·339	·377 ·337 ·338	·427 · <b>345</b> ·333	·403 · <b>345</b> ·308	·373 ·312 ·301	·364 ·312 ·295	·312 ·302 ·277	·323 ·295 ·273	· 329 · 281 · 247	·319 ·302 ·253	·343 ·302 ·269	·370 ·333 ·281	·375 ·341 ·285	· <b>448</b> · 337 · 293	·417 ·328 ·301	·371 ·299	·331 ·237 ·242	·301 ·208 ·208	·327 ·275 ·269	57 32 112

AIR POLLUTION: DIURNAL INEQUALITIES (milligrams per cubic metre).

The departures from the mean of the day are adjusted for non-cyclic change.

#### 485. Richmond (Kew Observatory).

1923.

Month and Season.	Hour 1	G.M.T	3	4	5	6	7	8	9	10	11	Noon	13	14	15	16	17	18	19	20	21	22	23	Midt.	Non- cyclic change	
May June July Aug. Sept. Oct. Nov.	·12 ·12 ·15 ·10 ·04 ·04 ·03 ·10 ·10	** mg/m³* 8 — · 129 - · 178 - · 129 - · 103 - · 114 - · 128 - · 071 - · 045 - · 045 - · 061 - · 092 - · 083 - · 104						+ · · · · · · · · · · · · · · · · · · ·	+ · · · · · · · · · · · · · · · · · · ·	+ · · 088 + · · 103 + · · 108 + · · 046 + · · 067 + · · 009 + · · 037 + · · 042 + · <b>093</b> + · 047 + · 084	+ · · · · · · · · · · · · · · · · · · ·	+ · · · · · · · · · · · · · · · · · · ·	+ · · · · · · · · · · · · · · · · · · ·	+ · 044 + · 029 - · 029 + · 029 • · 000 + · 013 - · 026 - · 009 + · 051 - · 008	+ · · 043 + · · 044 - · · 017 + · 020 + · 016 - · 036 - · 041 - · 025 - · 009 + · 026 + · 055	+0·72 +·045 -·039 +·020 +·016 -·013 -·042 -·025 +·007 +·053 +·055	+ · · 084 + · 073 - · 018 + · 046 + · 016 + · 009 - · 042 + · 017 + · 007 + · 054 + · <b>144</b>	+·071 +·099 +·024 +·059 +·038 +·022 -·031 +·017 +·042 +·081 +·144	+·099 +·076 +·010 +·081 +·048 +·035 -·063 +·047 +·058 +·082 +·117	+ · · · · · · · · · · · · · · · · · · ·	+ · · · · · · · · · · · · · · · · · · ·	+ · · · · · · · · · · · · · · · · · · ·	+·014 -·065 +·030 -·028 -·054 ·000 -·033 -·021 -·025 -·040 -·026	·127 ·089 + ·021 ·079 ·086 ·058 ·066 ·034 ·060 ·062 ·077	+·013 -·038 +·013 ·000 ·000 +·012 -·013 ·000 -·023 +·013	· 287 · 331 · 238 · 298 · 227 · 115 · 168 · 181 · 221 · 238 · 313
Winter Eqn _x	·09	22 - ·121 20 - ·102 5 - ·133 8 - ·098 7 - ·076	·111 · · · · · · · · · · · · · · · · · ·	109 164 110	-·108 -·163	·055 ·129 ·061	+·011 ·049 +·012	+·051 +·028 +·056	+· <b>126</b> +·085	+·072 +·103 +·073	+·050 +·077 +·041	+·037 +·046 +·038	+·017 +·035 +·007	+·009 +·008	+·004 +·029 +·005	+·010 +·037 +·010	+ ·035 + ·082 + ·022	+·052 +·093 +·051	+·059 +·101 +·058	+·073 +·101 +· <b>093</b>	+·062 +·081 +·073	+·029 +·060 +·036	·021 ·021 ·016	—·064 —·087 —·045	·003 ·007 ·003	·203 ·290 ·219

#### DIURNAL INEQUALITIES OF DECLINATION AND HORIZONTAL FORCE.

Departures from the mean of the day corrected for non-cyclic change.

, ,	, ,		'			Ī.					T.,		1	$\overline{\Box}$	<del></del>	1		1	1	1	1	1	1
I	2	3	4 1	5 1	6	7 1	8 1	9	10	11	Noon	13	14	15	16	17	18	19	20	21	22	23	Midt.
486	i. Ri	chmon	d (Kei	w Obs			JATIO	N (M	leasure	d pos	sitive	toward	is the	West	.) (Or	dinary	days)	)·		-		1!	923.
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-0.79	-o·35	-0.19	-0.09	-0.13	-0.35	-0.36	-0.73	-o·78	1+0.08	+1.21	+2.06	+2.36	+2.14	+1.46	+1.00	+0.51	+0.14	-0.40	-o·86	-1.31	-1:62	-1.63	-1.41
-1.16	-1.15	-1.08	-1.02	-1.12	-1.55	-2.17	-2.82	-2.46	-0.74	+1.85	+3.99	+4.85	+4.44	+3.16	+1.79	+0.76	+0.34	-o·o8	-o·61	-r·03	-1.45	-1.43	-1.31
-0.84	-0.89	-1.02	-1.38	-2.24	-2.91	-3.53	-3.45	-2.63	-0.89	+1.35	+3.39	+4.48	+4·48	+3.81	+2.40	+1.36	+0.72	+0.15	-0.04	-0.27	-0.47	-0.72	<b>~o⋅8</b> 6
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DECLINATION (Measured positive towards the West) (Ordinary days).  486. Richmond (Kew Observatory).  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O-52	DECLINATION (Measured positive towards the West) (Ordinary days).    -0.52	DECLINATION (Measured positive towards the West) (Ordinary days).  19  DECLINATION (Measured positive towards the West) (Ordinary days).  19  DECLINATION (Measured positive towards the West) (Ordinary days).  19  DECLINATION (Measured positive towards the West) (Ordinary days).  19  DECLINATION (Measured positive towards the West) (Ordinary days).  19  DECLINATION (Measured positive towards the West) (Ordinary days).  19  DECLINATION (Measured positive towards the West) (Ordinary days).  19  DECLINATION (Measured positive towards the West) (Ordinary days).  19  DECLINATION (Measured positive towards the West) (Ordinary days).  19  DECLINATION (Measured positive towards the West) (Ordinary days).  19  DECLINATION (Measured positive towards the West) (Ordinary days).  19  DECLINATION (Measured positive towards the West) (Ordinary days).  19  DECLINATION (Measured positive towards the West) (Ordinary days).

DECLINATION (Quiet days).

#### 487. Richmond (Kew Observatory).

1923.

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Jan.	-0.40	-0.05	+0.14	+0.52	+0.11	-0.14	-0.41	-0.82	-1.01	-0.23	+0.4	8 + 1·o	$9 + 1 \cdot 5$	0+1.	29 +0.	59 +0.6	6 +0.39	+0.16	-0.15	-0.52	-0.78	-0.93	-0.94	-0.75
Feb.	-0.42	-0.25	-0.22	-0.19	-0.40	-0.73	-0.97	-1.42	-1.55	-0.92	+0.6	7 + 1 • 7	$0 + 2 \cdot 4$	3+2.	20 + 1 • ;	35 +0.5	0 +0.10	+0.00	-0.02	-0.15	-0.22	-0.29	-0.52	-o∙83
Mar.	-0.65	-0·60	-0.62	-0.69	<b>-0</b> ∙87	-1.02	-1.38	-1.98	-2.31	-1.47	+0.6	+2.2	8 + 3 - 4	2+3	19 +2.	19 + 1 • 1	2 +0.16	+0.20	+0.05	-0.03	-0.14	-0.30	-0.73	
April	-0.87	-0.78	-0.03	i -o∙95	-1.40	-1.97	-3.06	<b>-4</b> ·03	-3.60	-1.24	+1.6	1+4.0	8 +4.9	5 +4 **	20 + 3.0	$\infty + 1 \cdot 7$	3 +0.98	3+0.41	-0.04	-0.09	-0.21	-0.28	-0.71	-0.92
May	-0.13	-0.41	-0.70	-1.38	-2.29	-3.01	<b>-3⋅66</b>	-3.56	-2.79	-1.03	+1.5	3 + 3 · 20	6  <b>+4·2</b>	6 + 3 •	99 + 2 - 8	31 + 1 · 5	2 +1.08	3 +o⋅83	1+0-49	-0.12	<b>−0·18</b>	-0.11	-0.25	-0.09
June	+0.08	-0.13	-o·8q	-1.51	-2.57	-3.46	-3.70	-3.88	-3.42	-1.4	+0.7	1+2.8	3  <b>+</b> ∡∙0	5 +4.	323 1 + 3 ⋅ 8	381+2.6	21+1.36	+o⋅60	十0・21	+0.11	1十0.07	+0.07	+0.24	-0.00
July	-0.30	<b>-0∙37</b>	-0.21	-0∙85	-1.64	-2.54	<b>-3·12</b>	-3.01	-2.37	-1.25	+0.30	+2.0	8 +3.3	4 +3.4	19 +2.8	35 + 1.7	9 + 1 • 12	+0.46	+0.58	+0.10	+0.13	+0.02	-0.02	-0.20
Aug.	-1.01	-1.03	-1.12	-1.27	-1.97	-2.73	-3.23	-3.07	-1.91	-0.13	+2.5	+4.2	7 +4.9	9+4:	35 +2.9	99 + 1 · 2	9 +0.27	-0.27	-0.17	-0.09	-0.27	-0.45	-0.75	
Sept.	-0.00	-0.98	-1.09	-1.31	-1.57	-1.95	-2.65	-3.23	-2.54	-0.90	+1.9	2 +4.10	+4.8	0 +4∵	38 +2.	88 + 1.3	7 +0.37	1+0.17	+0.12	-0.27	-0.57	-0.25	-0.88	_
Oct.	-0.80	-0.71	-0.67	<b>⊸</b> 0∙74	-0.68	-1.05	-I:37	-2.10	-2.32	-0.51	+1.9	1+3.1	1+3.9	9 +2.6	95 + 1 .	9 +0.0	6 +0.3	+0.27	-0.00	-0.50	-0.37	-0.57	-1.00	
Nov.	-0.59	-0.48	-0.00	-0.05	-0.51	-0.65	-0.92	-1.22	-1.15	-0.13	+1.2	+2.2	+2.1	8+1.	17 +0.	7 +0.7	0+0.48	-0.01	-0.27	-0.47	-0.70	-0.00	-0.05	-0.93
Dec.	-0.23	-0.10	+0.03	-0.10	+0.01	-0.22	-0.21	-0.88	-0.59	+0.09	+1.1	+T.0	1.2	9 + 1 . 2	101+0.9	7 +0.2	0 +0.07	+0.04	-0.41	-0.00	-0.03	-0.70	-0.73	-0.00
Ì												1	1		1	ľ		1	1				1	
Year	-0.55	-0.40	-0.56			7.60	2.08	9.44	2.12	-0.77		140.0	1.2.4	2	نمدام		1 +0.57	140.25	0.00	-0.20	-0.33	-0.41	-0.60	-0.74
1 Can	~.55	-0.49	J-0.30	-0.71	-1-12	-1.02	-2.00	-2.44	-2-13	-0.77	T1-2	T 2 7.	3 70.3	<b>U</b> T5'	79 72	50 T1 2	1 -0.37	70.23	0 00	-0 20	0 33	4-	0.00	- /-
				ĺ			}				1	}	ļ				1		1				- 1	
Vinter	-0.40	-0.22	-0.03	+0.04	-0.12	-0.43	-0.70	-1 -09	-1.07	-0.30	+0.00	+ r · 6	8 + 1 . 9	3 + 1 .	54 +0.0	15 +0.5	9 +0.28	+0.07	-0.21	-o∙∡8	-0.60	-0.70	-0.76	-0.84
1		Ī	1	1	l .	·	1				ļ			1	1	1	1		1				ſ	•
Eanx.	-0.82	-0.77	-0.83	-0.02	-1.13	-1.50	-2.11	-2.85	-2.60	-1.03	+1.5	1 + 3.4	I +4·2	1 + 3 • 6	58 +2.	1 +1.2	2 +0.46	+0.26	+0.02	-0.15	-0.32	-0.42	-0.83	-0.97
				1			l				1		1	l l	- 1	1	1	i	1 .					
Sumr.	-0.34	-0.49	-0∙81	-1.25	-2.12	-2.94	-3.43	-3.38	-2.62	-0.97	+1.30	+3.1	I +4·1	6+4.0	04 + 3 •:	3 + 1 - 8	1 +0.96	+0.41	+0.20	+0.02	<b>-0∙0</b> 6	-0.11	-0.20	-0.40
		,-	1 1								•	]	1	1	1		J	]	1			İ	i	
								<u>_</u>					<del></del>											

HORIZONTAL FORCE (Quiet days).

#### 488. Richmond (Kew Observatory).

1923.

Feb. Mar. April May June July Aug.	+-+-+	2·4 2·3 0·4 2·1 3·4 0·8 0·7	- 4· - 2· - 1· - 3· + 0· + 1·	3 - 4 - 8 - 3 + 1 - 8 -	4.0 1.6 4.5 0.9 0.9 1.4 0.8	- 3· - 1· - 3· - 1· - 1· - 1·	7 - + + + + + + + + + + + + + + + + + +	- 1·3 - 0·6 - 1·8 - 2·0 - 1·6 - 0·9 - 0·1	+++++	3·1 3·0 2·9 1·6 0·9 3·5 1·3 2·8	++++	3.9 - 2.0 3.9 - 3.6 3.6	+ 7· + 3· - 4· - 5·	6 + + - 9 5	0.9 1.3 -11.4 -11.0 -16.4 -12.0 -14.5	- 8. - 7. -19. -14. -17. -13. -18.	3 - 4 - 1 - 3 - 5 - 7 - 6 -	11 · 3 9 · 9 20 · 1 15 · 0 18 · 0 14 · 4 18 · 3 16 · 8	7 - 1 · 3 - 9 · 1 - 15 · 1 - 10 · 0 - 16 · 1 - 11 · 2 - 9 · 5	1 - 4 1 - 5 1 - 7 0 - 4 1 - 10 1 - 2 7 - 5 2 - 4	·8 ·2 ·4 ·9 ·5 ·7 ·2	- 1·3 - 3·0 - 2·7 - 2·6 - 5·3 - 0·8 - 1·6	- 0 0 2 2 2 2 4 + 2 2 2 0	·5+ ·1+ ·5+ ·6+ ·8-	0.6 1.9 6.2 7.4 6.9 2.8	+ 3 + 10 + 10 + 9 + 4 + 10 + 3	· 8 + · 4 + · 0 + · 1 + · 7 + · 7 + · 9 +	- 7·4 - 3·8 -10·5 -13·0 -11·9 - 8·4 -11·2	+ 7 + 4 + 10 + 13 + 11 + 10 + 7	9++++++++	5·3 5·1 9·6 10·0 12·4 12·8 11·4	+ 3 + 4 + 8 + 9 + 12 + 10 + 10 + 8	9+3++2++3+	- 2·5 - 4·9 - 7·7 - 6·7 - 9·0 - 7·1 - 9·1	+ 1 2 5 5 + 4 4 4 4 4 6 + 6 + 6	·6 + ·8 + ·2 + ·6 + ·5 +	- 0·8 - 1·5 - 4·1 - 2·6 - 4·3 - 2·1 - 2·0 - 4·0
Nov. Dec.	<b> </b> –	1.7	- 2.	61 -	1.6	- o·	· 2 +	2 · I	1+	3.3	+ 3	3·8 -	+ 3⋅	5 -	- 0.2	- 5.	2 -	7.2	- 6·6	<b>5</b> – 4	· I] ·	- 2.0	<b>–</b> 0	•9  -	· 0 · I	+ 2	·8  <del>- </del>	- 5.9	+ 5	4+	2.6	+ 1	이+	- I·I	+ I	•4 -	- 0.2
Year	_	1.3	- 2.	1 -	1.8	- 1.	3 +	0.1	+	1 · 1	+ 1	1.8	- o·	3 -	· 6·1	-11.	7 -	12 · 6	- 9·1	- 4	•3	- 1.5	<b>+ o</b>	-8	2.6	+ 5	.7	- 8•1	+ 8	7+	7.5	+ 6.	2 +	- 5.0	+ 3	+ ه٠	. 1.1
																			- 4.7																		
Eqnx.	-	0.2	- 0.	9 -	0.6	- 0.	3 +	1.0	+	2.5	+ 3	· I -	+ 0.	6 -	6.3	-14	5 -	15 · 1	-11.0	- 5	•2	- 2·3	- o	· 5 +	o·8	+ 4	-8 +	7.3	+ 8	0+	7.6	+ 6.	6+	- 6.8	+ 4	·6 +	2.9
iumr.	+	0.4	- 0.	6 -	1.5	- I·	2 -	0.3	-	1 · 2	- 1	.7	- 6.	4 -	13.5	-16.	o -:	16 · 4	-11.5	- 5	. و٠	- 2·4	+ 2	4+	6.3	+ 8	-8	-11 - 1	+12	1+	11.5	+10	6+	7.5	+ 4	•7 +	2.8

#### 489. Richmond (Kew Observatory).

1923.

Month,	Quiet days	ELEMENT. D and H, abs	olute obser-		FO	RCE.		RANGE	OF INEQ	UALITY.	AVERAG	GE DEPA	RTURE
Season		1			<del></del>	1		" Ordi-	Quiet	days.	" Ordi-	Quiet :	Days.
Year.	Declination (West).	Inclination.	Horizontal Force.	North.	West.	Vertical.	Total.	nary" Days. D'.	D.	Н.	nary" Days. D'.	D.	Н.
January February March April May June August September October November December Winter Equinox	0 / 14 3 · 0 14 1 · 8 14 1 · 4 13 59 · 4 13 57 · 6 13 57 · 6 13 55 · 8 13 54 · 9 13 54 · 0 13 52 · 8 13 57 · 3 57 · 3 57 · 3 57 · 3 57 · 4	66 57.0 66 56.8 66 57.4 66 57.1 66 57.5 66 57.5 66 57.3 66 57.4 66 57.4 66 57.4 66 56.3 66 56.8 66 56.7	7 18392 18392 18394 18392 18396 18394 18395 18397 18397 18393 18394 18393	7 17842 17843 17846 17846 17852 17851 17852 17856 17857 17854 17857 17861	7 4465 4459 4457 4446 4442 4437 4436 4429 4413 4406 4436	γ 43224 43216 43243 43229 43234 43247 43246 43205 43203 43227 43218 43229	7 46974 46967 46992 46978 46985 46994 46996 46959 46959 46956 46979	3·78 4·63 6·31 10·02 7·79 8·93 7·41 8·51 8·02 6·35 4·34 3·52 3·99 7·67	2·51 3·98 5·73 8·98 7·92 8·21 6·61 8·22 8·13 5·87 3·50 2·54 3·02 7·06	γ 12·4 19·2 16·8 30·7 28·3 31·6 26·7 30·1 27·7 22·6 13·1 10·6 11·9 23·1	0·77 1·14 1·49 2·20 1·81 2·05 1·67 1·89 1·83 1·55 0·99 0·82 0·92	0·59 0·76 1·13 1·75 1·65 1·76 1·33 1·69 1·21 0·80 0·59 0·67	γ 3·4 4·3 3·8 6·8 6·7 8·1 5·6 6·6 5·4 4·3 2·7 2·4
Summer	13 57.3	66 57.3	18395	17853	4436	43243	46993	8.01	7:59	28.5	1.85	1.59	6.5
Year 1923 1922 1921 1920 1919 1918 1917 1916 1915 1914	13 57·3 14 8·8 14 19·9 14 31·0 14 40·9 14 50·4 14 59·6 15 8·8 15 18·4 15 27·8 15 37·0	66 57.0 66 57.6 66 57.7 66 57.9 66 57.7 66 58.4 66 58.0 66 57.5 66 56.6 66 55.8 66 55.8	18394 18394 18399 18410 18416 18429 18437 18457 18463 18488	17851 17836 17827 17822 17815 17814 17809 17816 17808 17818	4436 4495 4555 4615 4667 4720 4770 4823 4874 4929 4982	43230 43251 43266 43297 43305 43361 43366 43395 43376 43406 43449	46980 47000 47016 47049 47058 47115 47122 47156 47141 47179 47226	6·23 6·55 7·51 8·12 8·73 9·31 ————————————————————————————————————	5.87 6.68 7.07 7.91 8.52 9.23 10.18 8.73 7.30 6.13 6.87	21·3 22·3 22·6 28·3 28·0 30·1 34·0 30·0 24·8 22·2 18·1	1·50 1·67 1·83 2·10 2·26 2·28	1·23 1·40 1·47 1·83 1·84 1·91 2·16 1·84 1·60 1·30 1·45	4·3 4·7 4·8 6·5 6·3 7·7 8·3 7·0 5·7 4·9

#### MAGNETIC CHARACTER OF EACH DAY.

#### 490. Richmond (Kew Observatory).

1923.

			`										
Date	Jan.	Feb.	March	April	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
I	0	I	0	0	0	0	I	0	I	I	1	0	
2	0	0	0	0	0	0	1	0	0	0	2	0	
3	0	0	0	0	I	0	0	I	I	0	I	0	
4	I 0	I 0	0	0	I 0	I	0	I 0	0	0	0	I	-
5	Ū	"		ľ		1	"	ľ	0	"	0	0	-
6	1	0	0	0	0	I	1	1	0	0	0	0	-
7 8	0	I	I	0	0	0	1	0	0	0	I	9	-
	0	0	0	I	0	0	I	0	0	0	0	0	
9	0	0	0	I	ő	0	0 2	0	I . I	I	0	I	_
•	Ū	ľ		1	"		2	Ŭ		1 *	°	I	_
11	0	0	0	1	0	0	1	o	r	1	0	0	
12	0	0	0	I	0	1	I	I	0	I	2	0	-
13	I	0	0	I	0	2	0	I	0	0	1	0	-
14	I	I	I	I	0	I	0.	I	I	I	0	1	
15	0	0	I	0	0	1	0	I	0	2	0	0	
16	o	o	1	o	o	0	0	o	o	2	o	o	
17	0	I	0	0	2	0	0	0	0	2	0	0	_
18	0	1	I	0.	2	0	1	0	1	2	0	0	-
19	0	0	0	0	I	0	I	0	0	I	0	0	_
20	. 2	0	I	I	I	0	0	0	0	0	0	0	_
21	2	o	0	I	0	1	0	0	0	0	0	0	
22	I	0	0	2	0	0	1	0	0	0	1	0	_
23	I	0	0	I	0	0	I	0	0	0	I	I	_
24	I	0	2	I	0	0	0	0	0	0	0	I	_
25	0	?	2	0	0	0	0	0	0	0	0	1	-
26	o	2	1	0	0	0	0	o	2	0	0	2	_
27 28	0	2	I	0	0	0	I	0	2	1	1	I	_
	0	I	1	0	0	0	0	0	2	0	I	1	
29	I		I	0	I	0	0	0	1	0	I	0	_
30	I		0	0	I	2	0	0	I	0	1	0	
31	0		1		0		0	I		I		0	_
io. of o's.	20	18	18	18	22	21	18	23	18	18	18	21	233
No. of	9	7	11	11	7	7	12	8	9	9	10	9	109
No. of 2'8.	2	3	2	1	2	2	1	0	3	4	2	1	23
Mean Chrotr.	0.42	0.46	0.48	0.43	0.35	0.37	0.45	0.26	0.20	0.55	0.47	0.32	0.42

NON-CYCLIC CHANGE (24h.-0h.).

#### 491. Richmond (Kew Observatory).

- 19**23.** 

Month, Season	Ordinary Days.	Quiet	Days.
or Year.	D'.	D.	H.
	,	,	γ
Ian	-0.07	+0.20	+o·1
Feb	-0.14	-0.22	+2.7
Mar	-o·o3	+0.10	+2.3
Apr	+0.06	-0.50	-0.3
May	-0.04	+0.12	+2.0
June	+0.03	<b>-0.06</b>	+2.7
July	_o.o8	-o·o8	+4.1
Aug	-0.11	0.00	+2.2
Sept	+0.04	+0.04	.—0∙8
Oct	-0.10	+o·36	+3.3
Nov	<b>–o∙o</b> 3	-o·38	+0.0
Dec	-o.oı	-0.24	+2.0
Winter	-o·o6	-o·16	+1.4
Equinox	-0.01	+0.08	+1.2
Summer	<b>–0·05</b>	-o.o1	+2.8
Year 1923	-0.04	-o·o3	+1.8
1922	+0.0i	+0.13	+2.4
1921	+0.03	+0.07	+3.6
1920	+0.04	+0.16	+3.3
1919	-0.11	+0.04	+5.4
1918	-0.04	-0.11	+4.0
1917		+0.13	+4.0
1916	_	-0.03	+3.0
1915		-0.31	+2.6
1914		+0.03	+1.1
1913		+0.01	+2.1
L		<u> </u>	

492. MEAN VALUES, FOR THE YEARS SPECIFIED, OF THE MAGNETIC ELEMENTS AT OBSERVATORIES WHOSE PUBLICATIONS ARE RECEIVED AT KEW OBSERVATORY, RICHMOND.

				192	3.			1922	2.	,		1921	L.	
Place.	Latitude.	Longitude.	Declina- tion.	Inclina- tion.	Hori- zontal Force.	Vertical Force.	Declina- tion.	Inclina- tion.	Hori- zontal Force.	Vertical Force.	Declina- tion.	Inclina-	Hori- zontal Force.	Vertical Force.
Sodankyla, Finland Lerwick, Shetland Islands Pavlovsk, Petrograd, Russia Sitka, Alaska Rude Skov, Denmark  Eskdalemuir, Scotland Meanook, Alberta Stonyhurst, Lancs., England Potsdam, Prussia De Bilt, Utrecht, Holland  Valencia, Cahirciveen, Ireland K w, Richmond, Surrey, England Greenwich, London, England Val Joyeux, near Paris, France Munich, Bavaria Nantes, France Pola, Istria Agincourt, Ontario Tortosa, Spain  Coimbra, Portugal Coimbra, Portugal Cheltenham, Maryland San Fernando, Spain Tucson, Arizona Dehra Dun, near Simla, India *Hongkong, China Honolulu, Hawaii Honolulu, Hawaii Teoloyucan, Mexico Toungoo, Burma Alibag, Bombay, India Vieques, Porto Rico Antipolo, Manila, Philippine Is. Kodai-Kanal, India †Batavia, Java	N. , 67 22 60 9 59 41 57 3 55 51 56 51 28 48 49 48 49 47 1 44 52 43 47 40 49 40 12 38 44 36 28 32 15 30 19 22 18 21 19 19 45 18 56 18 39 18 9 14 36 10 14 50 11	26 39 E. 111W. 30 29 E. 135 20 W. 12 27 E.  3 12 W. 13 21 W. 2 28 W. 13 4E. 13 1E. 5 11 E. 10 15 W. 0 19 W. 0 0 2 1 E. 11 37 E. 1 34 W. 13 51 E. 79 16 W. 13 51 E. 79 16 W. 10 50 W. 6 12 W. 110 50 W. 76 3 E. 114 10 E. 158 4 W. 99 11 W. 96 27 E. 72 52 E. 65 26 W. 121 10 E. 77 28 E. 106 49 E.	16 13·8 W. 27 23·3 E. 15 17·6 W. 6 56·9 W. 16 50·2 W. 18 46·5 W. 13 57·3 W. 13 23·5 7 0·9 W. 11 30·6 W. 14 54·2 W 13 32·6 W 1 38·6 E. 0 23·2 W 9 14·0 E 0 52·2 E.	N. 72 33·6 71 20·1 69 38·8 77 53·2 68 41·6 66 36·5 66 33·5	7 14655 15858 16676 12881 17308 18365 18603 18378 17852 18394 18452 19664 20212 15784 23328 23110 25027 32926 37284	7 46652 46943 46652 46943 44954 60025 44377 42920 42905 43038 44242 43230 43187 41504 57849 36680 37433 33168 22177	° ', 1 22·6E 2 58·9E. 30 29·1E. 7 33·8 W. 16 25·8 W. 27 28·5 E. 15 30·9 W. 7 7·6 W. 7 8·9 W. 11 1·9 W. 18 57·0 W. 14 8·8 W. 13 46·7 W. 12 31·5 W 6 56·2 W. 11 39·7 W. 15 4·7 W. 16 27·7 W. 13 41·6 W. 13 47·5 E. 1 43·2 E. 0 21·5 W. 9 57·1 E 0 29·7 W. 0 12·6 E.	1001.  N.  75 40·5  71 17·3  74 22·4  69 2·6  69 40·0  77 53·3  68 42·4  66 35·7  66 52·3  64 39·6   74 44·6  57 35·5  58 17·0  70 57·6  53 50·1  59 29·0  45 8·6  30 46·0  39 24·4   23 7·2  25 5·0  51 33·1   4 40·1  S.  20 0·3	7 12561 15895 15560 17087 16680 12902 17305 18577 18615 18382 17849 18394 18442 19661 15809 23314 23096 19020 25033 26839 32927 37279 28794 39156 36967 27695 37878 36784	79 49187 46927 55631 44614 45012 60126 44402 42918 42903 43054 44289 43251 43176 41517 57961 36725 37369 55115 45533 33091 22194 23658 16717 17303 34880 3093 22990	1 13·3 E	N., 75 37.6 71 14.2 74 22.6 69 1.2 69 40.3 77 53.7 68 43.0 66 34.5 66 52.6 68 3.4 66 57.7 66 53.0	7 12605 15936 15570 17105 16695 12909 17315 18591 18629 18389 17848 18399 18449 19670 22094 15839 23301 23110 19069 25041 26875 32945 37295 37190 28824 39132 36956 27761 38116 37832 36766	49188 46910 55679 44607 45062 60190 44449 42911 42898 43065 44299 43266 43218 41548 38537 58065 36754 37448 55200 45564 33025 22199 22125* 23683 16704 17226 34868 11028 3071 22925
Apia, Samoa  Mauritius  Pilar, Cordova, Argentina  Christchurch, New Zealand	13 48 20 6 31 40 43 32	57 33 E. 63 53 W. 172 37 E.	10 16·3 E. 10 49·2 W.  17 11·7 E.	30 6·6 52 33·7  68 12·0	35248 22982  22209	30017  55526	10 39·9W.	30 5·6 52 36·2  68 11·2	35241 23019  22217	30112  55507	10 10·7 E. 10 30·7 W. 7 40·2 E. 17 4·6 E.	30 3·8 52 37·1 25 39·2 68 10·3	35265 23061 25241 22241	30185 12122 55528

^{*} The first set of values for 1921 refer to the new hut; the second set of values for 1921 refer to the old hut; the values for 1922 refer to the new hut.

#### 493. ADDITIONAL VALUES FOR EARLIER YEARS.

				1920	•			1919.	•			1918	3.	
Pavlovsk, Petrograd, Russia O'Gyalla, Pesth, Hungary Pola, Istria San Fernando, Spain Tsingtau, Kianchow, China Lukiapang, Shanghai, China Helwan, Egypt	N., 59 41 47 53 44 52 36 28 36 4 31 19 29 52	30 29 E. 18 12 E. 13 51 E. 6 12 W. 120 19 E. 121 2 E. 31 21 E.	° , 2 42·7 E	N., 71 11·1 53 37·5 52 7·0 45 30·7 41 12·8	γ 15978  25021 30817 33175 29956	γ 46897   39610 33773 26236	2 35·2E. 7 1·6W. 14 8·5W. 4 9·9W. 3 20·0W. 1 30·6W.	53 44·6 52 7·4 45 31·0	γ 16019  22111 25101 30812 33187 29941	38539	2 27·8E. 5 21·9W. 7 11·0W. 14 12·4W. 4 8·2W. 3 18·8W. 1 38·4W.	60 9·0 54 2·2 52 6·9 45 31·0	γ 16063 20917 22113 24976 30827 33212 29948	7 46867  38533  39621 33817 26126

[†] Means based on absolute observations.

# Air Ministry METEOROLOGICAL OFFICE

# OBSERVATORIES' YEAR BOOK 1923

Comprising the results obtained from autographic records and eye observations at the observatories at Lerwick, Aberdeen, Eskdalemuir, Cahirciveen (Valencia Observatory), Richmond (Kew Observatory), and Benson.

### **BENSON**

Published by the authority of the METEOROLOGICAL COMMITTEE



LONDON:

PRINTED AND PUBLISHED BY HIS MAJESTY'S STATIONERY OFFICE.

#### BENSON OBSERVATORY.

Latitude			 	 51° 37′ N
Longitude			 	 1° 7′ W
Height above	Sea	Level	 • •	 57 metres.

#### INTRODUCTION.

## Notes on the tables of Upper Air Temperatures obtained from soundings with registering balloons at Benson, Richmond, and Liverpool. 1923.

The tables are presented in the same form as those appearing in the Observatories' Year Book for 1922. The Dines pattern meteorograph was solely employed as before, the instruments being constructed in the Observatory workshop.

The method of operation remained substantially the same as that described

in the Computer's Handbook.*

In the computations of pressure-height a value of gravity constant with height has been assumed, and equal to 981·2; the effect of humidity on the density of the air has been neglected.

A total of 46 soundings were made during the year, of which 25 instruments were found and returned; a somewhat poor result. Of 6 soundings made from Kew Observatory in Oct.-Nov.-Dec. only one was returned. In a number of cases the heights reached were poor owing to bad quality and premature failure of the balloons.

In most cases the mean of the record on the ascent and descent was employed entirely in computing the published figures. In a few cases where the difference between the two was greater and more systematic than usual, the colder record was used alone; in a few other cases where the difference was pronounced near the ground only, what was judged to be the ascending record was alone employed for this particular layer, the rest being determined from the mean as usual.

The figures given in the table of lapse rates do not in every case agree with the temperatures appearing in the table of temperature-heights. The reason is that both were determined independently from the original data, which can sometimes profitably

be read to ·5 degree, and then rounded off to the nearest whole degree.

During the year a new method of making pressure-temperature marks was employed in the calibration of the instruments. This allows of the pressures of calibration being determined on the record to within about ·5 millibar, a

considerable improvement on former practice.

Experiments were made to determine the extent to which the record of pressure was affected by hysteresis of the aneroid box, and to what extent the effect might cause error as between the conditions of an actual sounding in which the pressure change is slow, and those of the calibration test in which it is comparatively rapid. The results seemed to show that with new instruments used immediately after construction there might be an appreciable difference between the two, in the sense that at pressures of 300 mb. or less the pressure record during the ascending part of the sounding might be 7 or 8 millibars too low as determined by comparison with the calibration marks. At higher pressures the discrepancy fell off. When an instrument had been used its behaviour became more consistent, and this particular error appeared to cease to be appreciable.

It is clear that in the cases of a few soundings the minimum pressure recorded may have been appreciably affected by this error, and that in consequence the maximum height claimed may have been too great. If 7 mb. be taken as the maximum error likely to have occurred, this at 18 km. would involve an error in the height determination of about 0.6 km., making the true maximum 17.4 instead of 18. The possible error falls off rapidly as the height decreases.

The position is uncertain and it is impossible to state what the error is likely to be in any particular case; all that can be done is to state the maximum error likely to have occurred, and the fact that the mean error is probably decidedly less than half

the maximum.

As a further effect of hysteresis, during the descending part of a sounding the pressure seemed to be recorded systematically too low by an amount of perhaps 6 or 7 millibars in the middle region of a high ascent, falling off to something less than this on either side. Individual instruments sometimes yielded results decidedly worse than the above, and in all cases it appeared to be a permanent error, which while it might grow a little less, was not eliminated by ageing or continued use. If a correction be applied to the recorded temperature-pressures to allow for the error, it results for an average sounding in the troposphere in an increase in the difference between the temperatures recorded at any pressure on the ascent and descent.

The effect is to make the recorded temperatures on the descent too high by about I degree at a height of 5 or 6 kilometers, with a tendency for the error to fall off above and below. When the mean of the two records is employed the resultant

error is halved and ceases to be serious.

Some experiments were also made to determine whether in daylight the thermograph was appreciably affected by either:

(1) A trail of heated air left behind by the balloon;

(2) Direct radiation from the sun.

The result, as far as it went, was to show that under the conditions ordinarily prevailing in regard to the suspension of the instrument and the rate of ascent of the balloon, No. (1) was negligible and No. (2) was in general quite small. Both these conclusions have since been confirmed.*

In Table 494 occur the entries "Type of Tropopause" and " $H_c$  = Height of Tropopause." These are defined as follows:—

Type I. The stratosphere commences with an inversion, and  $H_c$  is the height of the first point of zero temperature gradient.

Type II. The stratosphere begins with an abrupt transition to a temperature gradient below 2a per kilometre without inversion, and  $H_c$  is the height of the abrupt transition.

Type III. There is no abrupt change of temperature gradient, and the base of the stratosphere is taken at the point where the mean fall of temperature for the kilometre next above is 2a or less, provided that it does not exceed 2a for any subsequent kilometre.

^{*} The Meteorological Magazine. August, 1923. Page 165.

#### UPPER AIR TEMPERATURES.

#### SOUNDINGS WITH REGISTERING BALLOONS, 1923.

Lat. 51° 37′ N.

Long. 1° 7′ W.

Height above M.S.L. 57 metres.

T = Temperature in Degrees absolute above 200a. 494. Banson. P =Pressure in millibars. H = Height in kilometres above M.S.L.

					,								
No.	422.	424.	425.	426.	428.	429.	430.	431.	432.	433∙	434∙	435∙	436.
Date.	Feb. 6.	Feb. 8.	Feb. 9.	Feb. 12.	Feb. 14.	Feb. 15.	Feb. 16.	Feb. 17.	Mar. 8.	Apr. 2.	Apr. 3.	Apr. 4.	Apr. 6.
Start G.M.T	10 h. 45 m.	16 h. 53 m.	16 h. 43 m.	7 h. 12 m.	7 h. 23 m.	7 h. 13 m.	7 h. 21 m.	7 h. 24 m.	17 h. 33 m.	17 h. 55 m.	17 h. 57 m.	18 h. o6 m.	17 h. 43 m.
$H_t = \text{Greatest Height}$	11·1 km.	8·3 km.	13·4 km.	9·7 km.	16·4 km.	10·9 km.	9·8 km.	11·8 km.	11·7 km.	12.8 km.	13·0 km.	11·6 km.	10.0 km.
$T_t = $ Corresponding Temperature.	212 a.	226 a.	222 a.	223 a.	223 a.	221 a.	221 a.	227 a.	22I a.	219 a.	213 a.	210 a.	216 a.
$P_t = \text{Corresponding}$ Pressure.	215 mb.	317 mb.	149 mb.	262 mb.	95 mb.	224 mb.	261 mb.	191 mb.	190 mb.	166 mb.	161 mb.	199 mb.	250 mb.
Place of Fall	Edenham, Lincs.	Brooke, Oakham.	Moreton, Ongar, Essex.	Cobham, Surrey.	Ruckinge, Ashford, Kent.	Dartford, Kent.	North- fleet, Kent.	Woking, Surrey.	Atherfield, I.O.W.	Sible, Heading- ham,Essex.	Little- hampton, Sussex.	Newbold Verdon, Leicester- shire.	Preston, Upping- ham, Rutland.
Distance	135 km.	114 km.	92 km.	58 km.	151 km.	93 km.	103 km.	50 km.	109 km.	121 km.	97 km.	112 km.	113 km.
Bearing	20°	14°	83°	122°	113°	102°	100°	130°	187°	<b>7</b> 3°	155°	351°	14°
Geostrophic Wind— Time G.M.T	10 h.	18 h.	18 h.	7 h.	7 h.	7 h.	7 h.	7 h.	18 h.	18 h.	18 h.	18 h.	18 h.
Speed	20 m/s.	9 m/s.	18 m/s.	9 m/s.	8 m/s.	8 m/s.	8 m/s.	11 m/s.	13 m/s.	10 m/s.	5 m/s.	9 m/s.	8 m/s.
Deg. from N	200°	250°	180°	230°	140°	160°	230°	265°	. 55°	115°	165°	160°	120°
Wind (Anemometer) Speed	14·0 m/s.	4·0 m/s.	5·5 m/s.	2·0 m/s.	7·0 m/s.	1.0 m/s.	3.0 m/s.	4·5 m/s.	7·5 m/s.	1 · o m/s.	3.5 m/s.	6·5 m/s.	5.5 m/s.
Deg. from N	105	235		225	120	140		230	40	90	170	125	
Type of Tropopause	r.		ı.	11.	ı.	ı.	Ι.	1.	1.	Ι.	ı.	ı.	?
$H_c = \text{Height of}$ ,	10·65 km.		10·77 km.	8·77 km.	10·16 km.	10·59 km.	9·68 km.	9.05 km.	9·44 km.	10·22 km.	12.00 km.	11·44 km.	9.64 km.
$P_c = \text{Pressure at ,, } \dots$	230 mb.		255 mb.	302 mb.	250 mb.	235 mb.	266 mb.	290 mb.	272 mb.	250 mb.	190 mb.	204 mb.	265 mb.
$T_c = \text{Temp. at}$ ,,	211 a.	_	215 a.	223 a.	217 a.	220 a.	219 a.	225 a.	220 a.	214 a.	211 a.	210 a.	216 a.
P ₉ (Pressure at 9 km.)	298 mb.		298 mb.	293 mb.	299 mb.	299 mb.	296 mb.	292 mb.	291 mb.	303 mb.	306 mb.	300 mb.	293 mb.
$P_s$ (Pressure at M.S.L.)	1002 mb.	980 mb.	1007 mb.	1016 mb.	1019 mb.	1015 mb.	1009 mb.	1005 mb.	1016 mb.	1021 mb.	1017 mb.	1006 mb.	1005 mb.
$T_m$ (Mean Temp. 1 to 9 km.).	252 a.		251 a.	246 a.	249 a.	251 a.	249 a.	247 a.	244 a.	251 a.	254 a.	252 a.	248 a.

NOTES. 495.

- No. Strong cold wind at surface low cloud developing. Pronounced inversion at 0.70 km. of about 5 degrees. Ci-Cu moving from WSW. Sky overcast. Pressure Distribution. Large deep Low South of Iceland, nearly stationary. 422.
- Quiescent region behind a "V" shaped depression. Traces of a small inversion near the ground. Weather "bc."

  Pressure Distribution. Large deep Low South of Iceland. A "V" shaped secondary passed over the Midlands about 8 hours previously.
- Inversion near the ground. Isothermal patch from 1.0 to 1.3 kms. at temp. 273. Cirrus moving slowly from West. Weather "bc."

  Pressure Distribution. Large Low off Ireland. Secondary over Holland moving East. Quiescent region between in which the sounding was made. 425.
- 426.
- Inversion of about 4 degrees near the ground. Another at 2·4 km. of 1 degree. Cirrus nearly stationary. Weather "bx." Calm.

  Pressure Distribution. A Low situated WSW of Ireland, Low over the Mediterranean, High over Spain and Scandinavia. Quiescent region over France. A secondary developing off Land's End.
- Traces of an inversion below 0.5 km. Small inversion at about 3.5 km. A.Cu. from West at 9 h. Weather overcast with St. and A. St. *Pressure Distribution*. A large shallow Low over Atlantic. Small High over Spain. Small secondary over the Channel moving East. 428.
- Marked inversion near the ground. A small isothermal patch occurred below the base of the Stratosphere, Ht. 9.45 km., Temp. 223.5 a. Alto clouds nearly stationary 429. Weather overcast with alto and lower clouds.

Pressure Distribution. Large shallow Low West of Ireland. Quiescent region over France.

- Marked inversion below o 3 km. Small but definite inversion at 4.6 km. of about 1 degree. Weather "b."

  Pressure Distribution. Large shallow Low WNW of Ireland. Region of indefinite gradients around the Straits of Dover and South East England.
- Traces of an inversion near the ground. Weather "bc." Pressure Distribution. Large shallow Low SW of Iceland. Small Low over the Irish Sea.
- Weather overcast, with low clouds.
  - Pressure Distribution. High to the North of Scotland, Low over Germany.
- Traces of a small inversion near the ground. Small isothermal patch at 2·3 km. Small inversion at 3·3 km. Weather "cz" with St. and Cu. clouds. Pressure Distribution. High over Scandinavia, Low to the South West of Iceland. 433
- Marked inversion at 4.3 km. Brief slackening of temperature gradient at 6.7 km. Weather "oz" with St. and Cu. clouds. Shower soon after ascent. Pressure Distribution. High over Scandinavia, Low over Iceland. Indefinite gradients over the Bay of Biscay.
- Inversion near ground on descent. Small inversion at 4·3 km., trace of a smaller one at 5·1 km. Weather "c," with A.Cu. and St. Cu. clouds.

  Pressure Distribution. A shallow low region covering the West of England, Ireland and Channel developing into a more pronounced Low over the mouth of the 435.
- 436. Small inversions on descent at 0.9 km. and 1.5 km. Weather overcast with slight rain and a sheet of Stratus at about 1 km. Pressure Distribution. A Low off Ireland slowly moving East. Small Low over France producing an Easterly gradient over Benson.

#### UPPER AIR TEMPERATURES.

#### SOUNDINGS WITH REGISTERING BALLOONS, 1923.

Lat. 51° 37′ N.

Long. 1° 7′ W.

Height above M.S.L. 57 metres.

494. T = Temperature in Degrees absolute above 200a. Benson. P =Pressure in millibars. H = Height in kilometres above M.S.L.

· No.	437•	438.	439.	447.	<b>44</b> 8.	449.	450.	451.	454.*	456.	458.	466.†
Date.	April 24.	Мау 3.	May 24.	July 5.	July 6.	Aug. 4.	Aug. 6.	Aug. 7.	Sept. 14.	Sept. 27.	Sept. 28.	Dec. 11.
Start G.M.T $H_t = \text{Greatest Height}$	18 h. o8 m. 9·7 km.	17 h. 47 m. 12·2 km.	14 h. 40 m. 5·5 km.	18 h. 27 m. 18·0 km.	16 h. 52 m. 17·9 km.	15 h. 46 m. 15·8 km.	7 h. 19 m. 9·7 km.	7 h. 20 m. 14·9 km.	15 h. 00 m. 14·2 km.	18 h. o8 m. 6·6 km.	17 h. 58 m. 16·2 km.	15 h. 43 m. 4·2 km.
$T_t =  ext{Corresponding Temp.}$	217 a.	210 a.	256 a.	223 a.	219 a.	219 a.	225 a.	228 a.	224 a.	257 a.	210 a.	263 a.
$P_t =  ext{Corresponding Pressure}$	271 mb.	193 mb.	509 mb.	79 mb.	81 mb.	114 mb.	281 mb.	131 mb.	133 mb.	450 mb.	103 mb.	605 mb.
Place of Fall	Horsham, Sussex.	South Godstone, Surrey.	Woking- ham, Berks.	Preston, Hitchin, Herts.	Stewkley, Leighton Buzzard.	Millhill, Middle- sex.	Gerrard's Cross, Bucks.	Great Saling, Braintree, Essex.	Hexham, Northum- berland.	Bulphan, Essex.	Newchurch Romney Marsh, Kent.	Barnes, Middlesex.
Distance	81 km.	90 km.	28 km.	65 km.	41 km.	58 km.	38 km.	ioi km.	185 km.	100 km.	154 km.	6 km.
Bearing	139°	120°	142°	60°	36°	88°	95°	74°	18°	100°	114°	8o°
Geostrophic Wind— Time G.M.T	18h.	18 h.	13 h.	18 h.	18 h.	18 h.	7 h.	7 h.	13 h.	18 h.	18 h.	18 h.
Speed	5 m/s.	8 m/s.	<5 m/s.	6 m/s.	10 m/s.	5 m/s.	4 m/s.	8 m/s.	7 m/s.	8 m/s.	5 m/s.	8 m/s.
Deg. from N	225°	225°	indefinite	180°	135°	200°	285°	260°	250°	240°	300°	215°
Wind (Anemometer)— Speed	ı.o m/s.	6·0 m/s.	1.5 m/s.	ı.o m/s.	6·5 m/s.	3.5 m/s.	2·5 m/s.	2·5 m/s.	_	5.0 m/s.	2·5 m/s.	ı·o m/s.
Deg. from N	295°	190°	330°	135°	110°	210°	285°	220°	-	220°	270°	170°
Type of Tropopause		I.		I.	III.	ı.		ı.	ı.		r.	
$H_c$ = Height of ,,		11·98 km.		12·09 km.	11·39 km.	12·08 km.		12·29 km.	9·67 km.		13·52 km.	
$P_c = \text{Pressure at}$ ,	<u></u>	199 mb.		201 mb.	225 mb.	205 mb.		195 mb.	268 mb.		161 mb.	
$T_c = \text{Temp. at}$ ,		209 a.	_	213 a.	221 a.	217 a.		219 a.	219 a.		206 a.	
$P_9$ = Pressure at 9 km	301 mb.	316 mb.		322 mb.	322 mb.	326 mb.	314 mb.	321 mb.	297 mb.	_	325 mb.	
$P_s$ (Pressure at M.S.L.)	1018 mb.	1018 mb.	1022 mb.	1020 mb.	1019 mb.	1024 mb.	1019 mb.	1017 mb.	1000 mb.	1025 mb.	1027 mb.	1027 mb.
$T_m$ (Mean Temp. 1 to 9km.)	251 a.	261 a.		265 a.	265 a.	267 a.	260 a.	265 a.	252 a.		266 a.	

^{*} Ascent from Liverpool—lat, 53° 24' N.; long. 2° 58' W.

#### 495.

447.

No. Inversion at about 2·2 km. Isothermal patch from 2·8-3·2 km. Very small lapse rate between 2·2 and 4·4 km. Weather "cz" with A. Cu. not lower than 2·5 km. 437. Pressure Distribution. A Low South of Iceland, travelling East. Region of indefinite gradients over the Channel.

NOTES.

438.

Inversion on descent at something below 0.35 km. Weather "b" with Cirrus and A. Cu. moving from WNW.

Pressure Distribution. Several Highs to the South East, South West, and West of the Southern part of England. Low over Iceland.

Inversion at 2·25 km. A lapse rate of temperature of 13·5 degrees per km. was found on the ascent between 0·3 and 0·7 km. Weather "be" with Cu. clouds nearly 439. stationary Pressure Distribution. A High over Atlantic, Low over the Faroes moving South East. Gradient over Southern England somewhat indefinite.

Small inversion near the ground. Traces of another small one at 1.6 km. Weather "b" with A. Cu. moving very slowly from South West.

Pressure Distribution. High over Baltic, a Low West of Spain. Very small and indefinite gradients over British Isles.

Traces of an inversion near the ground. Small inversion at about 1.2 km. Weather "b" with Ci. St.

Pressure Distribution. High over Baltic, a Low South West of Ireland. Slight gradients over the British Isles.

- Inversion at 1.6 km. Isothermal patch 2.24 to 2.66 km. Weather "b." Very little wind in lower layers, with A. Cu. and Ci. Cu. nearly stationary. Pressure Distribution. A High over South East England and Belgium. A Low West of Ireland moving North East.
- Isothermal patches 1.85-2.10 km. and 2.64-2.97 km. Weather "b." Cirrus moving slowly from West. Pressure Distribution. Region of slight indefinite gradients. A Low South of Iceland.

451. Isothermal patch 1.85-2.21 km. Well marked inversion of about 1 degree at 4.7 km. Weather cloudy. St. Cu. sheet at about 2 km. St. Cu. and A.Cu. moving from West South West.

Pressure Distribution. A Low South of Iceland, quiescent region over France.

Isothermal patch 1.22 to 1.70 km. Small inversion at 3.9 km. 454.

Pressure Distribution. A Low off the Hebrides moving North East.

- Inversion of 3 degrees near the ground. Another of 2 degrees at 0.9 km. with an isothermal patch above it from 1.2 to 1.8 km. Weather overcast, with low Stratus. Pressure Distribution. A Low South of Iceland. A High over Germany. 456.
- Several small inversions and isothermal patches between 1 and 4 km. Weather overcast, with low Stratus at about 0.3 km.

Pressure Distribution. Extensive Anticyclone centered over Eastern France and including the South of England in its central area.

466. Inversion at 1.3 km. with steady rise of temperature to 2 km. Weather "om."

Pressure Distribution. Deep depression over Iceland, High over France and Germany.

[†] Ascent from Kew-lat. 51° 28' N.; long. 0° 19' W.

#### SOUNDINGS WITH REGISTERING BALLOONS. BENSON, 1923.

T= Temperature in Degrees Absolute. P= Pressure in millibars. H= Height in kilometres above M.S.L.

No.	422.	424.	425.	426.	428.	429.	430.	431.	432.	433.	434.	435.
Date.	Feb. 6.	Feb. 8.	Feb. 9.	Feb. 12.	Feb. 14.	Feb. 15.	Feb. 16.	Feb. 17.	Mar. 8.	April 2.	April 3.	April 4.
Start (G.M.T.)	10.42	16.23	16.43	7.12	7.23	7.13	7.21	7.24	17.33	17.55	17 57	18.06

#### HEIGHTS AND TEMPERATURES CORRESPONDING WITH ISOBARIC SURFACES. 496. Benson.

1923.

Pressure	Н.	Т.	Н.	T.	Н.	Т.	H.	T.	Н.	T.	Н.	T.	Н.	T.	Н.	<i>T</i> .	Н.	Т.	Н.	<i>T</i> .	Н.	T.	Н.	T.
Millibars.	km.	a.	km.	a.	km.	a.	km.	a.	km.	a.	km.	a.	km.	a.	km.	a.	km.	a.	km.	a.	km.	a.	km.	a.
100									16.08	23	•••		•••	•••				•••		0	60			10
200					11.2	17	•••		11.58	21	···		<u>_</u>	• • • •	11:51	26	11.40	20	11.63	18	11.69	11	11.56	
300	8.96	23			8.94	23	8.86	22	8.99	23	8.99	26	8.90	23	8.84	25	8 · 80	21	9.06	21	9.11	26	9.00	26
400	7.03	38	6.75	36	7.00	39	6.96	30	7.05	36	7.05	36	6.97	36	6.90	36	6.91	31	7.14	36	7.14	42	7.03	39
500	5.43	52	5.17	49	5.40	50	5.42	43	5.48	46	5.47	49	5.40	48	5.33	44	5.38	4 ^I	5.56	49	5.23	54	5.44	51
600	4.07	59	3.84	55	4.04	57	4.10	54	4.14	57	4.12	58	4.05	54	4.01	52	4.07	51	4.21	57	4.17	56	4.09	56
700	2.88	68	2.67	62	2.88	64	2.93	63	2.97	62	2.94	64	3.90	61	2.85	60	2.92	59	3.04	65	3.00	64	2.92	64
800	1.82	76	1.63	69	1.84	69	1.90	66	1.93	69	1.90	69	1.86	68	1.82	67	1.90	65	1.99	71	1.95	71	1.87	73
1	0.86	75	0.70	75	0.01	74	0.97	73	0.99	73	0.96	7.4	0.92	75	0.89	74	0.97	72	1.04	79	1.00	79	0.95	79
900			,			/	0.13	7.5	0.14	1	0.12		0.07	,	l ´		0.14		0.18		0.13			
1000	•••	•••	•••		l		• 13		1				- /		1						`	i		

#### PRESSURES AND TEMPERATURES AT GIVEN HEIGHTS.

1923.

497. B	enson.				-	PRE	SSURE	S A	ND TI	MP.	ERAIU	KES	Al	31 V E	LN HE	IGH	15.						194	, <b>J.</b>
Height.	P.	T.	P.	T.	P.	T.	P.	T.	P.	T.	<i>P</i> .	T.	P.	T.	P.	Т.	P.	T.	P. ,	T.	· P.	T.	Р.	T.
Kilometres.	mb.	a.	mb.	a.	mb.	a.	mb.	a.	mb.	a.	mb.	a.	mb.	a.	mb.	a.	mb.	a.	mb.	a.	mb.	a.	mb.	a.
18.0								1												• • • •		• • • •	•••	
17.0				<b> </b>															• • • •	• • • •	•••		•••	•••
16.0									101	23									•••	• • • •	• • • •		•••	
15.0									118	23			•••	•••		•••			•••		•••		•••	***
T.1.0					<b>.</b>		<b>l</b>		138	23	İ	l											•••	
14.0	•••				159	22	l		161	23											163	13	•••	
13.0	• • • •				185	19	l	<b> </b>	187	22									189	19	190	11	•••	
11.0	217	11			217	14		<b> </b>	219	20			•••		216	27	213	21	221	16	223	13	219	12
10.0	255	15			255	15			256	17	257	22	•••		251	26	249	21	259	15	262	19	257	18
100												26	206	00	202	0.5	291	21	303	21	306	26	300	26
9.0	298	23		•••	298	23	293	23	299	23	299	26	296	22	292	25		25	352	29	354	35	348	34
8.0	347	30	333	27	346	30	342	25	348	29	348	31	344	29	340	29	340 395	30	408	37	409	43	402	39
7.0	402	38	386	34	400	39	398	30	403	36	403	37	399	35	394 455	35 40	457	35	470	46	469	50	463	47
6.0	462	47	446	4 I	461	47	460	37	465	43	464	46   52	459 528	43 51	524	47	527	44	540	52	537	57	531	54
5.0	529	53	512	50	528	53	530	46	534	50	533	32	320	5.	3-4	47	3-7	77	34-	] ]-	337	١,٠	33	"
4.0	606	50	587	55	604	57	607	55	611	58	609	59	604	54	602	52	606	52	617	59	614	57	607	57
4·0 3·0	689	59 67	671	60	689	63	694	63	697	62	695	63	690	61	686	59	693	59	704	65	700	64	692	63
2.5	734	71	716	63	735	65	740	63	744	66	74 ^I	67	736	64	733	63	740	61	750	69	746	67	738	68
2.0	781	75	763	67	784	69	789	66	793	69	790	69	786	67	782	66	789	64	799	71	795	71	787	72
1.5	831	77	813	69	835	71	841	68	844	71	842	71	837	71	834	69	841	68	.850	74	846	7.5	₋ 837	75
		'					0.6		0		906	ا ـ ا	807	_	887	72	896	7.	905	78	900	79	891	79
1.0	885	77	866	73	889	73 78	896	73	899	73	896	74	891	74		73		71	962	78 82	956	19	946	79 82
0.5	941		922	77	946		955		957		954	77	949 1002	77	945 998	77	955 1008	78	1014	85	1000	85	999	86
G.L	995	77	973	79	999	79	1009	72	1011	77	1007	74	1002	74	990	10	1000	'	1 1 1 4	3	1 2009	-3	999	
		1 1		1	i	i i		1	I	į.		1	ı	; 1		1	l	1		1	<u> </u>		·	

Note.—The temperatures are derived from the original tabulations which are generally made to the nearest half-degree and are shown to the nearest whole degree.

LAPSE	RATE	OF	TEMPERATURE	BETWEEN	GIVEN	HEIGHIS.

498. Be	nson.				Degrees a	bsolute per l	kilometre.					1923.
Kilometres.		1 1	<u> </u>	1	1	1	1		1		1	
17 to 18	•••					]	•••		•••	•••	•••	•••
10 to 17	•••			1			•••		•••	•••		•••
15 to 16	•••		.).		-o·5		•••		•••	•••	1	•••
14 to 15	•••				0.0		•••			•••	•••	•…
13 to 14	•••				0.5		•••	•••		•••		
12 to 13			-3.0		-1.0						-1.2	•••
11 to 12	•••	<b>i</b>	<i>-</i> 5·0		-2.0		•••			-2.5	1.2	6·0
10 to 11	3.2		1.0		-3.5			-0.5	0.0	-o·5	7.0	8.0
9 to 10	7.5	,	7.5		6.5	4.0		1.0	-o·5	6· <b>o</b>	6.5	8.0
8 to 9	7·5		7.5	2.5	6.5	4.5	7.0	3.2	4.2	7.5	9.0	
7 to 8	8.0	6.5	9.0	5.0	6.5	6.5	6.5	6.2	5·0	8.0	8∙0	5·0 8·o
6 to 7	9.0		7.5	7.5	7.0	9.0	7.5	5·0	5.0	.o	7.0	
5 to 6	6.5	7·5 8·5	$6\cdot 5$	8.5	7.0	6·o	8·o	6.5	9.0	6.0	7.5	7.0
4 to 5	6.0	5.0	4.0	9.0	8·o	6.5	.3.0	5.2	8.0	7.0	0.0	2.5
3 to 4	7.5	5.0	6∙0	7.5	4.0	4.5	6.5	7.0	7.0	6.5	6.5	7.0
2.5 to 3.0	8.0	6.0	5.0	1.0	8·o	8.0	7.0	8.0	5.0	6.0	6.0	9·0 8·0
2.0 to 2.5	8.0	7.0	ĕ.o	6∙o	6.0	4.0	6.0	6.0	5.0	4.0	8.0	6.0
1.5 to 2.0	4.0	6.0	6.0	4.0	4.0	4.0	7.0	7.0	8∙0	7.0	8∙0	
1.5 to 2.5	-1.0	7.0	4.0	10.0	3.0	6∙0	7.0	7.0	7.0	8.0	9.0	7.0
0.5 to 1.0		8.0	9.0	1	٦ -	6·o	7.0	8∙0	7.0	8·o	6.0	7.0
0.2 10 1.0	7 1.0	1	1 7 .	> 1.0	} 5·o	1 7.0	8.0	2:0	16 /	7.0	1 1	9.0

5.5 2.0 5.0 -7.0 -8.0 -2.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7

T=Temperature in Degrees Absolute.

P=Pressure in millibars.

H=Height in kilometres above M.S.L.

																<del></del>										
No.	436	5.	437	,.	438	3.	439		447	7.	448	3.	449		450	).	451		454	1.	45	56.	45	3.	466.	
Date.	Apri	il 6.	April	24.	May	3.	May	24.	July	y 5·	July	6.	Aug.	4.	Aug.	6.	Aug.	7.	Sept.	14.	Sept.	27.	Sept.	28.	Dec. 1	1.
Start (G.M.T.)	17.4	13	18.	8	17.	¥7	14.4	.0	18.2	7	16.5	2	15.4	6	7.1	19	7.2	:0	15.0	)	18	·8	17.5	8	15.43	3
400 0	,		·					· · · · ·		DEC	CODE	DCD.				100	D. DIG	CII	DEACE	<del>-</del>	,.				1001	
	enson.	1	1	1	<u> </u>		<u> </u>	1	<u> </u>	1	CORR	1			<u> </u>			i			İ	1 1		<i>"</i> ]	1923	
Pressure. Millibars.	H.	<i>T</i> .	H, km.	a.	H.	a.	H. km.	a.	H.	T. a.	H.	T. a.	H. km.	a.	H.	a.	H.	T. a.	H. km.	a.	H.	a.	H.	т. а.	km.	a.
100 200 300	 8·85	 19	 9·02	22	 11·95 9·36	 9 29			16·51 12·12 9·50	19 13 32	16·57 12·15 9·50	18 19 31	 12·24 9·58	 17 35	 9·31	28	 12·13 9·47	 19 34	 11·57 8·94	24 23			 12·19 9·55	 13 33		
400 500	6·95 5·39	34 47	7·09 5·49	38 51	7·36 5·72	45 57			7·48 5·81	49 61	7·48 5·83	47 61	7·53 5·85	51 63	7·33 5·70	44 56	7·43 5·75	50 63	7·00 5·40	39 51	 5·84		7:5 ² 5:8 ₄	51 62		
600 700 800	4·04 2·87 1·82	57 65 71	4·13 2·95 1·92	59 63 65	4.33 3.11 5.03	66 73 81	4·24 3·05 2·00	61 68 69	4.41 3.19 2.08	67 77 86	4·42 3·19 2·08	69 78 87	4.43 3.19 2.08	71 78 83	4·31 3·09	66 75	4·34 3·11	69 77 82	4·04 2·86 1·80	60 66	4.43 3.19 2.08	71 78 87	4.42 3.19	72 79 83	3.08	 69 74
900	0.89	75	1.00	74	1.02	88	1.06 0.19	78 	1.09	91	1.08 0.19	93	1.11	87 95	1.04 0.10	79 82 	1.03 0.12	86 	0·86 0·00	73 75 	I·10 0·21	88	1·11 0·23	85 89	1.07	73 79
497. B		•		1		חסם	ECCIII	) TCC	AND	TEN	IPERA	THE	DEC AT	·	VEN	111214	CHTC		liaa.l	•					192	2
		_T				<u>-</u> -				ı 1									<u>-</u>	"	P.	T.	P.	T.	P.	T.
Heights. Kilometres.	P. mb.	a.	P. mb.	a.	mb.	т. а.	P. mb.	a.	P. mb.	a.	P. mb.	a.	P. mb.	a.	P. mb.	a.	P. mb.	a.	P. mb.	a.	mb.	a.	mb.	a.	mb.	a.
18·0 17·0 16·0							 		79 93 109	19 19	 93 109	 19 18					•••				 		107	 10	•••	
15.0			•••						127 148	18	128 149	18	129	18				23	 138	24			126 149	8		
13.0 12.0 11.0	•••		•••		 198 233	 9 15			174 204 239	17 13 19	175 205 239	18 19 21	177 207 243	17 17 23	•••		175 204 238	21 19 22	161 188 219	25 25 24			175 206 241	8 15 21		
0.0 10.0	250 293	18	301	21	272 316	23 31			278 322	27 36	278 322	27 35	282 326	31 40	 314	30	²⁷⁷ 321	29 39	255 297	20			281 325	29		
8·0 7·0 6·0	34 ² 397 459	25 34 42	350 405 466	30 39 47	366 420 482	41 48 55	····		37 ² 4 ² 7 488	45 53 59	372 427 489	43 51 60	375 429 490	48 55 61	363 418 480	38 47 54	369 424 484	45 53 61	346 400 460	31 39 47	  490	 61	374 429 490	47 55 61		
5·0 4·0	527 604	50 57	534 611	55 59	626	61 67	543 619	58 63	556 632	65 71	557 632	71	558 633	68 75 80	548 624	60 69	551 625	67 71	527 603	53 60	558 633	67 74	557 632	73	621	64
3·0 2·5 2·0	688 734 782	63 67 70	743	65	755	73 77 81	705 751 800	68 70 69	716 760 807	79 83 87	716 760 808	79 84 88	716 760 808	80 82 83	708 753 800	75 77 79	709 753 801	77 81 82	687 732 780	65 67 71	716 761 808	80 84 87	716 761 809	79 80 83	707 753 801	69 72 74
1.0	833 887	71	844 900	69 73	8 <b>53</b> 906	85 89	851 906	74 78	857 909	87 92	857 908	90 95	858 911	83 88	850 904	81	850 903	8 ₄ 86	831 885	73 75	858 910	89	859 912	83 86	853 908	73 73
0.5 G.L	944 998	77 79	957 1010	78 80	961	93 93	963 1015	83 86	963 1014	97 99	962 1013	99 	967 1018	93 97	961 1012	 87	959 1010	89 89	941	79	966 1018	89 88	968 1020	89 91	966 1026	78 81
	Note	-The	tempera	atures	are der	ived	from the	e orig	inal tab	ulatio	ons which	are g	generally	made	to the	neare	st half-de	egree	and are s	shown	to the	neares	st whole	degre	<b>).</b>	
498. B	enson.				L	APS	E RA	TE (	OF TI		ERATU Degr <b>e</b> e						HEIGI	HTS-	-contin	ued.					192	23.
Kilometres.	1			•	 	•	ļ	•	-2.5			· · · · · · · · · · · · · · · · · · ·			<u> </u>				<u> </u>							
16 to 17 15 to 16 14 to 15		•		•		•			0.0 -0.3	5	0.0 -1.0	·	-0·5							•		٠.	- 2 · · - 2 · ·	) )		.
13 to 14 12 to 13 11 to 12		•				•		•	-0.5 -5.6	5	-1·0 1·0 2·5	1	-1.0 -0.5 6.5			1	-2·0 -1·5 2·5	,	0.5	5			6· 7·	5		•
10 to 11 9 to 10 8 to 9	 2·0 7·0		٠.		8.6	5	٠٠ ا		8·6 9·6 8·	) )	5·5 8·0 8·0	•	7·5 9·5 8·0	i	 8·c		7·0 9·5 6·5	;	-4·0 3·0 7·5	)		••	7· 9·	O		
7 to 8 6 to 7	9·0 8·0	) )	8· 8·	5·5 8.5 8.6 8.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5 7·5 8.5 7·0						) )	8·0 9·0 6·0	,	7·0 6·5 6·5	; ;	9·0 7·0 6·0	)	8·5 7·5 6·5	; ;	9·6 7·5	) 5		••	7· 6· 7·	5 5		•
5 to 6 4 to 5 3 to 4	8·6 7·3	5	3.0	) )	6.0	) )	4 · . 5 · .	5 5	5 · . 5 · . 8 · .	5 5	5·5 8·c	<b>,</b>	7·0 5·0	)	8 · 5	5	4·0 5·5	) ;	7·0	) 5	7· 6·	5 o	5·	o o	5·5	5
2.5 to 3.0 2.0 to 2.5 1.5 to 2.0	7.0 6.0 2.0	Э	S34   55   550   61   543						7.0	0	9·0 8·0 4·0	) )	4·0 2·0 1·0	)	2·0 5·0 3·0	)	7·0 3·0 4·0	)	5·0 8·0 4·0	)	8· 7· 2·	0 0	7· 0·	0	5·0 4·0	0
1.0 to 1.5 0.5 to 1.0 Surface 0.5	5·6	0	10.0	0	6·6 8·6	)	9·6	0	10.0	О	9·0 8·0	)	0.0 10.0	)	\right\} 5.5		4·0 5·0 2·0	) )	3·0	)	-4· 6· -4·	o	5· 5·	О	9·0 7·0	0
		_			<u> </u>		<u> </u>		<u> </u>		<u> </u>		<u> </u>		<u> </u>		1		<u> </u>		<u> </u>		<u> </u>		<u> </u>	

Note.—The lapse rates are derived from the original tabulations which are generally made to the nearest half-degree.